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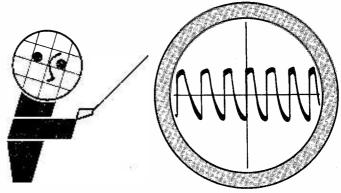
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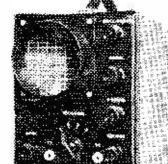
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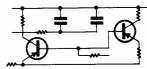
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VOL. 49 NO. 1 ISSUE 795 MAY 1973

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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SUBSCRIPTIONS

Subscription Rates for one year to any part of the world £2.65 including postage. Enquiries to Subscription Department, IPC Magazines Ltd., Carlton House, 68 Gt. Queen Street, London, WC2 5DD. Phone 01-242 4477 Binders and indexes can be supplied by the Binders Dept. at the same address.

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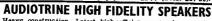
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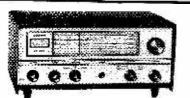
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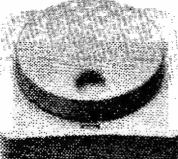
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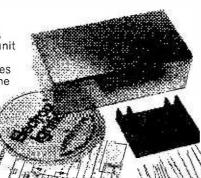
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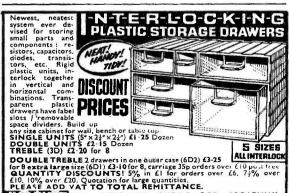
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Capacity µF							70	7p
1.0						79	.,	70
2.2					70	,,	7n	Źρ
4.7				7p		7p	7p 7p	7p
10			70	- 2	7p	7p	7p	7p
22 47 100			7p 7p 7p	70		7p	70	8p
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220	70	7p	7p	8p	90	100	17p	26p
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2200	14 ₀	16p	22p	25p	36p	40p		
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Code	Power	Tolerance	Range
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c c	1/8W	5%	4·7 Ω-470K Ω
	1/4W	10%	4·7 Ω-10M Ω
C	1/2W	5%	4-7 Ω-10M Ω
C	1W	10%	4·7 Ω-10M Ω
MO	1/2W	2%	10 Ω-1M Ω
WW	1W	$10\% \pm 1/20 \Omega$	0-22 Ω-3-9 Ω
ww	3W	5.9/	1 Ω-10 Κ Ω
ww	7W	5%	1 O~10K O

C—carbon film, high stability, low noise.
MO—metal oxide, Electrosil TR5, ultra low noise.
WW—wire wound, Plessey.

Values: E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades.

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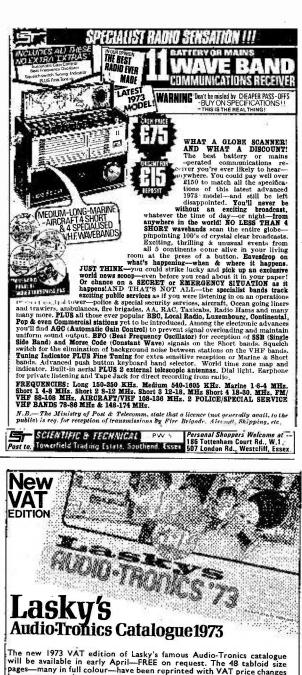
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METROSOUND ST60	77.00	50.95
PIONEER SA500A	51·81	98 · 95 35 · 95
SA600A	105 · 03 139 · 21	65·95 99·95
SA800 SA1000 QL600A Quadraphonic	171 - 40	107.95
QL600A Quadraphonic Convertor	130.83	93.95
QD 210 Quadraphonic	47.14	32 - 95
QA 800A Quadraphonic QA 800A Quadraphonic QC800A Pre-amp. QM800A Pow. amp. Reverberation 202w RANK ROTEL 210. RANK ROTEL 310. RANK ROTEL 310. RANK ROTEL RA 310. RANK ROTEL RA 310. RANK ROTEL RA 210. ROGERS Ravensbourne Ravensbourne (cased) Ravensbrook (kased) Ravensbrook (kased) SINCLAIR 2000	Sp Pric	e 159 · 95
QM800A Pre-amp QM800A Pow. amp	Sp. Pric	e 114 95 e 135 95
Reverberation 202w	60 · 45 38 · 39	43·50 28·50
RANK ROTEL 310	57·20	39 - 95
RANK ROTEL RA 810	116.05	83 50
RANK ROTEL RA 1210 ROGERS Ravensbourne	141 · 90 77 · 00	101 · 95 59 · 50
Rayensbourne (cased)	82.50	64 95
Ravensbrook (cased) Mk. II	63 - 25	48 - 50
SINCLAIR 2000	38·50 49·50	27·75 34·95
PROJECT 605 SOLARVOX 20. 10 watts RMS per	32 - 95	23 · 75
channel	43 - 95	26 95
channel	51 - 65	35 - 95
channel SOLARVOX MA801 2 x 8 watts RMS plus MATRIX 4 channel SOLARVOX MA813 2 x 18 watts plus MATRIX 4 channel TANDREG TA300	42.30	29.75
SOLARVOX MA813 2 x 18 watts	FC - FO	
TANDBERG TA300	56 · 52 76 · 89	42·95 59·95
TANDBERG TA300 TANDBERG TA300M WHARFEDALE Linton amplifier. Amplifiers listed all take both ceran	87·45 71·50	72·50 50·95
Amplifiers listed all take both ceran cartridges.	nic and m	agnetic
TUNERS AKAI AT550 AM/FM/MPX/FET AKAI AT550 AM/FM/MPX/MOS. FET AMSTRAD Multiplex 300 FM ARMSTRONG M8 Decoder *DULCI FMT 7 FM JVC Nivico MCT V5E/VT500 AM/FM LEAK Delta FM	84 10	61 95
AMSTRAD Multiplex 300 FM	131 · 09	96·95 26·95
ARMSTRONG M8 Decoder	10 - 45	7 75
JVC Nivico MCT V5E/VT500 AM/F	M 80.96	14·90 62·95
MCT V7E AM/FM LEAK Delta FM	115·25 74·43	94 · 95 52 · 95
LEAK Delta FM LEAK Delta FM LEAK Delta AM/FM METROSOUND FMS 20	83 · 79 51 · 70	62 25
PHILIPS RH 690	45 66	36 95 33 50
METROSOUND FMS 20. PHILIPS RH 690. PHILIPS RH 621. PIONEER TX500A AM/FM. PIONEER TX600 AM/FM. RANK ROTEL 320. ROGERS Ravensbourne in Teak Cas Ravensbourk (asset)	102 · 61 72 · 47	78 · 80 48 · 95
PIONEER TX600 AM/FM	100 - 35	68 · 95 39 · 95
RANK ROTEL 620	87-86	62 · 95
Ravensbrook (cased)		44 · 95 34 · 95
SINCLAIR 2000	42·44 42·44	28 · 95 28 · 95
Project 60 Tuner (stereo)	23 - 57	16 - 95
All Tuners listed are complete w Decoder except where starred.	ITN MPX	Stereo
TUNER/AMPLIFIERS		
AKAI CR80T AM/FM Tuner Ampli- fier with built in Eight Track Tape	140 70	
RecorderAKAI AA8030	140 · 78 131 · 09	84 · 95 96 · 95
AKAI AA8080AKAI AS8100S Ouadranhonic	178 07 243 85	131 · 95 181 · 95
Recorder AKAI AA8030. AKAI AA8080. AKAI AS8100S Quadraphonic AKAI AA8500 AKAI 6300	235-97	166-95
AREN A 2600	130 31 104 62	74 · 95 55 · 95 7 · 75
ARMSTRONG M8 Decoder ARMSTRONG 525	10·45 84·96	66 · 50
ARENA 2800 ARENA 2800 ARMSTRONG M8 Decoder ARMSTRONG 525 ARMSTRONG 526 GOODMANS Module 80, 35w. RMS Module 80 Compact	96.81	74 - 95
module of Compact	100 10	66 · 95 119 · 95
Module 90	112 · 04	85 · 95
100W, RIVIS	130-86	99-95
GOODMANS Module 110, Compact	230.65	175.95

These prices are effective April 1st, 1973 and are calculated assuming a V.A.T. rate of 10%. Should the V.A.T. rate differ, please check prices before ordering.

Rec. Retail Comet

THE POST OF THE PARTY OF THE PA	Price	Price
TUNERS/AMPLIFIERS—continue	d £ p 149⋅93	£ p 124⋅95
JVC Nivico 4MM 1000 Quadraphonic JVC Nivico VR 550/5501 AM/FM.	93 - 68	75.95
VR 5521L AM/FM and SEA	164 - 74	135-95
4VR 5414 Quadraphonic	211 82	176 95
KYOTO 1000 AM/FM Tuner/Ampli-	211.02	110.33
fler with built in Stereo Cassette		
Recorder. Complete with two	79 - 90	E7.05
speakers and two microphones	163 - 83	57·95 123·95
PHILIPS RH 720	202 · 41	154-95
PIONEER SX525	134 86	92.95
	184 - 72	126-95
SX626	222 - 39	152 95
SX727 SX828	285 21	196.95
	216.81	150 - 95
QX 4000 Quadraphonic QX 8000 Quadraphonic ROTEL RX 150A	274 - 69	190 95
POTEL BY 450A	65 - 68	47 - 95
POTEL BYSON A	84-10	61 - 95
ROTEL RX200A	101 - 12	74.95
ROTEL RX 400A	140 · 01	103-95
ROTEL RX 600A	178.07	131-95
ROTEL RX 800A	121 68	89.95
COLABYOV TAM 440E 0 " E etc.	121.00	09.93
ROTEL RX 154A Quadraphonic SOLARVOX TAM 1105 2 x 5 watts RMS AM/FM Multiplex comp.		
with 2 speakers and featuring		
Matrix 4 channel	36 · 28	28 - 95
Matrix 4 channel	99.79	83.95
TANDBERG TR1000 FM MPX (teak)	146 86	124 - 95
	159 09	133 - 95
TANDBERG TR1010 AM/FM MPX	118 06	64 95
TELETON CR55TELETON R8000 AM/FM	39.74	20 95
WHARFEDALE LINTON WE40	107-66	81 95
All Tunor/Amplifore listed take man	107.00	
All Tuner/Amplifiers listed take mag	netic car	triuges
except Teleton R8000 and Kyoto 1 ceramic only. All include MPX Stere	OUU WIIIG	lar with
ceramic only. An include WFA Stere	o mecon	iel with
the everation of Assessment values		
the exception of Armstrong where	M8 dec	oder is
extra.	M8 dec	oder is
extra.	M8 dec	oder is
extra.	12·65	10·50
extra.	12 · 65 31 · 02	10·50 24·95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2	12 · 65 31 · 02 39 · 16	10·50 24·95 32·25
TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP5 M II	12 · 65 31 · 02 39 · 16 15 · 25	10 · 50 24 · 95 32 · 25 9 · 75
TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP5 M II	12.65 31.02 39.16 15.25 12.85	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50
TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP5 M II	12.65 31.02 39.16 15.25 12.85 18.78	10·50 24·95 32·25 9·75 9·50 12·95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD SL55B	12.65 31.02 39.16 15.25 12.85 18.78 46.40	10·50 24·95 32·25 9·75 9·50 12·95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD SL55B	12.65 31.02 39.16 15.25 12.85 18.78 46.40	10.50 24.95 32.25 9.75 9.50 12.95 30.60 27.50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD 401 GARRARD SL56B GARRARD 401 GARRARD SL75B	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73	10.50 24.95 32.25 9.75 9.50 12.95 30.60 27.50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD 401 GARRARD SL56B GARRARD 401 GARRARD SL75B	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD 401 GARRARD SL56B GARRARD 401 GARRARD SL75B	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57	10 · 50 24 · 95 32 · 25 9 · 75 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD 50 GARRARD 401 GARRARD SL72B GARRARD SL72B GARRARD SL72B GARRARD AP76	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD 54B GARRA	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44	10 · 50 24 · 95 32 · 25 9 · 75 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25 34 · 25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SL65B GARRARD SL65B GARRARD SL65B GARRARD SL65B GARRARD SL72B GARRARD SL72B GARRARD SL72B GARRARD AP76 GARRARD ZE70 100A GARRARD ZE70 100S GOLDRING G101P/C	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25 34 · 25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SL65B GARRARD SL65B GARRARD SL65B GARRARD SL65B GARRARD SL72B GARRARD SL72B GARRARD SL72B GARRARD AP76 GARRARD ZE70 100A GARRARD ZE70 100S GOLDRING G101P/C	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 12 · 85 14 · 40 40 · 40 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70	10·50 24·95 32·25 9·50 12·95 30·60 27·50 26·95 37·25 19·50 20·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SL65B GARRARD SL65B GARRARD SL65B GARRARD SL65B GARRARD SL72B GARRARD SL72B GARRARD SL72B GARRARD AP76 GARRARD ZE70 100A GARRARD ZE70 100S GOLDRING G101P/C	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 12 · 85 14 · 40 40 · 43 30 · 73 26 · 82 25 · 57 47 · 44 28 · 05 29 · 07 38 · 61	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25 16·95 37·25 34·25 19·50 20·25 26·50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD 545B GARRARD 55B GARRAR	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25 34·25 34·25 20·25 20·25 20·25 20·25 20·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD 545B GARRARD 55B GARRAR	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 39 · 60 39 · 60 48 · 84	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·59 20·25 31 31·25 31·25 31·25 31·25 31·25 31·25 31·25 31·25 31·25 31·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 5455B GOLDRING 6155B GOLDRIN	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25 34·25 34·25 20·25 20·25 20·25 20·25 20·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SP25 MK.	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61 48 · 84 48 · 84 48 · 84 48 · 84 48 · 84	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25 37 · 25 26 · 50 33 · 55 5 · 50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD 5155B GOLDRING 6155B GOLDRING 6155B GOLDRING 6155B GOLDRING 6155B JVC Nivico SRP 473 Quadraphonic, including niinth and cover	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61 48 · 84 48 · 84 48 · 84 48 · 84 48 · 84	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25 37 · 25 26 · 50 33 · 55 5 · 50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 51958 GOLDRING G1759	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 18 · 78 · 46 · 40 · 43 · 30 · 73 · 30 · 73 · 47 · 44 · 28 · 05 · 29 · 70 · 38 · 61 · 39 · 60 · 48 · 25 · 50 · 65 · 07 · 65 · 88 · 13 · 98 · 31 · 9	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 20 · 25 34 · 25 34 · 25 19 · 50 20 · 26 · 50 26 · 50 33 · 50 55 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5455B GARRARD 5456B GARRARD 5	12 · 65 31 · 02 39 · 16 15 · 25 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 29 · 70 38 · 61 39 · 60 48 · 84 82 · 50 65 · 07 65 · 88 13 · 96 17 · 71	10 · 50 24 · 95 32 · 25 9 · 750 12 · 95 30 · 60 27 · 50 20 · 25 31 · 25 31 · 25 26 · 50 33 · 50 49 · 95 9 · 25 9 · 25 9 · 25 9 · 25 26 · 50 49 · 95 9 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SP25 Mc. II GARRARD SP25	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 12 · 85 · 13 · 78 · 46 · 40 · 43 · 30 · 73 · 30 · 73 · 30 · 73 · 30 · 73 · 36 · 82 · 51 · 57 · 44 · 28 · 05 · 29 · 70 · 38 · 61 · 39 · 60 · 48 · 84 · 82 · 50 · 65 · 07 · 65 · 88 · 13 · 96 · 17 · 71 · 19 · 40 · 19 · 71 · 71 · 71 · 71 · 71 · 71 · 71	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25 19 · 50 26 · 50 33 · 50 55 · 50 49 · 95 52 · 95 52 · 50 52 · 50 52 · 50 52 · 50 53 · 50 54 · 50 55 · 50 56 · 50 57 · 50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SP25 Mk. II GARRARD SP25 Mc. II GARRARD SP25	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 12 · 85 · 13 · 78 · 46 · 40 · 43 · 30 · 73 · 30 · 73 · 30 · 73 · 30 · 73 · 36 · 82 · 51 · 57 · 44 · 28 · 05 · 29 · 70 · 38 · 61 · 39 · 60 · 48 · 84 · 82 · 50 · 65 · 07 · 65 · 88 · 13 · 96 · 17 · 71 · 19 · 40 · 19 · 71 · 71 · 71 · 71 · 71 · 71 · 71	10 · 50 · 50 · 50 · 50 · 50 · 50 · 50 ·
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SP25 Mk.	12 · 65 · 31 · 02 · 39 · 165 · 12 · 85 · 12 · 85 · 12 · 85 · 12 · 85 · 14 · 74 · 40 · 43 · 30 · 73 · 26 · 82 · 50 · 65 · 88 · 17 · 74 · 94 · 64 · 82 · 50 · 65 · 76 · 76 · 77 · 74 · 74 · 74 · 74 · 74	10 · 59 · 59 · 50 · 50 · 50 · 50 · 50 · 5
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5L95B GARRA	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 12 · 85 · 12 · 85 · 14 · 44 · 40 · 40 · 40 · 40 · 40 · 40	10 · 50 · 50 · 50 · 50 · 50 · 50 · 50 ·
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5L95B GARRA	12 · 65 · 31 · 02 · 39 · 16 · 18 · 18 · 18 · 18 · 18 · 18 · 18	10 · 59 · 24 · 955 · 32 · 255 · 30 · 60 · 25 · 37 · 37 · 37 · 37 · 37 · 37 · 37 · 3
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5L95B GARRA	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 12 · 85 · 12 · 85 · 14 · 44 · 40 · 40 · 40 · 40 · 40 · 40	10 · 50 · 50 · 50 · 50 · 50 · 50 · 50 ·
TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD SL958 GARRARD SL95	12 · 65 31 · 02 39 · 16 10 28 39 · 16 10 28 39 · 16 12 · 85 12	10 50 24 95 32 25 9 50 12 95 30 60 27 50 27 50 27 50 37 25 26 50 33 50 49 95 52 95 12 25 12 25 12 25 12 55 77 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD 5155B GOLDRING 6175C GOLDRING 6175C GOLDRING 6175B GOLDRING	12 · 65 · 31 · 02 · 39 · 16 · 18 · 18 · 18 · 18 · 18 · 18 · 18	10 · 59 · 24 · 955 · 32 · 255 · 30 · 60 · 25 · 37 · 37 · 37 · 37 · 37 · 37 · 37 · 3
TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD SL95B GARRARD ZE0 100A	12 · 65 · 31 · 02 · 39 · 16 · 16 · 17 · 17 · 17 · 17 · 17 · 17	10 - 50 24 - 95 32 - 25 9 - 75 9 - 75 9 - 75 9 - 75 20 - 27 20 - 25 26 - 50 27 - 25 26 - 50 33 - 50 55 - 50 49 - 95 52 - 95 53 - 95 54 - 95 55 - 95 55 - 95 56 - 95 57 - 95 57 - 95 57 - 95 59 - 95 50
tne exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5L95B GOLDRING 6L12P GOLDRING 6L12P GOLDRING 6L12P GOLDRING 6L13B GOLDRING 6L13B JYC Nivico SRP 473 Quadraphonic, including plinth and cover McDONALD MP80 McDONALD MP80 McDONALD MP80 McDONALD 5L95B M	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 18 · 78 · 46 · 40 · 43 · 30 · 73 · 26 · 82 · 51 · 57 · 47 · 44 · 28 · 05 · 51 · 57 · 47 · 44 · 28 · 05 · 65 · 08 · 13 · 96 · 17 · 19 · 49 · 64 · 95 · 77 · 70 · 10 · 00 · 00 · 116 · 05 · 65 · 04	10 - 50 24 - 95 32 - 25 9 - 75 9 - 75 9 - 75 12 - 95 30 - 60 27 - 59 20 - 25 26 - 50 37 - 25 34 - 25 34 - 25 39 - 50 39 - 50 30 - 50 3
THE exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 5455B	12 · 65 · 31 · 02 · 39 · 16 · 16 · 17 · 17 · 17 · 17 · 17 · 17	10 - 50 24 - 95 32 - 25 9 - 75 9 - 75 9 - 75 9 - 75 20 - 27 20 - 25 26 - 50 27 - 25 26 - 50 33 - 50 55 - 50 49 - 95 52 - 95 53 - 95 54 - 95 55 - 95 55 - 95 56 - 95 57 - 95 57 - 95 57 - 95 59 - 95 50

The following Turntables are complete with base, plinth, plastic cover and cartridge. Fully wired and ready for use. All at special prices.

GARRARD SP25 Mk. III with Goldring G800 Special Price 17-75 Special Price 17-75 Special Price 17-25 Special Price 18-25 Special Price 18-25 Special Price 18-25 Special Price 24-25 Special Price 24-25 Special Price 24-25 Special Price 25-95 Special Price 26-95 Special Price 12-10 Special Price 12-10 Special Price 12-10 Special Price 12-10 Special Price 13-25 Speci

	16 48		
	Rec.	Retail Price	Comet Price
SPEAKERS		£D	£n
AKAI SW 155 AMSTRAD ACQUST	A 1500 (nair)	70·95 44·00	50 · 95 25 · 95
AKAI SW 155 AMSTRAD ACOUST AMSTRAD ACOUST AMSTRAD 138 (pair)	A 2500 (pair)	55.00	32 95
	Teak :	28 · 60 175 · 45	15 · 50 125 · 95
Band M/ DMO		65-89	46 95
B and W DM4 B and W D5 (pair) CELESTION COUNTY		46·75 55·99	35·95 41·95
CELESTION COUNTY	(pair)	46 · 13	34·50 37·95
Ditton 120 (pair) Ditton 15 Ditton 25		52·80 35·20	25·50 51·50
Ditton 25		71·50 59·40	51 - 50
Ditton 44 Ditton 66 FERROGRAPH S1 inc		108-90	42 · 95 78 · 75 75 · 95
FERROGRAPH S1 inc	stand	104 · 50 46 · 33	75·95 34·95
GOODMANS Minister Havant (pair)		53 · 77 72 · 19	38 - 50
Magister Double Maxim (pair		72 · 19 63 · 45	46 · 75 45 · 95
Mezzo 3 Magnum K2	,	39 · 27	26 95
Magnum K2 Goodwood		50·82 60·50	34 · 95 41 · 95
Dimension 8 DIN 20 NT Kit (pair		79 - 68	54 - 95
DIN 20 NT Kit (pair KELETRON KS4 (pair)	22 · 95 22 · 66	16 · 50 14 · 50
KS6 (pair) r) r)	28 - 16	17 · 95
KS8 (pair)		36·30 46·86	23 · 50 30 · 50
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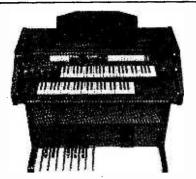
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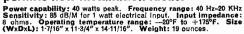
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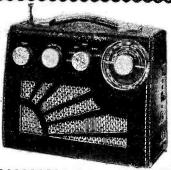
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100 0 28	0.37	0.52	0.52	0.55	0.64	0.70	1.54
200 0 . 39	0.41	0.54	0.54	0 63	0.67	0.83	1.76
400 0 . 48	0.52	0.62	0.62	0.74	0.83	1.03	1.93
600 0.59	0.63	0.75	0.75	0.85	1.07	1.38	_
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100	0.04	0.07	0.06	0.15	0.18	0.26	0.83
200	0.06	0.10	0.07	0.16	0.22	$0 \cdot 27$	1.10
400	0.07	0.15	0.08	0.22	0.30	0.41	1.38
600	0.08	0.18	0.11	0.26	0.38	0.50	2.05
800	0.11	0.19	0.12	0.28	0.41	0.61	2.20
1000	0.12	0.28	0.16	0.33	0.51	0.70	2.75
1200		0.37	-	0.42	0.63	0.83	_

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Anode voltage (Vdc)	170min	175min	5	
Cathode Current (mA)	2.3	14	8	All indicators
Numerical Height (mm)	16	13	9	point. All side
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Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality made until neorporates no less than eight elilion planar transistors, two of these are specially selected low noise NOV derives for use in the input star. no ress unan eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages. Three switched stereo lopuls, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable base and treble controls.

SPECIFICATION Frequency Response Harmonic Distortion

Inputs: 1. Tape Head
2. Radio, Tuner
3. Magnetic P.U.

All input voltages are for an output of 250mV. Tape and P.U. inputs equalised to RIAA curve within \pm 1dB. from 20Hz to 20KHz.

Bass Control Treble Control

Treple Uontrol
Filters: Rumble (High Pass)
Scratch (Low Pass)
Signal/Noise Ratio
Input overload
Supply
Dimensions

 $\begin{array}{l} 20 \, \text{Hz} \, - \, 20 \, \text{K} \, \text{Hz} \, \pm \, 1 \, \text{dB} \\ \text{better than } 0 \cdot 1 \, \% \\ 1 \cdot 25 \, \, \text{mV} \, \, \text{into } 50 \, \text{K} \, \Omega \\ 35 \, \, \text{mV into } 50 \, \text{K} \, \Omega \\ 1 \cdot 5 \, \, \text{mV into } 50 \, \text{K} \, \Omega \end{array}$ ± 15dB at 20Hz ± 15dB at 20KHz ± 15dB at 20KHz 100Hz 8KHz

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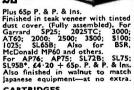
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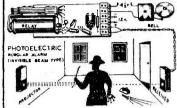
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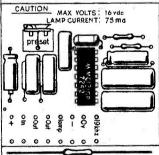
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The 15 watt miniature model CCN.
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Test voltage 4000v. A.C.
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It's the RT-VC system that screws together to save you pounds! Unisound comprises two superb speakers and an amplifier/record deck plinth—all beautifully finished in simulated teak. The stereo amplifier (4 web) for changing to 8 ohms) is based on the famous Mullard Unilex system brought up-to-date by RTVC using integrated circuits. Turntable is the proven Garrard 2025TC complete with stereo cartridge and tinted acrylic cover. Speakers are big EMI Turn-cone units all ready for mounting in their elegant cabinets, which simply need screwing and glueing together. Easy step-by-step instructions. £26-12 complete plus £1-40 packing + £1-40 post. Diamond Stylus £1-25 extra. Stereo headshones with adaptor £4 extra. Send for leaflet. Stereo headphones with adaptor £4 extra. Send for leaflet.

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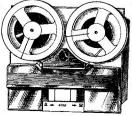
50 WATT AMPLIFIER. Output Power: 45 watts points 30Hz and 18KHz. Total Distortion: less than 2% at rated output.

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Suitable 3 speed tape deck, less heads. Caters up to 7ins. spools. Unused but store soiled hence no warranty. nlus £1p&p



WHY did you buy this copy of *Practical Wireless?* Were you influenced by advanced publicity or advertising: are you a regular reader with a devotion to follow our activities month by month; or are you one of many thousands who pick up this magazine to seek guidance on what makes radio and electronics tick? It has been said that people read Practical Wireless to learn something about the subject. After all, it is a technical field that demands some education and understanding and it is really this aspect that makes most people read.

To supplement professional career requirements there is a growing band of people who are bank clerks, clergymen, accountants, businessmen, as well as students and technicians who are seeking part time courses on the practical side of radio and electronics. Some colleges are able to offer facilities, subject to minimum class size, but we have heard of cases where they cannot find enough qualified engineers who are willing to spend extra time in the evenings to instruct these students. It is a pity because it often means that a course has to be dropped because of

So we come back to magazines; Practical Wireless is used in schools and colleges to a great extent because it provides an excellent support service to instructors, many of whom cannot always find sufficient time in addition to their everyday jobs to make full preparation for classes. Practical Wireless is a leader because its articles and designs are "down-to-earth" and, in spite of competition from elsewhere, we still offer the greatest constructional project support to instructors, technicians and engineers, while encouraging the confidence of newcomers.

This month we have rubber-stamped this policy by giving you for the first time a unique supplement containing eight extra straightforward constructional projects for the home, attractively presented with abundant illustrations and a full colour cover picture. To make it easier for you to find this supplement and worthwhile to keep for reference, we have printed it on a pleasant shade of "apple-green" coloured paper-another first for Practical Wireless.

Don't let this divert your curiosity too far from our other usual features because you will also find much more to interest you in this issue. For the benefit of quick and easy reference you will also find our contents list just inside the front cover, together with information on many aspects of our service. And watch out for next month's issue too for more special attractions, some of which are mentioned in this issue.

M. A. COLWELL-Editor

The June issue, on sale May 4th, will include a new easy competition to win a Digital Multimeter, a special feature on what to look for when buying Hi-Fi Equipment, and "Special Valves in Electronics", plus the usual abundance of constructional projects.

Further details on page 48.

B.R.C. change their name

RITISH Radio Corporation Limited announced on the 1st April that it has changed its name to Thorn Consumer Electronics Limited. It continues to manufacture and market audio and TV products under the Ferguson, HMV, Ultra and Marconiphone brands and remains wholly-owned subsidiary of Thorn Electrical Industries Ltd.

VAT

To the best of our knowledge, the prices quoted in this issue were correct at the

time of going to press.
As from April 1st, 1973, there is no purchase tax but a large number of goods carry Value Added Tax.

The "N.F.A.C."

THE National Federation of Aerial Contractors Limited is making an attempt to "clean up" the aerial contracting industry.

The Ministry of Posts and Telecommunications listed 55,000 complaints of bad reception in their recent annual report. Out of 32 listed causes of complaints. the largest numbers were for "inefficient aerial installations" and the N.F.A.C. feels that it can help this state of affairs by alerting the consumer and all who employ aerial contractors that there are in existence a very "Rooftop large number of Racketeers".

Plans currently being considered by the Federation include random inspections of members' installations and a system whereby new companies applying for membership will have their work inspected in addition to the trade references that are already required. A special Standards Committee will hear reports of faulty workmanship.

By this system, the N.F.A.C. hopes to assist in narrowing the field of consumer complaints and possibly convince dealers that they mean to play their part in cleaning up the aerial contracting industry.

Mullard film on I.C. design

ULLARD Ltd. have announced a new 16mm colour film lasting 18 minutes. It's called The Computer-Aided Design of Integrated Circuits and is available on free loan from the Mullard Film Library, 269 Kingston Road, Merton Park, London, SW19 3NR.

The film, which was shot mainly on location at the Mullard semi-conductor plant at Southampton, describes in detail the use of the computer and its peripheral equipment in such functions as IC design and layout, mask-making and testing at every stage of production.

Tandberg in the jungle

SERGEANT J. Murtagh of the Royal Signals is seen in the picture using a Tandberg Series 11 portable tape recorder. This machine and a TP4-1 portable radio accompanied a recent British Trans-Americas expedition which took in 18,000 gruelling miles from Alaska to the tip of South America. The purpose of the journey was to survey a road through the uncrossed 300 miles of swamp and jungle bordering the Panama canal which blocks the Pan American highway system.

During the trip, the expedition kept in touch with the outside world with the TP4-1 receiver, picking up BBC news broadcasts and weather reports.

In the jungle and swamps, the electrical equipment was carried in man-packs or by ponies and although it was partially immersed in water, rolled on several times by the ponies and carried through thick mud, it continued to function without a fault.



Sgt. Murtagh of the Royal Signals.

Signals "piped" through waveguide

THE core of a system which, when fully implemented, will transmit 300,000 phone conversations or 200 colour TV signals at the same time through a waveguide "pipe" is now operating at the GEC-Marconi works at Great Baddow.

This equipment will be used by Post Office engineers in a field trial system to be installed between the Post Office Research Station at Martlesham, Suffolk and a Post Office site at Wickham Market, 15 kilometres away.

The new "pipe" is a 50mm diameter circular waveguide capable of supporting signals throughout the frequency band from about 32 to 110GHz. The photograph shows 32-50GHz channel separating filters and band-branching assembly.

Texan reprints

R EPRINTS of the "Texan" 20+20W Stereo Amplifier are available.

They may be obtained by sending 35p (30p+5p) postage/packing to "Texan" Reprint, c/o Chief Cashier, Practical Wireless Tower House, Southampton Street, London WC2E 9QX.

World Radio Club

FURTHER to the item on the World Radio Club in the March issue, we have been informed by the programme Producer that an extra broadcast in the BBC World Service will be made each week at 20.30 GMT on Thursdays.

The midday edition has now been moved to 13·30 GMT on Wednesdays. The other Friday and Sunday transmissions remain unaltered. BBC, Bush House, P.O. Box 76, Strand, London WC2B 4PH.

Some S.E.R.T. meetings

HE Society of Electronic and Radio Technicians, Faraday House, 8-10 Charing Cross Road, London, W.C.2. will be holding the following meetings:

April 11: "Test Equipment" by B. Ellison from Tektronix. Venue is The Conference Theatre, I.B.A., 70 Brompton Road, London, S.W.3 and the lecture commences at $7 \cdot 00$ p.m.

April 5: "Colour TV Forum and Exhibition". This will be held in the Byng Kendrick Suite, University of Aston, Birmingham, commencing at 7.00 p.m.

April 24: "The CVC5 Colour Receiver" by A. E. Thomas from ITT. This will be held in the Cleveland Scientific Institution, Corporation Road, Middlesborough. Meeting starts at 7.30 p.m.



HIS is a self-contained receiver which may be used over the range 115-150MHz, or 140-190MHz, according to the coil fitted. It was actually found to maintain good efficiency even up to 210MHz. A vertical telescopic aerial or improved aerial system will provide reception on the internal speaker, an outlet being present for headphones when required. An optional preamplifier is also described.

The receiver has a superregenerative detector, which is a great advantage from the point of view of simplicity. This type of detector is highly sensitive, and it should be possible to copy a signal of under $1\mu V$. There is also only one tuned circuit, so no alignment or ganging difficulties arise. The bands include the 2-metre amateur band (144-146MHz). In terms of sensitivity, most signals which can be well received with the simpler type of converter-communications receiver combination can also be received satisfactorily with this receiver.

A disadvantage sometimes encountered with this type of receiver is tricky tuning and hand-capacity

effects. These do not arise here, due to sound construction and a metal case and so actual use of the receiver is easy.

Circuit Details

Fig. 1 is the circuit, employing a junction f.e.t. in the first stage. The rod or other aerial is coupled by L1, and L2 is tuned by ∇ C1. The network R2, C4, R3 and C5 gives a suitable quench frequency and regeneration is controlled by ∇ R1. To modify the tuning range, L2 only need be changed.

A three-stage audio amplifier assembled on a separate circuit board follows. Tr2 is the first audio amplifier, Tr3 the driver, and Tr4/5 the output pair, operating a small speaker in the case. The outlet takes a jack plug for an external speaker or phones, if wanted, and VR2 is the volume or audio gain control. R12 is a small pre-set potentiometer, which allows working conditions for the output pair to be suitably adjusted.

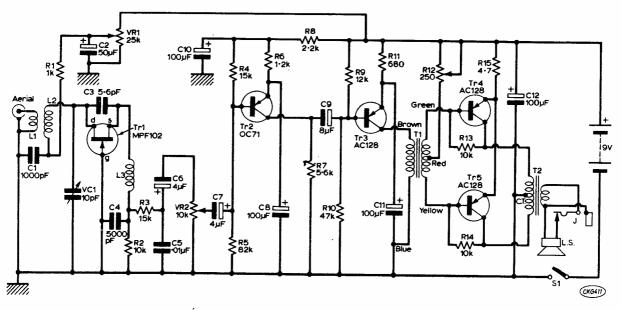


Fig. 1 : Circuit of the main receiver. The circuit of the pre-amplifier is shown in Fig. 4. The heading photograph shows the two units bolted together.

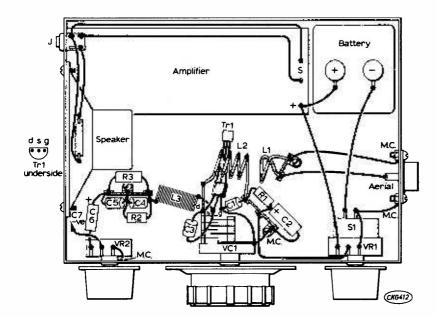


Fig. 2: Layout of the main components and audio amplifier board within the cabinet. When the preamplifier is fitted the coaxial aerial socket is removed and used on the preamplifier box.

Photograph looking into the top of the receiver which may help when locating components as in Fig. 2 above.

Cabinet Construction

Flanged universal chassis members 7×3 in form the front and back, and similar parts 5×3 in are the sides. The top and bottom are 7×5 in flat plates.

The front member is drilled for VC1, VR1 and VR2, as in Fig. 2. Also punch or drill holes for a co-axial socket on the right hand side, or for an insulated terminal or socket, if a co-axial feeder is not required here.

An opening is cut in the left member for the speaker, taking care that this will clear the amplifier and other parts. Perforated zinc or expanded metal is placed over the aperture, and the speaker is bolted on. The jack outlet is placed as shown.

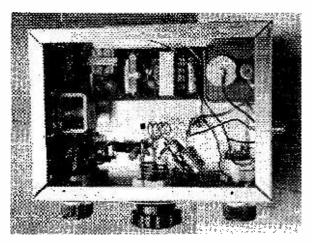
The four flanged members are then assembled by bolts through the holes present in them. Four holes are drilled in one 7 x 5in plate, these are marked through so that the flanges can be drilled to suit. The case bottom can then be attached. Two rubber feet were placed on the front bolts, to raise the front of the receiver slightly.

It is easier to assemble the receiver if the sides and back are left off until later. When all construction is finished, the top 7 x 5in flat plate is fixed with four self-tapping screws.

Detector Stage

This is wired as in Fig. 2. A 3-lead holder is used for Tr1. This avoids possible damage from heating while soldering, and also allows the transistor to be changed, if necessary. The MPF102 is listed as having a top frequency of 200MHz. Some were found to perform satisfactorily at well above this, but others, not up to specification, would only operate at relatively low frequencies.

The holder drain tag is soldered directly to the lower fixed plates pillar of VCl. The leads of C3 are cut short, and this item is soldered from the source tag, to the top pillar of VCl. A stout wire is also soldered to this pillar, projecting back about ¹2in so that L2 can be changed without unsoldering other items.



A stout lead from the gate tag goes to the moving plates contact of VC1, just clearing the moving plates. The tag strip holding R1 and C2 is raised on a long bolt, so that wires from C1 are as short as possible. A wire projects upwards about ¹₂in to take the other end of L2.

L1 is a single turn of insulated wire. Coupling can be adjusted by rotating this small tag strip slightly on its fixing bolt, but it is not very critical.

L3 is self-supporting, and is 30 turns of 26swg enamelled wire, wound on a ¹4in diameter object which is afterwards removed. Turns are closewound. One end is soldered to the tag supporting R2, C4 and R3, and the other end is soldered to the source tag of Tr1 holder.

The potentiometers and other parts can then be wired as in Fig. 2. A lead will run from VR2 under the speaker to the input pin of the audio amplifier.

Audio Amplifier

This is assembled on Veroboard 5×1^{3} 4in, as in Fig. 3. First drill two holes for the chassis bolts, position the board in the case, and mark and drill

matching holes in the metal bottom. Tags held with the bolts form earthing points, Fig. 3. The bolts are 1 ₂in long, so that extra nuts hold the assembly clear of the metal case, lock-nuts underneath securing the amplifier. A piece of card 5×1^{3} ₄in may be put between the amplifier and case bottom, though shorts to the metal will not arise if joints are kept close to the board.

Coils

These are self-supporting, wound with 18swg, 20-swg or other stout wire, with spaced turns. A coil having 4 turns, $^{1}2$ in outside diameter, and $^{7}8$ in long, was found to tune 115-150MHz. This is suitable for 2 metre reception.

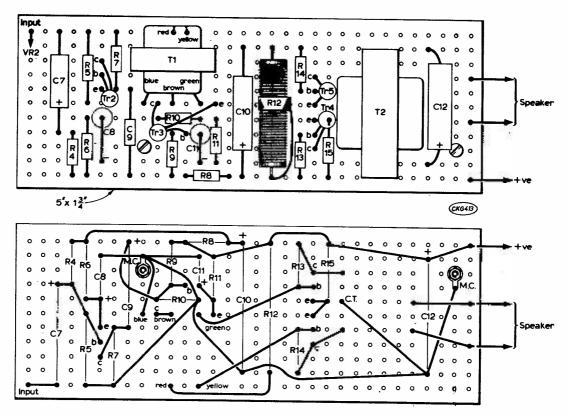


Fig. 3: Diagrams of the component layout and wiring of the audio amplifier board.

Take care to fit the electrolytic capacitors as indicated. With a unit of this kind, it is helpful to place black 1mm sleeving on the negative line leads, and red sleeving on positive leads. With another colour for other wiring, it will be easy to check connections if this should prove necessary.

The amplifier may be tested before fixing it. Place the slider of R12 at about the central position. Connect the speaker and a 9V battery, negative to one of the chassis tags. Either place a meter in one battery lead and move the slider of R12 for a current of 10mA, or adjust R12 to place just enough resistance in circuit for speech to sound normal. If R12 is at a very low value, current drawn will be small but cross-over distortion will be present.

For this test, input can be from any convenient source; a signal generator, diode tuner, pick-up, or from the first stage of the completed receiver. If VR2 is not in circuit, avoid overloading the amplifier by the test signal.

The amplifier is fitted as shown, negative return being through the metal case. Connect the speaker leads and amplifier to the jack so that the contacts which open silence the speaker, when phones or an external speaker are in use. A coil $^{1}2$ in long and $^{7}16$ in in diameter, having three turns, tuned 192-150MHz, while a similar coil having two turns allowed 216MHz to be reached.

Stray circuit capacitances and the length of connecting leads influence the frequencies tuned. The frequency can be raised by reducing the number of turns, or by stretching the coil to separate turns, or by reducing the overall diameter.

Operating notes

When VR1 is advanced, a position should be found where a strong hiss begins. This is roughly the correct setting for VR1, though it will be found that further slight adjustment may be helpful, depending on the strength of the signal tuned in.

The hiss should cease when any signal of sufficient strength is tuned in, provided VRI has not been turned too far. VR2 adjusts volume in the usual way, and can probably be advanced about half way, for the internal speaker.

If superregeneration is impossible on some part of the band, move L1 a little further from L12. This

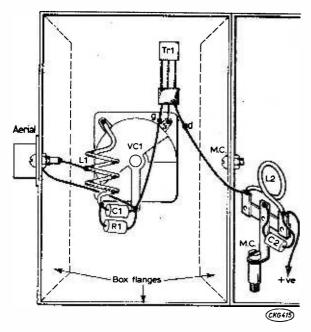


Fig. 5: Positioning of the few components within the preamplifier box.

 3×2 in and 1 2in or so thick is then placed between the flanges, and another piece of wood is placed level with this, and the whole gripped tightly in a vice. The 7×3 in member is then bent into a $3 \times 2 \times 2$ in box, with the flanges inwards. Fig. 5 shows this part from behind. The front is drilled for VC1, and one side for the co-axial or other aerial socket. Three holes are also drilled in the other side, to match up with the holes which are exposed when the co-axial socket is removed from the receiver.

The 7 x 2in piece is bent at 2in from each end, in the same manner, so will fit on to enclose the box. It is held with a number of self-tapping screws.

Pre-amplifier Wiring

The transistor holder (or transistor) is soldered directly to VC1, as in Fig. 5. All leads are as short as possible.

L1 is wound with 18 or 20swg copper wire, and is similar to the coil in the receiver, but will generally have to be stretched somewhat, or have

★ components list

R1 220 Ω ‡W, 5% C1 0.01 μ F

C2 0.01µF

VC1 10pF or similar miniature variable, or pre-set.
Tr1 MPF102 Holder optional

Universal Chassis flanged side 7x3in. (Home Radio) Aluminium 7x2in. Knob, tag-strip, etc.

The components listed above for the pre-amplifier are additional to those required for the main receiver.

about one less turn. If maximum volume is with VC1 fully open, this shows that L1 should be changed, by removing a turn, spacing turns further apart, or winding a new coil of smaller diameter.

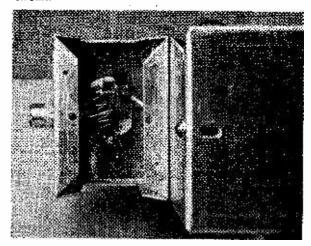
The position of the aerial tapping depends somewhat on the use of a co-axial fed dipole or similar aerial, or a short vertical rod type aerial. This tapping can usually be about one-quarter to one-third the total number of turns from the C1 (earthed) end.

Two bolts fix the r.f. stage to the side of the receiver, and a lead from Tr1 drain passes through the original aerial socket hole to L2.

Receiver Changes

The tag strip holding L2 is replaced by one having two insulated tags. A lead from one tag is run to a positive pin on the a.f. amplifier and C2 is connected from this tag to the chassis tag, as in Fig. 5. The drain lead is taken to the other tag.

L2 is one turn of insulated wire, positioned near the detector coil. Coupling is adjusted for best regeneration, by bending the loop L2 to adjust the distance to the detector coil, as with the original circuit.



Rear view of the completed pre-amplifier bolted to the receiver.

It was found that results were better with coupling in one phase. To check for this, twist L2 180°, to change its sense with relation to the detector coil.

As mentioned, L2 can be resonant over a narrow band. This increases gain, but makes it a little more troublesome to change coils or cover a wide band of frequencies. If this method is to be tried, wind L2 with one or two extra turns, compared with the detector coil, using insulated wire to avoid shorts. It is then necessary to stretch or compress L2, or change the number of turns, until it is found to peak up signals in the wanted frequency range. The resonant effect is quite flat, but these adjustments, and the degree of coupling with the detector coil, and position of the aerial tapping, can make quite a difference to reception.

Because superregenerative receivers are notorious for their radiation it is strongly recommended that the pre-amplifier be fitted as an essential part of the receiver. Complete screening, as described by the author, is very important.



FETRONS

'HE field effect transistor (FET) is currently being used in the front end of a.f. and r.f. circuits, as well as being developed into simplified forms of logic circuitry for micro-miniature applications such as wrist watches and pocket calculators. Aside from the manufacturers of such luxury items, our attention is turned here to more domestic matters such as television receivers, radio transmitters and receivers. Where thermionic valves are still being used, there is some reluctance to effect a total conversion to semiconductor techniques. We can have the best of both worlds because we can now replace valves in some circumstances with direct equivalent improved performance transistors. Particular areas of application also include unattended relay stations, and telecommunications terminals, as well as domestic receivers.

TRIODE EQUIVALENT

These transistors, called "fetrons," have emerged from the military applications stable and are being made available for other applications, although very little is generally known about the performance so far. The fetron is basically an arrangement of two n-channel field effect transistors (Fig. 1) connected to provide the equivalent working characteristics of a triode valve but with a much better frequency response at both ends of the spectrum. This is because the fetron has an extremely low channel resistance and inter-electrode capacitance. Furthermore, since there are

no heaters, operation is immediate on switch-on.

OTHER FEATURES

The life of the fetron is likely to be much greater than the thermionic valve under normal working conditions and the degradation of operational characteristics is minimal. Other important features include a higher amplification factor (almost ten times that of a valve) and a lower noise figure. Since no heaters are used, power requirements are simplified to just one high tension supply.

PENTODE CHARACTERISTIC

Both the thermionic valve and the FET are voltage controlled devices, hence design equations are virtually the same. Although the pentode an ode voltage-current characteristics are similar to the drain characteristics of the fetron, the latter are more clearly defined at the cut-off region

or "knee" and exhibit stable current drain for various drive conditions (Fig. 2).

Since the main purpose of the fetron is to act as a direct replacement for the triode valve, it is essential that it should withstand high voltages and have a matched gm. The single junction FET cannot do this, but when two specially selected FETs are cascaded the problem is overcome. It is also possible to reduce the Miller (gate to source capacitance) effect by using a low capacitance, small signal, high gm FET at the input circuit, coupled with a high voltage output FET.

With the arrangement shown in Fig. 1, the output FET acts as a voltage dropper for the input FET and the Miller effect capacitance of each is in series. The output impedance is also greater than in a valve pentode, resulting in the excellent characteristics shown in Fig. 2. Since the input gate circuit is effectively a reversed bias junction, it presents a very high resistance load to the signal source.

Fig. 3 shows the transfer characteristic of a fetron which has been made

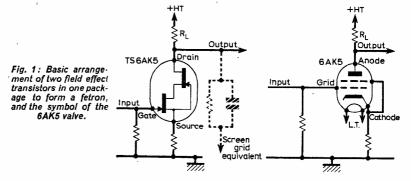


TABLE 1:

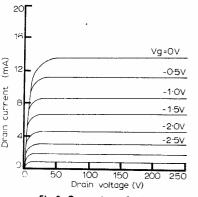
TYPICAL PENTODE DI	EVICE CHARA	CTERISTICS-
PARAMETER	6AK5	TS6AK5
Plate voltage breakdown	350V	350V
Plate resistance	$0.5M\Omega$	5·0MΩ
Transconductance	$5,000\mu$ mhos	4,500µmhos
Plate current (Rk=200Ω)	7·5mA	7:0mA
Grid voltage for lb=10µA	-8·5V	-5·0V
Amplification factor	2.500	22,500
Input capacitance	4 · 0pF	6·5pF
Output capacitance	0·02pF	0 · 02pF
Useful frequency limit	400MHz	600MHz

TABLE 2:

TYPICAL TRIODE DEVICE CHARACTERISTICS (EACH SIDE)—Rk=2-70 Ω, Eb=130V				
PARAMETER	12AT7	TS12AT7		
Plate voltage breakdown	400+V	350V		
Plate resistance	15kΩ	250kΩ		
Transconductance	4,000µmhos	3,000µmhos		
Plate current (Rk=240Ω)	5.0mA	9 · 0m A		
Grid voltage for Ib=I10µA	-7·0V	-7·0V		
Amplification factor	60	750		
Input capacitance	2 · 2pF	25pF		
Output capacitance	1.5pF	3.5pF		

up from selected FETs to approximate closely that of a particular valve (shown dotted) operating within the same limits. If special requirements include partial operation beyond this FET cut-off then clearly a more appropriate FET device must be selected for this, perhaps providing a higher current for the same control voltage. The gm or transconductance ratio of the fetron gives a true square law property with consequent harmonic distortion figures of an extremely low order. In fact, harmonics beyond second order are claimed to be negligible.

Although the simulation of the "screen grid" principle can be effected within the fetron package, the similarity of the transfer curves to those of a pentode must not be taken as an assumption that the fetron is an ideal replacement for the pentode, even though the noise figure may be lower. The fetron has a markedly improved performance over the triode due to square law operation.



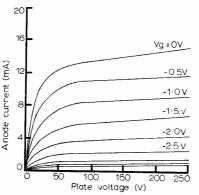
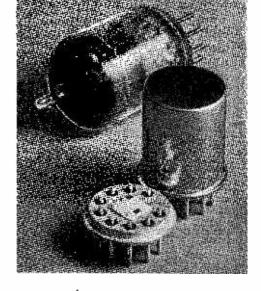
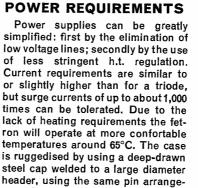


Fig. 2: Comparison of output drain characteristics with those of the 6AK5 anode.





Fetrons that have been made so far include replacements for the 6EW6, 6JC6, 6AK5 and 12AT7 but with ready made FET junctions currently available it is expected that the majority of common types can be simulated. More familiar types such as 6V6 and 6AQ5 are next on the list. The type number given to fetrons consists of the equivalent valve number but prefixed TS. Hence the

ment for connections.

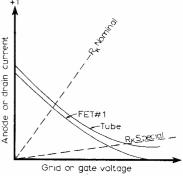


Fig. 3: Transfer characteristic of a fetron compared with a valve.

fetron for replacing the 12AT7 is TS12AT7.

The manufacturer who has announced these activities in fetrons is the American company Teledyne Semiconductors, who are selling in the U.K. via the distributors GDS Sales Ltd. of Slough. Prices are higher than for valves but this is offset by the long term performance advantages described. GDS Sales quotes £8 for the TS12AT7 and £6.50 for the TS6AK5 for orders of 1 to 99, these being the first available in the U.K. Although this price is high the long term advantages of reliability and performance are compensatory.Small orders for these devices are being handled by the subsidiary company Best Electronics (Slough) Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Bucks, SL1 3UZ.

Elsewhere in this issue we are taking a closer look at some of the valves that still have a unique role to play in radio and electronics. Look out for our special feature "Special Valves for Communications".

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31

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١.	TRA	NSI	STORS	3	2N4931 2N5172	2·70 0·08	AF116 AF117	0·25 0·20		0·10 0·10	BF271 BF272	0.2
	(4301 (4302	0·1 0·1				0.22	AF118	0·50 0·22	BC307 V	0·10 0·09	BF273 BF274	0.5 0.2
1 :	G303 G306	0.2	5 Green	0.10	2N5176	0.32	AF124	0.24	BCJ08A	0.09	BF457	0.2 0.5
1 2	CF309	0.8	Orang		2N5245 2N5190	0.92	AF126	0·20 0·19	BC309	0.10	BF458 BF459	0-8 0-5
2	G344 A G345 R	0.2	5 2N3054	0.47	2N5192	0·96 1·24	AF189	0·20 0·38	BC309B	0 10 0 10	BF821 BF821 A	2.1
2	(1371 (G374	0·18	2N3055	0.46 0.60	2N5194	1.10	AF170 AF172	0·25 0·25	BC327	0.80 0.24	BF828 BF861	0.9 0.2
	G381 G417	0·29 0·20	2N3390 2N3391	0·20	2N5195 2N5245	1·46 0·43	AF178 AF179	0·55 0·65	BC328	0·22 0·19	BFS98 BFW10	0-2 0-6
2	N109 N174	0.49	2N3391	A 0.22 0.18	2N5457	0.35	AF180 AF186	0.60	BC338	0·19 0·35	BFW11	0.6
2	N176	0.78	2N3393	0.12	2N5459	0.88 0.88	AF200	0·40 0·85	BCY31	0.40	BFW15 BFX13	0.80 0.23
2	N274 N335	0.78	2N3402	0·12 0·17	3N138	0.68 1.65	AF239 AF240	0·41 0·72	BCY32 BCY32	0·60 0·75	BFX29 BFX30	0·2
2	N351 N376	0.98 1.00	2N3404	0·19 0·24	3N140	1·86 0·92	AF279 AF280	0·54 0·54	BCY33 BCY34	0·84 0·85	BFX37 BFX44	0.86 0.86
	N384 N388 A	0.98		0·27 0·10		0.81 0.58	AFY42 AF211	0·74 0·55	BCY38 BCY39	0·40 1·05	BFX63 BFX68	2.48
	N 404 N 456	0·43 0·75	2N3415	0·10 0·15	8N143	0·75 0·92	AL102 AL103	0.75 0.70	BCY40 BCY42	0.50 0.15	BFX84 BFX85	2·48 0·30 0·24 0·28
2	N456A N457A	0.75	2N3417	0·21 1·25	3N158	0·81 0·84	ASY26 ASY27	0·80 0·86	BCY43	0·15 0·21	BFX86	0.24
2	N491 N584	8.25	2N8571	1.12	3N 159	1.17	ASY28	0.28	BCY58 BCY59	0.22	BFX87 BFX88	0.20
2	N591	0·26 0·84 0·15	2N3572 2N3702	0 97 0 10	3N187 3N200	1·80 2·49	ASY29 ASY50	0.80 0.20	BCY66 BCY67 BCY70	0·66 0·94	BFX89 BFY10	0-46 0-86
2	N696 N697	0.15	2N3704	0·10 0·14	3N201	1 05	A8¥55 A8Z21	0-85 0-55	BCY71	0·17 0·22	BFY11 BFY17	0·46 0·96 0·26
2	N698 N699	0.25	2N3705 2N3706	0·10 0·09	40050 40251	0·78 0·81	AU103 BC107	1·25 0·14	BCY72 BCY87	0·18 3·47	BFY18 BFY19	0-28 0-28
2 2	N706 N706 A	0·10 0·12	2N3707 2N3708	0.10	40309	0.88	BC108 BC109	0·18 0·14	BCYSS	2.40 0.80	BFY20 BFY29	0.50 0.40
2	N708 N7 0 9	0·18 0·88	2N3709 2N3710	0.09 0.12	40310 40313	0 50 0 92	BC118 BC114	0·18 0·12	BCY89 BCZ10 BCZ11	0.85 0.50	BFY37 BFY41	0.20
2	N711 N718	0.80 0.21	2N3711	0.80	40316 40318	0.50 0.92 0.92	BC115 BC116	0·15 0·15	BD115	0.75	BFY43 BFY50	0.62
2	N718A	0.80	2N3712 2N3718	0.95 1.08	40322 40360	0·92 0·46	BC116A	0.18	BD116 BD121	0.75 0.75	BFY51	0-48 0-69 0-16 0-18 0-16
2	N720 N721	0.50 0.55	2N3714 2N3715	1·15 1·28	40361 40362	0·48 0·50	BC117 BC118	0·21 0·11	BD123 BD124	0·82 0·67	VFY52 BFY53	0.10
2	N914 N916	0·22 0·17	2N3716 2N3773	1·80 2·35	43063 40389	0.88	BC119 BC121	0.27 0.23 0.29	BD130 BD131	0·57 0·40	BFY56 BFY64	0·84 0·41
2	N918 N919	0.80 0.20	2N3774 2N3775	8·38 4·19	40394	0·46 0·56	BC123 BC125	0.15	BD132 BD135	0·50 0 48	BFY75 BFY76	0.40
	N929 N930	0·14 0·14	2N3776 2N3777	5·95 4·84	40395 40406	0-50 0-44 0-88	BC126 BC132	0·20 0·80	BD136 BD137	0·49 0·55	BFY77 BFY78	0.22 0.24 0.86
2)	N1090 N1091	0.28	2N3778 2N3779	2·25 3·15	40407 40408	0.50	BC134 BC135	0·11 0·11	BD138 BD139	0·63 0·71	BFY90 BRY39	0.80
21	N1131 N1132	0.20 0.20	2N3780 2N3781	4·50 3·67	40409 40410	0·52 0·58	BC136 BC137	0·15 0·15	BD140 BDY10	0.88 1.25	B8X19 B8X20	0·18 0·14
21	N1184	1.27	2N3782	8.37	40411 40414	2·25 8·55	BC138	0.20	BDYII	1.50	BBX21	0.20
21	N 1302 N 1303	0·16 0·16	2N3789 2N3790	1·76 2·20	40438 40467.A	1.44 0.69	BC140 BC141	0.84 0.89	BDY17 BDY18	1.50 1.75	BSX 26 BSX 27	0.84 0.84 0.25
21	N1304 N1305	0·20 0·20	2N3791 2N3792	2·06 2·20	40468 A 40600	0·44 0·69	BC142 BC143	0·24 0·21	BDY 19 BDY 20	1·97 0·92	BSX 28 BSX 29	0.25 0.47
21	N1306 N1307	0·22 0·22	2N3794 2N3819	0·10 0·37	40601 40602	0.67 0.46	BC144 BC145	0·24 0·21	BDY38 BDY60	0·65 0·90	BSX 59 BSX 60	0·47 0·68 0·78
21	N1308 N1309	0·25 0·25	2N3820 2N3823	0·47 0·62	40603 40604	0.58 0.56	BC147 BC148	0·11 0·10	BDY61 BDY62	0·85 0·75	BBX61	0.49
21 21	N1483 N1507	0.90 0.24	2N3824 2N3826	0·75 0·28	40636	1.10	BC149 BC153	0·13 0·18	BF115 BF117	0·28 0·43	BSX76 BSX77	0·15 0·20
	N1613 N1631	0·20 0·85	2N3854 2N3854A	0.16	40673 AC107	0.50 0.85 0.16	BC154 BC157	0·18 0·14	BF119 BF121	0.58 0.25	A8X78 B8W70	0·25 0·28
21	11637 11638	0.80 0.27	2N3855 2N3855A	0.16	ACI13 ACI15	0.16	BC158 BC159	0·13 0·14	BF123 BF125	0.27 0.25	BSY24 BSY25	0·20 0·15
21	(1671 (1701	1·25 1·10	2N3856	0.16	AC117 AC121	0·20 0·13	BC160 BC167B	0.37	BF127 BF152	0.27 0.20	BSY26 BSY27	0.20
21	11702 11711	2.15	2N3858	0.16	AC126 AC127	0·25 0·25	BC168B	0.13	BF153	0.29	BSY28	0·15 0·15
21	11093 12102	0·17 0·84	2N3858A 2N3859	0.16	AC128 AC141K	0·25 0·80	BC169B BC169C		BF154 BF158 BF159	0·16 0·15 0·27	BSY 38 BSY 39	0·15 0·15
21	12147	0·80 0·70	2N3859A 2N3860	0.16	AC142K AC151V	0·25 0·14	BC170	0·18 0·11	BF160	0.28	BSY51 BSY52	0·25 0·25
21	12148 12192	0.60 0.40	2N3866 2N3877	0·70 0·25	AC152V AC153	0·17 0·22	BC171 BC172	0·18 0·11	BF161 BF163	0·85 0·20	BSY53 BSY54	0·25 0·80
21	72192 A 72193	0.40 0.40	2N3877A 2N3878	1.22	ACI53R ACI54	0.25 0.20	BC182 BC182L	0·10 0·12	BF166 BF167	0·85 0·18	BSY56 BSY65	0·79 0·15
2N	72193A 72194	0·42 0·27	2N3879 2N3900	1·91 0·20	AC176 AC176K	0·18 0·20	BC183 BC183L	0.08	BF173 BF177	0·19 0·25	BSY78 BSY79	0·40 0·40
	72194A 72195	0·80 0·87	2N3900A 2N3901	0.21 0.32	AC187K	0.20	BC184 BC184L	0·11 0·11	BF178 BF179	0·25 0·80	BSY790 BSY95A	0.45
2N 2N	(2195A (2218A	0.18	2N3903 2N3904	0·20 0·17	AC188K ACY17	0.26 0.25	BC186 BC187	0·25 0·25	BF180 BF181	0.85 0.82	BU104 BU105	1·42 2·25
2N	2219 2219A	0·87 0·51	2N3905 2N3906	0.21 0.22	ACY18 ACY19	0·15 0·20	BC204 BC205	0·11 0·10	BF182 BF183	0.80 0.40	C111 D40N3	0.58 0.62
21	2220 2221	0.20 0.20	2N4036 2N4037	0.63	ACY20 ACY21	0·20 0·18	BC206 BC207	0·11 0·10	BF184 BF185	0·17 0·17	GET111 GET113	0.45 0.20
21	72221A 72222	0.33 0.31	2N4058	0.42 0.16	ACY22 ACY28	0·18 0·13 0·18	BC208 BC209	0.09 0.10	BF194 BF195	0.14	GET114	0.20
2N	2222A	0.41	2N4059 2N3059	0.09	ACY30 ACY39	0.42 0.55	BC211 BC212K	0.30	BF196	0·15 0·15	GET115 GET119	0·50 0·85
2N	2368 2369	0·11 0·89	2N4060 2N4061	0·11 0·11	ACY40 ACY41	0.17	BC212L	0·10 0·16	BF197 BF198	0·15 0·15	GET120	0.25
2N	12369 A 12646	0·17 0·50	2N4062 2N4302	0·11 0·25	ACY44 AD136V	0·17 0·81 0·96	BC214L BC236	0·23 0·16	BF199 BF200	0·18 0·85	GET535 GET536	0·20 0·20
	2647 2711	1·20 0·12	2N4303 2N4913	0.32	AD140 AD140	0.50 0.55	BC237 BC238	0.08	BF224J BF225J	0·14 0·19	GET538	0.20
2N 2N	2712 2713	0·12 0·17	2N4914 2N4915	0.80 0.87 0.95	AD142	0.20	BC239 BC251	0·09 0·20	BF257 BF238	0·22 0·22	GET873 GET880	0·12 0·80
2N	2714 2904	0.17	2N4916 2N4917	0·20 0·17	AD143 AD149V	0·45 0·66	BC252 BC253	0·20 0·18 0·28	BF244 BF245	0·16 0·33	GET883 GET887	0·20 0·20
2N	2904 A	0·18 0·25	2N4918 2N4919	0.50	AD149V AD150	1·26 0·63	BC257 BC258	0.09 0.09	BF246 BF247	0·48 0·49	GET890	0.22
	2905 2905 A	0·26 0·23	2N4920	0.58 0.60	AD161 AD162	0·87 0·87	BC259 BC261	0·13 0·20	BF254	0.14	GET895	0.25
2N	2906	0.18	2N4921 2N4922	0.50 0.55	AD161 }	PR 0.69	BC262	0.18	BF255 BF257	0·15 0·41	RETU	
	2906A 2907	0·23 0·18	2N4923 2N4926	0·80 0·80	ADZ11 ADZ12	1·50 1·75	BC263 BC300	0·23 0·42	BF258	0.46	OF	
2N	2907A	0.25	2N4927 2N4928	1·00 1·80	AF106 AF109R	0.27 0.40	BC301 BC302	0·34 0·27	BF259 BF261	0·48 0·23	POS	T
	2923 2924	0·12 0·12	2N4929 2N4930	2·23 2·25	AF114	0.25	BC303	0.54	BF264	1.45	SERVI	CE
			13p per or		AF115 urone 25:	0·24	BC304	0.43	BF270	0·25		

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8N7422	0.48	0.42	8N7450	0.20	0.18	8N7492	0.75	0.70
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IN914	7p	AA129	15p	BAY18	171p	OAS	17p
IN916	7p	AAZ13	12p	BAY31	7p	OAIG	20p
IN4007	20p	AAZ15	120	BAY38	25p	OA9	10p
1844	7p	AAZ17	10p	BY100	15p	OA47	89
18113	15p	BA100	15p	BY103	22p	OA70	79
IB120	12p	BA102	25p	BY122	47 tp	0A78	100
18121	14p	BA110	250	BY124	150	0A79	7p
18130	8b	BA114	15p	BY126	15p	OASI	8p
18131	10p	BA115	7p	BY127	17p	OA82	100
IB132	12p	BA141	17p	BY164	57p	OA90	770
18920	7p	BA142	17p	BYX10	220	OA91	7p 7p 7p
18922	8p	BA144	12p.	BYZ10	85p	OA95	70
IS923	12p	BA145	170	BYZII	32p	OA200	79
18940	5p	BA154	12p	BYZ12	80p	OA202	100
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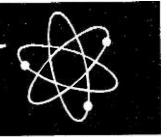
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CIRCUIT

In the basic circuit, Fig. 1, the reference voltage is determined by a zener diode ZD which controls the output voltage. Trl, a power transistor, takes a small current from the zener diode, amplifies it, and feeds the resulting current to the output circuit.

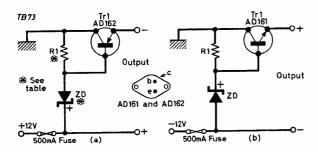


Fig. 1: Basic stabilising circuits for a) negative and (b) positive "earth".

With the output circuit left open Tr1 remains off, but as soon as a load is connected the current will increase until the voltage at the output is a little less than that of the zener diode. If for any reason the output voltage increases the voltage across Tr1's base-emitter decreases causing the collector current to drop. Conversely, if the output voltage decreases the base-emitter voltage will increase, raising the collector current. The overall effect being that the output voltage will remain constant despite varying load currents.

OVERLOAD

Although the basic circuit will work quite satisfactory, if the output leads are accidentally shorted together a heavy current will flow which may damage the transistor before the fuse can blow. To insure against this the circuit can be modified to the form shown in Fig. 2. Here, no matter what the load, even a short circuit, no more than 330mA will flow. Under normal loads the voltage across R2 will be less than the 500mV or so required to start Tr2 conducting, so the circuit will work as in Fig. 1.

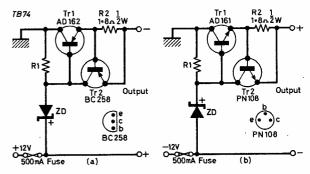


Fig. 2: Protected circuits for negative or positive "earth".

However when the current exceeds 280mA this will no longer obtain and Tr2 will start to draw current from the zener diode. At first this will have no effect, but if the voltage across R2 increases further Tr2 will draw more and more current until finally the zener will stop conducting, thus enabling the output voltage to fall to a level where no more than 330mA flows.

Output Voltage	ZD (400mW)	R1 (₺W)
6V	6·2V	680Ω
7⋅3V	7·5V	390Ω
9V	9·1V	22 0Ω

CONSTRUCTION

The unit is built into an aluminium box approx. $3\times2\times2$ in. (Type AB12) the power transistor being bolted to the box after applying silicone grease. The few components are connected directly to the pins of the power transistor. Since the quiescent current is only about 13mA no on-off switch is fitted.

BACK NUMBERS

We regret that the back numbers department of P.W. has now closed and consequently we are unable to supply these. Requests for specific back issues can usually be included in our 'CQ' section; there is no charge for this but it is a service between readers and P.W. is unable to meet any of these requests.

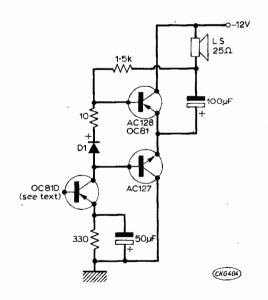
TWO VERSATILE TRANSISTOR AMPLIFIERS

As an independent service engineer one is often called on to repair car radios whose age, or foreign origin, make it difficult, if not impossible, to obtain spares. Quite often there is a burnt-out output or driver transformer which would normally result in the set involved being scrapped. To avoid this it has been possible, over a period of time, to evolve two output stages which employ no transformers or "difficult" components. The transistors used are easily obtained and cheap. In fact, one aspect of the design was to take advantage of the excomputer panels now widely on sale, which contain large numbers of suitable transistors, etc.

CIRCUIT No.1

The first design is intended to take the place of the relatively low-powered output stage used by several firms in hybrid car radios. A typical set employed two "12 volt h.t." valves and three transistors, an OC81d driving a pair of OC81's. The original OC81d is retained, but with a slightly different emitter resistor, and feeds directly into a complementary pair, AC127 and AC128.

The actual construction is so simple that it may be done on a seven-way tag strip. It will usually be possible to use the heat sinks previously fitted to the OC81's. The sole drawback, if such it be, is that the loudspeaker has to be changed to a high impedance type.

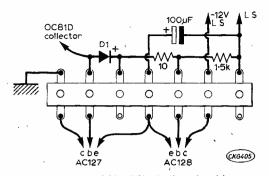


Two transistor output stage added to existing OC81D stage in receiver.

CIRCUIT No.2

It was to provide more power than the AC127/128's could give, and also to avoid having to use special loudspeakers, that the second circuit was evolved. It consists of an amplifier, a driver, and a complementary stage, which in turn drives the output transistors. In this circuit the computer panels really came into their own. Those used contained mainly

C. E. MILLER



Suggested layout of Circuit No. 1 using a tag strip.

2G302's (p.n.p.), 2N1091's (n.p.n.), OC23's (p.n.p. output) and OA10 diodes. There were also some anonymous devices which looked, and behaved, like OC81's. The alternatives for the various transistors, etc., in the design are as follows:—

Tr1. AC128, OC81, 2G302.

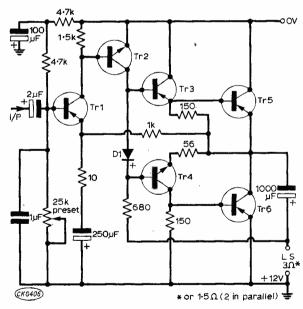
Tr2. AC127, AC176, 2N1091.

D1. AA119, OA10, AC128 with base/collector strapped.

Tr3, as Tr1.

Tr4, as Tr2.

Tr5, Tr6. AD149, OC23. (Etc.—any large output type).



Higher powered output stage of Circuit 2.

As a final construction point, the output transistors should be mounted on a piece of aluminium of some 30 sq. in. This may conveniently be shaped to act as a screen for the rest of the amplifier. The prototype was deliberately mounted in the worst possible place, in a confined space close to the vehicle heater, but no overheating has been observed.



There are 195 other good reasons for buying AMTRON electronic kits

Apart from the five items shown above, there are another 195 kits to choose from in the vast AMTRON range of electronic kits.

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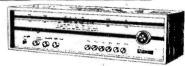
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384	-26		-65	EBC41	-49	EM87	-50	PCL84	.88	UBC41	-45
3V4	-47		-69	EBC81	.30	EY51		PCL85		UBF80	.34
5U4G	-31	30FL14	-68	EBC90	-22	EY86		PCL86		UBF89	-32
5V4G	-35	30L1	.29	EBF80	.32	EY87	-29	PCL88		UCC84	.38
bY3GT	-30		.70	EBF83	-39	EZ40	-39	PCL800		UCC85	-35
5Z4G	.35	30L17	-70	EBF89	-29	EZ4I	•39	PCL805	-38	UCF80	-30
6/30L2	.54		.54	ECC81	.17	EZ80	.21	PENA4		UCH42	-58
6AM6	.13	30P12	-69	ECC82	.20	EZ81	.22	PEN36C		UCH81	-30
6AQ5	.22	30P19	.54	ECC83	.35	EZ90		PFL200		UCL82	-32
6AT6	.20		-56	ECC85	-34	GZ30	-34	PL36		UCL83	-55
6AU6	.20	30PL13	-89	ECC804	-54	GZ32	-40	PL81		UF41	-52
6BA6	-20	30PL14	-80	ECF80	-30	KT41	.77	PL81A		UF89	-80
6BE6	-21		-45	ECF82	-26	KT61	.55	PL82		UL41	-58
6BJ6	.41		-25	ECH35	.55	KT66	.78	PL83	-38	UL84	.80
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6J7G	.24		-54	ECL82	-29	PABC8	0 -31	PY32	• 52	Z77	-22
6 K 7 G	-12		-87	ECL86	-35	PC86	-44	PY33	-52	Transist	
6K8G	-36		-28	EF39	.38	PC88	-44	PY81	.25	AC107	-17
6Q7G	.35		-22	EF41	-57	PC96	.42	PY82	-25	AC127	-18
68L7GT	.32		-36		-23	PC97	.38	P¥83	.26	AD146	-87
6SN7GT	-32	DF91	-16	EF85	-28	PC900	.29	PY88	•33	AF115	.20
6V6G	-28		-36	EF86	-30			PY800	-81	AF116	-20
6V6GT	-28		.20	EF89	-26	PCC85	.23	PY801	-31	AF117	.20
6X4	.23	DK32	-33	EF91	.13	PCC88	-38	R19	-30	AF125	-17
6X5GT	.28	DK91	-28	EF92	-27	PCC89	•43	R20	-70	AF127	.17
10P13	-53		.50	EF98	-65	PCC189	.48	U25	.73	OC26	.25
12AT7	.17	DK96	.45	EF183	-27	PCC808	.70	U26		OC44	.12
12AU7	.20	DL35	-40	EF184	-29	PCF80	-26	U47		OC45	-12
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20F2	-67	DL96	-38	EL34	-48	PCF80	.58	U78		OC75	.12
20P3	-75	DY86	-24	EL41	.54	PCF80		U191		OC81	.12
25L6GT	-19			EL84	-23			U193		OC81D	-12
25U4GT	-57	DY87	-24	EL90	-26	PCF80		U251	-61	OC82	.12
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Age cannot wither them

HERE wireless engineers foregather, talk inevitably veers toward: 'I remember...'

It is either a model with such idiosyncracies that a catalogue of 'common faults' would have called for an appendix to the service manual, a manufacturer whose crass perfidy extended to an invoice before the goods arrived —or worse, so long afterwards that one had to guess at the cost of the spares before one dared complete the repair—or a customer.

But my subject today is not so much the trials and tribulations of the working engineer as this harking back' tendency we all evince, once we converse with fellows of like mind. Go to a meeting of the RSGB, the SERT, the BARTG or even your local Gramophone Society and before the last strains of the demonstration or mutters of the lecture have died away, everybody is avidly recounting his or her personal experiences.



. , . a donkey-driven gramophone.

Watching two members of the Royal Television Society taking coffee last week reminded me of Ralph Richardson and John Gielgud in the Royal Court Theatre production of Home. Parallel tracks of reminiscence, meeting rarely at some way-station. From the few words I caught in that BBC Hospitality Room, member A was waffling on about videotape while the other had some bee in

his bonnet about phase-lock loop and pulse-code-modulation.

Henry was dying to know how Mr. B allied the two subjects, but couldn't find out because the charming production assistant he was trying to chat up with his memories of Marconi would insist on relating her opinions of Arthur Negus every time I had to pause for breath.

All this is brought on by hearing about the Fetron.

The Fetron is a genuine solid state substitute, mounted in a case like a valve, with pin formation and characteristics of the valve it is meant to replace.

You can read the ins and outs of it in the "Special Product Report" elsewhere in this issue, if it grips your curiosity like it did mine. Suffice it to say on this page that all those "everlasting" relay stations, built around valves designed to run forever, could not die without putting up a fight first.

Use of the Fetron saves major circuit modification when a valve-change is needed. Ain't science wunnerful?

Trouble is, Henry took a look at the types available and found there listed the dear old 12AT7. Now the TS12AT7 sounds a good idea until you remember some of those old 'universal' radiograms, and one or two series-heatered television sets that used them.

What happens if you plug in a Fetron? Have they made a resistive heater 'bridge', or do we have to solder a resistor across the socket? And, if we do, shouldn't there be a thermistor provided? Should we not also protect the h.t. line because the Fetron is operative immediately?

So many questions... reminds Henry of that unfortunate chap in an electronics magazine who offered a simpler way of getting over some stabiliser problems. Only snag was, somebody had to remember to turn the control back to zero after use unless the

next chap along blew the thing up—you know, the way your loudspeaker creases when you have left the amplifier gain up high and a 'friend' flicks your stylus!

Well, the upshot of this poor chap's sensible economy was that



. . . and the inevitable happened.

electronic geniuses wrote in, both calling him gormless and detailing complicated protection circuits that would automatically switch off, from any given function. I wonder if Mrs. Mary W. would like one built into every TV?

I remember one TV we could never switch 'Off' because the maker had fitted too-substantial suppressors across the contacts.

We all tend to hark back. You should see the glee with which Colin Riches unearths a donkey-driven gramophone. At the wedding of a friend's daughter, hardly out of her teens, one of the speakers, Marketing Director of a worldwide Telecommunications company, had to remind the reception that his first acquaintance with the charming Sally was when she sat in his lap—at eighteen months—and the inevitable happened.

He might, at least, have reminded them of the days when he was hawking cheap radios round the council estates. It is just as funny a story. Remind me to tell it to you, one day . . .

Special Valves

PART1 COMMUNICATION TYPES

M.K.TITMAN B. Sc(Eng), C. Eng, MIEE.

THERMIONIC devices still have a wide range of applications in modern electronic circuits and, despite the semiconductor takeover, they remain essential components in a variety of applications from high power r.f. amplifiers to electro-optical transducers.

The requirement for valves for u.h.f. and s.h.f. has led to the development of special techniques. The following valves were all developed from the necessity to exploit new ways to enable communication systems to use the wide bandwidths available at u.h.f. and microwave frequencies. The principles used are mathematically complex but their operation can be readily understood.

DISC SEAL VALVES

The form of construction used for both triode and tetrode configurations is illustrated in Fig. 1. The structure consists of a thimble-like cathode, spaced from a parallel wire grid further separated from a disc anode. The structures are very rigidly held by the ceramic space discs and because of the annular configuration co-axial input and output terminations can be used. The advantage of this system is that high power operation with reasonable efficiency in the GHz region is possible.

Disc seal triodes are used for amplifier and oscillator applications from 0.5GHz to 4GHz frequencies, at power levels of 1W to 600W. Typical values of gm are 6mA/V to 25mA/V. At lower power levels

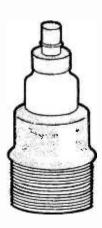
(<25W) the envelope is designed for convection cooling but forced air cooling is used for the higher power levels. Examples of this valve type are the ES157 at 2W, and TDO4-20 at 12W.

KLYSTRONS

Klystrons are also essentially microwave valves which operate as oscillators in the frequency range from u.h.f. to more than 100GHz. Generally they are available for discrete commercial frequencies such as 6, 7, 8 or 9GHz and mechanical tuning by micrometer adjustment is possible.

The klystron consists of a cavity (or for power devices, multiple cavities) through which a stream of electrons is beamed from a normal electron gun assembly, as shown in Fig. 2. The electrons are velocity modulated by a field produced by a toroidal modulating structure known as a rhumbatron. The electrons therefore become bunched in regions of high electron density and rarified in low density regions, as they travel through a further section known as the drift space. Consequently if critical frequencies are utilised the bunching allows resonant oscillation to occur in a mode controlled by the rhumbatron.

Power levels for high frequencies are in the region of 1kW with special u.h.f. power devices operating at 460 to 1000MHz at levels of 20kW. The electronic tuning range for such devices is from 30 to 100MHz,



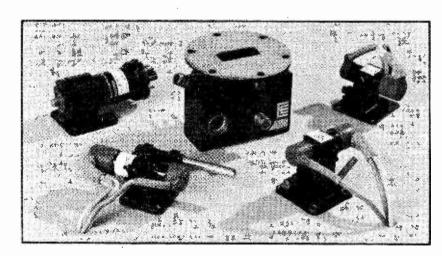


Fig. 1: at left, shows the general configuration of a disc seal valve. The picture shows a collection of oscillator klystrons, the centre one being used in communications relay equipment. The others are used in radar local oscillators.

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ACY20 20p BF196 ACY21 19p BF200	15p CR1/051C 45p OC72 35p CR1/401C 60p OC76 14p CRS3/05AF	25p 2N706 10p 7400	30P 0	·150, 0·220 5p
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AF117 25p BFY51 AF118 44p BFY52	15p LIC723C/5 £1 02 ORP12	50p 2N1303 17p 7451 40p 2N1304 24p 7453	20p S	Stock values Price each
AF124 25p BFY53	1/p L C/41C/5 45p On-01	40 p 2N1305 24 p 7454 50 p 2N1306 30 p 7460	20p 10	00pF, 150pF, 220pF, 330pF, 470pF, 560pF, 680pF, 820pF, 000pF, 1500pF, 2200pF, 3300pF, 4700pF, 5600pF, 6800pF, 3p
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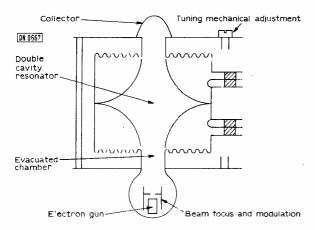


Fig. 2: Internal arrangement of a klystron valve.

whilst the mechanical range is considerably more. Typical device types are the KS6, 7, 9 family and YK1010 to 1090. Most of these utilise waveguide outputs but some have coaxial probes. The higher power devices require forced air cooling, whilst the u.h.f. power units need a cooling water supply.

TRAVELLING WAVE TUBES

These are microwave power amplifier valves used extensively in communication systems particularly for microwave links. The basic construction is shown in Fig. 3 and consists of an electron gun assembly, a modulating helix structure and a collector electrode. The electron gun forms a narrow electron beam focused by means of the grid and anode. The beam passes along the axis of an accurately formed helix structure and is continually focussed by a magnet system. The modulating microwave frequency is passed along the helix and travels at approximately the same speed as electrons in the beam. Thus the r.f. field produces an electric field which velocity modulates the electron beam as it travels along the helix axis. After modulation the electron beam bombards the collector electrode which is often water cooled.

For low power valves the helix is of wire but for power devices a ring bar structure is used. As the helix is in a long glass envelope, heat dissipation is by radiation and thus the power is limited, especially since the mechanical helix structure must be very accurate. For very high power devices a ring-bar helix system is used and is a development of the

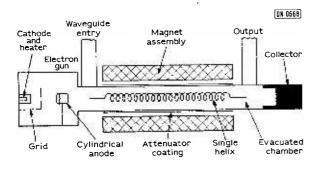


Fig. 3: Diagram to illustrate the construction of a travelling wave tube.

cross-wound opposite band helix system. Where very high power is necessary the ring bar structure is supported by annular beryllium insulators of high thermal conductivity.

Travelling wave tubes are very efficient microwave amplifiers which produce amplitude modulated output signals. The frequency range is determined by the mechanical structure and the helix in particular and, for the simple helix, it is roughly an octave about the centre frequencies from 1 to 9GHz.

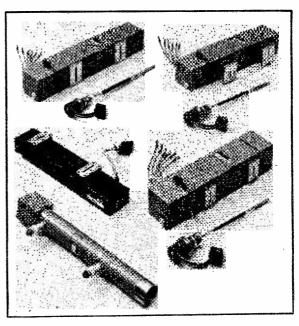
Power levels for continuous operation are usually 1 to 10W but kilowatts are possible while operation in pulsed modes can result in peak power levels in the megawatt region. The band-width at high power levels is usually reduced to as low at 10% or 400MHz at 4GHz.

Both forward and backward wound helices are used and typical gains in the X band are in the region of 30 to 40dB, with noise factors of 20 to 28dB. Generally they are designed to fit into special mountings which incorporate the permanent magnet systems. The input and output are usually taken directly from waveguide connections, with the forward wave tubes operating as amplifiers and the backward wave tubes as oscillators. Typical forward wave types are LB4-20 and 30, at 4GHz and LB6-15 to 25 at 6GHz, with backward wave oscillators like the YH1100 and BA16.

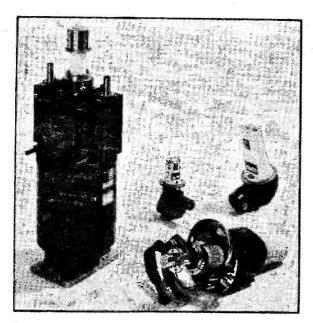
MAGNETRONS

These are essentially high efficiency oscillator valves and are used for producing fixed frequency, fixed amplitude oscillations and, in a pulsed mode, are widely used in radar equipment. The normal frequency is in the X band (5·2 to 10·9GHz) although other bands are covered.

The magnetron, as illustrated in Fig. 4, consists of one or more very carefully machined cylindrical cavities with a cathode adjacent to the cylinder and formed of a thin wire. A permanent magnet provides



A selection of travelling wave tubes used for communications in the S, C and X-bands. Three are replaceable types, shown beside their mounts.



In this collection of magnetrons the large one is an L-band 2.3MW tunable pulse magnetron intended for high power surveillance radar. In the foreground is a 25kW CW model for industrial use. The remaining two magnetrons are rated at 50kW and 900kW pulse operation in the S-band

a magnetic flux at right angles to the cylinder and thus at right angles to the electric field formed by the diode. Electrons released from the cathode travel in a circular path and at a given frequency just graze the anode. The oscillation frequency is determined by the physical characteristic of the cylinder and therefore is often fixed. Slight tuning is however provided with some magnetrons.

Continuous-wave magnetrons are available in the frequency range 8 to 9.5GHz at power levels of 6W to 20W. Typical operating conditions are Va=1kV, Ia=50mA, Vh=6·3 and Ih starting at 1A. Typical types are JPT 9-01 and JPG 8-01.

Pulsed magnetrons are designed for short pulse durations in the region 1 to 5 µs for X band devices at approximately 9GHz. Power outputs range from 25W to 50kW with devices such as JPT9-02 and YJ1050. The lower frequency 1.25GHz (L Band) and 5.5GHz (C Band) devices operate at higher power levels up to 1,000kW.

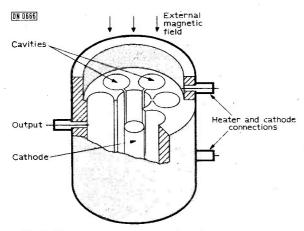


Fig. 4: General arrangement of a multiple cavity magnetron.

FUTURE TRENDS

Although trends continue towards the use of semiconductor devices, the power transmitter valve at all frequencies cannot yet be replaced directly. Thus power valves at all frequencies are still of very considerable use and development continues to improve all these designs.

A trend which undoubtedly will continue is the replacement of high power microwave transmitters by low power solid state components such as varactor chains. This has been made possible by improved receiver and aerial design.

We are indebted to the English Electric Valve Co. of Chelmsford for permission to reproduce the photographs in this article.

TO BE CONTINUED

ELEVISION

MAY ISSUE

THE LID OFF VARICAPS

What exactly is a various tuner, how does it: work and what goes wrong with it? This month Keith Cummins looks at all aspects of varicap tuners and sums up the pros and cons. Including an Insight into the tricky servicing problems that can arise with their

Transistor if Preamplifier

It is often worthwhile converting dual-standard sets to single-standard operation and fitting a modern transistor u.h.f. tuner. When this is done it is convenient to remove the v.h.f. tuner, but this usually means the needs for extra gain between the u.h.f. tuner and the l.f. strip. A simple transistor j.f. pre-amplifier that has been used in converting sets such as the BRC 850 chassis is leatured this month. this month.

ASSESSING COLOUR RECEIVER **PERFORMANCE**

'in the concluding article in his series E. Hoare provides a detailed account of how to assess the colour performance of receivers— purity and convergence etc. and the operation of the colour circuits.

SERVICE NOTEBOOK

Amongst the items in Secret Wilding Service Notebook this month is a detailed procedure for tackling that common condition; lack of e.h.t.

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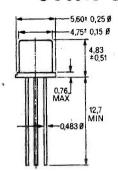
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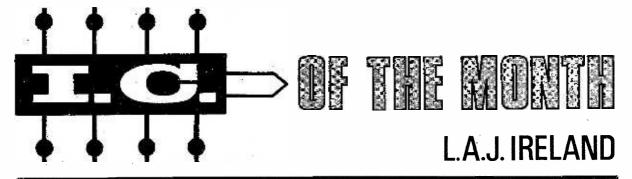
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EBF89	15p	PCL83	I5p	6BW7	12p
ECC81	12p	PCL84	15p	6U4	12p
ECC82	12p	PL82	10p	6F23	20p
EF91	5p	PL83	10p	20PI	15p
EY86	22p	PL36	17p	20P3	12p
EF183	20p	PY8I	I Op	30F5	12p
EF184	20p	PY801	l7p	30FL1	20p
		PY800	i7p		



Number 37

SGS NE555 Precision Timer

highly stable timing device, type NE555, recently released by SGS, is the topic for this month's article. It allows precision timing from microseconds to hours with a mere handful of components; its uses however are not limited solely to the timing field as it can also find wide application in such diverse spheres as pulse generation, frequency division, pulse-width modulation, etc., to mention but a few. Such versatility coupled with low cost should make it an attractive i.c. to the amateur experimenter and a few of its more interesting features and applications will be outlined in the following notes.

Applications

A block diagram of the NE555 is shown in Fig. 1 and the first application to be considered is its use as an accurate timer, Fig. 2. The timing period is set by one additional resistor capacitor network with additional terminals allowing control over the triggering and resetting of the device. The external

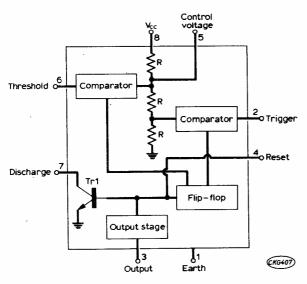


Fig. 1: Block diagram of the NE555 timing device.

capacitor connected between pin 7 and earth is initially held discharged by the short circuit path of the saturated transistor Trl. When a negative trigger pulse is applied to pin 2 the flip-flop changes state and biases off Tr1 thereby allowing C1 to charge via R1. The time constant associated with R1C1 determines the rate at which C1 charges and when its voltage reaches 2 ₃ V_{cc} the threshold comparator

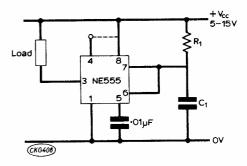


Fig. 2: Typical application of the NE555. The values of R1 and C1 for a delay of 1 second would be 1M Ω and 1 μ F.

resets the flip-flop and discharges C1 in addition to providing an output pulse at pin 3. One of the great advantages of this type of circuit is that the timing rate, for all practical purposes, is independent of the supply voltage. Timing periods from as short as 1 microsecond to as long as 1 hour may be obtained with this rather simple arrangement.

Multivibrator

Another interesting application of the NE555 is obtained when pins 2 and 6 are joined together as illustrated in Fig. 3. Here the device is operated as

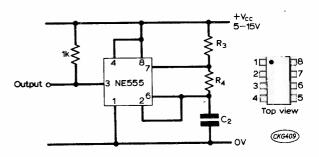


Fig. 3: In this circuit the NE555 is used as a free-running multivibrator.

a free-running multivibrator with the frequency and duty-cycle set by the R3-R4-C2 arrangement. The combined value of R3 and R4 in conjunction with C2 determines the frequency while the duty cycle is set by the ratio R3/R4. As the transistors fabricated in the silicon chip are of the highest quality excellent square waves are obtained from the output at pin 3. Once again, in this arrangement the operating frequency is independent of the power supply voltage.

Pulse-width modulator

The final application of the NE555 to be considered is its use as a pulse-width modulator. Here an external square wave generator's output is connected to pin 2 with the modulating signal applied to pin 5 as indicated in Fig. 4. (Incidentally, another NE555 operated in the astable mode will function quite well

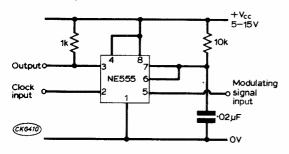


Fig. 4: Yet another application is as a pulse-width modulator.

as the clock generator.) As the control voltage on pin 5 increases, it affects the threshold voltage of the comparator resulting in an increase of the pulse width. The exact opposite occurs as the modulating voltage decreases so the output train of pulses obtained at pin 3 has a frequency identical to the clock input frequency with the pulse width controlled by the modulating signal.

A few of the more interesting applications of the NE555 i.c. have been reviewed in this article and further uses of the device are left to the ingenuity of the experimenter. The NE555 is available from Quarndon Electronics Ltd., Slack Lane, Derby.

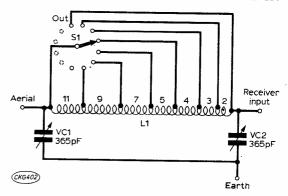


Improving VHF Radio April PW

Although our information was taken from a normally reliable valve and transistor manual the connections for the BF200 transistor in Fig. 6 were incorrect. They should read, clockwise from the tag: emitter, base, collector and shield.

Receiver Matching Unit F. G. RAYER

AN end-connected wire of random length is often used as a short wave aerial and this can, in fact, give good results if reasonably high and clear of earthed objects. At some frequencies, when the aerial length is a half wave or multiple of a half wave, the end impedance at the receiver can be very high, over 1000 ohms. At the other frequencies (a quarter wave or odd number of quarter waves) the impedance is low, probably under 50 ohms. Therefore, for an efficient transfer of energy from the aerial to the receiver at all fre-



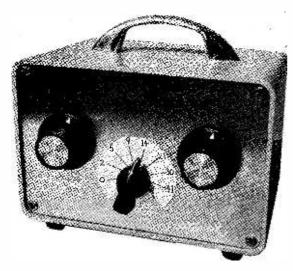
Flg. 1: above, shows the circuit of the receiver matching unit. When switched to "Out" the two variable capacitors should be turned to minimum capacity.

quencies, some matching device is needed. The one described here covers about 3.5MHz to 30MHz, and it is over this range that such an accessory is most likely to prove useful.

THE PI NETWORK

In the circuit, Fig. 1, the tapped inductor L1 has a variable input capacitor VC1 and variable output capacitor VC2. A 12 position rotary switch S1 allows turns to be selected as follows—0, 2, 5, 9, 14, 21, 30, and 41, the last four positions remaining unused. This switch and adjustment of VC1 and VC2 allows a wide range of aerials to be matched to the receiver.

Many communications receivers have a nominal aerial input impedance of about 75 ohms while others, and especially some popular older models, are 600 ohms. On some frequencies the aerial may chance to match the receiver. The Receiver Matching Unit will then give no improvement in signal strength, but can be left in circuit by setting VC1



and VC2 at minimum and the switch at "O".

At other frequencies the switch is progressively rotated to bring more turns into circuit, each time adjusting VC1 and VC2 for best results. This is merely a matter of peaking the matching unit controls for best volume, or best S-meter reading. Where the mis-match is bad, quite a significant improvement should be had. If peaking the signal by ear, switch off the receiver a.g.c. or choose a weak signal or adjust for maximum general noise picked up by the aerial.

capacitors. Solid dielectric components are not recommended. A value of 350pF or so is useful for the lower frequencies, but for the h.f. bands only 200pF or even 150pF capacitors may be suitable, if to hand.

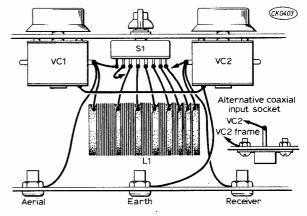
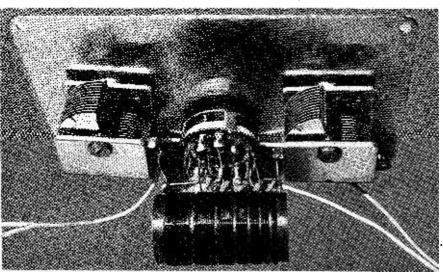


Fig. 2: Wiring diagram of the matching unit. Unused positions on the switch have been ignored.

Fig. 2 shows construction, the coil being supported by its leads. The plastic case used was $6\times4\times4$ in. but had no removable back, so flying leads were left just long enough to reach Aerial, Receiver, and Earth terminals fitted at the rear. Communication receivers often have a 75 ohm co-axial aerial input socket when a co-axial socket can be fitted to the



The photograph, right, shows the author's prototype unit. The mutiple leadouts from the coil are sufficient to hold it firmly on the switch.

The coil is wound with 22 s.w.g. enamelled wire on a paxolin tube 1in. in diameter and about 2in. long. Anchor the wire through small holes near one end. Wind 2 turns side by side, and twist a small loop. Leave a space of about $\frac{1}{16}$ in. and wind 3 turns, making a further loop. Continue in this way, adding 4, 5, 7, 9 and 11 turns, with a small space between each section. Scrape all the loops and solder on leads for the switch.

Solder the leads to the switch so that the first position shorts the whole coil, subsequent positions leaving 2 turns, 5 turns, 9 turns, and so on, in circuit, position 8 having no connection so that the whole coil is in use.

VC1 and VC2 are each 365pF miniature air-spaced

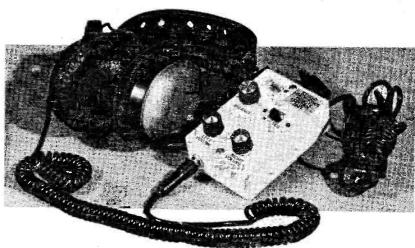
back of the matching unit. The inner conductor of the co-axial lead to the receiver will be the aerial lead, and the outer braiding will act as the earth connection no earth being needed on the unit.

The switch has a scale showing the number of turns in circuit. The lowest frequency reached depends on the aerial and receiver, but can extend down to 1.5MHz in some cases. On some ranges, the unit is useful in reducing second channel interference. If a numbered dial is fitted to each capacitor a very useful chart can be made up showing dial readings and switch positions for the various amateur and short wave broadcast bands, which will considerably shorten the time taken to tune the unit to any particular frequency.

INNEXTMONTH'S URELESS

STEREO HEADPHONES REMOTE CONTROL UNIT

Listen to your stereo records and radio programmes in the comfort of your armchair, perhaps several feet away from the amplifier. Settle down and enjoy the music in the "ideal stereo" position. You don't have to get up to adjust volume or balance controls because you have this small unit on your lap to do it remotely, with balance meter and socket for private listening on stereo phones. Easy construction details given next month.



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TRICOLOUR

Mood Lighting System

PART TWO

JUREK BUDEK*

e but effect

THE P.W. Tricolour provides a versatile but straightforward form of colour lighting effect that is much improved on earlier designs, due largely to the use of the principle of zero voltage switching. Last month's article explained how this was done so now it is time to do the construction and see the results.

Construction

In the *P.W. Tricolour* lighting system, the bass frequencies are 'presented' by the red lamps, middle frequencies by the green lamps and treble frequencies by the blue lamps. The control unit referred to in the following text is the *P.W. Tricolour* filter and control unit.

The construction of the control unit is not complicated if care is taken to follow the drawings and assembly notes. Before connecting any mains supply to any unit, double-check all wiring against the circuit diagrams (last month) and wiring diagrams, making quite sure that all thyristors, triacs and diodes are correctly connected.

It is recommended that sockets are used for mounting the integrated circuits. *Do* not solder the I.C.'s directly to the printed circuit board.

Assemble the eight way socket to the back panel in such a manner that when plug is inserted the five core cable to the lamps leads horizontally away from the fuse assembly.

The lights output socket is a Bulgin type P552 and the plug to fit this (for the lamps unit lead) is a Bulgin P551.

Attach the fuse holders, rubber grommets and speaker socket to the back panel. Assemble the components on to the printed circuit board, making sure that no accidental solder bridges occur across adjacent copper pads. The heat sink for the triacs is "live" and should not be connected to, or allowed to come in contact with, any metal part except the triac mountings, which are also the connections to their "main terminal 2". For safety connect this, the "zero" voltage indicated on the mains transformer, to the neutral terminal of the mains, and connect the control unit chassis to earth on the mains plug.

Insert the rubber grommet for the l.e.d. lamp

indicator into the front panel. Switches S1, S2, S3 and S4 are as used in the Texan amplifier.

The mains switch shown on the front panel uses detachable connecting clips, but any suitably rated mains switch is suitable. The front panel is mounted on the front of the chassis frame with spacers so that clearance of the control fixing nuts provides a neat and uncluttered appearance to the panel. The assembly

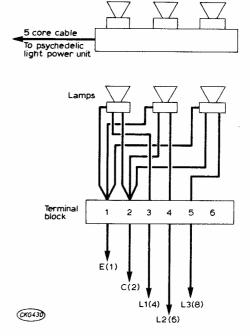


Fig. 13: The simplest arrangement in which one control unit drives three lamps, each 100 to 150 watts. E represents the earth or chassis connection via tag 1 on the Bulgin 8 pin plug|socket arrangement. The figures in parenthesis are the pin numbers. C is the common lead to the lamps—which is the 240V live lead. 11, L2 and L3 are the leads to the respective lamps shown as LP1, LP2 and LP3 (Fig. 12 last month).

^{*} TEXAS INSTRUMENTS LIMITED

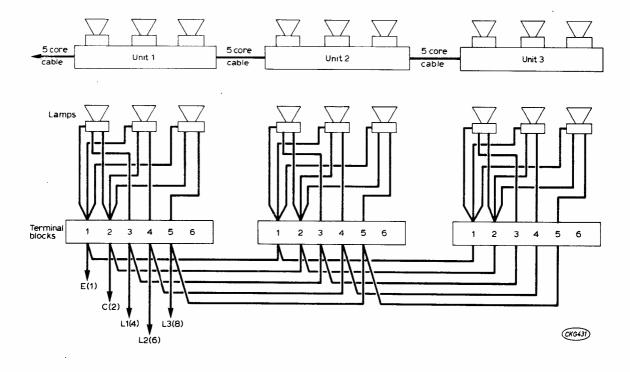


Fig. 14: Three banks of lamps, each 100w maximum, driven from one control unit.

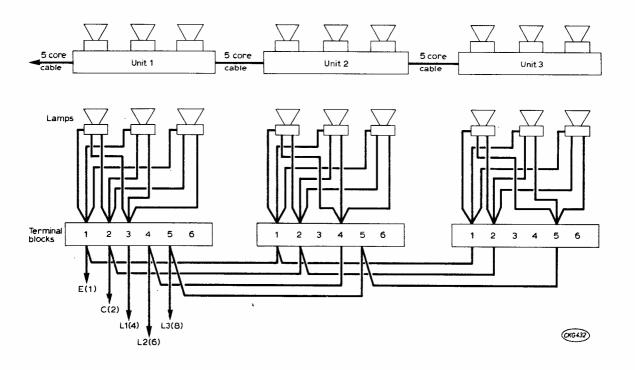


Fig. 15: Three banks of lamps, each 100W maximum, controlled by one frequency range.

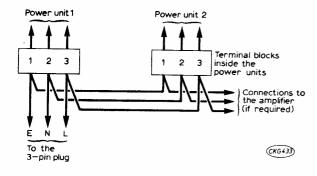


Fig. 16: Mains terminal block connections when using two control units.

uses 6BA nuts and bolts.

The three triacs and their associated heat sink uses 4BA nuts and bolts.

Fuses FS1, FS2 and FS3 are in the bass (red lamp), middle (green lamp) and treble (blue lamp) circuits respectively.

Unit Arrangement

The equipment consists of two units. One unit contains the control for the psychedelic lights, the filter circuits and the necessary power supply. It is advisable, but not essential, that this unit is located near to the 13A power socket and amplifier. The second unit is mobile and consists of three colour lamps mounted on a panel with a five core flexible cable attached to it. This unit can be hung on the wall, left on the table, or placed in some other convenient position.

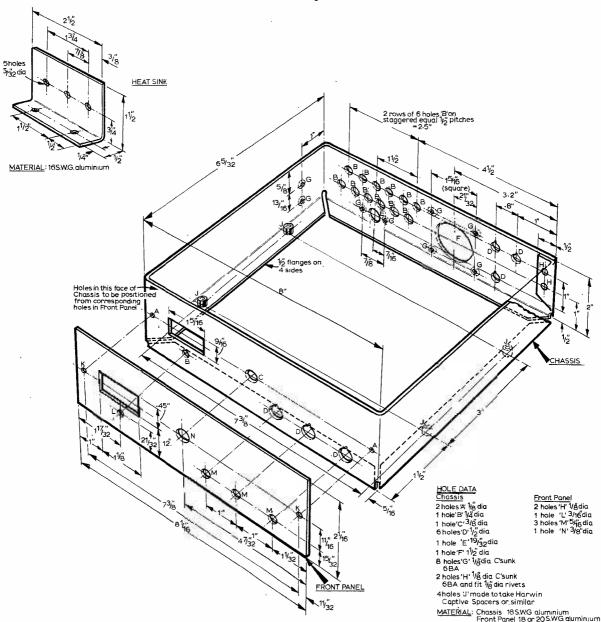


Fig. 17: Details of chassis construction and drilling with the heat sink shown top left, front panel left.

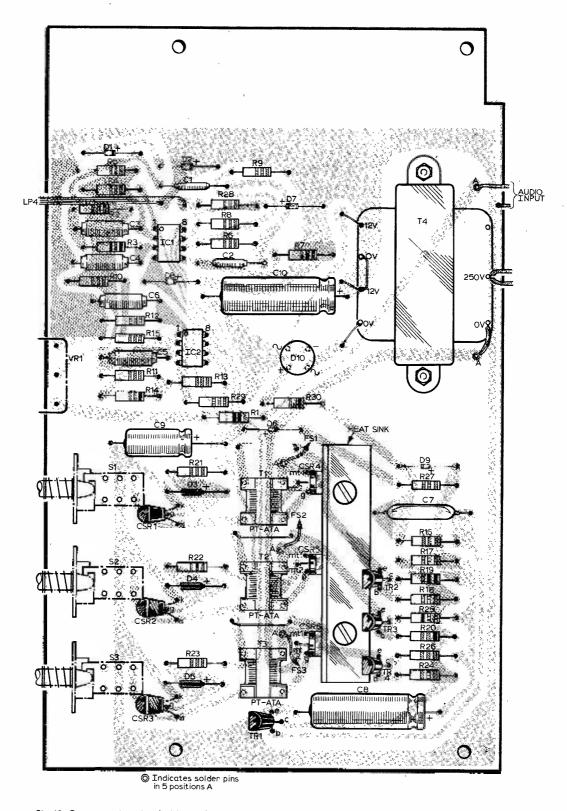
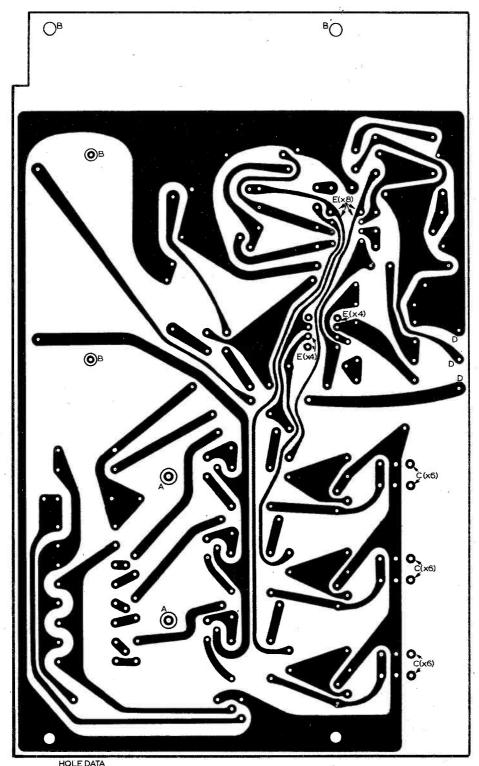


Fig. 18: Component layout and wiring to the printed circuit board. It will be observed that there are two leads from the 250V tag on T4. One lead is the live (L) lead from the mains terminal block. The other lead goes to tag 2 on the lights output socket.



HOLE DATA
2 holes' A' 5/32' dia 3 holes' D' 1.8mm dia
6 holes' B' 1/8' dia 16 holes' E' 1/32' dia
18 holes' C' 1.3 mm dia
All other holes 1.0 mm dia

Fig 19: Full size pattern and drilling positions of the printed circuit board.

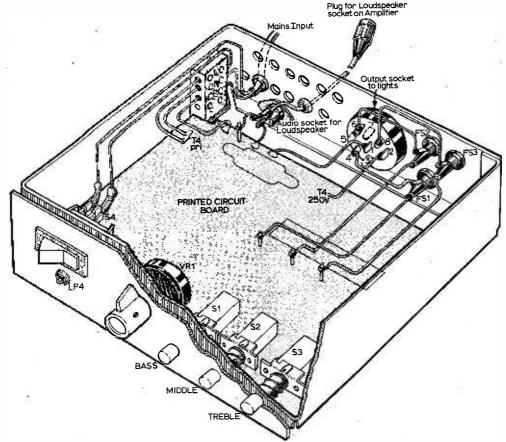


Fig. 20: Wiring of chassis mounted components to the printed circuit board. Tag 1 on the lights output socket goes to chassis (and mains earth). The live lead (L) from the mains terminal block goes to the 250V tag on T4 transformer.

The power control unit is capable of supplying three of these lamp units in parallel, each with its three coloured 100 watt lamps, i.e. a total power capability of 3×300 watts. Each lamp unit has a six way terminal block for interconnecting as shown in the diagrams.

Fig. 13 shows the connections for a single lamp unit. The five core cable is terminated with a plug suitable for connecting to the control unit. The figures in brackets show the pin numbers on the plug used. Connected thus, the three lamps will flash in accordance with frequency ranges present in the music.

Fig. 14 shows a triple unit arrangement, where each unit is connected in the same way as shown in Fig. 13. Here, however, the overall light level is increased and flexibility of lamp positioning is allowed, each lamp unit maintaining its three frequency range response.

A great deal of experimentation of lamp arrangement is worthwhile to achieve the best effect to suit your room and music. Fig. 15 gives another arrangement, using three lamp units, which is basically similar to that shown in Fig. 14, except that here each lamp unit will flash according to one frequency range.

The interconnections between speaker, amplifier and control units are also straightforward. Simply connect the speaker's DIN plug into the control unit and then plug in the cable from the control unit, now terminated with a DIN plug, into the amplifier. This should be done while all power is switched off. The amplifier should be connected via the control unit to a suitable loudspeaker before switching on.

The arrangement for a stereo system is very simple. Two control units and two lamp sets are required. A three core cable from a 13A socket is connected to the terminal board of control unit 1. From the same terminal board the second three core cable is connected to control unit 2 as shown in Fig. 16.

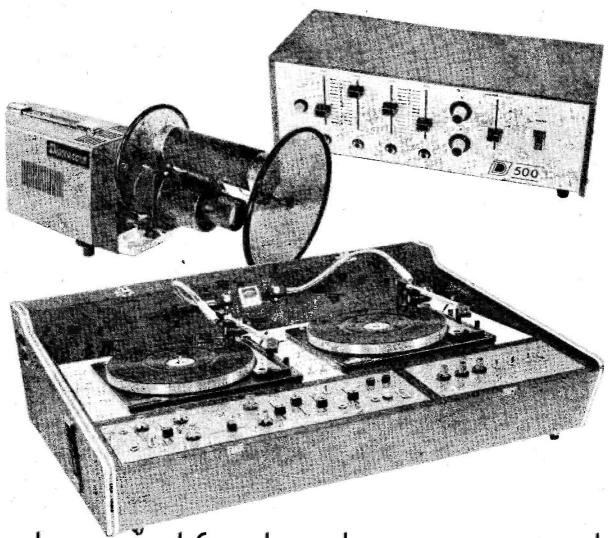
The advantage of this arrangement is obvious, i.e. only one 13A plug is used for both control units. If required, the power supply to the amplifier can also be taken from the terminal board of control unit 2 as shown in Fig. 16, thus achieving further simplification.

The interconnections between the control units, amplifier and speakers are similar to that described for the mono system but duplicated. Connect one speaker DIN plug into control unit 1 and then plug in the cable from it into the amplifier socket. This is repeated for the second speaker and control unit.

The effectiveness of the association of the light and music can be further improved if the lamps are placed near the speaker from which they are actuated. It is extremely effective when standing each lamp unit on or behind each speaker cabinet and projecting the lights up the walls behind.

The printed circuit board shown in this issue is for the zero voltage control version of the *P.W. Tricolour* only. A different printed circuit board, alternative components and slight alterations to the metalwork will be required for the version with lamp dimming facilities.

TO BE CONTINUED



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ADJUSTABLE SPANNER

The picture shows a self-adjusting spanner suitable for all nut sizes from $\frac{7}{6}$ in. to $\frac{13}{6}$ in. A.F.

The end of the tool is placed over the nut and turned until the "tongue" of the spanner locks onto the nut.

It is constructed from chromevanadium steel and weighs $5\frac{1}{2}$ ozs. Finish is either matt (£1·49) or polished (£1·79). Thunder Screw Anchors Ltd., Victoria Way, Burgess Hill, Sussex, RH15 9NF.



TUAC EQUIPMENT

Tuac Ltd., are marketing a new range of ready-assembled modules and complete units. They are a "waawaa" unit, fuzz box, disco "auto fade", octave doubler and a phase-splitter.

Leaflets which are issued in conjunction with Tuac kits can be obtained on receipt of a 3p stamp from: Transistor Universal Amplification, Co. Ltd., 163 Mitcham Road, London, SW17 9PG.

AUTO GROOVE-KLEEN



If you have an autochanger record playing unit, you have not been able up to now, to use a groove-cleaning brush to remove the dust and dirt from the records.

Bib seem to have solved this problem with their model 45 unit which just sticks onto the cartridge housing. Obviously to avoid any increase in stylus weight, the tone-arm should be re-balanced or the calibration control reduced by two grammes.

Due to the design, the velvet shoe and brush will not drag across the record when the tone arm moves from the end of one record to the outside of the record stack.

After the records have been played, the velvet shoe can be lifted off for cleaning with the separate brush supplied.

The price of this unit is 98p plus tax. Bib Sales, P.O. Box 78, Hemel Hempstead Herts.

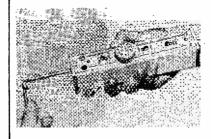
GUIDE TO SEMICONDUCTORS

Motorola Semiconductors Ltd. have published a "master selection guide". It includes in its 150 pages brief technical details of 17 diode families from 4-layer to zener, hybrid circuits, microwave devices, optoelectronic components, rectifiers, triacs, diodes, linear integrated circuits and much more than we can describe here. The guide, which is free of charge, may be obtained from Motorola Semiconductors Ltd., York House, Empire Way, Wembley Middlesex.

TRANSISTOR TESTER

Transistor tester type TT169 has been announced by Avo. It is designed for GO/NO-GO in-circuit testing of p.n.p. and n.p.n. signal or power transistors. The tester is battery operated and small enough to be held in the hand. Front panel lights show whether a device is faulty or OK.

The TT169 comes with all the necessary leads and connector in a plastic case. The price is £17.50 plus VAT and readers may obtain them from the usual retailers and distributors. Avo Limited, Avocet House, Dover, Kent.

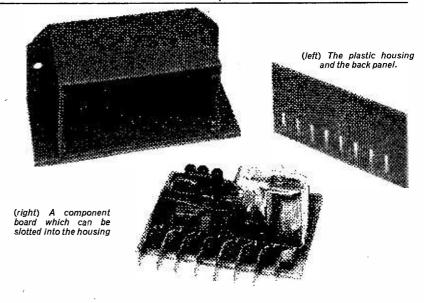


COMPONENT HOUSING TYPE LK8

Logikontrol Ltd., announce a compact component housing. It is made from high impact polystyrene and measures 90 x 50 x 37m.m. and at 25·4m.m. to the inch, you can work it out for yourselves! The internal volume is 10c.c. and it has facility for 2 printed circuit boards on which the components can be mounted.

Printed circuit connections and a snap-fit lid eliminate the need for a special plug and socket.

These units which are available in five different colours may be obtained from large component suppliers or in quantities of 10 upwards from Logikontrol direct, the 10 off price being 22p each. Logikontrol Ltd., 17 Little Edward Street, London, NW1 4AT.



R.A. PENFOLD

THIS is a simple device which is easy to construct and which when placed ahead of a medium wave receiver will enable it to cover the 80 and 160 metre amateur bands. The unit is self contained, and is housed in a diecast box measuring 4^3_4 in $\times 2^5_3$ jin. An external long wire aerial and an earth are required.

Only two transistors are used, including a field-effect type in the mixer stage. Frequency stability is excellent as the oscillator is crystal controlled.

Heterodyne Principle

What is required of the converter is to receive a signal in either the 160 or 80 metre band and change this signal to a frequency which lies in the MW band. This can be achieved by heterodyning.

This is a process in which two signals are mixed to produce at the output, (a) the original two frequencies, (b) the sum of the two, and (c) the difference between the two. By the use of tuned circuits in the output, whichever of the two new frequencies produced is required can be selected.

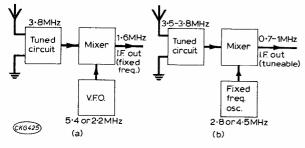


Fig. 1: Diagrams showing methods of converting a signal to a fixed or variable intermediate frequency.

The manner in which this process can be used in a converter is shown in Fig. 1. In the type of converter shown in Fig. 1a, the circuit is arranged so that the frequency to which the tuned circuit at the input is tuned is different from the operating frequency of the oscillator by the i.f. The tuning capacitors for the aerial tuned circuit and the oscillator would be ganged.

An example is given in the diagram of how a 3.8 MHz signal is converted to a 1.6 MHz i.f. There are two oscillator frequencies which will allow this (3.8 - 1.6 = 2.2 MHz), or 3.8 + 1.6 = 5.4 MHz). In this type of converter the receiver is tuned to the i.f., and the tuning is carried out on the converter.

A second type of converter is shown in Fig. 1b. This type is often used in 2 and 4 metre VHF

amateur band converters. This time the tuning is carried out on the receiver, the oscillator on the converter being at a fixed frequency. The aerial tuned circuit should either be a broadband unit i.e. resonant over the entire band which is to be tuned, or should be tuneable over this range. Again there are two possible oscillator frequencies (3.8 - 1 = 2.8 MHz, 3.5 - 0.7 = 2.8 MHz, 3.8 + 0.7 = 4.5 MHz, 3.5 + 1 = 4.5 MHz).

This type of converter has the advantage that the oscillator can be crystal controlled, simplifying alignment and giving very good stability. This type is also very much more simple and inexpensive. The system does have drawbacks as discussed later but the author's converter, which is of this type, has proved very successful.

Practical Circuit

A circuit diagram of the converter is shown in Fig. 2. Tr2 is operated as a Pierce oscillator the crystal being used on its parallel resonant frequency. The primary winding of the oscillator r.f. transformer, L5, forms the collector load for Tr2. R2 biases the transistor, C3—C5 produce a centre tap on the crystal, this centre tap being earthed.

Tr1 is the f.e.t. mixer stage. L1 is the aerial input coupling winding and L2 the aerial tuned winding. This can be tuned over the range 70-230 metres by VC1. Tr1 is used in the common-source mode, source bias being provided by R1 and C1 is its decoupling capacitor. Tr1's source and R1 are connected via the

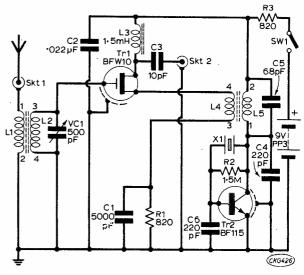


Fig. 2: Complete circuit of the converter unit.

secondary winding on the transformer, L4. The voltage across L4 modulates Trl's drain and source voltages and thus mixes the oscillator signal and the input signal. A small r.f. choke, L3, forms the drain load for Tr1, the mixed output being coupled to the receiver via C3.

SW1 is the on-off switch, and R3 reduces the 9V supply to the required level. C2 is the supply decoupling capacitor.

The crystal frequency is chosen so that it can be used to convert signals in both the 80 and 160 metre bands to the MW band, the desired band being selected by tuning VC1—L2 to the correct frequency. Using a 2.8MHz crystal the 80 metre band will be converted to 0.7 - 1MHz (3.8 - 2.8 = 1, 3.5)-2.8 = 0.7), and the 160 metre band will be converted to 0.8 - 1MHz (2.8 - 1.8 = 1, 2.8)-2 = 0.8).

It is not essential for the crystal to operate exactly on 2.8MHz, as if it is a little either side of this frequency the converter will still operate but the tuning range on the receiver over which the amateur bands are covered will be slightly altered. A 2.794MHz crystal was used on the prototype.

Construction

The circuit is housed in an STC diecast box. The wiring is broken into two sections, a 5-way tagstrip on which the oscillator is constructed, and a 6-way tagstrip on which the mixer is built.

Diagrams illustrating the wiring of these two tagstrips are shown in Fig. 3 (mixer) and Fig. 4 (osc.). These two diagrams also show all other wiring of the converter. All the wiring is quite straightforward and should present no difficulty, even to a beginner. The only point which should be noted is that the screen lead of Tr1 is too short to reach to the appropriate tag unless a short piece of insulated wire is used to lengthen it.

Figure 5 shows the interior layout of the unit and also gives details of the mounting bracket of the crystal. This bracket is constructed from 18-22 swg sheet aluminium. The two tagstrips are mounted by ¹2in 6BA bolts, a stand-off insulator ¹4 to ³8in long being used to hold them clear of the sides of the case.

The battery is held in place by being trapped between the front, and rear of the case. A pad of expanded polystyrene, foam rubber or a similar material should be glued to the rear of the case where the battery would otherwise come into contact with it. This is to make it fit more firmly and to insulate the battery terminals from the case.

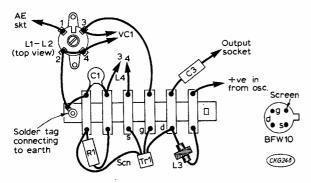


Fig. 3: Method of wiring the mixer stage components.

★ components list

Resistors R1 820Ω $1.5M\Omega$ All ±W, 5 per cent types R3 820Ω

Capacitors

- 5000pF
- 0 022μF polystyrene etc.
- 10pF ceramic or silver mica C3
- C4
- 220pF polystyrene or silver mica 68pF polystyrene or silver mica 220pF polystyrene or silver mica

Semiconductors

Tr1 BFW10 or similar f.e.t. Tr2 BF115

Miscellaneous L1/2 Repanco RA3; L3 miniature r.f. choke, about 1.5mH; L4/5 Repanco RO3; SW1, on-off switch; STC discast box, size 2 (4½ x 3½ x 2 ½zin.); HC6U crystal, about 2.8MHz with holder (see text) (Henry's Radio); 1-off each 5-way and 6-way tag strip; 2-off coax sockets; Knob; Battery and clip.

As supplied, the exterior finish of the diecast box is rather rough and dirty. If the case is to be painted it will be necessary to thoroughly clean it first with a scouring pad. If preferred it can be cleaned in this way, and then polished to a bright natural finish.

Using the Converter

An external aerial is required; this merely consists of a length of wire which is mounted as high as possible and is as long as possible. An earth of some sort is essential for the correct operation of the circuit, although this does not necessarily have to be a very efficient one. The prototype is fitted with coaxial sockets for the aerial, earth and output connections.

Ideally the converter should be used in conjunction with a broadcast receiver which requires an external aerial. The receiver and the converter are connected by a short screened cable. In this way there is a minimum of interference picked up on the MW band directly by the receiver.

It was found possible to use the converter with an

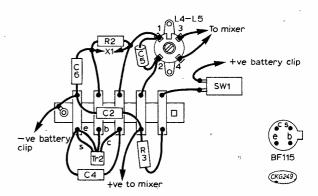


Fig. 4: Tagstrip construction of the oscillator stage.

ordinary transistor receiver. C3 should be removed, and a piece of wire connected in its place. It is then merely necessary to take a short lead from the converters output socket, and to place this alongside the receiver's ferrite aerial.

In this way it was found possible to receive a number of amateur stations on both the 80 and 160 metre bands. MW stations received directly by the receiver can prove bothersome, especially after dark.

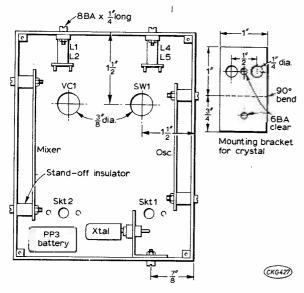


Fig. 5: Layout of components and tagstrips inside the die-cast box.

Operating the controls on the converter is very simple, as there are only two. SW1 is the on-off switch. VC1 tunes the converter to the desired band. With this control turned almost fully anti-clockwise it should be found possible to tune the 80 metre band and with it turned almost fully clockwise it should be possible to tune 160 metres.

With VC1 approximately adjusted in this way, it should be possible to receive a few signals. VC1 can then be peaked for maximum sensitivity. A simple dial can be marked around the control knob of VC1 showing the areas over which the amateur bands are tuned.

Results

Using the converter with a 132ft. longwire aerial at about 20ft., in conjunction with a 6 transistor MW portable receiver, a large number of amateur stations have been heard. The 160 metre band is of course used mainly for local working, and a.m. is still used to a certain extent. Stations up to about 50 miles distant have been received on this band without too much difficulty.

Due to its simplicity, the circuit does have one drawback. Top Band is not only used for amateur transmissions but also for maritime ones. These transmissions are fairly powerful and occasionally when tuning the 80 metre band transmissions from ships in the nearby Thames estuary did break through. Conversely, a local amateur using a powerful SSB transmitter on 80 metres did tend to break through on the 160 metre band.

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SHORT WAVE RECEIVER CHOICE by MALCOLM CONNAH

By far the largest portion of my mailbag consists of lettters from readers asking my advice on the choice of a receiver. I have often said that this is a very difficult subject on which to give advice, partly because the letters give very little information and partly because "one man's meat is another man's poison".

In order to assist the less technically minded reader to select a receiver to meet his requirements I am going to devote this article to discussing the various features of receivers which are important for good short wave reception.

1. Frequency Coverage: The most common type of receiver is the General Coverage Receiver. This type of receiver usually tunes from 540kHz to 30MHz in four bands. One of these bands covers the medium wave band leaving three bands of short wave coverage.

Due to the number of stations on the bands it is very desirable to have a separate bandspread, or fine tuning, control. This control has the effect of expanding a small portion of the tuning scale making it much easier to tune in a particular station. The much-advertised transistor portable receivers are usually lacking in this respect.

An alternative method of frequency coverage is found in the more expensive receivers which have a number of bands each covering 500kHz of the spectrum. These receivers usually cover the Amateur bands only but can be ordered with coverage of the Broadcast bands. The tuning of these receivers is so fine that a separate bandspread control is not required.

In general the listener must ensure that the receiver covers the bands in which he is interested and that the tuning can be finely controlled.

2. Number of Conversions: The number of conversions that a receiver has is the number of different i.f.'s (Intermediate Frequencies) that it has. The normal single conversion receiver has a single i.f. usually in the range 455-470kHz, although 1.6MHz is sometimes used. The double conversion receiver has two different i.f.'s. In general, the more i.f.'s a receiver has, the better the selectivity and image rejection will be.

3. RF Stages: Some of the simpler receivers available have no r.f. stage and the signal is passed from the aerial to the mixer stage directly. The addition of an r.f. stage will increase the sensitivity of the receiver and also improve the image rejection of a single conversion set. As mentioned last month this problem can be overcome by adding a preselector between the aerial and the receiver.

4. Operating Modes: The Broadcast Bands listener is usually only interested in amplitude modulated (a.m.) signals and this mode of operation is, therefore, essential. If the set is also to be used for reception of Amateurs provision should be made for code (c.w.) reception, this also allows reception of single sideband (s.s.b.) transmissions. However, the provision of a product detector gives much better s.s.b. reception. If the provision also exists for manual selection of the upper or lower sideband this facility can be used during the reception of a.m. signals to avoid interference and fading effects.

5. Selectivity: The selectivity of a receiver is its ability to separate stations on adjacent frequencies. It is extremely useful to have the facility of varying the selectivity of the receiver. When interference is heavy a narrow selectivity can be used to cut out the interference. Mechanical or crystal filters help to improve the selectivity of a receiver.

6. Stability: It is essential for a good receiver to be stable in operation. With some valve receivers the heating effects involved caused frequency drift and other annoying effects. The introduction of transistors and, in particular, field-effect transistors has greatly improved the situation due to the low heating effects associated with these devices.

7. Valves vs. Transistors: Apart from improving stability, as mentioned above, transistors have many advantages in communication receivers. They have a longer life, require simpler power supplies and are low cost. The benefits of this are that transistor receivers tend to be smaller, lighter in weight, less expensive and also have the option of being operated from an external battery.

8. Automatic Volume or Gain Control (a.v.c. or a.g.c.) Almost every receiver has some form of a.v.c. or a.g.c. which adjusts the gain of the receiver to compensate for changes in signal strength. A receiver with variable a.v.c. or a.g.c. is to be preferred as the optimum setting can then be used.

9. Extras: Most receivers have various extras of which the following are the most useful. (a) The provision of a headphone socket. (b) An aerial trimmer to match the aerial to the set. (c) A signal strength meter (S-meter) to assist with tuning. (d) A crystal calibrator to check the dial accuracy. (e) A noise limiter which should be variable if possible. (f) A notch filter to reduce hetrodynes.

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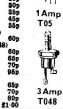
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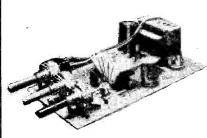
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COMMERCIAL RADIO by CHARLES MOLLOY

OMMERCIAL radio in the UK has come a step nearer with the start of medium wave tests in the London area by the Independent Broadcasting Authority. Kevin Peel (Hornchurch Essex) has heard the IBA on 557kHz with transmissions of music and announcements stating that the tests were being made by the IBA for an indefinite time. The choice of frequency is a surprise as the two IBA London stations are expected to be on 1151kHz (London News) and 1546kHz (London Entertainment). The first regular broadcasts from the IBA are scheduled to start this year with the opening of the London stations to be followed in 1974 by others in the provinces.

Harold Emblem (Mirfield, Yorkshire) has logged a number of medium wave stations in the Persian Gulf area between 0230hrs and 0300hrs GMT. He reports Kuwait on 539kHz; Tabriz, Iran on 645kHz; Bagdad 760kHz; 'The Voice of the Arab Emirates' Dubai 1250kHz with an Arabic religious programme followed by pop music at 0300hrs; Teheran 1325kHz; Kuwait 1345kHz. Harold mentions that Kuwait

539kHz can be heard during the evening under Budapest, which uses the same frequency. Baghdad on 760kHz is also audible in the evening.

Commercial radio is well established in Spain where several chains of low power locals operate alongside the government owned Radio Nacional Espana networks. The commercial stations are allocated call signs and about 150 of these outlets can be found all over the band. Those most frequently heard in the UK are EAJ5 Radio Sevilla on 809kHz; EAJ1 Radio Barcelona on 827kHz; EAJ2 Radio Espana (Madrid) 917kHz; EAJ29 Radio Intercontinental 953kHz; EAJ8 R. San Sebastian 1025kHz; EFE14 La Voz de Madrid 1097kHz; EAJ15 Radio Reloj (Barcelona) 1124kHz; EFJ43 Radio Juventud Bilbao 1133kHz; ECS11 Radio Centro Madrid 1385kHz; EAJ20 Radio Sabadell 1475kHz; EFE25 La Voz de Calabria 1570kHz. The common channels 1106kHz, 1133kHz, 1394kHz, 1412kHz, 1430kHz, 1475kHz, 1502kHz, 1520kHz and 1570kHz are crowded with stations. They sign-off for the night from 2300hrs GMT onwards and at this time the DXer can hear one station after another dominate a channel only to close down and leave the frequency free for a weaker occupant. Many a rare catch can be had at this time.

L. J. Hook asks for information about the MW Command receiver. Also known as the BC946 it was part of the ARC5 aircraft communications equipment used in the last war. It performs very well on the medium waves but it does require some modification as it was designed to work from a 28 volt aircraft supply.

IBA ON VHF

by SIMON DAVID

HIS new v.h.f. section will be a regular feature giving news and views on transmissions usually found on the 88 to 108MHz dial, but may be extended to include related topics. VHF is generally taken to include transmissions between 30 and 300-MHz, i.e. below 10 metres, but since this area is also covered in David Gibson's Short Wave column, this section has been specially started to provide some information more appropriate to broadcasting.

Since f.m. broadcasts began in the U.K. on a regular basis, it has been continually predicted that the medium wave band was due for banishment. This has not come about however and the medium wave is in fact still being exploited. What is expected is that the new Independent Broadcasting Authority Stations will use the upper reaches of the f.m. dial for stereo programmes, but will not necessarily use the same transmitters as the BBC. Receivers within close proximity of a BBC transmitter and collecting signals of around $100\mu V$ may find that they will be able to pick up a 20mV signal from the local IBA station.

One of the main headaches is expected to come from cross modulation effects due to emergency services being tuned in close to the commercial channels. This will undoubtedly result in a number of semi-redundant old tuners, although there is no fear of upsetting their present usefulness for BBC programmes. Whether politics come into this we are not too sure, but it is strange how the commercial side of broadcasting frequently has to accept second rate operational conditions.

In order to help find space for the new IBA com-

mercial radio stations, the BBC will be nudging its local stations along the v.h.f. tuning scale a little, changing the operating frequencies of Radios London, Medway, Oxford, Brighton, Bristol, Leicester, Nottingham, Stoke, Humberside, and Sheffield. These adjustments are expected later this year when the appropriate details should be given in the local Press and Radio Times.

The new station at Carlisle is still expected to "appear" on 95 6MHz, but it looks as if Swaledale will be "lost" for want of a suitable site for a relay station

Although some way off yet, it is not a bad idea to look into the needs and possibilities of incorporating very sharp rejection filters to suppress adjacent local transmitters. The use of a field effect transistor at the front end will also help to reduce cross modulation effects. Several tuners have automatic gain control and since this would not be helpful in this situation it is worth incorporating a switch so that it can be cut out of service as necessary.

Furthermore, the mixer stage design becomes critical and the noise generated here must be at a very low level. This will mean that the r.f. circuit will not have such a high gain as in the past but this can be made up by increasing the gain through the i.f. stages.

The use of phase-lock integrated decoders will provide tuners with lower distortion and better frequency response, both of which have become necessary for good stereo reception.

We shall always be pleased to hear of readers' experiences of v.h.f. reception, especially those who listen in to continental stations. Please be brief and confine your letters to stations received, aerial and tuner used and the effect of interfering transmissions.





SHORT WAVES by DAVID GIBSON, G3JDG

HIS month's postbag has been conspicuous by the very marked absence of 14MHz logs. It seems that the twenty-metre-only addicts are as dead as their band these days. Meanwhile, back at the eighty-metre ranch it's been a right merry r.f. square dance. The amount of DX on eighty has been quite remarkable with west coast W stations romping in at times. In fact, stations further down the globe have also put in an almost regular appearance on this band; Mexico, Brazil and Argentine, etc. Some real goodies have put in an appearance for the persistent enthusiast. Callsigns like DU1EJ and VS6DO have shown that your reciever dial need not read above 4MHz in order to log some rewarding DX signals both on phone and c.w.

News from VE land. An enthusiastic band of Canadian Amateurs are building a large oceangoing trimaran. Their object is to put the 40 most "wanted" countries on the air. I will pass on information about their ports of call as soon as I hear.

Great hopes that an Amateur station will be allowed on Clipperton Island. Callsign to listen for will probably be FO8C. Anyone heard the station reported to be located in the Spanish Sahara yet?

Time to pass on to some queries, curses and comments. Michael Green (Cheshire) uses a UR1A. The drawing of his antenna system bears a harrowing resemblance to the national grid. (Bet he's the only s.w.1 who tunes topband in rubber gloves and wellies). Michael queries queer callsigns heard in the wee small hours on 80 metres s.s.b.; Rudolph, Scrooge, Virgin Mary and Snowman. Michael's problem is simply, "How do I QSL them?" (Perhaps the nearest Asylum is licensed?).

Letter from a long, long way off bears the signature of Lindsay Pennell and the post mark Hong Kong (Ah, those were the days, Chow Mein butties and cocoa on the Kowloon ferry). Lindsay wonders why so few G s.w.l.s hear the Hong Kong throng signing VS6. There are some 40 licensed Amateurs many of them being very active into Europe. Confess now, you're all logging VS6's and not telling your Auntie David.

Simon Baines (Hitchin) reports a number of W stations including W5NMA, heard on forty metres s.s.b. Gear is a five-vale receiver, transistor b.f.o. and 30ft of wire end fed.

M. Harrison (Derby) sends in a log of numerous G stations heard on topband. Incidentally, a good non-G to listen for on 1.8MHz is W1BB/1 whose stalwart support and interest in topband is well known all over the world. It is interesting to note that PY1DVG has been heard on 1.8MHz.

Kevin Smith is thirteen summers old and lives in Brighton. (Wish I was and did.) Whereas most boys of 13 are the proud possessors of pieces of string and marbles, Kevin settles for a CR100 and a 215ft long wire end fed. His best areas on topband were: DL8PC, GI3GRD, GM4BBL, GW3ZQN all on s.s.b., and OK1ATP on c.w. His log for 28MHz reads: CN8BF, CN8CF, CR4BS, CR7AF, CR7IZ, CT2AT, ET3USF, ET3USP, KV4CF, ST2SA, VP2LAF, WB4WOI/P, ZE4JW, ZS6AD, 4Z4ME, 6W8DL, 7Q7RM, 9G1HE, 9H4D, 9J2AY, 9J2DT all s.s.b.

Best times for listening on eighty metres are from midnight to around 0300 hours according to Alan Smith (Lancs). He bemoans the Lids who test incessantly by blowing into the mike (it's unhygienic but they can't touch you for it). Alan has a JR31), 60ft end fed and an a.t.u. Heard on eighty: EP2TW, Kluat. K2LQA, KP4AN, KV4CI, PY4BTK, VE1ADV, VP2LI. VP7ND, WIGEY, W2BXA. W3WGH, W4AG, ZB2CF, ZS1MH, ZS3GH, 9H1CW, 9V1RE. A cheap day excursion to 14MHz s.s.b. raised: EP2ES, HZ1AB, KG6JBE, KL7HFA, KX6BQ, LUIDAC, MP4TEE, VEIASJ, VE3MO, VK3ADR. YK1AA, ZL1KN, ZL1WE, ZL2AVE, ZL2BQC, ZL3QN.

David Sharred (Birmingham) had a quick tour of eighty metres. Main listening times were "after my paper-round", and the gear is a CR150/2 with a V-shaped antenna (60ft each leg). Goodies bagged on 3.5MHz: CN8BF, JY1, K5PFL, KV4AM, OA6NCT, PI1ROS, VE3CDP/W9, W2HCW, W4MYA, W9QLD, WA5JMK, WB4MCI/P4, ZK2BO, ZL4BT, ZL4KF, ZS3GH, 3A2EG, 5U7AX. On twenty metres David's best were VK5RN and VK6XO.

Where are all you v.h.f. types hiding? No logs at all for lonely little 70MHz and only one for 144MHz. **Michael Prescott** (Lancs.) uses a Roamer 10 receiver and a two metre dipole. He reports signals from the following: G3AHD/A, G3PVC, G3VIM, G3XIM, G3VME, G8EYO/A, G8ESU, G8GYS, G8VLE and G8XDL. Well done Michael, you've kept the v.h.f. flag flying—just.

For the contest and Rally enthusiasts, April is a busy, busy month. Jottings from my Events diary read: April 1, White Rose Mobile Rally at Leeds; 1, WAB phone contest (l.f.); 8, WAB c.w. I.f. contest; 8, eighty metre QRP (low power) contest; 15, four metre portable contest (no excuse now for not sending in a log); 21-22, Bermuda contest (phone); 29, Rugby DF qualifying round; May 5-6, two metre and 70cm open contest (another chance for the v.h.f. s.w.ls to shine); 5-6, Bermuda contest (c.w.); 6, Spalding Tulip Time Mobile Rally.

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Operation

When a voltage is applied to the circuit, the capacitor C1 starts to charge up through R1 and VR1. Initially the emitter of Tr1 will be at negative potential but as the capacitor charges, the voltage at this point rises. When it reaches a certain point, b1 and b2 are virtually short circuited and current will pass through R2, R3 and Tr1. At the same time C1 will be discharged through R3 and the device will become open circuit again. The same process will start all over again so that a series of pulses appears across R3 via C2. Since the output will be a series of pulses whose rise and fall times are very rapid, only a low value capacitor is necessary despite the low value of R3. The output will be in the form of a positivegoing pulse; if a negative-going pulse is required this capacitor should be connected to b2. A sawtooth waveform is available from the emitter but it should only be connected to a high impedance load otherwise the operation of the relaxation oscillator will be

The frequency of the pulses depends on the relationship of the resistance made up from VR1 and R1 and the capacitor C1. Resistor R1 limits the current

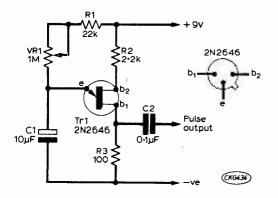


Fig. 1: Circuit and suggested valves for the pulse generator.

No. 48 PULSE GENERATOR

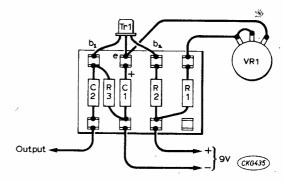


Fig. 2: Practical layout of components on a piece of tagboard.

through the emitter so that it cannot be connected directly to the positive line; this would cause damage to the device.

Experimenting

There is room for experiment here; C1 can be altered in value from $500\mu F$ down to $0\cdot01\mu F$. The high value will produce pulses with very long intervals; it is difficult to say how long as the natural leakage through the electrolytic will play a major role. If a low leakage device is used the time intervalcan be a minute or more. Using the low value capacitors the pulses could extend to ultrasonic frequencies.

* components list

R1	22kΩ ¼W, 5 per cent	1p	
R2	2·2kΩ ,,	1p	
R3	100Ω ,,	1p	
VR1	1MΩ linear pot	12p	
C1	10μF 12V	5p	
C2	0·1μF mylar, etc.	4p	
Tṛ1	2N2646	40p	
		64p	
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changed. No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering.

Modifications

The output can be taken to an amplifier to act as a metronome. In fact if only a low level output is required, a high impedance loudspeaker (50Ω to 80Ω) can take the place of R3; in this case of course C2 will not be needed.

A suggested layout is shown in Fig. 2 making use of a small piece of tag board; this is far from critical and almost any layout may be used.

OTLINES

ON RECENT DEVELOPMENTS

o you ever have that feeling that you are being watched? Well, maybe you are at that and have been for the past 13,000 years. A theory has been put forward that we are getting intelligent messages from space. To be more precise, from an interstellar "thingy" which is buzzing round the earth—probably in an orbit which is similar to that of the moon. (Good gracious, Holmes).

LONG WAY ROUND

Before you rush out and wave your hanky at the sky, hear what the experts have done about it. It is all tied in with things called longdelayed echoes. These observed as far back as 1928. A transmitter using 15kW on 9550kHz was radiating its Morse signal which in turn was being received by a number of receiving stations. A Morse signal was being sent and received almost instantaneously. Now a signal can go two waysdirect to the receiver by the shortest route and also in the opposite direction. This latter signal can quite easily travel right round the world before it is received by our receiver. Thus two signals are heard; the direct one, and the one which goes the "long" way round. The latter takes about one seventh of a second and is heard as an "echo" of the direct signal which, because it travels direct (therefore less distance) arrives almost instantaneously i.e., with negligible delay.

So far so good. But imagine the effect on the minds of the listeners when other echoes were heard—not delayed by one seventh of a second but at various intervals varying from about three seconds to 15 seconds! These long-delayed echoes were also noticed independently at other times, on other dates, by different receiving stations listening to a different transmitter and on a different frequency.

Then, someone plotted a graph of one of these echo sequences and another piece of the intrigueing jigsaw came to light. The plotted points bore a striking likeness to the constellation Bootis. Other echo sequences were plotted and produced patterns which were clearly

The hypothesis has been put that the long-delayed echoes are being returned to Earth from a space probe; a probe which arrived from

identifiable with other constellations.

probe; a probe which arrived from the Bootis constellation 13,000 years ago. Moreover, the probe was sent to search for evidence of intelligent life in the form of radio transmissions.

People who are in doubt about the validity of all this should bear in mind that all the evidence so far corroborates this hypothesis. So closely, in fact, that EMI engineers are to set up a high-power transmitter and high gain antenna (probably around 144MHz) in order to put the hypothesis to the test. Are they just being starry-eyed? I do not think so.

Once a complete digit is generated it is safely entrusted to the memory of a computer. Here, it is checked to see if it is eligible. If it is, then it will be stored in the computer's memory, if it is not, it will be discarded.

Ernie presses on until the memory or store has 60 numbers in its care. These are then "written" onto magnetic tape and this is then "played" to another computer for checking and finally linking the lucky numbers to the bondholders' names and addresses.

I am already making the most careful measurement of the noise generated by a pair of zener diodes well, you never know.

ERNIE

Apart from driving the fastest milk cart in the west, Ernie has achieved fame in other ways. For example, he painstakingly avoids selecting your premium bond number every month without a single complaint or grumble. To date, his selections have paid happy punters prizes amounting to some £350 million—none of which has yet reached your scribe!

So it is with ageing joy and renewed hope that I report a new Ernie who will produce the monthly list of prizewinners in under three hours. The old Ernie used to take ten days to complete the same task.

Before we non-winners get too elated, let us examine what we are up against. Just what (or who) is Ernie and how does he choose winners?

First, Ernie comes from Ernie Harrison, Managing Director of Racal, whose idea it was. Ernie himself (the number picker) has been described as the most advanced electronic system in the world for generating numbers in a completely random fashion. How does he/it go about the task?

The first job is to monitor the noise level of a pair of zener diodes (actually, a pair for each digit). Each "pair" noise is amplified and then compared with a reference voltage. Because of the nature of noise there are peaks, and each time one of these exceeds the set reference level it is counted and used in the production of a digit,

TRANSISTORISED TED?

How about an electronic government, a big computer tucked away beneath Parliament in a Guy Fawkesproof vault? Maybe not yet, but in America the computer has managed to secure itself a small governmental foothold.

The House of Representatives is to vote by computer. Problem has been the 435-name list of members and the time wasted in correcting attendance errors. Other little hitches like finding a vote recorded from a member who wasn't even there were also proving annoying. The mind boggles.

The new system means that each member has a small plastic "card". He can use this card to vote at any one of some 50 stations located at various points about the House. Behind the Speaker's seat is a score-board which gives the latest updated score on how the voting is going. Electronic voting is reckoned to save at least 50 per cent of the time previously taken for such a task. The computer will also give written records of votes simultaneously plus an instant breakdown of these into States or Parties as required.

Look out members of Parliament you might be replaced by a pair of zener diodes one day—they're cheaper, smaller and generate less noise!



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H9	2	OCP71 Light Sensitive Photo Transistor	50p
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H35	100	Mixed Diodes, Germ, Gold bonded, etc. Marked and Unmarked.	50p
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H39	10	Integrated Circuits, 6 Gates BMC 962, 4 Flip Flops BMC 945	50p
H40	20	BFY50/2, 2N696, 2N1613 NPN Silicon uncoded TQ-5	50p
H41	2	Sil Power transistors comp pair BD131/132	50p
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		THE RIASS TYPE	
B83	200	Trans. manufacturers' rejects all types NPN, PNP, Sil. and Germ.	50p
B84	100	Silicon Diodes DO-7 glass equiv. to OA200, OA202	50p
B86	100	Sil. Diodes sub. min. IN914 and IN916 types	50p
B88	50	Sil. Trans. NPN, PNP equiv. to OC200/I 2N706A, BSY95A, etc.	50p
Bì	50	Germanium Transistors PNP, AF and RF	50p
H6	40	250mW. Zener Diodes DO-7 Min. Glass Type	50p
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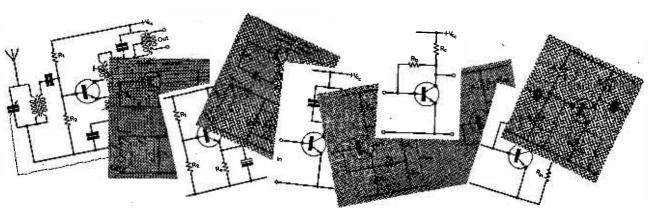
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TRANSISTOR CIRCUITRY for beginners

PART 16

H.W. HELLYER & MICHAEL HOLLIER

Practicalities

A BC109 is chosen to give an open-loop gain of 260, with an input of about 30mV at 1kHz. We shall aim to keep this level constant for further tests. Connecting the two resistors of Fig. 76 to the input, we have the virtual earth type of circuitry. This has been discussed at some length in previous articles. It can now be simplified to the triangle of Fig. 77,

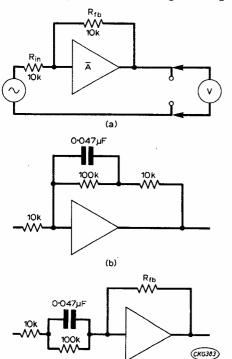


Fig. 77: (a) Simplified representation, with the symbols denoting an inverting amplifier. (b) a frequency-dependent development, and (c) the bass cut variation, with the frequency-selective portion before the feedback loop.

(c)

the input shown conventionally at the blunt end; the output at the sharp end (i.e., the 'arrow' points the way the signal is going). Fig. 77 is a simplified diagram, the letter A within its triangle denoting that it is an amplifier.

Previously you will have noted reference to an 'inverter'. By this, is meant that the input is 180° antiphase to the output. In Fig. 77, we see a bar over the A, denoting an inverter. For the benefit of old-timers like me, this can be regarded as exactly parallel to valve technology: a positive-going waveform at the grid produces a negative-going waveform at the anode.

If previous articles have been followed, it will be noted that the closed loop gain, which is the circuit gain calculated after feedback has been applied, is derived from the formula: $G_{\rm o}\!=\!R_{\rm fb}/R_{\rm in}$.

If we now make R_{in} equal to $10k\Omega$ and R_{fb} also $10k\Omega$, the closed loop gain is unity, i.e., 10/10. In practice, we shall measure 0.8 rather than 1. If, with R_{in} at $10k\Omega$ and R_{fb} at $100k\Omega$, giving a theoretical gain of 10, we were again to measure, we should find the answer more like 7.7. Carrying this experiment a little further—and please do not merely take our word for this; try it and see for yourself—we find that with R_{in} at $100k\Omega$ and feedback resistors varying between $10k\Omega$ and $1M\Omega$, the closed loop gain varies between 0.1, via 0.98 (at $100k\Omega$) and 5.8. Which only goes to prove that the actual gain is always less than calculated, and, secondly, the lower the circuit impedance, the greater the error.

Practically, therefore, it would seem that our circuit was not the best. But, as it is typical of the majority of commercial designs, we make no apology. It has to be remembered that the tone control circuitry does not have to contribute a lot of gain. We do not normally need a gain at any frequency of more than 'times 10', plus a stage gain of around 4, and so a maximum gain of about 40. Refinements will be added, never fear...

Reverting to Fig. 77(a) and making R_{in} $10k\Omega$, with a similar value for R_{fb} , we obtain a gain of 0.98, and the virtual earth point is at the junction of the two resistors. If we insert a resistor as shown at

Fig. 77(b) we reduce the gain somewhat, 0.96, but let's return to that later, the important point being that we can arrange the gain that we require by choice of $R_{\rm in}$ and $R_{\rm fb}$.

Here I part with Mike and assert that many modern circuits are resolved and arranged (rather than designed) by what are euphemistically called 'empirical methods'; more cynically described as 'hit or miss'. With the basis of existing circuits and a mass of mathematics that go to support them, the modern designer takes for granted the previous researches, and builds upon them. Exceptions, like John Linsley Hood, who question every fact and do their own research, are as rare as gold nuggets in a leadmine.

All of which digression leads me to Fig. 77(b). Here we have R_{in} at $10k\Omega$ with a similar feedback resistor R_{fb} in series with a $0\cdot 047\mu F$ capacitor (itself, practically, paralleled by $100k\Omega$). The impedance of the feedback network can, if you want to be meticulous, be calculated at any point in the frequency range.

This is all very fine, but, in practice, we can say that at very high frequencies the capacitor will be an effective short-circuit. In these circumstances, the circuit becomes effectively $R_{\rm in}/R_{\rm fb}$ having unity gain. Lowering the frequency raises the reactance $X_{\rm c}$ until it eventually becomes an open-circuit, and, in comparison with the $100 {\rm k}\Omega$ previously mentioned, the gain will be nearly 11. Theory gives us 110/10, practice a little less, hence my question-begging formula. We shall settle for a gain of around $20 {\rm dB}$, which is ten times the input voltage.

In the frequency range that C is effective we will have an impedance change in the feedback network giving us a slope of 6dB/octave. At frequencies below where unity gain is produced, the slope will flatten, so that further reduction of frequency does not change the output from unity gain. At frequencies above where the effective $R_{\rm fb}$ is $110k\Omega$, i.e., for a theoretical gain of x11, the curve again flattens. The transitions from slope to flat are not sudden and our dotted curves show the practical results obtained.

Turnover

Reference has already been made to ft, and by this we mean the turnover frequency, (in the case of Fig. 75 we have two turnover points, at 3dB positive or negative position on the curve, depending on the way the calculations are carried out, as should become apparent).

The f_t points can be calculated from the formula $f_t = \frac{1}{2\pi CR}$ where the frequency is in hertz; the

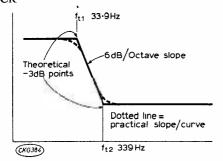


Fig. 78: The bass lift curve in theory (solid line) and in practice (dotted line).

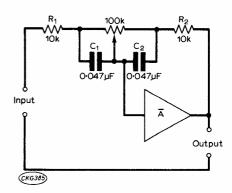


Fig. 79: A combined bass lift and cut circuit.

constant 2π can be taken as 6.28, C is in farads and R in ohms. Taking the component values of Fig. 77(b), we obtain a lower frequency turnover point of 33.9Hz while the upper frequency turnover point works out to 339Hz.

In practice, of course, the points are not definite. The plotted curve, as can be shown later, follows rather the dotted than the hard line of Fig. 78. Plotting the curve obtained from a 'hook-up' replica of Fig. 76, we get the actual curve of Fig. 78, from a generator with a 600Ω source impedance, and reading across the 'open' output with a high impedance valve-voltmeter. (Amendment, please: our habit these days is to use the battery-powered millivoltmeter so the use of the term 'valve-voltmeter' is mostly a matter of habit—although we certainly continue to use our old faithful instruments where the low value of hum and noise will not prove an embarrassment.)

One of the reasons for the smoothing of a theoretical curve is, of course, that other circuit considerations take effect. In theory, we take the two extremes, when the $0.047\mu F$ capacitor is in parallel with the $100k\Omega$ resistor and the $10k\Omega$ resistor is not effective, and when the capacitor is in series with the $10k\Omega$ resistor, the effect of the $100k\Omega$ resistor then being ignored. In practice, of course, it cannot be ignored: its real effect is to modify our $10k\Omega$ to $9k\Omega$ under these circumstances.

Taking the worked theoretical examples:

These figures agree very nearly with our practical measurements, This, from the curve of Fig. 78., gives us our Bass Lift circuit.

Bass cut

If we now reverse the networks $R_{\rm in}$ and $R_{\rm fb}$ as depicted in Fig. 77(c), we get an inverse of the previous curve. That is to say, we get bass cut instead of bass lift, because the feedback is now resistive, while the input circuit, up to the 'virtual earth point', is frequency-dependent.

Combining both these circuits, as in Fig. 79, we get bass cut and lift according to the position of the slider of the control. With the slider on the left, C1 is effectively short-circuited and we are left with

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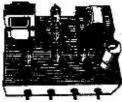
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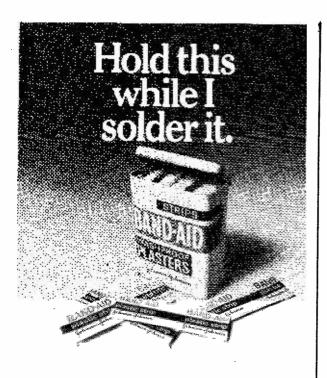
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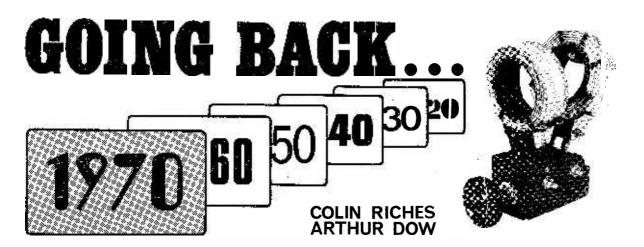
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UITE a large number of letters addressed to us involve queries or seek information on the date or origin of bits and pieces of old wireless equipment or valves. So this month we thought that we would try to give some very broad indications of the form of construction and appearance of domestic wireless sets at the interesting stage of their development. This should enable readers to date a piece of apparatus, if called upon to express an opinion, or if an interesting bit of gear is found in a junkshop.

History

From the turn of the century when Marconi was experimenting with the first tuned spark transmitter, until 1922 when the first official broadcast was made and valve circuits had been developed to the extent that they were no longer regarded as freak, the amount of equipment produced was comparatively small and that which remains is mostly in safe hands.

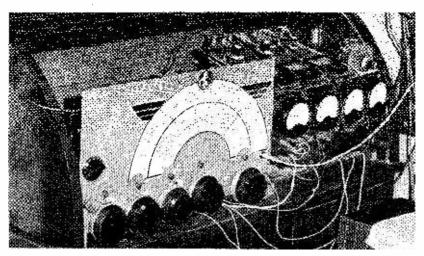
Once broadcasting had begun the boom in home constructed receivers got under way very rapidly since there were few commercial receivers available at that time. It is this period from about 1922 until the mid-30's that is probably of most interest to

those who specialise in collecting vintage wireless equipment and with which we will concern ourselves here.

Components

There were many firms supplying components such as coils and holders, tuning condensers, audio transformers and valves as well as ebonite panels and associated hardware. Basket-wound or wave-wound coils were frequently home-made and plugged into holders which were adjustable from the panel to vary the coupling between the coils. Resistors looked like cartridge fuses and were pushed in to clips. The grid-leak was often changed to suit the 'softness' of the detector valve or it might be a panel-mounted variable resistance.

'Spaghetti' resistors had the resistance wire wound on a flexible core and looked like a piece of string with end tags. These could be connected directly between terminals of components. Most components such as audio transformers, valveholders and condensers etc. had terminals, usually 6BA, often with a soldering tag. Sets of this period were characterised by the great effort that went into the wiring up.



We don't want to start an argument but we think that Mr. A. Rea of Hull could be our oldest reader, at 80 years plus. Wireless is still his hobby and he is very proud of the John Scott-Taggart ST900, shown above, built many years ago, probably about 1937. He can feed the output of the receiver into a tape recorder or into a valved amplifier using a pair of PX25's which feeds no less than five loudspeakers around the place.

Square sectioned copper wire was common, always arranged with neat corners or angles and straight parallel runs and neat loops under the terminals. The need for short, direct wiring was not appreciated then, and indeed, was probably of little importance where only medium and long waves were concerned and stage gains were very low.

Construction

Such receivers were built on a wooden baseboard to which the components were fixed with woodscrews and an ebonite panel was fixed to one edge of the board. Along the back edge was a row of terminals, mounted on a strip of ebonite, for connecting the set to the accumulator, high tension battery, grid bias battery, aerial and earth and headphones or speakers. Incidentally, the cabinets for these sets were also given a great deal of attention and often were works of art in themselves to ensure that they fitted in with the rest of the furniture. Indeed, the receiver was often built in to an existing piece of furniture. The panels of sets of this period were a mass of knobs and controls with possibly a rheostat for each filament, variable grid-leaks, tuning condensers for each stage, coil coupling controls and reaction controls. Later, when shorter wavelengths were in use, metal panels were employed in order to prevent 'hand capacity' effects which upset the rather critical tuning.

Balves

Valves can be dated fairly accurately from a study of their physical characteristics. At the beginning of the period we are discussing, say 1922-24, the Marconi-Osram R valve was common along with the Mullard ORA and the Cossor P1 all of which were bright emitters with tungsten filaments. Generally they had a metal sleeve base and a pinch on top of the glass envelope, formed during the evacuation process. 1924-25 saw the introduction of the dull emitter valves using oxide-coated filaments such as the MO DE5, Mullard DO6 and the Cossor WR1. These valves still had the pinch on top but the bases were the more familiar moulded type.

Between 1925 and 1927 saw the advent of the now famous Mullard PM range of valves which were dull emitters with filament voltages from two to six volts. The pinch was now concealed in the base of the valve thus eliminating a very vulnerable feature of the older valves.

The first 'mains' type valves emerged in 1927 with the heaters, usually four volts, being run from a mains transformer instead of accumulators or batteries. In the early 30's r.f. type valves appeared with sprayed-on metallic coating for screening purposes and the glass envelopes, especially for the audio amplifier valves, developed a waisted section at the top of the envelopes intended to support the mica discs of the electrode assembly and thus reduce any tendency to microphony.

For those that are really interested in these old radios there is no finer pastime than trying to get one of them to work even if it means using equivalent modern components as replacements for faulty parts. Our CQ column is open to those readers who wish to appeal to other readers for old components if it is felt that only a 100% genuine vintage receiver is acceptable.

TRANSISTOR CIRCUITRY FOR BEGINNERS-

continued from page 72

the effective bass lift circuit of Fig. 77(b). With the slider to its right we get the alternative condition, with C2 short-circuited and the bass cut circuit of Fig. 77(c).

Balance

Take the case of the slider at its middle position. Then, the input and output circuits are identical and balanced. That word, BALANCED is important. It is the basis of the Baxandall tone control circuit—one of the most elegant solutions to an audio problem yet posed, and not to be under-rated. In the full circuit, the impedance change with the slider control moved (a change in frequency-dependence, looked at in the basic way of our approach) is exactly balanced with the movement of the slider in the other

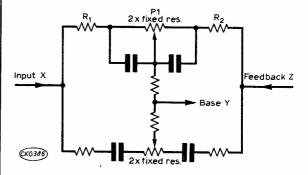


Fig. 80: The eventual network to be inserted in the feedback loop, giving bass and treble lift and cut.

section of the ganged potentiometer. It remains only that the ganged potentiometers themselves shall be within at least 1dB of linearity.

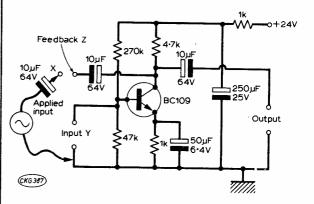


Fig. 81: The basic amplifier circuit over which the feedback is applied.

From the simple experiments we have already carried out, we know that when the input resistance, $R_{\rm in}$ is equal to the feedback resistance $R_{\rm fb}$, then the theoretical gain is unity. In practice, findings are not far removed from the theoretical. At intermediate positions of the sliders, we shall get variations from the theoretical norm, between maximum bass and maximum cut.

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1000pf	q0f	4700pf	10p
2200af	10p	10,000pf	10p

Ceramic	- plate	63V (C3	33)
1-8pf	8-2nf	33pf	120pf
2-2pf	10pf	39pf	150pf
3-3pf	12pf	47pf	180pf
3-9pf	15pf	56pf	220pf
4-7pf	18pf	68pf	270pf
5 -6pf	22pf	82pf -	330pf
6-8pf	27pf	100pf	
ali 5p. e	ach		

mylar fi	lm		100V		
1000pf 2000pf 5000pf	2p 2p 2p	·01μF ·02μF ·04μF ·05μF	3p 3p 3p 3p	-068μF -1μF -2μF	4p 4p 5p

10pf to 10,000 47 & 68.	pi ii: iiiuiii	hies n		each
metallised p	olyester	25	0V (C28	0)
·01μF 3p	·068µF	34p	·47µF	8p
-015μF 3p	·1µF	4p	-68µF	11p
022μF 3p	-15μF	40	1uF	13p
033μF 3p	-22μF	5p	1.5µF	20p
047uF 3p	·33µF	81p	2 2 uF	24p

		- 2.		
metallised	polyester		400V (C28	81)
·01µF 41p	047µF	6p	22µF	10p
015µF 41p	-068µF	6p	33µF	140
022 IF 41p	1µF	7p	47µF	150
033 JF 51p	-15uF	80		

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Type SD.541	05.3	mm x 85mm ri	ronts
50uA	£2.60	500mA	£2.35
	£2.55	1 amp	£2.35
100uA	£2.55	5 amp	42.35

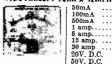
Type SD.460 46mm x 59.5mm Fronts 50 uA £2.40 1 7 amp.

50-0-50µA	£2.35	5 amp	£2-18
100μΑ	£2:35	10 amp	
100-0-100µA	£2:35	5V. D.C	£2:18
$200\mu A$	£2.35	10V. D.C.	£2·1
500μA		20V. D.C	
ImA	£2·15	50V. D.C	
5mA	£2·15	300V. D.C.	
10mA	49.15		
50mA		15V. A.C	£2.30
100mA		300V. A.C	£2-30
500mA	£2·15	VU Meter	£2.5

*MOVING IRON-ALL OTHERS MOVING COIL

Please add postage

Type MR.85P. 41in. x 41in. fronts



The limbor. 4 till. X 4till. Hones			
The second secon	50mA	£3·10	
100	100mA	£3.10	
	500mA	£8·10	
1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	1 amp	£3·10	
T. March	5 amp	£3-10	
A Contract of the Contract of	15 amp	£3·10	
36	30 amp	£3.20	
6 ** 0 TO 10 10 10 10 11 11 11 11 11 11 11 11 11	20V. D.C.	£3-10	
	50V. D.C.	£3-10	
50μA £3.95	150V. D.C.	£3 10	
50-0-50μA £3·40	300V. D.C.	£3.10	
100µA £8:40	15V. A.C	£3-10	
100-0-100µA £3 30	300V. A.C	£3.10	
200μA £3-30	S Meter 1mA	£3.15	
500μA £3·20	VU Meter	£3-95	
500-0-500μA £3·10	1 amp. A.C.*	£3.10	
1mA £3·10	5 amp A.C.*	£3-10	
1-0-1mA £3:10	10 amp. A.C.*	£3.10	
5mA £3·10	20 amp. A.C.*	£8-10	
10mA £8-10	30 amp. A.C.*	£3.10	

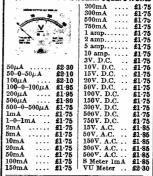
I Type mk.	34P. 48	in. square fronts
50μA	£3-40	10V. D.C £2.20
50-0-50μA	£2.85	20V. D.C £2.20
100μΑ	£2.85	50V. D.C £2.20
100-0-100μA	£2.75	300V. D.C. £2.20
500μA	£2.55	15V. A.C £2.30
1mA	£2-20	300V. A.C £2:30
5mA	£2-20	S Meter 1mA £2.30
10mA	£2.20	VU Meter £3.50
50mA	£2-20	1 amp. A.C. * £2.20
100mA	£2-20	5 amp. A.C. * £2.20
500mA		10 amp. A.C. *£2.20
1 amp		20 amp. A.C. * £2.20
5 amp	£2-20	30 amp. A.C. * £2.20

Type MR.65P. 31in. x 31in. fronts

	50μΑ	£3.70	10V. D.C £2.40
	50-0-50µA	£3.00	20V. D.C £2.40
	100μΑ	£3.00	50V. D.C £2.40
	100-0-100µA	£2.90	150V. D.C. £2.40
	200μΑ	£2.90	300V. D.C. 42-40
	500μA	£2·65	15V. A.C £2.55
	500-0-500μA	£2·40	50V. A.C £2 55
i	1mA	£2-40	150V. A.C £2.55
į	5mA	£2-40	300V. A.C £2-55
ı	10mA	£2-40	500V. A.C. £2-55
İ	50mA	£2-40	8 Meter ImA £2.60
ļ	100mA	£2-40	VU Meter £3.70
ì	500mA	£2-40	50mA A.C. * £2.40
١	1 amp	£2.40	100mA A.C. * £2.40
	5 amp	£2·40	200mA A.C. * £2.40
Į	10 amp	£2-40	500mA A.C. *£2.40
i	15 amp	£2-40	1 amp. A.C. * £2-40
i	20 amp	£2-40	5 amp. A.C. * 22.40
ı	30 amp	£2.55	10 amp. A.C. * £2.40
ı	50 amp	£2.75	20 amp. A.C. * \$2.40
ł	5V. D.C	£2-40	30 amp. A.C. * £2.40
1	0172.0	WW 20 .	50 amp. A.C. 22-40

Send for illustrated brochure on SEW Panel Meters—discounts for quantities.

Type MR.38P. I 21/32in. square fronts



Type MR.45P. 2in. square fronts

S Meter 1mA VU Meter ...

OULA	20.00	n wind" 27.90
50-0-50μA	£2.30	10V. D.C. £1.85
$100\mu A$	£2:30	20V. D.C £1.85
100-0-100µA	£2·05	50V. D.C £1.85
200µA	£2.05	300V. D.C. £1.85
500μA	£1.95	15V. A.C £2.00
500-0-500µA	£1.85	300V. A.C £2-00
lmA	£1.85	S Meter 1mA £2.05
5mA	£1.85	VU Meter £2.50
10mA	£1-85	1 amp. A.C. * £1.85
50mA	£1.85	5 amp. A.C. * £1.85
100mA	£1.85	10 amp. A.C. * £1.85
500mA	£1.85	20 amp. A.C. * £1.85
i amp	£1.85	30 amp. A.C. * £1.85



"SEW" EDGWISE METERS Type PE.70. 3 17/32in. x 1 15/32in. x

Zzin. deep			
50μA		500μA	£3.05
50-0-50μA 100μA	£3·30 £3·30	1mA	£2·70
100-0-100µA	£3.20	300V. A.C	
2 0 0μA	£8·20	VU Meter	£8·75

"SEW" BAKELITE PANEL METERS

Type MR.65. 31in. square fronts



25μA 50μA 50-0-50μA

100μA 100-0-100μA

500μA 500-0-500μA 1mA 1-0-1mA

5mA ... 10mA 50mA 100mA 500mA

£1.85

4	50 amp,	£2·15
8	5V. D.C	£2·15
	10V. D.C	£2-15
	20V. D.C	£2·15
	50V. D.C	£2·15
	150V. D.C.	£2·15
	300V. D.C.	£2·15
8.85	50mV. D.C.	£2.40
1.00	100mV. D.C.	£2.40
60	30V. A.C. *	£2.20
.60	50V. A.C. *	£2.20
-50	150V, A.C. *	£2.20
-45	300V. A.C. *	£2.20
15	500mA A.C. *	£2·15
15	1 amp. A.C. *	£2.15
15	5 amp. A.C. *	£2·15
.15	10 amp. A.C.	
15	20 amp. A.C. *	
15	30 amp. A.C.	£2.15
15	50 amp. A.C. *	£2.15
15	VU Meter	£3-40

Type S-80 80 mm. square fronts

ь А	£3.50	
-050µA	£3.40	- 8
)μΑ ˙	£3.40	- 1
0-0-100µA	£3.30	- 3
$\mu_{\mathbf{A}}$	£3.05	. 3
À	£2.85	- 1
V. D.C	£2.85	1
V. D.C	£2-85	5 a
OV. D.C.	£2 85	300
mn D.C	20.02	***

£2



"SEW" EDUCATIONAL **METERS**



Type ED.107. Size overall 100mm x 90mm x 108mm

A new range of high quality moving coil instruments ideal

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meter movement is easily accessible to demonstrate internal working. Available in the following ranges:

1-0-1mA	£5.50 £5.10 £4.85 £5.10 £4.85	50V. d.c 300V. d.c Dual range	£4-85
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Tests PNP or NPN transistors. Audio indication. Operates on two 1-5v batteries. Complete with all instructions and the second of
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P. & P. 20 p.

High quality ceramic construction. Windings embedded in vitreous enamel. Heavy duty brush wiper. Continuous rating. Wide range ex-stock. Single hole fixing, \$in. dia. shafts. Bulk quantities available. 25 WATT. 10/25/50/100/250/500/1000/2500 or 5000 ohms. \$00p. P. & P. 10p. 50 WATT. 10/25/50/100/250/500/1000/2500 or 5000 ohms. £1-15 P. & P. 10p. 100 WATT. 1/5/10/25/50/100/250/500/1000 or 5000 ohms. £1-16 P. & P. 15p. 150

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S-260 General Purpose Bench Mounting





S-260B Panel Mounting 1 Amp 2.5 Amp

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VOLTS
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Solid state. Variable output 5-20 voit D.C. up to 2 amp. Independent meters to monitor voltage and cur-rent. Output 229/240 V. A.C. Size 74" × 54" × 34". £14.97. P. & P. 25p.



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Built in gearbox. All brand new and boxed. 30 RPH CW; 2 RPH CW; 20 RPH CW; 2 RPH ACW; 30 RRH CW; 50p each Post 12p.



from 9v battery. Com-nlete with all in-structions, etc. £3.95. P. & P. 20p. HOMER INTERCOMS

Tests ICO and B. PNP / NPN. Operates

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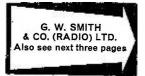
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Ideal for home, office, stores, fac-tories, etc. Supplied complete with batteries, cable as free instructions. and

2 Station, £2.97, 3 Station £5.25, P. & P. 15p. 4 Station £6.62, P. & P. 17p.

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0/115/250V. shrouded.	Step up or	step down. Fully
80 W	£2·10	
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Input 88 125 VAC or 176 250VAC. Output 120V AC. or 240 VAC. 200 VA rating. £11.97, carr. 50p.



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Moving Coil. Ideal for language teaching, com-munications. Headphone imp. 16 ohms. Micro-phone imp. 200 ohms.



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20,000 O.P.V. Overload protection 5/25/100/500/1000 VDC. 10/50/250/1000 VAC. 50/LA/250mA. 20K/2 meg ohm. -5 to +62db. £4-97. P. & P. 15p.



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MULTITESTER
High sensitivity tester.
200,000 o.p.v Overload
protection. Mirror scale.
Ranges: protection. Mirror scale. Ranges: 0 / 06 / 3 / 3 / 30 / 120 / 600 / 1200V. D.C. 0 / 3 / 12 / 60 / 300 / 11, 200V. A.C. 0 / 61AA / 1.2mA / 120mA/ 600mA / 12A. D.C. 0 / 12A. A.C. - 20 to + 63dB. 0 / 2K / 200K / 2 meg / 200 meg objess.

200 meg ohms. £16.95. Post 30p

MODEL TE-200

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O.P.V. Mirror scale, overload protection, 0/5/25/125/1,000V. D.C. 0/10/50/250/1,000V. A.C. 0/50 μA/250 mA. 0/60K/6 meg Ω. -20 to +62db. 43-95. P. & P. 15p.



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30,000 O.P.V. with overload protection mirror scale
0/56/2-5/10/25/100/25/100/25/500/2
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2 amp. D.C. 0/60/K/6 Meg./
60 Meg Ω
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00,500 o.p.v. Mirror Scale,
00,502-5/10/500/1000 v

D.C. 10/25/250/1000 V. A.C. 0/25/250/250 MA/
10/250/4A/25/25/250 MA/
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20MEH/20 MEG. - 20 +62db.
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0/100mA/1/10 Amp AC 0/5K/50K/500K/5 MEG/ 50

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100mA/1A; /1A: Resistance ohms/3/30/300K/3m Ω . Complete with batteries. test leads, instructions and sturdy steel carrying case.

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Completely portable, simple
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Ranges 0/8/30/800V AC
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10 / 50 / 100 / 500 / 1000V.
A.C. 50µA / 250mA. 6K / 6



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20k Ω/Volt D.C. 8k Ω/ Volt AC. Mirror scale. -6/3/12/30/120/600 V D.C. 3/30/120/600 V A.C. 50/600μA/60/600 mA. 10/100K/1 Meg/10 Meg Ω -20 to +46db. 26-97. P. & P. 12p.



TMK MODEL TW-50K
46 ranges, mirror scale,
50 K/Vol. D.C. 6K/Volt A.C.
D.C.: Volta 125, 26 1.25,
25, 5, 10, 25, 50, 125, 250,
500, 1000V, A.C. Volts: 1.6,
3, 6, 10, 25, 50, 125, 250,
1000V. D.C. Current: 25,
50 LA, 2-5, 5, 25, 50, 250,
500mA, 5, 10 amp. Resistance:
10 K, 100 K, 1 MEG, 10 MEG
CD. Decibels: -20 to +81·5db
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K228A
Taut band
suspension.
Overload
protection.
Polarity
reversing
switch. 30,000 o.p.v.
500 / 1000 / 2500 V. D.C. 0 / 15 / 50 / 150 /
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120/300/600/1200/00/00/
120/300/600/01/200/00/00/
1200 V. A.C.
15/30/12/30/60/150/300/600/
1200 V. A.C.
15/30/12/3/3/6/30/60/150/300mA
6/12 AMP. DC. 2K/200K/2
Mg/20 Mg ohm -20 to
+63dB. £13-50. P. & P. 20p.



MODEL C-7080 EN Giant 6" mirror scale. 20,000 a,p.v. 0 / :25 / 1 / 2-5 / 1 0 / 50 / 256 / 1000 / 5000 V. D.C. 0 / 2-5 / 100 / 5000 V. D.C. 0 / 2-5 / 100 / 500 / 25 / 250 / 1000 / 5000 V. A.C. 0 / 50µA / 1 / 10 / 100 / 500mA / 10 amp. D.C. 0 / 2K / 200K / 20 meg - 20 to + 50 dB.



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U4312 MULTIMETER Extremely sturdy instru-electrical use. 667 o.p.v. 0/3/1-5/7-5/30/60/150/300/ 600/900 VDC and 75mV. trument for general 0/-3/1-5/7-5/30/60/150/300 600/900 VAC. 600/900 VAC. 0/300μA/1-5/6/15/60/150 600MA/1-5/6 AMP. D.C. 0/1-5/6/15/60/150/600MA/ 1-5/6 AMP. AC. 0/200 Ω/3K/30K Ω.



0/2001/3R/30A M. Acturacy DC 1%. AC 1-5%. Knite edge pointer, mirror scale. Compl. te with sturdy metal carrying case, leads and instructions. 29-50 plus P. & P. 25p.

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Full capabilities for measuring A, B and ICO. NPN or PNP. Equally adaptable for check-ing diodes. Supplied complete with instructions, battery and leads. £7.50. Post 20p.



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100,000 o.p.v. mirror scale/ overload protection. 0/12/ 6/3/12/30/12/0900 v Do-0/6/30/12/0/600. V AC. 0/12/ 600µA/ 12/300mA/12 AMP DC. 0/10 K/1 MEG/100MEG. —20 to +50db. 0·01~2 MFD. Transistor tester measures Alpha, beta and Ico. Complete with batteries, instructions with batteries, instruction and leads. £13.50. P/P 25p.

A. (164. ft.)



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Checks true A.C. beta in / out. Checks Icbo. Checks diodes in / out. Checks SCR, etc. Beta HI 10 - 500.

HI 10 - 500, LO 2 - 50. Icbo 0-5000μA. 220/240 V A.C. operation £17.50. Post 25p.



Input impedance 10 meg

omms.
Ranges:
0 / 25 / 1 / 2.5 / 10 / 50/
250 / 1000V. D.C.
0 / 2.5 / 10 / 50 / 250 /
1000V. A.C.

1000V. A.C.
0 / 25μA / 2·5 / 25 / 250
MA D.C.
- 20 to + 62dB
0 / 5K / 50K / 500K / 5meg/
500meg ohms.
214-95. Post 30p



Input impedance 10 meg ohms. 0 / 3 / 1·2 / 6 / 30 / 120 / 600V. D.C. 0 / 3 / 12 / 60 / 120 / 600V. A.C. 0 / 120µA / 120mA D.C. 0 / 1K / 100K / 10 meg /100 meg ohms £15-97. Post 15p.



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CI-5 PULSE OSCILI OSCOPE

OSCILLOSCOP:
For display of pulsed and periodic waveforms in electronic circuits.
VERT. AMP. Bandwidth 10MHz. Sensitivity at 100KHz VEMS/mm. 3-25;
Preset triggered sweep 1-3,000usec.; free tunning 20-200,000HZ in nine ranges. Calibrator pips. 220 × 360 × 430mm. 115-230V. AC operation.
339-00. Carr. paid.

TO-3 PORTABLE OSCILLOSCOPE



3 in, tube, Y amp, Sensitivity 0-1v p-p/CM. Bandwidth 1-5 cps-1-5 MHz. Input imp, 2 meg Ω 25pF X amp, sensitivity 0-9v, p-p/CM. Bandwidth 1-5cps-800kHz. Input imp, 2 meg Ω 20pF, Time base, 5 ranges 10 cps 300 kHz. Synchronization.

Sol KHZ. Synchronization.
Internal/external. Illuminated
scale 140×215×330 mm. Weight 154b.
220/240V. A.C. Supplied brand new with
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5 mc/s Pass Band. Separate
Y1 and Y2 amplifiers.
Rectangular 5in. × sin.
Rectangular 5in. × sin.
CR.T. Calibrated triggered sweep from 2 u/sec.
to 100 mill-sec. per compression of the calibrator. Supplied complete with all accessories and instruction manual
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GENERATOR
Franges 400k Hz-30raHz.
An inexpensive instrument for the handyman.
Operates on 9v battery.
Wide easy to read scale.
800kHz modulation.
828 v. 22 v. 348 v.

52 × 52 × 32 in. Complete with instructions and leads. £7.97. Post 25p.



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MEASURING BRIDGE

A new portable bridge offering excellent range and couracy at low cost. Ranges: R.

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6 Ranges ± 19.

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HENRYS 6 Ranges ≥ - % C.10pF ± 1110mFd

1. 1/100. 6 Ranges ± 1%. Bridge voltage at 1,000 cps. Operated from 3 volts. 100μA.

Meter indication. Attractive 2 tone metal case. Size 7‡ × 5×21. \$20. P. & P. 25p.

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GRID DIP METER
Transistorised. Operates as
Grid Dip, Oscillator, Absorption Wave Meter and Oscillating Detector. Frequency
range 440Kc/s-290Mc/s in
6 coils. 500µA Meter. 9V
battery operation. Size 180 ×
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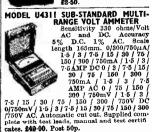
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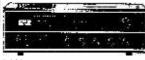


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Standard, 2" long × 4" diameter. This will break currents of up to 1A, voltage up to 250V. Price 10p cash 90n par dozen.

currents of up to 1A, voltage up to 250V. Price 10p each, 90p per dozen.

Flat. Flat type, 2" long, just over \(\frac{1}{2}\) thick, flattened out, so that it can be fitted into a smaller space or a larger quantity may be packed into a square solenoid. Rating 1A 200V. Price 30p each 43 per dozen.

Small ceramic magnets to operate these reed switches 9p each, 90p dozen.

Dyr Reed Relays. Solenoids on moulded bobbins within magnetic shields—printed circuit, or panel mounting.

mount	ing.		
Ref.	Coil Resistance	Reed Switches	Price
71005	2 K	1 normally open	25p
81916	5 K	1 normally open	
		1 normally closed	75p
05003	4 K	l normally open	25p
62040	1500 & 500 ohms	1 normally open	35p
		ef. 53001. Contains	
mally	open reeds within	in a solenoid. Opera	ates on
600 m	W. Coil resistan	ce 9K ohms. Price	£1.95

Multiple Reed Relay, Ref. 631. 2 normally open 1 normally closed coil resistance 30 chms. Price 75p.

MULLARD AUDIO AMPLIFIERS



All in module form, each ready built comple heat sinks and connection tags, data supplied. Model 1153 500mW power output 65p. Model 1172 750mW power output 85p.
Model EP9000 4 watt power output £1.65.
EP9001 twin channel or stereo pre amp. £1.60
10% discount if 10 or more ordered.

CENTRIFUGAL BLOWER
Miniature mains driven blower centrifugal type blower unit by Woods. Powerful but specially built for quiet running—driven by cushioned induction motor with specially built low noise bearings. Overall size $44'' \times 41'' \times 41'' \times 41''$ when mounted by flange, air is blown into the equipment but to suck air out, mount it from centre using clamp. Ideal for cooling electrical equipment or fitting into a cooker hood, film drying cabinet or for removing flux smoke when soldering etc., etc. A real bargain at 21.85.





GOOD COMPANION I.C. VERSION

We can now offer these again in I.C. version using Ferranti
ZN414 and Mullard AF Module 1172. Cabinet size approx. ZN414 and Mullard AF Module 1172. Cabinet size approx 11in. wide \times 8in. high \times 3in. deep. Complete assembly instructions—Excellent tone wood cabinet £5.75 + 25p

MIGHTY MIDGET
Probably the tiniest possible radio, as described in Practical Wireless, January '73. All electronic parts \$2 post paid.

THIS MONTH'S SNIP

10 AMP DIMMER/CONTROLLER

For the control of lighting of stage or studio or portable equipment in workshops etc. This has socket outlets each controlled by 5 AMP Solid State regulator. Also fitted with master switch fuse and neon indicator and terminating with 6 feet of flex. Overall length 17in. 3½in. x 1½in. deep. £7.50, plus 25p P. & P.



PORTABLE ELECTRIC DRILL

Very superior quality made by a famous Dutch Toolmaker. Model No. ASM 830. 300w - 2 speed 2290/3900. With ¾" chuck 830. 300w - 2 speed 2290/3900. With ¾" chuck achuck key, also separate side handle and chuck key, also separate side handle and hammer facility for dealing with concrete, etc. An equivalent British made drill would cost that without the hammer attachment £7.95. Have either model on approval for 7 days.



DISTRIBUTION

PANELS

Just what you need for work bench or lab. 4 × 13 amp, sockets in metal box to take standard 13 amp, fused plugs and on/off switch with neon warning light. Supplied complete with 7 feet of heavy cable. Wired up ready to work, £2.25 20p post and ins.

CAPACITOR DISCHARGE CAR IGNITION



This system which has proved to be amazingly efficient and reliable was first described in the Wireless World about a year ago. We can supply kit of parts for an improved and even more efficient version (Practical Wireless, June). Price 25-95 plus De-luxe model including pilease state whether for positive or negative systems.



24-HOUR TIME SWITCH

24-HOUR TIME SWITCH Made by Smiths, these are AC mains operated, NOT CLOCKWORK. Ideal tor mounting on rack or shelf or can be built into box with 13A socket. Two completely adjustable time periods per 24 hours, 5A changeover contacts will switch circuit on or off during these periods. 28-50 post and ins. 25p. Additional time contacts 60p pair.

THYRISTOR LIGHT DIMMER

For any lamp up to 1kw. Mounted on switch plate to fit in place of standard switch. Virtually no radio interference. Price \$2.95, plus 20p post and insurance. Industrial model 5A \$2.



BATTERY CONDITION TESTER BATTERY CONDITION TESTER Made by Mallory but suitable for all batteries made by Ever Ready and others, most of which are zinc carbon types but also mercury manganese—nicad—silver oxide and alkaline batteries may be tested. The tester puts a dummy load on the battery and the meter scale indicates the condition depending upon which section the pointer rests. The section reads "replace" "weak" or "good". The tester is complete in its case, size 3½" × 6½" × 2" with leads and prods. Price \$2.25 plus 20p postage.

SPIT MOTOR



200-250v Induction Motor, driving a carter gear box with 1½" of output drive shaft running at 5 revs per minute. Intended for roasting chickens, also suitable for driving models—windmills, coloured disc lighting effect, etc. etc. £1.85 plus 20p post and insurance.

TERMS: 10% discount if ten of an item ordered, send postage where quoted—other terms, post free if order for these over £6.00 otherwise add 20n.

CONTROL DRILL SPEEDS

DRILL CONTROLLER NEW IKW MODEL

Electronically changes speed from approxi-mately 10 revs. to maximum. Full power at all speeds by finger-tip control.

Kit includes all parts, case, everything and full instructions. £1.50. 13p post and p.

Made up model also available.

MAINS TRANSISTOR POWER PACK

PACK
Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit comprises: mains transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip only £1.

SWITCH TRIGGER MATS



So thin is undetectable under carpet but will switch on with slightest pressure. For burglar alarms, shop doors,

etc. 24" × 18" £1.40 13" × 10" £1.00

PP3 BATTERY CHARGER
Almost 3 times the life can be obtained from PP3 battery if you re-charge it from the mains—this ready to use charger with instructions only 50p.



15A ELECTRICAL

Heart in your sleep:
All these and many
other things you can do
if you invest in an electrical programmer. Clock
by famous maker with 15 amp. on/off switch.
Switch on time can be set anywhere to stay on
up to 6 hours. Independent 60 minute memory
jogger. A beautiful unit. Frice £1.95 + 20p p. & p.
or with glass front, chrome bezel, 75p extra.

BAKELITE INSTRUMENT
CASE
Size approx. 6½" × 3½" × 2½"
deep with brass inserts in four
corners. This is a very strong case
eultable to house listruments and special rigs, etc. Price 45p each. Fixolin lid 10p extra.



TELEPHONES

RADIO ALARM CLOCK, LAMP DIMMER, INTERCOM-AMPLIFIER, LIGHT POWERED RADIO, BABY ALARM, TWO TONE DOOR BELL, TAPE TUNER, WATER LEVEL DETECTOR.
To receive kits for these and other projects featured in this issue send S.A.E. for PW Kits List.

ROCKER SWITCH
13 amp self-fixing into an oblong hole.
Size approximately 1" × \mathbb{1}" Sp each,
10 for 72p.



SLIDE SWITCHES



Slide Switch. 2-pole changeover panel mounting by two 6B.A. serews. Size approx. In × iin rated 250V lamp. 6p each. 10 for 54p. 100 for £510, 500 for £24. Ditto as above but for printed circuit 5p each, 10 for 65p, 100 for £425. Sub Ministers Slide Switch, DPDT 19mm

(\$\frac{1}{2}\$in approx.) between fixing centres. 18p each or 10 for \$1.08. SP Change over spring return 250v 1 amp. 10p.



SPRING COIL LEADS as fitted to telephones, 4 core 15p each, 10 for £1.35.3 core 10p each 10 for 80p.

V.A.T. Please add V.A.T. 10% on total order after April 1st.

J. BULL (ELECTRICAL) I

(Dept. P.W.) 7 Park Street, Croydon CRO IYD Callers to: 102/3 Tamworth Road, CROYDON

BSR LATEST SUPERSLIM STEREO & MONO

Plays 12", 10" or 7" records. Auto or Manual. A high quality unit backed by BSR reliability with 12 months' guarantee. AC 200/250v. Size 18\(\frac{1}{2}\) > 11\(\frac{1}{2}\)in Above motor board 8\(\frac{1}{2}\)in. Below motor board 2\(\frac{1}{2}\)in.



with STEREO and MONO XTAL £8-25 Post 250

ANOTHER RCS BARGAIN!
4 TRANSISTOR MONO AMPLIFIER
Powerful 8 watts output, 15 ohm. AG mains operated with
transformer 3-Controls, volume, treble, bass and On/Off
switch with knobs. Ready made on printed circuit board.
Fused inputs and outputs. Famous make,

Size 8" wide × 4" deep × 3" high. Price £5.95 post 25p.

Suitable 7" × 4" Speaker £1:00.

RCS DE-LUXE 3 WATT AMPLIFIER. Ready made, tested. Printed circuit. 3 watts output. Tone and volume controls. Complete with output valve and rectifier, two knobs, and high performance londspeaker, Double wound fully isolated mains transformer. A.C. mains 200/250V. Response 50-12,000 cps. Sensitivity 300mV. £4 Post

BSR SINGLE PLAYER

Heavy duty 4-speed motor with separate pick-up arm fitted LP 78 stereo compa- £5.50 tible cartridge.



HI-FI PICK UP CARTRIDGES. Stereo/Mono 9TA £2:50; GP94 £2:50; GP93 £2. Sapphire Mono GP91 £1:50; Powerpoint LP/78 60p

GARRARD DECCA DISCO DECK

Single play Stereo/ Mono Deram transcription head and arm. Four speeds. 10\forall in. turntable. Anti-rumble filter. Bias compensation aboratory motor.



METAL PLINTH AND PLASTIC COVER

Cut out for most Garrard or B.S.R.

Most will play with cover in position.

12\(\frac{1}{2} \times 14\(\frac{1}{4} \times 7\(\frac{1}{2}\) in.

Covered in black leatherette.

ALSO AVAILABLE IN SOLID NATURAL MAHOGANY WAX POLISHED FINISH—AT SAME PRICE

SPECIAL OFFER! SMITH'S CLOCKWORK 15 AMP TIME SWITCH

Single pole two-way Surface mounting with fixing screws. Will replace existing wall switch to give light for return home, garage, automatic anti-burglar lights etc. Variable knob Turn on or off at full or intermediate settings. Two types available 0 to 60 minutes or 0 to 6 hours. Fully insulated. Makers last list price \$4.50. Brand new and fully guaranteed.

OUR PRICE 21.50 P. & P. 15p or 23 pair. (STATE TYPE A OR B WHEN ORDERING.)

BLANK ALUMINIUM CHASSIS. 18 s.w.g. $2 \pm in$, sides. $6 \times 4 \pm in$, 45 p; $3 \times 6 \pm in$, 53 p; $10 \times 7 \pm in$, 65 p; $12 \times 8 \pm in$, 85 p; $14 \times 9 \pm in$, 90 p; $16 \times 6 \pm in$, 90 p; $12 \times 3 \pm in$, 50 p; $16 \times 10 \pm in$, £1. 14 \times 611. 169; 10 \times 611. 159; 12 \times 611. 169; 18 \times 611. 159; 14 \times 611, 169; 10 \times 711. 199; 12 \times 611. 299; 12 \times 611. 289; 16 \times 611. 289; 14 \times 911. 349; 12 \times 121. 409; 16 \times 1011. 509.

1		
i	RADIO BOOKS (Post 3p)	
1	Handbook of transistor equivalents	40p
ı	Handbook of Simple Transistor Circuits	35p
1	Master colour code folder	15p
1	Boys' book of crystal sets and simple circuits	18p
1		TOD
1	Universal gram motor speed indicator	8p
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į		75p
1	Hi Fi, PA and Disco Amplifier Design	
1	Practical Transistor Novelty Circuits	40p
Į	Resistor colour code disc calculator	
	Engineers' and Machinists' reference tables	20p
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R.C.S. STABILISED POWER PACK KITS R.C.S. STABLISED POWER PACK KITS
All parts and instructions with Zener Diode, Printed Circuit,
Bridge Rectifiers and Double Wound Mains Transformer.
Input 200/240v a.c. output voltages available 6 or 9 or 12
or 15 or 13 or 20V d.c. at 100mA or less.
PLEASE STATE VOLTAGE REQUIRED. £2.20 Post
Details S.A.E. Size 33 × 1½ × 1½ n. 15

R.C.S. GENERAL PURPOSE TRANSISTOR PRE-AMPLIFIER BRITISH MADE Ideal for Mike, Tape, P.U., Guitar, etc. Can be used with Battery 9-12v, or H.T. line 200-300v, D.C. operation. Size $1^{2^{\prime}} \times 1^{2^{\prime}} \times 2^{\gamma}$. Response 25 c.p.s. to 25 Kg/s, 26 db gain. For use with valve or transistor equipment. Full instructions supplied. Details S.A.E.

MAINS TRANSFORMERS ALL POST

6 or 12v. outputs. 1½ amp. 40p; 2 amp. 55p; 4 amp. 85p LUCAS 2DS500 Full wave Bridge 70v. 5 amp. 95p.

MAINS ISOLATING TRANSFORMER

Primary 0-110-240v. Secondary 0-240v. 3 amps. 720 watts. Insulated terminals. Varnish impregnated. Fully enclosed in steel case with fixing leaf. £10 carr. Famous make. (Value £19) OUR PRICE. 500 Carb. eused as 300 watt auto transformers 240-110V.

NEW TU	BULAF	ELECTROLY	TICS	CAN TYPES	3
2/850V	14p	250/25V	14p	50 + 50/350V	85
4/350V	14p	500/25V	20p	60+100/350V	58
8/450V	14p	1000/25V	35p	32+32/250V	18
16/450V	15p	100 0/50 V	47p	32+32/450V	83
32/450V	20p	8+8/450V	180	350 + 50/325V	50
25/25V	10n	8+16/450V	20p	32+32+32/350	V43
50/50V	10p	16+16/450V	25p	100 + 50 + 50/350	V48
100/25V	10p	32 + 32/350	25p		
LOW VO	LTAGE	ELECTROL	TICS.		
1 9 4 5	Q 14	95 90 50	100 0	00mF 15V 10n	

1, 2, 4, 5, 8, 16, 25, 30, 50, 100, 200mF 16V 10p.
500mF 12V 15p; 25V 20p; 50V 30p.
1000mF 12V 17p; 25V 35p; 50V 47p; 100V 70p.
2000mF 6V 25p; 25V 42p; 50V 57p.
2500mF 50V 62p; 3200mF 25V 47p; 50V 65p.
5000mF 6V 25p; 12V 42p; 25V 75p; 35V 85p; 50V 95p.

CERAMIC 1pf to 0 01mf, 4p. Silver Mica 2 to 5000pf, 4p. PAPER 350V-01 4p; 0-5 13p; 1mf 15p; 2mf 160V 15p. 500V-0-001 to 0-05 4p; 0-1 5p; 0-25 8p; 0-47 25p. SILVER MICA. Close tolerance 10, 2-2-500pf 8p; 560-2,200pf 10p; 2,700-5,600pf 20p; 6,300pf-0-01, mid 80p each. TWIN 640K "0-0" 208pf+176pf, 65p; Slow motion drive 365pf+365pf with 25pf-25pf, 50p; 50pr 4160. SHORT WAYE SINGLE. 10pf, 30p; 25pf, 55p; 50pf, 55p.

SHORT WAVE SINGLE GANG. Precision Silver Plated Gangable Tuning Condensers.

Values up to 100pF.

Section Couplers supplied FREE with two or more gangs.

NEON PANEL INDICATORS. 250V AC/DC Amber, 20p. RESISTORS, 4 w., 4 w., 1 w., 20%, 1p; 2 w. 5p, 10 \(\text{to to 10M}\). HIGH STABILITY. 4 w. 2% 10 ohms to 6 meg., 10p. Ditto 5 \(\text{NS} \). Preferred values 10 ohms to 10 meg., 4p. WIEE-WOUND RESISTORS. 5 watt, 10 watt, 15 watt, 10 ohms to 10 oK, 10p each; 2w 0-5 ohm to 8.2 ohms 10p. TAPE OSCILLATOR COIL. Valve type, 35p.

WEYRAD PSO - TRANSISTOR COILS

P51/1 or P51/236p P50/3V36p

Mullard Ferrite Rod 8 × §in. 20p. 6 × §in. 20p.

VOLUME CONTROLS | 80 Ohm Coax 4p yd. Long spindles. Midget Size 5 K. ohms to 2 Meg. LOG or LIN. L/S 15p. D.P. 25p. STREEO L/S 55p. D.P. 75p. Edge 5 K. S.P. Transistor 25p Ideal 825 and colour.

Edge oa. S.f. Transstor 20p ' Adeat ozo and Colour.' - p 1 linch DiaMetter WAVECHANGE SWITCHES, 25p. 2 p. 2-way, or 2 p. 3-way, 07 3 p. 4-way, 25p each. 1 p.1 2-way, or 4 p. 2-way, or 4 p. 3-way, 25p TOGGLE SWITCHES, sp. 14p; dp. 22p; dp. dt. 22p. Shb-miniature, sp. 30p; dp. 37p; dp. dt. 45p.

E.M.I. $13\frac{1}{2} \times 8$ in. SPEAKER SALE!

With twin tweeters.
And crossover. 10
watt. State 3 or 8 or 15 ohm. As illustrated. Post 25p

With flared tweeter cone and ceramic magnet. 10 watt.

Bass res. 45-60 ops.
Flux 10,000 gauss.

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TEAK CABINET 16×10×9in. £5-50

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GOODMANS 61 in. HI-FI WOOFER

8 ohm, 10 watt. Large ceramic magnet. Special Cambric cone surround. Frequency response 30-12,000 cps. Ideal P.A. Column. Hi-Fi Enclosure Systems, etc. Suitable cabinet 12 × 8 × 6 24-00. Suitable Tweeter 22-00.



ELAC CONE TWEETER

The moving coil diaphragm gives a good radiation pattern to the higher frequencies and a smooth extension of total response from 1,000 cps to 18,000 cps. Size 3½ × Sin, deep. Rating 10 watt, 3 ohm or 15 ohm models.

Crossover 95p.

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GOODMANS 8 in. WOOFER

8 ohm 12 watt. Deep cone. Heavy ceramic magnet. Bass resonance 35 cps. Frequency response 30-8,000 cps.

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LOUDSPEAKERS P.M. 3 OHMS. 7 × 4m. 21 25; 61m. £1.50; 8 × 5in. £1.60; 8in. £1.75; 10 × 6in. £1.90; 10in. £2.00. SPECIAL OFFER! 80 ohm, 2½ in. ½in. 35 ohm, 2in.; 3in. 5in. 25 ohm, ½in. 3in. dia; 15 ohm. £1.50 ohm. ½in. dia; 3in. dia; 15 ohm. £1.50 ohm. ½in. dia; 5in. /6 × 4in.; 7 × 4in.; 8 × 5in 3 ohm, ½in. 3in. 3in. 5in. dia. (6 × 4in., 8 ohm, £1.60). RICHARD ALLAN TWIN CONE LOUDSPEAKERS. Sin. diameter 4 wat; 10in. diameter 5 wat; 12in. diameter 6 wat; 3 or 8 or 15 ohm models £2.20 each. Post 15p. SPEAKER COVERING MATERIALS. Samples Large S.A.E. Horn Tweeters 2-16Kc/s, 8W 8 ohm or 15 ohm £1.95. De Luxe Horn Tweeters 2-18 Kc/s, 15W, 15 ohm 23. TWO-WAY 3,000 c.p.s. CROSSOVERS 3, 8 or 15 ohm 95p.

FM/VHF TUNING HEART
88 to 108 M/GS British made. 2 Transistors ready alignedrequires 10-7 M/GS IF. Complete with tuning gang. Con
nections supplied but some technical experience essential.
OUR
43-95

STEREO / MONO HEADPHONES



Now Model with new type slider volume controls. Stereo / Mono switch. 3 ohms. £10. High Quality with tweeters and volume controls. 3 ohm. £7. Budget Model. 3 ohm. £2.25. HEADPHONE JUNCTION BOX with switch £1.75. Mono Stethoscope. 8 ohms. 65p. EAR PIECES. Crystal. £5p. Magnetic. 8 ohms. 18p. Magnetic. 250 ohms. 23p. ACOS. 1000 ohms. 53p.

BRITISH MADE STEREO MULTIPLEX DECODER

Brand New. 7 transistors plus integrated circuit. Fibre glass printed circuit board. Size 2½ · 6½ · 8in. Pre-aligned. Complete with stereo beacon indicator. 127 d. coperation. 400mV output for 100µV input. Full instructions for any FM Tuner. Some technical experience essential. £6.50

DIPOLE LOFT AERIAL £1.50. Post 15p CABLE 4p yard.



COANIAL PLUG 10p, PANEL SOCKETS 10p, LINE 18p, OUTLET BOXES, SURFACE OR FLUSH 25p, BALANCED TWIN RIBBON FEEDER 300 ohms, 5p yd. JACK SOCKET Std. open-circuit 14p, closed circuit 25p; Chrome Lead Socket 45p, Phono Plugs 5p, Phono Socket 5p, JACK PLUGS 5td. Chrome 15p; 35mm Chrome 12p, DIN SOCKETS Chassis 3-pin 10p; 5-pin 10p. DIN SOCKETS Lead 3-pin 18p; 5-pin 15p. DIN FLUGS 3-pin 18p; 5-pin 25p. VALVE HOLDERS 5p; CERAMIC 8p; CANS 5p.

MINIMUM POST AND PACKING 15p.

COMPON

Illustrated Colour Brochure, Radio Books & Component Lists 10p. Written guarantee.

E.M.I. WOOFER AND

45.75 THE PAIR, Post 25p. (Available separately. Woofer £4.25; Tweeter £1.90).

21-90.

Comprising a few example of a Woofer 103: 6 im. with a massive Ceramic Magnet, 44oz. Gauss 13.000 lines. Aluminum Cone centre to improve middle and top response. Also the E.M.I. Tweeter 3 in. square has a special lightweight paper cone and magnet flux 10.000 lines. Crossover condenser and full instructions supplied.

Impedance Standard 8 ohms
Maximum power 12 watts
Maximum power 12 watts
Useful Response 35 to 18,000 cps
Bass Resonance 45 cps
SUITABLE ENGLOSURE 20 13 9in.
MODERN DESIGN. TEAK WOOD FINISH.



£9.90 Post 25p



8in. or 10in. ELAC

Dual cone plasticised roll sur-Dual cone plasticised roll sur-round. Large ceramic magnet. 50-16,000 cps. Bass resonance 55 cps. 8 ohm impedance. 8in. 10 watts, 10in. model. 12 watts music power. Post 25p

HI-FI SPEAKER

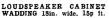
TEAK VENEER SPEAKER CABINET

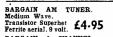
Fluted Wood Front

MODEL "A". 20 13 For 12in. dia. or 60 £9 Post 25p 10in. speaker.

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BARGAIN 4 CHANNEL
TRANSISTOR MONO
MIXER. Add musical
highlights and sound effects
to recordings. Will mix highlights and sound enecta-to recordings. Will mix Microphone, records, tape and tuner with separate controls into single output. 9 volt battery £3.95

operated.
STEREO VERSION OF ABOVE BARGAIN PM TUNER.
9 volt. Printed circuit.
9 volt. Printed circuit.
9 volt. Printed circuit.
8 volt. Printed circuit.
9 v

£4.50

THE "INSTANT" BULK TAPE ERASER & HEAD DEMAGNETISER. Suitable for cassettes, and all sizes of tape reels. A.C. mains 200/250V. Leaflet S.A.E. 47.50 Post £2.50 Post



WAFER HEATING ELEMENTS

WAFER HEATING ELEMENTS
OFFERING 1001 USES for every type of heating and
drying applications in the home, garage, greenhouse,
factory (available in manufacturing quantities). Approx.
size 10; 8; ½, in. Operating voltage 2002/500°. a.c.
250 watts approx. Printed circuit element enclosed in
asbestos fitted with connecting wires. Completely flexible
providing safe Black heat. British-made for use in photocopiers and print drying equipment.
Ideal for home handymen and experimenters. Suitable
for Heating Pads, Food Warmers, Convector Heaters, etc.
Must be clamped between two sheets of metal or asbestos,
etc., to make efficient clothes dryers, towel rails ideal for
aring cupboards. Ideal for anti-frost device for the garage
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Use in the greenhouse for seed raising and plant protection.
Invaluable aid for bird houses, incubators, etc., etc. Can
be used in series for lower heat. Or in parallel for higher
heat applications.

ONLY 40p EACH (FOUR FOR £1-50)

ALL POST PAID Discounts for quantity.

BAKER 12in, MAJOR £10

Post 25p



30-14,500 c.p.s., 12in. double cone, woofer and tweeter cone together with a BAKER ceramic magnet assembly having a flux density of 14,000 gauss and a total flux of 145,000 Maxwells. Bass 145,000 Maxwells. Bass resonance 40 c.p.s. Rated 20 watts. NOTE: 3 or 8 or resonance 40 c.p.s. Kate 20 watts. NOTE: 3 or 8 c 15 ohms must be stated.

Module kit, 30-17,000 c.p.s ith twe tweeter. £12.50 instructions

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BAKER "BIG SOUND" **SPEAKERS**

Robustly constructed to stand up to ong periods of electronic power. As used by leading groups Useful response 30-13.000 cps. Bass Resonance 55 cps

GROUP "25" 12in. 25 watt 3, 8 or 15 ohms.

GROUP "35" 12in. 35 watt 3, 8 or 15 ohms.

GROUP "50" 15in. 50 watt 8 or 15 ohms.

Post 25p



£8.80

£9.90

Post 25p

Post 25p

CALLERS ONLY: DE-LUXE 100 WATT AMPLIFIER CHASSIS. 7 Valve version. 4 inputs, 10 wide range controls. For Mikes, Discos, Organs, Guitars, etc. 4. 8 and 15 ohm matching.

Q MAX CHASSIS CUTTERS

A die, punch and Allen Screw

in. Round in. Round Lin. Round Key "T" for in. Round in. Round
in. Round
in. Round
in. Round
in. Round
in. Round
in. Round
in. Round
in. Round
in. Round

1 in. Round £1 43 | 1in. Square 5p 1 in. Round £1 50 | with key £1 93 above

SLIDER VOLUME **CONTROLS**

Mono LOG or LINEAR Size 3 5. 1 . 5 in, with knobs. 5K, 10K, 25K, 50K, 100K, 250K, 500K, 1 MEG, 2 MEG.

65p EACH



E.M.I. TAPE MOTORS, 120 volts AC each, 1,200 r.p.m. 4 pole or 2 in series 240 volts AC. Size 3; 2½ 2½ 2;in. (illustrated). Post 15p. 2;in. (flustrated). Fost 1op.

BALFOUR GRAM. MOTORS.
120v. or 240v. AC. 1,200 r.p.m. 4 pole
50mA. Spindle 3 3/20. Size
2½ 2½ 1½in. Post 15p

85p

E.M.I. GRAM. MOTORS. 120V or 240V AC. 2.400 r.p.m. 2-pole 70mA. Spindle ; ä.in. £ Post 15p Post 15p

BAKER HI-FI SPEAKERS

HIGH QUALITY - BRITISH MADE

REGENT

12in. 15 watts

An inexpensive unit for the beginner in high fidelity and for general purposes. May to used to improve any Radio. used to improve any Radio. Amplifier, Hi-Fi or Television

Bass Resonance Flux Density 12,000gauss Useful response 45-13,000cps 3 or 8 or 15 ohm models.

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DE-LUXE Mk II 12in 15 watts

Especially designed to provide full range reproduction at an economical cost. Suitable for use with any high fidelity system. Built-in concentric

system. Built-in concentric tweeter cone.

Bass Resonance 30cps
Flux Density 14,000gauss
Useful response 25-16,000cps 8 or 15 ohms models

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SUPERB 12in. 20 watts

A high quality loudspeaker, its remarkable low cone resonance ensures clear reproduction of the deepest bass. Fitted with a special bass. Fitted with a special tweeter one resulting the reproduction in the remarkable efficiency in the upper register.

Bass Resonance 25cps
Flux Density 16,500zauss
8 or 15 ohms models.

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AUDITORIUM 12in. 25 watts

A full range reproducer for high power, Electric Guitars, public address, multi-speaker systems, electric organs. Ideal for Hi-Fi and Discotheques.
Bass Resonance 350

35cps Flux Density 15,000gauss Useful response 25-16,000cps 8 or 15 ohms models.

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AUDITORIUM 15in. 35 watts

high wattage loudspeaker exceptional quality with a of exceptional quality with a level response to above 8,000 cps. Ideal for Public Moderation of the second of the

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Hi-Fi Enclosure Manual containing 20 plans designs, crossover data and cubic tables. 42p. Post Free.

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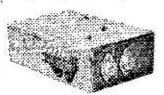
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PRACTICAL ELECTRONICS " SCORPIO" **ELECTRONIC IGNITION** SYSTEM



This Capacitor-Discharge Electronic Ignition system was described in the November and December issues of Practical Electronics, it is suitable for incorporating in any 12V ignition system in cars, boats, go-karts, etc., of either pos. or nee, earth and up to six cylinders. The original coil, plugs, points and contact-breaker capacitor fitted in the vehicle are used. No extra or special components are required: Helps to promote easier starting (even under sub-zero conditions), improved acceleration, better high-speed performance, quicker engine warm-up and improved fuel economy. Eliminates excessive contact-breaker point burning and the need to adjust point and sparkplug gaps with precision. Construction of the unit can easily be completed in an evening and installation should take no longer than half an hour. A complete complement of components is supplied with each kit together with ready-drilled roller-tinned professional quality fibre-glass printed-circuit board, custom-would transformer and fully-machined die-cast case. All complete assembly an approx. Complete assembly and wiring manual ZSp, refundable on purchase of kit. Price: £10-50 plus 50p P. & P.

DABAR LIGHTING EFFECTS



SINGLE CHANNEL SOUND TO **LIGHT UNIT** STL/I

Single channel "Sound to Light "unit with slider fader controls for audio trigger level and background

Switchable for response to High Mid and Lowfrequency audio input signals selected by fascia control, D.J. Pulse-Flash push button D.J. Pulse-Flash push button fitted to fascia for manual flashing of lamp load. Neon load indicator fitted

Constructed on glassfibre printed circuit material with attractive black anodised fascia panel. Input and load connections via Cinch printed circuit connector. Maximum Load IkW at 250V 50Hz. R.F.I. filtered.

Price: £13 each post free U.K.

S.A.E. All Enquiries please



THREE CHANNEL SOUND TO **LIGHT UNIT** STL/3

Three channel "Sound to Light unit with slider fader controls for audio trigger level and back-ground load dimmer.

An attractive unit with indepen-dent control of High, Mid and Low frequency audio trigger levels. Slider fader background or dimmer controls on each channel

D.J. Pulse-Flash push buttons on each channel together with neon load indicators.

Constructed on glassfibre printed circuit material with attractive black anodised fascia panel, Input and load connections at rear so unit is ideally suited for mounting into disco-console Maximum Load I 5kW per channel at 250V 50Hz.

R.F.I. filters incorporated. Price: £38-50 each post free U.K.

Trade enquiries Welcome

PSYCHEDELIC LIGHTING UNIT Mk. 3



This unit represents a natural progression from our phenomenally successful Mk. I and 2 Units. As before the drive voltage is derived directly from the amplifier output or across the speakers. The unit converts the audio frequency signals into a three-coloured light display; the colour depending on the frequency of the signal and the intensity on the loudness of the audio source.

intensity on the loudness of the audio surce.

The unit is constructed on professional fibre-glass printed-circuit board material and uses latest full-wave triac circuitry. There is a master-level control, together with independent sensitivity controls for each channel The original minimum ambient light level controls have been redesigned permitting their use as faders; allowing dimming from max. to zero at the turn of a knob. R.F.I. suppression is now incorporated as standard as well as provision for D.J. "Pulse-Flash" controls. The choice of two inputs enables operation from both high and low power amplifiers. Max. power 1-5kW per channel at 240V a.c. Complete assembly built and tested Size 9in x 7in x 3in. Price £25 carr. paid.

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GLADSTONE RADIO

66 ELMS ROAD, ALDERSHOT, Hants

(Closed Wednesday)



F.M. TUNER AMPLIFIER for 88-102 MHz. Self-powered for 200-250v. a.c. Valves ECC85, EFS9, EFS9, ECC82, 2 diodes, metal rect. Chassis 10" × 6" × 6". Audio amp. module giving 3W. into 16-bm. Price \$14 (nost.56n). 6". Audio amp. me Price £14 (post 50p).

Kit and wiring instrs. for 12V windscreen wiper delay control; metal box $3\frac{1}{4}'' \times 1\frac{3}{4}''$ with fixing strap, relay and all compts. £1.50 (post 20p).

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B. Charger 12v. at 1¼A, 60p (20p)

E. 250v. at 50 m.a., & 6.3v at 1¼A, 50p (20p)

H. 99v. at 100m.a., & 220v. at 50m.a. \$5p (20p)

J. 37v. 2A, 24-0-24v. 150m.a. &2.50 (50p)

J. 37v. 2A, 22-0-24v. 20v. 4A. 15v. 1A. 6.3v. 5A. &2 (50p)

L. 275-0-275v. 50m.a. 6.3v. 2¼A & 6.3v. ¼A, 75p (25p)

M. 110v. input; 200-0-200v. 50m.a. 6.3v. 1¼A, 60p (25p)

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STEREO AMPLIFIER 2 × 3W. Printed circuit. Valves
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Controls on-off, balance, ganged vols., gauged tones;
With knobs. Also available for 110v. a.c. Only 28 (p. & p. 50p)
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TRANSISTOR RADIO PARTS Gang capacitors. Min. 180pt + 180pt **20p** (8p); 150 + 110pt **30p** (10p) 250 + 250pt dust cover 30p (8p); 250 + 250p dust cover, slow motion **20p** (5p); triple 335pt direct drive with slow motion **60p** (10p).

Driver transformers. 2-5 to 1+1 **20p** (8p); 5-7 to 1+1 **20p** (8p); Output trans. 2x OC81 to 3-ohm **25p** (5p); 2x OC82 to 3-ohm **20p** (5p); Edgewise pots (s.p.) $\frac{3}{2}$ " (dia 2-5K or 5K 15p (5p); 2x SK 1" dia **25p** (5p); pts with $\frac{5}{6}$ 4" dia spindle 2-5K 4" ong spindle **15p** (5p) with knob; 2-5K 1" dia **25p** (5p); pts with $\frac{5}{6}$ 4" dia spindle 2-5K 4" ong spindle **15p** (5p) with knob; all pots with s. pole

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SN7409				69p	SN7474	41p	38p	SN74100	1.80p	1·75p
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	47 μF 100μF 220μF 330μF 1000μF 4700μF	6 ½ p 6 ½ p 6 ½ p 6 ½ p 13 p 29 p	15μF 33μF 68μF 150μF 220μF 680μF 1000μF 1500μF 2000μF	6 ½ P 6 ½ P 8 P 9 P 17 P 17 P 25 P 43 P	47μF 100μF 150μF 220μF 470μF 680μF 1000μF 2200μF	6 ½ 9 10 11 19 25 25
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1	470μF	I Op	40 VO		$220 \mu F$	19
1	1000μF	Пр	6·8μF	6 ½P	$330 \mu F$	22
1	1500μF	20p	15μF	6 <u>₹</u> p	470μF	26
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AL100 77p	BCY70 17p	NKT40583p	2N3054 55p	BY126 16p	3≹in × 5in
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AL103 55p ASY26 31p	BCY72 17p BD123 66p	86p	2N3405 44p	BYX10 24p	Vero Pins (bag o
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MULLARD POLYESTER'S

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Carbon track 500 Ω to 2·2M Ω
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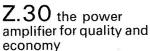
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Sinclair Project 60

Now-the Z.50 Mk.2

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with free manual

The Z.30 provides excellent facilities for the constructor requiring a high fidelity audio system of less power than that available from Z.50's. Using a power supply of 35 volts. Z.30 will deliver 15 watts RMS into 8 ohms, or 20 watts RMS into 3 ohms using 30 volts. Total harmonic distortion is a fantastically low 0.02% at 15 watts into 8 ohms with signal to noise ratio better than 70 dB unweighted. Input sensitivity 250mV into 100K ohms. Size 80 x 57 x 13 mm (3_1° x 2_2° x $\frac{1}{2}$) Z.30, Z.50 and Z.50 MK.2 modules are compatible and interchangeable.

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If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

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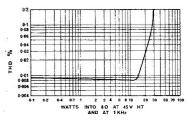
Input impedance 100 K Ω Input (for 30w into 8 Ω) 400mV Signal to noise ratio, referred to full 0/p at 30v HT 80dB or better Distortion 0.02% up to 20W at 8 Ω . See curve Frequency response 10Hz to more than 200 KHz \pm 1dB Max. supply voltage 45v (4 Ω to 8 Ω speakers)

(50v 15Ω speakers only)
Min. supply voltage 9v

Load impedance — minimum : 4Ω at 45v HT Load impedance — maximum : safe on open circuit



manual £5.48



Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48
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SPECIFICATIONS—Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV. correct to R.I.A.A. curve ±1dB:20 to 25,000 Hz. Ceramic p.u. – up to 3mV: Aux – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 7dB. Tone controls: TREBLE+12 to —12dB at 10KHz: BASS +12 to —12dB at 100Hz. Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207 mm.

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SPECIFICATIONS—Number of transistors:18 plus 20 in i.C. Tuning range: 87.5 to 108MHz. Sensitivity: 7μV for lock-in over full deviation. Squelch level: Typically 20μV. Signal to noise ratio: > 65dB. Audio frequency response: 10Hz - 15KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2μV. Cross talk: 40dB. Output voltage: 2x 150mV R.M.S. maximum Operating voltage: 25–30VDC.Indicators: Stereo on:tuning. Size: 93 x 40 x 207mm.

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SPECIFICATIONS

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ļ	EF98	0.75	GZ34 0.60	PL33 0.40	U404 0.70
ļ	EF183	0.80	HABC800.55	PL36 0.55	U801 0.80
	EF184	0.35	HK90 0.50	PL81 0.50	UABC80
	EF804	1.25	KT66 2.35	PL82 0.45	0.40
	EK90	0.82	KT88 2-25	PL83 0.45	UAF41 0.70
ļ	EL34	0.50	N78 1.60	PL84 0.40	UAF42 0.60
	EL36	0.50	PABC800.40	PL302 0.95	UB41 0.65
	EL37	1.70	PC86 0.60	PL504 0.75	UBC41 0.55
	EL41	0.75	PC88 0.60	PL508 0.90	UBC81 0.45
	EL81	0.55	PC92 0.05	PL509 1.10	UBF80 0.40
	EL83	0.50	PC97 0.50	PL801 1.00	UBF89 0.40
l	EL84	0.25	PC900 0.48	PL802 0.95	UBL1 0.70
l	EL85	0.43	PCC84 0.40	PM84 0.60	UBL21 0.70
ı	EL86	0.40	PCC85 0.40	PY31 0.35	UC92 0.45
ı	EL90	0.42	PCC88 0.55	PY33 0.63	UCC85 0.45
į	EL360	1.15	PCC89 0.55	PY80 0.40	UCF80 0.70
l	EL821	0.60	PCC189 0.60	PY81 0.30	UCH21 0.60
١	EL822	1.40	PCC805 0.95	PY82 0.35	UCH42 0.70
ı	ELL80	0.75	PCC806 0.95	PY83 0.38	UCH81 0.40
ı	EM34	1.00	PCF80 0.30	PY88 0.40	UCL81 0.60
l	EM71	0.80	PCF82 0.35	PY800 0.47	UCL82 0.85
١	EM80	0.45	PCF84 0.60	PY801 0.50	UCL83 0.65
i	EM81	0.60	PCF86 0.60	PZ30 0.88	UF9 0.65
ł	EM83	0.50	PCF87 1:10	QQV02-6	UF11 0.60
	EM84	0.35	PCF801 0.50	2.25	UF41 0.65
	EM85	1.00	PCF802 0.50	QQV03-10	UF42 0.65
	EM87	0.70	PCF805 0.90	1.25	UF43 0.65
l	EN91	0.40	PCF806 0.75	QQV03-20A	UF80 0.85
	EY51	0.40	PCF808 0.90	5,25	UF85 0.40
	EY80	0.75	PCH2000.70	TT21 3.40	UF89 0.40
	EY81	0.40	PCL81 0.50	TT22 3.50	UL41 0.65
	EY83	0.55	PCL82 0.35	U18/20 0.75	UL84 0.48
	EY86	0.40	PCL83 0.65	U25 0.85	UM84 0.80
	EY87	0.48	PCL84 0.45	U26 0.85	UY1N 0.50
	EY88	0.43	PCL86 0.45	U31 0.70	UY11 1.00
	EZ40	0.50	PCL88 1.25	U37 6.50	UY41 0.48
	EZ41	0.75	PCL200 0.75	U52 0.40	UY82 0.50
	EZ80	0.28	PCL8001,10	U76 0.40	UY85 0.40
	EZ81	0.29	PCL801 0.95	U78 0.40	W729 B76



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ACY18 ACY19 ACY21 ACY21 ACY21 AD140 AD161 AD211 AF115 AF115 AF115 AF118 AF127 AF180 AF127 AF180 AF299 AF299 AF294 0.12 0.35 0.25 0.20 0.20 0.20 0.40 0.25 0.20 0.20 0.25 0.20 0.25 0.20 2N2218 2N2219 2N2369 A 2N2477 2N2646 2N2905 2N2923 2N2924 0.20 0.15 9.65 0.40 0.25 0.12 0.13 0.12 0.50 0.60 0.60 0.25 0.25 0.60 0.45 0.20 0.15 0.12 0.10 2N2924 2N2926 2N3053 0.20 2N3054 2N3055 2N3055 2N3133 2N3134 2N3391 0.50 0.60 0.25 0.25 0.17 2N3392 2N3393 0.15 2N3394 2N3395 2N3402 2N3403 2N3404 2N3414 2N3415 2N3702 2N3702 2N3703 2N3704 2N3707 2N3709 AUY10 BC107 BC107 BC108 BC109 BC113 BC118 BC134 BC147 BC148 OC72 OC73 OC75 OC76 OC78 OC78D OC81 OC81D OC83 OC139 OC140 OC141 OC170 OC171 0.12 0.32 0.20 0.15 0.25 0.10 0.30 0.15 0.25 0.20 0.20 0.20 0.20 0.20 0.10 0.10 0.12 0.15 0.15 BC149 BC152 BC158 BC175 BC186 0.30 0.35 0.60 0.25 0.25 2N3710 0.10 0.20 2N3819 0.25 0.35 0.25 0.50 0.25 0.15 0.30 0.20 0.17 0.25 0.30 0.25 0.30 0.15 0.30 BCY30 BCY31 BCY33 BCY34 2N3906 28702 28746 AC113 AC125 0.80 OC200 OC201 OC202

BCY72 BCZ10

BCZ1

OC203

0.40









PCL805 0.50

PD500 1.30

PF86 0.70



Y63 0.75

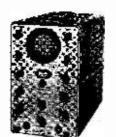
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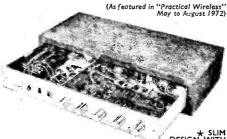
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SIMPLE PROJECTS FOR THE HOME

8 PAGE SUPPLEMENT



This oscillator produces a pleasing tone, different in frequency for either of two doors. By using a suitable centre-tapped transformer T1, the collector circuit of each transistor can drive the base of the other transistor.

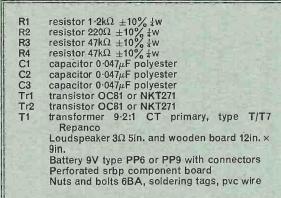
Assembly is on a perforated srbp board and wired as in Fig. 2. This board is fitted in the speaker cabinet or to a flat speaker panel fitted across the corner of the room.

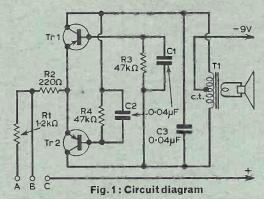
One push-button switch is wired to A, and the other to B. The return leads of both switches go the common terminal C. When one switch is operated both R1 and R2 are in circuit, while with the second push R2 only is present. Wires A-C can run to the front door, and B-C to the back door.

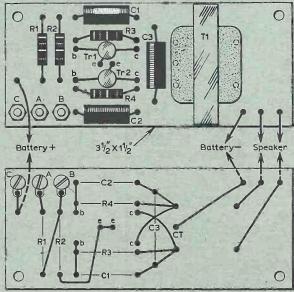
The note can be altered by changing the resistance of R1 or R2 or the capacitance of C1, C2 or C3.

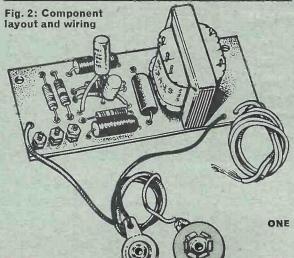
Connections for OC81, NKT271: collector wire nearest spot, then base, emitter.

components











Ready-made amplifier module used to give press-button calling and communication in both directions. Fig. 1 is the complete circuit.

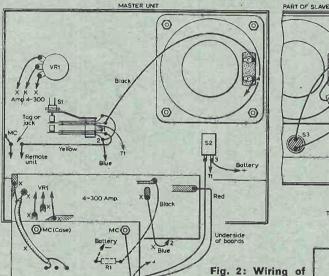


Fig. 2: Wiring of module in the master unit on the left and partly cutaway view of remote unit

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To master unit

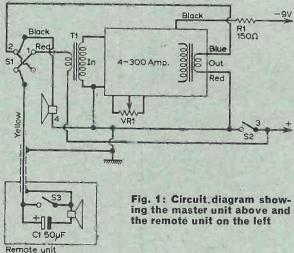
Pers Till.

S1 is the "push-to-call and push-to-speak" switch. When it is pressed, the circuit is completed in such a way as to cause an audio tone (R1 limits current in this condition). S2 switches the unit on so that the master position may speak to the remote position, or vice versa. S3 at the remote unit causes a tone at the master unit, to gain attention.

At the master unit, press S1 a few times to gain attention, then close S2, with S1 released to listen. Press S1 again to speak. Switch off with S2 when contact is finished. At the remote unit, press S3 a few times to call master unit and await reply. VR1 is set to a suitable volume level, and is ready wired to the 4-300 unit.

components

resistor 150Ω ±10% ¼ watt potentiometer supplied with amplifier module capacitor 50µF 12V electrolytic transformer 9.2:1 CT primary, type T/T7 VR1 T1 S1 2-pole, changeover spring loaded push button, type S746 with S768 operator, or type S415 Bulgin S2 single-pole, on-off toggle switch single-pole, on-off push button Loudspeakers 3Ω 2½in. or 3½in. Battery 9V type PP6 or PP9 and connectors Amplifier module type 4-300 Component board srbp $3\frac{1}{2}$ in. \times $2\frac{1}{2}$ in. Case 8in. \times 6in. \times 6in. (Master unit) Case 4in. × 4in. × 4in. (Remote unit) PVC connecting wire and knob Nuts and boits 6BA and 4BA Soldering tags 6BA



Numbers 1 to 4 in Fig. 1 refer to connection points 1 to 4 in Fig. 2. Fig. 2 shows the master unit. Two 6BA bolts secure the 4-300 amplifier and also the srbp board for T1 and R1. Solder coloured leads to S1 as indicated before fitting this item. Input and output circuits and T1 are continued on page three-

A sensor, on the end of twin flexible lead, can be placed in a water tank, swimming pool, bath or wash-boiler. A buzzer sounds when the water level reaches the sensor.

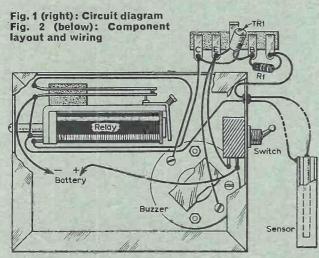
The minimum battery current drain is about 0.3mA; rises to about 400mA when water reaches the sensor.

Fig. 1 shows the circuit. The presence of water shorts the sensor probe and allows base current to flow through R1, resulting in a collector current of about 40-50mA to close the relay. The buzzer sounds until the sensor is removed from the water, or the device is switched off.

Fig. 2 shows all wiring, in a case made from aluminium. The tag strip (shown detached) is mounted vertically in the adjacent corner of the case. Space is left for a flat 3-cell 4.5 volt battery.

components

R1 resistor $10k\Omega \pm 10\% \frac{1}{2}$ watt transistor OC76 or any high gain pnp type single-pole, on-off switch relay 100Ω coil, single-pole on-off contacts, 3-6V operation Battery $4\frac{1}{2}$ to 6V depending on relay obtained Buzzer $4\frac{1}{2}$ to 6V Sensor probe (see text) Case 6in. × 4in. × 2in. aluminium box or chassis with lid.



INTERCOM AMPLIFIER continued from page two

positioned to avoid feedback which would cause instability. In addition to VR1, the 4-300 has a preset sensitivity control, which can be left at about the middle of its travel.

Easy connecting of a remote unit lead can be by a jack plug and socket, the outer conductor being the common positive return. Do not connect or disconnect while battery is switched on.

The equipment will operate as a baby alarm by placing the remote unit near the cot and closing S2.

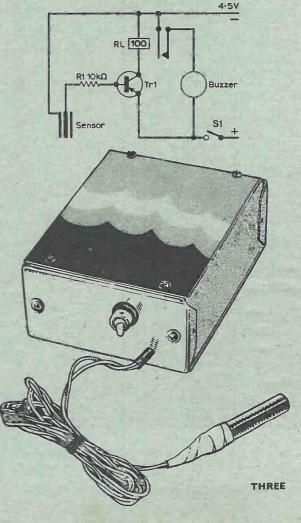
Connections to the 4-300 amplifier module are shown in Fig. 2, indicating appropriate copper pads used for connections. MC indicates connection made to the metal case by soldering tags. \$1 does not necessarily need to resemble that shown in Fig. 2 but can be any style with the operation as in components list.

SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973



The sensor is made in coaxial form to avoid any accidental short (and wrong indication) by metal items. It has an outer metal tube about 2in. long by \$\frac{3}{2}\$ in. diameter, with a slightly shorter internal pin (actually a length of 4BA threaded rod). The inside part is fixed by a tight binding of insulating tape, or by an insulated sleeve. The sleeve and pin must not touch. Several feet of thin twin flex are soldered on, the sensor inner part going to R1.

An alternative probe can be a coaxial plug as used for TV aerial wire, although it must be kept free from corrosion.





This portable medium wave tuner gives an output for a tape recorder or amplifier.

Note that the AA119 diode has a black mark to denote plus polarity; wrong polarity here will upset avc action. Components are positioned as in Fig. 2 and wired as shown in

grey. The perforated srhn board is bolted to the metal bracket carrying VR1, VC1/2 and S1. MC is the metal case connection.

A bracket, srbp strip, and strip of card wrapped round the rod and drawn tight with a

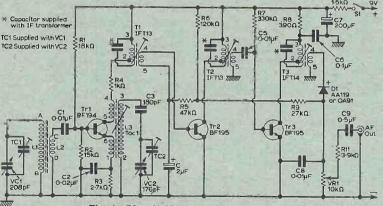
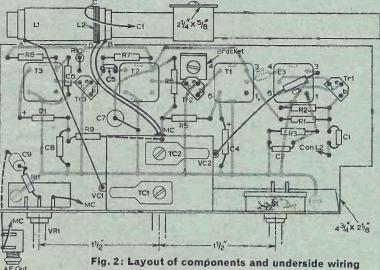
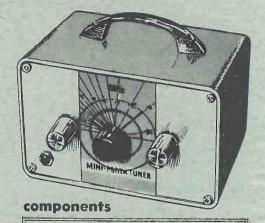


Fig. 1: Circuit diagram of the tuner





205	isto	PC

R1	18kΩ	R7	330kΩ
R2	15kΩ	R8	390Ω
R3	2·7kΩ	R9	27kΩ
R4	1kΩ	R10	1.5kΩ
R5	47kΩ	R11	3-9kΩ
R6	120kΩ		

All resistors ±10% 4 watt

Potentiometer Diode VR1 $10k\Omega \log$. D1 AA119 or **OA91**

Capacitors

C1 $0.01\mu F$ mica or ceramic C2 $0.02\mu F$ mica or ceramic C3 $180\mu F$ mica or ceramic

C4 2µF electrolytic

0·01μF mica or ceramic 0·1μF polyester 200μF 9V electrolytic

C7

C8 0·01μF polyester

C9 0·5μF polyester (Note: C9 not required if used only with IC-12 audio amplifier)

Variable Capacitors

VC1 & VC2 208+ 176pF with trimmers type 00 Jackson (slow motion optional)

Preset Trimmers

TC1, TC2 fitted to VC1, 2

Transistors

Tr1 BF194 Tr2 BF195 Tr3 BF195

L1, L2 Medium wave ferrite rod aerial coil type MW/FR5 Denco L3 Oscillator coil type TOC1 Denco

Transformers

T1 I.F. transformer type IFT13 Denco I.F. transformer type IFT13 Denco

T3 I.F. transformer type IFT14 Denco

Switch

S1 Single-pole, on-off toggle switch

Miscellaneous

Perforated srbp, 0.15in. matrix 43in. x 21in.

Control panel and bracket 43in, x 2in. aluminium

Nuts and bolts 6BA, pvc wire Case, insulated, of wood or plastic This radio aram is designed to awaken you at a preset time set on the clock movement, and to switch off automatically if required.

Use the "Tape Tuner" (page four of this supplement) with an integrated circuit audio amplifier. The synchronous clock runs from 250V a.c. mains and is supplied with contacts which are set by a front mounted control. A second control sets the duration, then automatically switching off. (A minute timer ringer is also provided, but is not used in this circuit.)

The master or programming switch, which is arranged as in Fig. 1 and shown in two views in Fig. 2, allows the radio to be switched on irrespective of the clock settings, or switched off separately, giving complete freedom of operation without any need to change clock settings.

components

Tape tuner as described on page four of Supplement Amplifier i.c. type "Super IC12" with heat sink (Sinclair)

Electric programmer clock as illustrated with switch contacts glass and bezel (various advertisers)
Loudspeaker'8Ω to match IC12

Switch single pole, 3-way to select operation Connection block, 3-way for mains connection Fabric or expanded aluminium speaker grille Case approx. 10in \times 7in. \times $4\frac{1}{2}$ in.

A mains connector joins mains leads and clock leads.

The i.c. amplifier is mounted on brackets. The whole unit is powered by a PP9 9V battery. A mains unit could be fitted instead and several proprietary brands can be purchased or the reader can make his own. All units can be mounted in a suitable wooden case.

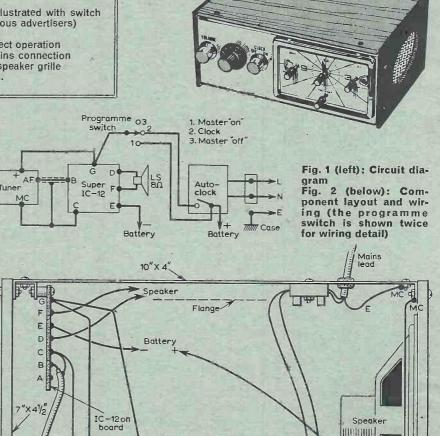
TAPE TUNER

continued from page four nut and bolt hold the ferrite rod aerial.

The i.f. transformers T1, T2, T3 are pre-aligned but the effect of slight core adjustment can be tried. Adjust TC1 and TC2 at the high frequency (200 metres) end of the band, and the core of L3 (if necesary). The position of L1/L2 on the ferrite rod is adjusted at the low frequency end of the band.

Note that the specified case is insulated material, not metal to avoid screening the ferrite rod aerial. Audio output should be heard on high impedance phones connected to the output jack socket. The output is of high impedance and should be fed into the high impedance input of a tape recorder via screened cable (but see also the Radio Alarm Clock).

Transistor connections as indicated by top view in Fig. 2. ●



Radio

Alarm

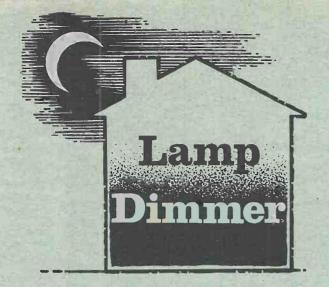
Clock

MC

Tuner

Flange

Prog. switch



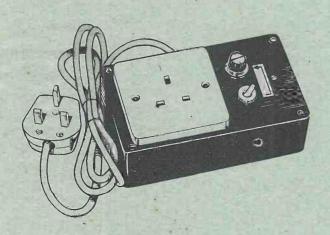
This lamp dimmer is constructed in an electrical switch box. The 40432 triac is rated at 0.5A without a heat sink, or 1A with the type 5F clip-on heat sink shown. With 240V a.c. mains, this is suitable for lamp loads of 120 watts and 240 watts respectively. An alternative triac type 40430 can also be used.

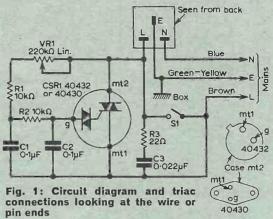
The dimmer can be fitted in place of an ordinary lamp switch. With the portable unit shown, the dimmer box and a 13A type outlet are assembled in a larger box. A table or standard lamp can be plugged into it, or it can be used for heat control of a soldering iron. This unit is not rated for power drills and is not suitable for them nor for fluorescent lamps.

Fig. 1 is the circuit, with wiring to integral 13A type outlet. The metal box, Fig. 2, provides screening. Complete closure by a metal plate was not found necessary. The triac case is connected, via a soldering tag bolted to the heat sink or case, to VR1. It must be insulated from the box and any other metal part. Flexible leads to VR1 and S1 allow these to be positioned in the front holes.

Assure proper earthing is maintained right up to any appliance controlled by the unit. The mains plug is fitted with a 3A fuse.

Triac connections shown in diagram.





components

R1 resistor $10k\Omega \pm 10\% \frac{1}{2}$ watt
R2 resistor $10k\Omega \pm 10\% \frac{1}{2}$ watt
R3 resistor $22\Omega \pm 10\% \frac{1}{2}$ watt
VR1 potentiometer $250k\Omega$ linear
C1 capacitor $0\cdot1\mu$ F 1,000V d.c. or 300V a.c.
C2 capacitor $0\cdot1\mu$ F 1,000V d.c. or 300V a.c.
C3 capacitor $0\cdot022\mu$ F 1,000V d.c. or 300V a.c.
CSR1 triac type 40432 with heat sink clip type 5F or triac type 40430
S1 Single-pole, on-off toggle switch 250V a.c.
Metal electrical switch box $2\frac{3}{4}$ in. \times $2\frac{3}{6}$ in. \times $1\frac{3}{6}$ in. or $6\frac{1}{4}$ in. \times $3\frac{1}{4}$ in. \times 2in. with 13A mains socket Tag strip 8-way,knob,pvc wire,rubber grommet

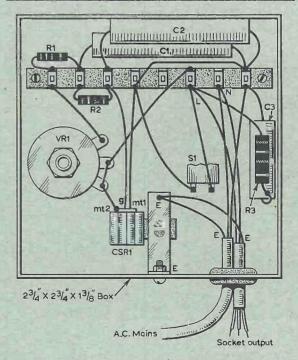


Fig. 2: Component layout and wiring
SUPPLEMENT TO PRACTICAL WIRELESS—MAY 1973

The input transducer is a small loudspeaker, followed by Tr1 and Tr2 as amplifiers. VR1 is a sensitivity control, allowing adjustment of the sound level at which the unit operates.

All components except the speaker and VR1 are mounted on the perforated srbp board in Fig. 2. Underside wiring is shown in grey. Points A, B and C carry connecting wires to VR1. Wires A and C are connected so that sensitivity increases as the control knob is rotated from the "off" position in the usual way. The case is an aluminium box or chassis.

Test by connecting a meter to the output terminals. A brief pulse of current is indicated when switching on, due to C5. The reading should then remain at zero, rising to 100-250mA while snapping the fingers or speaking quietly.

Place the unit adjacent to the source of sound. Where extraneous sounds may operate the unit, reduce sensitivity by turning back VR1 just enough to avoid this.

Twin bell wire or a long twin flexible lead run from the output terminals to the bell or relay. A diode 1N4148 should also be connected across the output terminals to suppress back e.m.f. through Tr4; diode plus to collector.

Connections for OC71, OC81: Collector nearest spot, then base, emitter.

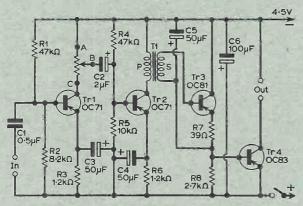


Fig. 1: Circuit diagram of the amplifier

components

Miscellaneous

Miniature 40 ohm speaker Perforated srbp board 4in. × 2½in. Screw terminals or sockets

Resistors R1 47kΩ R2 8·2kΩ R3 1·2kΩ R4 47kΩ All ±5% ‡w	R5 R6 R7 R8	10kΩ 1·2kΩ 39Ω 2·7kΩ	
Potentiometer			
VR1 5kΩ with sw	itch S	1 attac	ched
Capacitors			
C1 0.5µF polyeste	er	C4	50μF 6V electrolytic
C2 2µF 6V electro			
C3 50µF 6V elect	rolytic	C6	100μF 6V electrolytic
Transistors			
Tr1 OC71		Tr3	OC81
Tr2 OC71		Tr4	OC83
112 0011		114	000
Transformer			
T1 9-2:1, CT prim	- me 41	- TI	TT Dansure



This alarm gives a warning by means of a bell, buzzer or lamp, so it can be used as a baby alarm, or as an extension for a door-bell or telephone bell. As it is sound operated, no direct connection is necessary to a telephone or other equipment.

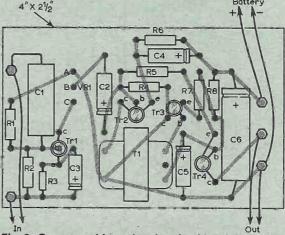


Fig. 2: Component layout and underside wiring shown grev



Case, aluminium or wood, 10in. × 4in. × 3in.



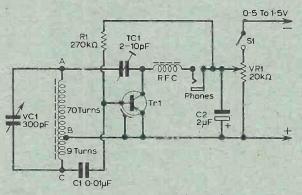


Fig. 1: Circuit diagram

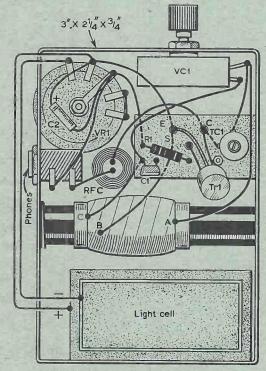
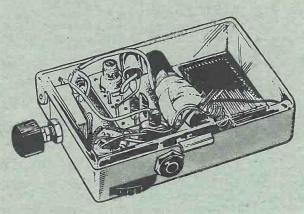


Fig. 2: Component layout and wiring



components

R1	resistor 270 Ω ±10% $\frac{1}{4}$ watt
VR1	potentiometer 20k Ω miniature edge control with switch S1
C1	capacitor 0·1μF low voltage
C2	capacitor 2µF 6V or higher electrolytic
VC1	variable capacitor 300pF mica dielectric
TC1	trimmer capacitor 2-10pF screw driver control
Tr1	transistor AF117 or similar pnp type
RFC	R.F. cored choke 5mH
	Ferrite rod 3in. diameter, 2in. long
	Wire 26 s.w.g. enamelled copper wire for tuning coil
	Phones high impedance with jack plug and socket
	Solar cell 0.5volt or dry cell 1.5V
	Component board 1 in. × in. and box
	PVC connecting wire

Simple regenerative receiver providing headphone reception of local medium wave stations only. Power derived from a mercury cell when energised from daylight or good artificial light. A 1.5 volt dry cell can be used instead.

Tuned circuit consists of 79 turns of 26 s.w.g. enamelled copper wire (A to C) close wound on ferrite rod $\frac{2}{3}$ in. diameter, in parallel with small tuning capacitor VC1. This coil has a tapping (B) nine turns from one end (C). Trimmer capacitor TC1 controls regeneration and is set so that oscillation is just possible with VR1 near maximum voltage setting when using a single 0.5V solar cell.

Tuning coil is wound on thin card or thick paper tube so that it can be moved along ferrite rod for best reception. A few feet of flexible wire aerial connected at A may help reception. Phones should be high impedance 2,000 ohms or more and connected via jack socket on box. Small components are mounted on perforated srbp board and wired underneath. Keep wires short. Minimum recommended box size 3in. x 2¼in. x ¾in. Connections for AF711: collector wire nearest spot, then screen, base, emitter.

COMPONENT SUPPLIES

Components should be readily available from several of our advertisers including the following: Arrow Electronics, Chromasonic Electronics, Electrokit, Electrovalue, Henry's Radio, Home Radio (Components), A. Marshall & Son, Trannies, J. Bull (Electrical) and others.

Sub-standard, unmarked or other components that are not as specified in components lists cannot be guaranteed as suitable substitutes. Constructors should satisfy themselves before buying.