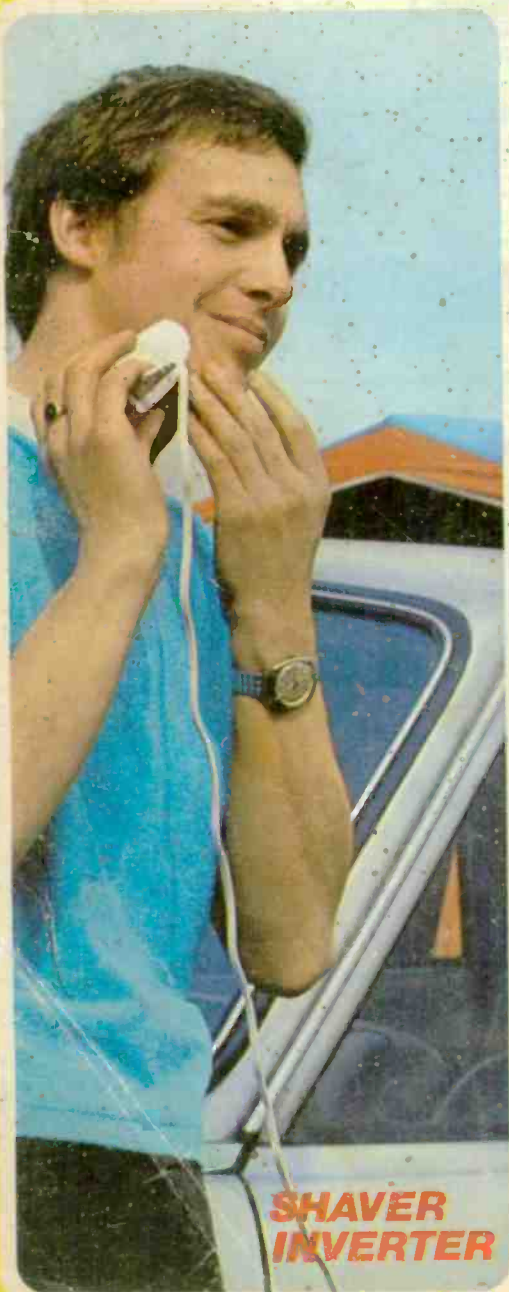


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JULY 72

15p



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Circuit Board with all holes drilled, 7 1/2" x 5 1/2". Central hole 1 1/2" for speaker magnet and cut out for PP9 batt.; Koecker w/change switch and mounting bracket; 2 gang tuning capac.; 3 I.F.S.; Osc. Coil, Ferrite rod with coils and holder, Potentiometer and knob; Circuit Booklet showing component values and positions. All for £1.75 (25p Post). Worth £5.

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Printed circuit board approx. 5 1/2" x 4 1/2" with all holes drilled; wavechange switch/on-off; ferrite rod, aer. coils and holder; vol. control; 3-gang capacitor for tuning; L.W. & M.W. coils R.F. & AER; 4 trimmers; 1st and 2nd I.F. coils; osc. coil; 2 operating knobs; booklet showing all component values and circ. dia.; all for £2 (post 25p).

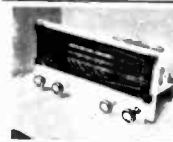
Miniature A.M. transistor tuning gang 250+250pt; 1 1/2" x 1 1/2" x 1"; gearing 3:1 to 3/8" dia. moulded bush; plastic dust cover; Plessey; 25p post paid.

STEREO AMPLIFIER Type SHV—2 x 3 watts

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3 Wave band long-med-short, Gram., 200-250V. A.C. Ferrite aerial. Chassis 13 x 7 x 6in. Dial 13 x 4in. Double wound mains transformer 5 valves; ECH81, EF89, EBC81, EL84, EZ80. Price £10.63. (37p P. & P.) Output trans. for 3-ohm speaker. Some slightly tarnished at £10 carr. pd.

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280-0-280V 60MA. 6.3V 2jA. 6.3V 700mA £1 (27p)
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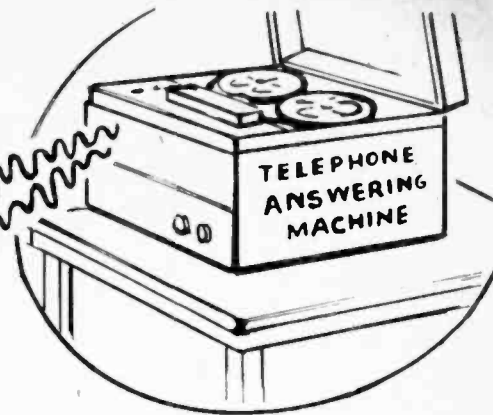
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Sinclair PRO602 x Z30/PZ5	£15.00
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Sinclair 2000 Mk. II	£21.50
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Wharfedale Linton	£37.50
Goodmans Max Amp	£37.95
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Alpha Highgate 150	£44.25
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Please add £1.25 P. & P. per pair

Amstrad 138	£15.95
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Wharfedale Melton 2	£47.45
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Celestion Ditton 15	£33.50
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Goodmans Double Maxim	£48.25
Goodmans Mezzo 3	£44.95
Goodmans Magister	£74.00
Sinclair Q16	£12.50

£3.20*



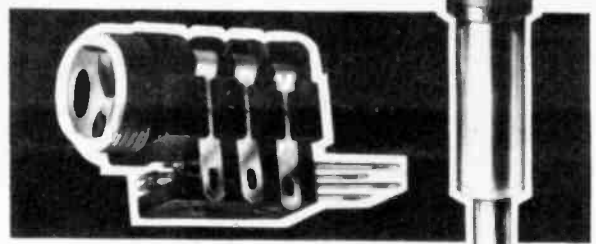
Plus 35p p. & p. Finished in teak veneer with tinted dust cover fully assembled. For Garrard SP25; 2025TC; 3000; AT60; 2000; 2500; 3500; 5100; 1025; SL65B; Also for McDonald MP60 and others. For AP76; AP75; SL728; SL75; SL95B; £4.20 plus 35p P. & P. Also finished in walnut to match Japanese equipment—at no extra.

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Tune into the world with this amazing communications receiver. A truly exceptional unit in performance and looks—leatherette with stainless steel trim. Looks good anywhere. Use either as a portable with standard batteries or plug it directly into 220-240 volt domestic mains supply. 14 Transistors; 9 diodes; thermistor. Internal ferrite rod antenna plus telescopic aerial. Separate tone, volume and tuning controls with push-button selectors for the 8 WAVEBANDS. Complete with Hi-Fi earphone for personal listening. Frequency ranges: Long wave 150-350Kcs. Medium 353-1600Kcs. Marine 1.6-5.5Mc. Short Wave 12-24Mc. FM/VHF 88-108Mc. Aircraft 108-135 Mc. PUBLIC SERVICE BANDS 135-174Mc. Fully guaranteed.

N.B.—The Ministry of Post & Telecommunications has pointed out that a licence (not generally available to the public) is required for reception of transmissions by Fire Brigade, Aircraft, Shipping, etc.

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Everyday Electronics, July 1972



DRILL CONTROLLER
NEW IKW MODEL
 Electronically changes speed from approximately 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. \$1.50 plus 13p post and insurance. Made up model also available. \$2.25 plus 13p post & p.

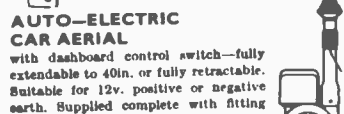
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220/240v. 50 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10 amps. Extremely well made by a German Electrical Company. Overall size 2 1/2 x 2 x 2in. \$1 each.



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Double Leaf Contact. Very slight pressure closes both contacts. 5p each, 60p doz. Plastic push-rod suitable for operating. 5p each, 45p doz.



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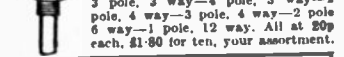
with dashboard control switch—fully extendable to 40in. or fully retractable. Suitable for 12v. positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. \$5.75 plus 25p post and ins.

TOGGLE SWITCH

3 amp. 250v. with fixing ring 7 1/2 each, 75p doz.

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5 amp changeover contacts, 5p each, 41 doz. 15 amp Model 10p each or \$1.05 doz.



MINIATURE WAFER SWITCHES

2 pole, 2 way—4 pole, 2 way—3 pole, 2 way—4 pole, 3 way—2 pole, 4 way—3 pole, 4 way—2 pole 6 way—1 pole, 12 way. All at 20p each, \$1.80 for ten, your assortment.



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26 yards length 70W. Self-regulating temperature control. 50p post free

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Learn in your sleep: Have radio playing and kettle boiling as you awake—switch on lights to ward off intruders—have warm house to come home to. All these and many other things you can do if you invest in an electrical programmer. Clock by famous maker with 15 amp. on/off switch. Switch on time can be set anywhere in the day on up to 6 hours. Independent 60 minute memory logger. A beautiful unit. Price \$1.95 + 20p p & p or with glass front chrome bezel 75p extra.



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Mini Immersion Heater. 350w 200/240v. Boils full cup in about two minutes. Use any socket or lamp holder. Have at bedside for tea, baby's food, etc. \$1.25, post and insurance 14p. 12v. car model also available same price. Jug heater \$1.50 plus p & p. 14p



SNAP ACTION SLIDE SWITCH

Rated 5a. 240v. Made by Arrow. Type fitted in the handles of electric drills, vacuums, etc. 5p each, 10 for 45p.

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For digital instruments, counters, timers, clocks, etc. Hi-vac XN. 3. Price \$1.45 each, 10 for \$13.

12 WAY SUB-MINIATURE MULTI-CORE CABLE

7-0076 copper cores each core P.V.C. insulated and of different colour. P.V.C. covered overall and approx. 3/16in. thick. Price 20p per yard.

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Almost zero resistance in sunlight increases to 10 K Ohms in dark or dull light, epoxy resin sealed. Size approx. 1in. dia. by 1/2in. thick. Rated at 50m MW, wire ended. 45p with circuit. Also ORP 12 light cell 45p.

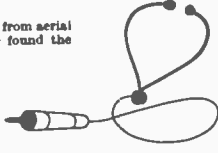


CAPACITOR DISCHARGE CAR IGNITION

This system which has proved to be amazingly efficient. We offer a kit of parts as PW circuit \$5.95 + 20p. De-luxe model with prepared circuit boards \$8.95. When ordering please state whether for positive or negative systems. Also available, ready made ignition systems for 6v vehicles. \$5.95 plus 20p.

ELECTRONIC IGNITION

RADIO STETHOSCOPE
 Easiest way to fault find—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio, TV, amplifier, anything—complete kit comprises two special transistors and all parts including probe tube and crystal earpiece. \$3—twin stethoscope instead of earpiece 75p extra post and ins. 20p.



STANDARD WAFER SWITCHES

Standard size 1 1/2" wafer—silver-plated 5-amp contact, standard 1" spindle 2" long—with locking washer and nut.

No. of Poles	2 way	3 way	4 way	5 way	6 way	8 way	9 way	10 way	12 way
1 pole	40p	40p	40p	40p	40p	40p	40p	40p	40p
2 poles	40p	40p	40p	40p	40p	40p	40p	40p	40p
3 poles	40p	40p	40p	40p	70p	70p	70p	85p	85p
4 poles	40p	40p	40p	70p	70p	70p	70p	\$1.20	\$1.20
5 poles	40p	40p	70p	70p	70p	85p	85p	\$1.45	\$1.45
6 poles	40p	70p	70p	70p	85p	\$1.20	\$1.20	\$1.95	\$1.95
7 poles	70p	70p	70p	85p	\$1.20	\$1.20	\$1.20	\$2.20	\$2.20
8 poles	70p	70p	85p	\$1.20	\$1.20	\$1.20	\$1.20	\$2.20	\$2.20
9 poles	70p	70p	85p	\$1.20	\$1.45	\$1.45	\$1.45	\$2.45	\$2.45
10 poles	70p	70p	85p	\$1.20	\$1.45	\$1.45	\$1.45	\$2.70	\$2.70
11 poles	70p	85p	\$1.20	\$1.20	\$1.70	\$1.70	\$1.70	\$2.95	\$2.95
12 poles	70p	85p	\$1.20	\$1.20	\$1.70	\$1.70	\$1.70	\$3.20	\$3.20

THIS MONTHS SNIP

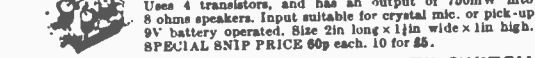
13 AMP TWIN GANG SOCKETS

Offered at less than wholesale price your opportunity to replace those dangerous adaptor—brown bakelite flush mounting—standard fitting. Unswitched 20p each, separately switched 30p each. Separately switched and with neon on/off indicators 45p each. Single sockets unswitched 10p each. Less 10% ten or more + 20p postage if order under \$5.



THYRISTOR LIGHT DIMMER

For any lamp up to 200 watt. Mounted on switch plate to fit in place of standard switch. Virtually no radio interference. Price \$2.50 plus 20p post and insurance.



MULLARD AUDIO AMPLIFIER MODULE

Uses 4 transistors, and has an output of 750mW into 8 ohm speakers. Input suitable for crystal mic. or pick-up 9V battery operated. Size 2in long x 1 1/2in wide x 1in high. SPECIAL SNIP PRICE 60p each, 10 for \$5.

HORSTMANN 'TIME & SET' SWITCH

(A30 Amp switch.) Just the thing if you want to come home to a warm house without it costing you a fortune. You can delay the switch on time of your electric fire, etc. up to 14 hours from setting time or you can use the switch to give a boost on period of up to 3 hours. Equally suitable to control processing. Regular price probably around \$3. Special snip price \$1.50 post and ins. 25p.

SHAVER INVERTER HORSES FOR COURSES ELECTRONOME

and other featured projects. To receive these kits quickly send quoted approx. price and any change due will be refunded.

24-HOUR TIME SWITCH

Made by Smiths, these are AC mains operated, NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be built into box with 13A socket. Two completely adjustable time periods per 24 hours, 5A changeover contacts will switch circuit on or off during these periods. \$2.50 post and ins. 25p. Additional time contacts 50p pair.

INTEGRATED CIRCUIT BARGAIN

A parcel of integrated circuits made by the famous Flessey Company. A once-in-a-lifetime offer of Micro-electronic devices well below cost of manufacture. The parcel contains 5 ICs all new and perfect, first-grade device, definitely not sub-standard or seconds. 4 of the ICs are single silicon chip GP amplifiers. The 5th is a monolithic NPN matched pair. Regular price of parcel well over \$5. Full circuit details of the ICs are included and in addition you will receive a list of many different ICs available at bargain prices 25p upwards with circuits and technical data of each. Complete parcel only \$1 post paid. **DON'T MISS THIS TERRIFIC BARGAIN.**

BATTERY CONDITION TESTER

Made by Mallory but suitable for all batteries made by Ever Ready and others, most of which are zinc carbon types but also mercury manganese—nicad—silver oxide and alkaline batteries may be tested. The tester puts a dummy load on the battery and the meter scale indicates the condition depending upon which section the pointer "reads". The section reads "replaces", "weak" or "good". The tester is complete in its case, size 3 1/2" x 6 1/2" x 2" with leads and prods. Price \$1.75 plus 20p postage.



Where postage is below \$5 add 20p over \$5 add 50p. Semi-conductors add 5p post. Over £1 post free. S.A.E. with enquiries please.

KITS FOR PREVIOUS PROJECTS

Unless otherwise stated, kits contain electronic parts only. The case and special items can be obtained locally. Also batteries are not included. Kits may be returned for refund if construction has not been started. We reserve the right to substitute components should deliveries be protracted so as to avoid undue delay.

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- SEAP INDICATOR \$2.75
- WINDSCREENS WIPER CONTROL \$2
- RECORD PLAYER. Amplifier components only. \$5.50
- DEMO DECK \$6.75 POST PAID
- FUZZ BOX \$1.95
- PHOTOGRAPHIC COLOUR TEMPERATURE METER \$3.65
- ASTRON RADIO \$2
- REMOTE TEMPERATURE COMPARATOR \$4.25
- ELECTRO LAUGH \$2
- AUTO ALERT \$2.50
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- BOLL MOISTURE METER \$3.00
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EDUCATIONAL KITS—all with pictorial instructions



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 Eagle educational kits. Japanese made, these are excellent value for money. We do not expect to be able to repeat this offer once stocks are sold. Brief description of each kit is given below and with 3 kits or more we give FREE an accurate 11 piece balance kit. Price of kits 50p each post paid. Special price for all 7 kits \$2.50 with free balance kit.

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KA2 Water Pump Kit. Thirteen parts. Top of pump is transparent so that operating parts may be observed. Small parts are brightly colored so they can be seen easily when working. Three types of pump may be made: Lift pump, Force Pump and Force Pump with reservoir and nozzle.

KA3 Buzzer Kit. Eleven parts. Transparent covers allow the operation of buzzer to be seen. Illustrates and teaches how electromagnetism with an automatic switch results in a operating buzzer.

KA4 2-Pole Magnet Kit. Twenty-four parts, including enamel wire, armature and pole piece, etc. Motor operates from 1 1/2 volt battery. Illustrates and teaches how electro-magnetism operates a motor.

KA7 Electro-Magnet Kit. Fifteen parts, includes compass. Makes two electro-magnets, one with one layer of wire and one with several layers of wire. Picks up tacks, nails and any small parts showing how magnetism works.

KA8 Current and Resistance Kit. Twenty-nine parts, including benzen and light bulb. Conduct interesting and educational projects to learn the application of "OHM'S LAW" and see the difference in current and resistance with different types and lengths of wire.

KA9 Bell Kit. Eight parts, including bell and push button switch. Build a complete electric bell and see how the hammer is triggered to make the bell ring.

PULSE GENERATORS

Sectronic, made by Smiths. Operated by single 1.5 volt battery or transformer and rectifier. Two models, one gives 10 pulses per second the other gives 5. In plastic enclosure, size approx. 4" x 1 1/2" x 1 1/2" deep. Price \$2 each 10 for \$16.

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 Mains Transformer. Primary 240v. tapped 220v. Secondary 20v. 1 amp. Price 60p each or 10 for \$5.40.

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B81	10	Reed Switches, mixed types large and small	50p
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H4	250	Mixed Resistors. Approx. quantity counted by weight	50p
H7	40	Wirewound Resistors. Mixed types and values.	50p
H8	4	BY127 Sil. Recs. 1000 PIV. 1 amp. plastic	50p
H9	2	OCPT1 Light Sensitive Photo Transistor	50p
H12	50	NKT155/259 Germ. diodes, brand new stock clearance	50p
H28	20	OC200/1/2/3 PNP Silicon uncoated TO-5 can	50p
H30	20	1 Watt Zener Diodes. Mixed Voltages 6.8 - 43V.	50p
H35	100	Mixed Diodes, Germ. Gold bonded, etc. Marked and Unmarked.	50p
H38	30	Short lead Transistors, NPN Silicon Planar types.	50p

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B86	50	Sil. Diodes sub. min. IN91 and IN916 types	50p
B88	50	Sil. Trans. NPN, PNP equiv. to OC200/1 2N706A, BSY95A, etc.	50p
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H15	30	Top Hat Silicon Rectifiers. 750mA. Mixed volts	50p
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AC126	0-15	OC171	0-23
AC127	0-17	OC200	0-25
AC128	0-15	OC201	0-25
AC176	0-20	2G301	0-13
ACY17	0-20	2G303	0-13
AF239	0-30	2N711	0-50
AF186	0-20	2N1302-3	0-13
AF139	0-20	2N1304-5	0-17
BC154	0-20	2N1306-7	0-20
BC107	0-10	2N1308-9	0-22
BC108	0-10	2N3819FET	0-45
BC109	0-10	2N4416FET	0-35
BF194	0-15		
BF274	0-20		
BFY50	0-15	Power Transistors	0-50
BSY25	0-13	OC20	0-30
BSY26	0-13	OC23	0-25
BSY27	0-13	OC25	0-25
BSY28	0-13	OC26	0-25
BSY29	0-13	OC28	0-30
BSY95A	0-10	OC35	0-25
OC41	0-15	OC36	0-37
OC44	0-13	AD149	0-30
OC45	0-10	AUY10	1-25
OC71	0-10	2S024	0-25
OC72	0-10	2N3055	0-50
OC81	0-13	Diodes	
OC81D	0-13	AA42	0-10
OC83	0-18	CA95	0-07
OC139	0-18	OA79	0-07
OC140	0-13	OA81	0-07
	0-15	IN914	0-04

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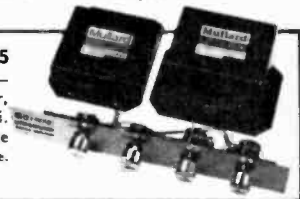
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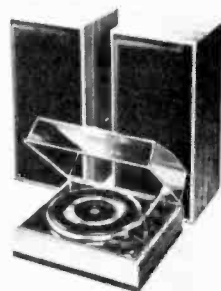
Speakers Duo Type II

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100v	0.33 µF	6p	25v	10 µF	7p
100v	0.47 µF	10p	25v	100 µF	9p
100v	0.68 µF	15p	25v	220 µF	11p
250v	0.01 µF	5p	25v	170 µF	14p
250v	0.015 µF	5p	25v	1000 µF	22p
250v	0.022 µF	5p	25v	2200 µF	42p
250v	0.033 µF	6p	35v	4.7 µF	7p
250v	0.047 µF	6p	35v	220 µF	14p
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AD162	27p	25p	NKT212	24p	19p	1N4004	8p	7p
AP139	28p	26p	NKT213	24p	19p	1N4005	10p	9p
BC107	9p	8p	NKT214	19p	17p	1N4006	12p	11p
BC108	8p	7p	NKT218	24p	19p	1N4007	18p	16p
BC109	8p	8p	NKT219	24p	19p	1N4148	4p	3p
BC147	8p	7p	NKT223	26p	20p	2N1302	16p	15p
BC148	8p	7p	NKT224	21p	18p	2N1304	21p	20p
BC149	8p	7p	NKT242	14p	12p	2N1613	14p	13p
BCY70	14p	14p	NKT243	51p	44p	2N1711	15p	14p
BCY71	20p	19p	NKT401	70p	56p	2N2904	20p	20p
BCY72	14p	12p	NKT402	75p	59p	2N2905	24p	22p
BDY20	91p	73p	NKT403	64p	50p	2N2966	19p	18p
BFX29	24p	23p	NKT453	41p	33p	2N2907	22p	21p
BFX50	19p	18p	OA47	6p	5p	2N3052	17p	16p
BFY51	18p	17p	OA79	6p	5p	2N3054	49p	47p
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METER BARGAINS



MODEL GT-800 MULTIMETER
A precision made pocket sized test meter, ideally suited for testing electronic circuits or electronic appliances. Supplied complete with test lead and batteries. RANGES—DC Voltages: 10, 50, 250, 1,000V (1,000 opV). AC Voltage: 10, 50, 250, 1,000V (1,000 opV). DC Current: 1mA, 100mA (Resistance: 0-150K ohms. Decibel: -10 to +22dB (at AC 10V range) £2-47. P. & P. 25p.



MULTIMETER 20,000 O.P.V.
Features large easy-to-read meter, wide choice of ranges. With test leads, batteries and manual. Size 4 1/2" x 3 1/2" x 1". RANGES D.C. Voltages 0.5-25-50-250-500-2500v. A.C. Voltages 0.5-15-50-100-500-1000v. D.C. Current: 0.50uA 2.5mA-250mA. Resistance: 0-6000 ohms 0-6 megohms (500 ohms and 30 Kohms, at centre scale). Capacity: 100uF to -0.001uF. 600Hz to 1KHz. Decibels: -20 to +22dB. £4-90. P. & P. 25p.



MODEL CT-620 MULTIMETER
RANGES—DC Voltages: 0.5, 25, 100, 500/1,000V (20,000 ohms/V). AC Voltages: 0.5, 25, 100, 500, 1,000V (10,000 ohms/V). DC Current: 0, 50uA, 0.5, 5, 50, 500mA. Resistance: 0, 6k, 600k, 6M, 60M ohms. Decibels: -20 dB to +62 dB in 5 ranges. £5-02. P. & P. 25p.



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A must for all tape users! Tape heads become permanently magnetized with constant use: this leads to background noise that prevents perfect recordings. Simply applied to recording head the V-313 leaves head free of magnetism. Cleans any tape head in seconds. **£1-72** P. & P. 15p.

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SPECIALLY MANUFACTURED IN U.S.A. FROM EXTRA STRONG PRE-STRETCHED MATERIAL. THE QUALITY IS UNEQUALLED. TENSILINED to ensure the most permanent base. Highly resistant to breakage, moisture, heat, cold or humidity. High polished splice free finish. Smooth output throughout the entire audio range. Double wrapped attractively boxed.

LP3 3" 250'	P.V.C.	28p	LP8 5 1/2" 1200'	ACETATE	75p
TT3 3" 450'	POLYESTER	37p	DT8 5 1/2" 1800'	POLYESTER	£1-12
DT3 3 1/2" 600'	POLYESTER	57p	TT8 5 1/2" 2400'	POLYESTER	£1-37
SP5 5" 600'	P.V.C.	42p	SP7 7" 1200'	P.V.C.	62p
LP5 5" 900'	ACETATE	50p	LP7 7" 1800'	ACETATE	75p
DT5 5" 1200'	POLYESTER	75p	DT7 7" 2400'	POLYESTER	£1-25
			TT7 7" 3600'	POLYESTER	£2-50

TAPE SPOOLS 3" 5p, 5 1/2" 7p, 7" 9p.
Post and Packing 3" 3p, 5 1/2" 5p, 5 1/2" 8p, 7" 10p (3 reels and over Post Free).



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- Rogers Ravensbrook II Stereo Amplifier teak **£38-50**
- Rogers Ravensbourne Stereo Amplifier teak **£49-00**
- Metrosound ST20E Stereo Amplifier teak **£25-50**
- Goldring GL72 less cartridge **£22-00**
- Garrard SP25 III with Goldring G800 cartridge **£15-00**



GARRARD SP25 MK III SINGLE RECORD PLAYER F I T T E D GOLDRING 800 MAGNETIC STEREO CARTRIDGE. COMPLETE IN TEAK FINISH WITH COVER. Total list price over £34.

PREMIER PRICE
£18-50
P. & P. 50p.

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Garrard AP76 less cartridge **£18-80**

Garrard 401 Transcription Unit List £40-15 **£27-40**

Garrard 2025 T/C with Stereo Ceramic Cartridge **£8-50**

Garrard 2025 T/C with Stereo Ceramic Cartridge ready wired in teak plinth with cover **£12-45**

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CARTRIDGE BARGAINS!
Goldring G800H £5.00; G800 £5.50; G800E £9.50; SHURE M3D £4.00; M44E £5.75; M55E £6.50; M75EII £10.90. P. & P. 10p

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(As used in SYSTEM 'ONE' above)

A truly high quality stereo amplifier—compare the specification, compare the price. Output: 5 watts per channel. Frequency response: 30-20,000 Hz - 2 db. Distortion: 1% Output impedance 8 ohms nom. Inputs equalised to R.I.A.A. Magnetic 4mV. Ceramic 100mV. Tuner 100mV. Tape 100mV. Tape out 150mV. Din sockets for inputs and outputs. Controls: Bass, Treble, Volume, Balance, Selector, Mono/Stereo switch. Stereo headphone socket. Attractive slim line design black leatherette cabinet with aluminium front panel. Size 12 1/2" x 6 1/2" x 2 1/2".

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MONO STETHOSCOPE SET Low imp. 52p. P. & P. 10p



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Fitted two 2 1/2" tweeters and crossover network. Impedance 8 or 15 ohm. Handling capacity 10W. Brand new. **£3-47** P. & P. 50p

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Battery operated 4-channel audio mixer providing four separate inputs. Size 6 x 3 1/2" in. suitable for crystal microphone low impedance microphone, with transformer, radio, tape, etc. Max. input 1.5v. Max. output 2.5v. Gain 6 db. Standard jack plug socket inputs, phono plug output. Attractive teak wood grain finish case. **£3** P. & P. 15p



MONO MODEL **£3** STEREO MODEL **£3.47** P. & P. 15p

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C60 (60 min.)	29p	3 for 81p
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P. & P. 10p.

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Enables you to work your transistor radio, amplifier, or cassette, etc. from A.C. mains through this compact eliminator. Just by moving a plug you can select the voltage you require — 6v, 7 1/2v or 9 volts. This means all your transistor power pack applications can be handled by this one unit. Approx. size: 2 1/2" x 2 1/2" x 3 1/2". OUR PRICE — £2.75p + 10p. P. & P. Same model suitably wired for the Philips Cassette — £3.00 + 10p. P. & P.

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Ideal for all those multi-way connections. This plug couples with a standard 8-pin valve holder. Plug .. 12p Socket .. 6p Please include 4p p. & p.

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Made from 18 gauge aluminium 4 sided chassis with corner brackets. All are 2 1/2" depth.
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An Audio Amplifier designed around the TAA621 Linear I.C. —
Supply Voltage .. 8-24V
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100K Double 250K 40p
250K Pole 500K each
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1N Switch 1N
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1 watt lots of 10-13p
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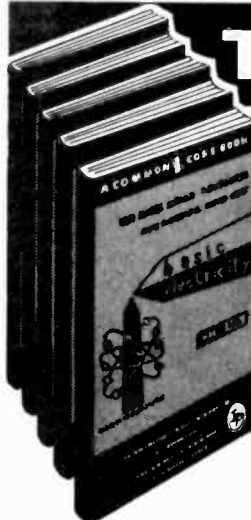
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A few only at this price. 3 1/2" long, 1 1/2" diameter. Merex Terminals. 40p each. Please include 5p p. & p.

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CLEAR PLASTIC METERS

TYPE SW.100
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50μA	\$2-60
50-0-50μA	\$2-45
100μA	\$2-45
100-0-100μA	\$2-55
500μA	\$2-50
1mA	\$2-10
20V. D.C.	\$2-10
50V. D.C.	\$2-10
300V. D.C.	\$2-10
5 amp. D.C.	\$2-10
5 amp. D.C.	\$2-10
300V. A.C.	\$2-10
VU Meter	\$2-75

BAKELITE PANEL METERS

TYPE S-80
80 mm.
square fronts



50μA	\$2-30
50-0-50μA	\$2-10
100μA	\$2-10
100-0-100μA	\$2-60
500μA	\$2-75
1mA	\$2-60
20V. D.C.	\$2-20
50V. D.C.	\$2-60
300V. D.C.	\$2-60
1 amp. D.C.	\$2-60
5 amp. D.C.	\$2-60
300V. A.C.	\$2-60
VU Meter	\$2-37

"SEW" CLEAR PLASTIC METERS

TYPE MR.52P. 4 1/2 in. x 4 1/2 in. fronts.



50μA	\$2-60
50-0-50μA	\$2-10
100μA	\$2-10
100-0-100μA	\$2-60
500μA	\$2-60
1mA	\$2-60
1-0-1mA	\$2-60
5mA	\$2-60
10mA	\$2-60
100mA	\$2-60
1 amp.	\$2-60
5 amp.	\$2-60
10 amp.	\$2-60
20 amp.	\$2-60
30 amp.	\$2-60
10V. D.C.	\$2-60
20V. D.C.	\$2-60
50V. D.C.	\$2-60
300V. D.C.	\$2-60
15V. A.C.	\$2-10
300V. A.C.	\$2-10
8 Meter 1mA	\$2-37
VU Meter	\$2-60
1 amp. A.C.*	\$2-60
5 amp. A.C.*	\$2-60
10 amp. A.C.*	\$2-60
20 amp. A.C.*	\$2-60
30 amp. A.C.*	\$2-60

TYPE MR.52P. 2 1/2 in. square fronts.

50μA	\$2-10
50-0-50μA	\$2-60
100μA	\$2-60
100-0-100μA	\$2-60
500μA	\$2-60
1mA	\$2-60
5mA	\$2-60
10mA	\$2-60
500μA	\$2-60
100mA	\$2-60
500mA	\$2-60
1 amp.	\$2-60
5 amp.	\$2-60
10 amp.	\$2-60
20 amp.	\$2-60
30 amp.	\$2-60
10V. D.C.	\$2-60
20V. D.C.	\$2-60
50V. D.C.	\$2-60
300V. D.C.	\$2-60
15V. A.C.	\$2-10
300V. A.C.	\$2-10
8 Meter 1mA	\$2-37
VU Meter	\$2-60
1 amp. A.C.*	\$2-60
5 amp. A.C.*	\$2-60
10 amp. A.C.*	\$2-60
20 amp. A.C.*	\$2-60
30 amp. A.C.*	\$2-60

TYPE MR.52P. 3 1/2 in. x 3 1/2 in. fronts.

50μA	\$2-37
50-0-50μA	\$2-75
100μA	\$2-75
100-0-100μA	\$2-85
500μA	\$2-85
1mA	\$2-85
5mA	\$2-85
10mA	\$2-85
500μA	\$2-85
100mA	\$2-85
500mA	\$2-85
1 amp.	\$2-85
5 amp.	\$2-85
10 amp.	\$2-85
15 amp.	\$2-85
20 amp.	\$2-85
30 amp.	\$2-85
50 amp.	\$2-85
5V. D.C.	\$2-20
10V. D.C.	\$2-20
20V. D.C.	\$2-20
50V. D.C.	\$2-20
150V. D.C.	\$2-20
300V. D.C.	\$2-20
15V. A.C.	\$2-30
300V. A.C.	\$2-30
150V. A.C.	\$2-30
300V. A.C.	\$2-30
8 Meter 1mA	\$2-37
VU Meter	\$2-87
50mA A.C.*	\$2-80
100mA A.C.*	\$2-80
500mA A.C.*	\$2-80
1 amp. A.C.*	\$2-80
5 amp. A.C.*	\$2-80
10 amp. A.C.*	\$2-80
15 amp. A.C.*	\$2-80
20 amp. A.C.*	\$2-80
30 amp. A.C.*	\$2-80

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SEW EDUCATIONAL METERS



TYPE ED.107. Size overall 100mm x 90mm x 108mm.

A new range of high quality moving coil instruments ideal for school experiments and other bench applications. 3" mirror scale. The meter movement is easily accessible to demonstrate internal working. Available in the following ranges:

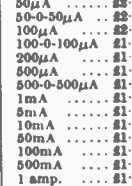
50μA	\$2-60
100μA	\$2-45
1mA	\$2-40
50-0-50μA	\$2-45
1-0-1mA	\$2-40
1A d.c.	\$2-40
5A d.c.	\$2-40
10V. d.c.	\$2-40
20V. d.c.	\$2-80
50V. d.c.	\$2-40
300V. d.c.	\$2-40
50-0-50μA	\$2-45
Dual range	
800mA/5A d.c.	\$2-85
5V/50V d.c.	\$2-85
10V. d.c.	\$2-40
20V. d.c.	\$2-80
50V. d.c.	\$2-40
300V. d.c.	\$2-40
5 amp. d.c.	\$2-40
5 amp. d.c.	\$2-40
300V. A.C.	\$2-10
VU Meter	\$2-75

TYPE MR.52P. 1 1/2 in. square fronts.



50μA	\$2-10
50-0-50μA	\$2-60
100μA	\$2-60
100-0-100μA	\$2-75
500μA	\$2-45
1mA	\$2-60
1-0-1mA	\$2-60
2mA	\$2-60
5mA	\$2-60
10 amp.	\$2-60
5 amp.	\$2-60
10 amp.	\$2-60
20 amp.	\$2-60
30 amp.	\$2-60
10V. D.C.	\$2-60
20V. D.C.	\$2-60
50V. D.C.	\$2-60
300V. D.C.	\$2-60
15V. A.C.	\$2-10
300V. A.C.	\$2-10
150V. A.C.	\$2-10
300V. A.C.	\$2-10
8 Meter 1mA	\$2-37
VU Meter	\$2-10

TYPE MR.45P. 2 in. square fronts.



50μA	\$2-35
50-0-50μA	\$2-10
100μA	\$2-10
100-0-100μA	\$2-60
200μA	\$2-60
500μA	\$2-60
1mA	\$2-60
5mA	\$2-60
10mA	\$2-60
50mA	\$2-60
100mA	\$2-60
500mA	\$2-60
1 amp.	\$2-60
5 amp.	\$2-60
10V. D.C.	\$2-60
20V. D.C.	\$2-60
50V. D.C.	\$2-60
300V. D.C.	\$2-60
15V. A.C.	\$2-10
300V. A.C.	\$2-10
150V. A.C.	\$2-10
300V. A.C.	\$2-10
8 Meter 1mA	\$2-37
VU Meter	\$2-35
1 amp. A.C.*	\$2-60
5 amp. A.C.*	\$2-60
10 amp. A.C.*	\$2-60
20 amp. A.C.*	\$2-60
30 amp. A.C.*	\$2-60

"SEW" BAKELITE PANEL METERS

TYPE MR.55. 3 1/2 in. square fronts.



25μA	\$2-50
50μA	\$2-50
50-0-50μA	\$2-35
100μA	\$2-35
100-0-100μA	\$2-35
500μA	\$2-35
1mA	\$2-35
1-0-1mA	\$2-35
5mA	\$2-35
10mA	\$2-35
50mA	\$2-35
100mA	\$2-35
500mA	\$2-35
1 amp.	\$2-35
5 amp.	\$2-35
10V. D.C.	\$2-35
20V. D.C.	\$2-35
50V. D.C.	\$2-35
300V. D.C.	\$2-35
15V. A.C.	\$2-10
300V. A.C.	\$2-10
150V. A.C.	\$2-10
300V. A.C.	\$2-10
8 Meter 1mA	\$2-37
VU Meter	\$2-35

EDGWISSE METERS

TYPE PE.70. 3 1/2 in. x 1 1/2 in. x 1 1/2 in. deep



50μA	\$2-10
50-0-50μA	\$2-10
100μA	\$2-10
100-0-100μA	\$2-10
200μA	\$2-10
500μA	\$2-10
1mA	\$2-45
300V. A.C.	\$2-45
VU Meter	\$2-60

Send for illustrated brochure on SEW Panel Meters—discounts for quantities.

MULTIMETERS for EVERY purpose!



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 20,000 O.P.V.
 Overload protection
 5/25/100/500/1000 VDC.
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 500A/2500mA. 20K/2 meg
 ohm. - 5 to + 62db.
 \$4-97. P. & P. 15p.



MODEL LT.101 1000 O.P.V.
 0/10/50/250/1000 V. D.C.
 0/10/50/250/1000 V. A.C.
 0/1/100 M.A. 0/150 K ohms.
 \$1-97. P. & P. 15p.



MODEL FL486
 20kΩ/Volt D.C.
 8kΩ/Volt A.C.
 Mirror scale.
 -63/12/30/120/600 V
 D.C. 3/30/120/600 V
 A.C. 50/600A/50/
 600 mA/10/100kΩ
 1 Meg/10 Meg Ω
 -20 to +46db. \$4-97. P & P 15p

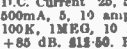
TMK MODEL MD.180
 Mirror scale. 20k/Volt D.C.
 10k Ω Volt A.C. 30/60/300/
 600/2,000 V. D.C. 6/120/
 1,200 V. A.C.
 Current 0-60μA/0-12/0
 300mA. 0-6K/0-6 Meg Ω.
 -20 to + 63 db. \$4-98;
 P & P 15p



MODEL 5025 67 Ranges.
 Giant 6 1/2 in. Meter, Polarity
 Reverse Switch.
 Sensitivity: 50K/Volt D.C.
 5K/Volt A.C. D.C. Volts
 -125, -25, 125, 25, 10, 25,
 50, 125, 250, 500, 1,000V.
 A.C. Volts: 1-5, 3, 6, 10, 25,
 50, 125, 250, 500, 1,000V.



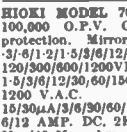
MODEL 500 30,000 O.P.V.
 with overload protection
 mirror scale 0/5/2/5/10/25
 100/250/500/1,000V. D.C.
 0/2/5/10/25/100/250/500/
 1,000V. A.C. 0/50μA/5/50/
 500mA. 13 amp. D.C.
 0/80K/6 Meg/60 Meg Ω.
 \$8-97. Post paid.



D.C. Current 25, 501A, 2.5, 5, 25, 50, 250,
 500mA, 5, 10 amp. Resistance: 2K, 10K,
 100K, 1MΩ, 10 MEG. Decibels: -20 to
 +85 db. \$11-50. P. & P. 171p.



TMK LAB TESTER.
 100,000 O.P.V. 6 1/2 in.
 Scale Buzzer Short Cir-
 cuit Check. Sensitivity:
 100,000 O.P.V. D.C. 5K/
 Volt A.C. D.C. Volts:
 5, -2.5, 10, 50, 250, 1,000
 V. A.C. Volts: 5, 10, 50,
 50, 250, 500, 1,000V.
 D.C. Current: 10, 100μA,
 10, 100, 500mA, 2.5, 10
 amp. Resistance: 1K, 10K, 100K, 10MEG,
 100MΩ. Decibels: -10 to +49 db.
 Plastic Case with Carrying Handle. Size:
 7 1/2 in. x 6 1/2 in. x 3 1/2 in. \$18-90. P. & P. 25p



HIOOKI MODEL 700X
 100,000 O.P.V. Overload
 protection. Mirror scale.
 -3/6/12/15/30/60/120/60/
 120/300/600/1200VDC
 15/50/125/50/100/300/600/
 1200 V.A.C.
 15/300A/5/6/30/50/150/300mA
 6/12 AMP. DC. 2K/200K/2
 Meg/20 Meg ohm -20 to
 +63 db \$13-50. P. & P. 20p.



RUSSIAN 22 RANGE MULTIMETER
 Model U437 10,000 o.p.v.
 A first class versatile in-
 strument manufactured in
 U.S.S.R. to the highest
 standards. Ranges: 2.5/10/
 50/250/500/1000V. D.C. 2.5/
 10/50/250/500/1000V A.C.
 DC Current 100 μA/1/10/
 100mA/1A. Resistance
 300 ohms/3/30/300K/3m Ω.
 *Complete with batteries,
 test leads, instructions and
 sturdy steel carrying case.
 OUR PRICE \$5-97. P. & P. 25p.

ROUND SCALE TYPE PENCIL TESTER



Completely portable, simple
 to use pocket sized tester.
 Ranges 0/3/30/300V AC
 and DC at 2,000 o.p.v.
 Resistance 0-200 ohms.
 ONLY \$1-97 P. & P. 15p

TMK MODEL 117 P.E.T. ELECTRONIC VOLTMEETER



Battery operated,
 11 meg input, 26
 ranges. Large 4 1/2"
 mirror scale. Size
 5 1/2" x 4 1/2" x 2 1/2".
 DC VOLTS 0.5-
 1200V. AC VOLTS
 3-300V RMS. 8-
 800V P.P. DC CUR-
 RENT -12-12MA.

Resistance up to 2000M ohm. Decibels
 -20 to + 61 db. Complete with leads/instruc-
 tions. \$17-50. P. & P. 20p.

TE-20C RF SIGNAL GENERATOR



Accurate wide range sig-
 nal generator covering
 120 Kc/s-500 Mc/s on
 6 bands. Directly cali-
 brated Variable R.F. at-
 tenuator, audio output,
 Xtal socket for calibra-
 tion. 220/240V. A.C.
 Brand new with instruc-
 tions \$18. Carr. 37p.
 Size 140 x 215 x 107
 mm.

TE22 SINE SQUARE WAVE AUDIO GENERATORS



Sine: 20cps to 200
 kc/s on 4 bands.
 Square: 20cps to
 30 kc/s. Output
 impedance 5,000
 ohms, 200/250V.
 A.C. operation.
 Supplied brand
 new and guaran-
 teed with instruc-
 tion manual and leads. \$17-50. Carr. 37p.

TE-20RF SIGNAL GENERATOR



Accurate wide range signal generator cover-
 ing 120 kc/s-260
 Mc/s on 6 bands.
 Directly calibrated
 variable R.F. at-
 tenuator. Operation
 200/240V A.C.
 Brand new with in-
 struction. \$16
 P. & P. 37p. S.A.E. for
 details.



240° Wide Angle 1mA Meters
 MW1-6 60mm square \$2-97;
 MW1-8 60mm square \$2-97;
 P. & P. extra

TO-3 PORTABLE OSCILLOSCOPE



3in. tube. Y amp. Sensitivity
 0.1v p-p/CM. Band-
 width 1-5 cps-1.5 MHz.
 Input imp. 2 meg Ω 25pF
 X amp. sensitivity 0.5v
 p-p/CM. Bandwidth 1-5cps
 -900kHz. Input imp. 2
 meg Ω 20pF. Time base,
 5 ranges 10 cps-300kHz.
 Synchronization. Internal/
 external. Illuminated scale 140 x 215 x 330
 mm. Weight 15lb. 220/240V. A.C. Supplied
 brand new with handbook. \$40-00. Carr. 50p.

HONEYWELL DIGITAL VOLTMEETER VT.100



Can be panel or
 bench

SEMI-CONDUCTORS/VALVES

ALL DEVICES BRAND NEW AND FULLY GUARANTEED

Transistors	2N3415	2N3416	2N3417	2N3418	2N3419	2N3420	2N3421	2N3422	2N3423	2N3424	2N3425	2N3426	2N3427	2N3428	2N3429	2N3430	2N3431	2N3432	2N3433	2N3434	2N3435	2N3436	2N3437	2N3438	2N3439	2N3440	2N3441	2N3442	2N3443	2N3444	2N3445	2N3446	2N3447	2N3448	2N3449	2N3450	2N3451	2N3452	2N3453	2N3454	2N3455	2N3456	2N3457	2N3458	2N3459	2N3460	2N3461	2N3462	2N3463	2N3464	2N3465	2N3466	2N3467	2N3468	2N3469	2N3470	2N3471	2N3472	2N3473	2N3474	2N3475	2N3476	2N3477	2N3478	2N3479	2N3480	2N3481	2N3482	2N3483	2N3484	2N3485	2N3486	2N3487	2N3488	2N3489	2N3490	2N3491	2N3492	2N3493	2N3494	2N3495	2N3496	2N3497	2N3498	2N3499	2N3500	2N3501	2N3502	2N3503	2N3504	2N3505	2N3506	2N3507	2N3508	2N3509	2N3510	2N3511	2N3512	2N3513	2N3514	2N3515	2N3516	2N3517	2N3518	2N3519	2N3520	2N3521	2N3522	2N3523	2N3524	2N3525	2N3526	2N3527	2N3528	2N3529	2N3530	2N3531	2N3532	2N3533	2N3534	2N3535	2N3536	2N3537	2N3538	2N3539	2N3540	2N3541	2N3542	2N3543	2N3544	2N3545	2N3546	2N3547	2N3548	2N3549	2N3550	2N3551	2N3552	2N3553	2N3554	2N3555	2N3556	2N3557	2N3558	2N3559	2N3560	2N3561	2N3562	2N3563	2N3564	2N3565	2N3566	2N3567	2N3568	2N3569	2N3570	2N3571	2N3572	2N3573	2N3574	2N3575	2N3576	2N3577	2N3578	2N3579	2N3580	2N3581	2N3582	2N3583	2N3584	2N3585	2N3586	2N3587	2N3588	2N3589	2N3590	2N3591	2N3592	2N3593	2N3594	2N3595	2N3596	2N3597	2N3598	2N3599	2N3600	2N3601	2N3602	2N3603	2N3604	2N3605	2N3606	2N3607	2N3608	2N3609	2N3610	2N3611	2N3612	2N3613	2N3614	2N3615	2N3616	2N3617	2N3618	2N3619	2N3620	2N3621	2N3622	2N3623	2N3624	2N3625	2N3626	2N3627	2N3628	2N3629	2N3630	2N3631	2N3632	2N3633	2N3634	2N3635	2N3636	2N3637	2N3638	2N3639	2N3640	2N3641	2N3642	2N3643	2N3644	2N3645	2N3646	2N3647	2N3648	2N3649	2N3650	2N3651	2N3652	2N3653	2N3654	2N3655	2N3656	2N3657	2N3658	2N3659	2N3660	2N3661	2N3662	2N3663	2N3664	2N3665	2N3666	2N3667	2N3668	2N3669	2N3670	2N3671	2N3672	2N3673	2N3674	2N3675	2N3676	2N3677	2N3678	2N3679	2N3680	2N3681	2N3682	2N3683	2N3684	2N3685	2N3686	2N3687	2N3688	2N3689	2N3690	2N3691	2N3692	2N3693	2N3694	2N3695	2N3696	2N3697	2N3698	2N3699	2N3700	2N3701	2N3702	2N3703	2N3704	2N3705	2N3706	2N3707	2N3708	2N3709	2N3710	2N3711	2N3712	2N3713	2N3714	2N3715	2N3716	2N3717	2N3718	2N3719	2N3720	2N3721	2N3722	2N3723	2N3724	2N3725	2N3726	2N3727	2N3728	2N3729	2N3730	2N3731	2N3732	2N3733	2N3734	2N3735	2N3736	2N3737	2N3738	2N3739	2N3740	2N3741	2N3742	2N3743	2N3744	2N3745	2N3746	2N3747	2N3748	2N3749	2N3750	2N3751	2N3752	2N3753	2N3754	2N3755	2N3756	2N3757	2N3758	2N3759	2N3760	2N3761	2N3762	2N3763	2N3764	2N3765	2N3766	2N3767	2N3768	2N3769	2N3770	2N3771	2N3772	2N3773	2N3774	2N3775	2N3776	2N3777	2N3778	2N3779	2N3780	2N3781	2N3782	2N3783	2N3784	2N3785	2N3786	2N3787	2N3788	2N3789	2N3790	2N3791	2N3792	2N3793	2N3794	2N3795	2N3796	2N3797	2N3798	2N3799	2N3800	2N3801	2N3802	2N3803	2N3804	2N3805	2N3806	2N3807	2N3808	2N3809	2N3810	2N3811	2N3812	2N3813	2N3814	2N3815	2N3816	2N3817	2N3818	2N3819	2N3820	2N3821	2N3822	2N3823	2N3824	2N3825	2N3826	2N3827	2N3828	2N3829	2N3830	2N3831	2N3832	2N3833	2N3834	2N3835	2N3836	2N3837	2N3838	2N3839	2N3840	2N3841	2N3842	2N3843	2N3844	2N3845	2N3846	2N3847	2N3848	2N3849	2N3850	2N3851	2N3852	2N3853	2N3854	2N3855	2N3856	2N3857	2N3858	2N3859	2N3860	2N3861	2N3862	2N3863	2N3864	2N3865	2N3866	2N3867	2N3868	2N3869	2N3870	2N3871	2N3872	2N3873	2N3874	2N3875	2N3876	2N3877	2N3878	2N3879	2N3880	2N3881	2N3882	2N3883	2N3884	2N3885	2N3886	2N3887	2N3888	2N3889	2N3890	2N3891	2N3892	2N3893	2N3894	2N3895	2N3896	2N3897	2N3898	2N3899	2N3900	2N3901	2N3902	2N3903	2N3904	2N3905	2N3906	2N3907	2N3908	2N3909	2N3910	2N3911	2N3912	2N3913	2N3914	2N3915	2N3916	2N3917	2N3918	2N3919	2N3920	2N3921	2N3922	2N3923	2N3924	2N3925	2N3926	2N3927	2N3928	2N3929	2N3930	2N3931	2N3932	2N3933	2N3934	2N3935	2N3936	2N3937	2N3938	2N3939	2N3940	2N3941	2N3942	2N3943	2N3944	2N3945	2N3946	2N3947	2N3948	2N3949	2N3950	2N3951	2N3952	2N3953	2N3954	2N3955	2N3956	2N3957	2N3958	2N3959	2N3960	2N3961	2N3962	2N3963	2N3964	2N3965	2N3966	2N3967	2N3968	2N3969	2N3970	2N3971	2N3972	2N3973	2N3974	2N3975	2N3976	2N3977	2N3978	2N3979	2N3980	2N3981	2N3982	2N3983	2N3984	2N3985	2N3986	2N3987	2N3988	2N3989	2N3990	2N3991	2N3992	2N3993	2N3994	2N3995	2N3996	2N3997	2N3998	2N3999	2N4000
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Integrated Circuits	FJH111	FJH112	FJH113	FJH114	FJH115	FJH116	FJH117	FJH118	FJH119	FJH120	FJH121	FJH122	FJH123	FJH124	FJH125	FJH126	FJH127	FJH128	FJH129	FJH130	FJH131	FJH132	FJH133	FJH134	FJH135	FJH136	FJH137	FJH138	FJH139	FJH140	FJH141	FJH142	FJH143	FJH144	FJH145	FJH146	FJH147	FJH148	FJH149	FJH150	FJH151	FJH152	FJH153	FJH154	FJH155	FJH156	FJH157	FJH158	FJH159	FJH160	FJH161	FJH162	FJH163	FJH164	FJH165	FJH166	FJH167	FJH168	FJH169	FJH170	FJH171	FJH172	FJH173	FJH174	FJH175	FJH176	FJH177	FJH178	FJH179	FJH180	FJH181	FJH182	FJH183	FJH184	FJH185	FJH186	FJH187	FJH188	FJH189	FJH190	FJH191	FJH192	FJH193	FJH194	FJH195	FJH196	FJH197	FJH198	FJH199	FJH200	FJH201	FJH202	FJH203	FJH204	FJH205	FJH206	FJH207	FJH208	FJH209	FJH210	FJH211	FJH212	FJH213	FJH214	FJH215	FJH216	FJH217	FJH218	FJH219	FJH220	FJH221	FJH222	FJH223	FJH224	FJH225	FJH226	FJH227	FJH228	FJH229	FJH230	FJH231	FJH232	FJH233	FJH234	FJH235	FJH236	FJH237	FJH238	FJH239	FJH240	FJH241	FJH242	FJH243	FJH244	FJH245	FJH246	FJH247	FJH248	FJH249	FJH250	FJH251	FJH252	FJH253	FJH254	FJH255	FJH256	FJH257	FJH258	FJH259	FJH260	FJH261	FJH262	FJH263	FJH264	FJH265	FJH266	FJH267	FJH268	FJH269	FJH270	FJH271	FJH272	FJH273	FJH274	FJH275	FJH276	FJH277	FJH278	FJH279	FJH280	FJH281	FJH282	FJH283	FJH284	FJH285	FJH286	FJH287	FJH288	FJH289	FJH290	FJH291	FJH292	FJH293	FJH294	FJH295	FJH296	FJH297	FJH298	FJH299	FJH300
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VALVES

Valves	6A3	6B2	6C4	6D2	6E5	6F6	6G7	6H6	6I5	6J6	6K6	6L6	6M6	6N6	6P6	6Q6	6R6	6S6	6T6	6U6	6V6	6W6	6X6	6Y6	6Z6	6AA6	6AB6	6AC6	6AD6	6AE6	6AF6	6AG6	6AH6	6AJ6	6AK6	6AL6	6AM6	6AN6	6AO6	6AP6	6AQ6	6AR6	6AS6	6AT6	6AU6	6AV6	6AW6	6AX6	6AY6	6AZ6	6BA6	6BB6	6BC6	6BD6	6BE6	6BF6	6BG6	6BH6	6BJ6	6BK6	6BL6	6BM6	6BN6	6BO6	6BP6	6BQ6	6BR6	6BS6	6BT6	6BU6	6BV6	6BW6	6BX6	6BY6	6BZ6	6CA6	6CB6	6CC6	6CD6	6CE6	6CF6	6CG6	6CH6	6CI6	6CJ6	6CK6	6CL6	6CM6	6CN6	6CO6	6CP6	6CQ6	6CR6	6CS6	6CT6	6CU6	6CV6	6CW6	6CX6	6CY6	6CZ6	6DA6	6DB6	6DC6	6DD6	6DE6	6DF6	6DG6	6DH6	6DJ6	6DK6	6DL6	6DM6	6DN6	6DO6	6DP6	6DQ6	6DR6	6DS6	6DT6	6DU6	6DV6	6DW6	6DX6	6DY6	6DZ6	6EA6	6EB6	6EC6	6ED6	6EE6	6EF6	6EG6	6EH6	6EI6	6EJ6	6EK6	6EL6	6EM6	6EN6	6EO6	6EP6	6EQ6	6ER6	6ES6	6ET6	6EU6	6EV6	6EW6	6EX6	6EY6	6EZ6	6FA6	6FB6	6FC6	6FD6	6FE6	6FF6	6FG6	6FH6	6FI6	6FJ6	6FK6	6FL6	6FM6	6FN6	6FO6	6FP6	6FQ6	6FR6	6FS6	6FT6	6FU6	6FV6	6FW6	6FX6	6FY6	6FZ6	6GA6	6GB6	6GC6	6GD6	6GE6	6GF6	6GG6	6GH6	6GI6	6GJ6	6GK6	6GL6	6GM6	6GN6	6GO6	6GP6	6GQ6	6GR6	6GS6	6GT6	6GU6	6GV6	6GW6	6GX6	6GY6	6GZ6	6HA6	6HB6	6HC6	6HD6	6HE6	6HF6	6HG6	6HH6	6HJ6	6HK6	6HL6	6HM6	6HN6	6HO6	6HP6	6HQ6	6HR6	6HS6	6HT6	6HU6	6HV6	6HW6	6HX6	6HY6	6HZ6	6IA6	6IB6	6IC6	6ID6	6IE6	6IF6	6IG6	6IH6	6IJ6	6IK6	6IL6	6IM6	6IN6	6IO6	6IP6	6IQ6	6IR6	6IS6	6IT6	6IU6	6IV6	6IW6	6IX6	6IY6	6IZ6	6JA6	6JB6	6JC6	6JD6	6JE6	6JF6	6JG6	6JH6	6JI6	6JJ6	6JK6	6JL6	6JM6	6JN6	6JO6	6JP6	6JQ6	6JR6	6JS6	6JT6	6JU6	6JV6	6JW6	6JX6	6JY6	6JZ6	6KA6	6KB6	6KC6	6KD6	6KE6	6KF6	6KG6	6KH6	6KJ6	6KK6	6KL6	6KM6	6KN6	6KO6	6KP6	6KQ6	6KR6	6KS6	6KT6	6KU6	6KV6	6KW6	6KX6	6KY6	6KZ6	6LA6	6LB6	6LC6	6LD6	6LE6	6LF6	6LG6	6LH6	6LJ6	6LK6	6LL6	6LM6	6LN6	6LO6	6LP6	6LQ6	6LR6	6LS6	6
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5 microphone inputs each with individual gain controls enabling complete mixing facilities. Battery operated. 9 1/2" x 8" x 3". Inputs Mic: 3 x 3mV 50K; 2 x 3mV 600 ohm. Phono meg. 4mV 50K. Phono ceramic 100mV 1 meg. Output 250mV 100K. £3-97. P. & P. 20p.



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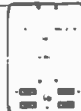
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everyday electronics

PROJECTS...
THEORY.....

VANISHING TRICK

The uninitiated might well be mystified as to how the private constructor obtains the circuit components and other special items he needs for his hobby. The sources of supply are certainly not all that apparent to an outsider.

Taking the country as a whole, outside the larger cities and certain towns it is rare indeed to find a shop dealing exclusively in electronic components. Nor do the numerous radio and television shops that grace every high street any longer offer that incidental service to the private constructor they, or their predecessors did, years ago.

MAIL ORDER

And yet in all, the turnover in electronic components and sundry items for private constructors has never been higher than at present. Likewise, the range and variety of parts offered to the individual has never been so extensive.

So what is the answer to this apparent paradox?

It is, quite simply, mail order. This method accounts for the greater bulk of business transacted in this area today.

AVAILABLE TO ALL

Mail order has considerable advantages to the individual purchaser. He can select from the retailers' advertisements or from their cata-

logues and lists, and order with confidence no matter what part of the country he resides in.

The system has certain snags, it has to be admitted. Occasional delays can cause irritation, and the need often to divide one's requirements among several suppliers can be a bit tiresome. But taking all into account the growth of the mail order retail business has been a great boon, especially to those living in the remote and less populated areas. No matter how isolated, they have the same extensive choice of components as constructors living in the large towns and cities.

UNDER THE BONNET

If the electronics industry had not invented the transistor, we feel sure the automobile industry would eventually have done so!

That ever available 12 volt battery is a prime mover in more senses than one. Since the arrival of the semiconductor it has been the inspiration for countless electronic gadgets.

This month we pamper the motorist yet again. We help him keep up appearances while touring or camping. It's a real face saver.



Our August issue will be published on Friday, July 21

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ART EDITOR J. D. POUNTNEY ● P. A. LOATES ● S. W. R. LLOYD
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**EASY TO CONSTRUCT
SIMPLY EXPLAINED**



VOL. 1 NO. 9

JULY 1972

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**Please
Note~
no back
issues**

Everyday Electronics, July 1972

We regret to inform readers that the publishers are no longer able to supply copies of past issues. Nor will any back issues be available in the future.

Sorry about this—but to avoid possible disappointment we can only urge our readers to place a regular order with their normal supplier; or alternatively to take out an annual subscription (for details see foot of facing page).

SHAVER INVERTER

A 240V a.c. supply for electric shavers from a 12V car battery
by C. J. Mills

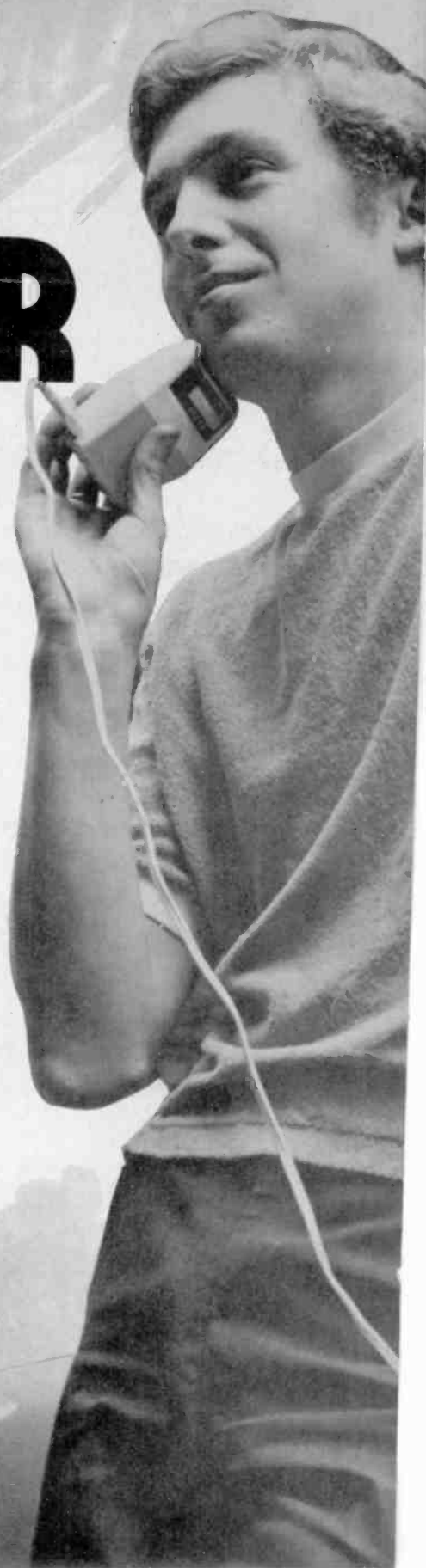
THIS inverter has been specially designed to power any mains type electric razor from a 12 volt car battery. Many inverters provide a d.c. output and will only power a.c./d.c. type razors. Most of the vibrating type razors can only work on a suitable a.c. supply.

Using the design given, a razor can be used anywhere a 12 volt supply (normally a car battery) is available; such as when camping, caravanning or boating. The unit is thus ideal for anyone who enjoys the "outdoor life" during the summer months.

DESIGN

The main problem usually encountered in making a low frequency inverter to drive mains equipment from batteries is the design and construction of a special transformer to suit the power output required. For small inverters with outputs up to about 20 watts, standard mains transformers with a centre tapped secondary winding can be used in reverse, with a separate circuit to drive the power transistors.

The driving circuit must provide two output square waves in anti-phase such as is obtained from a multivibrator.



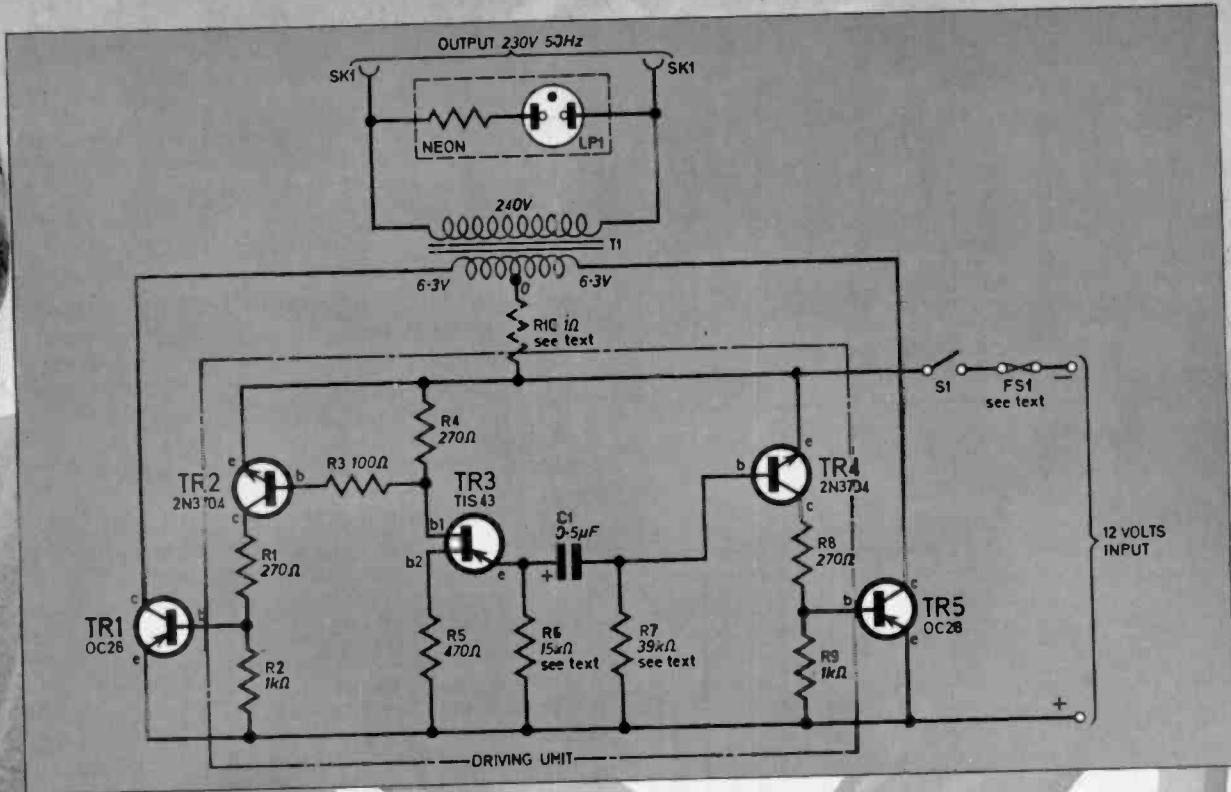


Fig. 1 Complete circuit diagram of the Shaver Inverter.

A unique type of multivibrator circuit developed by the author uses a unijunction because of its excellent frequency stability, in conjunction with two bipolar transistors as shown in the circuit diagram, Fig. 1.

CIRCUIT DESCRIPTION

The basic unijunction oscillator circuit will give a square wave output if a forward biased diode is connected in series with the capacitor.

Components.....

Resistors

R1	270Ω
R2	1kΩ
R3	100Ω
R4	270Ω
R5	470Ω
R6	15kΩ
R7	39kΩ
R8	270Ω
R9	1kΩ
R10	1Ω 5W wirewound (If used—see text)
All ½W ± 10% carbon except where stated	

SEE
**SHOP
TALK**

Capacitor

C1	0.5μF, 16V tantalum
----	---------------------

Semiconductors

TR1	OC28 germanium <i>npn</i> (or OC29—see text)
TR2	2N3704 silicon <i>npn</i>
TR3	TIS43 unijunction
TR4	2N3704 silicon <i>npn</i>
TR5	OC28 germanium <i>npn</i> (or OC29—see text)

Transformer

T1 240V primary with: 16.3V, 0.3A centre tapped secondary (for 5 watts output) or 9V-0-9V, 0.6A secondary (for 10 watts output) or 6.3V-0-6.3V, 0.6A secondary used with R10 in circuit (for 10 watts output)—see text for details and higher power types. In all cases the mains primary is used as the secondary winding in this circuit.

Miscellaneous

FS1	Fuse and holder (see text)
S1	S.p.s.t. toggle switch
LP1	Neon mains indicator lamp
SK1	Two pin mains line socket for connection to shaver, 6 way stand-off tag strip, mica washers and plastic insulation bushes for TR1 and TR5, metal case 4½ x 3½ x 2 inches, plain perforated Veroboard 2½ x 2 x 0.1 inch matrix with Veropins to suit, grommets, wire, 4BA fixings and earth tags.

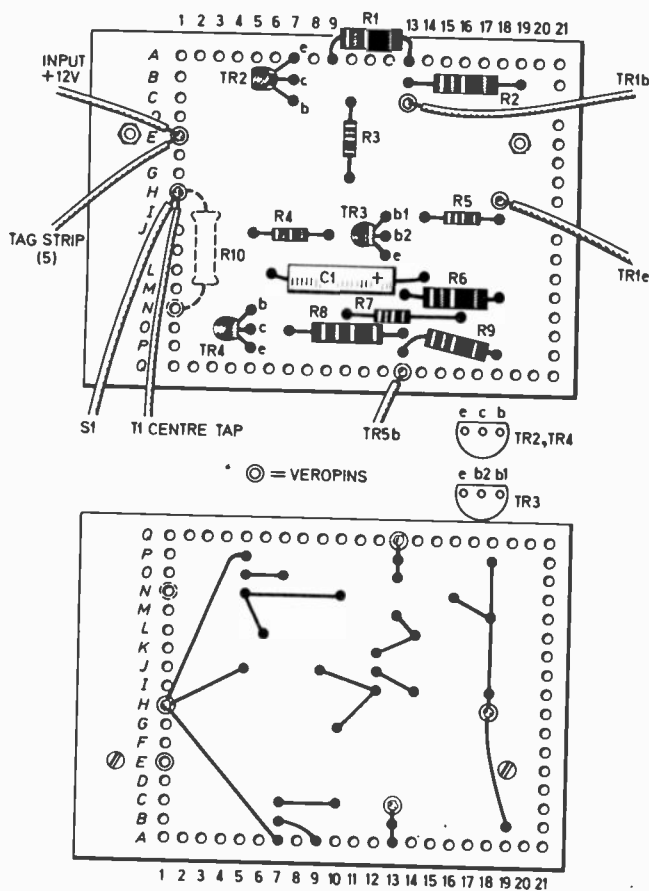


Fig. 2 Layout and wiring of components on the Veroboard.

In Fig. 1 the base, emitter diode of transistor TR4 is used and it is biased "on" by the base resistor R7. The collector is connected to a suitable resistor to provide one of the outputs. A second npn transistor, connected to the b1 base of the unijunction as shown, gives an output in phase opposition to the first.

CIRCUIT ACTION

When the supply voltage is connected the capacitor charges up through the base emitter diode of TR4 and through the 15 kilohm timing resistor, R6, until the trigger voltage of the unijunction is reached. During this charging time TR4 is held on by the charging current.

When the unijunction fires, its emitter voltage drops due to the emitter to base b1 current and this voltage drop is transferred to the base of TR4 by the capacitor, so that TR4 is turned off and the capacitor discharges through the TR4 bias resistor R7. At the same time the unijunction emitter, base b1 current flowing through the base resistance produces a voltage which switches on TR2 which stays on until the capacitor has discharged sufficiently to allow TR4 to conduct.

At this point the unijunction and TR2 are switched off, the capacitor starts charging again and the cycle is repeated.

The outputs from the collectors of TR2 and TR4 are coupled to the power transistors which switch the supply voltage across each half of the transformer alternately.

OUTPUT POWER

Using a 16.3 volt centre tapped 0.3 amp filament transformer with a test load resistance of 12 kilohms an output voltage of about 250 volts (approximately 5 watts) is obtained with a 12V d.c. input—alternatively, an 18 volt 0.6 amp transformer gives an output of 235 volts across 12 kilohms with an input voltage of 13 volts d.c.

For higher wattage outputs (up to 20 watts maximum for this design) a transformer with a 16 volt centre tapped secondary winding rated at 1 amp is required and the power transistors should be changed to OC 29 types.

Alternatively, if a 6.3-0.6-3 volt transformer is more readily available it can be used with a 1 ohm 5 watt resistor (R10) in series with the centre tap as shown dotted in Fig. 1. If this resistor is not used a link is made in its place.

CONSTRUCTION

A medium sized die cast box measuring 2 x 3 $\frac{1}{2}$ x 4 $\frac{1}{2}$ inches is a convenient form of case for the inverter and the power transistors can be mounted on the side to provide a heat sink, if they are suitably insulated by mica washers and plastic bushes.

The components of the driver circuit can be mounted on a piece of plain perforated Veroboard and connected up as shown in Fig. 2, using Veropins for support as shown. The layout is not critical but if it is similar to the circuit it makes checking easier.

The transistors should be soldered into circuit last and protected by using a heat shunt on each lead while soldering.

Wiring of the Veroboard to the remaining components is shown in Fig. 3. The wiring shown does not include R10 which is needed if a 6.3V-0.6.3V transformer is used. If R10 is used it is mounted as shown in Fig. 2 and the wire from T1 centre tap is connected to N1 not H1.

The fuse used depends on the transformer and output power. For a 5 watt unit use a 1 amp fuse, 10 watt use a 2 amp, and for 20 watt use a 5 amp fuse.

The input and output leads are brought out through grommets and a mains neon (LP1) connected across the transformer secondary winding is used as an indicator (mains type neons usually incorporate a resistor as shown in Fig. 1). A small tag strip is added for connection of transformer leads and some of the components.

Continued on page 482

SHAVER INVERTER

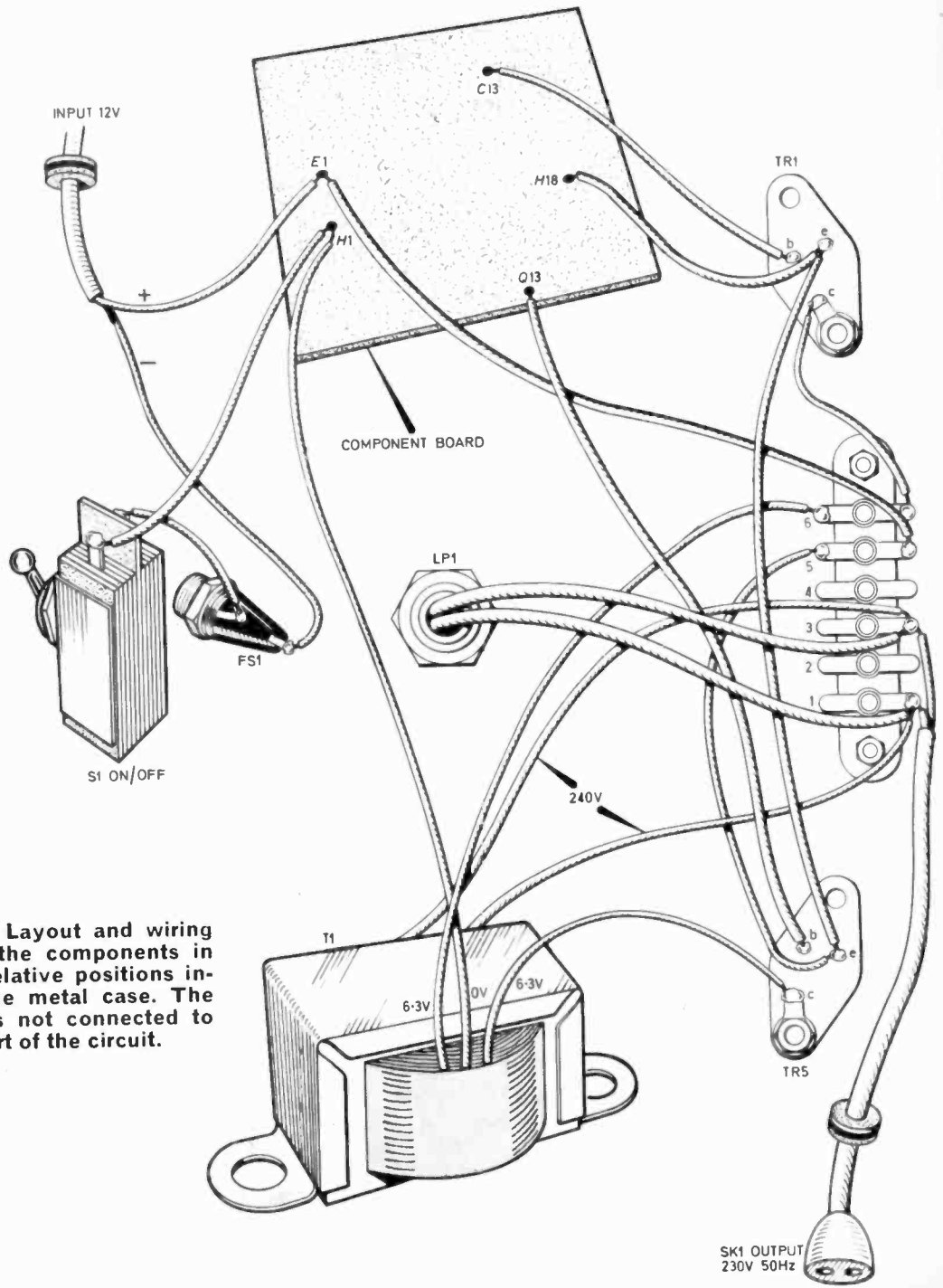


Fig. 3. Layout and wiring of all the components in their relative positions inside the metal case. The case is not connected to any part of the circuit.

The Electron Microscope



By B. V. Lamb

The electron microscope is a powerful tool indeed in the hands of the modern technologist. Its use covers the whole spectrum of science. As man continues to enjoy the results of recent discoveries in his environment, so the electron microscope (E.M.) will play an ever growing part in applied science.

APPLICATION

Application of the E.M. may be split into two main groups, discovery and diagnosis. Often of course, these two merge and overlap. An example of its diagnostic use may be drawn from the electricity generating industry. A steam pipe has burst. What caused it? Was there a flaw in the pipe? Did corrosion eat into the metal? A sample of the pipe seen under the E.M. will reveal the facts.

Biology will serve as an example of the E.M. as an instrument of discovery. Whilst looking at a section of tissue, some new feature of a cell make up might be noticed or some fresh aspect on a certain disease seen.

As we shall see later, there is much more to electron microscopy than merely looking at an image of a specimen. To look is not necessarily to "see"; looking is passive whilst seeing is active. The electron microscopist is a scientist, the image on the screen of his instrument is often the result of much careful planning and reasoning on what he can expect to see.

E. M. FOUNDATIONS

The E.M. owes its development to early work
Heading photograph: the Jeol—JEM 100B electron microscope.

done in the field of electron dynamics—that is, the study of electrons moving under the influence of an applied electric field. (A Cathode Ray tube is an example of applied electron dynamics.)

Electronics and vacuum techniques are vital too. E.M.s have been in use for several decades now but not until the early 1960s were some of the most exciting developments made.

TYPES OF E. M.

Two distinct types of E.M. exist. Both use electrons to bombard the sample. The first type is called the transmission electron microscope (T.E.M.) and this was the earliest E.M. design to appear.

The operation of the T.E.M. is similar to the light microscope in that it has lenses and apertures as has the optical instrument. The difference being of course, that the lenses on the T.E.M. are magnetic and they focus electrons.

The second type of E.M. is the scanning electron microscope (S.E.M.). This microscope is essentially like a closed television system in its working. Early S.E.M.s can be traced back to the 1930s and these were made in-house by universities and ambitious research organisations. It was not until the early 1960s that a commercial S.E.M. appeared.

Both the T.E.M. and the S.E.M. have their relative merits. The recent commercial availability of the S.E.M. although of great interest, has by no means replaced the T.E.M., indeed many laboratories have both instruments. After describing the working principles of these quite different microscopes, the advantages of each will be seen.

COST

Great Britain, Japan, Germany, Holland and the United States of America all produce front line instruments of exceptional specifications. As is to be expected, E.M.s are expensive and the rule "you get what you pay for" applies well here; £5,000 to £250,000 covers the whole range. The very high prices include special attachments and unusually high voltage installations.

An average T.E.M. might cost £25,000 and an S.E.M. of high specification the same. Because of the skills required in operating an E.M. and in preparing samples, any electron microscope unit involves large capital expenditure and running costs.

HOW THE T. E. M. WORKS

The basic essentials of a T.E.M. are shown in Fig. 1. At the top of the microscope sits the electron gun—so called because it emits electrons continuously at very high velocity.

The electron gun consists of the tungsten filament, the shield and the anode. The anode

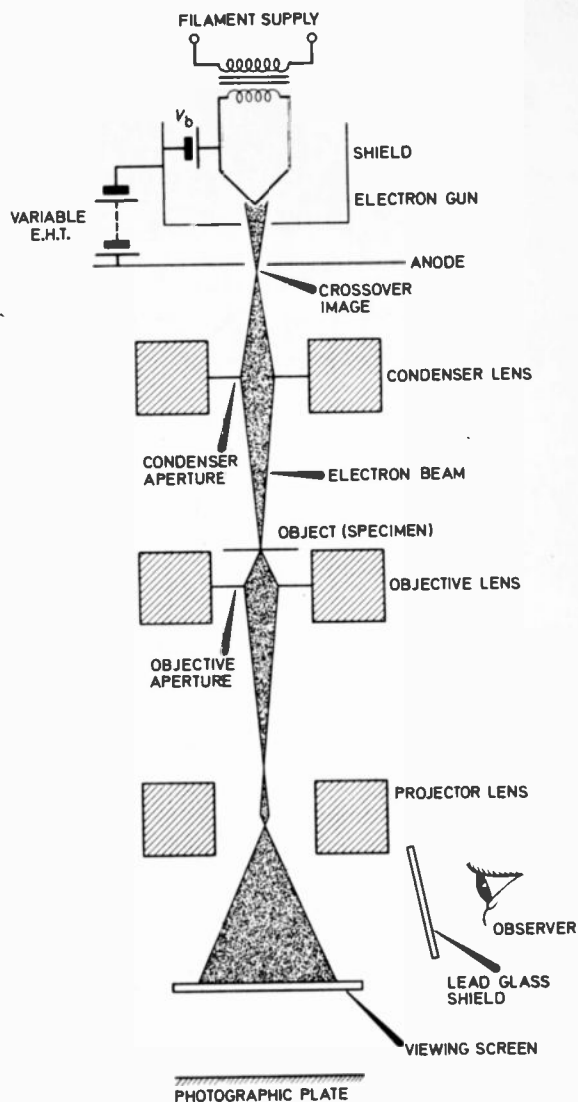


Fig. 1. Basic form of the transmission electron microscope. Additional optical accessories may be added to increase magnification.

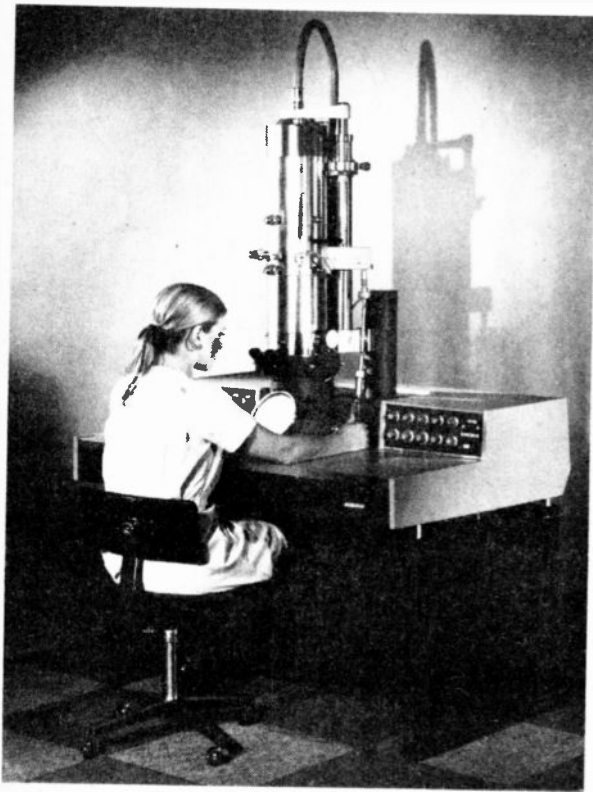
is connected to earth as is the positive side of the high voltage supply. A negative bias (V_b) is maintained between the filament and the shield. When current is supplied to the filament so that it is raised to a high temperature and air is pumped from the system, electrons are accelerated towards the anode.

The shield, being negatively biased, causes the beam of electrons to converge so that a crossover image of the filament is formed in the anode aperture. In this way a beam of electrons is projected from the gun and is now able to be aimed down the microscope.

As soon as the electron beam leaves the electron gun it is already beginning to diverge. The condenser lens is used to focus the diverging beam onto the sample.

This magnetic lens consists of a number of turns of copper wire on an iron ring. By varying the current through the coil the focus can be adjusted. The condenser lens also has an aperture that behaves in a similar way to optical microscope apertures—an opening of between 0.1 and 0.3 mm is typical.

The object (specimen) is held in a special holder either in or near to the objective lens. The finely focused pencil like beam of electrons strikes the specimen; and because the specimen is very thin and the electrons are travelling with great velocity, most of the electrons pass through the specimen. Once into the objective lens the electrons pass through the objective lens aperture (10 to 50 microns diameter) and are again focused to an intermediate image lower down the electron column.



The Philips high-resolution transmission electron microscope (EM201). This instrument can attain a resolution of 7 angstroms.

PROJECTOR LENS

The final lens is the projector and this gives the great magnification that one may expect. This lens projects the electron beam onto a flat glass viewing screen. The viewing screen has a layer of phosphorescent material coated to it; electrons striking the phosphor screen cause it to glow.

Underneath the screen is a compartment to take photographic plates when a permanent

record is required. The operator sits and looks down on the viewing screen through a lead-glass shield. Sometimes external optical magnification is used to increase the image size even more. T.E.M.s can give useful magnifications up to 500,000 times and the best instruments claim to be able to resolve detail down to 2 Angstroms.

The electron microscopist talks in terms of angstroms and microns as the mechanical engineer speaks of the thou. (1/1000 inch). An idea of just how small an angstrom (Å) is can be gathered by measuring the diameter of a human hair and expressing it in angstrom units. A human hair is about 1½ thou. in diameter.

1 Å = 10,000 Microns (10⁻¹⁰ Metre) and 1 thou. = 25.4 microns. Therefore 1½ thou. = 25.4 × 1.5 × 10,000 = 380,000 Å!!!

Although the ability to resolve smaller and smaller in detail is the goal towards which the E.M. manufacturer constantly works, this extremely fine resolution presents the operator with many difficulties. An illustration will help in understanding a major problem.

If we look at an area on an Ordnance Survey map, although the area will be given in fine detail its relation to the rest of the map can only be understood by looking at the whole of the map in "coarse resolution", i.e. taking a broad view of surrounding landmarks etc. So it is with the E.M. operator. Great resolution without knowledge of the image in relation to the whole structure can be meaningless.

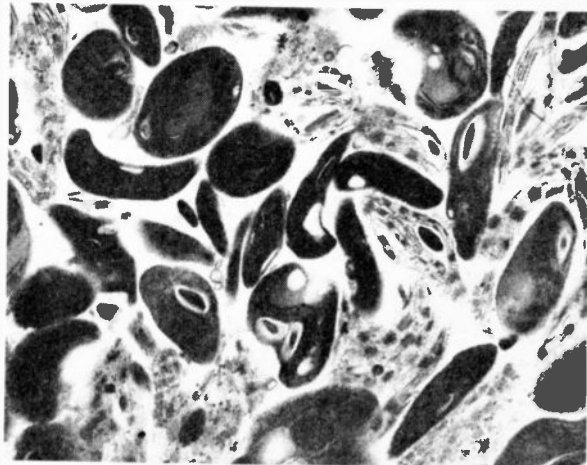
SAMPLE PREPARATION

As we have just seen by considering the basics of the T.E.M. the specimen must:—

1. Be cut thin, i.e. less than 1,000 Å thick.
2. Be able to withstand a vacuum.
3. Be undamaged by electrons striking it.

Considering each of these points separately. A thin slice of the specimen is required so that

A 0.5µm section of spinach chloroplasts at a magnification of 12000x, taken on the AEI, EM7 electron microscope.



most electrons will pass right through to form an image on the fluorescent screen. Actually, detail (contrast) in the sliced specimen is made apparent in the image because some of the electrons are scattered in their journey through it.

All atoms scatter electrons, the amount of scattering increases with atomic weight. As we shall see later, by staining the specimen with heavy atoms, a significant increase in contrast can be obtained.

The second requirement is that the specimen is able to stand up to a vacuum. When air is pumped from the electron column, gases and water vapour are rapidly sucked from the sample.

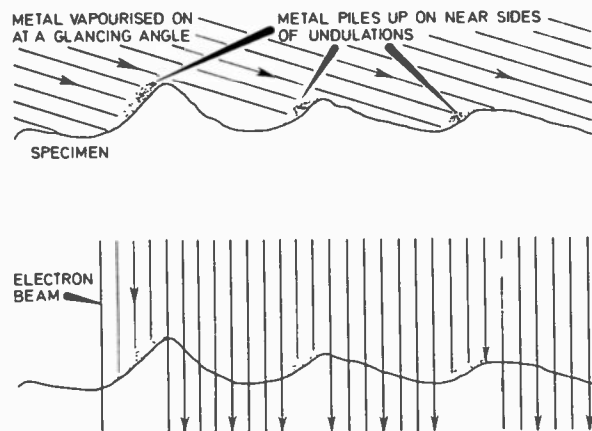
If a water-containing specimen such as a biological sample is subjected to vacuum it would quickly be rendered useless for viewing. Biological specimens are freeze-dried and are fixed in thin films and are then supported on grids of very thin wire. Micrographs are made through one mesh of the gauze.

Sample preparation requires skill and patience and is vital to producing meaningful images. To prepare some biological specimens can take two weeks from the time the sample arrives in its raw state to the moment it can be placed in the sample chamber of the T.E.M. Other samples of course, due to their inert make-up may be viewed with the minimum of preparation time.

REPLICAS

Sometimes it is necessary to produce a replica of the specimen. In this case the specimen surface is etched to produce relief and then the surface is plastic coated or metal is evaporated on. Carbon from an arc may also be used as the coating. The replica is then peeled off and introduced into the microscope sample chamber.

Fig. 2. Method of shadow casting using vaporised metal to provide greatly enhanced details.



As was discussed earlier, if the scattering of electrons in the sample is not sufficient to disclose fine detail (contrast in the image) then the specimen can be stained with a heavy metal. Osmium, atomic number 76, is frequently used.

Another method for showing up fine detail is known as shadow casting. This is achieved by vapourising metal onto the sample at a glancing angle. Metal piles up on the near side of undulations (see Fig. 2), and when the electron beam strikes the sample, greatly enhanced details are evident.

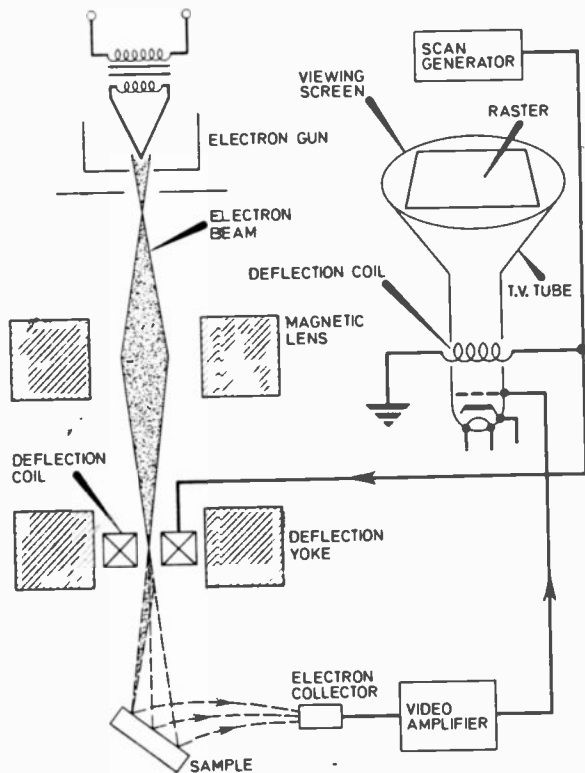


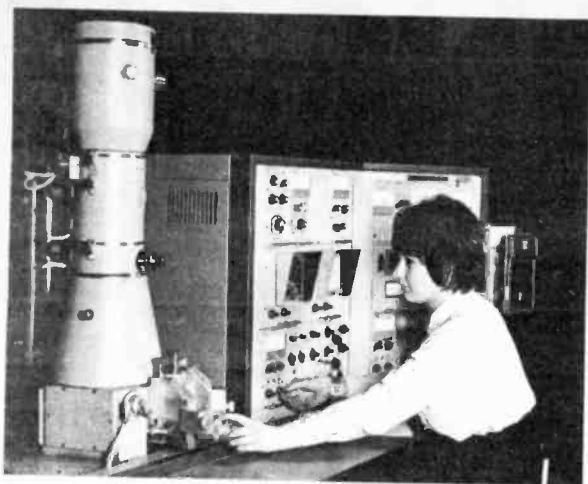
Fig. 3. Basis of the scanning electron microscope. Photographs of the screen can be taken using a special camera.

SCANNING ELECTRON MICROSCOPE

The S.E.M. is essentially a closed circuit T.V. system with refinements (see Fig. 3). Again there is the electron gun emitting electrons at high velocity, and magnetic lenses to focus and magnify. Also aperture plates to sharpen the image are present, just as in the T.E.M.

The inclusion of the deflection yoke and its associated circuitry marks the distinction of the S.E.M. from the T.E.M. The deflection yoke is powered by an a.c. waveform that causes the fine beam of electrons to scan across the sample in a regular way. (The a.c. waveform powering the deflection coil is also coupled to the T.V. monitor. This causes a raster on the T.V. tube.)

This very fine beam of electrons covering an



The Cambridge Scientific Instruments Stereo-scan S4. This is the latest scanning electron microscope from this company.

adjustable area of the sample causes secondary electrons to be emitted which in turn are collected by a secondary electron detector. The secondary electron detector is a device which converts electrons into photons of light which in turn are collected by a photomultiplier. The electrical output from the detector is connected to the T.V. monitor so that the spot causing the raster is modulated with information relative to the specimen surface.

Again, as in the T.E.M. the viewing screen can either be watched by the operator or photographed for a permanent record. Useful magnifications up to 50,000 times can be achieved in the S.E.M. The electron beam energy can vary from as little as 1kV to 50kV.

ADVANTAGES

The main attraction of the S.E.M. is in its ability to produce a three dimensional image of the specimen surface. Great depth of field is also achieved. The reason for these features is that the electron beam striking the surface resembles a fine sharp pin which is able to probe into the irregularities of the specimen. Unlike the T.E.M. the picture is formed by electrons emerging from the surface of the sample.

Although the T.E.M. has good depth of field, the usable depth is limited because the specimen has to be very thin.

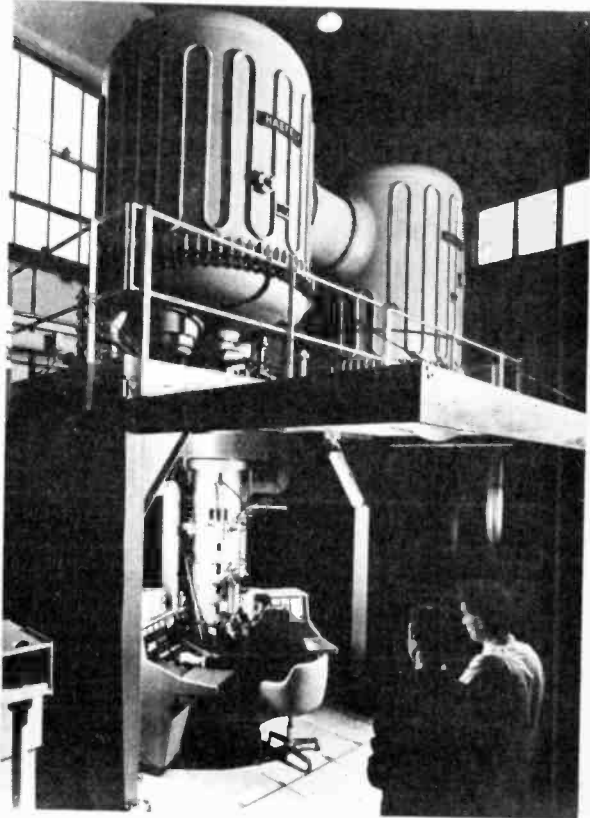
In the S.E.M. sample size is only limited by sample chamber considerations. Because sample slices are not required for the S.E.M. preparation time is dramatically lowered. Preparation for electrically conducting specimens consists of fixing them to the moveable specimen stage with a conducting glue. Biological samples and others that are not conductors need to be made conducting by evaporating a thin film of gold onto them. Coating thicknesses fall in the 10 to 100's

of angstrom region. As with the T.E.M., biological specimens require fixing and drying.

Over the past few years many photographs of sample images produced in the S.E.M. have been published. Many of these excite the imagination as the microscopical region of such objects as the wing of a butterfly or the detail of a nerve cell is revealed in three dimensions.

Key performance characteristics of both the T.E.M. and the S.E.M. will continue to improve as manufacturers strive to meet the demands of modern technology. □

The AEI, EM7 million volt electron microscope installed at the United Kingdom Atomic Energy Authority at Harwell.



PLEASE TAKE NOTE

Bee Counter circuit description—see Readers Letters page.

Potentiometer VRI in the Demo Deck is 100Ω not 300Ω as mentioned last month.

Wash Wipe control second paragraph page 441, the emitter wire of TR 3 should be soldered to J2, not the collector wire as stated.

ELECTRONOME

A simple design giving a performance similar to that of a mechanical metronome.

by F. C. Judd

ASIDE from being a simple exercise in electronics, the Electronome has a real application in music practice, for it produces a sound very like that made by a mechanical metronome and covers the same tempo range of approximately 40 to 225 beats per minute.

The resonant click is loud enough for music practice with piano, guitar, electronic organ and other musical instruments and the tempo rate is continuously variable.

Few components are required and almost any 3 to 5 ohm loudspeaker can be used for reproducing the sound.

CIRCUIT DESCRIPTION

The circuit as shown in Fig. 1 is quite simple and employs only two transistors which are connected to form a multivibrator type oscillator, i.e., one that generates a relatively square waveform signal of large amplitude.

The output to the loudspeaker is taken from TR2 collector via a large capacitor but as the leading edge of the square-wave is very fast and of large amplitude, a quite substantial spike of current is driven through the very low im-



Approximate
cost of
components
£1.75 plus case

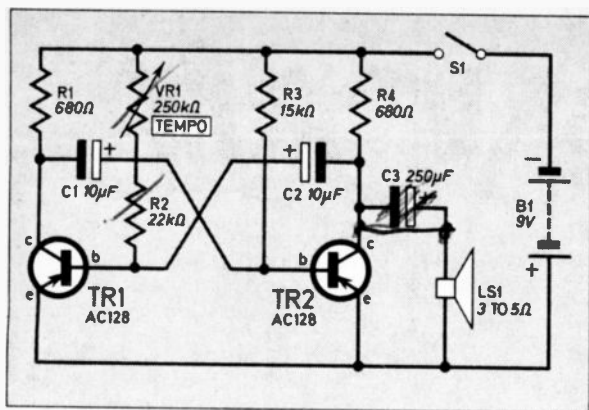


Fig. 1. Complete circuit diagram of the Electronome

pedance speaker coil. The speaker, therefore, responds only once, i.e., to the leading edge of the square-wave and thus produces a single loud click.

The same effect would be produced by momentarily connecting a 9V battery straight across the speaker coil. The multivibrator is in effect doing this repeatedly the repetition rate being variable by means of the tempo control VR1.

CONSTRUCTION

The prototype shown in the photograph is housed in a small box made of $\frac{1}{8}$ inch hardboard with joints at sides, top and bottom strengthened with $\frac{1}{2}$ inch by $\frac{1}{2}$ inch batten, or small blocks of wood. The front panel aperture for the speaker may be covered with any loose weave material. The tempo control VR1 and the on/off S1 switch are mounted on the front panel of the case.

The components for the oscillator are mounted on a piece of plain perforated circuit board $3\frac{1}{2}$ inches by $2\frac{1}{2}$ inches, as shown in Fig. 2, supported on a $\frac{3}{8}$ by $\frac{3}{8}$ inch piece of aluminium angle $3\frac{1}{2}$ inches long. The circuit board is attached inside the box by the aluminium angle.

The component layout and wiring on the board are shown in Fig. 2.

COMPONENT MOUNTING

Commence construction of the circuit board by attaching the positive and negative rails to the underside of the component board. These wires can be 16 or 18 s.w.g. tinned copper wire and they are attached by placing each end through the indicated holes and bending them over on top of the board. The components are mounted by their leads and soldered to the two rails or to each other as indicated in Fig. 2.

Mount all the components except the two transistors, check the layout and wiring with particular reference to the capacitor and battery polarities and, when satisfied that all is correct, mount the transistors.

Use a heat sink on each transistor lead, while it is being soldered, thus preventing the transistor from being overheated. Mount the transistors so that the spot (collector) is toward the negative rail. Connections for the AC128 transistors are also shown in Fig. 2.

The circuit can be checked out before assembly into the case by connecting up VR1 (tempo control), the loudspeaker and battery as shown in Fig. 3. A clearly defined repetitive click should be produced which, with VR1 at zero resistance, should be approximately 225 beats per minute and approximately 40 beats per minute at maximum resistance.

SCALE

Insert all the components in the case and mount the battery using a clip or an elastic band. A scale can be made up similar to that shown in Fig. 4 and calibrated by counting the clicks of the Electronome over a 15 second period.

If the clicks are counted in tens it is just possible to count at a rate of 225 per minute. It should be emphasised that Fig. 4 is given as a **guide only** and should not be used as the actual scale.

A back cover for the box, which can be made from hardboard, will complete assembly but if the box is to be painted or covered in fabric do this before mounting the speaker and controls.

Components....

SEE
**SHOP
TALK**

Resistors

R1 680Ω
R2 22kΩ
R3 15kΩ
R4 680Ω
All $\frac{1}{4}$ W 10% carbon

Capacitors

C1 10μF elect. 12V
C2 10μF elect. 12V
C3 250μF elect. 12V

Variable Resistor

VR1 250kΩ log. carbon

Transistors

TR1 AC128 germanium *pnp*
TR2 AC128 germanium *pnp*

Miscellaneous

S1 s.p.s.t. toggle or slide switch
LS1 3 to 5Ω moving coil loudspeaker approximately 3 to 5 in. diameter
B1 PP9, 9V battery and connector
Pointer knob, Veroboard—plain perforated $3\frac{1}{2} \times 2\frac{1}{2} \times 0.15$ inch matrix, aluminium angle $3\frac{1}{2} \times \frac{3}{8} \times \frac{3}{8}$ inches, wire, materials for case and dial, speaker grill material.

ELECTRONOME

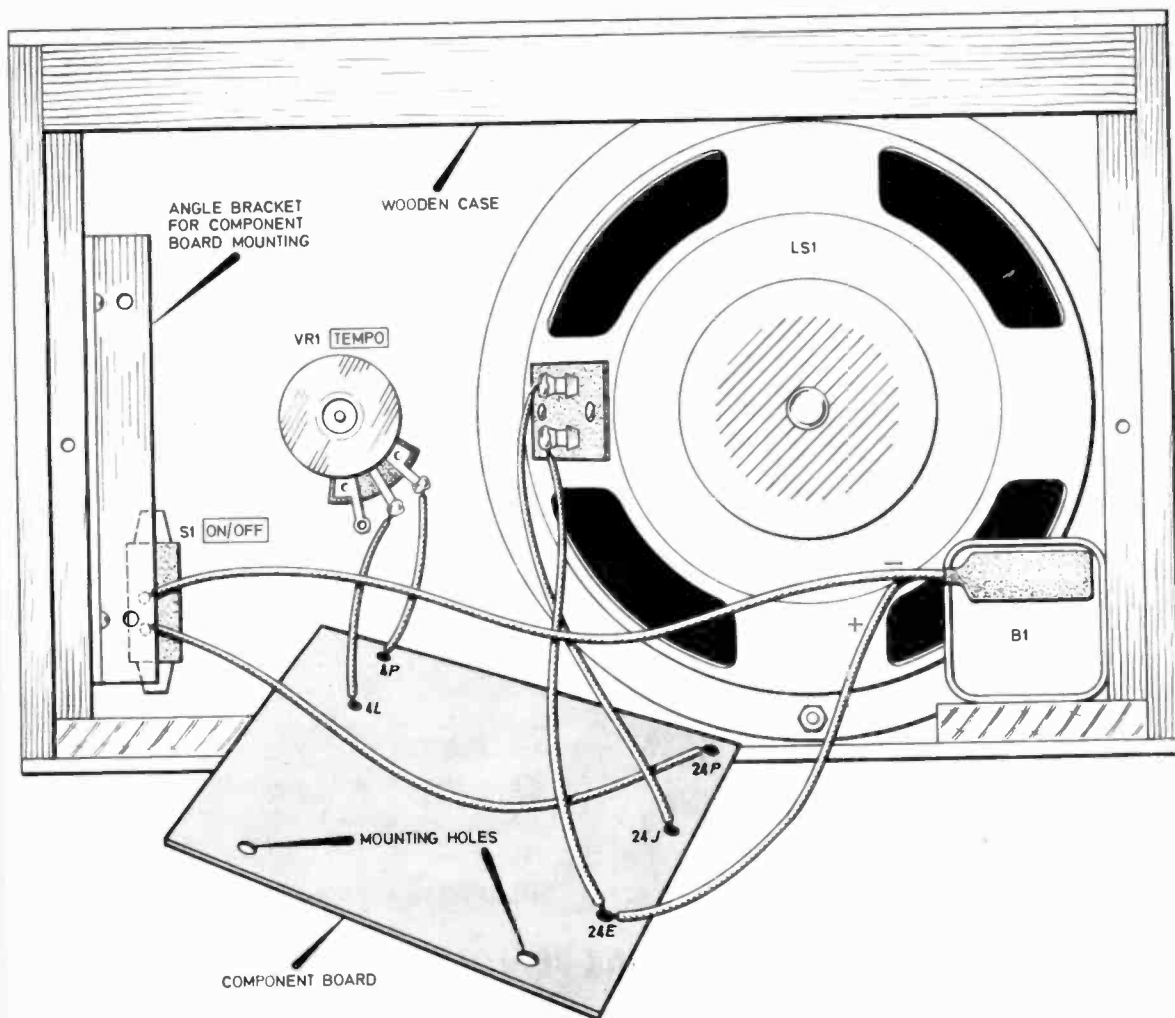


Fig. 3. Layout and wiring of the complete Electronome. The circuit board is shown removed for clarity.

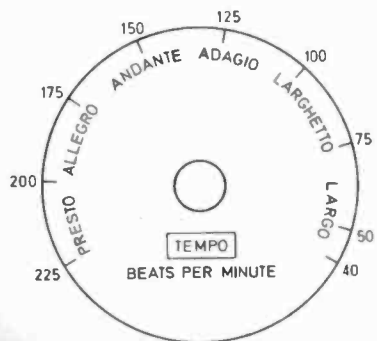


Fig. 4. A suggested design for the scale for VR1. The markings are given as a guide only.

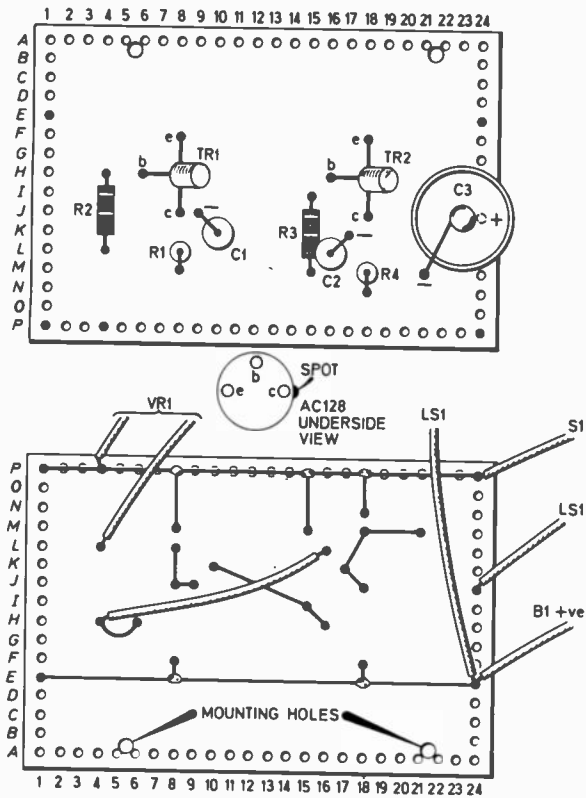
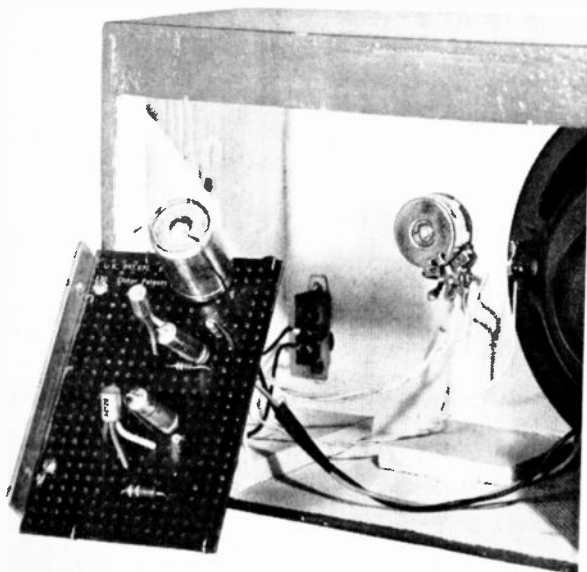


Fig. 2: Layout and wiring of the components mounted on the Veroboard

The battery should be an Eveready type PP9 for long life as the current consumption is 12 to 15mA. If the box is made to about the size given there will be plenty of room for the circuit board, speaker and a PP9 battery. The complete unit could, together with a small speaker, be housed in a smaller case should this be desired. □



Continued from page 472

TESTS AND ADJUSTMENTS

When the driving unit (the circuit mounted on the Veroboard—see Fig. 1) is completed it should be tested before connecting it to the power transistors and the transformer. Connect the circuit to a 12 volt supply observing polarity and measure the d.c. collector voltage (voltage between collector and positive line) of TR2 and TR4. They should read approximately half the supply voltage if the unit is operating correctly.

Any difference in the collector voltages will indicate an unequal mark to space ratio which can be corrected by adjustment of R6 or R7. If the collector voltage of TR4 is below 1 volt and TR2 is above 11 volts the unit is not oscillating. This may be due to the spread of the unijunction characteristics and R6 and/or R7 should be adjusted until oscillation is obtained.

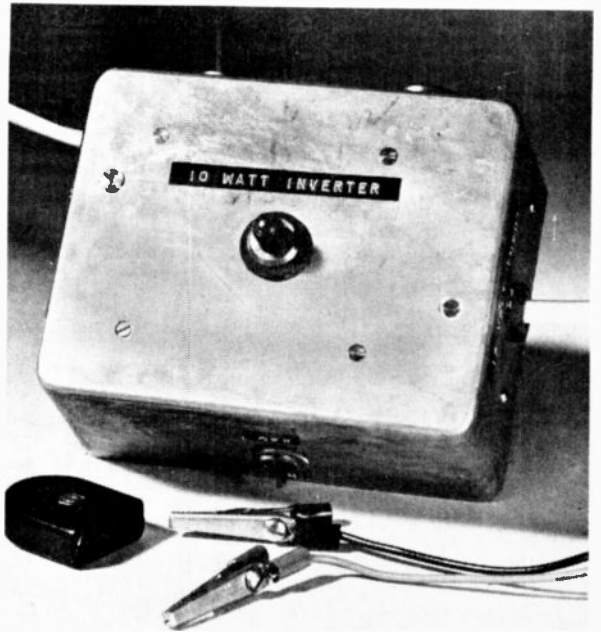
The resistors should be adjusted alternately in each direction and finally trimmed in small steps, to give approximately equal collector voltage readings. If an oscilloscope is available it is easy to see the effect of any adjustments and to trim the components R6, R7 and C1 for the correct wave shape and frequency.

The frequency of the complete unit is not critical if the shaver works satisfactorily.

WARNING

Although powered from a 12V supply the output of this inverter is high enough to deliver a very unpleasant shock.

Under certain circumstances the output from the unit could be very dangerous indeed and should be treated with the respect afforded to any mains supply. □



BEFORE we discuss buying problems this month we will try and clear up a few points of general interest that many readers seem to be unaware of. Firstly let us make it quite clear once again—we do not supply components in any shape or form.

The only thing we sell is this magazine, providing designs for which the necessary parts may be purchased from firms advertising in our pages or any other components retailer.



The approximate cost of components is not a price for the components available from any one shop, it is an approximate cost arrived at by us by selecting components from a number of suppliers, catalogues. It is not necessarily the cheapest price and it is quite definitely not the most expensive, it is published for your guidance only.

Many readers have written to us saying that they have paid £5 or £6 for components that we estimated would cost about £2; well this is quite possible. We point out that if you are cost conscious then look around before buying.

Letters

A second point that we would like to bring to your attention is the situation concerning readers letters. Although we have published notices stating that readers must enclose a stamped addressed envelope and that we can only answer letters concerning

published articles, (there is such a notice on the *Readers Letters* page) we are still receiving many letters with no s.a.e or letters requiring information or designs that, due to lack of time and, in some cases, information we are simply unable to answer.

As you can imagine we receive quite a few letters every day and unfortunately those with no s.a.e. or those requiring information we are unable to supply tend to be put at the bottom of the pile.

We cannot claim to answer letters by return of post but, provided you do as we request we will do our best to supply a satisfactory reply. If you feel like voicing your views—good or bad—on any electronic or associated subject we are always pleased to receive them and, if they are worthwhile, we may well publish your letter. Your criticisms are, in many cases, more useful than praise; so don't be frightened to put pen to paper.

Problems

Now to try and deal with some of the problems. We have had a number of reader's asking where the universal chassis parts that we have specified for some projects are available, the answer is Home Radio Components Ltd., who advertise their catalogue in our pages regularly.

Electronome

No buying problems for the *Electronome* but it may well be worth while to find a secondhand speaker from a radio or T.V. Since the sound quality is not an important factor in this design any speaker of the right impedance will be suitable and ex-equipment speakers are much cheaper than new ones.

Shaver Inverter

Few buying problems for the *Shaver Inverter* but do read the text and find out exactly what you need for the power output you require. Also note that depending on the transformer you use, you may or may not require resistor R10 which is a 1 ohm 5 watt wire-wound type.

When buying the neon make sure it is a mains type incorporating a series resistor as there are others available. Please take note of the warning given at the end

of this article. Although this unit is powered from a battery it provides mains output.

Horses for Courses

The switches used in *Horses for Courses* are a compromise on what is actually required. The unit only needs one three-pole four-way switch, one three-pole three-way switch and one single-pole three-way switch. However, since these types are not all available, two three-pole four-way switches and one single-pole 12-way switch were used in the prototype; these are all wafer switches of the break before make type. Only the required poles or switch positions being used, the others being left unconnected. The chance switch must be capable of being modified as shown in the text, so check this before buying.

This is one project where a number of different colour wires are very useful when wiring up. One way to get these without buying a vast number of coils of wire is to buy a length of multi-core wire and strip the outer insulation off, leaving the coloured inner wires.

The only other point to watch when buying for this project is the type and size of the chance knob. This knob should have no markings or pointers of any kind and be as heavy as possible so that it acts as a flywheel.

Supplier

This month's news item on the supply front is from Zeta Windings Limited who have supplied us with a 17-page catalogue listing many types of T.V. line output transformers, resistors, capacitors, cathode ray tubes and semiconductor plus a few other items. The main facility offered by this firm is its ability to manufacture transformers of any type to individual requirements for readers or authors. They operate a rewind and 1 off prototype service that takes about 3 to 5 days. The firm's facilities are available through the following addresses:

For callers only—Zeta Windings Ltd., 26 All Saints Road, London, W.11.

For mail order and callers—Tidman Mail Order, 236 Sandycombe Road, Richmond; or H. L. Smith Ltd., Edgware Road, London, W.2.



guide to circuit

Signal Waveforms



Alternating current or voltage



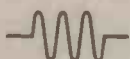
Positive going pulse



Negative going pulse



Sawtooth waveform



Pulse or burst of a.c.

Connectors



Twin tags or screw terminals

1



Short wire link with terminals numbered



Coaxial plug

2



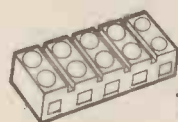
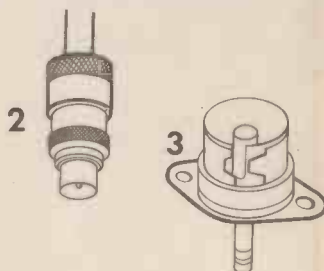
Coaxial socket

3



Multipin plug and socket

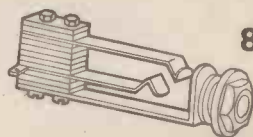
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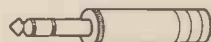
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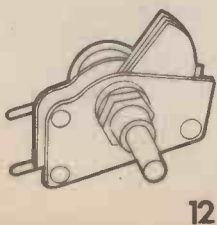
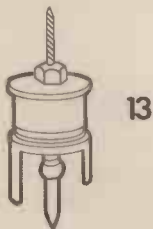
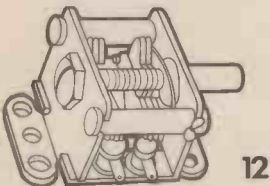
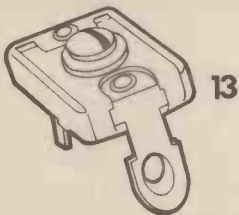
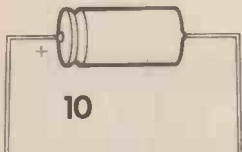
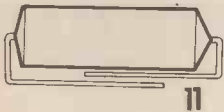
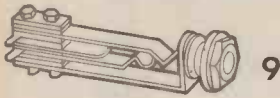


8



8,9

symbols . . . part 2



5

Single pin plug



6

Single socket



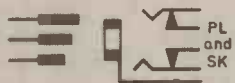
7

Fuse link, general symbol



8

Three pole concentric plug and jack



9

Three pole concentric plug and break jack

Capacitors



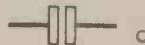
10

Polarized electrolytic capacitor



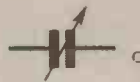
11

Fixed value capacitor (polarized if + sign added)



11

Non-polarized electrolytic capacitor



12

Variable capacitor



13

Capacitor with pre-set adjustment (trimmer)



TEACH-IN

... FOR BEGINNERS

By Mike Hughes M.A.

9

ALTERNATING CURRENT

NEARLY everything we have come across so far has concerned voltages which, although varying in magnitude, have stayed of the same polarity relative to a reference line (usually called the common or ground line). The reason for this is that all the experiments to date have been carried out with a battery, one terminal of which has been connected to this common line.

Because of this we have been able to limit our thoughts to current always passing through components in one direction (or not at all). All the experiments have been of the direct current or d.c. type. Last month, however, we did see that it was possible to get negative voltages generated even though we were working with a positive supply.

REFERENCE LINE

This is where we have to be very careful about defining the reference line, when circuits are being described, because potentials can often be positive or negative in a given circuit.

In the multivibrator last month, the potential at the collector of TR2 varied from approximately zero to +9V relative to the line common to the emitters; we measured this because we connected the negative terminal of our meter to the common rail.

We could have connected the positive terminal of the voltmeter to the positive rail and measured changes of collector potential with the negative terminal of the meter; we could have said that the potential varied from zero to about -9V relative to the positive rail.

Both of these measurements mean exactly the same and the important thing to grasp is that voltages always have to be related to a reference.

In the absence of a stated reference it is usual to assume that voltages are relative to the common line that is running (on the theoretical circuit drawing) right through the system as an unbroken straight line. Generally speaking this can be recognised as the line to which emitters of transistors are connected (sometimes through resistors).

This is not always the case and another way of recognising the reference line is to ascertain whether *pnp* or *nnp* transistors predominate.

If *nnp*—as is usually the case these days—the negative terminal of the power supply or battery can be taken as the common point and vice-versa for *pnp* transistors.

ALTERNATING CURRENT

Referring to the slow running multivibrator (last month's *Teach-In*) try measuring the potential of TR2 collector relative to +4.5V. See Fig. 1(a).

Do this by using VR1 (100 ohm) on the Demo Deck as a potential divider across the battery. Set its wiper to provide a potential of +4.5V and connect the negative terminal of your voltmeter to it and the positive terminal to the collector of TR2. Now see what voltages you read as the circuit oscillates.

You should see about +4.5V for positive half cycles and the meter will try to read backwards for negative half cycles. See Fig. 1(b). Reverse

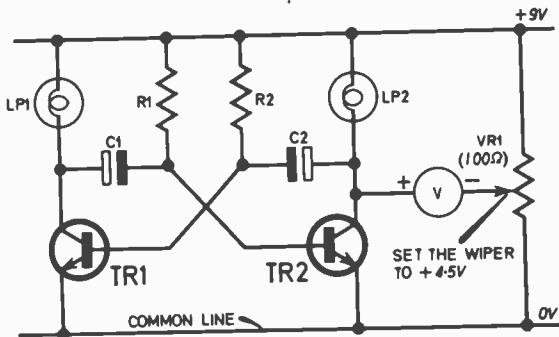
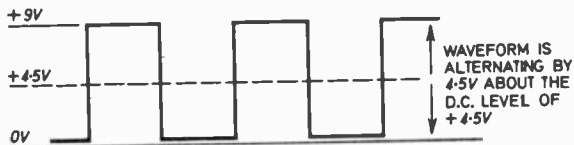


Fig. 1(a) (above). Measurement of the output voltage from the multivibrator of last month, about a d.c. level of +4.5V.

Fig. 1(b) (below). Voltage levels with respect to time observed on the voltmeter.



the meter connections and you will see that the voltages fluctuate from about +4.5V to -4.5V about our new reference point. We say that the voltage is **alternating** and the current flowing through the meter is **alternating current (a.c.)**.

We say that the voltage is alternating with an amplitude of 4.5V about the d.c. level of +4.5V. Again this means exactly the same as the other two methods of measuring we have mentioned.

ALTERNATOR

We very often come across voltages that alternate about a common line, e.g. from record player pick-ups and microphones, but perhaps the most common is the a.c. mains fed to our homes.

Mains is generated at the power station by an alternator which in its simple form is a coil of wire rotating between the poles of a magnet. See Fig. 2.

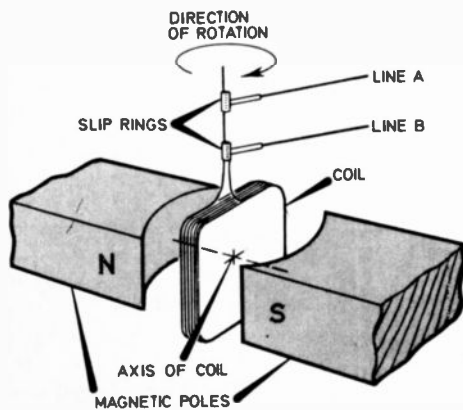


Fig. 2. Schematic diagram of an alternator.

When the axis of the coil is in line with the pole pieces, no voltage is generated but as the coil turns the e.m.f. between the wires coming from the slip-ring contacts increases until it reaches a maximum (peak) when the coil's axis is at right-angles to the pole pieces; it then starts to fall towards zero as the coil rotates towards 180 degrees of rotation (i.e. its axis is in line with the poles again but its direction is reversed). Fig. 3(a) (b) and (c).

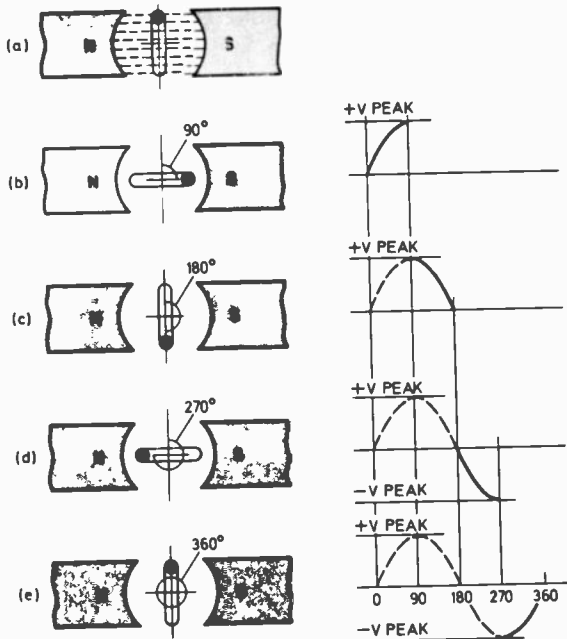


Fig. 3. Shows how one complete "sine wave" is generated from one complete revolution of the coil. The waveform is measured in terms of voltage on line B relative to line A.

Continuing its rotation the e.m.f. will rise again but with opposite polarity and after passing the 270 degree point will fall back to zero as 360 degrees of rotation is reached. Fig. 3(d) and (e).

If we consider the line "A" of Fig. 2 as the common (or neutral) the potential on the other will vary smoothly from zero through maximum positive, back through zero to maximum negative and back to zero.

SINE WAVE

If the coil turns at a constant rate, the waveform of the voltage produced is called a "sine wave" (because the voltage produced at any point of the coil rotation is equal to the maximum positive voltage, multiplied by the sine of the angle of rotation).

One cycle of the sine wave is equal to one complete turn of the coil, hence the number of revolutions of the coil per second sets the frequency, see Fig. 4.

In electronics you will find sine waves appearing very frequently because they are the most pure and simple waves that exist.

Because they are associated with circular movement, formulae based on sine wave theory frequently incorporate the term 2π which is merely another way of expressing angle of rotation.

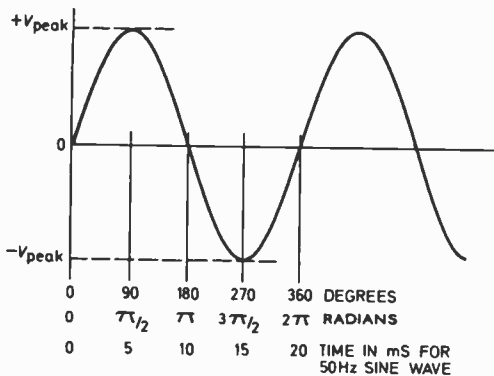


Fig. 4. A continuous sine wave. The discrete points marked can be considered in degrees or radians of rotation—or time if the frequency is known. Time is given for a 50Hz wave.

When the coil turns through 360 degrees (1 complete revolution) we say it has passed through 2π radians (where π (pi) is a constant equal to 3.142). You will see this expression used later on in the series.

TRANSFORMERS

One of the greatest attractions of alternating current is that it can be used in conjunction with a transformer to change voltage levels (both up and down) with insignificant loss of power.

A transformer consists of two coils of wire on a core of soft iron. This is shown by the circuit symbol in Fig. 5 together with some common types of transformer.

One of the coils on the transformer is called the "primary", which normally consists of many thousands of turns (for mains inputs) and the other, which is on the same core but electrically insulated from the primary, is called the "secondary".

The ratio of the turns between the primary and secondary controls the amount of voltage transformation in direction proportion.

On the Friedland transformer which we will be using in our experiments, there are three alternative secondary outputs: 3, 5 and 8V. In the case of the 8V output, the turns ratio would be about 8 on the secondary for every 230 on the primary.

If we pass a current through the primary we will magnetise the core, and the change in magnetisation will induce an e.m.f. across the secondary, the magnitude of this e.m.f. being proportional to the turns ratio. This e.m.f. will only be induced while the magnetic field is being changed by the primary current.

Thus, if we pass a direct current into the primary and keep it flowing, we will only get a brief e.m.f. produced in the secondary while the initial magnetisation takes place. When we stop the primary current, the magnetisation will die away fairly quickly (if the transformer is a good one) and this change of field in the opposite direction will induce another brief voltage pulse of opposite polarity.

You can see this using a 9V battery and the 1mA meter of the Demo Deck, Fig. 6.

Connect the 1mA meter directly across the 8V output of the transformer and then connect the battery across the primary (mains input terminals). If you watch the meter you will see a short "kick" (the direction depending on which way round you connect the battery). Break the primary circuit and you will see the meter needle "kick" in the opposite direction.

The movement will be so fast that you will not be able to make any actual measurement

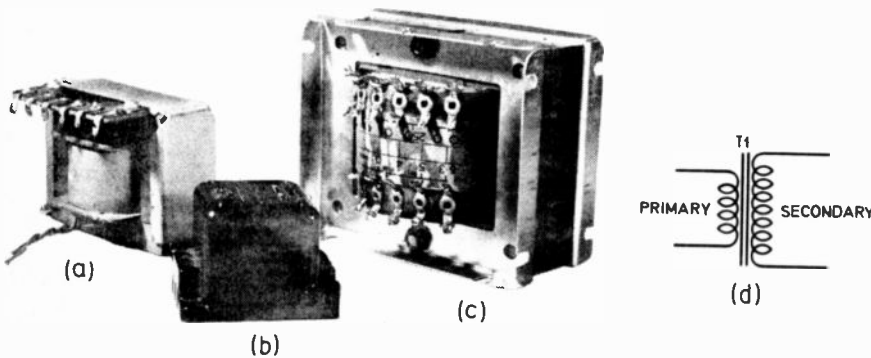


Fig. 5. (a) Ordinary mains / low voltage tapped transformer. (b) Friedland Bell transformer—used in this month's experiments. (c) Heavy duty mains type, three secondary windings, HT (500V) and heaters (6.3V). (d) Circuit symbol for an iron cored transformer.

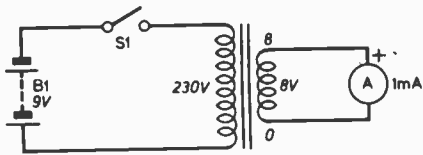


Fig. 6. Circuit diagram for showing current will only flow in the secondary when a change of current occurs in the primary.

but you will see the effect. After doing the experiment once, you might notice a reduction in pulse amplitude if you repeat the experiment; this is caused by residual magnetism held within the core (it does not demagnetise itself completely when you stop the current, hence the change in magnetisation will not be so great the next time you do it). To overcome this, reverse the battery connections between each experiment.

While a direct current in the primary will not cause a continuous current to flow in the secondary, variations in the primary will produce variations in the secondary voltage. This is very similar to the effect we had with capacitors where changes in potential on one plate caused changes on the other although continuous d.c. produced no change after the initial reaction.

Alternating voltages when applied to a circuit will cause current to flow in alternate directions. If we apply a.c. mains to the 230V input of our transformer, the current, and hence the magnetisation, will be constantly changing direction at the mains frequency—50Hz (50 complete sine wave cycles per second). This induces a 50Hz sine wave across the secondary winding but at a lower voltage.

POWER IN EQUALS POWER OUT

An important fact about this type of transformation is that, by and large, the power put into a transformer equals the power taken out (there are certain losses caused by core magnetisation but these are negligible and will be ignored at present). For example a medium voltage input at medium current will enable a secondary to give either a higher voltage at lower current or a lower voltage at higher current—depending on the turns ratio, see Fig. 7.

Power-wise you never get more out than you put in!

We are going to do some simple experiments using alternating current but first let's see how we can measure alternating voltages.

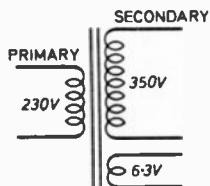


Fig. 7. This circuit symbol signifies a mains transformer with two secondary windings, the output voltages of which are shown.

A.C. MEASUREMENT

First just try and measure the 8V output of the transformer when its primary is connected to the mains. Remember to take great care that you do not touch any connections on the primary side—it is quite safe to handle the secondary.

Make a simple 10V voltmeter with a 10 kilohm resistor and the 1mA meter and connect it across the transformer's secondary terminals, Fig. 8.

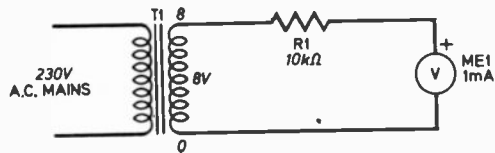


Fig. 8. The voltmeter will read zero volts because the meter settles at the average level.

You should read zero volts which you might think rather strange. It is not so strange if you realise that the needle is trying to swing up in a positive direction then back towards negative 50 times a second—it is physically impossible for it to move this fast. Instead it will settle down and register the average voltage, which is zero. Had you done this on the collector of TR2 of the 700Hz multivibrator (last month) you would again have read the average value but that would have been +4.5V.

In the case of a square wave of unity mark space ratio oscillating between zero and +9V, the peak voltage could be ascertained simply by doubling the average, but in the case of a sine wave alternating to equal amplitudes in both positive and negative directions, this is not possible.

HALF-WAVE RECTIFICATION

We can however prevent negative current flowing through the meter by incorporating a diode see Fig. 9. This is called "half wave rectification." Now only positive half cycles will affect the meter and we shall get a reading that is a form of average between zero and the peak of the positive half cycle but obviously it is not a simple average and the response of the meter movement will still play an important role in our measurement.

R.M.S.

Whatever happens, we are never going to be able to measure peak voltage using a moving coil meter. Meters designed for measuring alternating current work on the basis of average value; this level is called the root mean square value (r.m.s.) for the sine wave in question (and is indicated in Fig. 10). This value is the peak value divided by $\sqrt{2}$ (square root of 2).

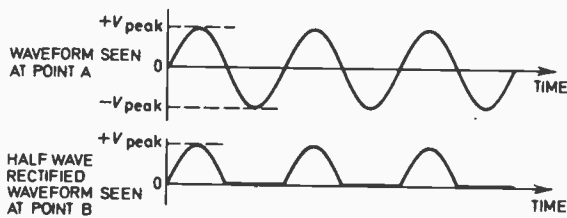
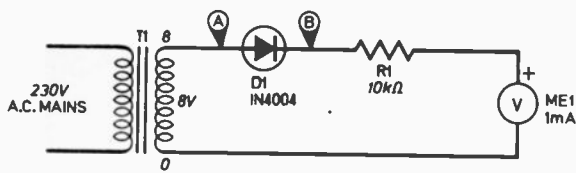


Fig. 9. After half-wave rectification the meter will display a reading of between zero and V_{peak} .

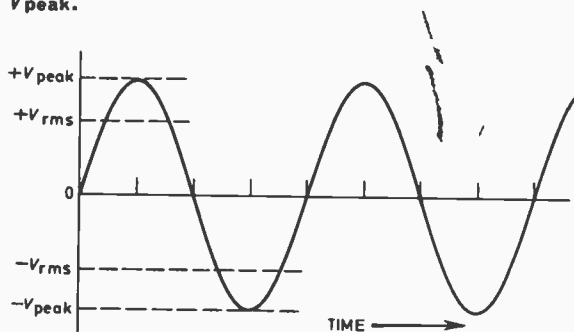


Fig. 10. A sine wave showing relative positions of V_{peak} and V_{rms} .

Conversely if we know our meter is calibrated in terms of r.m.s. values we can calculate the peak voltage by multiplying the r.m.s. value by $\sqrt{2}$. (The square root of 2 is approximately 1.414.)

$$\text{Thus } V_{\text{peak}} = V_{\text{rms}} \times \sqrt{2} \text{ or } V_{\text{rms}} = \frac{V_{\text{peak}}}{\sqrt{2}}$$

Unless otherwise stated always assume that the outputs of transformers are given in r.m.s. values. A mains voltage stated as 240V a.c. is an r.m.s. value; this means that on positive and negative peaks the sine wave will reach +340 and -340V respectively (this is why you should always use at least 400V rated components in mains circuits!). The output of our transformer is 8V r.m.s. therefore its peaks will be +11.2V and -11.2V.

A.C. VOLTMETER

You could experiment with series resistors, the 1mA meter and the single diode to make a simple 10V r.m.s. full scale a.c. voltmeter. You

will find that the series resistor will have to be less than 10 kilohm—probably 5.6 kilohm, but this will depend on the mechanical response of your meter. For the following experiments you would be well advised to use a high resistance voltmeter already calibrated for a.c. working.

DC POWER SUPPLY

We can use the components we have available to make a simple battery eliminator. This means we can use the mains to produce a low d.c. voltage that could be used to power simple transistor experiments—see circuit in Fig. 11. All we do is turn our transformed a.c. into a half wave rectified signal—which could be called an intermittent d.c. voltage. This is then fed to a large capacitor C1, which smooths out the ripples—rather like the diode pump circuit (*Teach-In Part 6*).

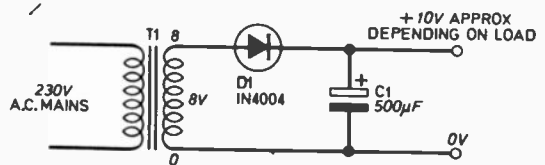


Fig. 11. Simple half-wave rectified power supply. The output voltage will vary, depending on the load, being at peak value for zero load.

Provided the current we draw from the capacitor is very much less than the charging up current, there should not be too much residual ripple caused by the half-wave rectified a.c.

The interesting thing about this circuit is that even though you use an 8V output transformer the d.c. voltage you obtain across the capacitor will be higher (between 10V and the peak of 11.2V). The actual value will depend on the amount of current you draw.

FULL WAVE RECTIFICATION

With half-wave rectification you do not use the full amount of energy available, because the negative half cycles are not used. We can carry out a process called full-wave rectification which in effect changes the negative going excursions of the a.c. waveform to positive going signals. These fill the "gaps" between the half wave rectified signals (see Fig. 9). In Fig. 12(a) the diodes are in a circuit called a "diode bridge."

When the potential of line "A" is positive with respect to line "B" (i.e. positive half cycles) current will flow through D2 and D3 which are forward biased, but both D1 and D4 will be reverse biased, thus the positive half cycle will charge the capacitor. During the negative half cycle (i.e. line "B" is now positive with respect to line "A") D4 and D1 will be forward biased hence charging the capacitor; D2 and D3 will be reverse biased—preventing a short circuit across the transformer secondary.

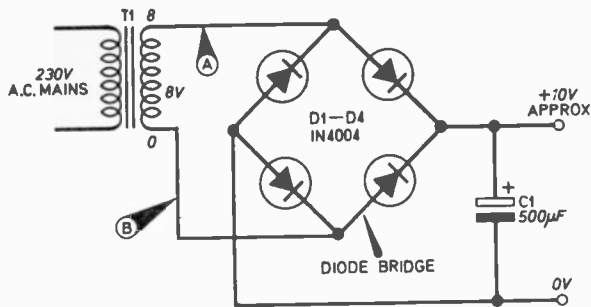
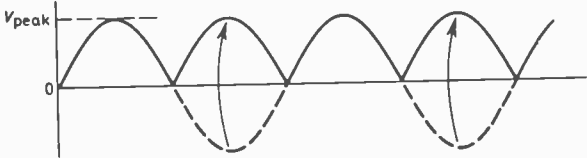


Fig. 12(a) (above). Circuit for demonstrating the principle of full-wave rectification.

Fig. 12(b) (below). Full-wave rectified sine wave.



The ripple will now be a signal having a frequency of 100Hz (see Fig. 12(b)) which can be more effectively smoothed by the capacitor, and since more total energy is being fed to the capacitor more current can be drawn out before the ripple increases to an objectionable level.

COMPONENTS

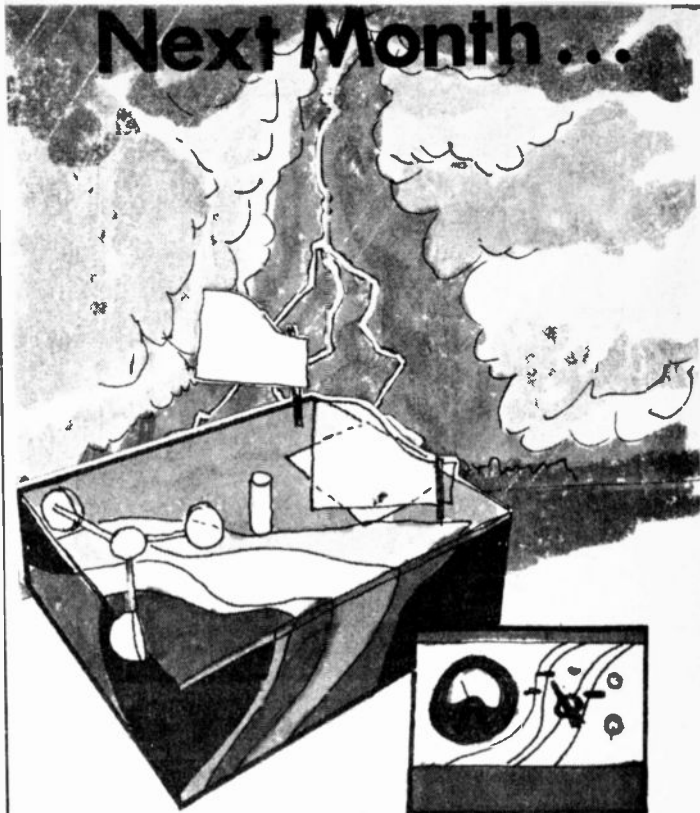
If you make these circuits we suggest you use 1 amp diodes such as the 1N4004 and 500µF 25V working smoothing capacitor for voltage measurement experiments; however if you want to make a good d.c. supply you should use the bridge circuit with a capacitor of about 5,000 µF at 25V working.



Next month: Reactance and Inductance

Additional components required for next months experiments are: resistors, 100 kilohm (1 off); capacitors, 0.22µF polyester (1 off); Ferrite rod, 6 inches long 1/4 inch diameter; 28 swg enamelled copper wire (2 oz.); 60/70V neon bulb without built in resistor.

Everyday Electronics, July 1972



Weather Station

Build your own weather station with an indoor monitor. This basic design monitors temperature, ambient light level, wind strength and direction, and incorporates a rain warning alarm.

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All in the August

issue of

On sale July 21





No radio listener or TV viewer on Saturday afternoons can fail to notice the emphasis on, and the interest in, the pedigree of race-horses. The same interest is shown at Cruft's, in the market garden and even the maternity home!

Now although the genetics of breeding is based upon very simple rules, chance also plays a very important part and the project to be described has been designed as a perfect demonstration of the theory of genetics known as Mendelism.

It should appeal immensely to teachers of genetics, zoology, biology or mathematics. For other readers the very simple unit may be used in conjunction with some paper "stage" money to produce a fascinating table-top game suitable for all the family in which horses are bred and raced.

MENDEL

Father Greggor Mendel (1822-1884) was a German monk who based his theory of genetics upon a study of the edible pea over a consider-

able number of years. It is possible that he had a general theorem to start with and proved it by his observations.

He published his findings in 1866 but they aroused little interest. Sixteen years after his death however, his work was revived and tested independently and simultaneously by three researchers, and Mendel became famous. His work is the foundation of all modern genetics.

Mendel proved that every inborn characteristic is the result of an equal contribution from the mother and father. These contributions he called "gamenes."

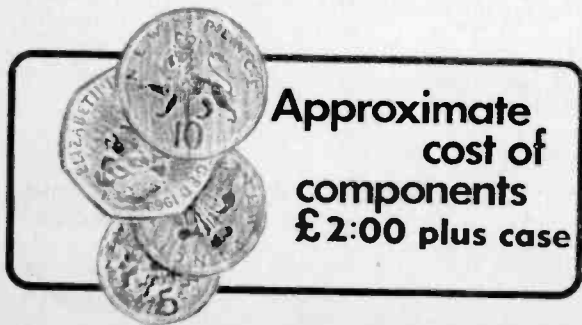
Let us assume that a certain species of moth has either a green, blue or yellow wing colour. The blue moth has two blue gamenes, the yellow moth has two yellow gamenes, while the green moth has one blue gamene and one yellow gamene.

If a blue moth mates with another blue moth, the offspring must all be blue, since neither parent can contribute a yellow gamene. Similarly for two yellow parents, only a yellow strain can be produced.

If however a blue/yellow mating occurs, the only possible offspring is green. There is no possibility of a yellow or blue strain since only one gamene is donated by each parent. With reference to Fig. 1(a) we can see that there is no chance of a blue, two chances of a green and no chances of a yellow.

If we let "0" represent blue, "1" green and "2" yellow, then the chance ratio of offspring from a blue/yellow mating is seen to be no "0", two "1" and no "2".

It can be seen from Fig. 1(b) that a blue/green



Horses for Courses

A device to explain simple genetics which can also be used to play an interesting horse breeding and racing game.

By D. R. DAINES

mating produces either two green or two blue offspring—no pure yellow since a yellow gamete is only evident in one of the parents. The ratio here is two "0", two "1" and no "2".

A green/green mating is shown in Fig. 1(c). Here it is possible to obtain one blue strain, two greens and one yellow, i.e. one "0", two "1" and one "2".

CHANCE

So far we have dealt with moths, where great numbers of offspring occur at each mating. What happens with animals, where there is usually only one or two progeny such as horses.

Here we can say that, over a large number of matings, and a large number of progeny, the same two parents will tend towards the above ratios.

It is clear where the chance factor lies. If a coin is spun, it may come down heads or tails. If it comes down heads it can't be said that it will come down tails next time, nor is it more likely to. It still remains an even chance.

All that can be said is that over a large number of throws, the number of heads will tend to equal the number of tails. Similarly with genetics. The chances are known but cannot be forecast.

HORSES

With the moths mentioned above, "0", "1" and "2" represented wing colours—blue, green, and yellow respectively.

If we now let "0", "1" and "2" represent the total absence of a trait, a weak trait, and a

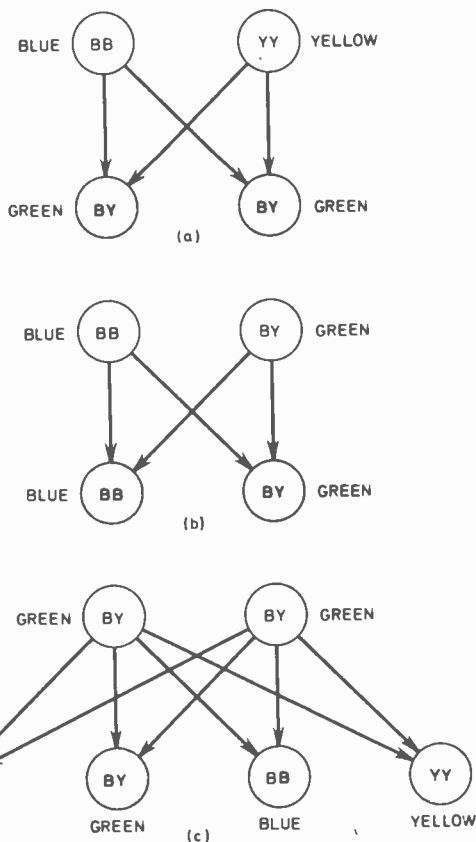


Fig. 1. Schematic diagram of the mating of moths of different wing colour. Offspring are shown shaded.

strong trait respectively, we can apply this simple theory of genetics to horse breeding.

If we assume we are dealing with one of the many characteristics (traits) of horses, such as stamina, speed, action etc. then the degree of the trait (trait factor) present can be represented by "0", "1" or "2".

If, for example, the factor of a particular trait in the sire is "1" and that the same trait in the dam is "2", then there are equal chances of the foal having a "1" or "2" trait.

We can therefore make up a "truth" table using the three trait factors of the parents. This is shown in Table 1.

Table 1: CHANCES OF OFFSPRING TRAITS AS A FUNCTION OF PARENTAL TRAITS

Sire	Dam	Offspring (Foal)
0	0	0
0	1	0 or 1 (equal chances)
1	0	0 or 1 (equal chances)
1	1	0, 1, or 2 (two chances of a 1)
0	2	1
2	0	1
1	2	1 or 2 (equal chances)
2	1	1 or 2 (equal chances)
2	2	2

CIRCUIT

The circuit diagram for illustrating this simple theory of genetics with a built in chance factor is shown in Fig. 2.

It is merely a passive switching network which is wired up to give the required results of Table 1.

The output is in the form of illuminated lamps LP1, LP2 and LP3, representing the "0", "1" and "2" trait factors respectively.

SWITCHES

Switch S1 is used to turn the unit on/off, this should be a toggle, push-to-make/release-to-break type. This ensures no cheating, or "fixing" of the chance selector can result; this will be evident later.

The "sire" switch S2 should be a single-pole three-way type. This type of switch is not generally available, so the prototype was built using a single-pole 12-way type.

The "dam" switch S3 should be a three-pole three-way type. The prototype, however, used a more readily available type, four-pole four-way, hence the unconnected terminals on this switch seen in the wiring diagram of Fig. 3.

The chance switch, S4, must be a three-pole four-way type—but it has to be modified to allow it to be spun freely. This is done by dismantling S4 and cutting away the sprung stops, see Fig. 4.

To dismantle, remove the small circlip located on the spindle just above the threaded portion. This is a fairly difficult task and is best done using a pair of long nose pliers to grip the clip and prising it apart with a pair of side cutters.

Next, bend back the four fixing legs enabling the backplate to be removed, and remove the rotor from its bearing. Cut away the sprung stops and fixed stop with a hacksaw or side cutters, file smooth and reassemble. The spindle should spin freely.

WIRING UP

The complete wiring diagram is shown in Fig. 3. It is advisable to use as many different coloured wires as possible to help identify connections and check-out after completion.

To begin, attach the three switches, S2, S3 and S4 to the labelled front panel of the case (see Fig 5 for dimensions) together with the lamps

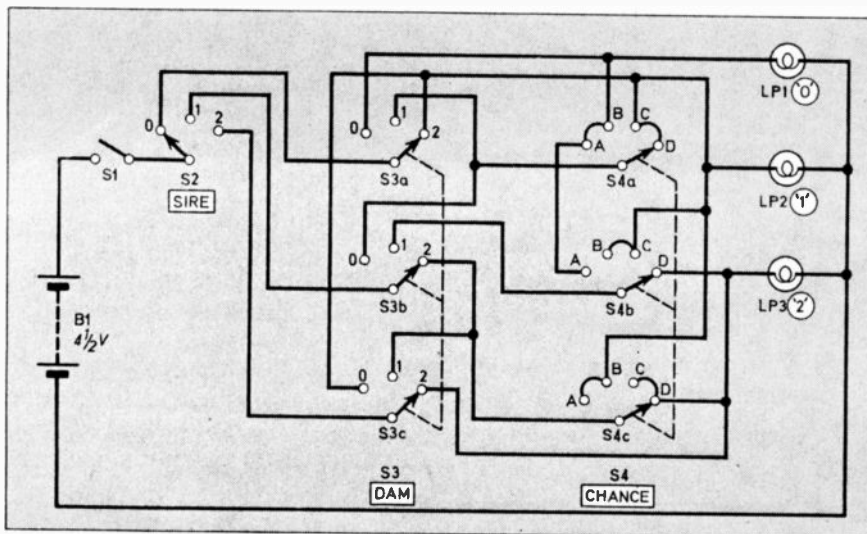


Fig. 2. The complete circuit diagram of the unit.

Horses for Courses

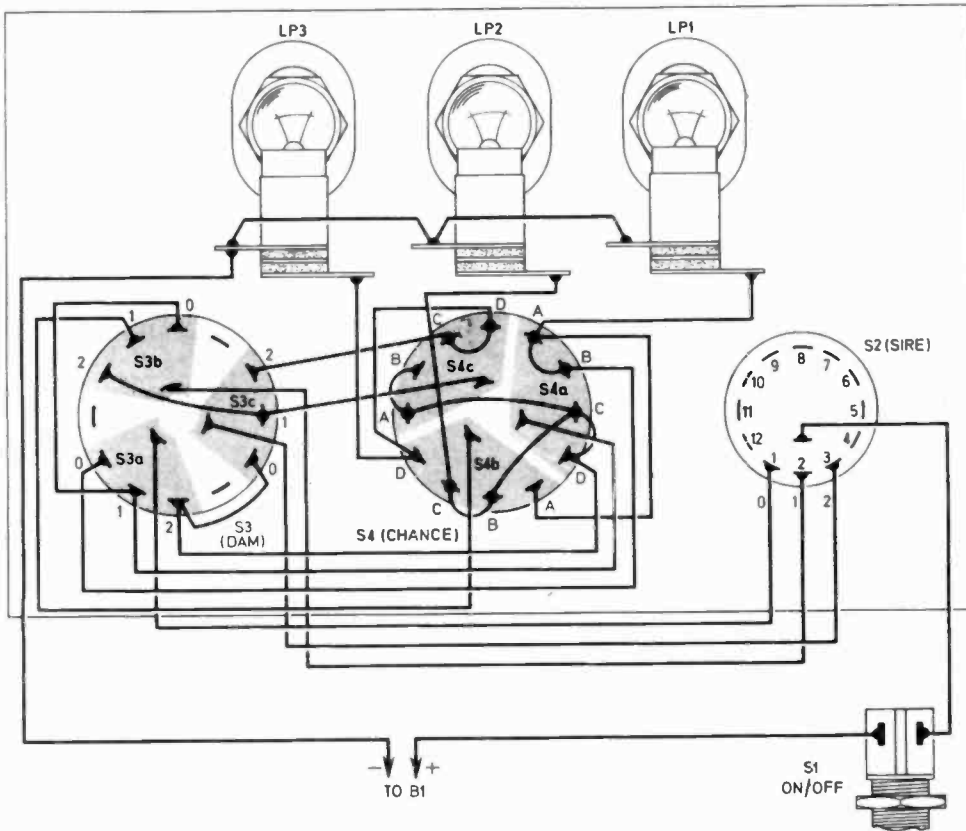


Fig. 3. The complete wiring diagram. The shaded region on S3 and S4 shows the pin connections associated with each of the three poles. B1 can be connected either way round.

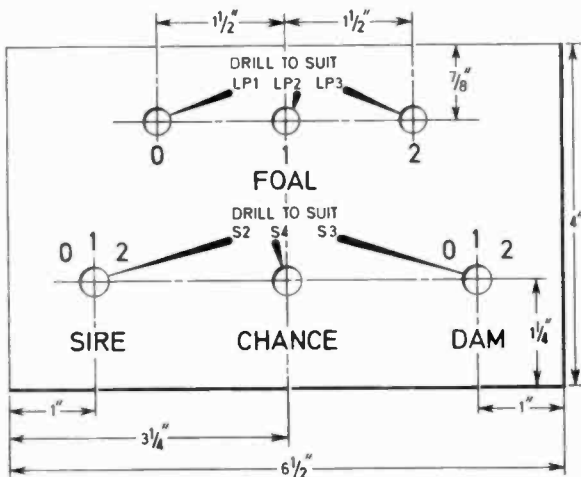
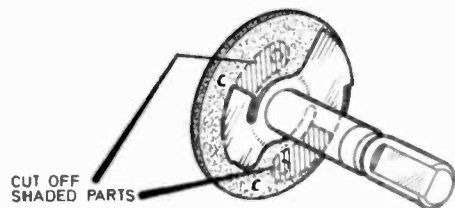
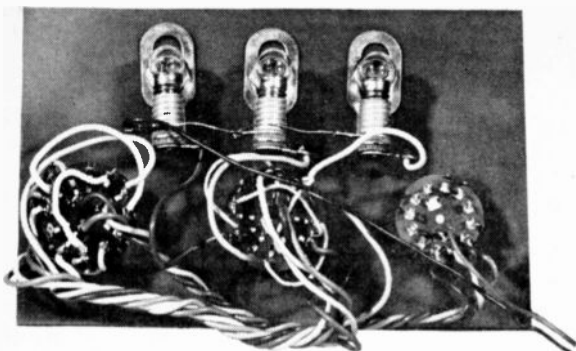


Fig. 4 (left). A suggested layout of the components on the front panel which in the prototype was made from coloured Perspex—but any material can be used.

Fig. 5 (below). The rotor of S4 removed. The shaded regions are to be cut away to enable it to be spun freely.





LP1, LP2 and LP3. Some sort of pin labelling is recommended to eliminate errors.

On each switch identify the poles and their corresponding pins—in the correct switching order: This can be done with a felt-tipped pen on the inside of the front panel alongside the switches.

Begin wiring from switch S2 to the poles of S3, and then connect the links between the three banks. This done, connect suitable lengths of wire from each of the nine pins from S3 to go to S4.

Next make the necessary link connections between the pins on this switch and then connect all the wires from S3 to the respective pins on S4.

To complete the wiring, connect the lamps, S1 and the battery in circuit.

Table 2: SWITCH POSITION/INDICATOR LAMP CHECK-OUT

S2 (Sire)	S3 (Dam)	A	S4 (Foal)			D
			B	C		
0	0	0	0	0	0	
0	1	0	0	1	1	
1	0	0	0	1	1	
1	1	0	1	1	2	
0	2	1	1	1	1	
2	0	1	1	1	1	
1	2	1	1	2	2	
2	1	1	1	2	2	
2	2	2	2	2	2	

TESTING

Table 1 shows the various off-spring traits as a function of parental traits, and the chances of obtaining them. These conditions are realised by the circuit and are indicated visually by the three lamps labelled "0", "1" and "2".

There are four positions on S4 (A, B, C, D) and for each of the combinations of S2 (sire) and S3 (dam) the lamps should light in accordance with Table 2. Test each combination carefully against Table 2, every combination should agree with this table.

Components....

Switches

- S1 Push to make/release to break toggle
- S2 Single-pole three-way wafer
- S3 Three-pole three-way wafer } see text
- S4 Three-pole four-way wafer (modified, see text)

Lamps

- LP1, LP2, LP3 4.5 or 6V bulbs (three off) and holders to suit

Miscellaneous

- B1 4.5V bell type battery (type 126)
- Knobs: Three off; 2 pointer types, 1 heavy unmarked type (for chance switch). Connecting wire—as many different colours as possible—use stranded type.

Example: When the sire switch is set to "1" and the dam to "2", for the four different positions of S4, the "1" lamp should light twice and the "2" lamp should light twice. The "0" lamp should never light for this combination.

Not more than one bulb should ever be on at the same time for any combination.

USING THE UNIT

The unit can be used to demonstrate the Mendelian theory in the following way.

With S1 in the off position, set the pointers of S2 and S3 to the chosen trait factors and then spin the chance switch S4. Depress S1 and take a note of the result (i.e. which lamp lights).

Do this a number of times recording the results each time and you will see that as a number of samples increases, so the tabulated result moves closer to the given ratio.

Alternatively, students may be instructed to formulate their own ratios over a number of samples using statistical methods.

BREEDING AND RACING GAME

This device can also be used to form the basis of a very interesting table top game for all the family in which horses are bred (using the unit described above) with the intention of producing horses for racing and further breeding. There is no limit to the number of players that may participate.

Other equipment required for the complete game are a race track, owners cards, paper "stage" money (Monopoly money is ideal), and a dice.

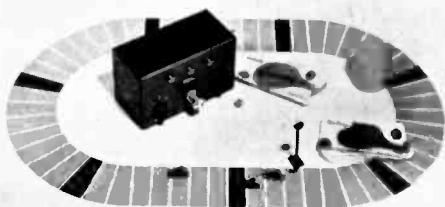
The race track can be made to any size or design. Fifty spaces between start and finish were found to be adequate.

Every eighth space should be distinguishable from the rest—coloured black for example as shown in photograph opposite. These black squares are to confer advantages (or disadvantages) to horses landing thereon as detailed later.

Owners' cards should be drawn up as detailed in Fig. 4 and one should be issued to each player.

No.		OWNERS CARD							
TRAIT		1st GENERATION	HORSE						
CODE	POINTS		I	II	III	IV	V	VI	VII
A	6	0							
B	4	0							
C	3	1							
D	2	0							
E	1	0							
F	-2	0							
POINTS TOTAL		3							
GENDER		F							
STUD									

Fig. 6. An owner's card. When the traits and gender of each horse have been determined, they should be marked as indicated. When a horse has been mated it should be marked accordingly in the space provided.



TRAITS

Six traits have been chosen for the horses and these have been coded A, B, C, D, E, F. The "A" trait being most advantageous and "F" being a positive disadvantage.

When a horse lands on a black space on the race track, depending on its traits, it advances (or goes back) a number of spaces given by Table 3.

Table 3: BLACK-SQUARE-ADVANTAGES FOR THE SIX TRAITS

A	B	C	D	E	F
6	4	3	2	1	-2

After breeding several generations it is probable that a horse will emerge with more than one trait. The total advantage when landing on a black square is given by the sum of the individual trait advantages.

Example:

A horse with traits "A", "C" and "F" would advance seven spaces when landing on a black square. This is made up (using Table 3) of $6+3-2=7$. If a horse has a strong trait denoted by a "2" on the owners card, then the advantage (or disadvantage) is doubled, i.e. a horse with a strong ("2") "C" trait advances 6 spaces when landing on a black space.

PRELIMINARIES

Every player is given an owners' card which he keeps throughout the game. Each in turn throws a dice twice, the first throw to determine the gender of the horse—stallion or mare (odd or even respectively). The second throw is to determine the trait of this first generation horse i.e. A, B, C, D, E or F. A throw of "six" gives trait "A"; "five" trait "B"; "four" trait "C"; "three" trait "D"; "two" trait "E"; "one" trait "F".

The first generation horse can only have one trait and this must be weak (denoted by a "1" written alongside the appropriate trait).

When this has been carried out by each player, racing or breeding can begin.

BREEDING

Breeding can be instigated in two ways: (1) by agreement between any two owners—the owner of the stallion charging the owner of the dam an agreed sum of money for the stallion's services. The foal resulting belongs to the owner of the dam.

The gender of the foal is determined by a throw of the dice, odd for colt, even for filly.

(2) By use of the National Stud for which the player pays a fee to the bank.

The National Stud horse has only one characteristic for which a dice is rolled as before. The characteristic is weak (i.e. "1"). The gender of the National Stud horse is assumed to be opposite to that of the player's horse, and the resultant foal belongs to the player. The owner's horse must be selected prior to drawing a horse from the National Stud, and these horses must then be bred.

Whether breeding is carried out using facilities (1) or (2), the procedure is the same, the owner of the eventual foal sets the trait factors of the sire and dam for each trait in turn to "0", "1" or "2" and spins the chance switch.

The trait factors (for each of the six traits in turn) are indicated by the three lamps. This factor is then entered alongside the trait in question on the owners' card.

Further breeding can be carried out between races by methods (1) and (2) above, or, if an owner has two or more horses on his card, of opposite sex, he can mate these to produce others.

Once a horse has been put to stud (mated) it can no longer race, but there is no limit to the

number of times a horse can be mated or the number of times an unmated horse can take part in a race.

RACING

The first race should be run after each owner has acquired one horse and subsequent races after another horse has been bred by one or more owners.

Owners are allowed to enter only one horse for each race, which must be declared before the start of the race, for which a standard sum is paid, and a fixed amount is added to this by the bank to constitute the prize money.

The horses are moved around the course with the aid of a dice in the usual way, coupled with the "black-space advantages" acquired by each.

MONEY MATTERS

The introduction of paper money into the game makes it much more interesting. This paper money can either be made up or, if Monopoly money is available this would be ideal.

The money should be located in a central bank and should contain a large number of monetary denominations such as £100, £50, £25, £10, £5 and £1 notes.

With an initial capital of £500 each player is sufficiently equipped to meet breeding and race

entrance fees. This amount is supplied by the bank.

Breeding charges between owners have to be agreed jointly by the owners making the contract—payment being made to the stallion owner.

For use of the National Stud for breeding purposes a fixed sum of £50 is payable to the bank.

If an owner wants to raise some cash, he can offer any of his stock for sale to the highest bidder, otherwise he may sell to the National Stud—if his horse has a point value of three or more—for a sum of £30 (payable to him by the bank). Once a horse is sold into the National Stud its racing and breeding days are over; it is put to grass (discarded).

The entrance fee per horse per race is £20 and the bank puts £40 to the total to form the prize money. On completion of a race, the prize money is divided up as follows: for two players, winner takes all; for three players, winner takes three-quarters, second one-quarter; four or more players, winner takes half, second and third, a quarter each.

WINNING POST

At the end of the game the winner is the owner with the most money and, incidentally, the most successful breeder. ▣

Ruminations

By Sensor

The Worm Will Turn

I was reading about some of the work now being done to enable an operator to communicate directly with a computer, using normal spoken English words. The computer would be designed to recognise certain words and to act appropriately when they are spoken.

The idea interested me because I feel that the operator ought to have a chance to answer back. For far too long he has been at the beck and call of his electronic "servant"; obeying instantly when told by the computer's flashing lights to; Input programme, Change tape, Input data, Call engineer; and so on. And if he fails to carry out his duties in the required manner, on flashes the light; Operator error and he gets a rocket from the computer manager for wasting his computer's time!

But imagine how different

things could be with direct speech input—*Scene: A computer room. Time. A.D. 1984.*

Operator enters and switches computer on.

Computer: "Operator number two. Input programme."

Operator, (after late night party): "Don't shout, I'm having a coffee first—and don't call me number two."

Computer: "You are identified in records as operator number two"

Operator: "Change the records, my name is Bert."

Computer: "Records cannot be changed except by use of master programming key held by director of MI55. Input data immediately."

Operator: (Looking at crossword and talking to himself). "Ah, anagram, seven letters, "He makes the sea pant"—must be an anagram of SEA PANT."

Computer: "Peasant."

Operator: "When I want your opinion I'll ask for it, bighead."

Computer: "All data must be input before 08.30 hours. Your records will be marked unpunctual, inefficient, undesirable. You will be fined and downgraded."

Operator: "I resign. So you can put that into your register and process it, you electronic moron.

I'm dropping out." Exit operator pursued by cries of Input data.

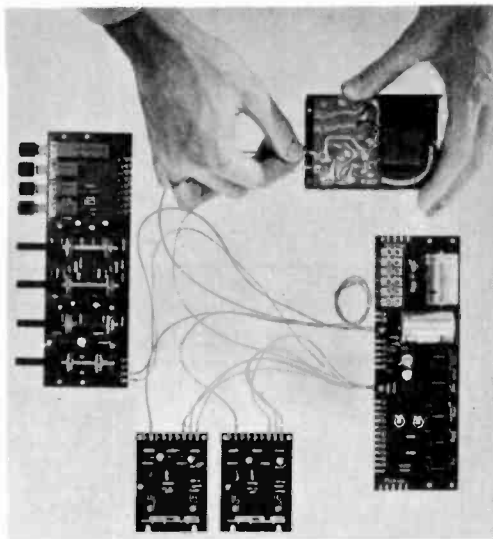
Computer Voice

Thinking about the way a computer speaks reminds me of the peculiar way of speaking that some of our radio announcers have these days? Their voices go up and down like a roller coaster with odd little pauses here and there. The female announcers are particularly prone to affect this mode of speech, and one assumes that somewhere there is a training school, probably very expensive and very exclusive, where young ladies with normal, interesting voices, are coached to produce what some official has decided is a "well modulated voice suitable for radio and television."

The writers of *Monty Python's Flying Circus* must have noticed what has been going on and they have parodied it brilliantly on several occasions.

There seem to be many organisations now that are intent on selling to us so many things that we are not only don't need but positively don't want. In my list of these unwanted goods and services I include "the well modulated voice" along with car parking fees and a few others.

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1N136	10p	2N3053	27p	2N5192	77p	AD150	50p	BC154	16p	BF177	25p
1N1763A	24p	2N3054	55p	2N5195	90p	AD161	33p	BC157	12p	BF178	31p
1N3754	20p	2N3055	50p	2N5457	30p	AD182	36p	BC158	11p	BF194	14p
1N3939	24p	2N3225	51p	2N5489	71p	AD186	36p	BC159	12p	BF195	15p
1N5402	23p	2N3405	52p	40250	89p	AF115	24p	BC167	11p	BF244	30p
1N5407	35p	2N3663	52p	40251	89p	AF116	22p	BC168	10p	BF254	15p
1844	5p	2N3702	10p	40361	45p	AF117	22p	BC169	11p	BF255	15p
18940	5p	2N3703	10p	40362	45p	AF118	22p	BC177	14p	BFX18	90p
2N696	17p	2N3704	10p	40406	53p	AF119	82p	BC178	13p	BFX29	29p
2N697	18p	2N3705	10p	40408	54p	AF124	24p	BC179	14p	BFX84	25p
2N706	12p	2N3706	10p	40412	67p	AF125	24p	BC182L	11p	BFX85	25p
2N930	21p	2N3707	10p	40430	125p	AF126	22p	BC1838	31p	BFX88	25p
2N1131	25p	2N3708	8p	40432	180p	AF127	22p	BC184L	30p	BFY50	25p
2N1132	25p	2N3709	10p	40512	179p	AF129	33p	BC186	14p	BFY61	25p
2N1302	10p	2N3710	10p	40602	48p	AF239	36p	BC212L	13p	BFY52	23p
2N1303	10p	2N3711	10p	40669	120p	AL102	77p	BC213L	18p	BFY39	30p
2N1304	26p	2N3731	180p	AC107	46p	AS926	27p	BC214L	9p	BBX20	10p
2N1305	26p	2N3732	15p	AC126	23p	AS927	36p	BC267	8p	BY164	44p
2N1306	33p	2N3819	20p	AC127	20p	AS928	26p	BC268	9p	BY238	16p
2N1307	33p	2N3820	58p	AC128	20p	AS929	29p	BC269	17p	BYX38-300	37p
2N1308	36p	2N3904	18p	AL141H	34p	AU111	97p	BC267	17p	BYX38-300R	37p
2N1309	36p	2N3906	20p	AL141HK	37p	B30C250	24p	BC269	17p	C407	17p
2N1596	76p	2N4036	52p	AC142H	25p	B30C550/300	33p	BC269	49p	C782	17p
2N1599	76p	2N4058	13p	AC149HK	28p	B1912	31p	BC300	37p	CA112	107p
2N1613	26p	2N4059	11p	AC157K	22p	B5041	72p	BC301	9p	E2512	107p
2N1711	26p	2N4060	16p	AC178	16p	B1092	21p	BC303	60p	EB383	10p
2N1893	54p	2N4061	11p	AC176K	17p	BA130	15p	BCY30	18p	EC401	18p
2N2147	114p	2N4062	11p	AC187K	17p	BA145	21p	BCY31	33p	EC402	18p
2N2218	38p	2N4124	15p	AC188K	23p	BA155	15p	BCY70	105p	EC481	120p
2N2218A	44p	2N4126	22p	*AC187K/188K	40p	BA156	13p	BCY71	100p	MJ491	135p
2N2219	38p	2N4284	24p		40p	BAX13	8p	BCY72	50p	MJ3E71	58p
2N2219A	51p	2N4286	15p	ACY17	31p	BH103/B	16p	BD121	81p	MJ2955	108p
2N2270	62p	2N4289	15p	ACY18	19p	BB103/G	16p	BD123	22p	OC83	28p
2N2369A	19p	2N4291	15p	ACY19	23p	BC107	12p	BD124	44p	MP109	37p
2N2483	35p	2N4292	15p	ACY20	20p	BU108	11p	BD130	22p	MP6531	28p
2N2484	42p	2N4410	24p	ACY21	21p	BC109	12p	BD131	92p	MP6534	24p
2N2646	47p	2N4443	88p	ACY22	16p	BC122	21p	BD132	24p	SNCT1	12p
2N2904	38p	2N4905	274p	ACY39	62p	BC125	15p	BD135	22p	Matched pair	
2N2904A	42p	2N4906	227p	ACT40	17p	DC126	30p	BD141	24p		
2N2905	44p	2N4991	44p	ACY41	18p	BC140	15p	BD136	24p		
2N2905A	47p	2N5062	42p	ACY44	31p	BC147	10p	BDY20	23p		
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 with axial leads. Values in µF/m
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	1/4W	5%	4-7 Ω-10M Ω	E12	1	0	8
	1/2W	5%	4-7 Ω-10M Ω	E24	1	2	1
MO	1/2W	10%	4-7 Ω-10M Ω	E12	2	5	2
	1W	10%	10 Ω-1M Ω	E24	4	3	2
	3W	5%	0-22 Ω-3-9 Ω	E12	7	7	6
	7W	5%	1 Ω-10K Ω	E12	9	9	8

Prices are in pence each for quantities of the same ohmic value and power rating. NOT mixed values. (Ignore fractions on total value of resistor order.)
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THEY MADE THEIR MARK

NO 3 Ampère By J. E. Gregory



Photograph: Science Museum London

LAST month's article showed how Volta's discovery enabled man to produce small electric power from batteries, but to obtain larger powers he had to make magnets move. The man who did much to establish the relationship between electricity and magnetism was the French mathematician and physicist Ampère who gave his name to the practical unit of electrical current. See Table 1.

INFANT PRODIGY

Andre Marie Ampère was born on January 22, 1775, in the village of Polemiex, near Lyons, the son of a merchant, who was also Justice of the Peace.

Young Andre showed his astonishing capabilities at a very early age, and it is said that he was calculating before he could read or write.

It was in 1793, Andre now eighteen that tragedy struck. Lyons had revolted against the tyranny of the French Revolution. The army of the Convention who hated all forms of authority captured the town, Andre's father was thrown into prison, and soon after publicly guillotined.

The shock of this was so great that Ampère remained in a state of apathy and near madness for almost three years.

Then in 1796 he met Julie Carron who gave him back his reason for living.

On August 2, 1799 at the age of 24, he married Julie and one year later a son John Jacque was born. Once again Andre was a happy man.

In 1804 tragedy struck Ampère a second blow, his wife died of a chest disease; he did little for five years. Then in 1809 after publishing a thesis on the mathematical

Everyday Electronics, July 1972

Table 1: AMP (A)

The flow of electric current is measured in amps. Just as last month we used the water pressure analogy for the volt, so we can compare electric current with the flow of water.

As a practical example the current which flows through a domestic chandelier holding four, 60 watt lamps connected to a 240V mains supply is one ampere.

In 1881 the ampere along with the volt was adopted at the first meeting of the International Electrotechnical Committee.

theory of gambling he was recommended for the post of Professor of Mathematics at the Polytechnic in Paris. In 1814 he was elected to the Academy of Science.

OERSTED GETS THE NEEDLE

On 11th September 1820 Ampère heard that the Dane Oersted had discovered that a magnetic compass needle moved when placed near a wire carrying an electric current.

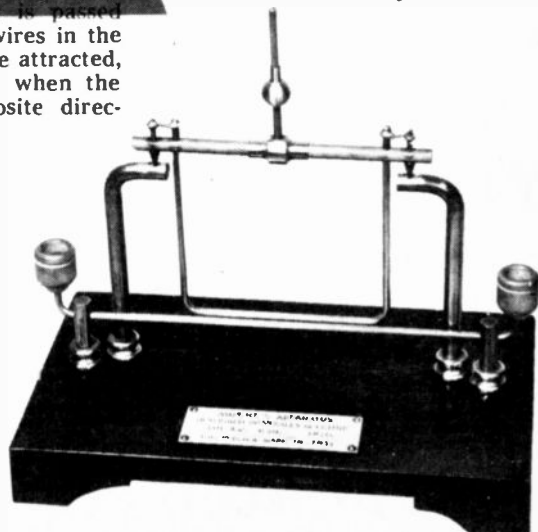
The news of this discovery so excited Ampère that he worked night and day experimenting on the relationship of electricity and magnetism, and on 18th September just one week later, presented to the academy the results of his experiments. These showed that when electric current is passed through two parallel wires in the same direction they are attracted, and they are repelled when the current flows in opposite direc-

tions. He also proved that the force of attraction or repulsion is directly proportional to the strength of the currents. This became known as Ampère's rule.

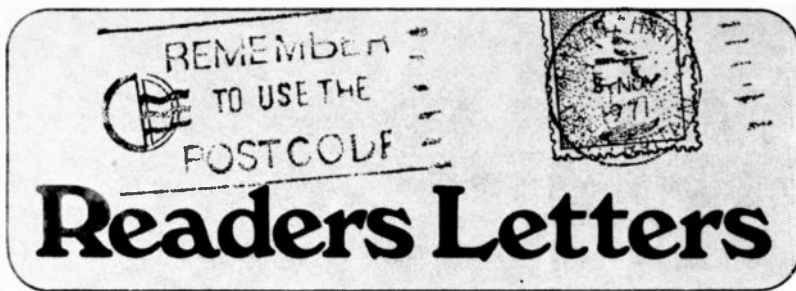
Ampère gave public demonstrations and one of his contemporaries reports "a gasp would go up from the audience as Ampère twisted insulated copper wire round an iron horseshoe, joined the ends of the wire to Volta's battery, and showed how the horseshoe attracted a quantity of nails, and how it let them fall the moment the current from the battery was shut off."

Ampère died in Marseilles on June 10, 1836 from a chest illness. James Clark Maxwell another famous 19th century physicist later described Ampère as "The Newton of Electricity"

Ampère's apparatus



Photograph: Crown copyright, Science Museum, London.



Saw Point

As a musician interested in the electronic aspects of music, I read with interest Mr. Judd's article on the *Audio Tone Generator*. He is however misleading about the question of sawtooth waveforms.

Although he is quite right when he says that a square wave contains only odd harmonics and the sawtooth wave consists of both odd and even harmonics, the waveform which he draws and which the integrating network on his generator will produce is not a sawtooth wave but, what is known in electronic music as a triangle wave. (I have also seen it referred to as a back-to-back sawtooth wave).

This waveform is symmetrical, and, like all symmetrical waveforms, consists only of odd harmonics. The difference between this and the square waveform lies in the phase relationship of the harmonic series and in the fact that they diminish in amplitude much more rapidly as their frequency increases.

The clarinet also has a symmetrical waveform and therefore only odd harmonics are present, but its timbre is totally unlike that of a square wave because the relative amplitude of their harmonics is different. If anything, a triangle wave sounds more like a clarinet.

R. Sherlaw Johnson
Stonesfield.

Stock Control

There is still one very basic problem which has slipped your attention, i.e. the building up of stock by the beginners. I wish you could advise us on the minimum quantity of various components we should keep in stock all the time, e.g. resistors (type, ratings, ohmic values and quantity of each type, etc.). Capacitors, diodes, transistors, nuts and bolts, chassis, cases, panels, heat-sinks, etc.

Very often when I set myself to build a project, I find it very embarrassing to get stuck for the shortage of some components and it gets more painful if the

local shop cannot help me either. I feel all the enthusiastic beginners would be very grateful if you could kindly help us in setting our stocks right at the beginning. Without proper guidance, at the start, all the component catalogues seem to be useless.

J. Whyte
London.

This is something we have been looking at and an article may be published in the future.

Solder Injector

Thank you for your very useful article on the *Signal Injector* in your March issue. I have constructed one with a few modifications, and I thought that some of your readers may be interested in the financial savings I made.

Firstly, I did not use the recommended Steradent tube (having no false teeth), but (to me) a more readily available case—the standard multicore solder tube. To the pointed end I fixed my nail directly using fibreglass paste (eg. Isoxon), this did away with the need for a miniature plug and socket. The switch was fixed to the plastic cap.

As regards the construction, I used a smaller piece of Veroboard, given away in your first issue (after making a *Windscreen Wiper Control*). The components specified were not at all critical; I used two OC 71 transistors and 0.1 μ F capacitors throughout to get excellent results.

May I take this opportunity to suggest a few ideas for future projects in your excellent magazine:—

1. A stabilised voltage dropper, so that a portable cassette player may be used off a car battery.
2. Short range transmitter (if legal?).
3. More audio and hi-fi projects.
4. Lighting effects controlled by music from an amplifier.

K. J. Twydell
Portsmouth.

Of the four items you suggest the transmitter is not legal in this country without a radio amateur's licence, the other three things will probably be future articles.

Join the Club

Readers may be interested in my slightly modified version of the *Demo Deck*.

I made my top in Formica and cut a recess to take a commercial "breadboard"; the single S-Dec unit with little spring-loaded clips and holes to take components. Hence there is no need for soldering or, even more important, dodgy desoldering which can result in damage. My S-Dec cost me £1, but I think, for a beginner, it is a good investment.

I am glad to see EVERYDAY ELECTRONICS making good progress. There certainly was a crying need for a journal of this type catering for raw amateurs. I would suggest that at some future date you consider forming a national club for electronics enthusiasts of humble skills. Who knows, it could lead to a healthy exchange of ideas, a feeling of camaraderie and (I've got grandiose ideas!) eventually a national exhibition. Why not? Indeed your E.E. symbol on the contents page would make a perfect badge.

Pity about these errors that are creeping in with too much frequency; it tends to undermine confidence a little. However, as a fellow journalist, I'll make allowances for a little while yet.

Incidentally, do I dare suspect a slip in Mike Hughes' Teach-in last month (May) where on page 371, top of column one, he refers to VR1 as "a 300 ohm potentiometer". I'm afraid those of us with *Demo Decks* followed an earlier design and made this a 100 ohm pot—or have I got my things in a twist?

Never mind, for an expert to try to put over an advanced science that's constantly on the move is one big headache when he has pupils at all levels of training and can't thump those of us who are a bit thick on the uptake.

T. Milligan
Kempston.

We must point out that The British Amateur Electronics Club caters for all interested in electronics. Details from the Hon. Secretary, Mr. J. G. Margetts, 17 Saint Francis Close, Abergavenny, Monmouthshire.

The value of VR1 should be 100 ohms.

Enlightening

Upon reading "Sensor's" article *Let There Be Light* I was surprised at his lack of knowledge concerning street lighting. Light operated switches have been used in street lighting systems for several years, the reason for not using them on every light is that

safe soldering



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AC187 25p		ST140 18p	2N2369A
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AC187 25p		2N3183 12p	2N2369A
AC187 25p		2N3184 12p	2N2369A
AC187 25p		2N3185 12p	2N2369A
AC187 25p		2N3186 12p	2N2369A
AC187 25p		2N3187 12p	2N2369A
AC187 25p		2N3188 12p	2N2369A
AC187 25p		2N3189 12p	2N2369A
AC187 25p		2N3190 12p	2N2369A
AC187 25p		2N3191 12p	2N2369A
AC187 25p		2N3192 12p	2N2369A
AC187 25p		2N3193 12p	2N2369A
AC187 25p		2N3194 12p	2N2369A
AC187 25p		2N3195 12p	2N2369A
AC187 25p		2N3196 12p	2N2369A
AC187 25p		2N3197 12p	2N2369A
AC187 25p		2N3198 12p	2N2369A
AC187 25p		2N3199 12p	2N2369A
AC187 25p		2N3200 12p	2N2369A
AC187 25p		2N3201 12p	2N2369A
AC187 25p		2N3202 12p	2N2369A
AC187 25p		2N3203 12p	2N2369A
AC187 25p		2N3204 12p	2N2369A
AC187 25p		2N3205 12p	2N2369A
AC187 25p		2N3206 12p	2N2369A
AC187 25p		2N3207 12p	2N2369A
AC187 25p		2N3208 12p	2N2369A
AC187 25p		2N3209 12p	2N2369A
AC187 25p		2N3210 12p	2N2369A
AC187 25p		2N3211 12p	2N2369A
AC187 25p		2N3212 12p	2N2369A
AC187 25p		2N3213 12p	2N2369A
AC187 25p		2N3214 12p	2N2369A
AC187 25p		2N3215 12p	2N2369A
AC187 25p		2N3216 12p	2N2369A
AC187 25p		2N3217 12p	2N2369A
AC187 25p		2N3218 12p	2N2369A
AC187 25p		2N3219 12p	2N2369A
AC187 25p		2N3220 12p	2N2369A
AC187 25p		2N3221 12p	2N2369A
AC187 25p		2N3222 12p	2N2369A
AC187 25p		2N3223 12p	2N2369A
AC187 25p		2N3224 12p	2N2369A
AC187 25p		2N3225 12p	2N2369A
AC187 25p		2N3226 12p	2N2369A
AC187 25p		2N3227 12p	2N2369A
AC187 25p		2N3228 12p	2N2369A
AC187 25p		2N3229 12p	2N2369A
AC187 25p		2N3230 12p	2N2369A
AC187 25p		2N3231 12p	2N2369A
AC187 25p		2N3232 12p	2N2369A
AC187 25p		2N3233 12p	2N2369A
AC187 25p		2N3234 12p	2N2369A

—apart from major towns—most street lights are extinguished at midnight, light operated switches cannot do this. Another reason is that the electricity boards own most of the time switches and to install light operated switches in place of these costs in the region of £12 to £15 per column. This cost has to be found out of the rates we pay because councils have to purchase these as opposed to timeswitches—the other side effect is higher electricity bills to councils due to the permanent all night lighting. We do not get enough power cuts to warrant this vast extra expense on the rates.

I am employed by a firm of street lighting contractors, fitting and maintaining public lighting.

B. W. Hawkins
Herts.

Clanger

I have been reading your magazine since it was first published and found it quite good. Unfortunately under the article about the *Bee Counter* in the May issue I think you have dropped a proverbial "clanger". The *Bee Counter* works as drawn in the circuit but the write up is all wrong. You say that TR1 is conduction when the l.d.r. has a low resistance (i.e. when illuminated) which of course it will not because it is a pnp transistor; TR2 will therefore be "off" until TR1 conducts.

When a bee passes between the lamp and the l.d.r. the resistance of the l.d.r. increases and the base potential becomes negative with respect to the emitter. This causes TR1 to conduct and a negative potential is then applied to TR2 causing it to conduct and the counter to operate.

I think your write up should have been along these lines. It looked especially funny after the previous article on semiconductors. Perhaps Mike Hughes will give a few lessons to the editorial staff!

W. Raymond
Old Trafford

You are of course quite right—we have asked Mike if he has any free time!

Circuit Operation

I was very pleased to receive the booklet *Constructors Companion* with the May issue. Now I know that little bit more about the modes of transistors, the explanation although brief was easily understood.

Will you please publish a feature about how circuits work, that is, the a.c. (signal) and d.c. conditions in circuits when in operation? For example, the pro-

gress of a signal from aerial to speaker; through all the components also the d.c. conditions of the circuit at the same time.

You will probably have noticed that, in all receiver circuits authors never give this explanation which I believe would be of considerable help to the understanding of how the circuits "work" especially in receivers.

Would it also be possible to have either a regular feature or a regular pull-out supplement of a list of circuits for doing a variety of things.

J. Bradley
Yorks.

We may well be publishing a series on basic circuit operation describing the function and operation of many of the "standard circuits" we use.

Convention

I would be most grateful if you could explain to me the logic of using "conventional current" in contemporary circuit diagrams.

You see, when I was at school my physics master dismissed this as being "guesswork on the part of the ancients (electrically speaking)." Thus he explained electrical phenomena in the light of "electron flow" and I was able to understand him sufficiently to construct simple valve radios, home electroplating appliances etc.

Similarly an R.A.F. radar instructor was able to acquaint us with the principles of the cathode ray tube etc., whilst we blockheads were undergoing operational training in bomber command during the war.

Much later in life I decided to take an exam involving some knowledge of electronics and thus went through a "refresher". Again, the instructor used "electron flow" as his means of explanation; again I understood.

To the best of my knowledge, all electro/mechanical devices which demonstrate a "current flow" visibly, do so in a way which shows that, whatever is flowing, is flowing from negative to positive (except in the interiors or prime sources).

Would you therefore be kind enough to inform me:

a) who re-introduced "conventional current flow"?

b) Why?

You see, if I knew the reason for using this terminology I would possibly better be able to reconcile myself with it and thus get down to some learnings instead of getting het up at symbols which appear, to me, just plain stupid!

A. K. Robinson
London, W.7.

As far as we know no one re-introduced conventional current flow—it has always been with us, ever since Volta's battery.

Unfortunately it is not easy to simply drop conventional current and use electron flow as all the laws concerning electricity and magnetism—which are, after all, the basis of the whole thing—are in terms of conventional current flow. Thus, although it is easy to explain such things as cathode ray tubes and transistors using electron flow, when it comes to teaching the basics of electricity then all the universal basic rules which are in terms of conventional current flow would have to be changed.

One-sided

While experimenting with tape loops, prompted by your May article, I discovered some promising effects by giving the tape a half turn before joining the loop. This produces a "one-sided" tape, with the interesting result that both tracks of the tape are scanned successively.

Unfortunately, half the cycle presents the shiny side of the tape to the head. However, by using triple-play (very thin) tape and turning the loop over after recording, interesting reverse/echo effects were obtained.

By the way, inserting a 1M Ω linear potentiometer in the collector load of TR2 of the *Signal Injector* circuit (March issue) makes an excellent tone generator, serving both purposes, at a saving of some £2.50.

R. Darbishire
Surrey.

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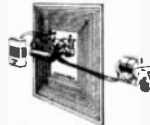


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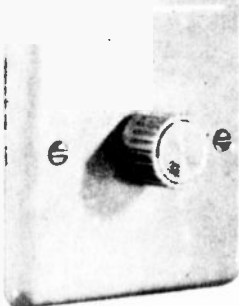
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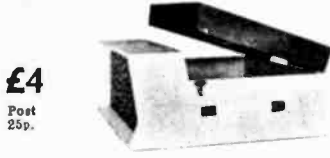
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TRANSISTORS

AC 107	15p	AL 102	50p	BC 212L	8p	ME 6101	14p	OC 140	17p	2N 2924	9p	IN 4007	13p
AC 126	15p	AL 103	49p	BC 213L	8p	ME 6102	15p	OC 170	22p	2N 3053	20p	W605	30p
AC 127	15p	AL 103	55p	BC 214L	8p	MP 8111	32p	OC 171	22p	2N 3053	49p	W02	35p
AC 128	15p	AL 111	95d	BD 121	50p	MP 8112	34p	OC 200	25p	2N 3702	12p	OA 90	8p
AC 176	22p	BC 107	8p	BD 123	60p	MP 8511	34p	OC 23	30p	2N 3704	12p	OA 91	6p
AC 141	15p	BC 108	8p	BD 130	45p	MP 8513	45p	OC 25	25p	2N 3703	12p	IN 4148	4p
AC 142	15p	BC 109	8p	BFY 50	18p	OC 41	18p	OC 28	30p	40836	55p	400mW Zeners	3-3-30v 10p
AC 143K	30p	BC 154	20p	BFY 51	12p	OC 44	18p	OC 29	30p				
AC 142K	30p	BC 154	10p	BFY 52	12p	OC 45	18p	OC 36	30p	Rectifiers			
AD 142	30p	BC 169	11p	BNV 93A	15p	OC 71	13p	OC 36	30p	IN 4001	5p		
AD 149	40p	BC 144	10p	ME 0402	18p	OC 72	18p	2N 697	13p	IN 4002	6p		
AD 150	44p	BC 149	10p	ME 0404	14p	OC 81	18p	2N 1171	24p	IN 4003	6p		
AD 140	40p	BC 182L	8p	ME 4101	10p	OC 81D	18p	2N 1304	25p	IN 4004	6p		
AD 161	11p	BC 183L	8p	ME 4102	12p	OC 83	20p	2N 1305	25p	IN 4005	11p		
AD 162	5p	BC 184L	8p	ME 6002	14p	OC 139	18p	2N 2646	47p	IN 4006	12p		

CAPACITORS

MULLARD POLYESTER CAPACITORS C280 SERIES
250V P.C. mounting: 0.01µF, 0.015µF, 0.022µF, 3p, 0.033µF, 0.047µF, 0.068µF, 31p, 0.1µF, 4p, 0.15µF, 0.22µF, 5p, 0.30µF, 61p, 0.47µF, 81p, 0.68µF, 11p, 1.0µF, 13p, 1.5µF, 20p, 2.2µF, 24p.

ELECTROLYTIC CAPACITORS—MULLARD C426 SERIES 8p each. (µF/V) 10/2-5, 40/2-5, 80/2-5, 160/2-5, 320/2-5, 500/2-5, 814, 32/4, 64/4, 125/4, 250/4, 400/4, 6-4/6-4, 25/6-4, 50/6-4, 100/6-4, 200/6-4, 320/6-4, 4/10, 16/10, 32/10, 64/10, 125/10, 200/10, 2-5/16, 10/16, 20/16, 40/16, 80/16, 125/16, 1-6/25, 6-4/25, 12-5/25, 25/25, 50/25, 80/25, 1/40, 4/40, 8/40, 16/40, 32/40, 50/40, 0-64/64, 2-5/64, 5/64, 10/64, 20/64, 32/64.

SILVERED MICA. 500v d.c. 8p each
Values (PF): 2-2, 5, 8-2, 10, 12, 15, 18, 22, 24, 27, 30, 33, 35, 39, 47, 50, 56, 68, 75, 82, 100, 120, 150, 180, 200, 220, 250, 7p each—270, 300, 330, 390, 400, 470, 500, 556, 680, 800, 10p each.—1000, 1500, 1800, 2200, 18p each.—2700, 3600, 20p each.—4700, 5000, 38p each.—5600, 6800, 8200, 10000.

RESISTORS
½ watt 10% carbon ½ watt 10% carbon 1p each
Range 2-2 ohms to 10 meg.
TR5 triple rated at ½—1 watt tin oxide resistor ±2% 3p each. Range 10 ohms—1 meg ohm.

SLIDE SWITCH
SPST 18p each SP Three Positions 12p each

MINIATURE NEON LAMPS
240v or 110v 1-4 5p, 5 plus 4 5p each.

LINEAR IC's
709c TO99 28p 41c TO99 80p
709c DIL 28p 741c DIL 36p

BARGAIN TTL's at 15p each
7400, 7401, 7402, 7403, 7404, 7410, 7420, 7430, 7440
7450, 7451, 7453, 7454.
35p each:

7442, 7470, 7472, 7473, 7474, 7476, 7486.
AND LOTS MORE

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RESISTORS

1/4W Iskra high stability carbon film—very low noise—capless construction. 1/2W Mullard CR25 carbon film—very small body size 7.5 x 2.5mm. 1/2W 2% Electroisil TRS.

Power watts	Tolerance	Range	Values available	Price 1-99	100+
1/4	5%	4.7Ω-2.2MΩ	E24	1 0p	0 8p
1/4	10%	3.3MΩ-10MΩ	E12	1 0p	0 8p
1/2	2%	10Ω-1M	E24	3 5p	3 0p
1/2	10%	1Ω-3.9Ω	E12	1 0p	0 8p
1	5%	4.7Ω-1MΩ	E12	1 0p	0 8p
1	10%	1Ω-10Ω	E12	6p	5 5p

Quantity price applies for any selection. Ignore fractions on total order.

DEVELOPMENT PACK

0.5 watt 5% Iskra resistors 5 off each value 4.7Ω to 1MΩ. E12 pack 325 resistors £2.40. E24 pack 650 resistors £4.70.

POTENTIOMETERS

Carbon track 5kΩ to 2MΩ, log or linear (log 1/2W, lin 1/4W). Single, 12p. Dual gang (stereo), 40p. Single D.P. switch 24p.

SKELETON PRESET POTENTIOMETERS

Linear: 100, 250, 500Ω and decades to 5MΩ. Horizontal or vertical P.C. mounting (0.1 matrix). Sub-miniature 0.1W, 5p each. Miniature 0.25W, 6p each.

TRANSISTORS

AC107 15p	BC107 10p	BF195 15p	OC81 12p	2N3703 12p
AC126 12p	BC108 10p	BFY50 22p	OC82D 12p	2N3704 13p
AC127 12p	BC109 10p	BFY51 22p	OC771 40p	2N3705 12p
AC128 12p	BC147 10p	BFY52 22p	ORP12 50p	2N3706 12p
AC131 12p	BC148 13p	BSY56 32p	2N2369 16p	2N3707 12p
AC132 12p	BC149 13p	OC26 45p	2N2646 60p	2N3708 10p
AD140 50p	BC157 13p	OC28 45p	2N2926R 9p	2N3709 11p
AD161 30p	BC158 13p	OC35 45p	2N2926G 9p	2N3710 11p
AD162 30p	BC159 13p	OC42 12p	2N2926V 9p	2N3711 11p
AF114 20p	BD131 75p	OC44 12p	2N2966 10p	2N4062 12p
AF115 20p	BD132 75p	OC45 12p	2N3054 58p	ZTX302 15p
AF116 20p	BF179 32p	OC70 12p	2N3055 60p	ZTX500 16p
AF117 20p	BF181 25p	OC71 12p	2N3442 140p	ZTX503 16p
AF118 38p	BF194 15p	OC72 12p	2N3702 13p	40362 58p

ZENER DIODES

400mW 5% 3-30V to 30V, 15p.

LINEAR IC's (DIL)	DIL SOCKET
709 50p	741 50p
710 50p	748 50p

DIODES RECTIFIER

DIODES RECTIFIER	SIGNAL	7p
BY127 1250V	1A	12p
BZY10 800V	6A	25p
BZY13 200V	6A	20p
IN4001 50V	1A	8p
IN4004 400V	1A	8p
IN4007 1000V	1A	12p

BRUSHED ALUMINIUM PANELS

12in x 6in—25p; 12in x 2 1/2in—10p; 9in x 2in—7p.

SLIDER POTENTIOMETERS

86mm x 9mm x 16mm, length of track 59mm. SINGLE 10K, 25K, 100K log. or lin. 40p. DUAL GANG, 10K + 10K etc. log. or lin. 60p. KNOB FOR ABOVE 12p. FRONT PANEL 65p. 18 Gauge panel 12" x 4" with slots cut for use with slider pots. Grey or matt black finish complete with fixings for 4 pots.

MULLARD POLYESTER CAPACITORS C296 SERIES

400V: 0.001μF, 0.0015μF, 0.0022μF, 0.0033μF, 0.0047μF, 2 1/2p. 0.0068μF, 0.01μF, 0.015μF, 0.022μF, 0.033μF, 0.047μF, 0.068μF, 0.1μF, 4p. 0.15μF, 6p. 0.22μF, 7 1/2p. 0.33μF, 11p. 0.47μF, 13p.

160V: 0.01μF, 0.015μF, 0.022μF, 0.033μF, 0.047μF, 0.068μF, 3p. 0.1μF 3 1/2p. 0.15μF, 4p. 0.22μF, 5p. 0.33μF, 6p. 0.47μF, 7 1/2p. 0.68μF, 11p. 1.0μF, 13p.

MULLARD POLYESTER CAPACITORS C280 SERIES

250V P.C. mounting: 0.01μF, 0.015μF, 0.022μF, 0.033μF, 0.047μF, 0.068μF, 3 1/2p. 0.1μF, 4p. 0.15μF, 0.22μF, 5p. 0.33μF, 6 1/2p. 0.47μF, 8 1/2p. 0.68μF, 11p. 1.0μF, 13p. 1.5μF, 20p. 2.2μF, 24p.

MYLAR FILM CAPACITORS 100V,

0.001μF, 0.002μF, 0.005μF, 0.01μF, 0.02μF, 2 1/2p. 0.04μF, 0.05μF, 0.068μF, 0.1μF, 3 1/2p.

CERAMIC DISC CAPACITORS

100pF to 10,000pF, 2p each.

ELECTROLYTIC CAPACITORS—MULLARD C426 SERIES

6p each (μF/V) 10/2.5, 40/2.5, 80/2.5, 160/2.5, 320/2.5, 500/2.5, 8/4.32 1/4, 64/4, 125/4, 250/4, 400/4, 6.4/6.4, 25/6.4, 50/6.4, 100/6.4, 200/6.4, 320/6.4, 4/10, 16/10, 32/10, 64/10, 125/10, 200/10, 2.5/16, 10/16, 20/16, 40/16, 80/16, 125/16, 1.6/25, 6.4/25, 12.5/25, 25/25, 50/25, 80/25, 1/40, 4/40, 8/40, 16/40, 32/40, 50/40, 0.64/64, 2.5/64, 5/64, 10/64, 20/64, 32/64.

MULLARD C437 SERIES

100/40, 160/25, 250/16, 400/10, 640/6.4, 800/4, 1000/2.5, 9p. 100/64, 160/40, 250/25, 400/16, 640/10, 1250/4, 1000/6.4, 1600/2.5, 12p. 160/64, 250/40, 400/2.5, 640/16, 200/4, 1000/10, 1600/6.4, 2500/2.5, 15p. 250/64, 400/40, 640/25, 3200/4, 1000/16, 1600/10, 2500/6.4, 4000/2.5, 18p.

ELECTROLYTIC CAPACITORS Miniature P.C. mounting

5p each. (μF/V) 10/12, 50/12, 100/12, 200/12, 5/25, 10/25, 25/25, 100/25.

VEROBOARD

2 1/2 x 3 1/2	0.1	0.15
2 1/2 x 5	22p	17p
3 1/2 x 3 1/2	24p	21p
3 1/2 x 5	24p	21p
3 1/2 x 7 1/2	28p	29p
17 x 2 1/2	75p	57p
17 x 3 1/2	100p	78p
17 x 5 (plain)	—	82p
17 x 3 1/2 (plain)	—	60p
17 x 2 1/2 (plain)	—	42p
2 1/2 x 5 (plain)	—	12p
2 1/2 x 3 1/2 (plain)	—	11p
Pin insertion tool	52p	52p
Spot face cutter	42p	42p
Pkt. 50 pins	20p	20p

JACK PLUGS AND SOCKETS

Standard screened	18p	2.5mm insulated	8p
Standard insulated	12p	3.5mm insulated	8p
Stereo screened	35p	3.5mm screened	13p
Standard socket	15p	2.5mm socket	8p
Stereo socket	18p	3.5mm socket	8p

D.I.N. PLUGS AND SOCKETS

2 pin, 3 pin, 5 pin 180°, 5 pin 240°, 6 pin Plug 12p. Socket 8p.

4 way screened cable 15p/metre

6 way screened cable 22p/metre

BATTERY ELIMINATOR

£1.50 9V mains power supply. Same size as PP9 battery.

THERMISTORS

VA1055 15p VA1066S 15p VA1077 15p R53 £1.35

COMPACT CASSETTES—IN PLASTIC LIBRARY BOX

C90 65p C120 85p

LARGE (CAN) ELECTROLYTICS

1600μF	64V	74p	3200μF	16V	50p
2500μF	40V	74p	4500μF	16V	50p
2500μF	50V	88p	4500μF	25V	£1.68
2500μF	64V	80p	5000μF	50V	£1.10
2800μF	100V	£3.00			

HIGH VOLTAGE TUBULAR CAPACITORS—1,000 VOLT

0.01μF 10p 0.047μF 13p 0.22μF 20p

0.022μF 12p 0.1μF 16p 0.47μF 22p

POLYSTYRENE CAPACITORS 160V 2 1/2%

10pF to 1,000pF E12 Series values 4p each.

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COMPONENTS**

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TRANSISTORS											
2G301	20p	2N3404	32p	40311	35p	BCY30	27p	BRX60	82p	NKT401	87p
2G302	20p	2N3405	45p	40312	47p	BCY31	30p	BRX61	82p	NKT402	80p
2G303	20p	2N3414	28p	40314	37p	BCY32	50p	BRX76	22p	NKT403	75p
2G306	42p	2N3415	28p	40320	47p	BCY33	25p	BRX77	27p	NKT404	82p
2G308	30p	2N3416	37p	40323	32p	BCY34	30p	BRX78	27p	NKT405	75p
2G309	30p	2N3417	37p	40324	47p	BCY38	40p	BRY10	27p	NKT406	82p
2G371	15p	2N3370	15p	40325	37p	BCY39	60p	BRY11	27p	NKT451	62p
2G37	20p	2N3372	97p	40329	30p	BCY40	50p	BRY14	15p	NKT452	62p
2G381	22p	2N3605	27p	40344	27p	BCY42	15p	BRY25	15p	NKT453	47p
2N404	22p	2N3606	27p	40347	57p	BCY43	15p	BRY26	17p	NKT603	32p
2N696	20p	2N3607	28p	40348	52p	BCY54	32p	BRY27	17p	NKT603	32p
2N697	17p	2N3702	11p	40360	42p	BCY58	22p	BRY28	17p	NKT674	37p
2N698	26p	2N3703	10p	40361	47p	BCY59	22p	BRY29	17p	NKT677	37p
2N706	12p	2N3704	11p	40362	57p	BCY60	97p	BRY32	25p	NKT713	25p
2N705A	12p	2N3705	10p	40370	32p	BCY70	20p	BRY36	25p	NKT741	30p
2N708	15p	2N3706	09p	40406	57p	BCY71	25p	BRY37	25p	NKT10419	30p
2N709	62p	2N3707	11p	40407	40p	BCY72	17p	BRY38	22p	NKT10439	37p
2N718	26p	2N3708	07p	40408	52p	BCZ10	27p	BRY39	22p		
2N726	30p	2N3709	09p	40410	62p	BCZ11	42p	BRY40	32p	NKT10519	37p
2N727	30p	2N3710	09p	40414	57p	BD116	11.12p	BRY51	37p		32p
2N914	17p	2N3711	12p	40484A	35p	BD121	11.00p	BRY52	32p	NKT20329	37p
2N916	17p	2N3715	11.25p	40600	57p	BD123	85p	BRY53	37p		47p
2N918	30p	2N3716	11.30p	AC107	30p	BD124	60p	BRY54	40p	NKT20339	37p
2N929	22p	2N3791	22.08p	AC126	20p	BD131	75p	BRY56	90p		37p
2N930	27p	2N3819	35p	AC127	25p	BD132	85p	BRY78	47p	NKT80111	77p
2N1090	22p	2N3823	97p	AC128	20p	BDY10	11.37p	BRY79	45p		
2N1091	22p	2N3854	27p	AC184	22p	BDY11	11.62p	BRY82	52p	NKT80112	77p
2N1131	17p	2N3854A	27p	AC185	22p	BDY17	11.50p	BRY89	57p		37p
2N1132	25p	2N3855	27p	AC187	62p	BDY18	11.25p	BRV95A	12p	NKT80113	77p
2N1302	17p	2N3855A	30p	AC188	37p	BDY19	11.97p	BRW41	42p		11.12p
2N1303	17p	2N3856	30p	ACY17	27p	BDY20	11.12p	BRW70	27p	NKT80211	82p
2N1304	22p	2N3856A	35p	ACY18	25p	BDY38	97p	C111	75p		82p
2N1305	22p	2N3858	25p	ACY19	25p	BDY60	11.25p	C424	27p	NKT80212	82p
2N1306	25p	2N3858A	30p	ACY20	25p	BDY61	11.25p	C425	35p		92p
2N1307	20p	2N3859	27p	ACY21	22p	BF102	21.00p	C426	37p	NKT80213	82p
2N1308	30p	2N3859A	32p	ACY22	20p	BF115	25p	C428	55p		92p
2N1309	30p	2N3860	30p	ACY28	20p	BF117	47p	C744	30p	NKT80214	82p
2N1307	17p	2N3866	11.50p	ACY40	20p	BF163	37p	DI16P1	37p		82p
2N1613	25p	2N3877	40p	ACY41	25p	BF167	18p	DI16P2	40p	NKT80215	82p
2N1631	35p	2N3877A	40p	ACY44	40p	BF173	19p	DI16P3	37p		92p
2N1632	30p	2N3878	37p	AD140	50p	BF177	18p	DI16P4	37p	NKT80216	82p
2N1638	27p	2N3900A	40p	AD149	57p	BF178	30p	GET102	30p		92p
2N1639	27p	2N3901	97p	AD150	62p	BF179	30p	GET113	20p	OC20	75p
2N1671B	11.00p	2N3903	35p	AD161	37p	BF180	35p	GET114	20p	OC22	50p
2N1711	25p	2N3904	35p	AD162	37p	BF181	32p	GET115	20p	OC23	60p
2N1889	32p	2N3905	37p	AF106	42p	BF184	25p	GET119	20p	OC24	60p
2N1893	87p	2N3906	37p	AF114	25p	BF185	42p	GET120	52p	OC25	50p
2N1947	82p	2N4058	17p	AF115	25p	BF194	17p	GET121	12p	OC26	77p
2N2144	57p	2N4059	10p	AF116	25p	BF195	15p	GET180	30p	OC29	62p
2N2160	57p	2N4060	12p	AF117	25p	BF196	42p	GET187	20p	OC29	62p
2N2193	40p	2N4061	12p	AF118	62p	BF197	42p	GET189	22p	OC35	50p
2N2193A	42p	2N4062	12p	AF119	20p	BF198	42p	GET189	22p	OC36	62p
2N2194	30p	2N4244	47p	AF124	22p	BF200	52p	GET186	22p	OC41	22p
2N2217	27p	2N4285	17p	AF125	20p	BF204	14p	GET187	22p	OC42	25p
2N2218	23p	2N4286	17p	AF126	20p	BF205	19p	GET189	22p	OC44	25p
2N2219	23p	2N4287	17p	AF127	17p	BF237	23p	MJ400	11.07p	OC45	12p
2N2220	25p	2N4288	17p	AF129	37p	BF238	23p	MJ420	11.12p	OC46	15p
2N2221	25p	2N4290	17p	AF128	42p	BF244	23p	MJ421	11.12p	OC70	15p
2N2222	30p	2N4291	17p	AF129	72p	BFW81	47p	MJ430	11.02p	OC71	12p
2N2270	47p	2N4292	12p	AF180	52p	BFX12	22p	MJ440	11.05p	OC72	12p
2N2297	20p	2N4303	57p	AF181	42p	BFX13	22p	MJ480	97p	OC74	32p
2N2368	17p	2N5027	58p	AF209	42p	BFX29	27p	MJ481	11.25p	OC75	22p
2N2369	17p	2N5028	57p	AF209	47p	BFX30	30p	MJ490	11.00p	OC76	22p
2N2369A	17p	2N5029	47p	AF290	62p	BFX42	37p	MJ491	11.37p	OC77	30p
2N2410	42p	2N5030	42p	AF211	32p	BFX44	37p	MJ800	22.17p	OC81	20p
2N2483	27p	2N5172	12p	AFY26	25p	BFX68	67p	MJF340	62p	OC81D	22p
2N2484	32p	2N5174	62p	AFY27	27p	BFX84	35p	MJF350	60p	OC83	25p
2N2529	22p	2N5175	22p	AFY28	27p	BFX85	27p	MJF351	60p	OC83	25p
2N2540	22p	2N5176	45p	AFY29	27p	BFX86	25p	MJF102	42p	OC139	32p
2N2613	35p	2N5232A	30p	AFY36	25p	BFX87	27p	MJF103	37p	OC140	32p
2N2614	30p	2N5246	45p	AFY50	25p	BFX88	25p	MJF104	37p	OC170	30p
2N2646	52p	2N5246	42p	AFY51	32p	BFX89	62p	MJF105	37p	OC171	30p
2N2696	32p	2N5249	67p	AFY54	25p	BFX93A	70p	MPH3638	32p	OC200	40p
2N2711	25p	2N5249	67p	AFY86	32p	BFY10	82p	NKT0013	47p	OC201	75p
2N2712	25p	2N5266	22.75p	AF103	11.82p	BFY11	42p	NKT014	47p	OC202	75p
2N2713	27p	2N5267	22.82p	ASZ21	42p	BFY17	22p	NKT125	27p	OC203	48p
2N2714	30p	2N5303	37p	BC107	10p	BFY18	32p	NKT126	27p	OC204	42p
2N2865	62p	2N5306	40p	BC108	10p	BFY19	32p	NKT128	27p	OC205	90p
2N2904	30p	2N5307	37p	BC109	10p	BFY20	11.00p	NKT135	27p	OC207	75p
2N2904A	32p	2N5308	37p	BC113	15p	BFY21	42p	NKT137	32p	OC271	42p
2N2905	37p	2N5309	62p	BC115	15p	BFY24	45p	NKT210	30p	ORP12	50p
2N2905A	40p	2N5310	49p	BC116A	15p	BFY25	25p	NKT211	30p	ORP61	50p
2N2906	25p	2N5354	27p	BC118	10p	BFY26	20p	NKT212	30p	P346A	22p
2N2906A	27p	2N5355	27p	BC121	20p	BFY29	50p	NKT213	30p	T1834	62p
2N2907	30p	2N5356	32p	BC122	20p	BFY30	50p	NKT214	22p	T1843	27p
2N2923	15p	2N5365	47p	BC125	20p	BFY41	50p	NKT215	22p	T1844	10p
2N2924	15p	2N5366	32p	BC126	20p	BFY42	62p	NKT216	37p	T1845	10p
2N2925	15p	2N5367	57p	BC140	37p	BFY50	28p	NKT217	42p	T1846	11p
2N2926	15p	2N5457	37p	BC147	10p	BFY51	20p	NKT219	30p	T1847	11p
Green	14p	28005	75p	BC148	10p	BPV52	23p	NKT223	27p	T1848	12p
Yellow	12p	28020	22.00p	BC149	12p	BPV53	17p	NKT224	25p	T1849	12p
Orange	12p	28102	50p	BC152	17p	BPV56A	57p	NKT225	25p	T1850	12p
2N3011	30p	28103	25p	BC157	20p	BPV75	40p	NKT229	30p	T1851	12p
2N3014	32p	28104	25p	BC158	12p	BPV76	42p	NKT237	35p	T1852	12p
2N3053	18p	28501	32p	BC159	12p	BPV77	57p	NKT238	35p	T1853	22p
2N3054	46p	28502	35p	BC160	62p	BPV90	67p	NKT240	27p	T1860	22p
2N3055	62p	28503	27p	BC167	11p	BPV58	27p	NKT241	27p	T1861	25p
2N3133	30p	3N83	40p	BC168B	10p	BPV59	25p	NKT242	20p	T1862	27p
2N3134	30p	3N128	70p	BC168C	11p	BPW80	25p	NKT243	62p	T1P29A	50p
2N3135	25p	28140	77p	BC169B	11p	BPX25	11.85p	NKT244	17p	T1P30A	80p
2N3136	25p	28141	72p	BC190C	12p	BPX29	45p	NKT245	20p	T1P31A	62p
2N3190	25p	3N142	55p	BC170	12p	BPY10	11.45p	NKT261	20p	T1P32A	75p
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2N3193	15p	40050	55p	BC182	10p	BRX20	37p	NKT272	20p	T1P35A	22.90p
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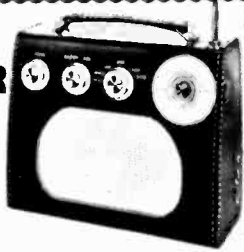
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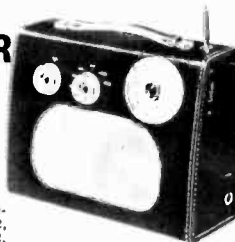
7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Built in Ferrite Rod Aerial for MW and LW. Retractable chrome plated Telescopic aerial for Short Waves. Push pull output using 600mw transistors. Car aerial and Tape record sockets. Selectivity switch. Switched earpiece socket complete with earpiece. 8 transistors plus 3 diodes. 8" x 2 1/2" Speaker. Air spaced ganged tuning condenser. Volume/on/off, tuning, wave change and tone controls. Attractive case in rich chestnut shade with gold blocking. Size 9 x 7 x 4in. approx. Easy to follow instructions and diagrams. Parts Price List and Easy Build Plans 25p (FREE with parts).

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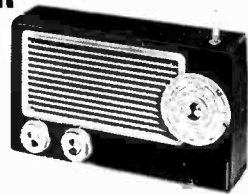
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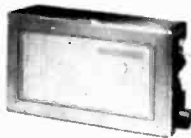
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POCKET FIVE

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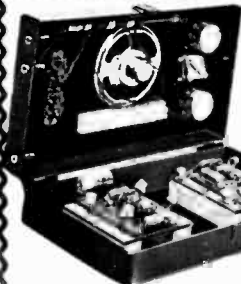
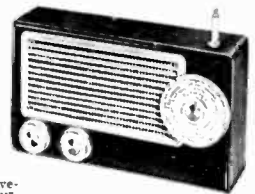


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