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TWO - DIMENSIONAL
LATERALLY - INTEGRATED ESTUARINE
NUMERICAL WATER QUALITY MODEL

VOLUME II - USER'S MANUAL

MALCOLM L. SPAULDING

FRANK M. WHITE

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(401) 792-6114

DEPARTMENT OF MECHANICAL ENGINEERING AND APPLIED MECHANICS

UNIVERSITY OF RHODE ISLAND

KINGSTON, RHODE ISLAND

1974

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This report, the second in a series of two, is a user's manual for a numerical water quality simulation model complete with Fortran IV program listings and verification runs. The first volume describes the detailed development of the model and its application to Narragansett Bay, Narragansett, Rhode Island. Additional copies of this volume, as well as volume one, can be obtained from the URI Marine Advisory Service, Narragansett Bay Campus, Narragansett, Rhode Island 02882. *no longer available*

USER'S MANUAL

A COMPUTER SIMULATION MODEL

TWO-DIMENSIONAL, LATERALLY-INTEGRATED, ESTUARINE

NUMERICAL WATER QUALITY MODEL

NABS (Narragansett Bay Study)

TDLIDO (Two-Dimensional, Laterally-Integrated

Dissolved Oxygen - Non-dimensional z axis)

TDLIDI (Two-Dimensional, Laterally-Integrated

Dissolved Oxygen - Dimensional z axis)

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I. INTRODUCTION

The computer programs outlined in this appendix are based on the laterally-averaged mass-transport equations as developed in the main body of this work. These programs have been written for an IBM 360/50 computer in Fortran IV H-level and at present (8/72) have been employed to study the conservative and dissolved oxygen-biochemical oxygen demand (D.O.-B.O.D.) systems. Indications are provided in Chapter A-V as to how this program can be extended to higher order reaction schemes . No attempt has been made to minimize computer time at the expense of program simplicity.

The programming approach used was specifically directed toward developing an accurate prediction model for the D.O.-B.O.D. system. Therefore the subroutine division of the program reflects this trend, with each routine performing a specific portion of the calculation for the D.O.-B.O.D. system

while the main program solves the finite-difference approximation of the basic mass-transport equation.

Both programs, non-dimensional z axis (TDLIDO) and dimensional z axis (TDLIDI) models will be presented in the following discussion, and indications will be made as appropriate to show how they differ in input, output and general operation.

II. ESTUARY MODEL

CONSERVATIVE SYSTEM

In order to check to assure that the boundary conditions and finite difference model were properly formulated, a conservative system option was built into the computer models. In addition this system can be used to study the movement of any conservative constituent in the estuary such as salinity, alkalinity, or chlorides.

D.O.-B.O.D. SYSTEM

One of the basic water quality descriptors is the dissolved oxygen system. Such a system involves two subsystems as shown in Fig. A-1:

(a.) Biochemical Oxygen Demand (B.O.D.)

-----System

(b.) Dissolved Oxygen (D.O.) System

These two systems combine to form a basic set

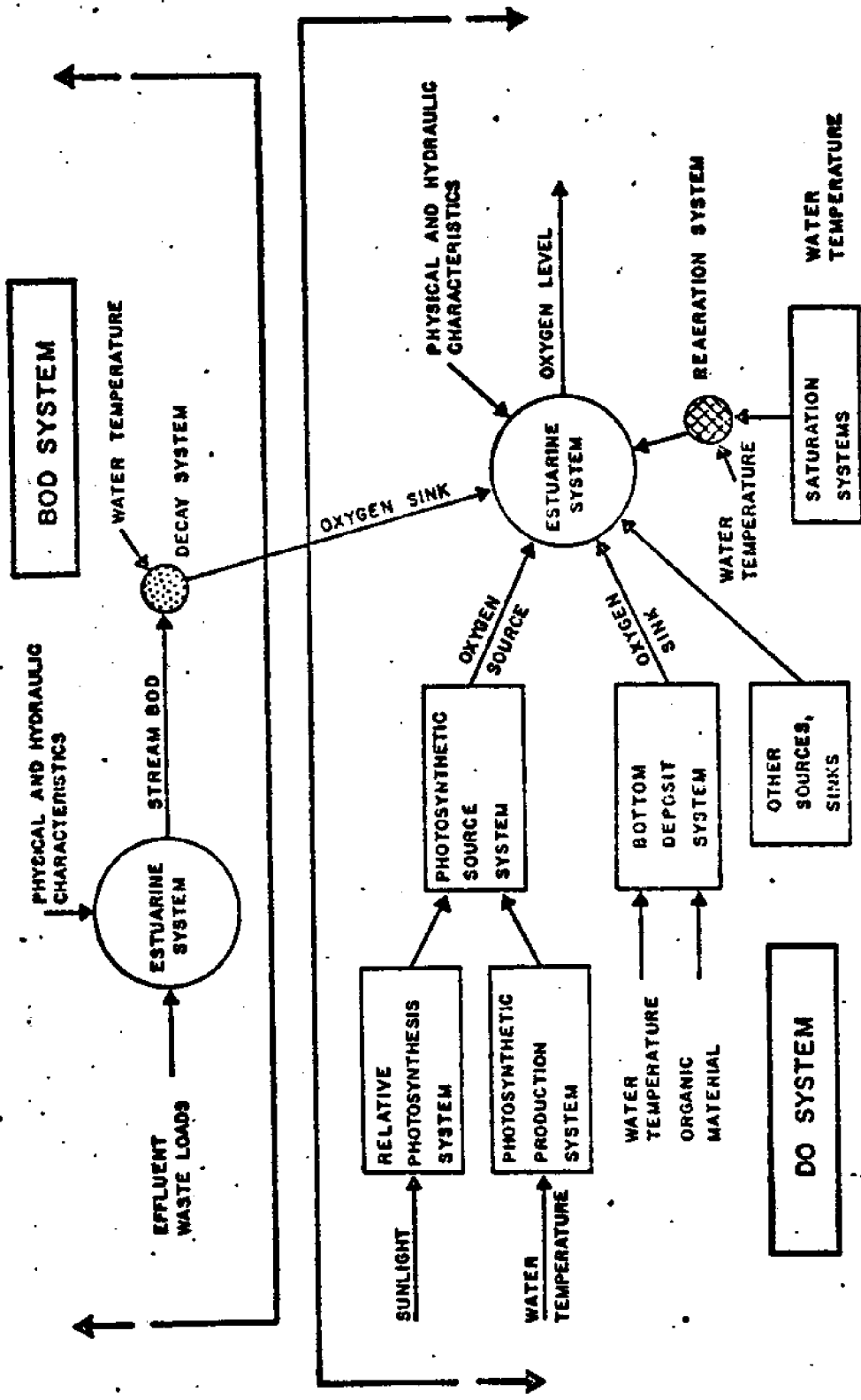


FIG. A-1 DISSOLVED OXYGEN SYSTEM

of two mass balance second order partial differential equations representing the two subsystems. In equation form they are given by

$$\frac{\partial L}{\partial t} = -u \frac{\partial L}{\partial x} - v \frac{\partial L}{\partial y} - w \frac{\partial L}{\partial z} + \frac{\partial}{\partial x} \left(e_x \frac{\partial L}{\partial x} \right) + \frac{\partial}{\partial y} \left(e_y \frac{\partial L}{\partial y} \right) +$$

$$\frac{\partial}{\partial z} \left(e_z \frac{\partial L}{\partial z} \right) - K_D L + J \quad (A1)$$

B.O.D. System

and

$$\frac{\partial c}{\partial t} = -u \frac{\partial c}{\partial x} - v \frac{\partial c}{\partial y} - w \frac{\partial c}{\partial z} + \frac{\partial}{\partial x} \left(e_x \frac{\partial c}{\partial x} \right) + \frac{\partial}{\partial y} \left(e_y \frac{\partial c}{\partial y} \right) +$$

$$\frac{\partial}{\partial z} \left(e_z \frac{\partial c}{\partial z} \right) + K_A (c_{SAT} - c) - K_D L + S_{DO}$$

(A2)

D.O. System

where

L - B.O.D. in mg/l

c - D.O. in mg/l

u, v, w - Tidal velocities in the x, y and z directions respectively

- e_x, e_y, e_z - Dispersion coefficients in the x, y, and z direction respectively
- J - Sources of B.O.D. in lbs./day
- K_D - B.O.D. decay coefficient
- K_A - D.O. reaeration coefficient
- c_{SAT} - Oxygen saturation value
- S_{DO} - Sources or sinks of D.O. in mg/l

The equations, after being laterally integrated, [Eqs. (A1) and (A2)] are employed to represent the D.O. - B.O.D. system in the computer models. It can be noted that only the carbonaceous B.O.D. has been modeled and the same is true for the decay coefficients in both the D.O. and B.O.D. equations. There has also been no direct account taken for the obvious biological activity present in the water column as well as benthic activities. Simple programming changes in both programs can be made to correct for these other effects if desired. There is, however, a general source-sink term in the oxygen balance equation which may be employed to simulate biological activities and their subsequent D.O. loadings.

The exact formulations of the various coefficients have been noted in the description of each subrou-

tine's function, leaving the possibility open of easily changing the formulations to suit particular estuarine environments.

III. PROGRAM OPERATION

DECK CONSTRUCTION

NABS-TDLIDO and TDLIDI programs were specifically designed for an IBM 360/50 computer in use at the University of Rhode Island, Kingston, Rhode Island. They were written in Fortran IV, Level H. There are, however, no special system subroutines used in the programs other than the normal exponential, sine, and absolute value types and therefore, the program should be adaptable to any computer that has a sufficiently large core available (about 256K for 16 x 50 arrays) and accepts Fortran IV, Level H as a programming language. A typical deck make up is shown in Fig. A-2.

In the preceding discussion a list of the control cards as described in Fig. A-2 will be presented along with an explanation of how they are to be completed.

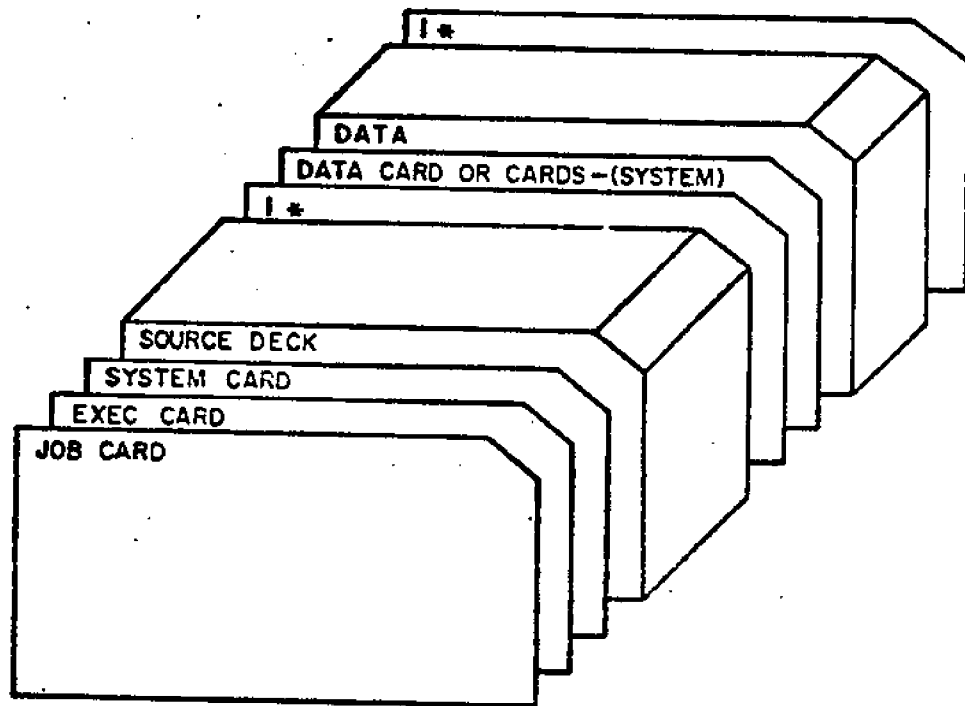


FIG. A-2 TYPICAL IBM 360/50 DECK MAKEUP

(a) The first card submitted of any deck must be a job card ('b' - denotes a blank card column)

<u>Card Columns</u>	<u>Required Information</u>
1 to 2	//
3 to 10	Registration code of user
11 to 15	b JOB b
16	(
17 to 26	Registered sponsor account code
27	,
28 to 30	estimated job time in minutes
31	,
32 to 34	estimated job line output in thousands
35	,
36 to 38	estimated card punched output
39)
40	,
41 to 71	users name, MSGLEVEL = 1

EXAMPLE:

//TDLIDO b JØB b (INØ100.010.010,250), SPAULDING,

MSGLEVEL = 1

(b) The second card is the system execution card.

```
//bEXECbFØRTHCLG' PARM.FORT = 'OPT=2'
```

(c) The third card is a system card. Since only FORTRAN is used in this program, the card must be punched

```
//FØRT.SYSINbDDb *
```

(d) The next group of cards consists of the program cards (i.e. the source deck). If an object deck is used the system control cards under (b), (c), and (f) must be changed accordingly.

(e) Following the source deck is an end card containing the following symbols

```
/ *
```

(f) The data control card indicates that the data is to follow. The format for this card is

```
//GØ.SYSINbDDb*
```

(g) All data is included in the next section and an outline is presented in the section on data input requirements as to the format of this data.

(h) Following the data deck is the end card of the format:

/*

If data of velocity fields or time varying water quality boundary conditions is to be read from a disc data file then the appropriate job control language (JCL) cards should be inserted at the end of the source deck to define the file name and other pertinent system information.

GRID SELECTION AND BOUNDARY VALUES

To set up a computation in a certain area, geographic information has to be transferred onto the grid points of the staggered grid system. It also must be decided what portion of the estuary or

estuary-river system are to be modeled. This criteria will in part be determined by the size of computer storage available and also by the expense of computer time. In order to see how a typical estuary grid system should be arranged we will consider an example for the dimensional case first.

Consider a typical Bay as shown in Fig. A-3. We wish to model this estuary from its mouth at the open ocean or sound to the head in the river. As a first step the maximum estuary depth and length from head to mouth are determined. With these dimensions the overall size or area to be modeled is found.

The next step is to formulate the size of the estuary grids in both the x (longitudinal) and z (vertical) directions. Care should be taken to assure that an intelligent choice is made between a fine grid size requiring large amounts of computer memory and time with subsequently good spatial resolution and a coarse grid system requiring considerably less

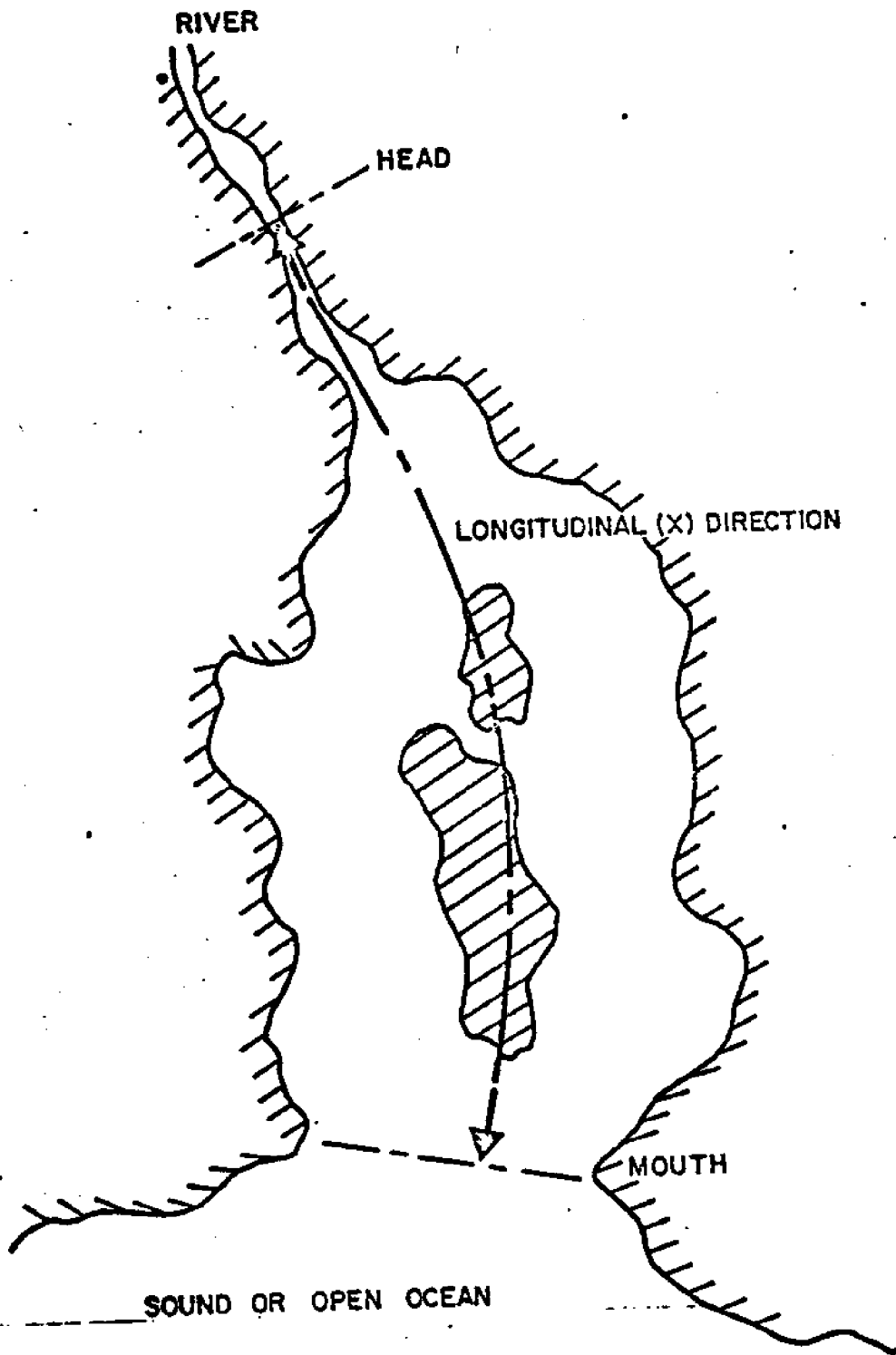


FIG. A-3 TYPICAL ESTUARY

computer memory and time but with poorer spatial resolution. Also in most estuaries the length is very much greater than the maximum depth so that the grid sizes are much smaller in the z direction than in the x direction leading to long thin grids which must be noted when viewing program output.

Let us assume that for our typical estuary the length from head to mouth is 5 nm. and the maximum depth is 20 ft. It is to be noted that the length measurement should be taken along a line that approximately represents the mean longitudinal tidal motion as shown by the dotted line in Fig. A-3. This procedure is used to help assure that the laterally-averaged approximation is as realistically represented for the actual application as possible. If the length were taken as a straight geographical distance large cross stream currents would be neglected due to the orientation of the x axis. Assuming a 3038 ft. (1/2 nm) grid size in the x direction and a 5 ft.

grid spacing in the z direction would mean a grid array $N=4$, $M=10$, where N is the number of vertical grids and M is the number of longitudinal grids.

However, due to computational considerations for boundary conditions, both open and closed, there must be at least one more grid space on all sides of the computational field. Hence for this particular problem, the grid array size must be $N=6$, $M=12$. In the computer program this grid array size is denoted as $NMAX$ and $MMAX$, i.e. where $N=1, NMAX$, and $M=1, MMAX$.

Another rule required by the finite-difference computational scheme is that there must be at least 2 grid squares in any direction. This allows the mass densities to change in both directions and prevents mass densities from being fixed artificially due to a computational inadequacy. As a review then, the computational scheme requires

- (1) At least one grid space on all sides beyond those required for actual

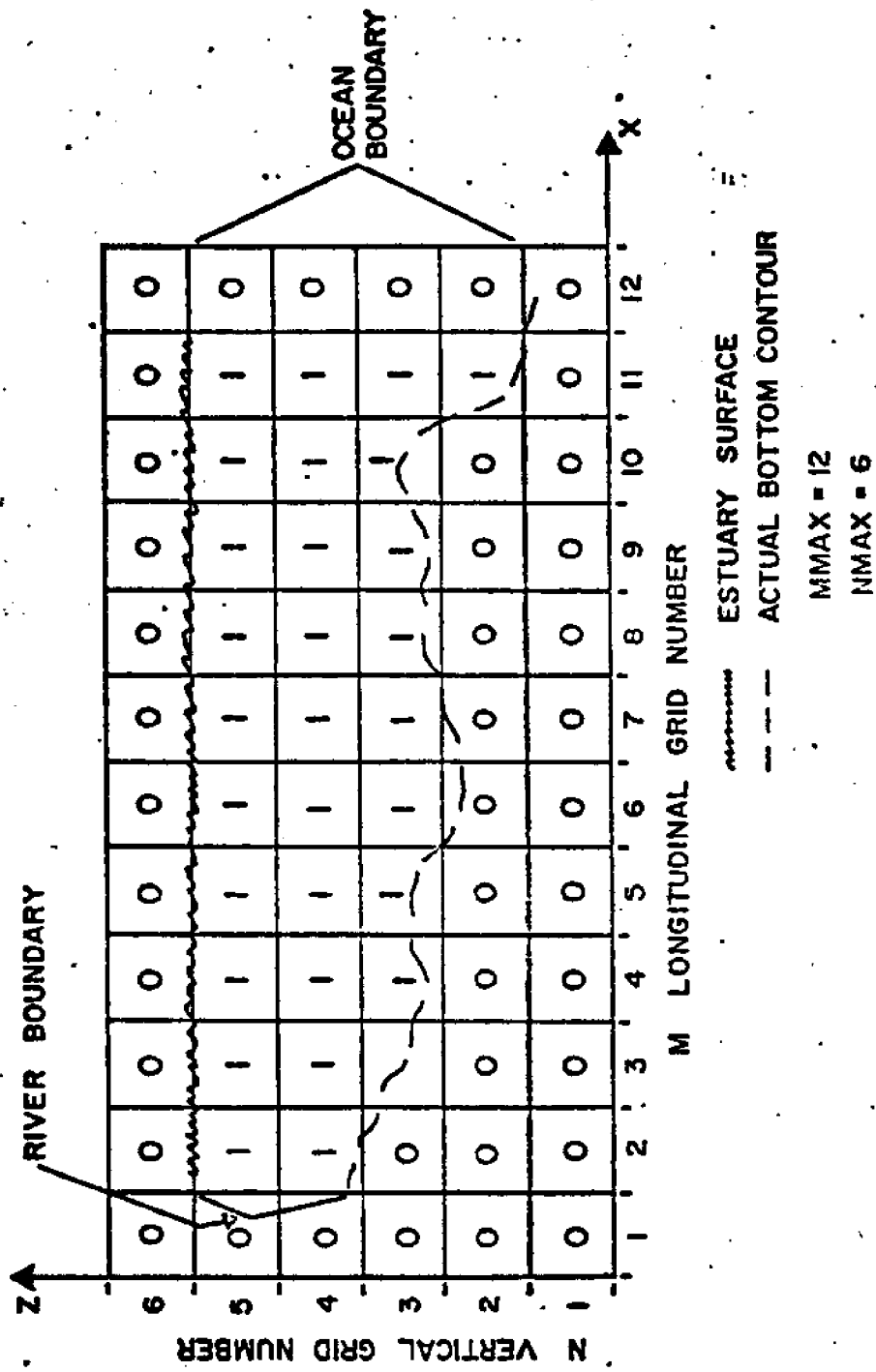


FIG. A-4 ESTUARY GRID COMPUTATIONAL FIELD FOR A TYPICAL DIMENSIONAL VERTICAL AXIS MODEL APPLICATION

estuary representation.

- (2) At least two computational grids in any direction.

To represent this information for computer programming purposes a computational grid field or array called $H(N,M)$ is formulated as shown in Fig. A-4. The locations where a one (1) appears indicate grids in which computations are to be performed and a zero (0) or default indicate that no computation is to be performed. Information on how these data are provided to the program is given in the Data Input section.

Throughout this discussion no reference has been made to the obvious fact that the sea level is not constant but varies according to the tidal stage. This variation in height from the mean sea level has been assumed small for the dimensional z axis model in comparison to the accuracy of estuary depths as computed from the computational grid field approximation. Cases of larger tidal variations can be handled only by the non-dimensional z axis model.

The next problem to be dealt with is that there are open boundary conditions at the river and ocean outlets to the estuary. To indicate for computational purposes where these outlets or open boundaries occur use is made of open boundary value control numbers $M\emptyset BD()$ and $N\emptyset BD()$, where each $M\emptyset BD$ value represents an open boundary on a given line M and each $N\emptyset BD()$ value represents an open boundary on a line N .

As an example let us develop the $M\emptyset BD$ and $N\emptyset BD$ values for the grid system shown in Fig. A-4. A visual check shows that no open boundaries occur along any line N and therefore there are no $N\emptyset BD$ values ($NBC=0$ where NBC is the number of $N\emptyset BD$ values); however, along lines $M=1$ and $M=12$ we have open boundary conditions. Since there are two open boundaries $MBC=2$, where MBC is the number of open boundaries along line M .

In formulating these boundary control values the first two numbers represent the M number of the open boundary. The second two digits repre-

sent the lower N number of the boundary, the third two numbers indicate the upper N number of the boundary and the last number gives an indication as to the position in the computational field of the bound. If the open bound is on the right or upper side of the grid where $M=M_{MAX}$, or $N=N_{MAX}$ then a value of one is chosen; if the open bound is on the left or lower side wher $M=1$ or near $N=1$, zero is used. For this example (Fig. A-4) then the $M\emptyset BD()$ values are

$$M\emptyset BD(1) = 01/04/05/0$$

and

$$M\emptyset BD(2) = 12/02/05/1$$

$$\text{then } MBC = 2$$

and the $N\emptyset BD()$ values are unneeded therefore

$$NBC = 0$$

If it is decided that open boundaries should be placed on any line N a similar procudeure to that shown above can be employed, with an analogous interpretation of the control numbers. For example, suppose that we decide to have one open boundary on line $N=2$, in grids $M = 4$ and 5 ,

then NBC = 1

NØBD = 02/04/05/0

A troublesome question concerning open boundaries is what can be done when other river flows or runoff water enter the estuary that cannot be adequately included as shown in Fig. A-4. If the entrance of this "side" flow is large enough in comparison to the volume of the water in the laterally averaged grid immediately adjacent to it then the mass density of a given constituent in that grid can be preset to an appropriate value to reflect this inflow. In general, however, this is not the case since the inflow volumes are usually considerably smaller than the volume of the estuary grid. Handling of this case is very difficult and has to be adjusted for each water quality parameter under study. As a typical example to simulate the B.O.D. loading produced by runoff water, the volume of storm water being deposited in the estuary would be converted into a B.O.D. loading in lbs./day and injected into appropriate grids along the

estuary surface.

The grid selection for the non-dimensional z axis model of the laterally-averaged mass-transport equation is considerably simpler than that for the dimensional model. After determining the size of the x grid spacing one has only to decide the maximum number of vertical grids desired for the total area being modeled. The active computational grid field $H(N,M)$ then becomes a rectangle. For the case outlined in Fig. A-4 assume that we desire to have 4 vertical grids then our grid computational field appears as a rectangle with ("1's") in spaces $N = 2,5$; and $M = 2,11$.

To account for the depth variation in each section another set of data input to the program giving the section depth at each grid location $M = 1, MMAX$ is required. This depth should correspond to the approximate mean sea level depth of the section.

The open boundary conditions for the river and ocean boundaries as shown in Fig. A-4 now become

MØBD(1) = 01/02/05/1 river

and

MØBD(2) = 12/02/05/1 ocean

It is seen that these values, in their ranges of N(02/05) are exactly the same, however, depth variations adjust this seemingly unrealistic grid approximation.

DATA INPUT REQUIREMENTS

In an effort to make data input for NABS-TDLIDO and TDLIDI as simple as possible Table A-1 has been developed which lists the data name, a general description including appropriate dimensions (i.e. ft., ft./sec, mg/l, etc.), the format for data cards, and any conditions that must be met for their use.

When searching for the information to fill these data fields especially in the cases of those specified on the staggered grid system an effort

should be made to find the values at those locations as this will give the most accurate representation of the area under study. This is particularly true for the estuary width matrix since the solution scheme for the difference equations is sensitive to width variations. For cases where islands are found in the middle of an estuary, the islands, conceptually, are moved against one shore and a new cross sectional bottom profile is estimated using either a mean or maximum depth as a reference and a bottom profile similar to the previous estuary section. Interpretation of model results has to be viewed carefully in light of this new profile adjustment.

Since these computer program models are only for the mass transport equation, values of the tidal velocity variations need to be predicted by other means. Provisions have been made in subroutine VELC to handle velocity inputs. Either the fields of the w and u velocities

can be specified at every half time step, an interval of $AT/2$ apart, or they can be computed from a Fourier series type formula based on experimental data or in the usual case a reliable one-dimensional tidal model (1) can be used to predict the tidal velocities and heights in the x direction and w velocities can be initially neglected since they are usually small. In any case, with some simple programming, subroutine VELC can be used to handle a variety of velocity input conditions.

To specify mass densities at open boundaries another subroutine called BOVAL is employed. At the present, since water quality data gathering is usually done in terms of season averages rather than instantaneous values, the mass densities at open boundaries are set constant. The program however can handle varying boundary conditions if so desired by simply adjusting the programming to read or calculate these conditions.

Additional information on how these velocity and mass density inputs are handles is described under the subroutine functional description for the appropriate routine.

In general to obtain the D.O.-B.O.D. coupled system from the computer program the control number ISALT is set equal to one (ISALT = 1), while for the conservative case, ISALT > 1. Careful checking of the data input conditions reveals which read statements are passed over or skipped for each case. Similar type control parameters are used for dispersion terms (IDIF), sources and sinks (ISOU), decay values (IDEC), and velocity input (IVEL) conditions and are noted accordingly in Table A-1.

Since the development of both the dimensionless and dimensional z axis models is analogous the data inputs to both models are very similar and differences are only in a few parameters. Therefore, Table A-1 will present the data input for the dimensional model with notations made under the conditions column, for variations caused by using the non-dimensional z axis model.

DESCRIPTION DATA NAME	FORMAT	CONDITIONS	NO. OF CARDS
AT- full time step for difference equation in sec.	F8.3		1
MAXST - total number of time steps to be completed	I3		1
NMAX,MMAX - the number of grids in the z and x directions	2I2		1
DDX,DDZ - x and z direction grid sizes in ft.	2F7.2	DDZ omitted for dimen- sionless model	1
IPUNCH - number of time steps at which punched output is desired	I3		1
NPR - total number of times printed output is desired			
NPRINT () - the time steps at which printed output is desired	I4		NPR
NFP - number of grids for which time varying plots of concentration are desired	I2		1

Table A-1 Data Input Specifications

DATA NAME DESCRIPTION	FORMAT	CONDITIONS	NO. OF CARDS
NP(I),MP(I) the N, and M numbers for grids in which time varying plots of concentration are desired	2I2		NFP
IGL,IGU - plots of D.O. & B.O.D. or conservative case are provided for column N=IGL to column N = IGU, plus vertically averaged values in each section	2I2	If IGL or IGU equal 0 only obtain vertical section averages	1
ISOU, IDIF, ISALT, IDEC, IVEL, ISMO - control parameters	5I2	ISOU- source of D.O. IDIF- diffusion coeff. ISALT- D.O. - B.O.D. or conservative case IDEC- Decay coefficient IVEL- velocity read in ISMO- width matrix smoothing	1
NBC, MBC - number of NOBD boundary conditions number of MOBD boundary conditions	2I2	IF NBC, MBC equals zero skips appropriate boundary conditions	1

Table A-1 Data Input Specifications (Cont'd.)

DATA NAME DESCRIPTION	FORMAT	CONDITIONS	NO. OF CARDS
NOBD () boundary conditions	I8	If NBC equals zero this read is passed over	NBC
MOBD () boundary conditions	I8	If MBC equals zero this read is passed over	MBC
A2,B2,SKK,V1 values for the computation of the decay coef- ficient (ref. sub- routine DECAY)	2F10. 4,F5.2, F6.1	If IDEC=1 these values are read and next read sk- ipped	1
DA,DB,DC,DE	4F15.8	If IDEC > 1 these values are read and pre- vious state- ment is skipped	1
SNETA,BET1,GAMS coefficients of the vertical dis- persion coef- ficient (ref. sub- routine DIFFU)	3F10.5	GAMS = 0.0 no wind cond- ition, BET1 = 0 constant den- sity profile	1
WH,WT,WL - wave - height (ft) wave period (sec) wave length (ft) employed in vertical dispersion coeffic- ient (ref. subroutine DIFFU)	3F10.5	WH,WT,WL must always be sp- ecified even if GAMS = 0.0 above	1

Table A-1 Data Input Specifications (Cont'd.)

DATA NAME DESCRIPTION	FORMAT	CONDITIONS	NO. OF CARDS
H(N,M) - Computational grid field	30I2		MMAX
B(N,M) - estuary width field in ft. (columns 1-10)	10F8.1		MMAX
B(N,M) - estuary width field in ft. (columns 11 to NMAX)	10F8.1		MMAX
JS(N,M) - estuary B.O.D. loadings in lbs/day (columns 1-10)	10F7.1	If ISALT > 1 passes over this read	MMAX
JS(N,M) - estuary B.O.D. loadings in lbs/day (columns 11- NMAX)	10F7.1	If ISALT > 1 skips this read	MMAX
DX(N,M) - x direction dispersion coefficient in ft ² /sec (columns 1-10)	10F5.2	If IDIF > 1 skips this read	MMAX
DX(N,M) - x direction dispersion coefficient in ft ² /sec (columns 11-NMAX)	10F5.2	If IDIF > 1 skips this read	MMAX
DZ(N,M) -vertical dis- persion coefficient in ft ² /sec. (columns 1-10)	10F5.2	If IDIF > 1 skips this read	MMAX
DZ(N,M) -vertical dis- persion coefficient in ft ² /sec (columns 11-NMAX)	10F5.2	If IDIF > 1 skips this read	MMAX

Table A-1 Data Input Specifications (Cont'd)

DATA NAME DESCRIPTION	FORMAT	CONDITIONS	NO. OF CARDS
COP(N,M) - initial value of D.O. or salinity mg/l (columns 1-10)	10F5.2		MMAX
COP(N,M) - initial value of D.O. or salinity mg/l (columns 11-NMAX)	10F5.2		MMAX
LS(N,M) - initial value value of B.O.D. in mg/l (columns 1-10)	10F5.2	If ISALT > 1 skips this read	MMAX
LS(N,M) - initial value of B.O.D. in mg/l (columns 11-NMAX)	10F5.2	If ISALT > 1 skips this read	MMAX
P(N,M) - source or sink of dissolved oxygen (mg/l) (columns 11-NMAX)	10F6.2	If ISCU > 1 skips this read, presets field to zero	MMAX
TS(N,M) temperature of water in (°F) (columns 1-10)	10F6.2		MMAX
TS(N,M) temperature of water in (°F) (columns 11-NMAX)	10F6.2		MMAX
SS(N,M) - salinity in estuary (columns 1-10)	10F6.2	Omitted if ISALT > 1	MMAX
SS(N,M) - salinity in estuary (columns 11-NMAX)	10F6.2		MMAX
DEP - mean sea level depth in ft.	F7.2	Used only for dimen- sionless model	MMAX

Table A-1 Data Input Specifications (Cont'd)

DATA NAME	FORMAT	CONDITIONS	NO. OF CARDS
DESCRIPTION			
U(N,M) -u velocity (+ ebb) ft/sec (columns 1-10)	10F6.2	IVEL must equal 1 to read this	MMAX
U(N,M) - u velocity (+ ebb) ft/sec (columns 11-NMAX)	10F6.2	IVEL must equal 1 to read this	MMAX
W(N,M) - w velocity (+ upward) ft/sec (columns 1-10)	10F6.2	IVEL must equal 1 to read this	MMAX
W(N,M) - w velocity (+ upward) ft/sec. (columns 11-NMAX)	10F6.2	IVEL must equal 1 to read this	MMAX

-Table A-1 Data Input Specifications (Cont'd)

COMMON AND DIMENSION STATEMENTS

When the final grid system has been decided upon, along with all the boundary specifications, the ~~COMMON~~ and ~~DIMENSION~~ statements of the program should be adjusted so as to require as little computer memory as is feasible. To help in this matter a table has been developed which shows the appropriate minimum storage allocations necessary. In Table A-2 the following notations are used:

- MMAX - Number of grid points in the x
direction
- NMAX - Number of grid points in the z
direction
- NBC - Number of NØBD boundary values
- MBC - Number of MØBD boundary values
- NFP - Number of grids for which time
varying concentrations are to
be plotted

COMMON BLOCK

ARRAY NAME	CONDITIONS	DIMENSIONS
NBD ()		1.5* MMAX
MBD ()		1.5* MMAX
NOBD ()		NBC + 1
MOBD ()		MBC + 1
AR ()		MMAX
DEP ()		MMAX
CS ()		MMAX
TS (,)		NMAX, MMAX
SS (,)		NMAX, MMAX
P (,)		NMAX, MMAX
CO (,)		NMAX, MMAX
LS (,)		NMAX, MMAX
JS (,)		NMAX, MMAX
H (,)		NMAX, MMAX
CT (,)		NMAX, MMAX
U (,)		NMAX, MMAX
W (,)		NMAX, MMAX
COP (,)		NMAX, MMAX

Table A-2 Storage Allocation Specification

COMMON BLOCK

<u>ARRAY NAME</u>	<u>CONDITIONS</u>	<u>DIMENSIONS</u>
D (,)		NMAX, MMAX
DX (,)		NMAX, MMAX
DZ (,)		NMAX, MMAX
B (,)		NMAX, MMAX
RAR(,)		NMAX, MMAX
CSC(,)		NMAX, MMAX
SE()	Unnecessary for dimension- al model	MMAX
SEP()	Unnecessary for dimension- al model	MMAX

Table A-2 Storage Allocation Specification (Cont'd.)

MAIN PROGRAM

ARRAY NAME	DIMENSIONS
AA ()	M MAX
BB ()	M MAX
CC ()	M MAX
DD ()	M MAX
AA2 ()	M MAX
BB2 ()	M MAX
CC2 ()	M MAX
DD2 ()	M MAX
E ()	M MAX
Q ()	M MAX
NPRINT ()	2 *M MAX

SUBROUTINE INIT

ARRAY NAME	DIMENSIONS
NU ()	N MAX

Table A-2 Storage Allocation Specification (Cont'd)

DIMENSION STATEMENTS

SUBROUTINE ANSW

<u>ARRAY NAME</u>	<u>DIMENSIONS</u>
NO ()	NMAX

SUBROUTINE PLOTS

<u>ARRAY NAME</u>	<u>DIMENSIONS</u>
A (,)	MMAX, 3
COAV ()	MMAX
LSAV ()	MMAX

SUBROUTINE AXVAL

<u>ARRAY NAME</u>	<u>DIMENSIONS</u>
NO ()	NMAX

Table A-2 Storage Allocation Specification (Cont'd)

NAMED COMMONS

/TIMV/

<u>ARRAY NAME</u>	<u>DIMENSION</u>
CODO (,)	MAXST, NFP
BOD (,)	MAXST, NFP
TIH (,)	MAXST, NFP
NP ()	NFP
MP ()	NFP

/CHEZY/

<u>ARRAY NAME</u>	<u>DIMENSION</u>
C ()	MMAX

Table A-2 Storage Allocation Specification (Cont'd.)

PROGRAM INPUT

Conservative Case

TDLIDI

D.O. - B.O.D. System

Conservative Case

TDLIDO

D.O. - B.O.D. System

SAMPLE INPUT - TDLIDI
(DIMENSIONAL VERTICAL AXIS MODEL)
CONSERVATIVE CASE

SAMPLE INPUT - TDLIDI

(DIMENSIONAL VERTICAL AXIS MODEL)

D.O. - B.O.D. CASE

25890.	25891.	25892.	25893.	25894.	25895.	25896.	25897.	25898.	25899.
26110.	26111.	26112.	26113.	26114.	26115.	26116.	26117.	26118.	26119.
21030.	21031.	21032.	21033.	21034.	21035.	21036.	21037.	21038.	21039.
20190.	20191.	20192.	20193.	20194.	20195.	20196.	20197.	20198.	20199.
17460.	17461.	17462.	17463.	17464.	17465.	17466.	17467.	17468.	17469.
17100.	17101.	17102.	17103.	17104.	17105.	17106.	17107.	17108.	17109.
21000.	21001.	21002.	21003.	21004.	21005.	21006.	21007.	21008.	21009.
14700.	14701.	14702.	14703.	14704.	14705.	14706.	14707.	14708.	14709.
21600.	21601.	21602.	21603.	21604.	21605.	21606.	21607.	21608.	21609.
9900.	9901.	9902.	9903.	9904.	9905.	9906.	9907.	9908.	9909.
16500.	16501.	16502.	16503.	16504.	16505.	16506.	16507.	16508.	16509.
14700.	14701.	14702.	14703.	14704.	14705.	14706.	14707.	14708.	14709.
1000.	1001.	1002.	1003.	1004.	1005.	1006.	1007.	1008.	1009.
1590.	1591.	1592.	1593.	1594.	1595.	1596.	1597.	1598.	1599.
1200.	1201.	1202.	1203.	1204.	1205.	1206.	1207.	1208.	1209.
660.	661.	662.	663.	664.	665.	666.	667.	668.	669.
360.	361.	362.	363.	364.	365.	366.	367.	368.	369.
3000.	3001.	3002.	3003.	3004.	3005.	3006.	3007.	3008.	3009.
2250.	2251.	2252.	2253.	2254.	2255.	2256.	2257.	2258.	2259.
1800.	1801.	1802.	1803.	1804.	1805.	1806.	1807.	1808.	1809.
4740.	4741.	4742.	4743.	4744.	4745.	4746.	4747.	4748.	4749.
5880.	5881.	5882.	5883.	5884.	5885.	5886.	5887.	5888.	5889.
4500.	4501.	4502.	4503.	4504.	4505.	4506.	4507.	4508.	4509.
6310.	6311.	6312.	6313.	6314.	6315.	6316.	6317.	6318.	6319.
5400.	5401.	5402.	5403.	5404.	5405.	5406.	5407.	5408.	5409.
5250.	5251.	5252.	5253.	5254.	5255.	5256.	5257.	5258.	5259.
6190.	6191.	6192.	6193.	6194.	6195.	6196.	6197.	6198.	6199.
5580.	5581.	5582.	5583.	5584.	5585.	5586.	5587.	5588.	5589.
17100.	17101.	17102.	17103.	17104.	17105.	17106.	17107.	17108.	17109.
18000.	18001.	18002.	18003.	18004.	18005.	18006.	18007.	18008.	18009.
20100.	20101.	20102.	20103.	20104.	20105.	20106.	20107.	20108.	20109.
19080.	19081.	19082.	19083.	19084.	19085.	19086.	19087.	19088.	19089.
20490.	20491.	20492.	20493.	20494.	20495.	20496.	20497.	20498.	20499.
35790.	35791.	35792.	35793.	35794.	35795.	35796.	35797.	35798.	35799.
34800.	34801.	34802.	34803.	34804.	34805.	34806.	34807.	34808.	34809.
29400.	29401.	29402.	29403.	29404.	29405.	29406.	29407.	29408.	29409.
31500.	31501.	31502.	31503.	31504.	31505.	31506.	31507.	31508.	31509.
33000.	33001.	33002.	33003.	33004.	33005.	33006.	33007.	33008.	33009.
35400.	35401.	35402.	35403.	35404.	35405.	35406.	35407.	35408.	35409.
31290.	31291.	31292.	31293.	31294.	31295.	31296.	31297.	31298.	31299.
29640.	29641.	29642.	29643.	29644.	29645.	29646.	29647.	29648.	29649.
30480.	30481.	30482.	30483.	30484.	30485.	30486.	30487.	30488.	30489.
26490.	26491.	26492.	26493.	26494.	26495.	26496.	26497.	26498.	26499.
24010.	24011.	24012.	24013.	24014.	24015.	24016.	24017.	24018.	24019.
34200.	34201.	34202.	34203.	34204.	34205.	34206.	34207.	34208.	34209.
41400.	41401.	41402.	41403.	41404.	41405.	41406.	41407.	41408.	41409.
35400.	35401.	35402.	35403.	35404.	35405.	35406.	35407.	35408.	35409.
28110.	28111.	28112.	28113.	28114.	28115.	28116.	28117.	28118.	28119.
25990.	25991.	25992.	25993.	25994.	25995.	25996.	25997.	25998.	25999.
26110.	26111.	26112.	26113.	26114.	26115.	26116.	26117.	26118.	26119.
21030.	21031.	21032.	21033.	21034.	21035.	21036.	21037.	21038.	21039.
21090.	21091.	21092.	21093.	21094.	21095.	21096.	21097.	21098.	21099.

32.7	31.7	31.0	32.2	32.3	0.0
32.3	32.5	32.3	32.5	32.3	0.0
32.9	32.7	32.6	32.5	32.4	0.0
32.9	32.7	32.6	32.5	32.4	0.0
32.4	32.3	32.3	32.2	32.3	0.0
32.5	32.4	32.4	32.3	32.3	0.0
32.5	32.5	32.4	32.3	32.2	0.0
32.5	32.4	32.4	32.3	32.2	0.0
32.5	32.4	32.4	32.3	32.2	0.0
32.4	32.3	32.2	32.2	32.1	0.0
32.2	32.2	32.7	32.7	32.9	0.0
33.0	33.0	33.0	32.9	32.8	0.0
33.0	33.0	33.0	33.0	33.0	0.0
33.1	33.0	33.0	33.0	33.0	0.0
33.1	33.0	33.0	32.9	32.9	0.0
33.1	33.0	33.0	33.0	33.0	0.0
33.1	33.0	33.0	33.0	33.0	0.0
33.1	33.0	33.0	33.0	33.0	0.0
33.1	33.0	33.0	33.0	33.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0

SAMPLE INPUT - TDLIDO
(DIMENSIONLESS VERTICAL AXIS MODEL)
CONSERVATIVE CASE

17.1
13.8
17.1
22.0
19.8
17.8
18.7
21.3
23.6
19.6
19.2
20.5
17.4
24.4
25.2
24.0
27.8
33.0
32.9
31.9
33.8
33.5
31.4
31.4
36.2
37.4
36.7
41.9
45.6
46.5
45.0
44.8
44.9
48.3
59.7
54.5
67.4
62.3
65.5

SAMPLE INPUT

FOR

TDLIDO

(DIMENSIONLESS VERTICAL AXIS MODEL)

SAMPLE INPUT - TDLIDO
(DIMENSIONLESS VERTICAL AXIS MODEL)
D.O. - B.O.D. CASE

0.0	32.6	32.6	32.5	32.4	32.3	32.2	31.7	31.6	31.2
0.0	32.6	32.6	32.5	32.5	32.4	32.3	31.9	31.6	31.5
0.0	32.7	32.6	32.6	32.5	32.4	32.3	32.1	31.7	31.6
0.0	32.7	32.7	32.7	32.6	32.5	32.4	32.2	31.9	31.7
0.0	32.8	32.8	32.7	32.6	32.5	32.4	32.3	32.0	31.8
0.0	32.8	32.8	32.7	32.6	32.5	32.4	32.3	32.1	31.9
0.0	32.8	32.8	32.7	32.6	32.5	32.4	32.4	32.2	31.9
0.0	32.8	32.8	32.8	32.7	32.6	32.4	32.4	32.3	32.0
0.0	32.9	32.9	32.8	32.8	32.7	32.5	32.4	32.3	32.1
0.0	32.9	32.9	32.9	32.8	32.8	32.7	32.5	32.4	32.2
0.0	33.0	32.9	32.9	32.8	32.8	32.7	32.6	32.5	32.4
0.0	33.0	33.0	33.0	32.9	32.8	32.7	32.5	32.5	32.4
0.0	33.0	33.0	33.0	33.0	32.9	32.8	32.7	32.6	32.5
0.0	33.0	33.0	33.0	33.0	33.0	32.9	32.9	32.7	32.6
0.0	33.1	33.0	33.0	33.0	33.0	33.0	32.9	32.8	32.7
0.0	33.1	33.1	33.1	33.0	33.0	33.0	33.0	32.9	32.8
0.0	33.1	33.1	33.1	33.1	33.1	33.0	33.0	33.0	32.8
0.0	33.1	33.1	33.1	33.1	33.1	33.0	33.0	33.0	32.9
0.0	33.2	33.2	33.1	33.1	33.1	33.1	33.1	33.1	33.0
0.0	33.2	33.2	33.2	33.2	33.1	33.1	33.1	33.1	33.1
0.0	33.3	33.3	33.3	33.3	33.2	33.2	33.2	33.2	33.1
0.0	33.3	33.3	33.3	33.3	33.2	33.2	33.2	33.2	33.2
0.0	33.3	33.3	33.3	33.3	33.2	33.2	33.2	33.2	33.2
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
27.5	27.4	27.3	27.3	27.2	0.0				
27.5	27.5	27.4	27.3	27.3	0.0				
27.6	27.5	27.5	27.4	27.3	0.0				
27.7	27.6	27.6	27.5	27.4	0.0				
27.8	27.7	27.7	27.6	27.5	0.0				
28.0	27.9	27.8	27.7	27.6	0.0				
28.3	28.0	28.0	27.9	27.8	0.0				
28.5	28.3	28.2	28.1	28.1	0.0				
28.7	28.5	28.3	28.2	28.2	0.0				
28.9	28.7	28.5	28.4	28.3	0.0				
29.0	28.9	28.7	28.6	28.5	0.0				
29.1	29.0	28.8	28.7	28.6	0.0				
29.2	29.0	28.9	28.8	28.8	0.0				
29.4	29.3	29.0	29.0	28.9	0.0				
29.6	29.5	29.2	29.2	29.0	0.0				
29.8	29.6	29.4	29.3	29.2	0.0				
30.0	29.7	29.6	29.4	29.4	0.0				
30.2	29.8	29.6	29.5	29.5	0.0				
30.4	30.0	29.9	29.7	29.6	0.0				
30.6	30.2	30.1	29.9	29.7	0.0				
30.9	30.3	30.2	30.0	29.9	0.0				
31.0	30.5	30.3	30.2	30.1	0.0				
31.0	30.5	30.3	30.2	30.2	0.0				
31.0	30.9	30.7	30.4	30.3	0.0				
31.1	31.0	30.9	30.7	30.6	0.0				
31.3	31.0	31.0	30.8	30.7	0.0				
31.6	31.3	31.0	31.0	30.8	0.0				

31.7	31.5	31.1	31.0	31.0	0.0
31.7	31.4	31.2	31.0	31.0	0.0
31.8	31.5	31.3	31.2	31.2	0.0
31.8	31.6	31.5	31.4	31.3	0.0
32.0	31.8	31.7	31.6	31.5	0.0
32.1	31.7	31.8	31.7	31.6	0.0
32.2	32.0	31.9	31.8	31.7	0.0
32.2	32.1	32.0	31.9	31.8	0.0
32.4	32.3	32.2	32.0	31.9	0.0
32.5	32.4	32.3	32.2	32.0	0.0
32.6	32.5	32.4	32.3	32.2	0.0
32.7	32.6	32.5	32.5	32.4	0.0
32.7	32.6	32.5	32.5	32.4	0.0
32.8	32.7	32.7	32.7	32.6	0.0
32.9	32.9	32.8	32.8	32.8	0.0
33.0	33.0	33.0	32.9	32.9	0.0
33.1	33.1	33.1	33.0	33.0	0.0
33.2	33.1	33.1	33.1	33.1	0.0
33.2	33.1	33.1	33.1	33.1	0.0
0.0	0.0	0.0	0.0	0.0	0.0

6.58
6.57
6.55
19.53
19.52
22.0
19.48
22.57
18.12
17.10
13.75
17.07
22.05
19.8
17.78
18.67
21.32
22.13
19.57
19.2
20.5
17.41
24.36
26.2
24.0
27.77
32.85
32.93
31.93
33.83
33.5
31.37

31.36
36.22
37.42
36.7
41.86
45.63
46.45
45.08
44.79
44.77
48.31
59.7
54.45
67.43
62.0
65.0

OUTLINE OF PROGRAM COMPUTATIONS

The following description, in logical step form, gives an indication of the computational flow of NABS-TDLIDO or TDLIDI. Indications will be made where needed to show how the flow differs for conservative (salinity) and non-conservative (D.O. - B.O.D.) water quality indicators. This outline, in no manner, is meant to represent a comprehensive flow chart for the program, but provides a useful procedural insight to its operation. More complete indications of each subroutines function is indicated in that section.

- (1) The initial heading (NABS-DO-BOD) is printed
- (2) The initial data fields with dimension (NMAX,MMAX) are preset to 0.0
- (3) The data as noted in the data requirements section is read (except for the velocity or any other time varying data)
- (4) Subroutine FIND is called which using the

boundary conditions and the grid computation field $H(N,M)$ sets up control numbers for the difference equations looping

- (5) Initial values of variables are written
- (6) Subroutine DECAY is called to compute the B.O.D. coefficient of decay (skipped for conservative case)
- (7) Subroutine SOLUB is called to compute oxygen saturation values (skipped for conservative case)
- (8) Time looping starts (NST = 1 number of time step)
- (9) Subroutine VELC is called to determine velocity field
- (10) Subroutine DIFFU is called to compute the dispersion coefficients -if they have not been read -in the x and z directions from empirical formulas
- (11) Subroutine REAR is called to calculate the surface reareation coefficient (skipped if conservative case)

- (12) Initial mass density values $LS(N,M)$ for B.O.D. are stored in the working table matrix $CO(N,M)$ (skipped for conservative case)
- (13) Initial mass density values $COP(N,M)$ for D.O. or salinity are stored in the working table matrix $CO(N,M)$ (skipped if B. O. D. looping from 12 has begun)
- (14) Using computational control NBD as set up in subroutine FIND the mass density on each column N is computed and stored in working table matrix $CT(N,M)$ using subroutine BOVAL to determine the open boundary conditions
- (15) Values of $CT(N,M)$ are placed into array $CO(N,M)$
- (16) If in B.O.D. looping sets $LS(N,M) = CT(N,M)$, for D.O. or salinity loop sets $COP(N,M) = CT(N,M)$. Therefore, for a conservative case one pass is made through steps (14)-(16)

while for D.O.-B.O.D., the B.O.D. equation is solved first and then the D.O. equation is solved, i.e. two passes through (14)-(16). This completes the first half time step.

- (17) Employing information gathered from reexecuting steps (9) - (13), then using computational controls MBD as set up in subroutine FIND and boundary values from subroutine BOVAL the mass densities on each row M are computed and stored in working table matrix CT(N,M), using similar arguments for D.O. and B.O.D. looping.
- (18) If print out is desired [NST=NPRINT ()], the computed results are printed and execution continues.
- (19) If punched output is required (NST = IPUNCH) this task is performed and execution continues.
- (20) The time is incremented by one step (AT) and subsequent time steps continue by returning to (9) (NST = NST+1)
- (21) When NST = MAXST or the number of time steps

equals the maximum number of time steps desired, execution is terminated and plots of the time varying concentrations for particular points along with the tidal height (dimensionless vertical axis) or velocity (dimensional vertical axis) are printed.

SIMPLE SUBROUTINE OUTLINE AND FUNCTIONAL DESCRIPTION

Main

In this description only the solution procedure for finite-difference equations will be shown, the other functions of MAIN having been more adequately described in the previous paragraphs.

Figure A-5 shows how the main relates to the other subroutines.

The solution of the finite-difference approximation to the laterally-averaged mass-transport equation as formulated with a Peaceman Rachford splitting tech-

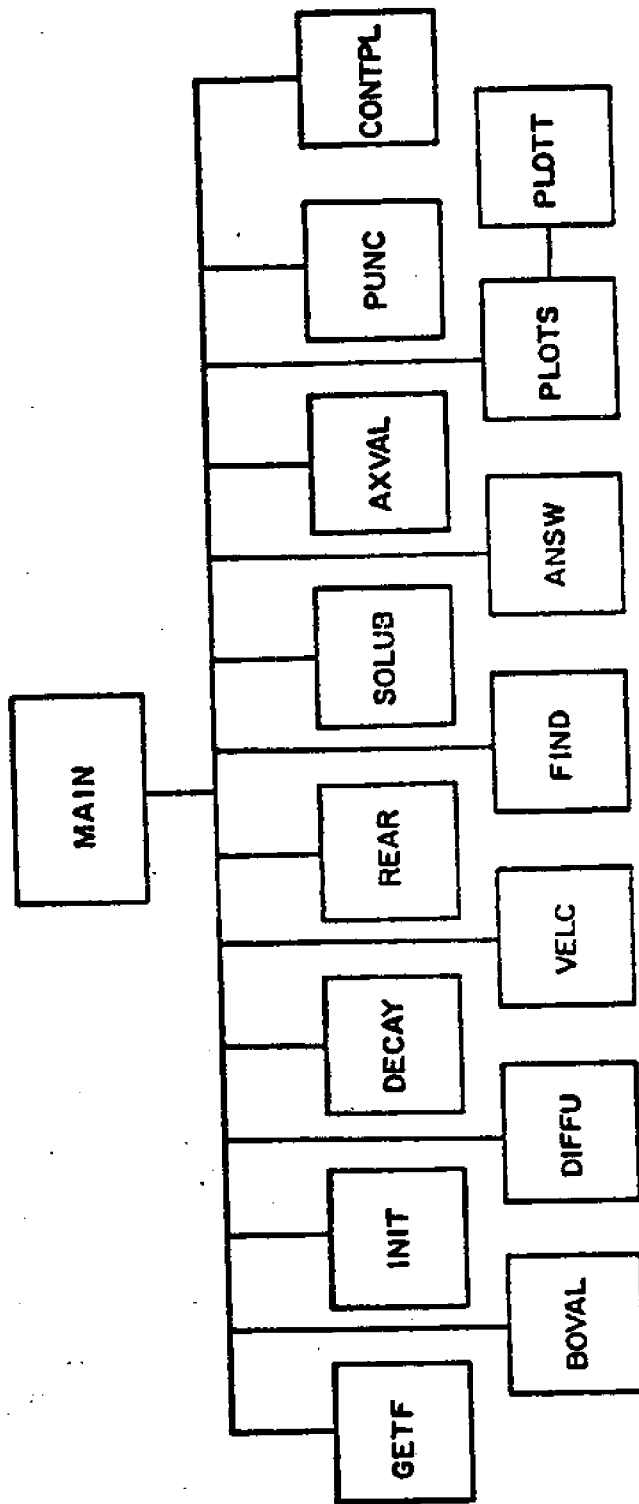


FIG. A-5 SIMPLE OUTLINE OF RELATIONSHIPS BETWEEN THE MAIN PROGRAM AND SUBROUTINES

nique is essentially completed in two steps. The mass densities for the first-half time step are computed along each column N and for the second half-time step along each row M.

Computation Of Mass Density On Row N

Taking the first NBD() value as formulated in subroutine FIND it is decomposed into its components. (A check of the functional description of subroutine FIND would be helpful in better understanding this presentation). The column N in which we are computing mass densities and the upper and lower boundary conditions are determined from this NBD value. Having established these conditions a DØ loop proceeds to find the coefficients of the implicit mass density equation for the first half time step on each row M until computation from the upper bound to the lower bound (i.e. M-small to M-large) has been completed for a given column N. Now a set of recursion terms

are calculated which incorporate the land-water or open boundary conditions and back substitution of the recursion terms in recursion equations gives the mass densities for each grid in the column. A similar procedure as outlined above is carried out until all the active computational columns have been completed or equivalently, when all the NBD values have been used.

Computation Of Mass Density On Row M

Now using the MBD values as found in subroutine FIND an analogous procedure to that described previously is performed for the second half of the time step but along the M rows.

Proceeding in this manner to solve the finite-difference equation once on each column N and once on each row M an entire time step is completed. For all subsequent time steps a similar procedure is followed.

Subroutine PLOTS

Subroutine PLOTS sets up D.O.-B.O.D. or conservative values to be plotted versus estuary longitudinal section number. It is designed to plot any column N or group of columns and also obtain vertical averages over each row M. Control numbers IGL and IGU control the upper and lower bounds of the N columns for plotting. If either or both IGL and IGU are zeros only the vertical averages are obtained.

Subroutine PUNC

This subroutine provides punched output D.O.-B.O.D. or conservative data at the IPUNCH number. Data so obtained can be used for an initial condition for a subsequent model run. For instance, if IPUNCH = 257 data at that time step would be punched.

Subroutine ANSW

Subroutine ANSW prints the main variables computed or employed during computation:

D.O. or conservative value COP(N,M)

B.O.D. LS(N,M)

tidal velocities U(N,M)

W(N,M)

Subroutine AXVAL

Prints the auxiliary variables computed or employed during computation

Dispersion DX(N,M), DZ(N,M)

Recreation Coefficient RAR(N,M)

B.O.D. decay coefficients D(N,M)

Oxygen surface solubility CS(M)

Subroutine FIND

Using the values in matrix H(N,M) which represents the grid computation field and the designation of the open boundary values as given by

MØBD(MBC) and NØBD(NBC) values, subroutine FIND develops a table of numbers for controlling the starting and stopping of consecutive computations over the rows (constant values of M or in the z direction) and columns (constant values of N or in the x direction) of the grid system. These values are denoted as NBD for the columns N and MBD for the rows M.

Values in these tables contain up to eight digits. By assigning letters to each digit we may more easily describe them. For example, a table value of NBD is SR/NO/NF/LU

SR gives information about the boundary type, S describes the lower bound and R the upper bound

i.e.

SR=00 land water boundary at both upper and lower bound of field

SR=01 land water boundary at lower bound and open boundary at upper bound

NO the column number of interest
MF lower value of active computational
grid M on column NO
LU upper value of active computational
grid M on column NO

Analogous results are also obtained for the MBD
values

Subroutine SOLUB

This subroutine computes the oxygen saturation
value at the estuary air-water interface according
to

$$C_{SAT} = (.0841 - .00256(TS) + .0000374(TS)^2) SS \\ + 14.161 - .394(TS) + .007714(TS)^2 - .0000646(TS)^3$$

where TS - temperature (°C)

SS - salinity in ‰

Subroutine REAR

This subroutine computes the reareation
coefficient for the D.O. equation according to the

Krenkel-Thackston (37) formula.

$$AR20 = .000125 \left(1 + \left(\frac{\bar{U}}{\sqrt{gH}} \right)^{1/2} \right) (U^*)$$

where

g - acceleration due to gravity ft/sec²

\bar{U} - mean longitudinal tidal velocity ft/sec

H - present estuary depth (ft)

$U^* = \bar{U} g^{1/2} / C_z$ - shear velocity

C_z - Chezy coefficient

and corrected for temperature

$$RAR = (AR20) (TS)^{POW}$$

where

TS - Temperature (°C)

POW - constant

Recreation values are computed only for the grids at the surface, but artificial recreation may be included by simple programming.

Subroutine VELC

This subroutine which is called every time step reads, computes, or presets the velocities in the entire grid field. If IVEL is greater than

1 the model at present (8/72) reads tidal height and velocity data from a disc data file and forces it to obey the one dimensional continuity equation using tidal height as the forcing parameter. If IVEL = 1 the model can read data for U and W at every half time step and assumes a conservative field.

Subroutine DECAV

The decay coefficient for the B.O.D.-D.O. equations is computed from either (if IDEC = 1)

$$K_D = A2 + B2(H)^{SKK} = D20$$

where A2, B2, and SKK are constants

H - estuary depth

and temperature corrected according to

$$K_D = (D20) (V1)^{TS-20}$$

where V1 - constant

TS - temperature of water

--or--(if IDEC>1)

$$K_D = DA + DB(TS) + DC(TS)^2 + DE(TS)^3$$

where DA, DB, DC, DE are constants and TS - temperature
(°C)

Subroutine DIFFU

This subroutine calculates the dispersion coefficients from empirical relations in both the x and z directions for IDIF = 2. For the x direction Elders modified formulation is employed

$$D_x = 14.3 H \bar{U} (2g)^{1/2} C_z^{-1} + DW$$

where

H - mean depth (ft)

\bar{U} - mean velocity at that time (ft/sec)

g - gravity (ft/sec²)

C_z - Chezy coefficient

DW - wind contribution

In the z direction Pritchard's model is used

$$D_z = \eta \frac{U_z^2 (H-z)^2}{H^3} (1 + \beta_{p R_i})^{-2} + \alpha \frac{z(H-z)}{p H} \frac{WH}{WT} e^{-\frac{2\pi z}{WL}} (1 + \beta_{p R_i})^{-2}$$

- $\eta_p, \beta_p, \alpha_p$ - empirical constants
 U - mean velocity at that time (ft/sec)
 z - depth measured vertically downward
 from MSL (ft)
 H - depth (ft)
 WH - wave height (ft)
 WL - wavelength (ft)
 WT - wave period (sec)
 R_i - Richardson number

If IDEC = 1 read statements are executed at every half time step to find D_x and D_z .

Subroutine BOVAL

BOVAL reads the boundary conditions of concentration for all specified boundary points for both D.O., B.O.D. and conservative constituents. This subroutine is called every half time step and therefore can simulate a time varying boundary condition by simply using a read statement in

place of setting the boundary mass densities constant.

It is noted that the boundary conditions are divided into two sections or conservative case (IPASS = 1) the first set of values are for B.O.D. on the open boundaries, while the second set are for the D.O. (IPASS = 2) on the open boundaries. In the set for D.O., if it is desired to have a saturation oxygen level boundary at any point on an open boundary then the mass density is set equal to $CS()$ of the nearest surface grid square which has been designated in the grid computation field $[H(N,M)]$ as a one.

Subroutine INIT

Writes the initial array variables or the initial conditions for the problem.

-----GRID COMPUTATION FIELD

ESTUARY WIDTH MATRIX 1000ft.

-----INITIAL CONCENTRATION (mg/L)

INITIAL BOD CONCENTRATION (mg/l)

WASTE LOADS IN 1000 lbs/day

SOURCES OR SINKS OF DO (mg/l)

TEMPERATURE FIELD ($^{\circ}$ F)

TIME AVERAGE SALINITY (‰)

AVERAGE SECTION DEPTH (ft) (for dimensionless z axis
model only)

In addition the subroutine performs a data smoothing operation on the width matrix to eliminate any step width gradients. The data input ISMO gives the number of passes through this smoothing operation. If ISMO equal zero width data smoothing is performed.

Subroutine GETF

Handles initial reading of array variables

H(N,M) - grid computation field

B(N,M) - estuary widths

JS(N,M) - point B.O.D. loadings

DX(N,M) - dispersion in the x direction

DZ(N,M) - dispersion in the z direction
COP(N,M) - D.O. or salinity
LS(N,M) - B.O.D.
P(N,M) - sources or sinks
TS(N,M) - temperature
SS(N,M) - salinity

The input data requirements in Table A-1 show the format requirements and dimensions to be employed.

Subroutine CMASS

When this routine is included it calculates the conservation of mass of a conservative substance. At each time step the mass in the field is computed and the total mass input and outflows from the time the model run was begun are used to calculate the present conservation of mass and is compared to the initial mass in the field at time $t=0$. Hence, a determination of the cumulative mass loss or gain of the estuary is determined.

Subroutine CONTPL

The stored values of concentrations for each time step are plotted along with the tidal height (dimensionless vertical axis model) or tidal velocity (dimensional vertical axis model) for the full number of time steps the program executes (MAXST).

PROGRAM OUTPUT

As with other phases of the program development the output has been labeled for a comprehensive D.O.-B.O.D. model, rather than left in a general form. The printed output of the program can be presented in roughly four groups: title page, control parameters, initial conditions, and time step calculated information. In an effort to make as concise and logical a presentation of this output as possible a list will be made in the following pages of this printed information and an indication of how these results can be

obtained or suppressed.

To help in more clearly understanding this list of program output, sample outputs from actual computer runs will be presented at the conclusion of this section. Cases for conservative and D.O.-B.O.D. reaction scheme for both TDLIDI and TDLIDO will be presented.

To aid in understanding the output matrices there will be a written explanation of the orientation of estuary surface, bottom and open boundaries given in the listings to follow:

(1) TITLE PAGE

The title page contains the name of the program, NABS - standing for Narragansett Bay Study. This is followed by the statement D.O.-B.O.D. showing that the program has been developed for that particular water quality system. Information on the programmer's name and address, and the date of last program revision are printed on subsequent lines.

(2) CONTROL PARAMETERS

Included in this section are the outputs which show how the estuary grid system appears after formulation and a list of control numbers employed to start and stop the looping for each of the split portions of the finite difference equation approximation.

(a) Computational Control Numbers

The number, NUM, of the computational control and the control numbers for both the x direction (constant column N) of computation, NBD, and z direction (constant row M) of computation, MBD are presented. A detailed review of the meaning of these numbers can be obtained in the description of subroutine FIND. The numbers NIND and MIND represent the total number of passes or loops through each computation plus one for the NBD and MBD control number respectively.

(b) Grid Computation Field

The number 1 in a grid space means that computations are to be performed for that grid or that the grid is active, (0) zero on the other hand meaning that the grid is inactive and no computation is performed. Numbers along the top of the page represent the column numbers N and the numbers on the left hand side are the row numbers M. To orient oneself then, the estuary surface is in column NMAX-1 and the ocean boundary is at the bottom of the page. This makes the river boundary coincide with the top of the page and the bottom contour towards the left side of the page.

(3) INITIAL CONDITIONS

In each of the arrays presented in this section the numbers along the top of the page indicate the column numbers N from 1 to NMAX (z direction) and the numbers along the left hand side indicate the

row or longitudinal estuary section number M from 1 to NMAX (x direction). For orientation purposes then the surface of the estuary is in column N = NMAX - 1, the open boundary to the ocean is in row M = MMAX, and the open boundary to the main inflowing river if one exists is in row M = 1. For a more physical approach if the printed computer output sheet is rotated 90 CCW the estuary surface is at the top, the estuary bottom is nearest you and the ocean and river boundaries to your right and left respectively.

(a) Estuary Width Matrix 1000 ft

The estuary width matrix as presented here may be smoothed by a simple averaging process to alleviate any computational problems caused by excessively steep spatial width gradients. Therefore, this output will not agree with the input width field data but should bear a close resemblance if smoothing has been used.

(b) Initial Concentration (MG/L)

The initial concentration of D.O. or conservative values are printed.

(c) Initial B.O.D. Concentration (mg/l)

If the solution to B.O.D. - D.O. equation is sought the initial B.O.D. concentration is printed in (mg/l), while for salinity or the conservative case this output is suppressed.

(d) Waste loads in 1000 lbs./day

As indicated this represents the steady B.O.D. loadings to the estuary in 1000 lbs./day. Time varying loads can be handled by placing the read statement for this quantity in subroutine VELC. In a conservative case this output is suppressed.

(e) Sources or Sinks of D.O. (mg/l)

To account for various D.O. loadings due to zooplankton, phytoplankton, benthic demands, etc. the steady state sources and sinks of D.O. are presented in (mg/l). This output is however suppressed for conservative type problems.

(f) Temperature Field ($^{\circ}$ F)

The constant estuary temperature field in $^{\circ}$ F is presented.

(g) Time Average Salinity (‰)

The time averaged salinity profile in (‰) for the estuary field is presented. These values should reflect an average over time which approximately corresponds to that used for the temperature field. This output is suppressed for the conservative case.

(h) Averaged Section Depth (ft.)

The average MSL depth of water columns for all longitudinal sections (M) are printed for the dimensionless z-axis model only.

Time Step Calculated Information

The information printed in this section can be obtained at the completion of every step, however since this adds considerably to computer time only a few of the time steps are actually written. Specifications for this output is accomplished by setting NPRINT () equal to the time step (NST) at which printout is desired.

In regard to the printing of the fields or arrays, and orientation of the output matrix, the exact same format as described in the initial conditions output section applies. There is however, in addition, the number of the

time steps (NST) and the actual time in hours from the start of the program. (Actual time = NST * time step(AT))

(a) Concentration of Dissolved Oxygen (mg/l)

The D.O. in (mg/l) or the conservative values at the completion of the time step given is printed.

(b) Concentration of B.O.D. (mg/l)

The B.O.D. (mg/l) values at the completion of the stated time step are printed. In a conservative case this output is suppressed.

(c) u Velocity Field (- FLOOD) -FPS

The u or x directed velocity component is presented in ft/sec. The notation (- FLOOD) is used to show that a negative u velocity corresponds to estuary flooding when the ocean entrance of the grid system occurs in row M = MMAX.

(d) w Velocity Field - FPS

The w or z directed velocity component is presented in ft/sec. This velocity is positive in the direction of ascending column numbers N for a given row M; therefore an upwelling velocity is positive.

(e) Dispersion Coefficient for x Direction (ft²/sec)

The dispersion coefficients for the x - direction as based on read values or a modified Elder's formulation are printed.

(f) Dispersion Coefficient for z Direction (ft²/sec)

The dispersion coefficients for the z direction as supplied or based on Pritchard's formulation are given.

(g) Reareation Coefficients X 1000000 (1/sec)

The reareation coefficients for the surface based on the Thackston-Krenkel (37) formulation are presented. By suitably adjusting the values in this array in subroutine REAR effects of artifical reareation can also be included. These results are suppressed for conservative cases.

(h) B.O.D. Decay Coefficients (1/sec) X 1000000

The B.O.D. decay coefficients in (1/sec) for the estuary are printed after having been water temperature corrected. This output is suppressed for the conservative cases.

(i) Surface Oxvgen Solubility (mg/l)

The surface oxygen saturation values for each

estuary section M are printed. This printout is also suppressed for conservative cases.

(j) Graphs

In order to present the data in a format for quick reviewing a plotting technique was developed. The scope of the graphical output is the ability to plot any given column N (i.e. dimensional or nondimensional water level depth) or successive series of columns against the rows (i.e. estuary longitudinal section numbers). For instance if column NMAX - 1 is plotted, the surface values of mass densities are obtained. In addition, a vertically averaged set of mass densities is also plotted against the longitudinal estuary section number. It is to be remembered that these plots are for the time step as given by the previous set of time calculated information.

(j1) D.O. (1) B.O.D. (2) in (mg/l) vs.

Estuary longitudinal section number

The D.O. given by the number (1) and B.O.D. noted by number (2) are plotted vs. estuary longitudinal section number. The estuary section number is given in ascending order on the left hand side of the page and the scaled by

the largest value, mass densities are shown at the bottom of the page. The chart number presented at the top of the page just under the title gives the column number N for which the plot was executed. If IGL or IGU in the read statements are set equal to zero this printout is suppressed. In the case of a conservative constituent its mass densities are printed under the number (1) and the number (2) is used simply to describe a reference state.

An abnormality in this IBM adapted special scientific subroutine is that whenever the mass densities of D.O. and B.O.D. are relatively close as determined by the scaling factor used for mass densities then a (2) is printed. This should however, cause no problem in interpretation as long as the phenomena is understood.

(j2) Average DO (1) B.O.D. (2) m (mg/l) vs.

Estuary Longitudinal Section Number

The notations and graph orientation of this plotted output is exactly analogous to that given above, the only difference being that all these values have been averaged over the vertical sections or constant M rows.

In addition to printed output the program also has the capability to provide punched output in the same format as required for initial mass density or concentration program inputs. This data is desired since the time required to "start" the program, that is to go from a uniform mass density field to its actual quasi-steady value is the order of many days. Avoiding this problem can be accomplished by developing a quasi-steady state condition and using it for the initial conditions to the program thus avoiding , to a large extent, the "start up" problem. For the D.O. - B.O.D. system both D.O. and B.O.D. are provided as output when NST, the time step, equals IPUNCH, end of the time step at which punched output is desired. A similar situation holds in the conservative case however only one array containing the salinity, alkalinity etc. is punched.

PROGRAM OUTPUT

Conservative Case

TDLIDI

D.O. - B.O.D. System

Conservative Case

TDLIDO

D.O. - B.O.D. System

SAMPLE OUTPUT - TDLIDI
(DIMENSIONAL VERTICAL AXIS MODEL)
CONSERVATIVE CASE

```

NN NN AA      SSSSS
NN NN AAA     SSSSSSS
NNN NN AA AA  SS
NNN NN AA AA  SS
NNN NN AA AA  SSSSSS
NN NN AAAAAA  SSSSSS
NN NN AAAAAA  SS
NN NN AA AA   SS
AA NN AA AA   SSSSSS
NN NN AA AA   SSSSS

```

```

DND (N)  HHR LU DND
D D D D  D C C D D
D D D D  -- RGD C C D D
D D C D  R P C C D D
D D D D  H-H C D DND

```

PROGRAM DEVELOPED BY - P. SPAULDING
UNIVERSITY OF PUERTO RICO HALL 222C
JUNE 1972

COMPUTATIONAL CONTROL NUMBERS

NUP	NPC	MAD
1	1094667	21415
2	1094547	31315
3	1094447	41215
4	1094347	51115
5	1094247	61015
6	1094147	70915
7	93031	80815
8	1093947	90715
9	1102747	101315
10	1112147	111115
11	120409	121115
12	121314	131115
13	121247	141115
14	111047	151115
15	1184247	161115
16	11150247	171115
17	0	181115
18	0	191115
19	0	201115
20	0	211115
21	0	221115
22	0	231115
23	0	241115
24	0	251115
25	0	261115
26	0	271115
27	0	281115
28	0	291115
29	0	301115
30	0	311115
31	0	321115
32	0	331115
33	0	341115
34	0	350115
35	0	360115
36	0	370115
37	0	380115
38	0	390115
39	0	400115
40	0	410115
41	0	420115
42	0	430115
43	0	440115
44	0	450115
45	0	460115
46	0	470115
47	0	480115
48	0	490115

MINC = 17 MIND = 47

	STEP NUMBER = 1										TIME = 0.000000									
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16				
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				

DISPERSION COEFFICIENT PPM 2 DIRECTION (FT/FT/SEC)	STEP NUMBER = 1	TIME = 0.031MS
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0
11	0	0
12	0	0
13	0	0
14	0	0
15	0	0
16	0	0
17	0	0
18	0	0
19	0	0
20	0	0
21	0	0
22	0	0
23	0	0
24	0	0
25	0	0
26	0	0
27	0	0
28	0	0
29	0	0
30	0	0
31	0	0
32	0	0
33	0	0
34	0	0
35	0	0
36	0	0
37	0	0
38	0	0
39	0	0
40	0	0
41	0	0
42	0	0
43	0	0
44	0	0
45	0	0
46	0	0
47	0	0
48	0	0
49	0	0
50	0	0

P.C. (1) 3 P.O.D. (2) IN MC/L VS ESTILARY LONGITUDINAL SECTION NUMBER
 CHART 14

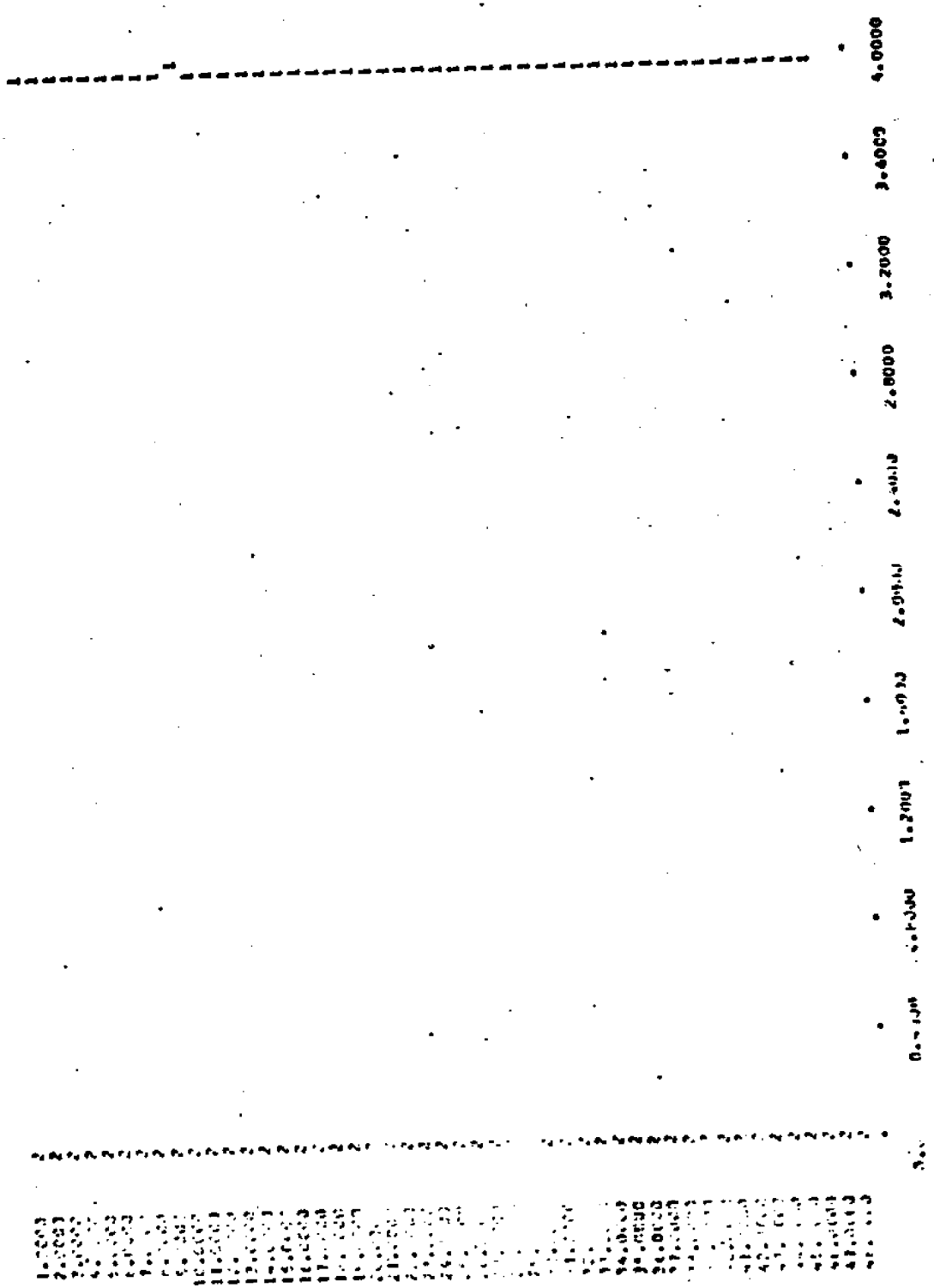
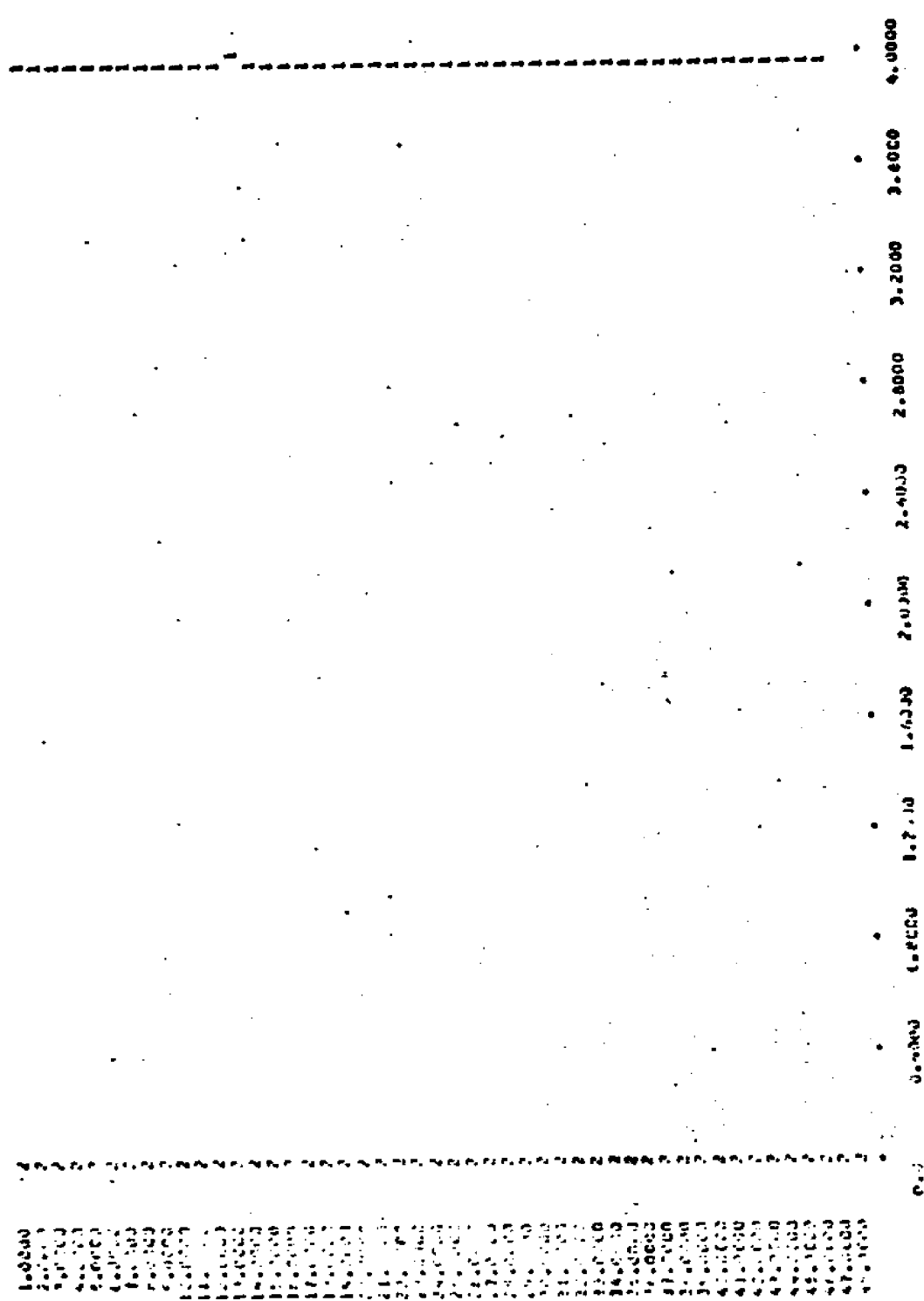
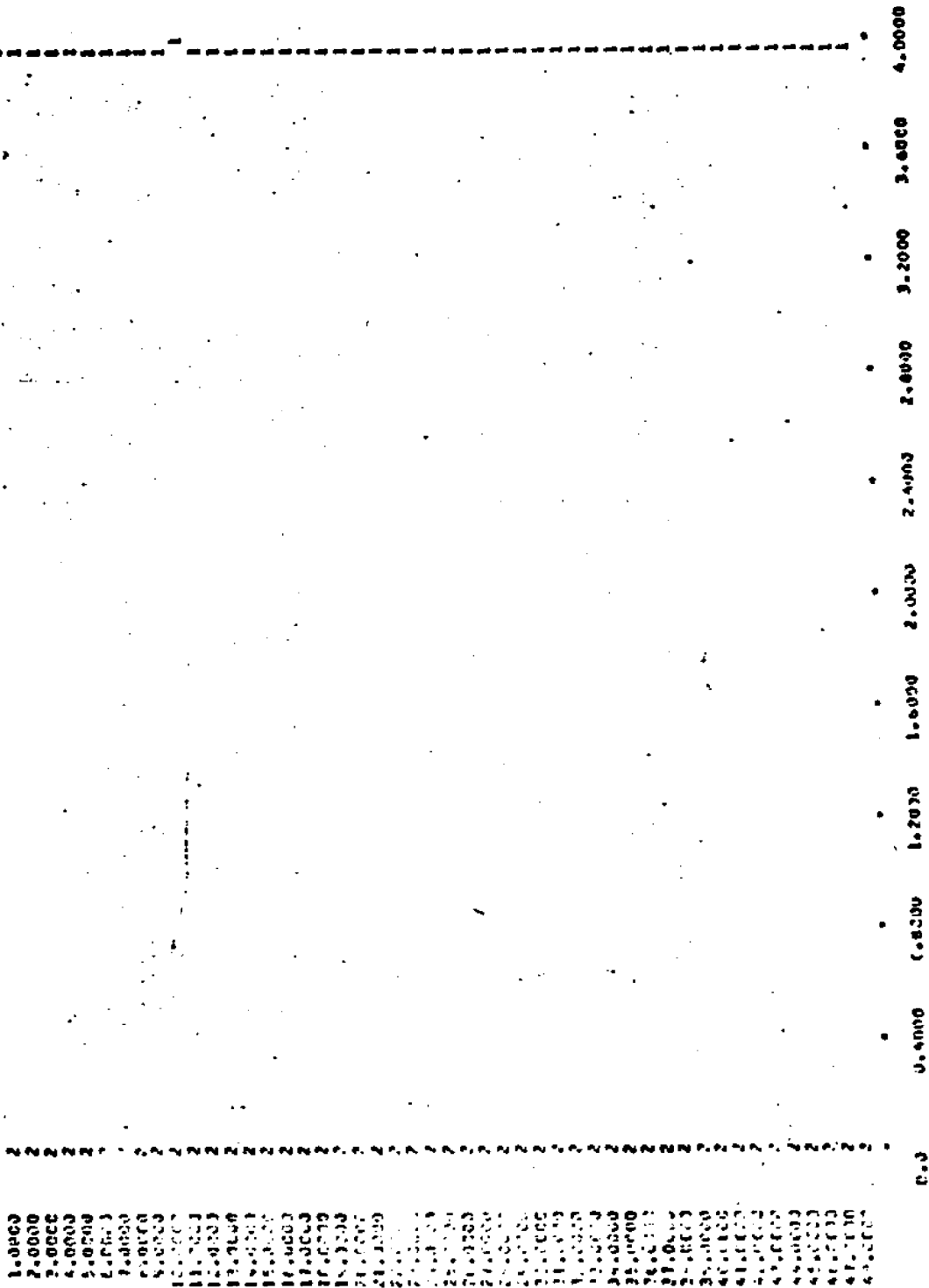


FIG. 110. M.I. 120 IN MG/A VS FIBER LONGITUDINAL SECTION NUMBER
CHART 15



AVERAGE C.O.D. (1) & S.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER CHART



P.C. 111 S. 6th St. 179 IN MEAL VS ESTILARY LINGUIODINAL SECTION NUMBER
CHART 14

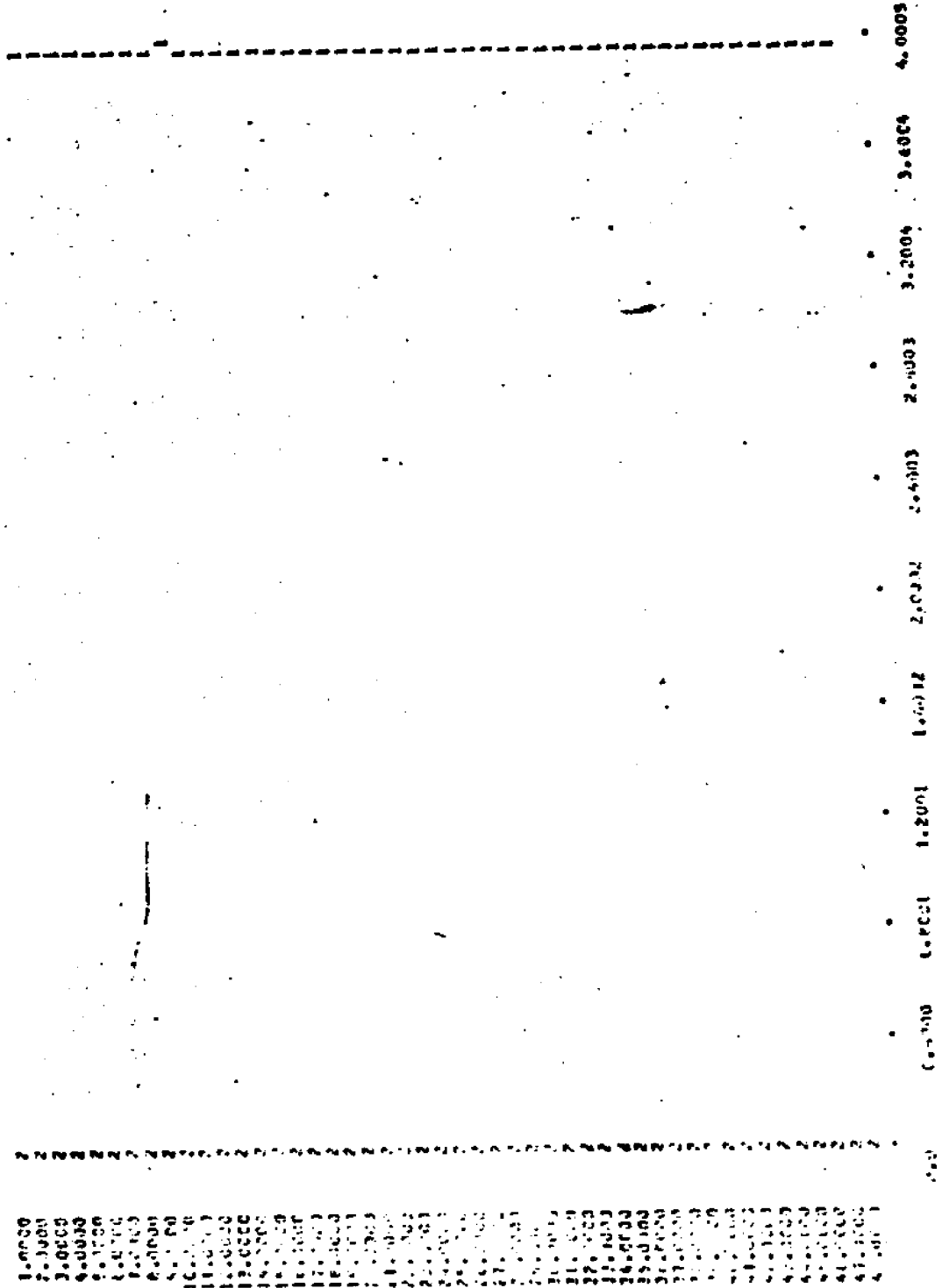
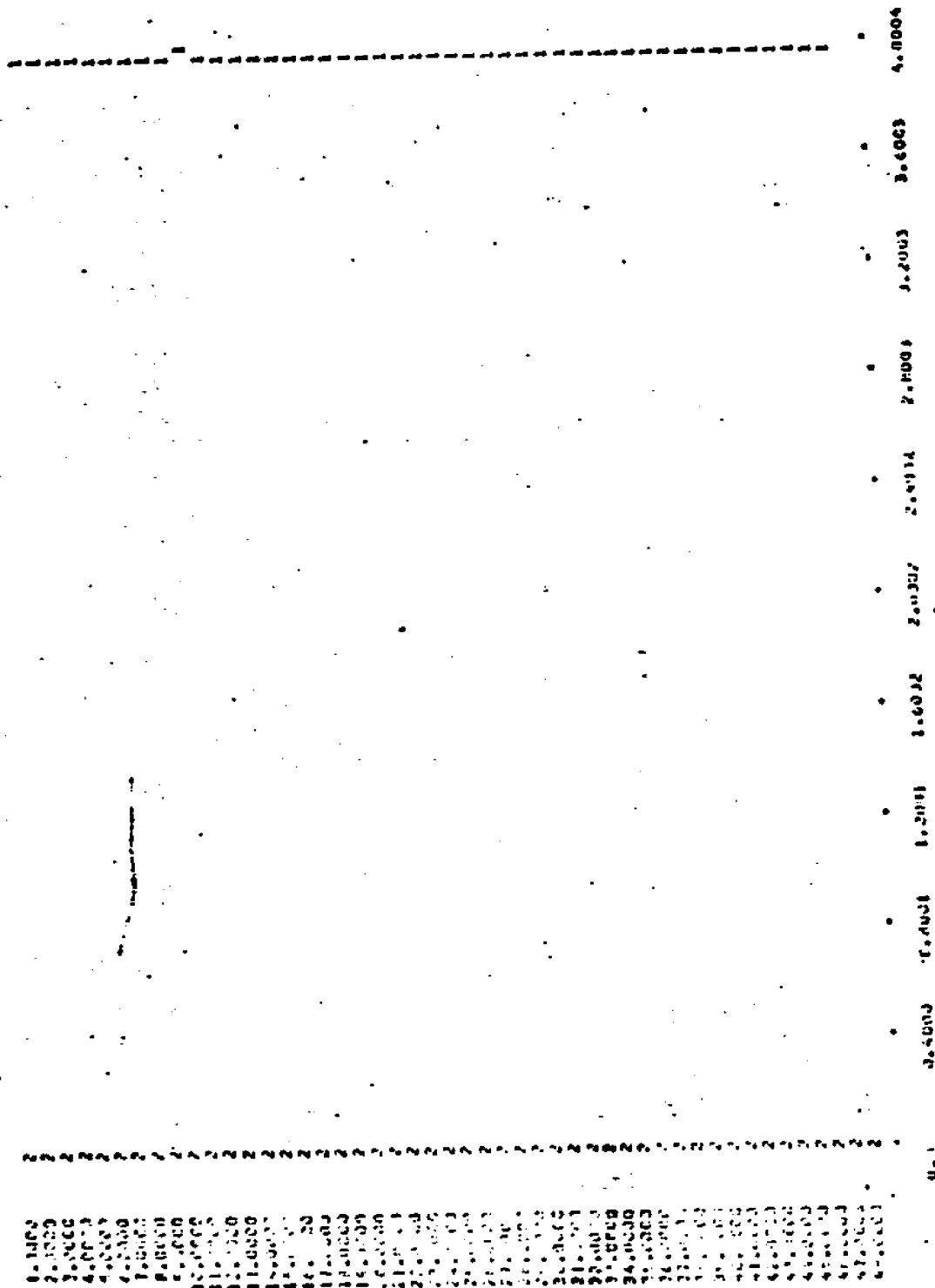


FIG. 111 1 A.C.B. (2) IN MG/L VS ESTARY LONGITUDINAL SECTION NUMBER CHART 15



AVERAGE C.C. III 1 H.O.D. CFI IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER CHART I

1.0000
 2.0000
 3.0000
 4.0000
 5.0000
 6.0000
 7.0000
 8.0000
 9.0000
 10.0000
 11.0000
 12.0000
 13.0000
 14.0000
 15.0000
 16.0000
 17.0000
 18.0000
 19.0000
 20.0000
 21.0000
 22.0000
 23.0000
 24.0000
 25.0000
 26.0000
 27.0000
 28.0000
 29.0000
 30.0000
 31.0000
 32.0000
 33.0000
 34.0000
 35.0000
 36.0000
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 42.0000
 43.0000
 44.0000
 45.0000
 46.0000
 47.0000
 48.0000

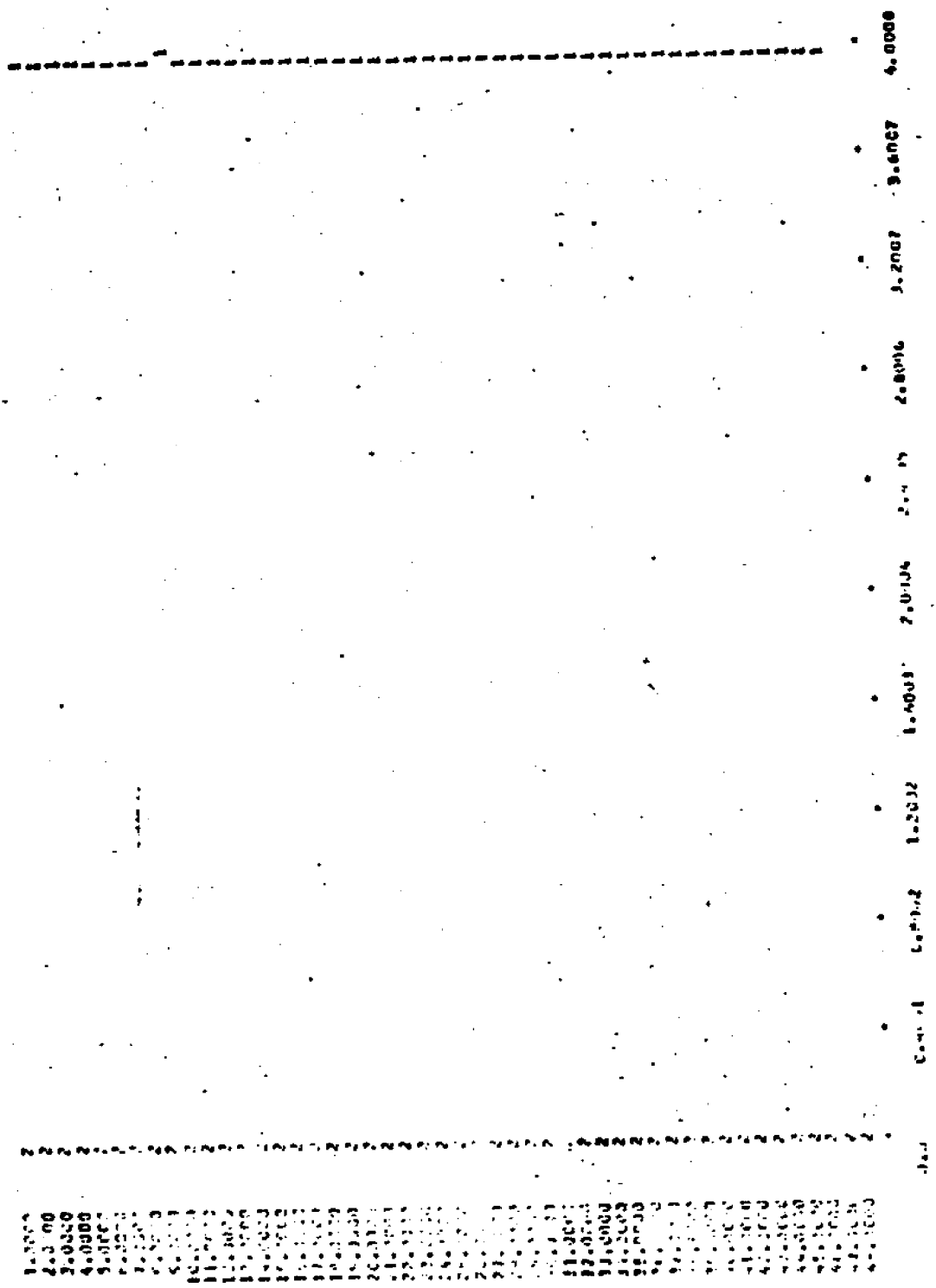
0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0 2.1 2.2 2.3 2.4 2.5 2.6 2.7 2.8 2.9 3.0 3.1 3.2 3.3 3.4 3.5 3.6 3.7 3.8 3.9 4.0 4.1 4.2 4.3 4.4 4.5 4.6 4.7 4.8 4.9 5.0

STEP NUMBER = 97 TIME = 3.301815

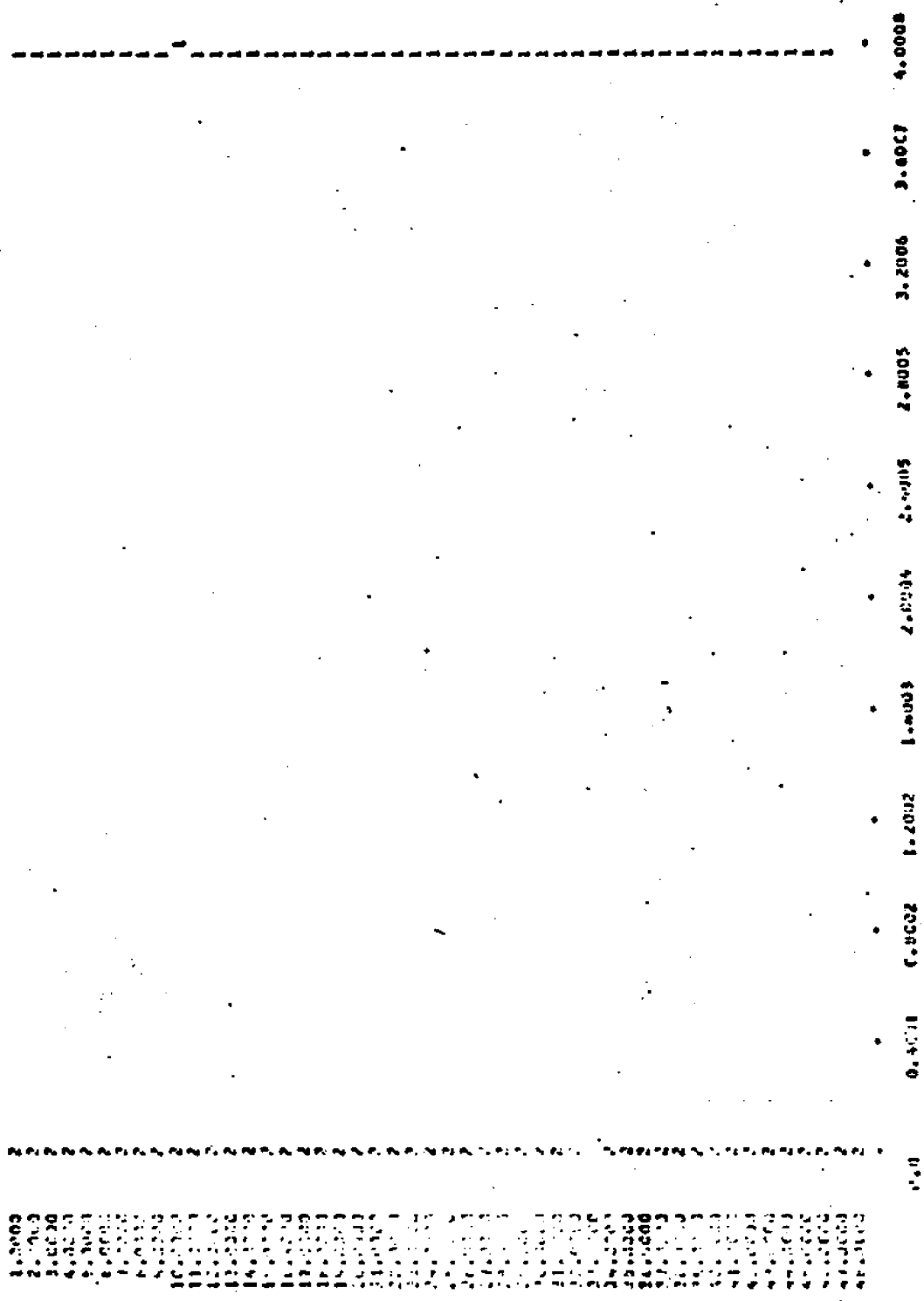
DISPERSION COEFFICIENT FOR 2 DIRECTION (FT/SEC)

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
8	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
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31	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
32	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
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41	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
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44	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
46	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
47	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
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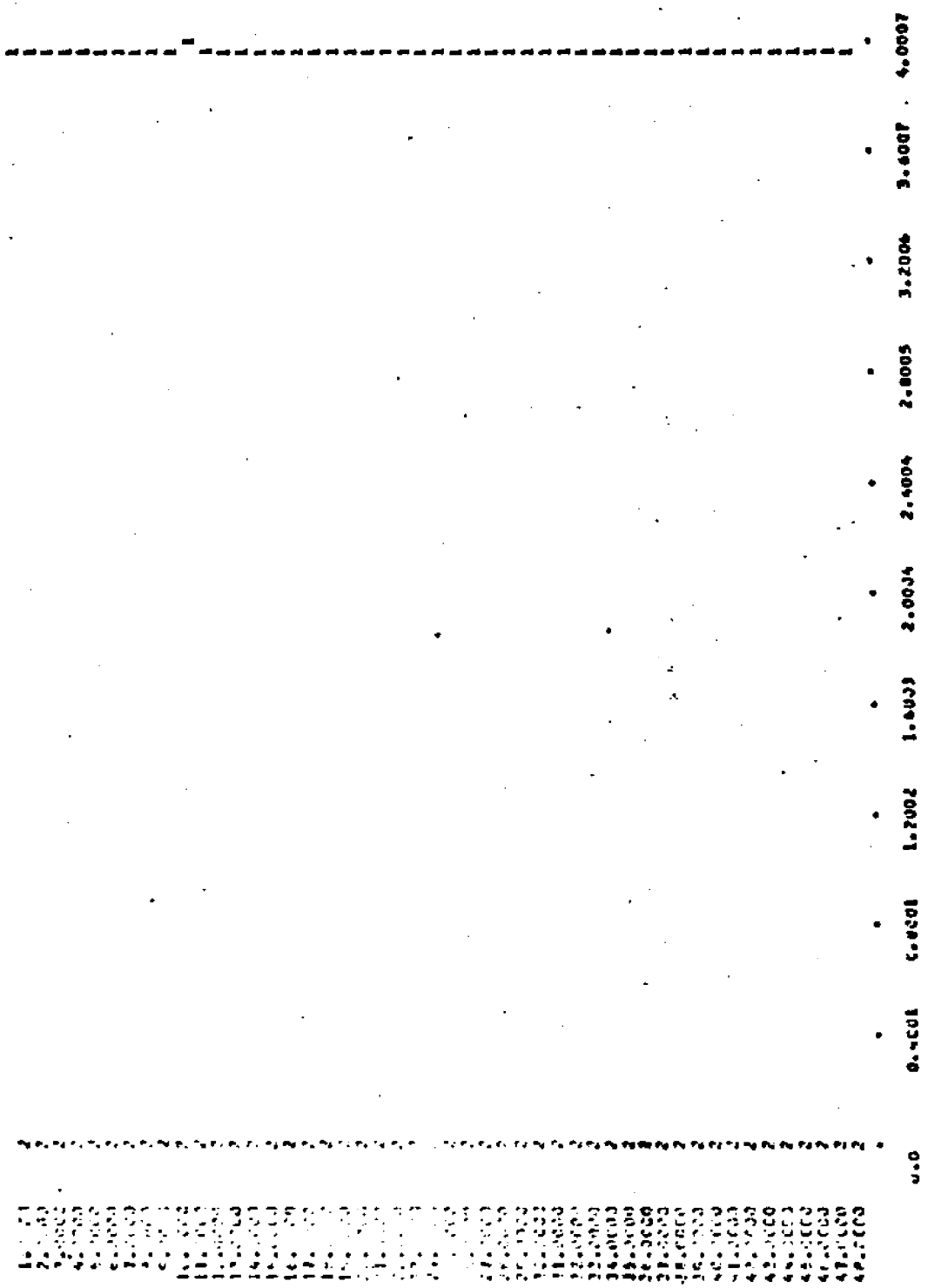
C.C. (1) S. 400.F. (2) IN NGA VS ESTUARY LONGITUDINAL SECTION NUMBER CHART 14



Figs. (1) & (2) IN REG. VS. TSTARY LONGITUDINAL SECTION NUMBER
 CHART 17



BATHY THERMOGRAPHY (BT) IN WGL VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1



PLCT OF P.C. 1113, N.S.P. 1131, AND TIDAL VELOCITY (DIPCA GRID N-14 No 7 TIME STEP- 0.03 HRS.

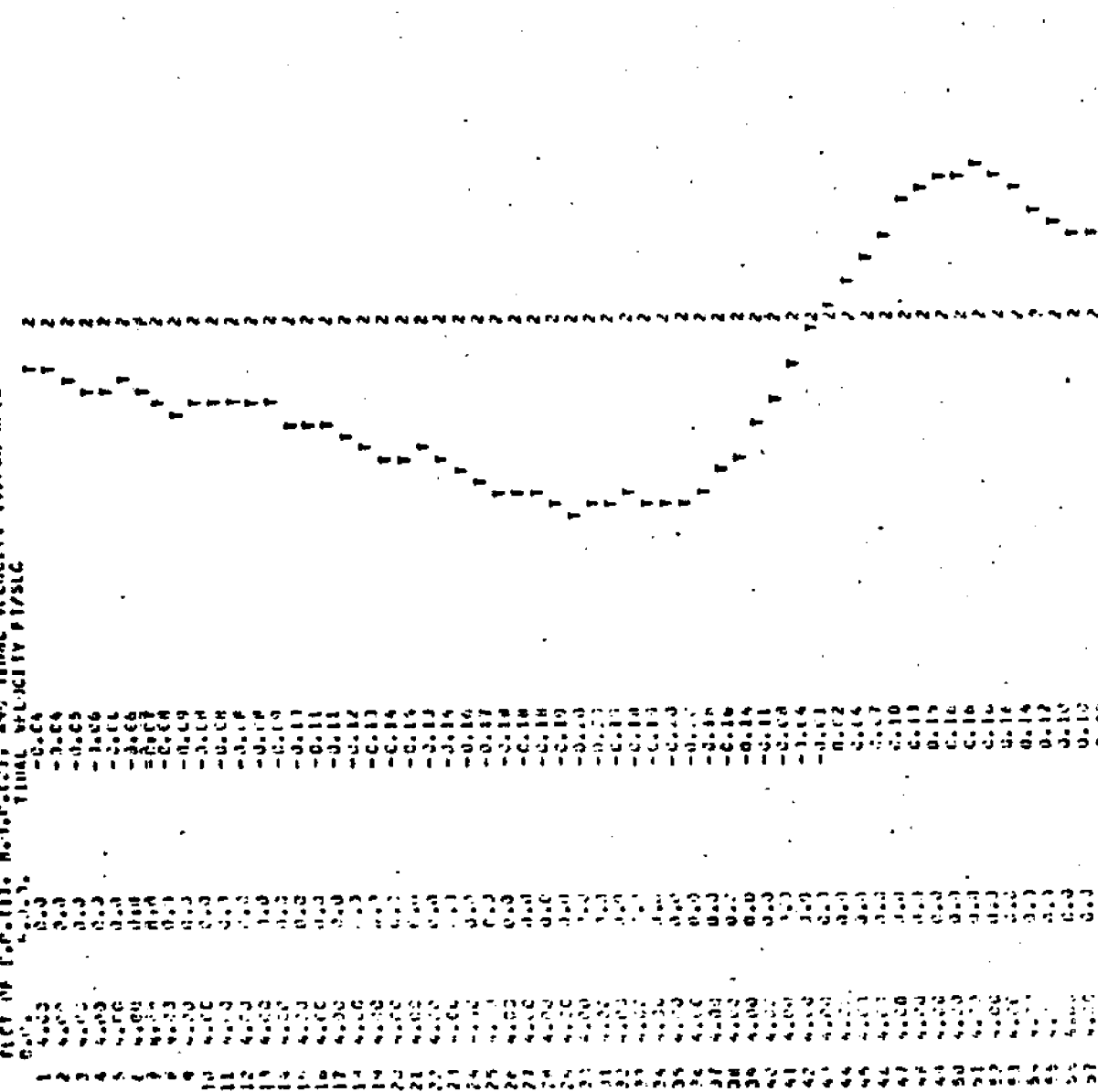
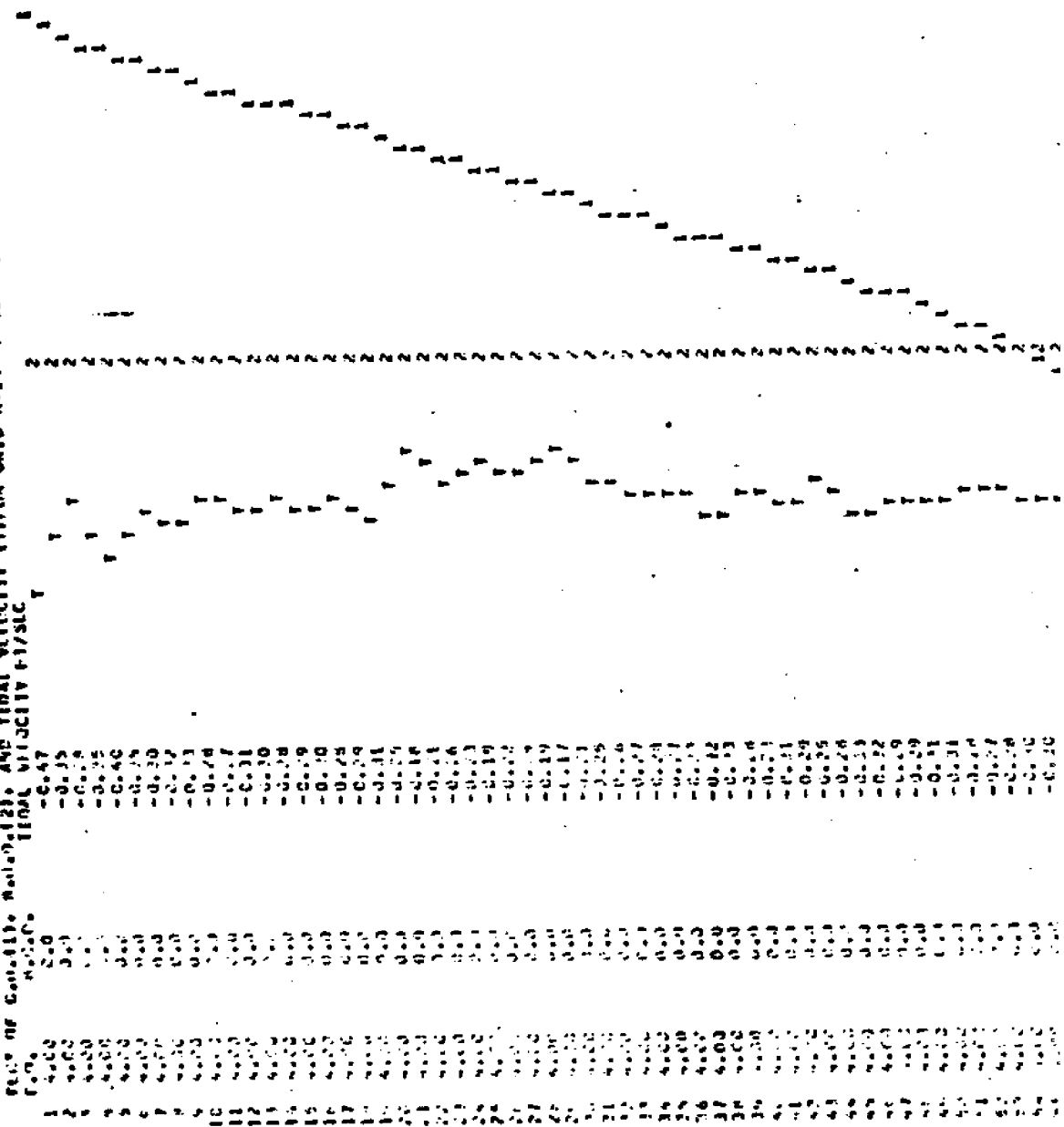


PLATE NO. 123, AND TIDAL VELOCITY (TIDOR GRID NO. 14) P. 45 TIME STEP = 0.03 HRS.



SAMPLE OUTPUT - TDLIDI
(DIMENSIONAL VERTICAL AXIS MODEL)
D.O. - B.O.D. CASE

COMPUTATIONAL CONTROL NUMBERS

NO	NAC	MAD
1	1010007	21415
2	1214367	31315
3	1010007	41215
4	1014367	51215
5	1014367	61215
6	1014367	71215
7	1010007	81215
8	1014367	91115
9	1014367	10115
10	1014367	11115
11	1010007	12115
12	1014367	13115
13	1014367	14115
14	1014367	15115
15	1014367	16115
16	1014367	17115
17	1014367	18115
18	1014367	19115
19	1014367	20115
20	1014367	21115
21	1014367	22115
22	1014367	23115
23	1014367	24115
24	1014367	25115
25	1014367	26115
26	1014367	27115
27	1014367	28115
28	1014367	29115
29	1014367	30115
30	1014367	31015
31	1014367	32115
32	1014367	33115
33	1014367	34115
34	1014367	35015
35	1014367	36015
36	1014367	37015
37	1014367	38015
38	1014367	39015
39	1014367	40015
40	1014367	41015
41	1014367	42015
42	1014367	43015
43	1014367	44015
44	1014367	45015
45	1014367	46015
46	1014367	47015
47	1014367	48015
48	1014367	49015
49	1014367	50015

VALUES OF SINES OF AN ANGLES

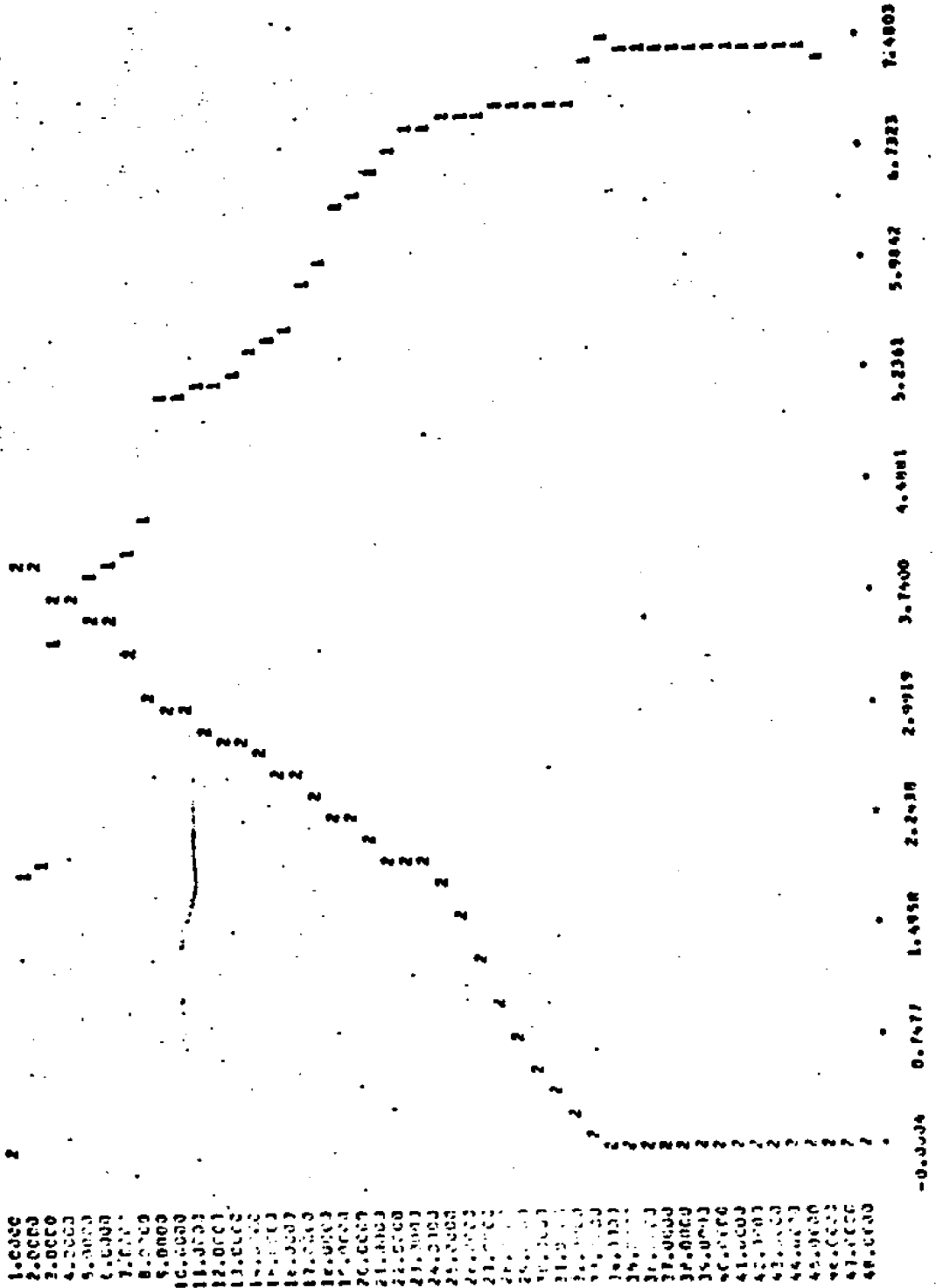
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	0.0175	0.0350	0.0525	0.0700	0.0875	0.1050	0.1225	0.1400	0.1575	0.1750	0.1925	0.2100	0.2275	0.2450	0.2625	0.2800
2	0.0350	0.0700	0.1050	0.1400	0.1750	0.2100	0.2450	0.2800	0.3150	0.3500	0.3850	0.4200	0.4550	0.4900	0.5250	0.5600
3	0.0525	0.1050	0.1575	0.2100	0.2625	0.3150	0.3675	0.4200	0.4725	0.5250	0.5775	0.6300	0.6825	0.7350	0.7875	0.8400
4	0.0700	0.1400	0.2100	0.2800	0.3500	0.4200	0.4900	0.5600	0.6300	0.7000	0.7700	0.8400	0.9100	0.9800	1.0500	1.1200
5	0.0875	0.1750	0.2625	0.3500	0.4375	0.5250	0.6125	0.7000	0.7875	0.8750	0.9625	1.0500	1.1375	1.2250	1.3125	1.4000
6	0.1050	0.2100	0.3150	0.4200	0.5250	0.6300	0.7350	0.8400	0.9450	1.0500	1.1550	1.2600	1.3650	1.4700	1.5750	1.6800
7	0.1225	0.2450	0.3675	0.4900	0.6125	0.7350	0.8575	0.9800	1.1025	1.2250	1.3475	1.4700	1.5925	1.7150	1.8375	1.9600
8	0.1400	0.2800	0.4200	0.5600	0.7000	0.8400	0.9800	1.1200	1.2600	1.4000	1.5400	1.6800	1.8200	1.9600	2.1000	2.2400
9	0.1575	0.3150	0.4725	0.6300	0.7875	0.9450	1.1025	1.2600	1.4175	1.5750	1.7325	1.8900	2.0475	2.2050	2.3625	2.5200
10	0.1750	0.3500	0.5250	0.7000	0.8750	1.0500	1.2250	1.4000	1.5750	1.7500	1.9250	2.1000	2.2750	2.4500	2.6250	2.8000
11	0.1925	0.3850	0.5775	0.7700	0.9625	1.1550	1.3475	1.5400	1.7325	1.9250	2.1175	2.3100	2.5025	2.6950	2.8875	3.0800
12	0.2100	0.4200	0.6125	0.8400	1.0500	1.2600	1.4700	1.6800	1.8900	2.1000	2.3100	2.5200	2.7300	2.9400	3.1500	3.3600
13	0.2275	0.4550	0.6825	0.9100	1.1375	1.3650	1.5925	1.8200	2.0475	2.2750	2.5025	2.7300	2.9575	3.1850	3.4125	3.6400
14	0.2450	0.4900	0.7350	0.9800	1.2250	1.4700	1.7150	1.9600	2.2050	2.4500	2.6950	2.9400	3.1850	3.4300	3.6750	3.9200
15	0.2625	0.5250	0.7875	1.0500	1.3125	1.5750	1.8375	2.1000	2.3625	2.6250	2.8875	3.1500	3.4125	3.6750	3.9375	4.2000
16	0.2800	0.5600	0.8400	1.1200	1.4000	1.6800	1.9600	2.2400	2.5200	2.8000	3.0800	3.3600	3.6400	3.9200	4.2000	4.4800
17	0.2975	0.5950	0.8925	1.1900	1.4700	1.7625	2.0475	2.3400	2.6400	2.9400	3.2400	3.5400	3.8400	4.1400	4.4400	4.7400
18	0.3150	0.6300	0.9450	1.2600	1.5400	1.8450	2.1475	2.4500	2.7600	3.0600	3.3600	3.6600	3.9600	4.2600	4.5600	4.8600
19	0.3325	0.6650	0.9975	1.3300	1.6125	1.9475	2.2600	2.5700	2.8800	3.1800	3.4800	3.7800	4.0800	4.3800	4.6800	4.9800
20	0.3500	0.7000	1.0500	1.4000	1.6800	2.0500	2.3800	2.6900	3.0000	3.3000	3.6000	3.9000	4.2000	4.5000	4.8000	5.1000
21	0.3675	0.7350	1.1025	1.4700	1.7500	2.1525	2.5000	2.8100	3.1200	3.4300	3.7400	4.0500	4.3600	4.6700	4.9800	5.2900
22	0.3850	0.7700	1.1550	1.5400	1.8200	2.2550	2.6100	2.9200	3.2300	3.5400	3.8500	4.1600	4.4700	4.7800	5.0900	5.4000
23	0.4025	0.8050	1.2075	1.6100	1.8900	2.3575	2.7200	3.0300	3.3400	3.6500	3.9600	4.2700	4.5800	4.8900	5.2000	5.5100
24	0.4200	0.8400	1.2600	1.6800	1.9600	2.4600	2.8300	3.1400	3.4500	3.7600	4.0700	4.3800	4.6900	5.0000	5.3100	5.6200
25	0.4375	0.8750	1.3125	1.7500	2.0300	2.5625	2.9400	3.2500	3.5600	3.8700	4.1800	4.4900	4.8000	5.1100	5.4200	5.7300
26	0.4550	0.9100	1.3650	1.8200	2.1000	2.6650	3.0500	3.3600	3.6700	3.9800	4.2900	4.6000	4.9100	5.2200	5.5300	5.8400
27	0.4725	0.9450	1.4175	1.8900	2.1700	2.7675	3.1600	3.4700	3.7800	4.0900	4.4000	4.7100	5.0200	5.3300	5.6400	5.9500
28	0.4900	0.9800	1.4700	1.9600	2.2400	2.8700	3.2700	3.5800	3.8900	4.2000	4.5100	4.8200	5.1300	5.4400	5.7500	6.0600
29	0.5075	1.0150	1.5225	2.0300	2.3100	2.9725	3.3800	3.6900	4.0000	4.3100	4.6200	4.9300	5.2400	5.5500	5.8600	6.1700
30	0.5250	1.0500	1.5750	2.1000	2.3800	3.0750	3.4900	3.8000	4.1100	4.4200	4.7300	5.0400	5.3500	5.6600	5.9700	6.2800
31	0.5425	1.0850	1.6275	2.1700	2.4500	3.1775	3.6000	3.9100	4.2200	4.5300	4.8400	5.1500	5.4600	5.7700	6.0800	6.3900
32	0.5600	1.1200	1.6800	2.2400	2.5200	3.2800	3.7100	4.0200	4.3300	4.6400	4.9500	5.2600	5.5700	5.8800	6.1900	6.5000
33	0.5775	1.1550	1.7325	2.3100	2.5900	3.3825	3.8200	4.1300	4.4400	4.7500	5.0600	5.3700	5.6800	5.9900	6.3000	6.6100
34	0.5950	1.1900	1.7850	2.3800	2.6600	3.4850	3.9300	4.2400	4.5500	4.8600	5.1700	5.4800	5.7900	6.1000	6.4100	6.7200
35	0.6125	1.2250	1.8375	2.4500	2.7300	3.5875	4.0400	4.3500	4.6600	4.9700	5.2800	5.5900	5.9000	6.2100	6.5200	6.8300
36	0.6300	1.2600	1.8900	2.5200	2.8000	3.6900	4.1500	4.4600	4.7700	5.0800	5.3900	5.7000	6.0100	6.3200	6.6300	6.9400
37	0.6475	1.2950	1.9425	2.5900	2.8700	3.7925	4.2600	4.5700	4.8800	5.1900	5.5000	5.8100	6.1200	6.4300	6.7400	7.0500
38	0.6650	1.3300	2.0000	2.6600	2.9400	3.8950	4.3700	4.6800	4.9900	5.3000	5.6100	5.9200	6.2300	6.5400	6.8500	7.1600
39	0.6825	1.3650	2.0525	2.7300	3.0100	4.0000	4.4800	4.7900	5.1000	5.4100	5.7200	6.0300	6.3400	6.6500	6.9600	7.2700
40	0.7000	1.4000	2.1050	2.8000	3.0800	4.1025	4.5900	4.9000	5.2100	5.5200	5.8300	6.1400	6.4500	6.7600	7.0700	7.3800
41	0.7175	1.4350	2.1575	2.8700	3.1500	4.2075	4.7000	5.0100	5.3200	5.6300	5.9400	6.2500	6.5600	6.8700	7.1800	7.4900
42	0.7350	1.4700	2.2100	2.9400	3.2200	4.3100	4.8100	5.1200	5.4300	5.7400	6.0500	6.3600	6.6700	6.9800	7.2900	7.6000
43	0.7525	1.5050	2.2625	3.0100	3.2900	4.4150	4.9200	5.2300	5.5400	5.8500	6.1600	6.4700	6.7800	7.0900	7.4000	7.7100
44	0.7700	1.5400	2.3150	3.0800	3.3600	4.5200	5.0300	5.3400	5.6500	5.9600	6.2700	6.5800	6.8900	7.2000	7.5100	7.8200
45	0.7875	1.5750	2.3675	3.1500	3.4300	4.6250	5.1400	5.4500	5.7600	6.0700	6.3800	6.6900	7.0000	7.3100	7.6200	7.9300
46	0.8050	1.6100	2.4200	3.2200	3.5000	4.7300	5.2500	5.5600	5.8700	6.1800	6.4900	6.8000	7.1100	7.4200	7.7300	8.0400
47	0.8225	1.6450	2.4725	3.2900	3.5700	4.8350	5.3600	5.6700	5.9800	6.2900	6.6000	6.9100	7.2200	7.5300	7.8400	8.1500
48	0.8400	1.6800	2.5250	3.3600	3.6400	4.9400	5.4700	5.7800	6.0900	6.4000	6.7100	7.0200	7.3300	7.6400	7.9500	8.2600
49	0.8575	1.7150	2.5775	3.4300	3.7100	5.0450	5.5800	5.8900	6.2000	6.5100	6.8200	7.1300	7.4400	7.7500	8.0600	8.3700
50	0.8750	1.7500	2.6300	3.5000	3.7800	5.1500	5.6900	6.0000	6.3100	6.6200	6.9300	7.2400	7.5500	7.8600	8.1700	8.4800

DISPERSION COEFFICIENT FOR Z DIRECTION (FTOFT/SEC) STEP NUMBER = 1 TIME = 0.03MRS

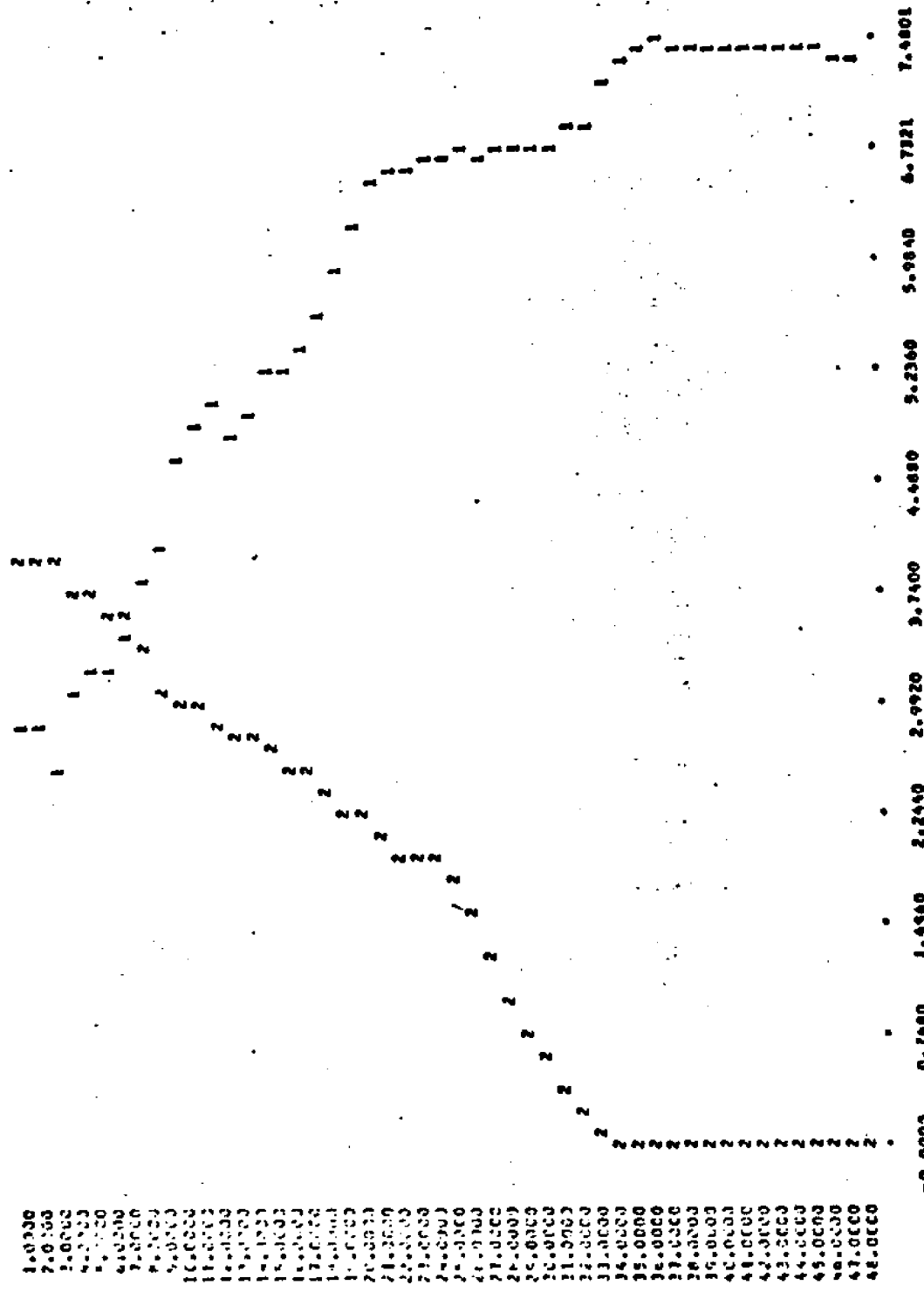
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
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2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
8	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
27	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
28	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
29	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
31	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
32	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
33	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
34	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
36	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
37	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
38	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
39	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
41	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
42	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
43	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
44	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
46	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
47	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
48	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

SURFACE OXYGEN SOLUBILITY (MG/L)
 0.0
 7.1817
 7.1828
 7.1891
 7.2025
 7.1932
 7.1976
 7.2017
 7.1924
 7.1922
 7.2058
 7.1802
 7.2056
 7.1511
 7.2214
 7.2110
 7.2445
 7.2261
 7.2191
 7.2512
 7.2155
 7.2839
 7.3051
 7.3146
 7.3265
 7.3313
 7.3334
 7.3362
 7.3519
 7.3579
 7.3531
 7.3531
 7.3475
 7.3479
 7.3027
 7.3171
 7.3115
 7.3009
 7.3412
 7.3607
 7.3637
 7.3627
 7.3764
 7.3627
 7.3582
 7.3622
 7.3582
 0.0

C. 11) 6 H.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 14



AVERAGE C.O. (1) & (2) IN MD/L VS ESTILARY LONGITUDINAL SECTION NUMBER

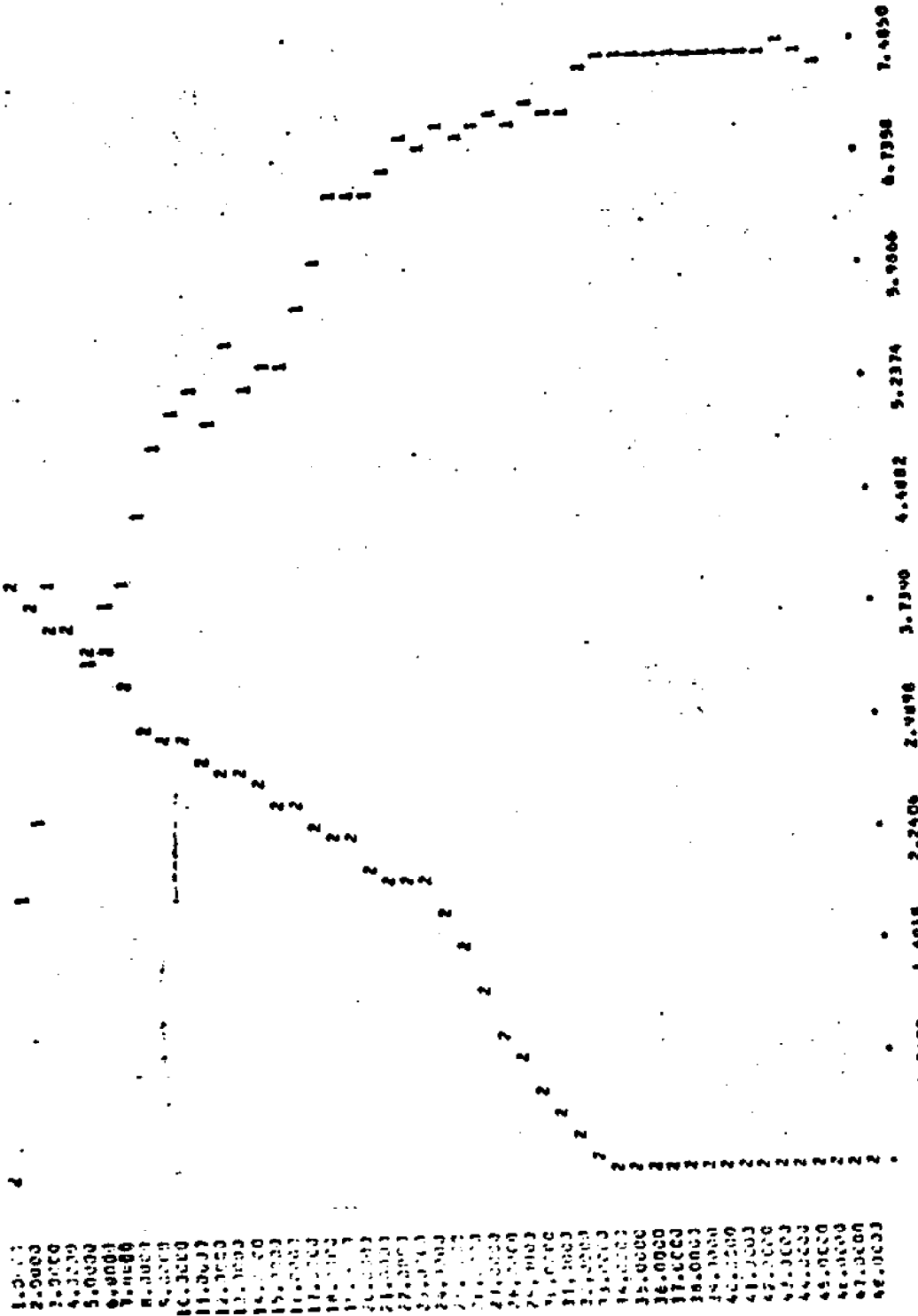


DIFFUSION COEFFICIENT FOR Z DIRECTION (FT/FT/SEC) STEP NUMBER = 50 TIME = 1.67HRS

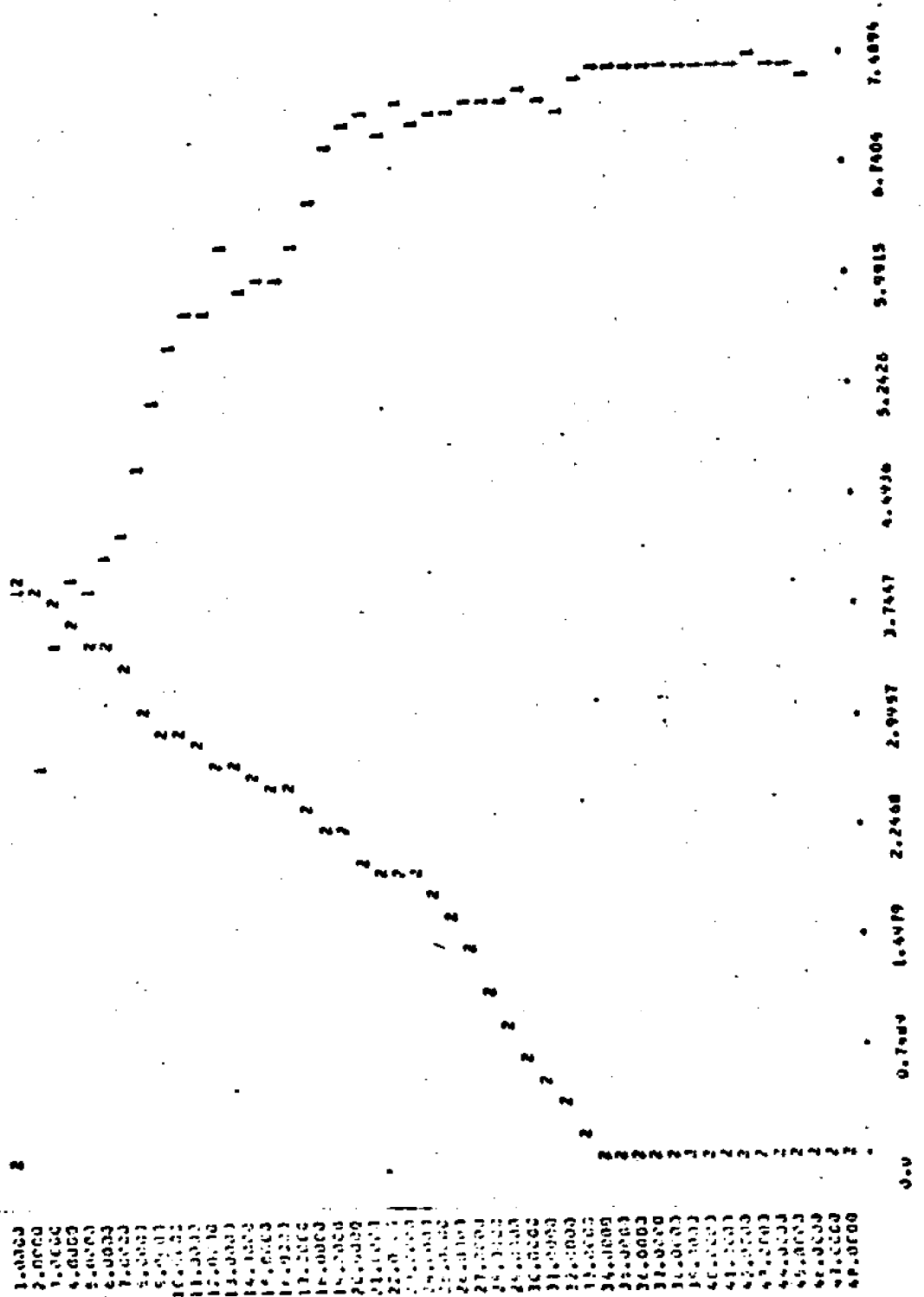
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
8	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
27	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
28	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
29	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
31	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
32	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
33	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
34	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
36	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
37	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
38	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
39	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
41	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
42	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
43	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
44	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
46	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
47	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
48	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

SURFACE OXYGEN SOLUBILITY (MG/L)
 3.0
 7.1717
 7.1848
 7.1891
 7.2025
 7.1532
 7.1916
 7.2017
 7.1926
 7.1922
 7.2058
 7.2102
 7.2054
 7.1511
 7.2214
 7.2316
 7.2445
 7.2561
 7.2352
 7.2512
 7.2745
 7.2839
 7.3051
 7.3146
 7.3265
 7.3311
 7.3314
 7.3302
 7.2924
 7.2619
 7.2921
 7.2911
 7.2919
 7.2579
 7.3027
 7.3171
 7.3315
 7.3508
 7.3512
 7.3402
 7.3451
 7.3351
 7.3374
 7.3452
 7.3457
 7.3457
 7.3452
 7.3452
 0.0

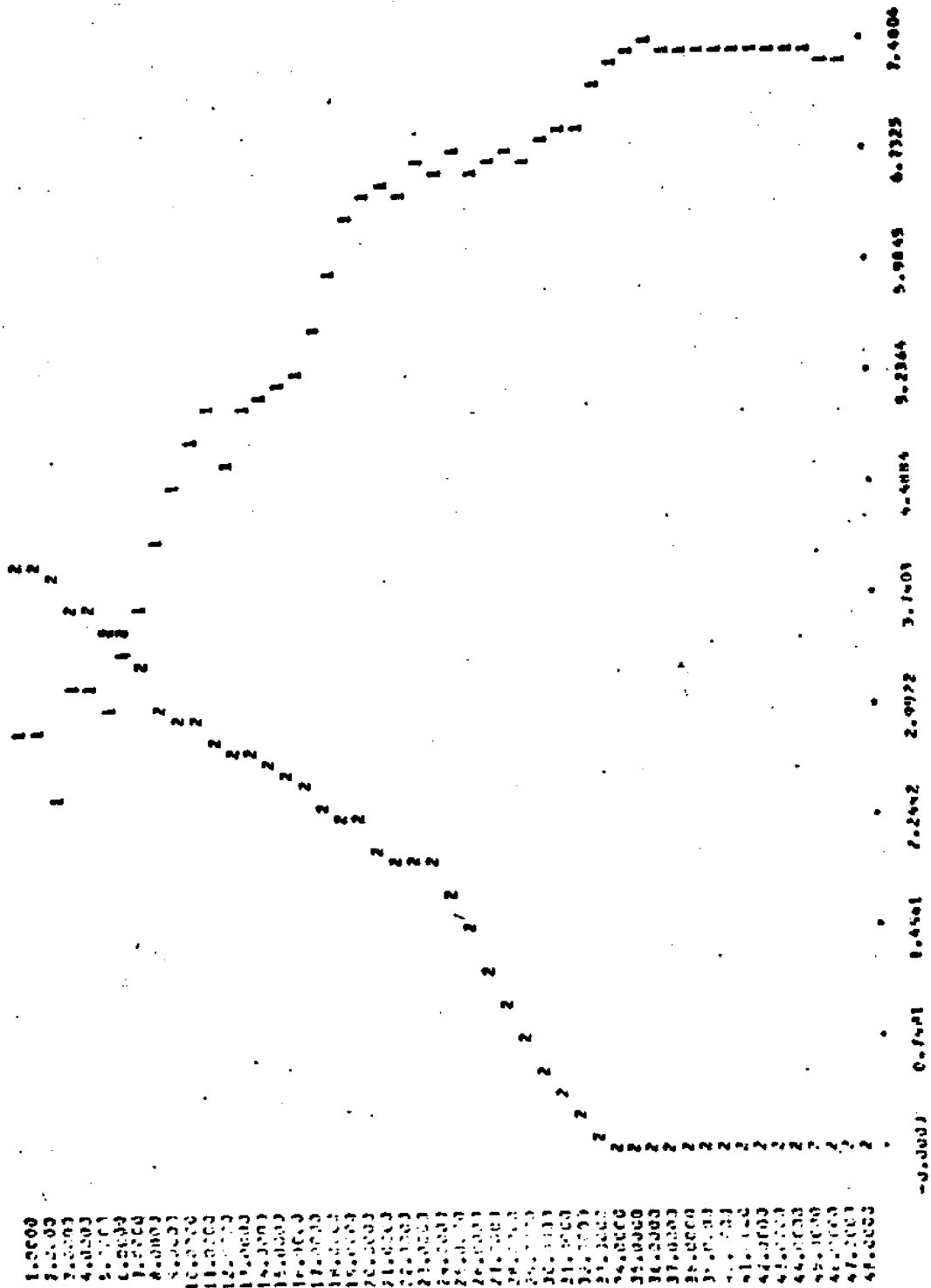
S.F. (11) S.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 14



C.P. 11) 8 C.A.U.R. (2) IN MO/L VS ESTILARY CONJUGATIONAL SECTION NUMBER
 CHART 15



AVERAGE D.O. (1) & B.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1



DISPERSION COEFFICIENTS FOR 2 DIRECTION (E/F) FT/SEC STEP NUMBER = 99 VINE # 3-304MS

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
7	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
8	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
9	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
10	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
11	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
12	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
13	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
14	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
15	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
16	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
17	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
18	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
19	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
20	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
21	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
22	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
23	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
24	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
25	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
26	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
27	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
28	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
29	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
30	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
31	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
32	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
33	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
34	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
35	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
36	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
37	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
38	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
39	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
40	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
41	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
42	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
43	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
44	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
45	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
46	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
47	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
48	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0

990 DECAY COEFFICIENTS & LOGCOOC (1/SEC)

STEP NUMBER = 99

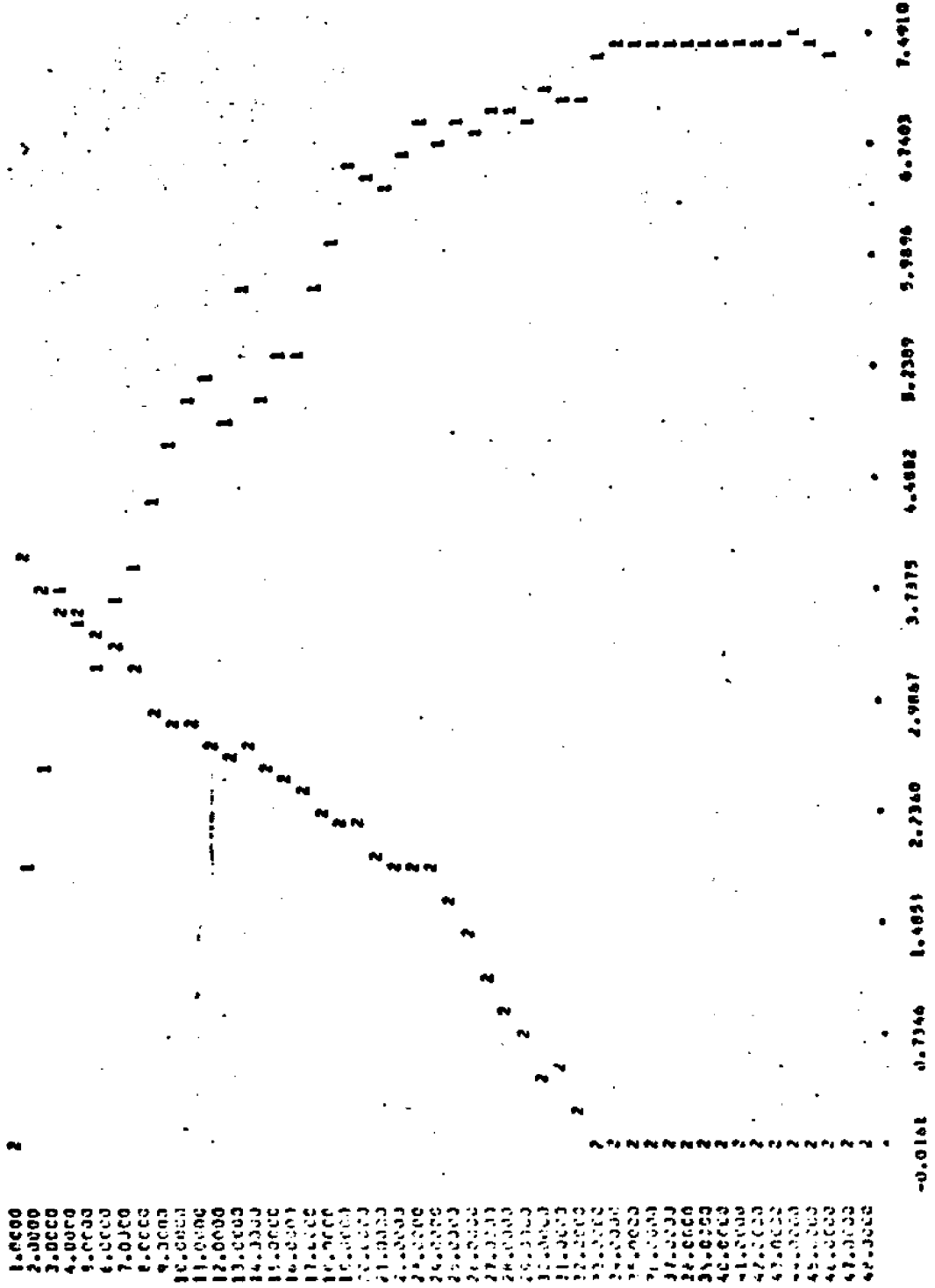
TIME = 3.30MS

STEP	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

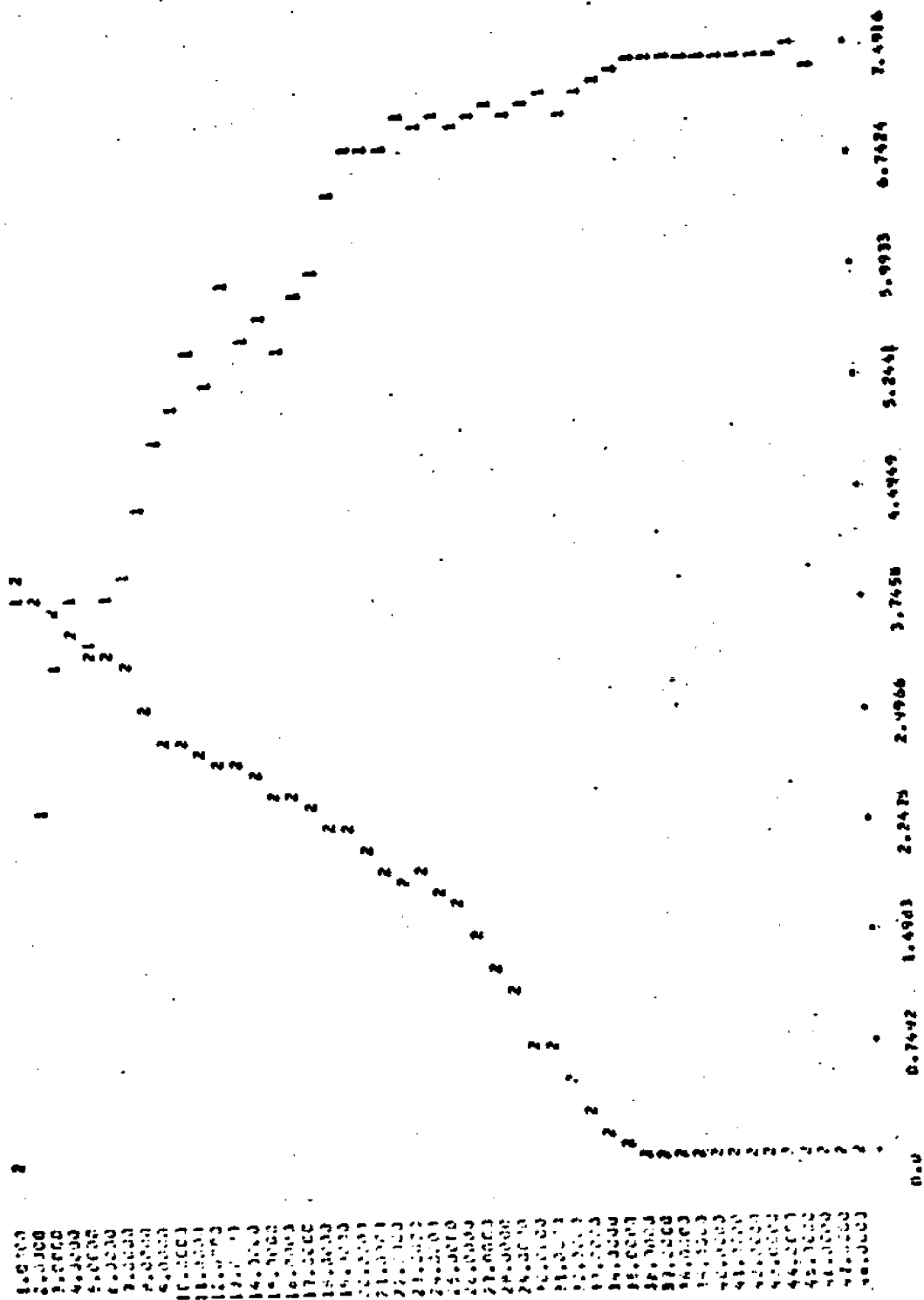
SURFACE OXYGEN SOLUBILITY (MG/L)
 O.C

7.1717
7.1648
7.1891
7.2029
7.1982
7.1574
7.2017
7.1624
7.1822
7.2058
7.2102
7.2094
7.1511
7.2214
7.2376
7.2462
7.2661
7.2297
7.2512
7.2764
7.2839
7.3051
7.3184
7.2709
7.3133
7.3534
7.3362
7.2579
7.2970
7.2531
7.2518
7.2585
7.2479
7.3027
7.3171
7.3115
7.3008
7.3412
7.3467
7.3257
7.3692
7.3754
7.3687
7.3692
7.3652
7.3682
0.C

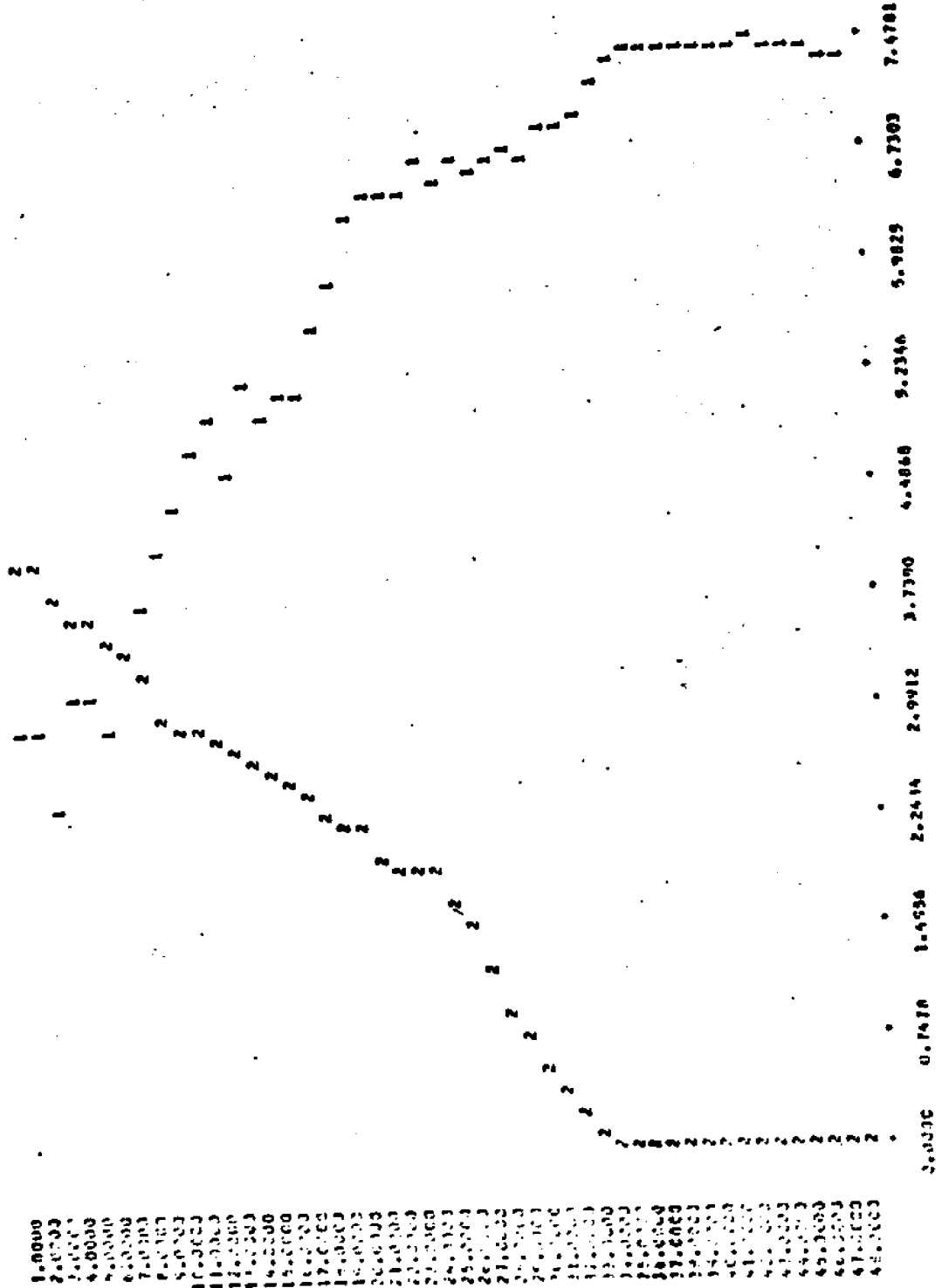
D.O. (1) & B.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 14

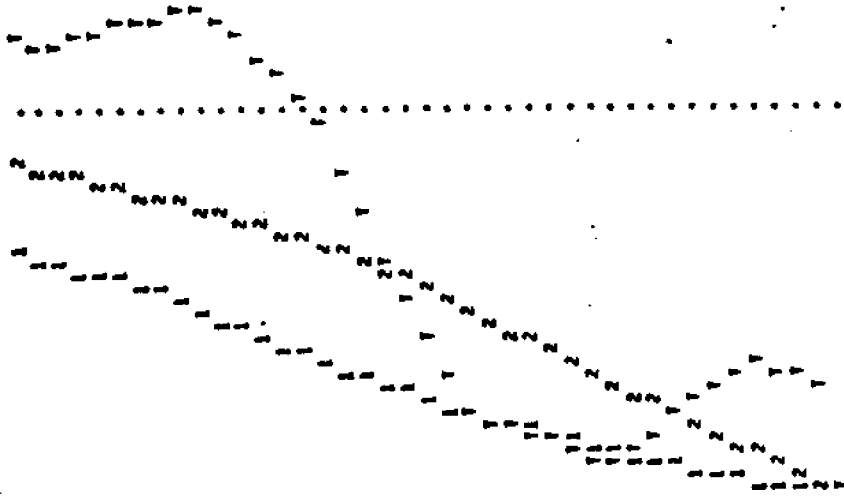


6.0. 111 1 6.0.0. 121 IN MEAL VS ESTLARY LONGITUDINAL SECTION NUMBER CHART IS

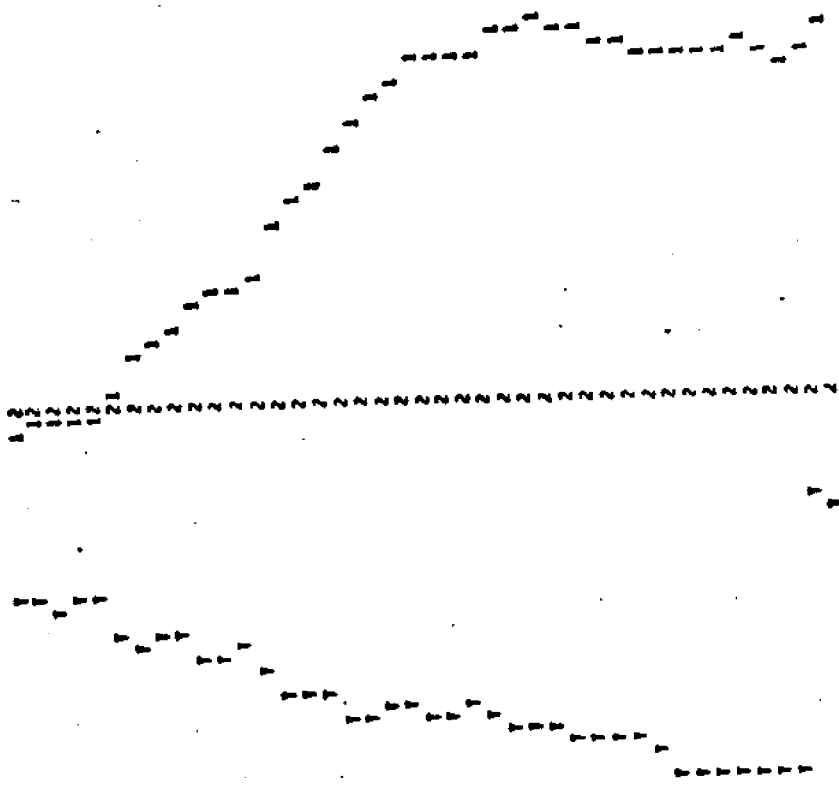


AVERAGE D.O. (1) & B.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1





59	3.80	1.21	0.69
60	3.30	1.21	0.67
61	3.79	1.50	0.07
62	3.79	3.50	0.08
63	3.79	3.50	0.69
64	3.79	3.50	0.69
65	3.79	1.50	0.69
66	3.79	1.50	0.10
67	3.79	1.50	0.10
68	3.79	3.50	0.10
69	3.79	3.50	0.09
70	3.79	1.49	0.09
71	3.79	1.49	0.09
72	3.79	1.49	0.09
73	3.79	1.49	0.09
74	3.79	1.49	0.09
75	3.79	1.49	0.09
76	3.79	1.49	0.09
77	3.79	1.49	0.09
78	3.79	1.49	0.09
79	3.79	1.49	0.09
80	3.79	1.49	0.09
81	3.79	1.49	0.09
82	3.79	1.49	0.09
83	3.79	1.49	0.09
84	3.79	1.49	0.09
85	3.79	1.49	0.09
86	3.79	1.49	0.09
87	3.79	1.49	0.09
88	3.79	1.49	0.09
89	3.79	1.49	0.09
90	3.79	1.49	0.09
91	3.79	1.49	0.09
92	3.79	1.49	0.09
93	3.79	1.49	0.09
94	3.79	1.49	0.09
95	3.79	1.49	0.09
96	3.79	1.49	0.09
97	3.79	1.49	0.09
98	3.79	1.49	0.09
99	3.79	1.49	0.09
100	3.79	1.49	0.09



59	7.49	-0.00
60	7.49	-0.33
61	7.49	-0.39
62	7.49	-0.43
63	7.49	-0.44
64	7.49	-0.42
65	7.49	-0.42
66	7.49	-0.46
67	7.49	-0.47
68	7.49	-0.48
69	7.49	-0.55
70	7.49	-0.54
71	7.49	-0.58
72	7.49	-0.59
73	7.49	-0.55
74	7.49	-0.56
75	7.49	-0.59
76	7.49	-0.59
77	7.49	-0.51
78	7.49	-0.39
79	7.49	-0.30
80	7.49	-0.30
81	7.49	-0.58
82	7.49	-0.60
83	7.49	-0.60
84	7.49	-0.61
85	7.49	-0.64
86	7.49	-0.63
87	7.49	-0.64
88	7.49	-0.63
89	7.49	-0.60
90	7.49	-0.63
91	7.49	-0.60
92	7.49	-0.72
93	7.49	-0.73
94	7.49	-0.71
95	7.49	-0.71
96	7.49	-0.70
97	7.49	-0.69
98	7.49	-0.60
99	7.49	-0.10

SAMPLE OUTPUT - TDLIDO
(DIMENSIONLESS VERTICAL AXIS MODEL)
CONSERVATIVE CASE

NN	AA	RRRRR	SSSSSS
NN	AAAA	RRRRRR	SSSSSSSS
NN	AA	RR	SS
NN	AA	RR	SS
NN	AA	RRRRR	SSSSSS
NN	AAAAAA	RRRRR	SSSSSS
NN	AAAAAA	RR	SS
NN	AA	RR	SS
NN	AA	RRRRR	SSSSSS
NN	AA	RRRRR	SSSSSS

DD	DD	RR	RR	DD
DD	DD	RR	RR	DD
DD	DD	RR	RR	DD
DD	DD	RR	RR	DD

PROGRAM DEVELOPED BY T. M. SPALDING
 UNIVERSITY OF PUERTO RICO, HATIE HALL 222C
 JUNE 1972

COMPUTATIONAL CONTROL NUMBERS

MIN	MAX	MIN	MAX
1	1132247	1	1132247
2	1132247	2	1132247
3	1132247	3	1132247
4	1132247	4	1132247
5	1132247	5	1132247
6	1132247	6	1132247
7	1132247	7	1132247
8	1132247	8	1132247
9	1132247	9	1132247
10	1132247	10	1132247
11	1132247	11	1132247
12	1132247	12	1132247
13	1132247	13	1132247
14	1132247	14	1132247
15	0	15	0
16	0	16	0
17	0	17	0
18	0	18	0
19	0	19	0
20	0	20	0
21	0	21	0
22	0	22	0
23	0	23	0
24	0	24	0
25	0	25	0
26	0	26	0
27	0	27	0
28	0	28	0
29	0	29	0
30	0	30	0
31	0	31	0
32	0	32	0
33	0	33	0
34	0	34	0
35	0	35	0
36	0	36	0
37	0	37	0
38	0	38	0
39	0	39	0
40	0	40	0
41	0	41	0
42	0	42	0
43	0	43	0
44	0	44	0
45	0	45	0
46	0	46	0
47	0	47	0
48	0	48	0

MIN = 15 MAX = 47

AVERAGE SECTION DEPTH FT.

1	6.600
2	6.600
3	6.600
4	12.200
5	17.300
6	22.300
7	19.500
8	21.800
9	19.000
10	17.100
11	15.600
12	17.100
13	22.000
14	19.400
15	17.600
16	19.700
17	21.900
18	23.600
19	19.600
20	19.200
21	20.500
22	17.900
23	26.500
24	26.700
25	24.800
26	27.400
27	31.600
28	32.900
29	31.900
30	31.600
31	33.500
32	31.500
33	31.600
34	35.700
35	37.500
36	36.700
37	41.800
38	42.600
39	40.800
40	47.000
41	44.800
42	44.800
43	49.300
44	49.800
45	54.600
46	67.600
47	67.100
48	65.500

U.S. GEOLOGICAL SURVEY
 LONGITUDINAL SECTION NUMBER
 CHART 34

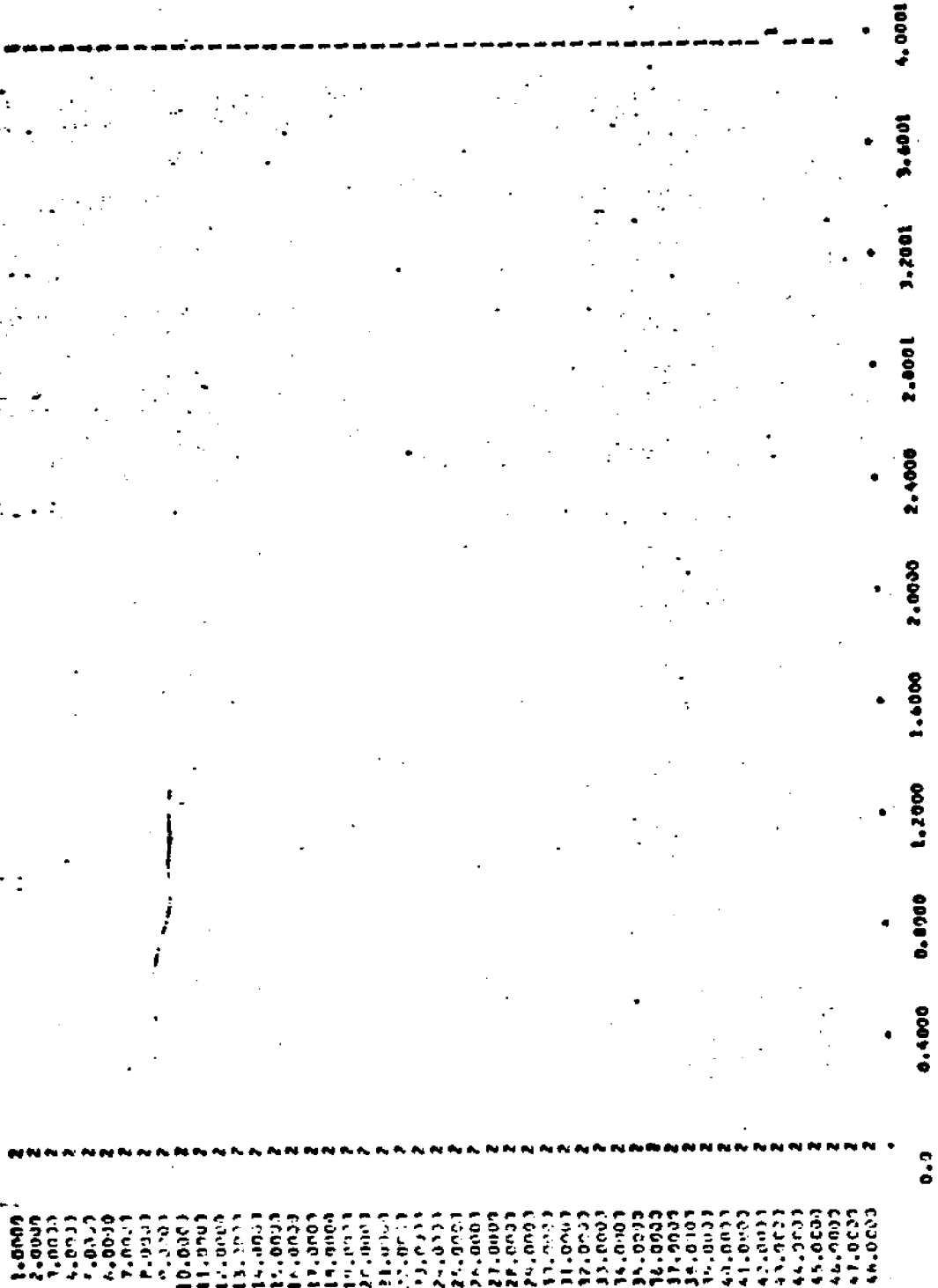
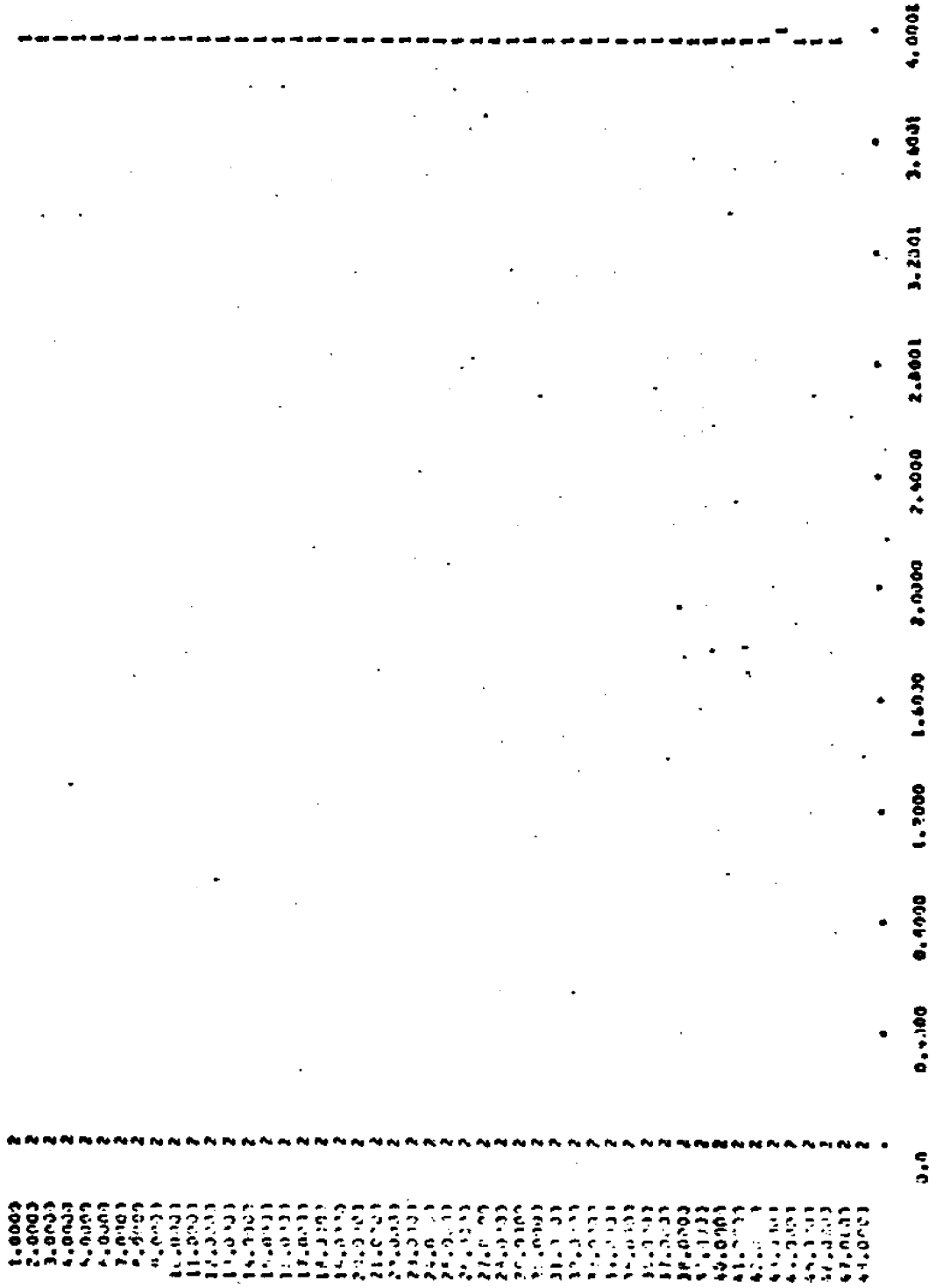
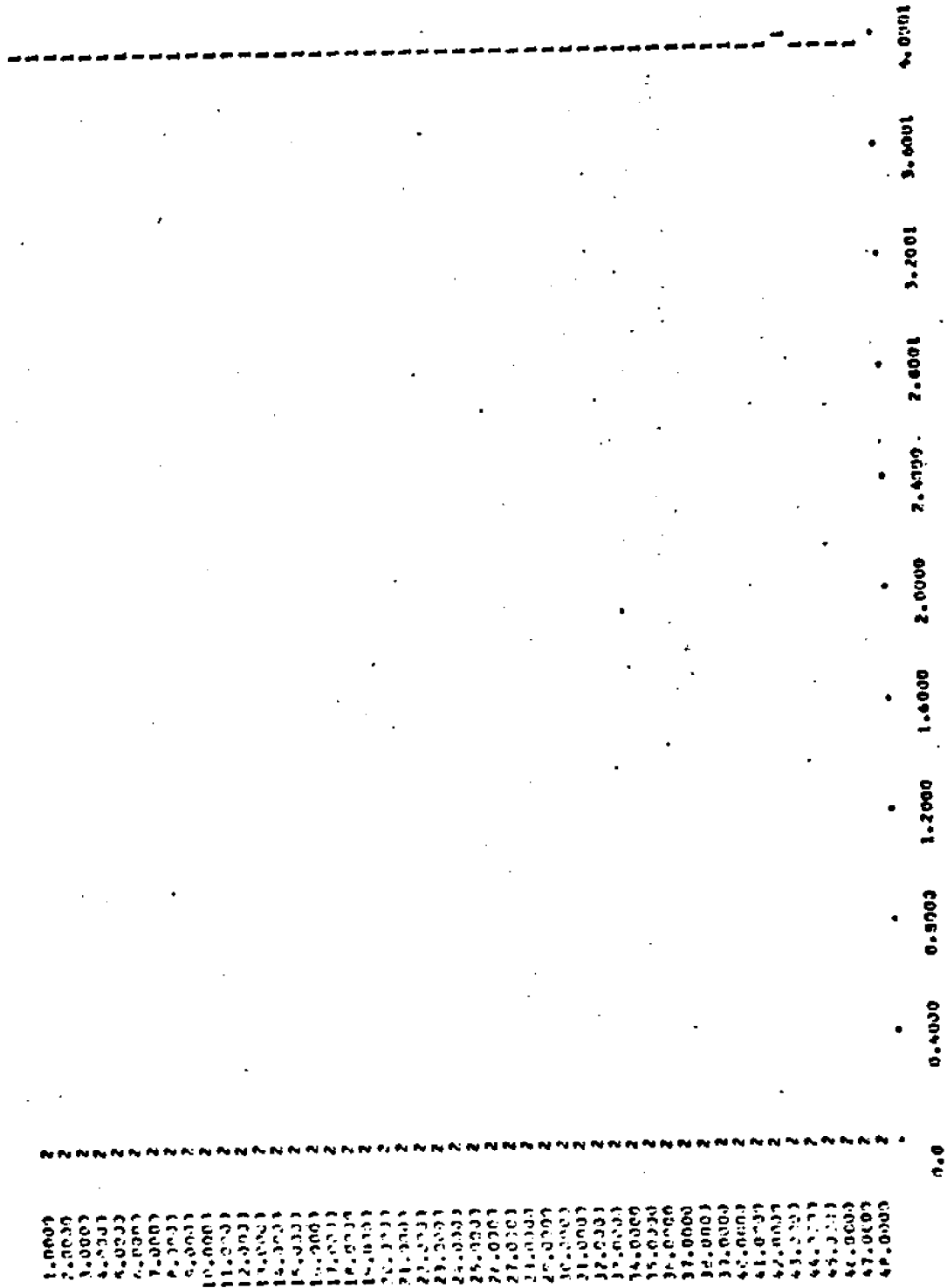


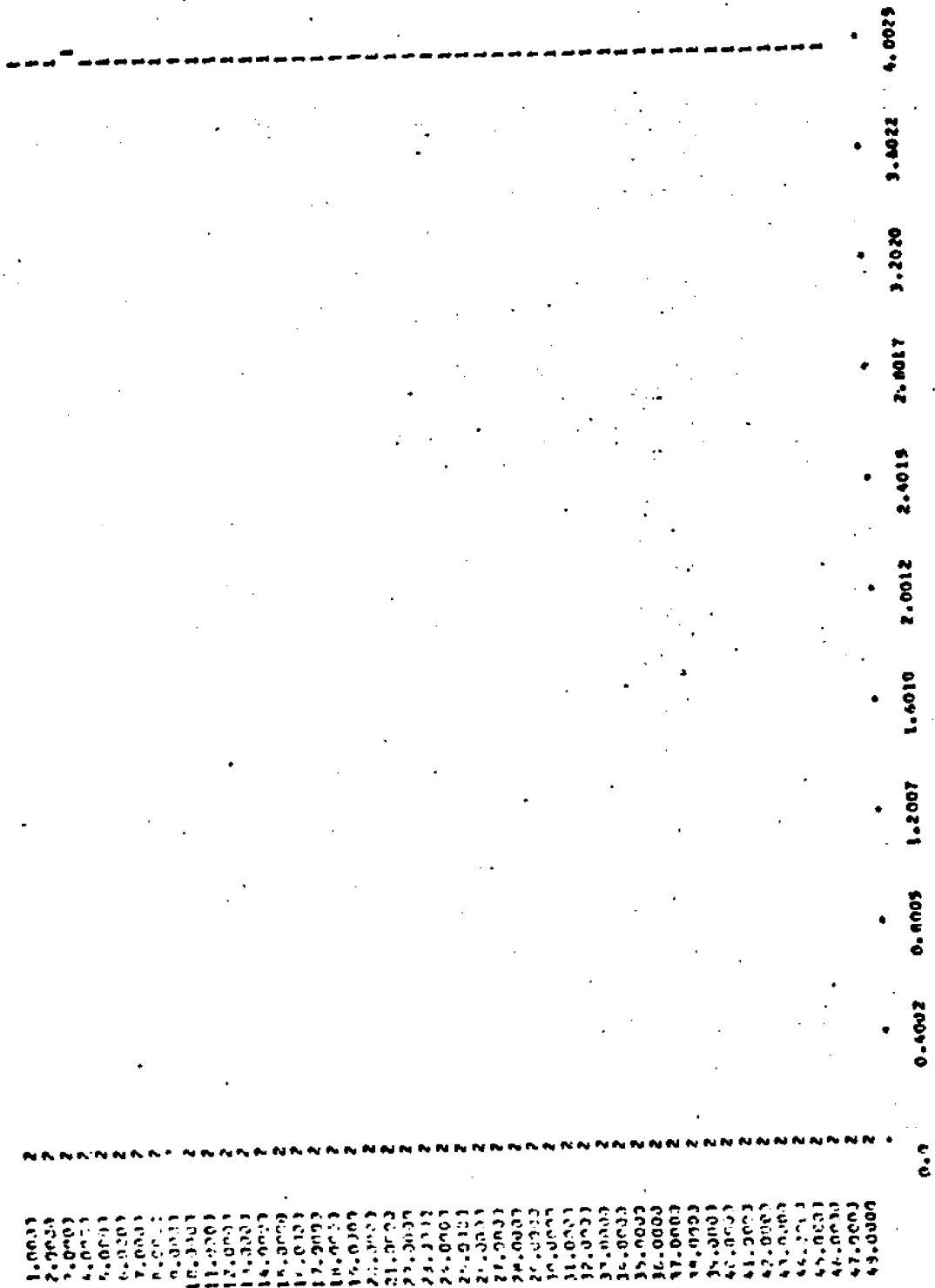
Fig. 111 - 4.0.0. (2) IN MG/L VS ESTIMATED LONGITUDINAL SECTION NUMBER
 CHART 15



AVERAGE D.O. (1) 9.0.0.0. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1



N.O. (1) & N.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 14



P.O. (11) & S.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 15

1.000	2	0.4002	0.5005	1.7007	1.8010	2.0012	2.4015	2.8017	3.2020	3.6022	4.0025
2.000	2										
3.000	2										
4.000	2										
5.000	2										
6.000	2										
7.000	2										
8.000	2										
9.000	2										
10.000	2										
11.000	2										
12.000	2										
13.000	2										
14.000	2										
15.000	2										
16.000	2										
17.000	2										
18.000	2										
19.000	2										
20.000	2										
21.000	2										
22.000	2										
23.000	2										
24.000	2										
25.000	2										
26.000	2										
27.000	2										
28.000	2										
29.000	2										
30.000	2										
31.000	2										
32.000	2										
33.000	2										
34.000	2										
35.000	2										
36.000	2										
37.000	2										
38.000	2										
39.000	2										
40.000	2										
41.000	2										
42.000	2										
43.000	2										
44.000	2										
45.000	2										
46.000	2										
47.000	2										
48.000	2										
49.000	2										
50.000	2										
51.000	2										
52.000	2										
53.000	2										
54.000	2										
55.000	2										
56.000	2										
57.000	2										
58.000	2										
59.000	2										
60.000	2										
61.000	2										
62.000	2										
63.000	2										
64.000	2										
65.000	2										
66.000	2										
67.000	2										
68.000	2										
69.000	2										
70.000	2										
71.000	2										
72.000	2										
73.000	2										
74.000	2										
75.000	2										
76.000	2										
77.000	2										
78.000	2										
79.000	2										
80.000	2										
81.000	2										
82.000	2										
83.000	2										
84.000	2										
85.000	2										
86.000	2										
87.000	2										
88.000	2										
89.000	2										
90.000	2										
91.000	2										
92.000	2										
93.000	2										
94.000	2										
95.000	2										
96.000	2										
97.000	2										
98.000	2										
99.000	2										
100.000	2										

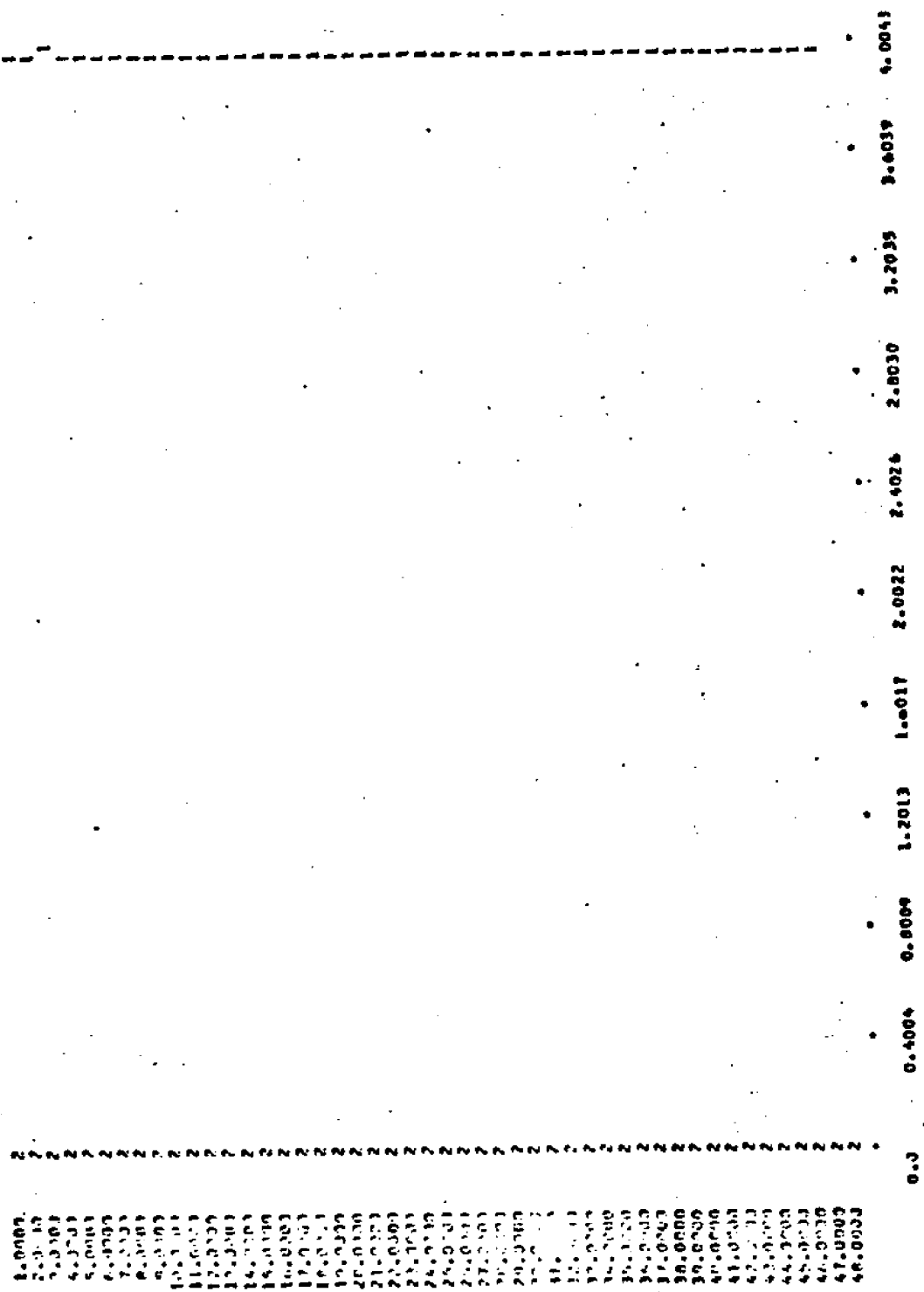
APPROX. 0.2 (1) & 0.000 (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1

1.0001	2	0.4002	0.4005	1.2007	1.4010	2.0012	2.4015	2.6017	3.2020	3.6022	4.0024
2.0002	2										
3.0003	2										
4.0004	2										
5.0005	2										
6.0006	2										
7.0007	2										
8.0008	2										
9.0009	2										
10.0010	2										
11.0011	2										
12.0012	2										
13.0013	2										
14.0014	2										
15.0015	2										
16.0016	2										
17.0017	2										
18.0018	2										
19.0019	2										
20.0020	2										
21.0021	2										
22.0022	2										
23.0023	2										
24.0024	2										
25.0025	2										
26.0026	2										
27.0027	2										
28.0028	2										
29.0029	2										
30.0030	2										
31.0031	2										
32.0032	2										
33.0033	2										
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36.0036	2										
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38.0038	2										
39.0039	2										
40.0040	2										
41.0041	2										
42.0042	2										
43.0043	2										
44.0044	2										
45.0045	2										
46.0046	2										
47.0047	2										
48.0048	2										
49.0049	2										
50.0050	2										
51.0051	2										
52.0052	2										
53.0053	2										
54.0054	2										
55.0055	2										
56.0056	2										
57.0057	2										
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59.0059	2										
60.0060	2										
61.0061	2										
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63.0063	2										
64.0064	2										
65.0065	2										
66.0066	2										
67.0067	2										
68.0068	2										
69.0069	2										
70.0070	2										
71.0071	2										
72.0072	2										
73.0073	2										
74.0074	2										
75.0075	2										
76.0076	2										
77.0077	2										
78.0078	2										
79.0079	2										
80.0080	2										
81.0081	2										
82.0082	2										
83.0083	2										
84.0084	2										
85.0085	2										
86.0086	2										
87.0087	2										
88.0088	2										
89.0089	2										
90.0090	2										
91.0091	2										
92.0092	2										
93.0093	2										
94.0094	2										
95.0095	2										
96.0096	2										
97.0097	2										
98.0098	2										
99.0099	2										
100.0100	2										

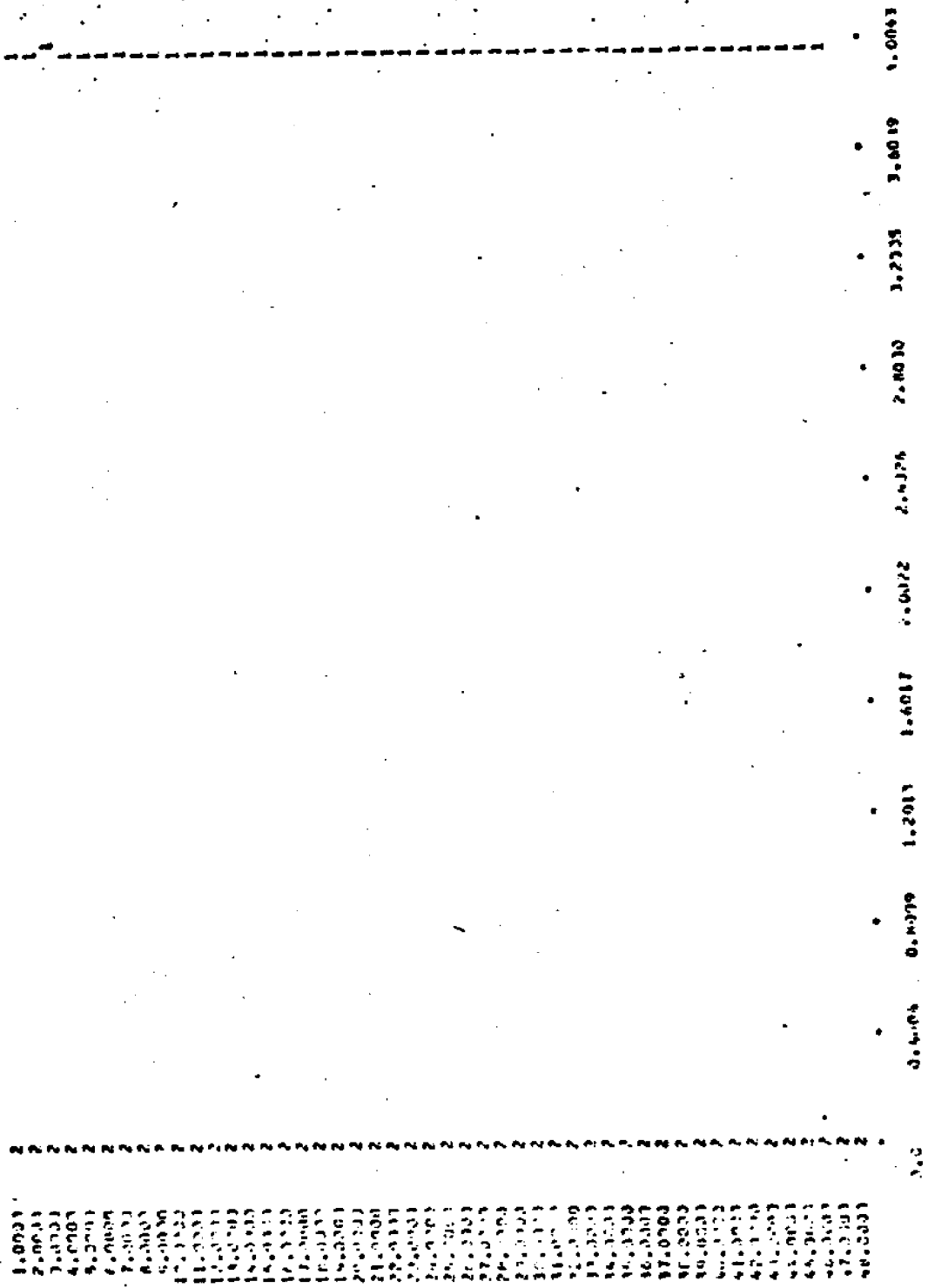
DISPERSION COEFFICIENT FOR Z DIRECTION IFT OF F/SECI STEP NUMBER = 99 TIME = 13.20483

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	0.0002	0.0013	0.0031	0.0056	0.0087	0.0119	0.0154	0.0191	0.0229	0.0268	0.0308	0.0348	0.0388	0.0428	0.0468	0.0508
2	0.0003	0.0017	0.0041	0.0075	0.0110	0.0145	0.0180	0.0215	0.0250	0.0285	0.0320	0.0355	0.0390	0.0425	0.0460	0.0495
3	0.0004	0.0022	0.0052	0.0095	0.0138	0.0181	0.0224	0.0267	0.0310	0.0353	0.0396	0.0439	0.0482	0.0525	0.0568	0.0611
4	0.0005	0.0027	0.0063	0.0109	0.0154	0.0200	0.0245	0.0290	0.0335	0.0380	0.0425	0.0470	0.0515	0.0560	0.0605	0.0650
5	0.0006	0.0031	0.0073	0.0121	0.0166	0.0211	0.0256	0.0301	0.0346	0.0391	0.0436	0.0481	0.0526	0.0571	0.0616	0.0661
6	0.0007	0.0036	0.0083	0.0133	0.0178	0.0223	0.0268	0.0313	0.0358	0.0403	0.0448	0.0493	0.0538	0.0583	0.0628	0.0673
7	0.0008	0.0041	0.0093	0.0145	0.0189	0.0234	0.0279	0.0324	0.0369	0.0414	0.0459	0.0504	0.0549	0.0594	0.0639	0.0684
8	0.0009	0.0045	0.0100	0.0154	0.0200	0.0245	0.0290	0.0335	0.0380	0.0425	0.0470	0.0515	0.0560	0.0605	0.0650	0.0695
9	0.0010	0.0049	0.0106	0.0161	0.0207	0.0252	0.0297	0.0342	0.0387	0.0432	0.0477	0.0522	0.0567	0.0612	0.0657	0.0702
10	0.0011	0.0052	0.0111	0.0167	0.0213	0.0259	0.0305	0.0351	0.0397	0.0443	0.0489	0.0535	0.0581	0.0627	0.0673	0.0719
11	0.0012	0.0056	0.0117	0.0174	0.0220	0.0266	0.0312	0.0358	0.0404	0.0450	0.0496	0.0542	0.0588	0.0634	0.0680	0.0726
12	0.0013	0.0060	0.0123	0.0181	0.0227	0.0273	0.0319	0.0365	0.0411	0.0457	0.0503	0.0549	0.0595	0.0641	0.0687	0.0733
13	0.0014	0.0064	0.0128	0.0187	0.0233	0.0279	0.0325	0.0371	0.0417	0.0463	0.0509	0.0555	0.0601	0.0647	0.0693	0.0739
14	0.0015	0.0068	0.0134	0.0194	0.0239	0.0285	0.0331	0.0377	0.0423	0.0469	0.0515	0.0561	0.0607	0.0653	0.0699	0.0745
15	0.0016	0.0072	0.0140	0.0201	0.0246	0.0292	0.0338	0.0384	0.0430	0.0476	0.0522	0.0568	0.0614	0.0660	0.0706	0.0752
16	0.0017	0.0076	0.0146	0.0207	0.0252	0.0298	0.0344	0.0390	0.0436	0.0482	0.0528	0.0574	0.0620	0.0666	0.0712	0.0758
17	0.0018	0.0080	0.0152	0.0213	0.0258	0.0304	0.0350	0.0396	0.0442	0.0488	0.0534	0.0580	0.0626	0.0672	0.0718	0.0764
18	0.0019	0.0084	0.0158	0.0219	0.0264	0.0310	0.0356	0.0402	0.0448	0.0494	0.0540	0.0586	0.0632	0.0678	0.0724	0.0770
19	0.0020	0.0088	0.0163	0.0224	0.0269	0.0315	0.0361	0.0407	0.0453	0.0499	0.0545	0.0591	0.0637	0.0683	0.0729	0.0775
20	0.0021	0.0092	0.0168	0.0229	0.0274	0.0320	0.0366	0.0412	0.0458	0.0504	0.0550	0.0596	0.0642	0.0688	0.0734	0.0780
21	0.0022	0.0096	0.0173	0.0234	0.0279	0.0325	0.0371	0.0417	0.0463	0.0509	0.0555	0.0601	0.0647	0.0693	0.0739	0.0785
22	0.0023	0.0099	0.0178	0.0239	0.0284	0.0330	0.0376	0.0422	0.0468	0.0514	0.0560	0.0606	0.0652	0.0698	0.0744	0.0790
23	0.0024	0.0103	0.0183	0.0244	0.0289	0.0335	0.0381	0.0427	0.0473	0.0519	0.0565	0.0611	0.0657	0.0703	0.0749	0.0795
24	0.0025	0.0107	0.0188	0.0249	0.0294	0.0340	0.0386	0.0432	0.0478	0.0524	0.0570	0.0616	0.0662	0.0708	0.0754	0.0800
25	0.0026	0.0111	0.0192	0.0253	0.0298	0.0344	0.0390	0.0436	0.0482	0.0528	0.0574	0.0620	0.0666	0.0712	0.0758	0.0804
26	0.0027	0.0115	0.0196	0.0257	0.0302	0.0348	0.0394	0.0440	0.0486	0.0532	0.0578	0.0624	0.0670	0.0716	0.0762	0.0808
27	0.0028	0.0119	0.0200	0.0261	0.0306	0.0352	0.0398	0.0444	0.0490	0.0536	0.0582	0.0628	0.0674	0.0720	0.0766	0.0812
28	0.0029	0.0123	0.0204	0.0265	0.0310	0.0356	0.0402	0.0448	0.0494	0.0540	0.0586	0.0632	0.0678	0.0724	0.0770	0.0816
29	0.0030	0.0127	0.0208	0.0269	0.0314	0.0360	0.0406	0.0452	0.0498	0.0544	0.0590	0.0636	0.0682	0.0728	0.0774	0.0820
30	0.0031	0.0131	0.0212	0.0273	0.0318	0.0364	0.0410	0.0456	0.0502	0.0548	0.0594	0.0640	0.0686	0.0732	0.0778	0.0824
31	0.0032	0.0135	0.0216	0.0277	0.0322	0.0368	0.0414	0.0460	0.0506	0.0552	0.0598	0.0644	0.0690	0.0736	0.0782	0.0828
32	0.0033	0.0139	0.0220	0.0281	0.0326	0.0372	0.0418	0.0464	0.0510	0.0556	0.0602	0.0648	0.0694	0.0740	0.0786	0.0832
33	0.0034	0.0143	0.0224	0.0285	0.0330	0.0376	0.0422	0.0468	0.0514	0.0560	0.0606	0.0652	0.0698	0.0744	0.0790	0.0836
34	0.0035	0.0147	0.0228	0.0289	0.0334	0.0380	0.0426	0.0472	0.0518	0.0564	0.0610	0.0656	0.0702	0.0748	0.0794	0.0840
35	0.0036	0.0151	0.0232	0.0293	0.0338	0.0384	0.0430	0.0476	0.0522	0.0568	0.0614	0.0660	0.0706	0.0752	0.0798	0.0844
36	0.0037	0.0155	0.0236	0.0297	0.0342	0.0388	0.0434	0.0480	0.0526	0.0572	0.0618	0.0664	0.0710	0.0756	0.0802	0.0848
37	0.0038	0.0159	0.0240	0.0301	0.0346	0.0392	0.0438	0.0484	0.0530	0.0576	0.0622	0.0668	0.0714	0.0760	0.0806	0.0852
38	0.0039	0.0163	0.0244	0.0305	0.0350	0.0396	0.0442	0.0488	0.0534	0.0580	0.0626	0.0672	0.0718	0.0764	0.0810	0.0856
39	0.0040	0.0167	0.0248	0.0309	0.0354	0.0400	0.0446	0.0492	0.0538	0.0584	0.0630	0.0676	0.0722	0.0768	0.0814	0.0860
40	0.0041	0.0171	0.0252	0.0313	0.0358	0.0404	0.0450	0.0496	0.0542	0.0588	0.0634	0.0680	0.0726	0.0772	0.0818	0.0864
41	0.0042	0.0175	0.0256	0.0317	0.0362	0.0408	0.0454	0.0500	0.0546	0.0592	0.0638	0.0684	0.0730	0.0776	0.0822	0.0868
42	0.0043	0.0179	0.0260	0.0321	0.0366	0.0412	0.0458	0.0504	0.0550	0.0596	0.0642	0.0688	0.0734	0.0780	0.0826	0.0872
43	0.0044	0.0183	0.0264	0.0325	0.0370	0.0416	0.0462	0.0508	0.0554	0.0600	0.0646	0.0692	0.0738	0.0784	0.0830	0.0876
44	0.0045	0.0187	0.0268	0.0329	0.0374	0.0420	0.0466	0.0512	0.0558	0.0604	0.0650	0.0696	0.0742	0.0788	0.0834	0.0880
45	0.0046	0.0191	0.0272	0.0333	0.0378	0.0424	0.0470	0.0516	0.0562	0.0608	0.0654	0.0700	0.0746	0.0792	0.0838	0.0884
46	0.0047	0.0195	0.0276	0.0337	0.0382	0.0428	0.0474	0.0520	0.0566	0.0612	0.0658	0.0704	0.0750	0.0796	0.0842	0.0888
47	0.0048	0.0199	0.0280	0.0341	0.0386	0.0432	0.0478	0.0524	0.0570	0.0616	0.0662	0.0708	0.0754	0.0800	0.0846	0.0892
48	0.0049	0.0203	0.0284	0.0345	0.0390	0.0436	0.0482	0.0528	0.0574	0.0620	0.0666	0.0712	0.0758	0.0804	0.0850	0.0896

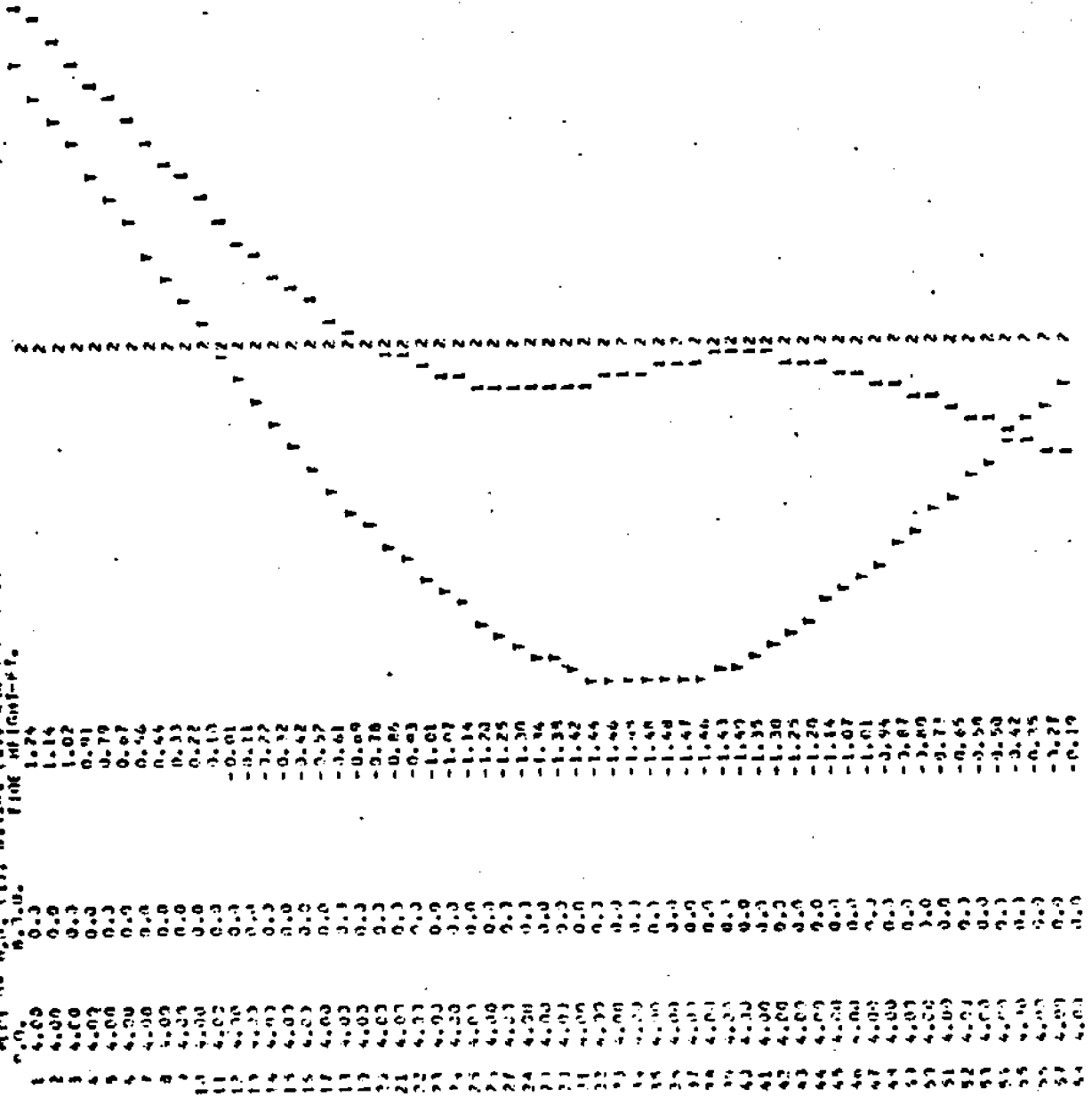
U.O. (1) & S.O.O. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 14

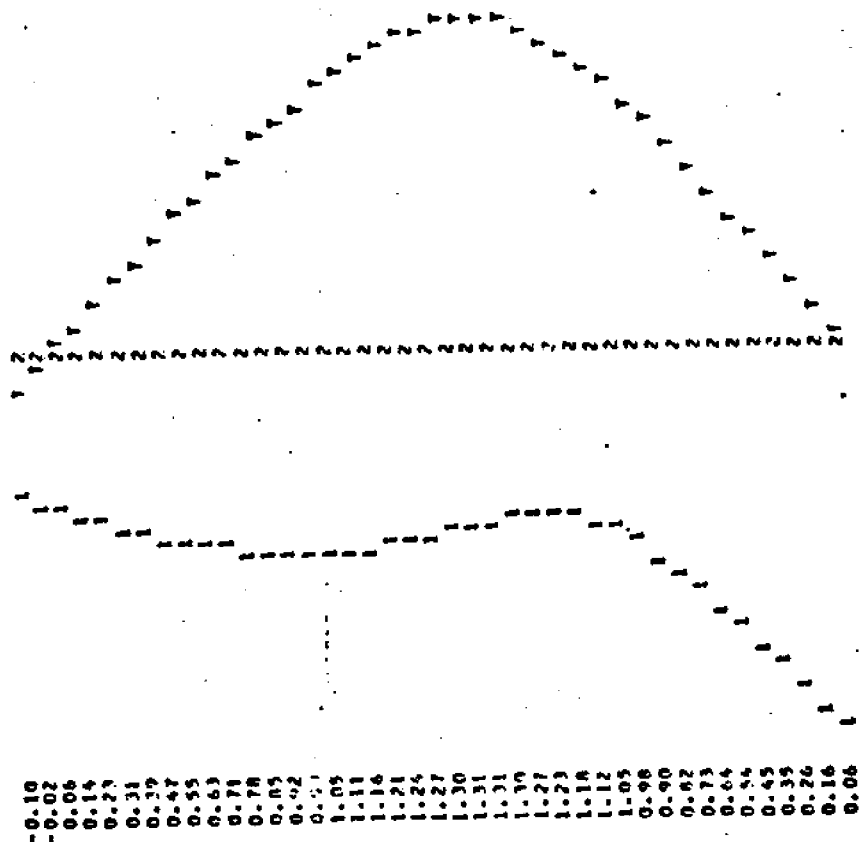


W.C. 111 E W.C.O. 121 IN MG/L VS STUDY LONGITUDINAL SECTION NUMBER CHART 15



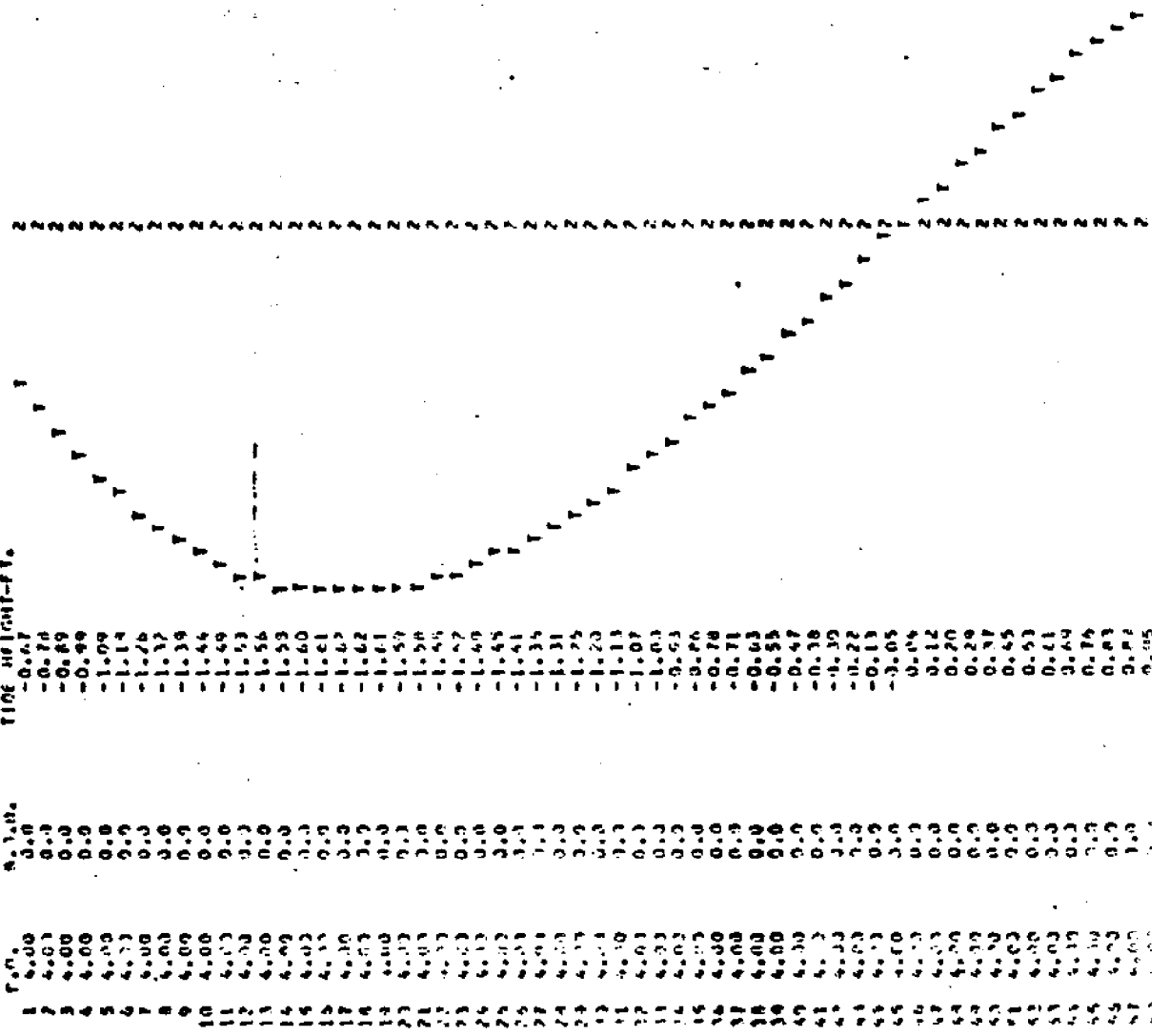
PLT 10 0.1, (1), N.O.P., (2), AND TIME HEIGHT (T) FROM GRID MEAN No 7 TIME STEP= 0.10 (MS.)





59	4.00	0.00
60	4.00	0.00
61	4.00	0.00
62	4.00	0.00
63	4.00	0.00
64	4.00	0.00
65	4.00	0.00
66	4.00	0.00
67	4.00	0.00
68	4.00	0.00
69	4.00	0.00
70	4.00	0.00
71	4.00	0.00
72	4.00	0.00
73	4.00	0.00
74	4.00	0.00
75	4.00	0.00
76	4.00	0.00
77	4.00	0.00
78	4.00	0.00
79	4.00	0.00
80	4.00	0.00
81	4.00	0.00
82	4.00	0.00
83	4.00	0.00
84	4.00	0.00
85	4.00	0.00
86	4.00	0.00
87	4.00	0.00
88	4.00	0.00
89	4.00	0.00
90	4.00	0.00
91	4.00	0.00
92	4.00	0.00
93	4.00	0.00
94	4.00	0.00
95	4.00	0.00
96	4.00	0.00
97	4.00	0.00
98	4.00	0.00
99	4.00	0.00
00	4.00	0.00

PLOT OF P.O. (1), 129, AND TIDE HEIGHT (T) FOR GRID N-14
 TIME HEIGHT-FT.



SAMPLE OUTPUT - TDLIDO
(DIMENSIONLESS VERTICAL AXIS MODEL)

D.O. - B.O.D. CASE

```

NN  NY  AA  NNMMN  SSSSS
NN  NY  AAAA  SSSSSSS
NNN  NN  AA  A3  RR  RR  SS
NNN  NN  AA  A4  RR  RR  SS
NNNN  NN  AA  RRMMR  SSSSSS
NN  NN  NY  AAAAAA  RRMMR  SSSSSS
NN  NY  NY  AAAAAA  RR  RR  SS
NN  NY  AA  AA  RRMMR  SSSSSS
NN  NY  AA  AA  RRMMR  SSSSSS

```

```

NN  NY  RR  NY  RR
O  O  O  --  RR  O  O  O
O  O  O  O  RR  O  O  O
O  O  O  O  RR  O  O  O

```

PROGRAM DEVELOPED BY W. S. SPILLING
UNIVERSITY OF PITTSBURGH WALSLEY HALL Z22C
JUNE 1972

COMPUTATIONAL CONTROL NUMBERS

MIN	MAX	MIN	MAX
1	1111247	29215	0
2	1120247	30215	0
3	1134247	40215	0
4	1150247	50215	0
5	1168247	60215	0
6	1187247	70215	0
7	1207247	80215	0
8	1228247	90215	0
9	1250247	100215	0
10	1273247	110215	0
11	1297247	120215	0
12	1322247	130215	0
13	1348247	140215	0
14	1375247	150215	0
15	1403247	160215	0
16	1432247	170215	0
17	1462247	180215	0
18	1493247	190215	0
19	1525247	200215	0
20	1558247	210215	0
21	1592247	220215	0
22	1627247	230215	0
23	1663247	240215	0
24	1700247	250215	0
25	1738247	260215	0
26	1777247	270215	0
27	1817247	280215	0
28	1858247	290215	0
29	1900247	300215	0
30	1943247	310215	0
31	1987247	320215	0
32	2032247	330215	0
33	2078247	340215	0
34	2125247	350215	0
35	2173247	360215	0
36	2222247	370215	0
37	2272247	380215	0
38	2323247	390215	0
39	2375247	400215	0
40	2428247	410215	0
41	2482247	420215	0
42	2537247	430215	0
43	2593247	440215	0
44	2650247	450215	0
45	2708247	460215	0
46	2767247	470215	0
47	2827247	480215	0
48	2888247	490215	0
49	2950247	500215	0

INITIAL CONCENTRATION (PPM/L)

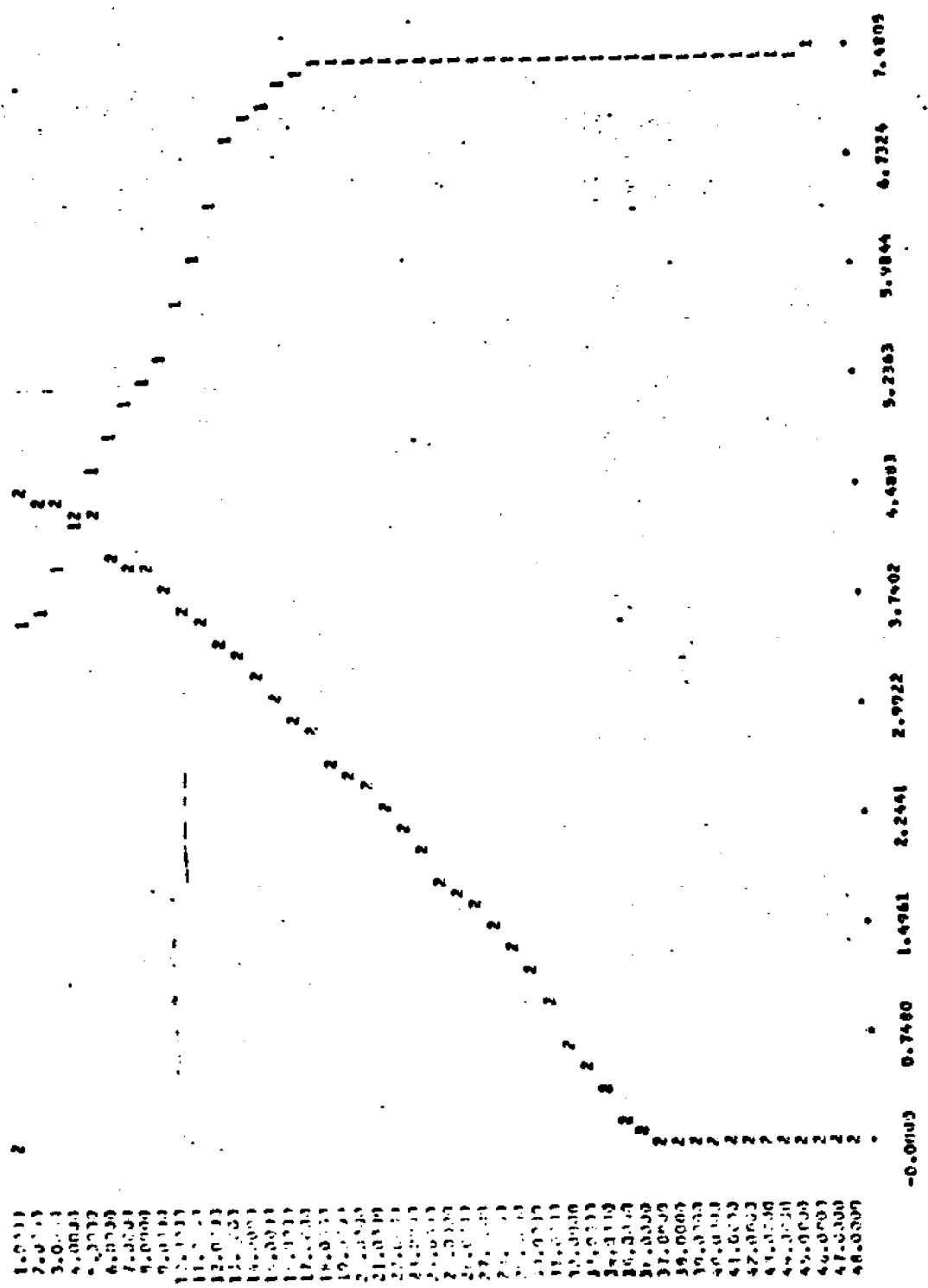
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.0	1.4	1.4	1.4	1.4	1.4	2.2	2.5	2.8	2.9	3.0	3.0	3.0	3.0	3.0	3.0
3	0.0	1.7	1.7	1.7	1.7	2.2	2.5	2.8	2.9	3.0	3.0	3.0	3.0	3.0	3.0	3.0
4	0.0	2.0	2.0	2.0	2.0	2.0	3.0	3.3	3.7	3.9	4.0	4.0	4.0	4.0	4.0	4.0
5	0.0	2.3	2.3	2.3	2.3	2.3	3.3	3.7	4.0	4.1	4.1	4.1	4.1	4.1	4.1	4.1
6	0.0	2.6	2.6	2.6	2.6	2.6	3.6	4.0	4.3	4.4	4.4	4.4	4.4	4.4	4.4	4.4
7	0.0	2.9	2.9	2.9	2.9	2.9	3.9	4.3	4.6	4.7	4.7	4.7	4.7	4.7	4.7	4.7
8	0.0	3.2	3.2	3.2	3.2	3.2	4.2	4.6	4.9	5.0	5.0	5.0	5.0	5.0	5.0	5.0
9	0.0	3.5	3.5	3.5	3.5	3.5	4.5	4.9	5.2	5.3	5.3	5.3	5.3	5.3	5.3	5.3
10	0.0	3.8	3.8	3.8	3.8	3.8	4.8	5.2	5.5	5.6	5.6	5.6	5.6	5.6	5.6	5.6
11	0.0	4.1	4.1	4.1	4.1	4.1	5.1	5.5	5.8	5.9	5.9	5.9	5.9	5.9	5.9	5.9
12	0.0	4.4	4.4	4.4	4.4	4.4	5.4	5.8	6.1	6.2	6.2	6.2	6.2	6.2	6.2	6.2
13	0.0	4.7	4.7	4.7	4.7	4.7	5.7	6.1	6.4	6.5	6.5	6.5	6.5	6.5	6.5	6.5
14	0.0	5.0	5.0	5.0	5.0	5.0	6.0	6.4	6.7	6.8	6.8	6.8	6.8	6.8	6.8	6.8
15	0.0	5.3	5.3	5.3	5.3	5.3	6.3	6.7	7.0	7.1	7.1	7.1	7.1	7.1	7.1	7.1
16	0.0	5.6	5.6	5.6	5.6	5.6	6.6	7.0	7.3	7.4	7.4	7.4	7.4	7.4	7.4	7.4
17	0.0	5.9	5.9	5.9	5.9	5.9	6.9	7.3	7.6	7.7	7.7	7.7	7.7	7.7	7.7	7.7
18	0.0	6.2	6.2	6.2	6.2	6.2	7.2	7.6	7.9	8.0	8.0	8.0	8.0	8.0	8.0	8.0
19	0.0	6.5	6.5	6.5	6.5	6.5	7.5	7.9	8.2	8.3	8.3	8.3	8.3	8.3	8.3	8.3
20	0.0	6.8	6.8	6.8	6.8	6.8	7.8	8.2	8.5	8.6	8.6	8.6	8.6	8.6	8.6	8.6
21	0.0	7.1	7.1	7.1	7.1	7.1	8.1	8.5	8.8	8.9	8.9	8.9	8.9	8.9	8.9	8.9
22	0.0	7.4	7.4	7.4	7.4	7.4	8.4	8.8	9.1	9.2	9.2	9.2	9.2	9.2	9.2	9.2
23	0.0	7.7	7.7	7.7	7.7	7.7	8.7	9.1	9.4	9.5	9.5	9.5	9.5	9.5	9.5	9.5
24	0.0	8.0	8.0	8.0	8.0	8.0	9.0	9.4	9.7	9.8	9.8	9.8	9.8	9.8	9.8	9.8
25	0.0	8.3	8.3	8.3	8.3	8.3	9.3	9.7	10.0	10.1	10.1	10.1	10.1	10.1	10.1	10.1
26	0.0	8.6	8.6	8.6	8.6	8.6	9.6	10.0	10.3	10.4	10.4	10.4	10.4	10.4	10.4	10.4
27	0.0	8.9	8.9	8.9	8.9	8.9	9.9	10.3	10.6	10.7	10.7	10.7	10.7	10.7	10.7	10.7
28	0.0	9.2	9.2	9.2	9.2	9.2	10.2	10.6	10.9	11.0	11.0	11.0	11.0	11.0	11.0	11.0
29	0.0	9.5	9.5	9.5	9.5	9.5	10.5	10.9	11.2	11.3	11.3	11.3	11.3	11.3	11.3	11.3
30	0.0	9.8	9.8	9.8	9.8	9.8	10.8	11.2	11.5	11.6	11.6	11.6	11.6	11.6	11.6	11.6
31	0.0	10.1	10.1	10.1	10.1	10.1	11.1	11.5	11.8	11.9	11.9	11.9	11.9	11.9	11.9	11.9
32	0.0	10.4	10.4	10.4	10.4	10.4	11.4	11.8	12.1	12.2	12.2	12.2	12.2	12.2	12.2	12.2
33	0.0	10.7	10.7	10.7	10.7	10.7	11.7	12.1	12.4	12.5	12.5	12.5	12.5	12.5	12.5	12.5
34	0.0	11.0	11.0	11.0	11.0	11.0	12.0	12.4	12.7	12.8	12.8	12.8	12.8	12.8	12.8	12.8
35	0.0	11.3	11.3	11.3	11.3	11.3	12.3	12.7	13.0	13.1	13.1	13.1	13.1	13.1	13.1	13.1
36	0.0	11.6	11.6	11.6	11.6	11.6	12.6	13.0	13.3	13.4	13.4	13.4	13.4	13.4	13.4	13.4
37	0.0	11.9	11.9	11.9	11.9	11.9	12.9	13.3	13.6	13.7	13.7	13.7	13.7	13.7	13.7	13.7
38	0.0	12.2	12.2	12.2	12.2	12.2	13.2	13.6	13.9	14.0	14.0	14.0	14.0	14.0	14.0	14.0
39	0.0	12.5	12.5	12.5	12.5	12.5	13.5	13.9	14.2	14.3	14.3	14.3	14.3	14.3	14.3	14.3
40	0.0	12.8	12.8	12.8	12.8	12.8	13.8	14.2	14.5	14.6	14.6	14.6	14.6	14.6	14.6	14.6
41	0.0	13.1	13.1	13.1	13.1	13.1	14.1	14.5	14.8	14.9	14.9	14.9	14.9	14.9	14.9	14.9
42	0.0	13.4	13.4	13.4	13.4	13.4	14.4	14.8	15.1	15.2	15.2	15.2	15.2	15.2	15.2	15.2
43	0.0	13.7	13.7	13.7	13.7	13.7	14.7	15.1	15.4	15.5	15.5	15.5	15.5	15.5	15.5	15.5
44	0.0	14.0	14.0	14.0	14.0	14.0	15.0	15.4	15.7	15.8	15.8	15.8	15.8	15.8	15.8	15.8
45	0.0	14.3	14.3	14.3	14.3	14.3	15.3	15.7	16.0	16.1	16.1	16.1	16.1	16.1	16.1	16.1
46	0.0	14.6	14.6	14.6	14.6	14.6	15.6	16.0	16.3	16.4	16.4	16.4	16.4	16.4	16.4	16.4
47	0.0	14.9	14.9	14.9	14.9	14.9	15.9	16.3	16.6	16.7	16.7	16.7	16.7	16.7	16.7	16.7
48	0.0	15.2	15.2	15.2	15.2	15.2	16.2	16.6	16.9	17.0	17.0	17.0	17.0	17.0	17.0	17.0

AVERAGE SECTION OF PIN PT.

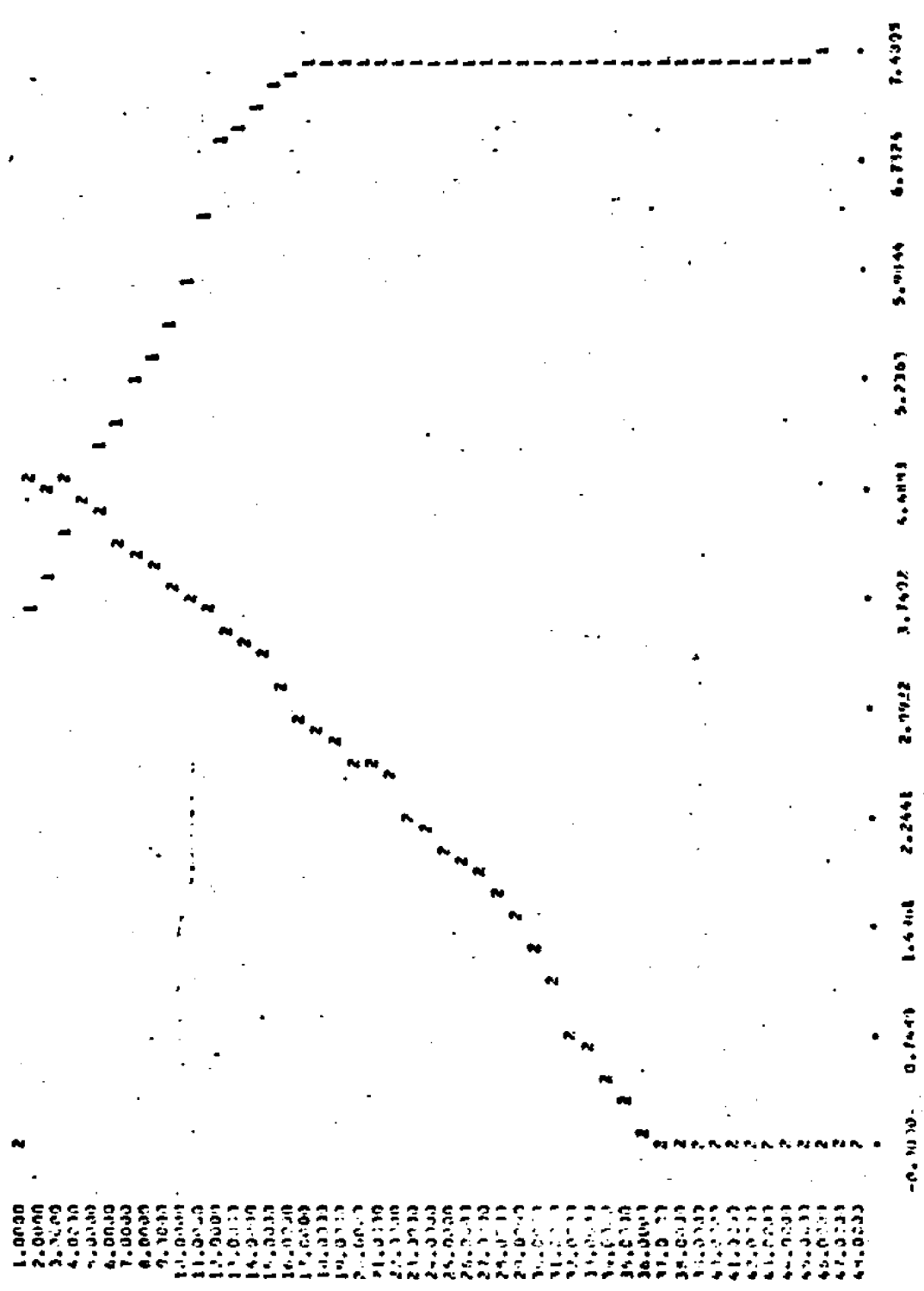
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6	22.700
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8	22.970
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10	17.137
11	15.750
12	17.073
13	22.050
14	17.433
15	17.753
16	18.073
17	21.321
18	22.134
19	17.373
20	17.290
21	20.931
22	17.613
23	29.300
24	29.033
25	27.760
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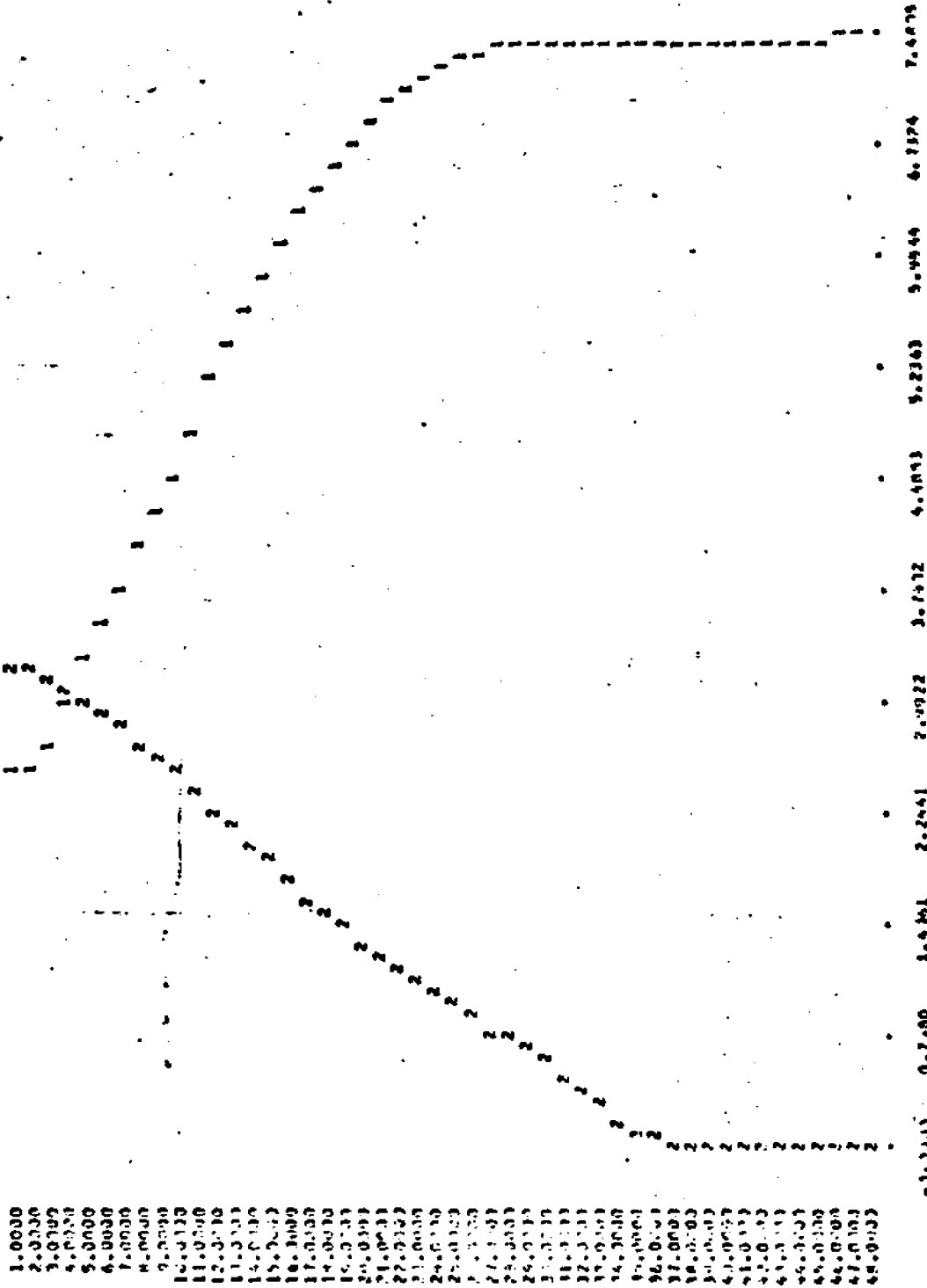
C.O. (1) & H.O.O. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHAPT 14



N.O. (1) 9 8.0.0. (2) IN HQ/A VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 15



AVERAGE U.O. III & R.O.D. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1

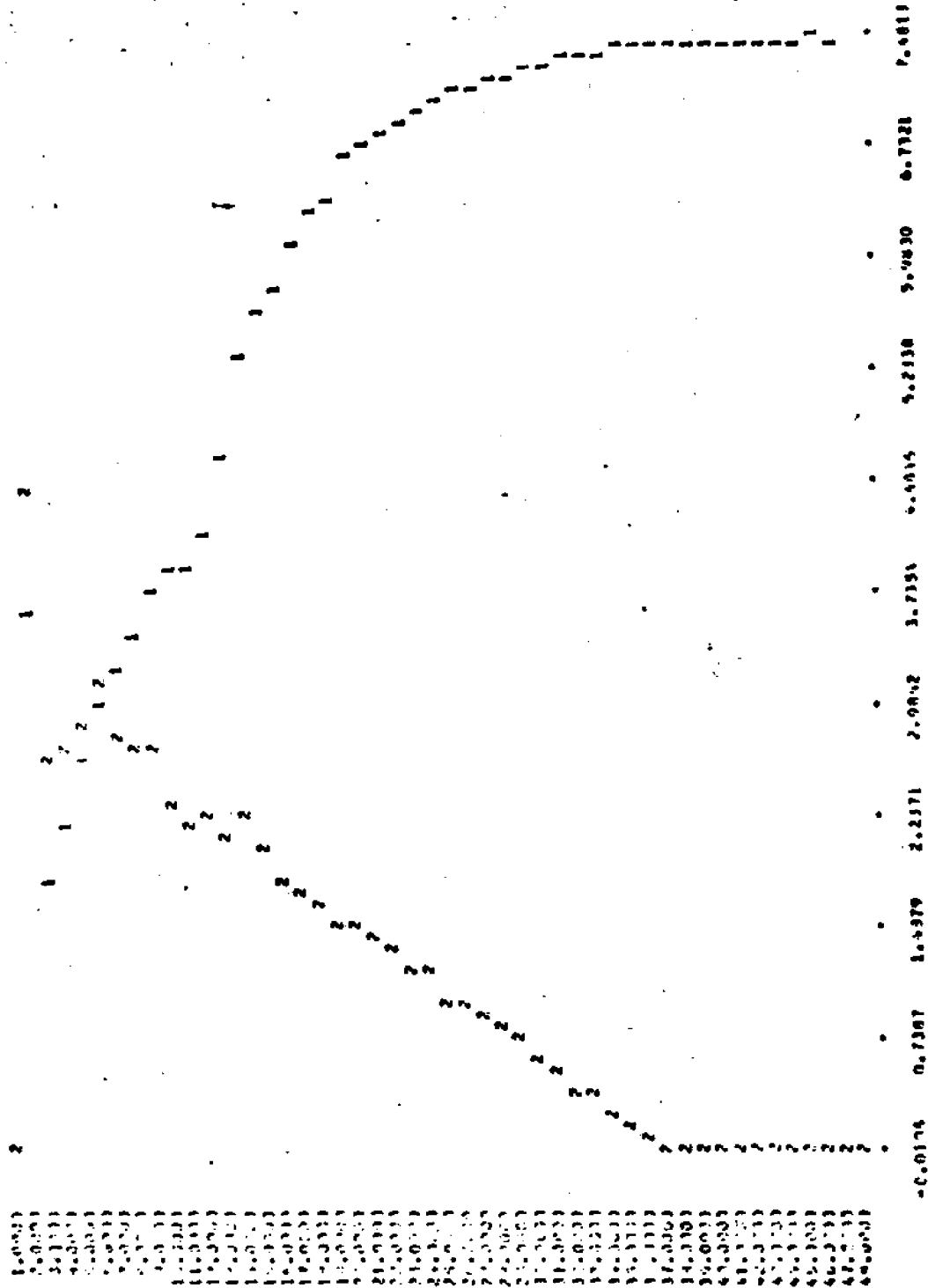


STEP NUMBER = 50 TIME = 6.67MRS.

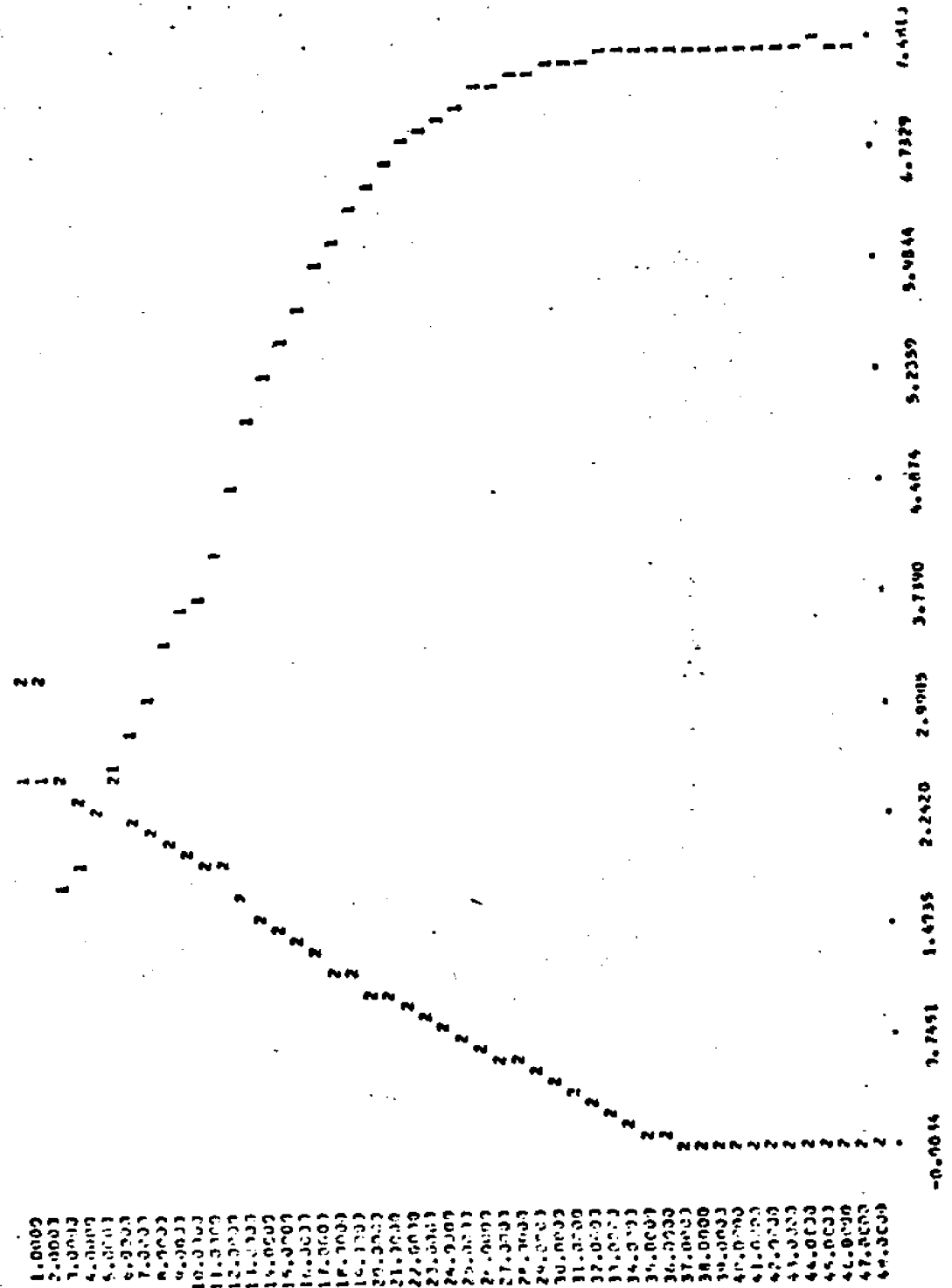
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2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SURFACE DRYSPM SOLUBILITY (MG/L)
 0.0
 7.7140
 7.7490
 7.7640
 7.7691
 7.7741
 7.7791
 7.7841
 7.7891
 7.7941
 7.7991
 7.8041
 7.8091
 7.8141
 7.8191
 7.8241
 7.8291
 7.8341
 7.8391
 7.8441
 7.8491
 7.8541
 7.8591
 7.8641
 7.8691
 7.8741
 7.8791
 7.8841
 7.8891
 7.8941
 7.8991
 7.9041
 7.9091
 7.9141
 7.9191
 7.9241
 7.9291
 7.9341
 7.9391
 7.9441
 7.9491
 7.9541
 7.9591
 7.9641
 7.9691
 7.9741
 7.9791
 7.9841
 7.9891
 7.9941
 7.9991
 0.0

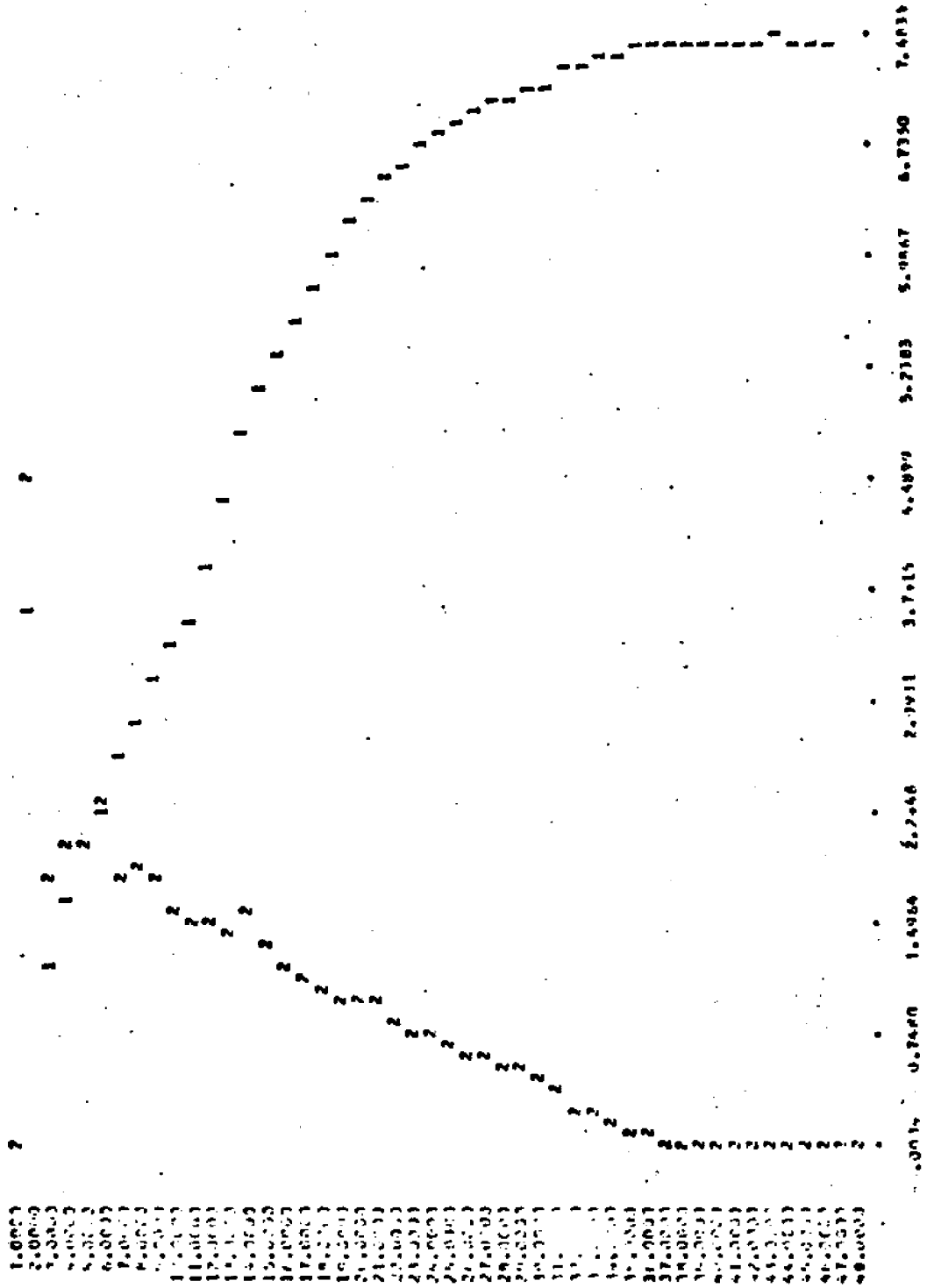
U.C. 113 & A.O.D. 123 IN MEZL VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 14



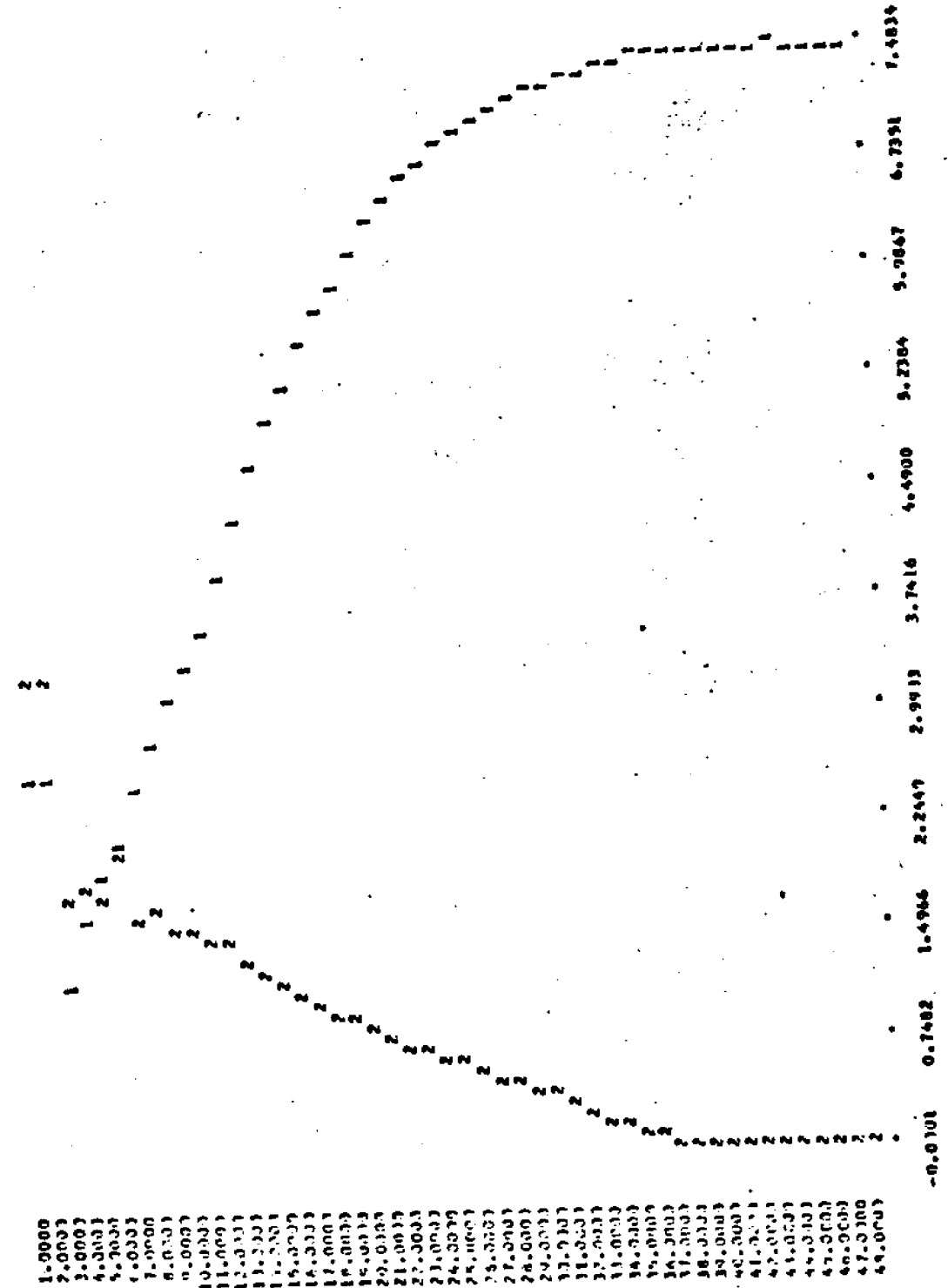
AVERAGE P.C. (1) & S.C. (2) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1



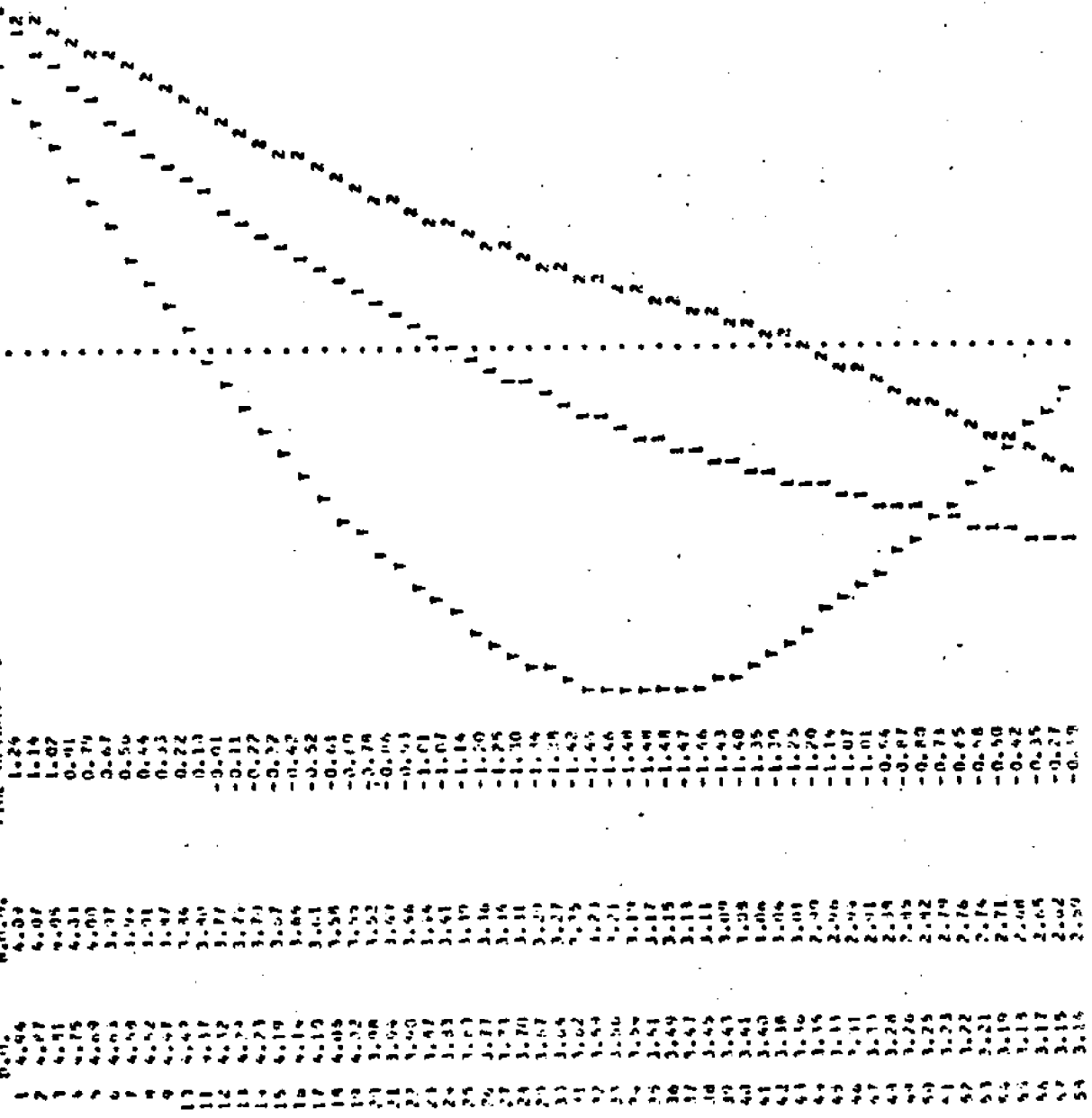
C.O. (1) & R.O.D. (2) IN MGA VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 14

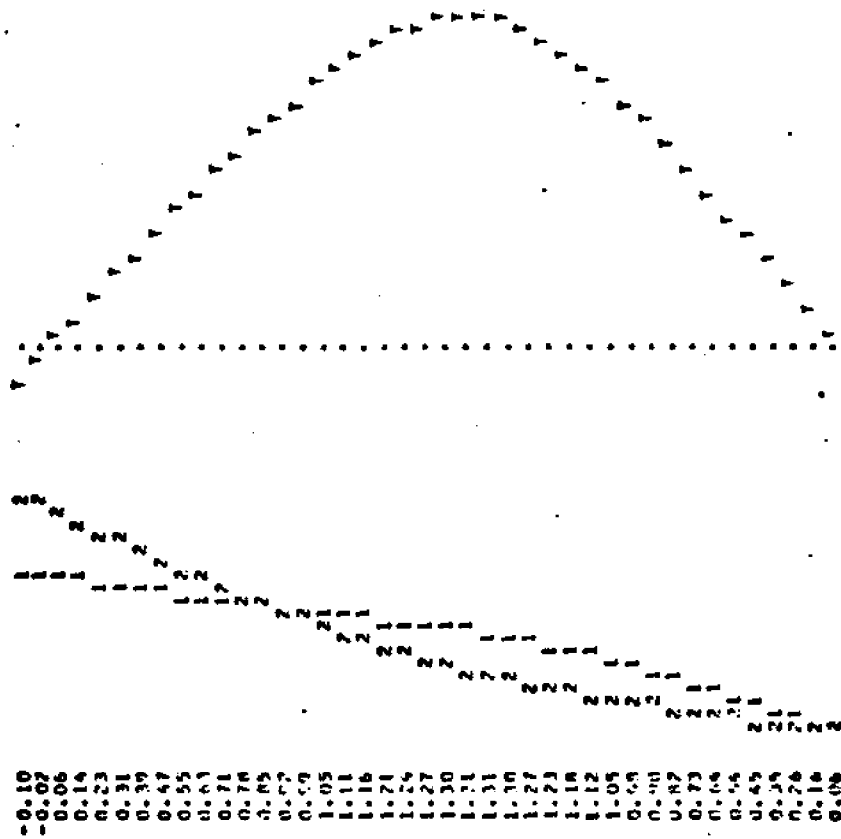


AVERAGE O.D. (11) & H.O.D. (20) IN MG/L VS ESTUARY LONGITUDINAL SECTION NUMBER
 CHART 1



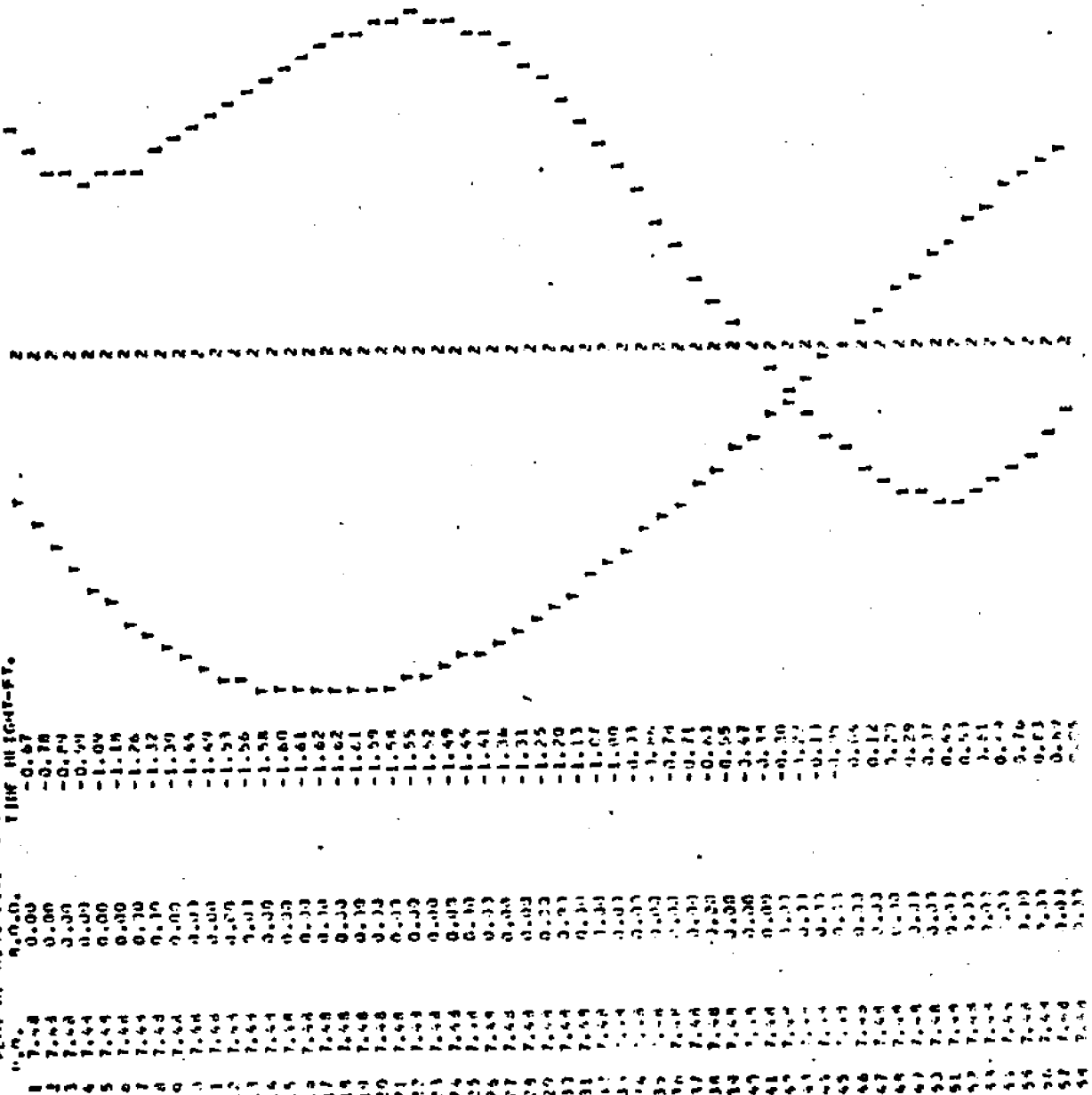
PLOT OF H.O. 113, H.O. 12, AND TIDE HEIGHT (1) FOR GRID No. 14 No. 7 TIME STEP 0.13 HRS.
 H.O. 113 TIME IN MIN-PT. H.O. 12 TIME IN MIN-PT.

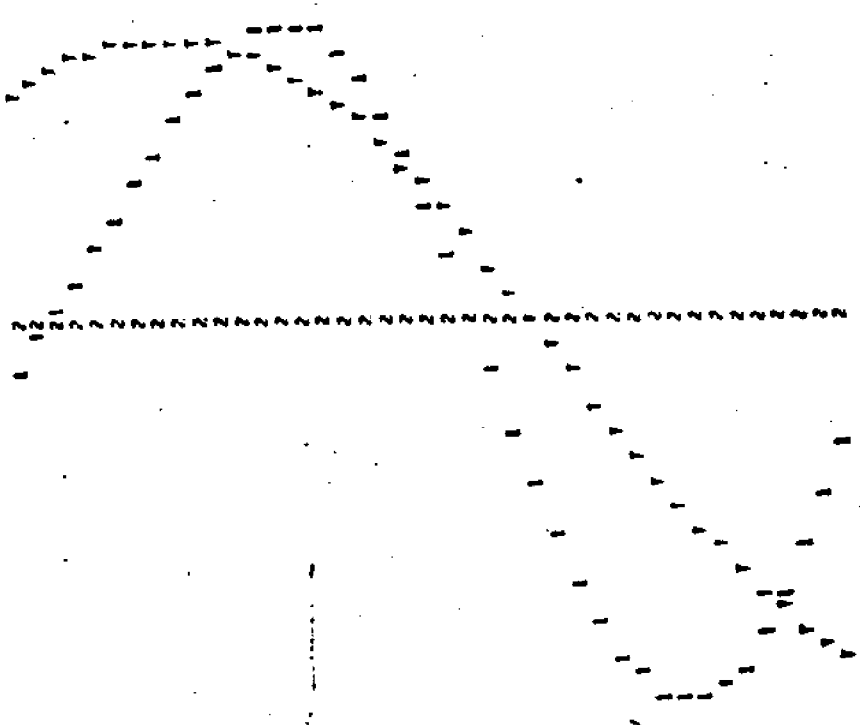




59	3.13	2.54	-0.10
60	3.12	2.53	-0.07
61	3.11	2.51	0.06
62	3.10	2.49	0.14
63	3.09	2.45	0.23
64	3.08	2.42	0.31
65	3.07	2.39	0.39
66	3.06	2.37	0.47
67	3.05	2.34	0.55
68	3.04	2.32	0.61
69	3.03	2.29	0.71
70	3.03	2.27	0.78
71	3.02	2.24	0.85
72	3.01	2.22	0.92
73	3.00	2.20	0.99
74	2.99	2.17	1.05
75	2.98	2.15	1.11
76	2.98	2.13	1.16
77	2.97	2.11	1.21
78	2.97	2.07	1.25
79	2.96	2.04	1.27
80	2.95	2.06	1.30
81	2.94	2.03	1.31
82	2.93	2.01	1.31
83	2.92	2.01	1.30
84	2.91	2.01	1.27
85	2.91	1.99	1.23
86	2.91	1.94	1.18
87	2.91	1.91	1.12
88	2.90	1.87	1.05
89	2.89	1.85	0.99
90	2.88	1.84	0.90
91	2.88	1.82	0.87
92	2.88	1.82	0.84
93	2.87	1.81	0.84
94	2.87	1.81	0.85
95	2.87	1.81	0.85
96	2.87	1.81	0.84
97	2.87	1.81	0.82
98	2.87	1.81	0.81
99	2.87	1.80	0.80

PLAT OF 0.0. 111. R.1.0. 123. AND FINE HEIGHT (1) FIM GRID No.14 MASS TIME STEP= 0.13 MMS.





52	7.48	0.09	1.01
53	7.48	0.00	1.06
54	7.48	0.39	1.80
55	7.48	0.39	1.14
56	7.44	0.03	1.17
57	7.58	0.30	1.19
58	7.54	0.03	1.21
59	7.57	0.33	1.22
60	7.54	0.30	1.22
61	7.44	0.00	1.20
62	7.48	0.00	1.18
63	7.58	0.00	1.15
64	7.58	0.00	1.11
65	7.53	0.03	1.06
66	7.57	0.03	1.11
67	7.54	0.03	0.54
68	7.58	0.03	0.87
69	7.44	1.33	0.70
70	7.48	0.00	0.69
71	7.58	0.00	0.59
72	7.58	0.00	0.59
73	7.54	0.00	0.38
74	7.58	0.00	0.26
75	7.58	0.00	0.15
76	7.54	0.00	0.03
77	7.54	0.00	-0.03
78	7.58	0.00	-0.21
79	7.58	0.00	-0.54
80	7.58	0.03	-0.55
81	7.48	0.03	-0.09
82	7.58	0.03	-0.77
83	7.53	0.00	-0.87
84	7.58	0.00	-0.00
85	7.54	0.00	-1.06
86	7.58	0.00	-1.14
87	7.58	0.00	-1.22
88	7.58	0.00	-1.30
89	7.54	0.00	-1.36
90	7.54	0.00	-1.42

IV DIGITAL COMPUTER PROGRAM LISTING

LISTING - TDLIDO
DIMENSIONLESS VERTICAL AXIS MODEL


```

13  FORMAT(2F10.4,F5.2,F6.1)
    GO TO 16
14  CONTINUE
    READ(5,15)DA,DB,DC,DE
15  FORMAT(4F10.8)
16  CONTINUE
    READ(5,40)ISALTA,RETI,GAMS
40  FORMAT(3F10.5)
    READ(5,41)M,N,T,WL
41  FORMAT(3F10.5)
    MINDO=MDC+1
    NINDO=NDC+1
    NSECT=M*MAX
    DO 100 M=1,M*MAX
    DO 100 N=1,M*MAX
    JS(N,M)=0.0
    CSC(N,M)=0.0
    RAN(N,M)=0.0
    LS(N,M)=0.0
    CD(N,M)=0.0
    CT(N,M)=0.0
    COP(N,M)=0.0
    P(N,M)=0.0
    U(N,M)=0.0
    V(N,M)=0.0
    D(N,M)=0.0
    DX(N,M)=0.0
    DZ(N,M)=0.0
    B(N,M)=0.0
    TS(N,M)=0.0
    SS(N,M)=0.0
100  CONTINUE
    DO 1500 JK=1,M*MAX
    SF(JK)=0.0
1500  SEP(JK)=0.0
    CALL GETF(M*MAX,M*MAX,(DIF,ISALT,ISCU)
    CALL FIND(MIND,NIND,M*MAX,N*MAX,MINDO,NINDO,NSECT)
    CALL INLT(M*MAX,M*MAX,ISALT,ISMD)
    TAU=AT/2.
    FAX1=TAU/(4.*DDX)
    NZ=M*MAX-2
    DDA=FLOAT(NZ)
    DDZ=1./DDA
    FAX2=TAU/(2.*(DDX**2))
    FAZ1=TAU/(4.*DDZ)
    FAZ2=TAU/(2.*(DDZ**2))
    IF (ISALT.CT.1) GO TO 555
    CALL DECAY(N*MAX,M*MAX,IDEC)
    CALL SOLUB(N*MAX,M*MAX)
555  CONTINUE
    NST=1
600  CONTINUE

```



```

514 IF(NST.EQ.*AXST) GO TO 400
CONTINUE
IF(NON.EQ.NINST) GO TO 405
NSRCH=1.0(NM)/100000
N=MIN(200)/10000-NSRCH*100
MF=MAX(100)/100-NSRCH*10000-N*100
L=MIN(200)-NSRCH*100000-N*10000-MF*100
NM=N-1
NM=N+1
MFF=MF-2
DO 503 N=MF,L
NM=N-1
MM=N+1
IF(H(N,NM).EQ.O.C) GO TO 61
GO TO 62
61 H(N,NM)=R(N,M)
CONTINUE
IF(H(NM,N).EQ.O.C) GO TO 63
GO TO 64
63 R(NN,M)=R(N,M)
CONTINUE
IF(H(NN,MM).EQ.O.C) GO TO 65
GO TO 66
65 H(NN,NM)=R(N,MM)
66 CONTINUE
IF(H(N,MM).EQ.O.C) GO TO 67
GO TO 68
67 U(N,NM)=C.O
OX(N,NM)=C.O
IF(MR.CGT.1.AND.*M.EQ.1) GO TO 362
GO TO 62
362 U(N,NM)=U(N,M)
OX(N,NM)=OX(N,M)
68 CONTINUE
IF(H(N,NM).EQ.O.C) GO TO 69
GO TO 73
69 O2(N,NM)=C.O
W(N,NM)=C.O
CO(N,NM)=CO(N,M)
70 CONTINUE
IF(H(NM,NM).EQ.O.C) GO TO 71
GO TO 72
71 CO(NM,NM)=CO(N,M)
W(N,NM)=C.O
O2(N,NM)=C.O
72 CONTINUE
H1=(DEP(NM)+(SE(NM)+SE(N))/2.
H2=(DEP(NM)+DEP(NM))/2.+SE(N)
H3=(DEP(NM)+(SE(N)+SE(NM))/2.
H4=(DEP(NM)+(SE(N)+SE(NM))/2.
H5=(DEP(NM)+(SE(N)+SE(NM))/2.
H6=(DEP(NM)+DEP(NM))/2.+SCP(N)

```



```

      GO TO 869
863  CONTINUE
      DO 87, M=1, MMAX
      GO 870 N=1, NMAX
870  CR(N, M)=CCP(N, M)
      AETS=0.0
      BETB=0.0
      BETA=0.0
      ALPHA=0.0
      BETR1=0.0
869  CONTINUE
867  CONTINUE
      CALL HOVAL(NMAX, MMAX, IPASS, NST)
      IF(NST.EQ.MAXST) GO TO 400
      NUM=1
414  CONTINUE
      IF(NUM.EQ.MIND) GO TO 405
      MSRCH=MRD(NU)/1000000
      M=MRD(NUM)/10000-MSRCH*100
      NF=MRD(NU)/100-MSRCH*10000-M*100
      L=MRD(NUM)-MSRCH*1000000-M*10000-NF*100
      NFF=NF-1
      MFM=M+1
      MM=M-1
      DO 406 N=NF, L
      MN=N-1
      VNN=N+1
      IF(H(N, MM).EQ.0.0) GO TO 80
      GO TO 81
80  R(N, MM)=P(N, M)
81  CONTINUE
      IF(H(N, M).EQ.0.0) GO TO 82
      GO TO 83
82  H(N, M)=B(N, M)
83  CONTINUE
      IF(H(N, MM).EQ.0.0) GO TO 84
      GO TO 85
84  R(N, MM)=F(N, M)
85  CONTINUE
      IF(H(N, M).EQ.0.0) GO TO 86
      GO TO 87
86  A(N, M)=0.0
      DZ(N, M)=0.0
87  CONTINUE
      IF(H(N, MM).EQ.0.0) GO TO 88
      GO TO 89
88  CONTINUE
      IF(MRC.GT.1.AND.MM.EQ.1) GO TO 360
      GO TO 361
360  OX(N, MM)=OX(N, M)
      GO TO 89
361  CONTINUE

```

```

      U(N,M)=0.0
      DX(N,M)=0.0
      CO(N,M)=CC(N,M)
89     CONTINUE
      IF(M(N,MM).EQ.0.0) GO TO 90
      GO TO 91
90     CONTINUE
      IF(MM.FO.MMX) GO TO 91
      CO(N,MM)=CC(N,M)
91     CONTINUE
      IF(M(N,M).EQ.0.0) GO TO 605
      GO TO 606
605    W(I,1)=0.0
      DZ(I,M)=0.0
606    CONTINUE
      SS1=1.0
      SS2=1.0
      SS3=1.0
      SS4=1.0
      IF(IPASS.FO.2) GO TO 5673
      IF(JSIN,M).GT.0.0.AND.U(N,M).GT.0.0) GO TO 5666
      GO TO 5667
5666   SS1=1.0
      SS2=1.0
      SS3=0.0
      SS4=2.0
5667   CONTINUE
      IF(JSIN,MM).GT.0.0.AND.U(N,MM).GT.0.0) GO TO 5668
      GO TO 5669
5668   SS1=0.0
      SS2=2.0
      SS3=1.0
      SS4=1.0
5669   CONTINUE
      IF(JSIN,M).GT.0.0.AND.U(M,M).LT.0.0) GO TO 5670
      GO TO 5671
5670   SS1=0.0
      SS2=2.0
      SS3=1.0
      SS4=1.0
5671   CONTINUE
      IF(JSIN,MM).GT.0.0.AND.U(M,MM).LT.0.0) GO TO 5672
      GO TO 5673
5672   SS1=1.0
      SS2=1.0
      SS3=0.0
      SS4=2.0
5673   CONTINUE
      M1=(DEP(M)+(SE(M)+SE(M))/2.
      M2=(DEP(M)+DEP(M))/2.+SE(M)
      M3=(DEP(M)+(SE(M)+SE(M))/2.
      M4=(DEP(M)+(SE(M)+SE(M))/2.

```



```

M5=DEF(M)+ (SEP(M)+SEP(M+1))/2.
M6=(DEF(M)+DEF(M+1))/2.+SEP(M)
M7=.25*(G(N,Y)+G(N,M)+H(NN,Y)+H(NN,M))
I1=H(N,M)+R(N,M)
B2=(NN,M)+3*INN,M)
B3=R(N,M)+P(NN,M)
M4=R(N,M)+P(N,M)
AA(N)=-FAZ1*M2*(N,M)-(FAZ2*M2*DZ(NN,M))/M6
M(N)=FAZ1*F1*(N,M)+M0*M0-FAZ1*M2*(N,M)+FAZ2*B1*DZ(N,M)/M6+
1 (FAZ2*M2*DZ(NN,M))/M6+M0*TAU*M0*D(N,M)*.5*3*ETB1+M0*TAU*M0*
2 4*F(N,M)*.5*ALPHA
CC(N)=FAZ1*M1*(N,M)-(FAZ2*B1*DZ(N,M))/M6
DD(N)=CC(N,M)+M0*M2-FAZ1*M4*(N,M)+M3*(CC(N,M)+SS1+CC(N,M+1)*SS2)
1 +FAZ1*M3*(N,M)+M1*(CC(N,M)+SS3+CC(N,M+1)*SS4)+FAZ2*M4*DX(N,M)*M3
2 *(CC(N,M)-CC(N,M+1))-FAZ2*M3*DX(N,M)+M1*(CC(N,M)-CC(N,M+1))-M2*
3 TAU*(-M0*FAZ1*(N,Y)+CC(N,M)+ALPHA*3*CC(N,M)+LS(N,M)+RETB*.5
4 +M0*FAZ1*(N,Y)+CC(N,M)+ALPHA*.5
5 M0*(N,M)+BETS-RC*JS(N,M)+ETA/(BC*DX*DDZ*M2))
406 CONTINUE
DO 900 K=NF,L
IF(K,FO,NF) GO TO 901
GO TO 902
901 NDF=NF+1
E(NDF)=-CC(K)/RA(K)
D(NDF)=DD(K)/RA(K)
GO TO 901
902 NJ=K+1
E(NJ)=-CC(K)/(B*(K)+AA(K)+E(K))
D(NJ)=(CC(K)-AA(K)*E(K))/(B*(K)+AA(K)+E(K))
IJL=L+1
E(IJL)=0.0
903 CONTINUE
IF(MSRCH.FO.10.CR.MSRCH.EC.11) GO TO 905
GO TO 906
905 NDF=NF+1
E(NDF)=0.0
D(NDF)=CC(NF,M)
906 CONTINUE
IF(MSRCH.FO.01.CR.MSRCH.EC.11) GO TO 907
GO TO 908
907 L1=L+1
E(L1)=0.0
D(L1)=CC(L1,M)
908 CONTINUE
900 CONTINUE
DO 910 J=NF,L
JJ=L+NF+1-J
J1=L+NF-J
CT(J1,M)=E(JJ)*CT(JJ,M)+D(JJ)
910 CONTINUE
NUM=NUM+1
GO TO 414

```



```

41 CONTINUE
   IF(15CU.GT.1) GO TO 42
   DO 33 M=1,MMAX
33  READ(5,36)(P(N,M),N=1,10)
   DO 340 M=1,MMAX
340 READ(5,36)(P(N,M),N=11,NMAX)
34  FORMAT(10F6.2)
42 CONTINUE
   DO 370 M=1,MMAX
370  READ(5,371)(TS(N,M),N=1,10)
   DO 372 M=1,MMAX
372  READ(5,371)(TS(N,M),N=11,NMAX)
371  FORMAT(10F6.2)
   IF(15ALT.GT.1) GO TO 410
   DO 35 M=1,MMAX
35  READ(5,36)(SS(N,M),N=1,10)
   DO 37 M=1,MMAX
37  READ(5,36)(SS(N,M),N=11,NMAX)
36  FORMAT(10F5.2)
410 CONTINUE
   DO 39 M=1,MMAX
39  READ(5,38)DEP(M)
38  FORMAT(F7.2)
   RETURN
   END

```



```

9      B(N,MM)=P(N,MM)
10     CONTINUE
      IF(B(M,N).EQ.0.0) GO TO 111
      GO TO 112
111    B(M,N)=B(N,MM)
112    CONTINUE
      IF(B(M,N,MM).EQ.0.0) GO TO 21
      GO TO 22
21     B(M,N,MM)=B(N,MM)
22     CONTINUE
      IF(B(M,N,MM).EQ.0.0) GO TO 23
      GO TO 24
23     A(M,N,MM)=B(N,MM)
24     CONTINUE
      IF(B(M,N,MM).EQ.0.0) GO TO 25
      GO TO 26
25     R(M,N,MM)=A(N,N,MM)
26     CONTINUE
      IF(B(M,N,MM).EQ.0.0) GO TO 27
      GO TO 28
27     A(N,N,MM)=R(N,N,MM)
28     CONTINUE
      H3=.125*(B(M,N,MM)+B(N,N,MM)+B(M,N,MM)+B(N,MM)+B(N,MM)+B(N,MM)+
1      B(N,N,MM)+B(N,N,MM))
      B(N,MM)=.5*(B3+B(N,MM))
20     CONTINUE
      DO 29 M=1,MMAX
      DO 29 N=1,NMAX
      IF(H(N,MM).EQ.0.0) GO TO 30
      GO TO 29
30     B(N,MM)=0.0
31     CONTINUE
29     CONTINUE
113    CONTINUE
130    CONTINUE
      DO 56 M=1,MMAX
      DO 56 N=1,NMAX
56     B(N,MM)=B(N,MM)/1000.
      DO 12 M=1,MMAX
      DO 12 N=1,NMAX
      IF(H(N,MM).EQ.0.0) GO TO 11
      GO TO 12
11     B(N,MM)=0.0
12     CONTINUE
      DO 57 M=1,MMAX
57     WRITE(6,570)M,(B(N,MM),N=1,NMAX)
570    FORMAT(3X,12,2X,2CF5.1)
      DO 59 M=1,MMAX
      DO 59 N=1,NMAX
59     B(N,MM)=1000.*B(N,MM)
      WRITE(6,50)
60     FORMAT(1H1,10X,'INITIAL CONCENTRATION (MG/L)')

```

```

61 WRITE(6,61) (NL(N), N=1, NMAX)
   FORMAT(1HC, 1CX, 2CI4)
   DO 67 M=1, MMAX
62 WRITE(6,63) M, (CCP(N, M), N=1, NMAX)
63 FORMAT(8X, 12, 2X, 2CF4.1)
   IF (ISALT.GT.1) GO TO 90
   WRITE(6,64)
64 FORMAT(1H1, 1CX, 'INITIAL SED CONCENTRATION (MG/L)')
   WRITE(6,65) (NU(N), N=1, NMAX)
65 FORMAT(1HC, 1CX, 2CI4)
   DO 66 M=1, MMAX
66 WRITE(6,67) M, (LS(N, M), N=1, NMAX)
67 FORMAT(8X, 12, 2X, 2CF4.1)
   WRITE(6,68)
68 FORMAT(1H1, 1CX, 'WASTE LOADS IN 1000 LBS/DAY')
   WRITE(6,69) (ML(N), N=1, NMAX)
69 FORMAT(1HC, 1CX, 2CI6)
   DO 70 M=1, MMAX
   DO 15 N=1, NMAX
15 JS(N, M) = JS(N, M) / 1000.0
70 WRITE(6,71) M, (JS(N, M), N=1, NMAX)
71 FORMAT(8X, 12, 3X, 2OF6.2)
   DO 16 M=1, MMAX
   DO 15 N=1, NMAX
16 JS(N, M) = JS(N, M) * 125.5448
   WRITE(6,72)
72 FORMAT(1H1, 1CX, 'SOURCES OR SINKS OF CO (MG/L)')
   WRITE(6,73) (NL(N), N=1, NMAX)
73 FORMAT(1HC, 1CX, 2CI4)
   DO 74 M=1, MMAX
74 WRITE(6,75) M, (D(N, M), N=1, NMAX)
75 FORMAT(8X, 12, 2X, 2OF4.2)
90 CONTINUE
   WRITE(6,80)
80 FORMAT(1H1, 1CX, 'TEMPERATURE FIELD (F)')
   WRITE(6,81) (TU(N), N=1, NMAX)
81 FORMAT(1HC, 1CX, 2CI5)
   DO 87 M=1, MMAX
82 WRITE(6,83) M, (TS(N, M), N=1, NMAX)
83 FORMAT(8X, 12, 2X, 2CF5.1)
   IF (ISALT.GT.1) GO TO 91
   WRITE(6,78)
78 FORMAT(1H1, 2CX, 'TIME AVERAGE SALINITY (2)')
   WRITE(6,79) (NU(N), N=1, NMAX)
79 FORMAT(1HC, 1CX, 2CI5)
   DO 84 M=1, MMAX
84 WRITE(6,85) M, (SS(N, M), N=1, NMAX)
85 FORMAT(8X, 12, 2X, 2CF5.1)
91 CONTINUE
   WRITE(6,86)
601 FORMAT(1H1, 2CX, 'AVERAGE SECTION DEPTH FT.')
   DO 803 M=1, MMAX

```

503
502

WRITE(6,602)M,DEF(M)
FORMAT(LX.12,3X,FF.3)
RETURN
END


```

START=.TRUE.
13 CONTINUE
12 CONTINUE
NUM=1
100 IF(NUM.EQ.NIAY) GO TO 300
N=NRD(NUM)/10000
NF=NRD(NUM)/100 -N*100
L=NRD(NUM)-N*10000-NF*100
MLEFT=NF-1
LRIG=L+1
NA=1
200 IF(NA.EQ.MIND)GO TO 210
M=NRD(NA)/10000
MROT=NRD(NA)/1000 -M*100
MTOP=NRD(NA)/10 -M*10000 -MROT*100
MFRN=NRD(NA)-M*100000-MROT*1000-MTOP*10
IF(MFRN.GT.1) GO TO 501
IF((N.GE.MROT).AND.(N.LE.MTOP)).AND.(MLEFT.EQ.M)) NRD(NUM)=
NRD(NUM)+1000000
IF((N.GE.MROT).AND.(N.LE.MTOP)).AND.(LRIG.EQ.M)) NRD(NUM)=
NRD(NUM)+1000000
GO TO 205
501 IF((N.GE.MROT).AND.(N.LE.MTOP)).AND.(MLEFT.EQ.M)) NRD(NUM)=
NRD(NUM)+7000000
IF((N.GE.MROT).AND.(N.LE.MTOP)).AND.(LRIG.EQ.M)) NRD(NUM)=
NRD(NUM)+20000000
205 NA=NA+1
GO TO 300
210 NUM=NUM+1
GO TO 100
300 CONTINUE
NUM=1
101 IF(NUM.EQ.MIN) GO TO 301
N=NRD(NUM)/10000
NF=NRD(NUM)/100 -N*100
L=NRD(NUM)-N*10000-NF*100
MROT=NF-1
LTOP=L+1
NA=1
201 IF(NA.EQ.NIND)GO TO 211
N=NRD(NA)/10000
MLEFT=NRD(NA)/1000-N*100
MRIGHT=NRD(NA)/10-N*10000-MLEFT*100
MFRN=NRD(NA)-N*100000-MLEFT*1000-MRIGHT*10
IF(MFRN.GT.1) GO TO 502
IF(M.GE.MLEFT.AND.M.LE.MRIGHT.AND.MFRN.EQ.N) NRD(NUM)=NRD(NUM)
1 + 10000000
IF(M.GE.MLEFT.AND.M.LE.MRIGHT.AND.LTOP.EQ.N) NRD(NUM)=NRD(NUM)
1 +1000000
GO TO 206
502 IF(M.GE.MLEFT.AND.M.LE.MRIGHT.AND.MFRN.EQ.N) NRD(NUM)=NRD(NUM)
1 + 20000000

```

```

      IF (N.GE.NLFF.AND.N.LE.NL5.VRIG.AND.LTOP.FC.NI *MDINUM)*MADINUM)
1    +2000000
206  M=M+1
      GO TO 201
211  N=N+M+1
      GO TO 101
301  CONTINUE
      WRITE(6,23)
23   FORMAT(1H1,20X,'COMPUTATIONAL CONTROL NUMBERS')
      WRITE(6,20)
      DO 22 J=1,NSECT
      WRITE(6,21) J,ARD(J),MDD(J)
22  CONTINUE
      WRITE(6,30) NIND,MIND
30   FORMAT(7,2X,'NIND = ',I2,5X,'MIND = ',I2)
20   FORMAT(7,3X,3HARD,2X,3HMDD,7X,3HPSD)
21   FORMAT(1H ,2X,I4,2X,I9,1X,I9)
      RETURN
      END

```



```

      S(N,M)=R(N,M)
13  CONTINUE
      IF(H(N,M).EQ.0.0) GO TO 14
      GO TO 15
14  U(N,M)=0.0
      R(N,M)=R(N,M)
      IF(M.EQ.1) L(N,M)=U(N,M)
15  CONTINUE
      IF(H(N,M).EQ.0.0) GO TO 19
      GO TO 20
19  R(N,M)=B(N,M)
20  CONTINUE
      B1=R(N,M)+R(N,M)
      B2=R(N,M)+R(N,M)
      B3=R(N,M)+R(N,M)
      B4=B(N,M)+B(N,M)
      W(N,M)=0.0
      DSM=(SE(MM)+SEP(MM)+SE(M)+SEP(M))/4.+CEP(M)
      DSM=(SE(MM)+SEP(MM)+SE(M)+SEP(M))/4.0+DEP(M)
      FACTA=1./P4*DSM
      U(N,M)=FACTA*(B3+U(N,M)+DSM-(DGM/TAU)*B1*(SEP(M)-SE(M)))
42  CONTINUE
18  CONTINUE
      RETURN
      END

```



```

NN=N+1
IF(SS(N,M).EQ.0.0) GO TO 18
IF(MIAN(M).EQ.0.0) SS(N,M)=SS(N,M)
SIGM1=-.053+.0149*SS(N,M)-.000482*(SS(N,M)**2)+.0000063*(SS(N,M)
1 **3)
1 SIGM1=-.053+.0149*SS(N,M)-.000482*(SS(N,M)**2)+.0000063*
(SS(N,M)**3)
DENSM=(SIGM1/1000.)+1.0
DENSL=(SIGM1/1000.)+1.0
DENDDIF=DENSL-DENSM
IF(ABS(DENDDIF).LT.0.000001) GO TO 18
DENAV=(DENSL+DENSM)/2.
R10=(6*(DENSM-DENSL))/(DNZ*DENAV+(DEP(M)+SE(M)))
R10=1.7*ABS(LIN(3))/(DEP(M)+SE(M))**2
R1=M10/R10
GO TO 19
16 R1=0.0
19 CONTINUE
R10=(1.+SE1)*R1**2
DZ(N,M)=(SNFT*HE*ADJ(U(N,M)))/R10+(GMS*H3)/R10
GO TO 11
10 DZ(N,M)=0.0
11 CONTINUE
9 CONTINUE
RETURN
END

```


CO(7,1)=2.2
CO(8,1)=2.5
CO(9,1)=2.8
CO(10,1)=2.9
CO(11,1)=3.1
CO(12,1)=3.2
CO(13,1)=3.5
CO(14,1)=3.7
CO(15,1)=2.7
CONTINUE
RETURN
END

9


```

12 WRITE(6,13)M,(UIN,P),N=1,NMAX)
13 FORMAT(8X,17,3X,2CF6.2)
   WRITE(6,14)NST,TIME
14 FORMAT(1H1,10X,1% VELOCITY FIELD -FPS.,5X,1STEP NUMBER =1,13,
1 5X,1TIME =1,F7.2,1HRS.1)
   WRITE(6,15)(NCIN),N=1,NMAX)
15 FORMAT(1HC,10X,20I6)
   DO 16 N=1,NMAX
16 WRITE(6,17)M,(U(N,M),N=1,NMAX)
17 FORMAT(8X,12,3X,2CF5.4)
20 CONTINUE
   RETURN
   END

```



```

20  WRITE(5,15)M,(RAX(N,M),N=1,NMAX)
15  FORMAT(1X,12,3X,2CF6.2)
    DO 40 M=1,MMAX
      N=NMAX-1
40  RAX(N,M)=RAX(N,M)/1000000.
      WRITE(6,16)INST,TIME
16  FORMAT(1H1,10X,'ROD DECAY COEFFICIENTS X 100000 (1/SEC)',5X,
1  'STEP NUMBER =',13,5X,'TIME =',F7.2,'HRS')
      WRITE(6,17)(INC(N),N=1,NMAX)
17  FORMAT(1H0,10X,2CF6)
      DO 23 M=1,MMAX
        DO 23 N=1,NMAX
23  D(N,M)=D(N,M)/1000000.
        DO 18 M=1,MMAX
18  WRITE(6,19)M,(D(N,M),N=1,NMAX)
19  FORMAT(1X,12,2X,2CF6.2)
        DO 41 M=1,MMAX
          DO 41 N=1,NMAX
41  D(N,M)=D(N,M)/1000000.
          WRITE(6,86)
86  FORMAT(1H1,10X,'SURFACE OXYGEN SOLUBILITY (MG/L)')
          WRITE(6,87)(CS(N),N=1,MMAX)
87  FORMAT(30X,F15.4)
50  CONTINUE
      RETURN
      END

```



```

LSAV(1)=LSAV(2)
N01=1
DO 7 J=1,MMAX
A(J,1)=PLCAT(J)
A(J,2)=CTAV(J)
7 A(J,3)=LSAV(J)
WRITE(6=8)
8 FORMAT(10I,5X,'AVERAGE D.C. (1) & B.O.D. (2) IN MG/L VS ESTUARY
1 LONGITUDINAL SECTION NUMBER')
NSN=4E
NSM=3
LSL=4E
NSS=0
CALL PLOTT(N01,A,NSN,NSM,LSL,NSS)
RETURN
END

```


C	PRINT TITLE	PLOT 075
C		PLOT 076
C	20 WRITE(6,1)ND	PLOT 077
C		PLOT 086
C	FIND SCALE FOR BASE VARIABLE	PLOT 087
C		PLOT 088
C	XSCAL=(A(N)-A(1))/(FLCAT(NLL-1))	
C		
C	FIND SCALE FOR CROSS VARIABLES	
C		PLOT 002
C	M1=M+1	PLOT 003
C	YMIN=A(M1)	PLOT 004
C	YMAX=YMIN	PLOT 096
C	M2=M*N	PLOT 097
C	DO 40 J=M1,M2	PLOT 098
C	IF(A(J)-YMIN) 28,28,29	PLOT 099
C	26 IF(A(J)-YMAX) 30,40,30	PLOT 100
C	28 YMIN=A(J)	PLOT 101
C	GJ TO 40	PLOT 102
C	30 YMAX=A(J)	PLOT 103
C	40 CONTINUE	PLOT 104
C	YSCAL=(YMAX-YMIN)/100.0	PLOT 105
C		PLOT 106
C	FIND BASE VARIABLE PRINT POSITION	PLOT 107
C		PLOT 108
C	X0=A(1)	PLOT 109
C	L=1	PLOT 110
C	MY=M-1	PLOT 005
C	I=1	PLOT 006
C	45 F=I-1	PLOT 113
C	XPR=X0+F*XSCAL	PLOT 114
C	IF(A(L)-XPR) 50,50,70	PLOT 115
C		PLOT 116
C	FIND CROSS-VARIABLES	
C	50 L2=L+1	
C	IF(L2-N) 51,51,54	
C	51 DO 52 IL=L2,N	
C	IF(A(IL)-XPR) 52,52,53	
C	52 CONTINUE	
C	L=IL	
C	GO TO 54	
C	53 L=IL-1	
C	54 DO 55 IX=1,LC1	
C	55 OUT(IX)=BLANK	PLOT 119
C	DO 60 J=1,MY	PLOT 120
C	LL=L+J*N	PLOT 121
C	JP=(A(LL)-YMIN)/YSCAL+1.0	PLOT 122
C	OUT(JP)=ANG(J)	PLOT 123
C	60 CONTINUE	PLOT 124
C		PLOT 125
C		PLOT 126
C	PRINT LINE AND CLEAR, OR SKIP	PLOT 127

```

WRITE(6,2)XPR,INT(I/2),I2=1,101
L=L+1
GO TO 80
70 WRITE(6,3)
80 I=I+1
IF(I-NLL) 45, 24, 96
84 XPR=A(I)
GO TO 50
C
C      PRINT CROSS-VARIABLES NUMBERS
C
86 WRITE(6,7)
YPR(1)=YMIN
DO 90 KN=1,6
90 YPR(KN+1)=YPR(KN)+YSCAL*10.0
YPP(11)=YMAX
WRITE(6,8)(YPR(IP),IP=1,11)
RETURN
END

```

```

PLOT 128
PLOT 129
PLOT 130
PLOT 131
PLOT 132
PLOT 133
PLOT 134
PLOT 135
PLOT 136
PLOT 137
PLOT 138
PLOT 139
PLOT 140
PLOT 141
PLOT 142
PLOT 143

```



```

JK=110*(TK(I)-ZD)/((ZD-ZD)/2.)*30.*31.
GO TO 47
42 CONTINUE
JK=31
47 CONTINUE
JK=31.0*(TIH(K,I)/ZC)*30.
LINE(I,J)=STAR
LINE(I,J)=CROSS
LINE(I,J)=TICK
40 *PTE(6,10)X,COO(K,I),ROD(K,I),TIH(K,I),(LINE(J),J=1,61)
10 FORMAT(20,1E,1X,F5.2,5X,F5.2,10X,F5.2,3X,61A1)
25 CONTINUE
RETURN
END

```


LISTING - TDLIDI
DIMENSIONAL VERTICAL AXIS MODEL


```

13  FORMAT(2F10.4,F5.2,F0.1)
    GO TO 10
14  CONTINUE
    READ(5,15)PA,DB,DC,DE
15  FORMAT(4F15.8)
16  CONTINUE
    READ(5,40)SNETA,BE11,GANS
40  FORMAT(3F10.5)
    READ(5,41)W,H,T,HL
41  FORMAT(3F10.5)
    NINDO=NHC+1
    NINDP=NRC+1
    DO 100 M=1,NMAX
    DO 100 N=1,NMAX
    JS(N,M)=0.0
    CSC(N,M)=0.0
    RAR(N,M)=0.0
    LS(N,M)=0.0
    CO(N,M)=0.0
    COP(N,M)=0.0
    CT(N,M)=0.0
    P(N,M)=0.0
    UL(N,M)=0.0
    W(N,M)=0.0
    Q(N,M)=0.0
    OX(N,M)=0.0
    OZ(N,M)=0.0
    R(N,M)=0.0
    TS(N,M)=0.0
    SS(N,M)=0.0
100  CONTINUE
    NSECT=NMAX
    CALL GETF(NMAX,NMAX, (DIF,ISALT,ISOU)
    CALL FINDMIND,MIND,NMAX,NMAX,NINDO,NINDO,NSECT)
    CALL INIT(NMAX,NMAX,ISALT,ISOU)
    TAU=AT/2.
    FAX1=TAU/(4.*DDX)
    FAX2=TAU/(2.*(DDX**2))
    FAZ1=TAU/(4.*DDZ)
    FAZ2=TAU/(2.*(DDZ**2))
    NST=1
600  CONTINUE
    CALL VELC(NMAX,NMAX,IVEL,NST,DDX,DDZ)
    IF(IDIF.EQ.1) GO TO 202
    CALL DIFFU(NMAX,NMAX,DDZ)
202  CONTINUE
    IF(ISALT.GT.1) GO TO 556
    CALL REAR(NMAX,NMAX)
556  CONTINUE
    IF(ISALT.GT.1) GO TO 556
    CALL DECAY(NMAX,NMAX,IDEC)
    CALL SOLUB(NMAX,NMAX)

```



```

NV=N-1
VNN=N+1
MFF=MF-1
DO 503 M=MF,L
MM=M-1
MMH=M+1
IF(H(N,MM).EQ.0.0) GO TO 61
GO TO 62
61 B(N,MM)=B(N,M)
CONTINUE
62 IF(H(NN,M).EQ.0.0) GO TO 63
GO TO 64
63 B(NN,M)=B(N,M)
64 CONTINUE
IF(H(NN,MM).EQ.0.0) GO TO 65
GO TO 66
65 B(NN,MM)=B(N,M)
66 CONTINUE
IF(H(N,MM).EQ.0.0) GO TO 67
GO TO 68
67 U(N,MM)=0.0
DX(N,MM)=0.0
IF(MRC.GT.1.AND.MM.EQ.1) GO TO 362
GO TO 68
362 U(N,MM)=U(N,M)
DX(N,MM)=DX(N,M)
68 CONTINUE
IF(H(NN,M).EQ.0.0) GO TO 69
GO TO 70
69 QZ(NN,M)=0.0
W(NN,M)=0.0
C(NN,M)=C(N,M)
70 CONTINUE
IF(H(NNN,M).EQ.0.0) GO TO 71
GO TO 72
71 CC(NNN,M)=CC(N,M)
W(N,M)=0.0
QZ(N,M)=0.0
72 CONTINUE
B0=.25*(B(N,M)+B(N,MM)+B(NN,M)+B(NN,MM))
B1=(B(N,MM)+B(N,M))
B2=B(NN,MM)+B(NN,M)
B3=B(N,MM)+B(N,MM)
B4=B(NN,M)+B(N,M)
AA2(M)=-FAX1*B3*U(N,MM)-FAX2*B1*DX(N,MM)
HB2(M)=3C-FAX1*B3*U(N,MM)+FAX1*B4*U(N,M)+FAX2*B4*DX(N,M)
1 +FAX2*B3*DX(N,MM)+TAU*BB*Q(N,M)+.5*BETS1+TAU*BC*RAR(N,M)+.5*ALPHA
CC2(M)=FAX1*B4*L(N,M)-FAX2*B1*Q(N,M)
DD2(M)=C(N,M)*BC-FAZ1*B1*W(N,M)*(C(N,M)+C(NNN,M))+
1 FAZ1*B2*W(NN,M)*(C(N,M)+C(NN,M))+FAZ2*B1*CZ(N,M)*
2 (C(NNN,M)-C(N,M))+FAZ2*B2*QZ(NN,M)*(C(NN,M)-C(N,M))
3 -TAU*(BC*RAR(N,M)+CSC(N,M)+ALPHA+BC*Q(N,M)+LS(N,M)*BETH*.5

```

```

4 +BC*PAR(N,M)*CO(N,M)*ALPHA*.5+BD*P(N,M)*BETS-RO*JS(N,M)*BETA/
5 (DDX*DDZ*BO))
503 CONTINUE
DO 100E K=MF,L
IF(K.EQ.MF) GO TO 1001
GO TO 1002
1001 MCF=MF+1
E(MCF)=-CCZ(K)/A8Z(K)
O(MCF)=ODZ(K)/A8Z(K)
GO TO 1003
1002 MQ=K+1
E(MQ)=-((CCZ(K))/(B8Z(K)+AAZ(K)*E(K))
O(MQ)=(ODZ(K)-AAZ(K)*O(K))/(B8Z(K)+AAZ(K)*E(K))
IJ=L+1
E(IJ)=O.C
1003 CONTINUE
IF(NSRCH.EQ.10.OR.NSRCH.EC.11) GO TO 1005
GO TO 1006
1005 MOF=MF+1
E(MOF)=O.O
O(MOF)=CO(N,MFF)
1006 CONTINUE
IF(NSRCH.FO.01.OR.NSRCH.EC.11) GO TO 1007
GO TO 1008
1007 JL=L+1
E(JL)=O.O
O(JL)=CO(N,JL)
1008 CONTINUE
DO 1100 J=MF,L
JJ=L+MF+1-J
JI=L+MF-J
CT(N,J1)=E(JJ)*CT(N,JJ)+O(JJ)
1100 CONTINUE
NUM=NUM+1
GO TO 514
805 CONTINUE
DO 350 M=1,MMAX
DO 350 N=1,NMAX
350 CO(N,M)=CT(N,M)
IF(ISALT.GT.1) GO TO 115
IF(IPASS.FO.2) GO TO 115
DO 116 M=1,MMAX
DO 116 N=1,NMAX
116 LS(N,M)=CO(N,M)
GO TO 862
115 CONTINUE
DO 860 M=1,MMAX
DO 860 N=1,NMAX
860 CO(N,M)=CO(N,M)
IF(ISALT.GT.1) GO TO 862
IPASS=IPASS-1
GO TO 1105

```



```

IF (MIN, EQ, MINO) GO TO 405
MSRCH=MSD(NUM)/100000
M=MIN(NUM)/10000-MSRCH*100
NF=NRD(NU*)/100-MSRCH*10000-M*100
L=MK7(NUM)-MSRCH*100000-M*10000-NF*100
LL=L-1
NFF=NF-1
MPM=M+1
MM=M-1
DO 406 N=NF,L
NN=N-1
NNN=N+1
IF (H(N,MM).EQ.0.C) GO TO 80
GO TO 81
80 R(N,MM)=B(N,M)
81 CONTINUE
IF (H(NL,M).EQ.0.C) GO TO 82
GO TO 83
82 B(N,M)=B(N,M)
83 CONTINUE
IF (H(NN,MM).EQ.0.C) GO TO 84
GO TO 85
84 B(N,MM)=B(N,M)
85 CONTINUE
IF (H(NN,M).EQ.0.C) GO TO 86
GO TO 87
86 M(NN,M)=0.0
D2(NN,M)=0.C
87 CONTINUE
IF (H(L,MM).EQ.0.C) GO TO 88
GO TO 89
88 CONTINUE
IF (MBC.GT.1.AND.MM.EQ.1) GO TO 360
GO TO 361
360 U(N,MM)=U(N,M)
DX(N,MM)=DX(N,M)
GO TO 89
361 CONTINUE
U(N,MM)=C.0
CO(N,MM)=CO(N,M)
DX(N,MM)=C.C
89 CONTINUE
IF (H(N,MMM).EQ.0.0) GO TO 90
GO TO 91
90 CONTINUE
IF (MMV.EC,MMAX) GO TO 91
CO(N,MM)=CO(N,M)
U(N,M)=0.0
DX(N,M)=0.0
91 CONTINUE
IF (H(NN,M).EQ.0.C) GO TO 405
GO TO 406

```

```

605  V(N,M)=0.0
      OZ(N,M)=0.0
606  CONTINUE
      SS1=1.0
      SS2=1.0
      SS3=1.0
      SS4=1.0
      IF(IPASS.FO.2) GO TO 5673
      IF(JS(N,M).GT.0.C.AND.U(N,M).GT.0.0) GO TO 5666
      GO TO 5667
5666  SS1=1.0
      SS2=1.0
      SS3=0.0
      SS4=2.0
5667  CONTINUE
      IF(JS(N,MM).GT.0.C.AND.U(N,MM).GT.0.0) GO TO 5668
      GO TO 5669
5668  SS1=0.0
      SS2=2.0
      SS3=1.0
      SS4=1.0
5669  CONTINUE
      IF(JS(N,M).GT.0.C.AND.U(N,M).LT.0.0) GO TO 5670
      GO TO 5671
5670  SS1=0.0
      SS2=2.0
      SS3=1.0
      SS4=1.0
5671  CONTINUE
      IF(JS(N,MM).GT.0.C.AND.U(N,MM).LT.0.0) GO TO 5672
      GO TO 5673
5672  SS1=1.0
      SS2=1.0
      SS3=0.0
      SS4=2.0
5673  CONTINUE
      B0=.25*(B(N,M)+B(N,MM)+B(NN,M)+B(NN,MM))
      B1=B(N,MM)+B(N,M)
      B2=B(N,MM)+B(N,M)
      B3=B(N,MM)+B(N,MM)
      B4=B(N,M)+B(N,M)
      AA(N)=-FAZ1*P2*(N,M)-FAZ2*P2*OZ(NN,M)
      B5(N)=FAZ1*B1*(N,M)+B0-FAZ1*P2*(N,M)+FAZ2*B1*OZ(N,M)
1  +FAZ2*P2*OZ(NN,M)+B0*TAU*(N,M)*.5*BETH1+B0*TAU*RAR(N,M)*.5*ALPHA
      CC(N)=FAZ1*P1*(N,M)-FAZ2*P1*OZ(N,M)
      DO(N)=CO(N,M)*B0-FAZ1*B4*U(N,M)+CO(N,M)*SS1+CC(N,MM)*SS21+FAZ1
1  +B3*U(N,MM)+CO(N,M)*SS3+CO(N,MM)*SS4+FAZ2*B4*OX(N,M)+CO(N,MM)
2  -CO(N,M))-FAZ2*P1*(N,MM)+CO(N,M)-CO(N,MM))-TAU*(-B0*KAR(N,M)*
4  CSC(N,M)+ALPHA*P1*O(N,M)+LS(N,M)*BETS*.5+H0*RAR(N,M)*CO(N,M)*
5  ALPHA*.5+B0*P(N,M)*BETS-B0*JS(N,M)*P1/(B0*DCX*OCZ))
406  CONTINUE
      DO 900 K=NF,L

```

```

IF (K.EQ.NF) GO TO 901
GO TO 902
901 NDF=NF+1
E(NDF)=-CC(K)/AA(K)
Q(NDF)=DD(K)/HH(K)
GO TO 902
902 NO=K+1
E(NO)=-CC(K)/(BS(K)+AA(K))*F(K)
Q(NO)=(DD(K)-AA(K)*O(K))/(BS(K)+AA(K))*E(K)
IJJ=L+1
E(IJJ)=C.O
903 CONTINUE
IF (MSRCH.EQ.10.OR.*SRCH.EQ.11) GO TO 905
GO TO 906
905 NDF=NF+1
E(NDF)=C.O
Q(NDF)=CT(NDF,M)
906 CONTINUE
IF (MSRCH.EQ.C1.OR.MSRCH.EQ.11) GO TO 907
GO TO 908
907 LI=L+1
FIL1)=2.O
OIL1)=C*LI,M)
908 CONTINUE
900 CONTINUE
GO 910 J=NF+L
JJ=L+NF+1-J
JI=L+NF-J
CT(JI,M)=E(JJ)*CT(JJ,M)+2IJJ)
910 CONTINUE
NUM=NUM+1
GO TO 4E4
405 CONTINUE
DO 351 M=1,NMAX
DO 351 N=1,NMAX
351 COIN,M)=CT(N,M)
IF (IS=LT.GT.1) GO TO 554
IF (IPASS.EQ.1) GO TO 913
554 CONTINUE
DO 1115 M=1,NMAX
DO 1115 N=1,NMAX
1115 COIN,M)=C(N,M)
IF (IS=LT.GT.1) GO TO 1110
GO TO 915
913 CONTINUE
DO 914 M=1,NMAX
DO 914 N=1,NMAX
914 LSN,M)=C(N,M)
915 CONTINUE
IF (IPASS.EQ.2) GO TO 1110
IPASS=IPASS+1
GO TO 864

```



```

41  CONTINUE
    IF (ISNO.GT.1) GO TO 42
    DO 33 M=1,M*MAX
33  READ(5,34)(P(A,M),A=1,10)
    DO 340 M=1,M*MAX
340 READ(5,34)(P(A,M),A=11,M*MAX)
34  FORMAT(10F6.2)
42  CONTINUE
    DO 370 M=1,M*MAX
370 READ(5,371)(TS(N,M),N=1,10)
    DO 372 M=1,M*MAX
372 READ(5,371)(TS(N,M),N=11,M*MAX)
371  FORMAT(10F6.2)
    IF (ISALT.GT.1) GO TO 410
    DO 35 M=1,M*MAX
35  READ(5,36)(SS(N,M),N=1,10)
    DO 37 M=1,M*MAX
37  READ(5,36)(SS(N,M),N=11,M*MAX)
36  FORMAT(10F6.2)
410 CONTINUE
    PFTURN
    END

```



```

9      R(N,MM)=R(N,MM)
10     CONTINUE
      IF(MIN(R,M).EQ.0.0) GO TO 111
      GO TO 112
111    R(MM,X)=R(N,M)
112    CONTINUE
      IF(M(NM,MM).EQ.0.0) GO TO 21
      GO TO 22
21     R(MM,MM)=R(N,M)
22     CONTINUE
      IF(R(MM,MM).EQ.C.C) GO TO 23
      GO TO 24
23     R(N,MM)=R(N,MM)
24     CONTINUE
      IF(R(N,MM).EQ.C.C) GO TO 25
      GO TO 26
25     R(MM,MM)=R(N,M)
26     CONTINUE
      IF(R(MM,MM).EQ.0.0) GO TO 27
      GO TO 28
27     R(MM,MM)=R(NM,MM)
28     CONTINUE
      IF(R(NM,MM).EQ.C.C.AND.R(MM,MM).EQ.0.0) GO TO 100
      GO TO 101
100    R(NM,MM)=R(N,M)
      R(N,MM)=R(N,M)
101    CONTINUE
      RB=.125*(R(NM,MM)+R(NM,M)+R(NM,MM)+R(N,MM)+R(N,MM)+R(NM,MM)+
1  R(N,M)+R(N,MM))
      R(N,M)=.5*(RB+R(N,M))
20     CONTINUE
      DO 29 M=1,NMAX
      DO 29 MM=1,NMAX
      IF(M(N,M).EQ.C.C) GO TO 30
      GO TO 29
30     R(N,M)=C.C
29     CONTINUE
113    CONTINUE
130    CONTINUE
      DO 56 M=1,NMAX
      DO 56 MM=1,NMAX
56     R(M,MM)=R(M,MM)/1000.
      DO 12 N=1,NMAX
      DO 12 MM=1,NMAX
      IF(M(N,MM).EQ.0.0) GO TO 11
      GO TO 12
11     R(N,MM)=C.C
12     CONTINUE
      DO 57 M=1,NMAX
57     WRITE(6,570)M,(R(N,M),N=1,NMAX)
570    FORMAT(12,2X,2CF5.1)
      DO 59 M=1,NMAX

```



```

59      DO 59 N=1,NMAX
        H(N,M)=1000.*H(N,M)
        WRITE(6,60)
60      FORMAT(1H1,10X,'INITIAL CONCENTRATION (MG/L)')
        WRITE(6,61)(NG(N),N=1,NMAX)
61      FORMAT(1H0,10X,2014)
        DO 62 N=1,NMAX
62      WRITE(6,63)M,(CCP(N,M),N=1,NMAX)
63      FORMAT(2X,12,2X,2CF4.1)
        IF(1SALT.GT.1) GO TO 90
        WRITE(6,64)
64      FORMAT(1H1,10X,'INITIAL BOD CONCENTRATION (MG/L)')
        WRITE(6,65)(VL(N),N=1,NMAX)
65      FORMAT(1H0,10X,2014)
        DO 66 N=1,NMAX
66      WRITE(6,67)M,(LSIN(M),N=1,NMAX)
67      FORMAT(2X,12,2X,2CF4.1)
        WRITE(6,68)
68      FORMAT(1H1,10X,'WASTE LOADS IN 1000 LBS/DAY')
        WRITE(6,69)(WC(N),N=1,NMAX)
69      FORMAT(1H0,10X,2016)
        DO 70 N=1,NMAX
        DO 15 N=1,NMAX
15      JS(N,M)=JSIN(M)/1000.0
70      WRITE(6,71)M,(JS(N,M),N=1,NMAX)
71      FORMAT(2X,12,3X,2CF6.2)
        DO 16 N=1,NMAX
        DO 16 N=1,NMAX
16      JS(N,M)=JSIN(M)*6.7269
        WRITE(6,72)
72      FORMAT(1H1,10X,'SOURCES OR SINKS OF OD (MG/L)')
        WRITE(6,73)(RUIN),N=1,NMAX)
73      FORMAT(1H0,10X,2014)
        DO 74 N=1,NMAX
74      WRITE(6,75)M,(PIN(M),N=1,NMAX)
75      FORMAT(1SX,12,3X,2CF4.2)
90      CONTINUE
        WRITE(6,80)
80      FORMAT(1H1,10X,'TEMPERATURE FIELD (F)')
        WRITE(6,81)(TL(N),N=1,NMAX)
81      FORMAT(1H0,10X,2015)
        DO 82 N=1,NMAX
82      WRITE(6,83)M,(TSIN(M),N=1,NMAX)
83      FORMAT(3X,12,2X,2CF5.1)
        IF(1SALT.GT.1) GO TO 91
        WRITE(6,78)
78      FORMAT(1H0,20X,'TIME AVERAGE SALINITY (X)')
        WRITE(6,79)(AL(N),N=1,NMAX)
79      FORMAT(1H0,10X,2015)
        DO 84 N=1,NMAX
84      WRITE(6,85)M,(SS(N,M),N=1,NMAX)
85      FORMAT(1SA,12,2X,2CF5.1)

```

91 CONTINUE
RETURN
END


```

START=.TRUE.
13 CONTINUE
12 CONTINUE
NUM=1
100 IF(NUM.EQ.MIND) GO TO 300
N=NRD(NUM)/10000
NF=NRD(NUM)/100 -N*100
L=NRD(NUM)-N*10000-NF*100
MFLEF=NF-1
LRIG=L+1
NA=1
200 IF(NA.EQ.MIND)GO TO 210
M=NRD(NA)/100000
NRGT=NRD(NA)/1000 -M*100
NTRP=NRD(NA)/10 -M*10000 -NRGT*100
MERN=MGO(NA)-M*10000-NRGT*1000-NTRP*10
IF(MERN.GT.1) GO TO 501
IF((N.GE.NRGT).AND.(N.LE.NTRP)).AND.(MFLEF.EQ.M) NRD(NUM)=
INRD(NUM)+1000000
IF((N.GE.NRGT).AND.(N.LE.NTRP)).AND.(LRIG.EQ.M) NRD(NUM)=
INRD(NUM)+1000000
GO TO 205
501 IF((N.GE.NRGT).AND.(N.LE.NTRP)).AND.(MFLEF.EQ.M) NRD(NUM)=
INRD(NUM)+2000000
IF((N.GE.NRGT).AND.(N.LE.NTRP)).AND.(LRIG.EQ.M) NRD(NUM)=
INRD(NUM)+2000000
205 NA=NA+1
GO TO 200
210 NUM=NUM+1
GO TO 100
300 CONTINUE
NUM=1
101 IF(NUM.EQ.MIND) GO TO 301
N=NRD(NUM)/10000
NF=NRD(NUM)/100 -N*100
L=NRD(NUM)-N*10000-NF*100
NRGT=NF-1
LTOP=L+1
NA=1
201 IF(NA.EQ.MIND)GO TO 211
N=NRD(NA)/100000
MLEF=NRD(NA)/1000-N*100
MRIG=NRD(NA)/10-N*10000-MLEF*100
MERN=MGO(NA)-N*10000-MLEF*100-MRIG*10
IF(MERN.GT.1) GO TO 502
IF(N.GE.MLEF.AND.(M.LE.MRIG.AND.NRGT.EQ.N) NRD(NUM)=NRD(NUM)
1 + 1000000
IF(N.GE.MLEF.AND.(M.LE.MRIG.AND.LTOP.EQ.N) NRD(NUM)=NRD(NUM)
1 +1000000
GO TO 206
502 IF(N.GE.MLEF.AND.(M.LE.MRIG.AND.NRGT.EQ.N) NRD(NUM)=NRD(NUM)
1 + 2000000

```

```

      IF (M.GE.MLEFF.AND.M.LE.MRIG.AND.LTOP.EC.N) MBD(NIM)=MBD(NUM)
1    +2000000
206 NA=NA+1
    GO TO 201
211 SUM=SUM+1
    GO TO 101
301 CONTINUE
    WRITE(6,23)
23  FORMAT(1H1,2CX,'COMPUTATIONAL CONTROL NUMBERS')
    WRITE(6,20)
20  FORMAT(///,3X,3HNUM,6X,3HNRD,7X,3HNRD)
    DO 22 J=1,NSECT
    WRITE(6,21) J,NRD(J),MBD(J)
22  CONTINUE
    WRITE(6,30) NIND,MIND
30  FORMAT(//,2X,'NIND = ',I2,5X,'MIND = ',I2)
21  FORMAT(1H ,2X,I4,2X,I9,1X,I9)
    RETURN
    END

```

```

SUBROUTINE VELC(MMAX,MMAX,IVEL,NST,OPX,DDZ)
COMMON NMF(90),MBO(50),NBOU(3),MBOB(3),AR(50),CBP(50),CS(50),
1 TS(16,50),SS(16,50),P(16,50),CO(16,50),CCP(16,50),LS(16,50),
2 JS(16,50),M(16,50),CT(16,50),U(16,50),W(16,50),C(16,50),
3 DX(16,50),DZ(16,50),R(16,50),RAR(16,50),CSC(16,50)
DIMENSION UU(50)

```

```

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C
C
C
C
C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C

```

VELOCITIES ARE READ IN OR CALCULATED

```

IF(IVEL.EQ.2) GO TO 200
DO 1 M=1,MMAX
1 READ(5,2)(U(N,M),N=1,10)
2 FORMAT(10F6.2)
DO 3 M=1,MMAX
3 READ(5,2)(U(N,M),N=11,NMAX)
DO 4 M=1,MMAX
4 READ(5,5)(W(N,M),N=1,10)
DO 6 M=1,MMAX
6 READ(5,5)(W(N,M),N=11,NMAX)
5 FORMAT(10F6.2)
GO TO 17
800 CONTINUE
READ(1,9)(UL(M),M=1,MMAX)
9 FORMAT(10F6.3)
DO 11 M=1,MMAX
DO 11 N=1,NMAX
IF(H(N,M).EQ.0.C) GO TO 11
U(N,M)=UU(M)
NSSN=NMAX-1
IF(N.EQ.NSSN) U(N,M)=0.0
11 CONTINUE
DO 16 M=1,MMAX
DO 16 N=1,NMAX
MM=M-1
MM=M+1
NN=N-1
NN=N+1
IF(H(N,M).EQ.0.C) GO TO 16
IF(H(NN,M).EQ.0.C) GO TO 12
GO TO 13
12 W(NN,M)=0.0
R(NN,M)=R(N,M)
13 CONTINUE
IF(H(N,MM).EQ.0.C) GO TO 14
GO TO 15
14 U(N,MM)=0.0
R(N,MM)=R(N,M)
IF(MM.EQ.1) U(N,MM)=U(N,M)

```

```

15 CONTINUE
   IF (H(NA,MM).EQ.0.C) GO TO 19
   GO TO 20
19  A(NA,MM)=B(N,M)
20  CONTINUE
   IF (H(N,MM).EQ.0.C) GO TO 50
   GO TO 51
50  CONTINUE
   IF (MM.EQ.MMAX) GO TO 51
   U(N,M)=0.0
51  CONTINUE
   B1=A(N,MM)+B(N,M)
   B2=A(N,MM)+B(NN,M)
   B3=A(N,MM)+B(N,MM)
   B4=A(NN,M)+B(N,M)
   W(N,M)=(((1.-1.)/(2.*DDX))*(B4*U(N,M)-B3*U(N,MM))+(B2/(2.*DCZ))*
1  A(NN,M)))/((2.*DDZ)/M1)
   IF (H(NNA,M).EQ.0.C) GO TO 21
   GO TO 22
21  U(N,M)=((2.*DDX)/A4)*((B2/(2.*DCZ))*W(NA,M)+(B3/(2.*DDX))*U(N,MM)
1  )
   W(N,M)=0.C
22  CONTINUE
16  CONTINUE
17  CONTINUE
   RETURN
   END

```



```

DO 9 N=1,NMAX
IF(H(N,M).EQ.0.0) GO TO 10
IZ=NMAX-N
SZ=FLIAT(IZ)
Z=SZ*CFZ-(DZ/2.
MF=((Z**2)*((DEP(M)-Z)**2))/(DEP(M)**3)
IF(L.FD.0.0.OP.WF.EC.0.0.OK.WT.EJ.0.0) GO TO 16
HA=(1-6.28*Z)/AL
HB=(Z*(DEP(M)-Z)*WB*EXP(HA))/(WT*DEP(M))
GO TO 17
16  HB=0.0
17  CONTINUE
  NN=N+1
  IF(H(NN,M).EQ.0.0) SS(NN,M)=SS(N,M)
  IF(SS(NN,M).EQ.0.0) GO TO 18
  SIGMU=-.093+.8149*SS(NN,M)-.000482*(SS(NN,M)**2)+.0000068*(SS(NN,M)
1  **3)
  SIGML=-.093+.8149*SS(NN,M)-.000482*(SS(NN,M)**2)+.0000068*
1  (SS(NN,M)**3)
  DENMU=(SIGML/1000.)*1.0
  DENSL=(SIGML/1000.)*1.0
  DENDIFF=DENSL-DENMU
  IF(ABS(DENDIFF).LT.000001) GO TO 18
  DENAV=(DENSL+DENMU)/2.
  R12=(0+(DENMU-DENSL))/(002*DENAV)
  RIC=(.7*ABS(LN.4))/DEP(M)**2
  R1=R12/RIC
  R1=ABS(R1)
  GO TO 19
18  R1=0.0
19  CONTINUE
  RID=(1.+R1*R1)**2
  DZ(N,M)=(SNETA*HE*ABS(U(N,M)))/RID+(GAMS*HE)/RIC
  GO TO 11
10  DZ(N,M)=0.0
11  CONTINUE
9   CONTINUE
  RETURN
  END

```



```

12 WRITE(6,12)M,(U(N,M),N=1,MMAX)
13 FORMAT(8X,12,2X,2CF6.2)
14 WRITE(6,14)NST,TIME
14 FORMAT(1H1,10X,'* VELOCITY FIELD -FPS.',5X,'STEP NUMBER =',13,
1 5X,'TIME =',F7.2,'HRS.>')
15 WRITE(6,15)(NC(N),N=1,NMAX)
15 FORMAT(1MC,10X,2016)
16 DO 16 M=1,MMAX
16 WRITE(6,17)M,(U(N,M),N=1,NMAX)
17 FORMAT(8X,12,3X,2CF6.4)
RETURN
END

```



```

20  WRITE(6,15)M,(RAR(N,M),N=1,NMAX)
15  FORMAT(1X,12,3X,2CF6.2)
    DO 40 M=1,MMAX
    N=NMAX-1
40  RAR(N,M)=RAR(N,M)/1000000.
    WRITE(6,16)NST,TIME
16  FORMAT(1H1,10X,'AND DECAY COEFFICIENTS X 1000000 (1/SEC)',5X,
1  'STEP NUMBER ',13,5X,'TIME ',F7.2,'HRS')
    WRITE(6,17)(D(N,M),N=1,NMAX)
17  FORMAT(1HC,10X,2016)
    DO 23 M=1,MMAX
    DO 23 N=1,NMAX
23  D(N,M)=D(N,M)/1000000.
    DO 18 M=1,MMAX
18  WRITE(6,19)M,(D(N,M),N=1,NMAX)
19  FORMAT(18X,12,2X,2CF6.2)
    DO 41 M=1,MMAX
    DO 41 N=1,NMAX
41  D(N,M)=D(N,M)/1000000.
    WRITE(6,86)
86  FORMAT(1H1,10X,'SURFACE OXYGEN SOLUBILITY (MG/L)')
    WRITE(6,87)(CS(M),M=1,MMAX)
27  FORMAT(30X,F15.4)
50  CONTINUE
    RETURN
    END

```



```

LSAV(1)=LSAV(2)
M01=1
DO 7 J=L,MAX
A(J,1)=PLCAT(J)
A(J,2)=CTAV(J)
7 A(J,3)=LSAV(J)
WRITE(6,*)
8 FORMAT(1H1,5X,'AVERAGE D.O. (1) & B.O.D. (2) IN MG/L VS ESTUARY
1 LONGITUDINAL SECTION NUMBER')
NSA=48
MSM=3
LSL=48
NSS=C
CALL PLOT(M01,A,NSA,MSM,LSL,NSS)
RETURN
END

```


C	PRINT TITLE	PLOT 075
C		PLOT 076
	20 WRITE(6,1)M)	PLOT 077
C		PLOT 086
C	FIND SCALE FOR BASE VARIABLE	PLOT 087
C		PLOT 088
	XSCAL=(A(N)-A(1))/(FLOAT(N)-1)	PLOT 089
C		PLOT 090
C	FIND SCALE FOR CROSS-VARIABLES	PLOT 091
		PLOT 092
	M1=N+1	PLOT M02
	YMIN=A(M1)	PLOT M03
	YMAX=YMIN	PLOT M04
	M2=M*N	PLOT 096
	DO 40 J=M1,M2	PLOT 097
	IF(A(J)-YMIN) 20,20,26	PLOT 098
26	IF(A(J)-YMAX) 40,40,30	PLOT 099
28	YMIN=A(J)	PLOT 100
	GO TO 40	PLOT 101
30	YMAX=A(J)	PLOT 102
40	CONTINUE	PLOT 103
	YSCAL=(YMAX-YMIN)/100.0	PLOT 104
		PLOT 105
C		PLOT 106
C	FIND BASE VARIABLE PRINT POSITION	PLOT 107
		PLOT 108
	XB=A(1)	PLOT 109
	L=1	PLOT 110
	MY=M-1	PLOT M05
	I=1	PLOT M06
45	F=I-1	PLOT 113
	XPR=XB+F*XSCAL	PLOT 114
	IF(A(L)-XPR) 50,50,70	PLOT 115
C		PLOT 116
C	FIND CROSS-VARIABLES	PLOT 117
50	L2=L+1	
	IF(L2-N) 51,51,54	
51	DO 52 IL=L2,N	
	IF(A(IL)-XPR) 52,52,53	
52	CONTINUE	
	L=N	
	GO TO 54	
53	L=IL-1	
54	DO 55 IX=1,101	
55	OUT(IX)=BLANK	PLOT 119
	DO 60 J=1,MY	PLOT 120
	LL=L+J*N	PLOT 121
	JP=(A(LL)-YMIN)/YSCAL)+1.0	PLOT 122
	OUT(JP)=ANG(J)	PLOT 123
60	CONTINUE	PLOT 124
		PLOT 125
C		PLOT 126
C	PRINT LINE AND CLEAR. OR SKIP	

<pre> C WRITE(6,2)XPR,(OUT(IZ),IZ=1,10) L=L+1 GO TO 80 70 WRITE(6,3) 80 I=I+1 IF(I-NLL) 45, 84, 86 84 XPR=4(N) GO TO 50 C C PRINT CROSS-VARIABLES NUMBERS C 86 WRITE(6,7) YOP(1)=YMIN DO 90 KN=1,9 90 YPR(KN+1)=YPR(KN)+YSCAL*10.0 YOP(11)=YMAX WRITE(6,8)(YPR(IP),IP=1,11) RETURN END </pre>	<pre> PLOT 127 PLOT 128 PLOT 129 PLOT 130 PLOT 131 PLOT 132 PLOT 133 PLOT 134 PLOT 135 PLOT 136 PLOT 137 PLOT 138 PLOT 139 PLOT 140 PLOT 141 PLOT 142 PLOT 143 </pre>
--	---

```

SUBROUTINE PUNC(NMAX,MMAX,ISALT)
REAL JS,LS
COMMON NAD(50),MAD(50),MORD(3),MORD(3),AR(50),DEP(50),CS(50),
1 TS(16,50),SS(16,50),P(16,50),CO(16,50),CDP(16,50),LS(16,50),
2 JS(16,50),M(16,50),CT(16,50),U(16,50),W(16,50),C(16,50),
3 UX(16,50),OZ(16,50),A(16,50),RAR(16,50),CSC(16,50)
C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C
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C
C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C C
DO 5 M=1,MMAX
5 WRITE(7,6)(CDP(N,M),N=1,10)
DO 7 M=1,MMAX
7 WRITE(7,6)(CDP(N,M),N=11,NMAX)
6 FORMAT(10F5.2)
IF(ISALT.GT.1) GO TO 8
DO 2 M=1,MMAX
2 WRITE(7,3)(LS(N,M),N=1,10)
DO 4 M=1,MMAX
4 WRITE(7,3)(LS(N,M),N=11,NMAX)
3 FORMAT(10F5.2)
8 CONTINUE
RETURN
END

```



```

JK=(CDDK(I)-ZCDD)/(Z4-Z0)/2.)*30.+31.0
GO TO 47
42 CONTINUE
JK=31
47 CONTINUE
JL=31.+(TTH(K,I)/ZC)*30.
LINE(JK)=STAR
LIP(IJJ)=CR+SS
LINE(JL)=TTH
40 WRITE(6,10)K,CDDK(I),RDDK(I),TTH(K,I),(LINE(J),J=1,61)
10 FORMAT(2X,13,1X,F5.2,5X,F5.2,10X,F5.2,3X,61A1)
25 CONTINUE
RETURN
END

```

V FUTURE ADAPTATIONS OF PROGRAM

The next step in the program development after more extensive verification on the other estuaries would be to extend the water quality modeling effort to include other reaction schemes such as that for nitrogen. Indications on how this might be achieved is outlined in the work of Leenderste and Gritton and the main body of this work (24,25).

Implementation of these procedures on the present model can be achieved by simply rewriting the governing equations and changing slightly the looping relations as defined in the general program outline given.

