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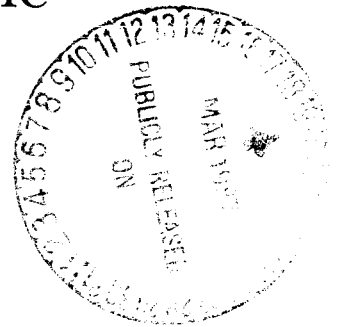
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Combined Aerodynamic and Structural Dynamic Problem Emulating Routines (CASPER)

Theory and Implementation

William H. Jones



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National Aeronautics
and Space Administration

Scientific and Technical
Information Branch

Summary

The Lewis Research Center of the National Aeronautics and Space Administration has, since 1950, dealt with a variety of turbomachinery airflow problems that have challenged current analytical abilities. Typically these flows are subsonic or transonic, time varying, and three dimensional. Furthermore the physical structures affecting these flows, usually turbomachinery blading, are also time varying above and beyond simple rotations about the axis of the machine. Typical flow problems include inlet distortion, aeroelastic instability (e.g., flutter), and, most recently, nonrecoverable stall.

In the mid 1970's the author saw the need for a computational tool to transcend these flow field difficulties. Although a number of computer programs exist to deal with subsets of these problems, a quick review at that time showed that almost all such programs withered away to oblivion in the combined presence of these difficulties. The author therefore set out to produce a computational tool to deal successfully with all facets of such problems at the same time.

Two key rules were established at the outset. First, data input was not to include empirical information relevant to a particular engine, blade, flow field, or otherwise. This requirement has been the downfall of many other programs. Such programs tend to be "tweaked" for a particular engine or configuration and then fail to predict well for a different situation.

The second key rule was that computational cost was not to be considered as a limiting factor (although this was not to preclude programming efficiency when possible). Historical perspective shows that programs that appear unthinkably large in one decade usually turn out to be trivially small for the computing equipment of the next decade. Since the computational tool to be developed was expected to have a long lifetime, it was regarded as unwise to accept current computational power as a guideline in sizing the program.

This report presents the theoretical basis of the resulting computational tool and discusses (briefly) the current implementation of the tool. No results are reported since only incomplete results were obtained before the project was discontinued for nontechnical reasons. Because of the scope and volume of the work, other facets of the work (usage instructions, problem

statement details, etc.) are held in abeyance for future reporting.

Introduction

CASPER is a collection of computer routines that provide a solution or, more precisely, a simulation of Navier-Stokes flow through and around arbitrarily shaped bodies. Flows calculated are truly three dimensional, time varying, and viscous. No symmetry is required. Flow boundaries may also be arbitrary, nonsymmetric, and time varying.

Traditional solutions to the airflow problem are usually Eulerian in nature: a grid is defined within the flow field and the flow parameters at each grid point are calculated. Usually this approach, which is appealing for field theory conceptualizations, is appalling for boundary satisfaction. Arbitrary, time-varying bodies will often foil the Eulerian scheme completely because of either the inability to fit a grid to the flow field or the inability to transform the problem (or its solution) to or from some solution space.

The fundamental solution concept in CASPER is the Lagrangian aerodynamic element (aeroelement). This simple approach of "observing" a vast number of "air balls" as they proceed through a test area exchanges the nightmare of field theory computation for the nightmare of data-base management and computation. The solution validity hinges on the assumption that a large collection of small-scale, discrete Navier-Stokes solutions involving an aeroelement and several of its nearest neighbor aeroelements (also referred to just as neighbors) will closely approximate a large-scale, continuous solution of a Navier-Stokes flow. If this assumption is valid (which current experience would seem to indicate is the case), CASPER becomes mostly an effort in bookkeeping and computational effectiveness.

CASPER follows each individual Lagrangian aeroelement as it moves through the defined boundaries, maintaining a complete supply of information about the aeroelement. This information includes the position, velocity, acceleration, temperature, pressure (including a history of recent aeroelement pressures), volume (including a history of recent aeroelement volumes), mass, and list of nearest neighbors. Motion through the

defined boundaries is in short, iterative steps. Each such step involves a complete data-base revision sequence, resulting finally in revised values for the acceleration of each aeroelement. (CASPER performs these calculations in a consistent set of mass-length-time units; that is, regardless of what unit system is used to supply information to CASPER, it is assumed that a unit force is equal to a unit mass times a unit length divided by a unit time squared.)

Another key feature of CASPER is that the data for each aeroelement are accessible individually from those of all other aeroelements. By arranging the calculation sequence into phases that segregate inputs from outputs, CASPER can be worked on in parallel during any given phase of calculation. The Parallel, Asynchronous Executive (PAX) provides the management services necessary to calculate results in parallel (ref. 1).

CASPER is currently resident on a UNIVAC 1100/42 computer system operating under the EXEC VIII operating system. The problem used for CASPER testing required some 100 million bytes of mass storage for holding aeroelement data and problem description information. This test problem was considered small in comparison with real problems of current interest in the aeropropulsion industry.

This report details the theoretical basis of CASPER, suggests the basic Navier-Stokes simulation iteration, and touches upon some implementation details. Although the basic algorithms appeared to be operational, work was terminated before complete results could be obtained that would support any success or failure judgments. Therefore no computational results are presented in this report.

Symbols

A	presumed surface area of an aeroelement
a	acceleration
b	second-order tensor transformation coefficients
C	coefficient relating fluid normal stress to fluid normal strain rate in a Newtonian fluid
C_{HT}	coefficient of interaeroelement conductive heat transfer
c_v	coefficient of specific heat at constant volume
e	fluid strain rate
f	generic functions
g	acceleration of gravity
h	gradient direction of gravitational potential
J	Jacobian operator (i.e., the matrix of second partial derivatives)

P_{HT}	power of interaeroelement conductive heat transfer
p	static pressure
R	ideal-gas constant
S	fluid stress
T	aeroelement static temperature
t	time
U	aeroelement internal energy
u	velocity
W_c	work of aeroelement compression
W_d	work of aeroelement viscous distortion
x	coordinate direction, or position in a coordinate frame
δ_{ij}	Kronecker delta function ($\delta = 1$ for $i=j$; $\delta = 0$ for $i \neq j$)
θ	sum of fluid normal strain rates
λ	coefficient relating fluid normal stress to fluid shear strain rate in a Newtonian fluid
μ	first coefficient of viscosity
μ'	second coefficient of viscosity
ρ	static density

Subscripts represent coordinate directions unless otherwise noted.

Theoretical Basis

Overview

CASPER exists not as a single program but as a library of aeroelement data-base modification modules. Each module provides one modification of the aeroelement data base. It is only when the user causes these modules to be executed in succession that a Navier-Stokes flow simulation occurs.

The following sections highlight the theoretical basis behind some of the modules. The discussions are oriented toward individual computational goals and occasionally overlap several software modules. The implementation of the theory in actual modules is discussed in a later section.

Aeroelement Accelerations

Aeroelement accelerations are based on the Navier-Stokes equation derived below. The derivation is drawn from reference 2.

Consider the aeroelement mass shown in figure 1. The net elemental fluid stress in the x_1 direction is

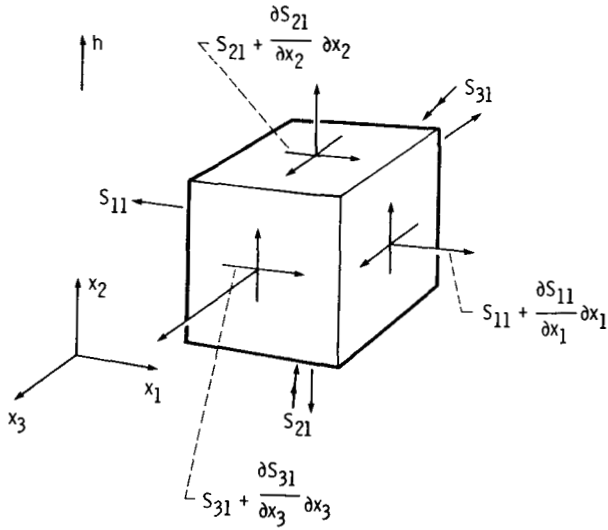


Figure 1.—Elemental fluid mass.

$$\left(\frac{\partial S_{11}}{\partial x_1} dx_1\right) dx_2 dx_3 + \left(\frac{\partial S_{21}}{\partial x_2} dx_2\right) dx_3 dx_1 + \left(\frac{\partial S_{31}}{\partial x_3} dx_3\right) dx_1 dx_2 = \frac{\partial S_{i1}}{\partial x_i} dx_1 dx_2 dx_3 \quad (1)$$

The force of gravity always acts in the negative h direction. The force of gravity in the x_1 direction is then

$$-g\rho \frac{\partial h}{\partial x_1} dx_1 dx_2 dx_3 \quad (2)$$

where g is the acceleration of gravity and ρ is the density of the aeroelement. By equating force to mass times acceleration (and thus assuming constant aeroelement mass), the following result is obtained:

$$\rho dx_1 dx_2 dx_3 a_1 = -g\rho \frac{\partial h}{\partial x_1} dx_1 dx_2 dx_3 + \frac{\partial S_{i1}}{\partial x_i} dx_1 dx_2 dx_3 \quad (3)$$

or

$$a_1 = -g \frac{\partial h}{\partial x_1} + \frac{1}{\rho} \frac{\partial S_{i1}}{\partial x_i}$$

where a_1 is the acceleration of the aeroelement in the first coordinate direction. This equation can be generalized for each axis as

$$a_j = -g \frac{\partial h}{\partial x_j} + \frac{1}{\rho} \frac{\partial S_{ij}}{\partial x_i} \quad (4)$$

The fluid is assumed to be Newtonian in nature, which confers upon it the following properties:

- (1) The fluid is isotropic.
- (2) The pressure p contributes directly to normal stresses.
- (3) Shear stresses are linearly related to shear strain rates.

If the coordinate system is taken to be that of the principal stresses and strains (which coincide for isotropic fluids), it is then assumed that

$$\left. \begin{aligned} S_{11} &= -p + Ce_{11} + \lambda e_{22} + \lambda e_{33} \\ S_{22} &= -p + \lambda e_{11} + Ce_{22} + \lambda e_{33} \\ S_{33} &= -p + \lambda e_{11} + \lambda e_{22} + Ce_{33} \end{aligned} \right\} \quad (5)$$

where S_{ii} is the principal fluid stress in the x_i coordinate direction and e_{ij} , the fluid strain rate, is

$$e_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

These equations can be rewritten as

$$\left. \begin{aligned} S_{11} &= -p + \lambda\theta + 2\mu e_{11} \\ S_{22} &= -p + \lambda\theta + 2\mu e_{22} \\ S_{33} &= -p + \lambda\theta + 2\mu e_{33} \end{aligned} \right\} \quad (6)$$

where

$$2\mu = C - \lambda$$

$$\theta = e_{11} + e_{22} + e_{33}$$

These equations can in turn be generalized as

$$S_{mn} = -p\delta_{mn} + \lambda\theta\delta_{mn} + 2\mu e_{mn} \quad (7)$$

Transforming to a primed, nonprincipal coordinate system gives

$$\begin{aligned} S_{ij} &= b_{mi} b_{nj} S_{mn} \\ &= b_{mi} b_{nj} (-p\delta_{mn} + \lambda\theta\delta_{mn} + 2\mu e_{mn}) \\ &= (-p\delta_{mn} + \lambda\theta\delta_{mn}) b_{mi} b_{nj} + 2\mu b_{mi} b_{nj} e_{mn} \\ &= -p\delta'_{ij} + \lambda\theta\delta'_{ij} + 2\mu e'_{ij} \end{aligned} \quad (8)$$

By dropping the primes the general relation

$$S_{ij} = -p\delta_{ij} + \lambda\theta\delta_{ij} + 2\mu e_{ij} \quad (9)$$

is obtained. The second coefficient of viscosity, $\mu' = \lambda + 2/3\mu$, is introduced and the relation becomes

$$S_{ij} = -p\delta_{ij} + \left(\mu' - \frac{2}{3}\mu\right)\theta\delta_{ij} + 2\mu e_{ij} \quad (10)$$

Substituting this expression into equation (4) produces

$$\rho a_j = -\rho g \frac{\partial h}{\partial x_j} - \frac{\partial p}{\partial x_j} + \frac{\partial}{\partial x_j} \left[\left(\mu' - \frac{2}{3}\mu\right)\theta \right] + \frac{\partial}{\partial x_i} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] \quad (11)$$

This equation is the Navier-Stokes relation and is used to obtain accelerations a_j based on the velocities and pressures of the aeroelements.

Calculation of Derivatives

CASPER calculates the derivatives of scalar quantities by inverting a Taylor series approximation to the function. The approximation is centered about the aeroelement location at which the derivative values are desired. The multidimensional Taylor series for a scalar function is

$$f(\bar{x} + \Delta\bar{x}) = f(\bar{x}) + \bar{\nabla}f(\bar{x})\Delta\bar{x} + \frac{1}{2}\Delta\bar{x}^T J[f(\bar{x})]\Delta\bar{x} + \dots \quad (12)$$

where

$$J[f(\bar{x})] = \begin{bmatrix} \frac{\partial^2 f(\bar{x})}{\partial x_1^2} & \frac{\partial^2 f(\bar{x})}{\partial x_1 \partial x_2} & \frac{\partial^2 f(\bar{x})}{\partial x_1 \partial x_3} \\ \frac{\partial^2 f(\bar{x})}{\partial x_2 \partial x_1} & \frac{\partial^2 f(\bar{x})}{\partial x_2^2} & \frac{\partial^2 f(\bar{x})}{\partial x_2 \partial x_3} \\ \frac{\partial^2 f(\bar{x})}{\partial x_3 \partial x_1} & \frac{\partial^2 f(\bar{x})}{\partial x_3 \partial x_2} & \frac{\partial^2 f(\bar{x})}{\partial x_3^2} \end{bmatrix}$$

This expression can be restated to consider the change in function value between two points in space as

$$f(\bar{x} + \Delta\bar{x}) - f(\bar{x}) = \bar{\nabla}f(\bar{x})\Delta\bar{x} + \frac{1}{2}\Delta\bar{x}^T J[f(\bar{x})]\Delta\bar{x} + \dots \quad (13a)$$

or

$$\Delta f = \bar{\nabla}f(\bar{x})\Delta\bar{x} + \frac{1}{2}\Delta\bar{x}^T J[f(\bar{x})]\Delta\bar{x} + \dots \quad (13b)$$

In CASPER, it is arbitrarily assumed that terms beyond the second order are negligible. Thus the truncated equation can be written in its expanded form as

$$\Delta f = \left\{ \frac{\partial f}{\partial x_1} \quad \frac{\partial f}{\partial x_2} \quad \frac{\partial f}{\partial x_3} \right\} \begin{Bmatrix} \Delta x_1 \\ \Delta x_2 \\ \Delta x_3 \end{Bmatrix} + \frac{1}{2} \{ \Delta x_1 \quad \Delta x_2 \quad \Delta x_3 \} \times \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} & \frac{\partial^2 f}{\partial x_1 \partial x_2} & \frac{\partial^2 f}{\partial x_1 \partial x_3} \\ \frac{\partial^2 f}{\partial x_2 \partial x_1} & \frac{\partial^2 f}{\partial x_2^2} & \frac{\partial^2 f}{\partial x_2 \partial x_3} \\ \frac{\partial^2 f}{\partial x_3 \partial x_1} & \frac{\partial^2 f}{\partial x_3 \partial x_2} & \frac{\partial^2 f}{\partial x_3^2} \end{bmatrix} \begin{Bmatrix} \Delta x_1 \\ \Delta x_2 \\ \Delta x_3 \end{Bmatrix} \quad (14)$$

In the following equation (as well as in subsequent equations of this section only), the subscript of the function value and the second subscript of position coordinates refer to values obtained with respect to the identified point in space. The first subscript of position coordinates identifies the coordinate direction as in previous equations. Thus x_{2i} represents the change in value in the second coordinate direction from the aeroelement position to the point "i" in space.

With this new subscript form in mind, equation (14) can be further expanded by using values from aeroelement neighbor "i" and the aeroelement itself as

$$\Delta f_i = \frac{\partial f}{\partial x_1} \Delta f_{1i} + \frac{\partial f}{\partial x_2} \Delta x_{2i} + \frac{\partial f}{\partial x_3} \Delta x_{3i} + \frac{1}{2} \{ \Delta x_{1i} \quad \Delta x_{2i} \quad \Delta x_{3i} \} \times \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} \Delta x_{1i} + \frac{\partial^2 f}{\partial x_1 \partial x_2} \Delta x_{2i} + \frac{\partial^2 f}{\partial x_1 \partial x_3} \Delta x_{3i} \\ \frac{\partial^2 f}{\partial x_2 \partial x_1} \Delta x_{1i} + \frac{\partial^2 f}{\partial x_2^2} \Delta x_{2i} + \frac{\partial^2 f}{\partial x_2 \partial x_3} \Delta x_{3i} \\ \frac{\partial^2 f}{\partial x_3 \partial x_1} \Delta x_{1i} + \frac{\partial^2 f}{\partial x_3 \partial x_2} \Delta x_{2i} + \frac{\partial^2 f}{\partial x_3^2} \Delta x_{3i} \end{bmatrix} \quad (15a)$$

or

$$\Delta f_i = \frac{\partial f}{\partial x_1} \Delta x_{1i} + \frac{\partial f}{\partial x_2} \Delta x_{2i} + \frac{\partial f}{\partial x_3} \Delta x_{3i} + \frac{1}{2} \left\{ \frac{\partial^2 f}{\partial x_1^2} \Delta x_{1i}^2 + \frac{\partial^2 f}{\partial x_1 \partial x_2} \Delta x_{1i} \Delta x_{2i} + \frac{\partial^2 f}{\partial x_1 \partial x_3} \Delta x_{1i} \Delta x_{3i} \right. \\ \left. + \frac{\partial^2 f}{\partial x_2 \partial x_1} \Delta x_{2i} \Delta x_{1i} + \frac{\partial^2 f}{\partial x_2^2} \Delta x_{2i}^2 + \frac{\partial^2 f}{\partial x_2 \partial x_3} \Delta x_{2i} \Delta x_{3i} + \frac{\partial^2 f}{\partial x_3 \partial x_1} \Delta x_{3i} \Delta x_{1i} + \frac{\partial^2 f}{\partial x_3 \partial x_2} \Delta x_{3i} \Delta x_{2i} + \frac{\partial^2 f}{\partial x_3^2} \Delta x_{3i}^2 \right\} \quad (15b)$$

If nine neighbor positions were available, the following matrix equation could be written:

$$\begin{pmatrix} \Delta f_1 \\ \Delta f_2 \\ \Delta f_3 \\ \Delta f_4 \\ \Delta f_5 \\ \Delta f_6 \\ \Delta f_7 \\ \Delta f_8 \\ \Delta f_9 \end{pmatrix} = \begin{bmatrix} \Delta x_{11} & \Delta x_{21} & \Delta x_{31} & \frac{1}{2} \Delta x_{11}^2 & \frac{1}{2} \Delta x_{21}^2 & \frac{1}{2} \Delta x_{31}^2 & \Delta x_{11} \Delta x_{21} & \Delta x_{21} \Delta x_{31} & \Delta x_{31} \Delta x_{11} \\ \Delta x_{12} & \Delta x_{22} & \Delta x_{32} & \frac{1}{2} \Delta x_{12}^2 & \frac{1}{2} \Delta x_{22}^2 & \frac{1}{2} \Delta x_{32}^2 & \Delta x_{12} \Delta x_{22} & \Delta x_{22} \Delta x_{32} & \Delta x_{32} \Delta x_{12} \\ \Delta x_{13} & \Delta x_{23} & \Delta x_{33} & \frac{1}{2} \Delta x_{13}^2 & \frac{1}{2} \Delta x_{23}^2 & \frac{1}{2} \Delta x_{33}^2 & \Delta x_{13} \Delta x_{23} & \Delta x_{23} \Delta x_{33} & \Delta x_{33} \Delta x_{13} \\ \Delta x_{14} & \Delta x_{24} & \Delta x_{34} & \frac{1}{2} \Delta x_{14}^2 & \frac{1}{2} \Delta x_{24}^2 & \frac{1}{2} \Delta x_{34}^2 & \Delta x_{14} \Delta x_{24} & \Delta x_{24} \Delta x_{34} & \Delta x_{34} \Delta x_{14} \\ \Delta x_{15} & \Delta x_{25} & \Delta x_{35} & \frac{1}{2} \Delta x_{15}^2 & \frac{1}{2} \Delta x_{25}^2 & \frac{1}{2} \Delta x_{35}^2 & \Delta x_{15} \Delta x_{25} & \Delta x_{25} \Delta x_{35} & \Delta x_{35} \Delta x_{15} \\ \Delta x_{16} & \Delta x_{26} & \Delta x_{36} & \frac{1}{2} \Delta x_{16}^2 & \frac{1}{2} \Delta x_{26}^2 & \frac{1}{2} \Delta x_{36}^2 & \Delta x_{16} \Delta x_{26} & \Delta x_{26} \Delta x_{36} & \Delta x_{36} \Delta x_{16} \\ \Delta x_{17} & \Delta x_{27} & \Delta x_{37} & \frac{1}{2} \Delta x_{17}^2 & \frac{1}{2} \Delta x_{27}^2 & \frac{1}{2} \Delta x_{37}^2 & \Delta x_{17} \Delta x_{27} & \Delta x_{27} \Delta x_{37} & \Delta x_{37} \Delta x_{17} \\ \Delta x_{18} & \Delta x_{28} & \Delta x_{38} & \frac{1}{2} \Delta x_{18}^2 & \frac{1}{2} \Delta x_{28}^2 & \frac{1}{2} \Delta x_{38}^2 & \Delta x_{18} \Delta x_{28} & \Delta x_{28} \Delta x_{38} & \Delta x_{38} \Delta x_{18} \\ \Delta x_{19} & \Delta x_{29} & \Delta x_{39} & \frac{1}{2} \Delta x_{19}^2 & \frac{1}{2} \Delta x_{29}^2 & \frac{1}{2} \Delta x_{39}^2 & \Delta x_{19} \Delta x_{29} & \Delta x_{29} \Delta x_{39} & \Delta x_{39} \Delta x_{19} \end{bmatrix} \begin{pmatrix} \frac{\partial f}{\partial x_1} \\ \frac{\partial f}{\partial x_2} \\ \frac{\partial f}{\partial x_3} \\ \frac{\partial^2 f}{\partial x_1^2} \\ \frac{\partial^2 f}{\partial x_2^2} \\ \frac{\partial^2 f}{\partial x_3^2} \\ \frac{\partial^2 f}{\partial x_1 \partial x_2} \\ \frac{\partial^2 f}{\partial x_2 \partial x_3} \\ \frac{\partial^2 f}{\partial x_3 \partial x_1} \end{pmatrix} \quad (16)$$

Given the aeroelement positions and the function values involved, this matrix equation could be inverted to yield all of the first and second derivatives of the scalar function at the location of the target aeroelement. It is assumed that only the derivatives

$$\frac{\partial f}{\partial x_1}, \frac{\partial f}{\partial x_2}, \frac{\partial f}{\partial x_3}, \frac{\partial^2 f}{\partial x_1^2}, \text{ and } \frac{\partial^2 f}{\partial x_2 \partial x_3}$$

$$\begin{pmatrix} \Delta f_1 \\ \Delta f_2 \\ \Delta f_3 \\ \Delta f_4 \\ \Delta f_5 \end{pmatrix} = \begin{bmatrix} \Delta x_{11} & \Delta x_{21} & \Delta x_{31} & \frac{1}{2} \Delta x_{11}^2 & \Delta x_{21} \Delta x_{31} \\ \Delta x_{12} & \Delta x_{22} & \Delta x_{32} & \frac{1}{2} \Delta x_{12}^2 & \Delta x_{22} \Delta x_{32} \\ \Delta x_{13} & \Delta x_{23} & \Delta x_{33} & \frac{1}{2} \Delta x_{13}^2 & \Delta x_{23} \Delta x_{33} \\ \Delta x_{14} & \Delta x_{24} & \Delta x_{34} & \frac{1}{2} \Delta x_{14}^2 & \Delta x_{24} \Delta x_{34} \\ \Delta x_{15} & \Delta x_{25} & \Delta x_{35} & \frac{1}{2} \Delta x_{15}^2 & \Delta x_{25} \Delta x_{35} \end{bmatrix} \begin{pmatrix} \frac{\partial f}{\partial x_1} \\ \frac{\partial f}{\partial x_2} \\ \frac{\partial f}{\partial x_3} \\ \frac{\partial^2 f}{\partial x_1^2} \\ \frac{\partial^2 f}{\partial x_2 \partial x_3} \end{pmatrix} \quad (17)$$

are nonzero. Thus the matrix equation is reduced to

This matrix, when inverted, yields two second-order derivatives that are not generally needed. Therefore CASPER algorithms invert only the first three rows of the matrix; however, this does not prohibit future implementations from performing the full inversion of the 9-by-9 matrix, should conditions warrant this.

CASPER provides an inversion (as specified above) of equation (17) for every aeroelement. Application of the inverted-matrix result quickly provides the gradient of any scalar quantity whose values are known on an aeroelement-by-aeroelement basis.

Some CASPER algorithms must calculate second derivatives of quantities. Since the CASPER derivative calculation procedure does not compute the information necessary to obtain these second derivatives directly, an alternative scheme is followed. In these cases the first derivatives of the quantity are calculated for all aeroelements in the normal manner; subsequently, the derivatives of the calculated first derivatives (in effect, the second derivatives of the quantity) are calculated by the same procedure.

Fluid Element Movement and Physical Boundaries

The most difficult task within CASPER is the movement of aeroelements through realistic physical boundaries. Two simplifying assumptions have been made. First, physical boundaries must be describable as mathematical entities rather than as collections of points in space. Second, the parameters governing these mathematical entities must be explicitly known during the period of time that motion is to take place.

The first assumption leads naturally to the formulation that any boundary is described as the locus of points in space-time for which

$$f(\vec{x}, t) = 0 \quad (18)$$

If

$$f(\vec{x}, t) > 0$$

the point in space-time is in the portion of space that is not occupied by the physical object behind the boundary.

If

$$f(\vec{x}, t) \leq 0$$

the point in space-time is in the portion of space occupied by that physical object.

Clearly, finding one such function that will suffice for any real problem (e.g., an axial-flow turbomachine) is a practical impossibility. Thus CASPER allows the range of influence of a given boundary to be limited by other described surfaces (known as surface truncations) and for many such truncated surfaces to be, effectively,

concatenated into any desired combination. Mathematically, truncation can be stated as follows: If for all indicated truncation surfaces i ,

$$f_i(\vec{x}, t) \geq 0$$

then

$$f(\vec{x}, t) = f(\vec{x}, t) \quad (19)$$

otherwise

$$f(\vec{x}, t) = 1$$

As currently implemented, truncation services can be nested to any practical depth. This allows truncation surfaces, themselves, to be truncated.

The concatenation of surfaces is a byproduct of surface truncation rather than a true mathematical conjunction mechanism. Since a truncated surface will always return a safe (nonviolating) surface value outside its range of influence, the problem description is free to supply another surface in that area of space-time. Thus, by limiting the range of influence of each surface, many surfaces can be provided to describe complex shapes.

Another key feature of the surface truncation mechanism is that the distinction between safe surface values obtained by truncation and those obtained by nontruncated surface evaluation is retained and available to the user. This feature is useful in defining other spatial structures.

Actual surfaces defined in CASPER also provide the gradient of the surface function and the velocity and acceleration of any point in space that is moving in free-body synchronism with the surface. These values are available everywhere in the space-time continuum with the possible exception of points of singularity for the surface function. These additional surface characteristics are always evaluated without regard to any described surface truncations. It is up to the invoking algorithm to establish the validity (or influence) of a given surface before using these additional characteristics.

The second major assumption, explicit knowledge of parameters, is necessary for the segregation of inputs and outputs. One of the goals of CASPER was a high degree of interaction between aerodynamic forces and structural motion; however, to include such interactions at the incremental aeroelement motion level would have given rise to a logical loop without resolution.

Thus the shape of all objects in a CASPER problem must be explicitly known at the outset of each incremental motion calculation. Time variations are allowed provided that they are explicitly known, as other parameters are, at the outset of computation for the incremental period. (Indeed, within the CASPER surface evaluation package, time variation parameters are

indistinguishable from all other parameters; only within the incremental motion package is a space-versus-time distinction made.)

This restriction does not inhibit relating aerodynamic force and structural motion. Instead, such considerations are moved to the point in time (truly a point, i.e., a span of zero duration) between successive incremental motion periods. At that point, surface parameters can be set to new values according to any desired scheme. Typically the newly revised aerodynamic load history would be used to project a new structural motion for the next incremental motion period. Presumably this new motion would affect the aerodynamics of the upcoming incremental motion period.

The process of aeroelement motion begins simply with the integration of the aeroelement accelerations. These accelerations are assumed to be constant through the time period. Thus

$$\begin{aligned} u_i(t + \Delta t) &= u_i(t) + \int_t^{t+\Delta t} a_i dt \\ &= u_i(t) + a_i \Delta t \end{aligned} \quad (20)$$

and

$$\begin{aligned} x_i(t + \Delta t) &= x_i(t) + \int_t^{t+\Delta t} u_i(t) dt \\ &= x_i(t) + u_i(t) \Delta t + \frac{1}{2} a_i \Delta t^2 \end{aligned} \quad (21)$$

At this point the constraints of boundaries must be accommodated. This is first enforced by requiring

$$f[\bar{x}(t + \Delta t), t + \Delta t] \geq 0 \quad (22)$$

for each appropriate boundary function f . Since boundaries that do not apply will presumably fall to surface truncations and report values for f of +1, this condition is sufficient. However, it soon becomes clear that for realistic problems the calculation burden of comparing millions of aeroelement positions to thousands of surfaces would best be avoided.

CASPER reduces this effort by requiring the definition of flow zones in the problem statement and the listing of any and all boundaries resident (in whole or in part) in each flow zone. Flow zones are defined by surfaces (usually truncated) in the same manner as physical boundaries. The condition for residence in a flow zone is

$$f(\bar{x}, t) \geq 0 \quad (23)$$

where f is appropriate for the particular flow zone and is not determined by truncation of the surface (i.e., if the surface evaluation encounters truncation and returns the automatic value of +1, the point of evaluation is not considered to be in the described flow zone). CASPER determines and retains for each aeroelement the current flow zone of residence. By reviewing the resident boundary list for the appropriate flow zone, the number of comparisons necessary to satisfy the conditions of equation (22) can be reduced.

Additional information establishing the neighbor flow zones for each flow zone is used to narrow the range of search when an aeroelement flows out of one flow zone and into another. Current implementations of CASPER do not support automatic, time-varying alterations of the information on flow-zone neighbors or flow-zone resident boundaries. However, there is nothing in the CASPER algorithms that prohibits the change of such information on a dynamic basis.

When aeroelement motion results in boundary violation (as in fig. 2), the point of violation is found by a simple bisection iteration, where the bisected variable is time and position is treated as parametric in time. When this point of violation is found, corrective measures are applied to the aeroelement datum to alter its path through space from the point of violation. First, the velocity of the aeroelement is reset in a calculation that equates the angle of incidence to the angle of reflection. Thus the aeroelement bounces elastically at the point of violation. This calculation is carried out with respect to the motion of the surface at the point of violation. In this way, if the aeroelement is motionless and the boundary is moving, velocity is imparted to the aeroelement to move it out of the way of the boundary. Second, if boundary violation occurs without apparent motion of the aeroelement normal to the boundary, the acceleration of the aeroelement normal to the boundary is set to zero. This corrects problems that can occur when the aero-

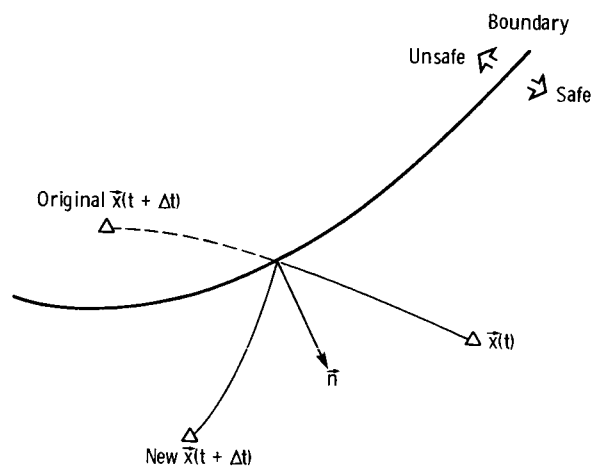


Figure 2.—Boundary violation.

element is differentially close to the boundary and has an acceleration that, at least in part, is into the boundary. (In this instance it can become computationally impossible to locate any point forward in time, even after velocity alteration, that does not produce a boundary violation.)

This formulation of boundary violation checking works well for surfaces with large object depths; however, for thin objects (such as corners and edges) a phenomenon referred to as "passthrough" becomes a problem. Regardless of the duration of the incremental motion period, sharp corners will fail to deflect some aeroelement paths that should be deflected (fig. 3). To reduce this effective dulling of sharp edges, the initial urge is to shorten the motion time, thus reducing the distance traveled between boundary checks. Although this is effective, it can also be quite costly since it brings with it increased resolution in the entire Navier-Stokes simulation process. CASPER offers an alternative by allowing the calculation of a user-specified number of intermediate aeroelement positions, which are all based on the original position, velocity, and acceleration information.

The intermediate-positions option allows the user to set the flow field resolution and the edge sharpness independently, provided that the edge sharpness is the more restrictive constraint. It is, of course, desirable not to oversharpen edges, since this still requires additional surface comparisons. It is expected that future implementations of CASPER will adjust edge sharpness dynamically. Probably a lower sharpness limit will be set

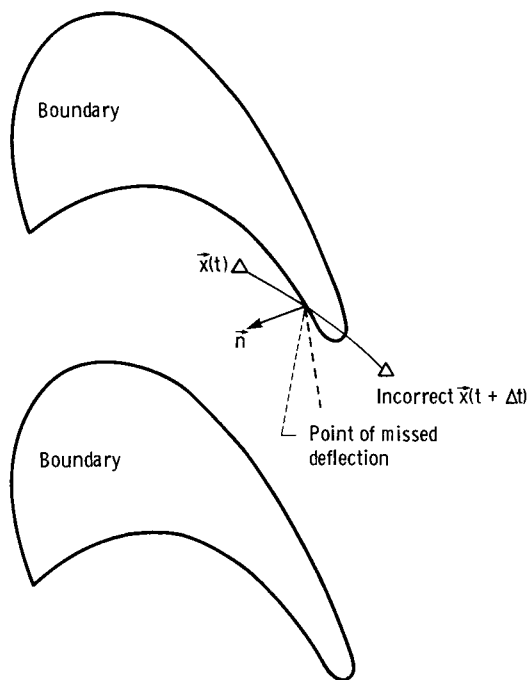


Figure 3.—Boundary passthrough phenomenon.

and will be increased from that point in proportion to the proximity of the boundary to the aeroelement.

Finally CASPER provides the ability, on an aeroelement-by-aeroelement basis, to disable the standard aeroelement motion algorithm from repositioning an aeroelement. In this event it becomes the user's responsibility to provide and invoke routines that move (or do not move, as appropriate) the affected aeroelements. This feature is intended, principally, for the simulation of boundary layer flows by attaching some aeroelements to the boundaries while other aeroelements flow past the attached aeroelements.

Thermodynamic Effects

All thermodynamic calculations in CASPER result in power quantities that, when multiplied by the time increment duration, give the amount of work transferred into a particular aeroelement. CASPER computes for each aeroelement the power of compression, the power of viscous aeroelement distortion, and the rate of heat flow (adjusted to units of power). In all cases flow of energy into the aeroelement is taken to be positive. At an appropriate time in the Navier-Stokes simulation loop, these powers are summed, multiplied by the time increment duration, and used to alter a total, internal energy value for each aeroelement. This internal energy is then related to aeroelement temperature through a simple coefficient-of-specific-heat relation.

From fundamental thermodynamics the compressive work done on an aeroelement is

$$W_c = \int p dv \quad (24)$$

The CASPER data base records the five most recent pressure and volume values for each aeroelement. The three most recent of each of these values (the most recent of which is the current value for the aeroelement) are used to establish parabolic approximations for pressure and volume as functions of time. These approximations are substituted into the expression for the work of compression, and the result is parametrically integrated from the time of the previous pressure and volume value to the time of the current values. Although currently the pressure and volume histories must be equally spaced in time, this constraint can be removed, if necessary, by simple programming (i.e., no other CASPER module depends on the spacing of pressure and volume histories). Finally the work of compression is divided by the time-increment duration to establish an equivalent power.

The power of viscous distortion arises from the resistance of the fluid to deformation. As delineated in reference 3, given the Newtonian fluid assumption of the Navier-Stokes equation, the distortion work can be calculated as

$$\begin{aligned}
W_d &= v \left[\frac{\partial}{\partial x_1} (u_1 S_{11} + u_2 S_{12} + u_3 S_{13}) \right. \\
&\quad + \frac{\partial}{\partial x_2} (u_1 S_{21} + u_2 S_{22} + u_3 S_{23}) \\
&\quad \left. + \frac{\partial}{\partial x_3} (u_1 S_{31} + u_2 S_{32} + u_3 S_{33}) \right] \\
&= v \left[\frac{\partial}{\partial x_i} (u_j S_{ij}) \right] \quad (25)
\end{aligned}$$

From equation (10) this becomes

$$W_d = v \frac{\partial}{\partial x_i} \left\{ u_j \left[-p \delta_{ij} + \left(\mu' - \frac{2}{3} \mu \right) \theta \delta_{ij} + 2 \mu e_{ij} \right] \right\} \quad (26)$$

Again, the computed work is divided by the duration of the time increment to obtain a power-of-viscous-distortion value.

Finally simple conductive heat flow between neighbor aeroelements is considered. Heat flow per unit time is simply taken to be proportional to the difference in the temperatures of the two aeroelements, the average of the heat transfer coefficients, the average presumed surface areas of the aeroelements, and the inverse of the distance between them. Thus

$$P_{HT} = \frac{(T_j - T_i)(C_{HT_j} + C_{HT_i})(A_j + A_i)}{4D_{ij}} \quad (27)$$

where the subscripts i and j denote distinct aeroelements and D_{ij} is the distance between those aeroelements. This computation yields a power term directly. It is only important to assure that the units of the coefficient of heat transfer are such as to yield a number consistent with the previously determined powers of compression and viscous distortion.

When all of the sources of energy are accounted for, the aeroelement temperature is revised on the basis of the assumption

$$\Delta U = c_v \Delta T \quad (28)$$

where c_v is the coefficient of specific heat at constant volume.

Convective heat transfer is not considered explicitly in the thermodynamic model since aeroelements are not constrained against intermixing. Aeroelements are not algorithmically required to maintain the same neighbors throughout the iterative loop process. Aeroelements are

free to follow independent paths through space, intermix with new neighbor aeroelements, and transfer heat with these new neighbors. This provides a crude convective heat transfer mechanism.

Pressure and Volume Calculations

CASPER provides the ability to calculate the current pressure and volume of aeroelements from current temperature, mass (which never changes throughout the computational lifetime of an aeroelement), and proximity of neighbors. Fundamental to this calculation is the estimation of volume. CASPER begins the volume estimation process by averaging the distances from the subject aeroelement to each of the nearest neighbors of the aeroelement. This value is then used as a radius for a simple spherical volume determination.

It was foreseen that a correction would be needed to accommodate aeroelements with a vacuum on one side and fluid on the other side. In this case an aeroelement with a large volume on one side would be miscalculated as having a normal volume on the basis of the proximity of neighbors on the other side. Therefore a correction based on the solid angle subtended by the nearest neighbors of the aeroelement was implemented. This angle is compared with the average solid angle for all aeroelements (usually obtained during the previous simulation cycle). As the solid angle of a particular aeroelement deviates below average, the initial volume estimate for that aeroelement is increased. Solid angle deviations that are above the average cause the aeroelement volume estimate to be decreased. However, the algorithm is such that the response to above-average solid angles is much less than to those below the average. Above-average solid angles would seem only to indicate an unusual dispersion of nearest neighbors about an aeroelement that is, in fact, fully immersed in the fluid continuum.

It is clear that these initial estimates will not be correct in an absolute sense but will be proportionately correct on an aeroelement-to-aeroelement basis. Thus a final correction is begun by summing all of the aeroelement volume estimates and comparing the result to the known total volume of the flow zones of the problem. A simple multiplicative correction factor is then produced and applied to the volume estimate of each aeroelement to convert proportionately correct values to absolutely correct values.

With the volume result available, the calculation of the density of each aeroelement (given the mass of that aeroelement) is trivial. Calculation of the pressure of each aeroelement (given the previously determined temperature of the aeroelement) is done through the ideal-gas law

$$p = \rho RT \quad (29)$$

CASPER supplies this gas law as a subroutine. Thus alternative gas laws (including table-lookup style laws) can be substituted merely by supplying an appropriate subroutine of the same name. In this way, real gases can be supported by the ingenious CASPER user.

Establishing Neighbor Aeroelements

Many CASPER algorithms hinge on knowing the identification of several (currently five) nearest-neighbor aeroelements for each aeroelement. This is primarily a bookkeeping chore and represents no theoretical insight at all. The criterion for selecting nearest neighbors is a straightforward center-to-center distance comparison of the aeroelements. The principal goal of nearest-neighbor-finding algorithms is to limit the computational cost by limiting the number of nearest-neighbor candidates. CASPER offers three nearest-neighbor-finding algorithms: (1) a full exhaustive search, (2) a search limited by flow zone relations, and (3) a search through the current nearest-neighbor tree.

The exhaustive-search algorithm for finding nearest neighbors of a particular aeroelement (referred to as the target aeroelement) is very simple. The distance from the target aeroelement to every other aeroelement in the population is computed and compared with the current list of nearest neighbors. If the new distance is shorter than the distance to one of the current nearest neighbors, a simple ordered-list replacement (which discards the furthest nearest neighbor and inserts the new nearest neighbor at the appropriate point in the list) is performed. This nearest-neighbor finder may produce dubious results in an algorithmic sense since no consideration is given to the possibility that boundaries may exist between the aeroelement and its selected neighbors. This is called bogus-nearest-neighbor-syndrome (BNNS).

The flow-zone-related search algorithm limits the number of nearest-neighbor candidates by requiring each candidate to be resident either in the flow zone of the target aeroelement or in a flow zone that is a neighbor to the flow zone of the target aeroelement. This approach can eliminate the problem of bogus neighbors being selected from flow areas that are physically close but problematically far. The improvement in search time is clear but may not be sufficient if there are still large numbers of aeroelements in each flow zone. If this nearest-neighbor search algorithm is to be used extensively, it is vital that the problem statement be designed with a feasible average number of aeroelements per flow zone.

The nearest-neighbor-tree search allows the user to specify an arbitrary number of candidates for inclusion in the nearest-neighbor search, thereby providing firm control of the search time. Candidates are drawn from the current nearest-neighbors tree for the target aero-

element (i.e., the current neighbors of the target aeroelement, the current neighbors of the neighbors of the target aeroelement, the current neighbors of the neighbors of the neighbors, and so on). Checks are made to ensure that redundant entries are not made in the neighbor tree and that the target aeroelement does not become its own nearest-neighbor candidate. This algorithm attempts to restrict BNNS by requiring that candidate aeroelements reside either in the flow zone of the target aeroelement or in a flow zone neighbor to the flow zone of the target aeroelement. This approach also assumes that the initial neighbor tree was an essentially valid, well-cross-linked representation of the true neighbor structure (in particular that, if followed far enough, the neighbor tree would eventually involve all aeroelements in the population). If the initial tree were not valid (for instance, if the target aeroelement and its five nearest neighbors all listed each other as neighbors), the neighbor-tree search algorithm would do nothing to improve the validity of the nearest-neighbor list of the target aeroelement.

Aeroelement Relocation

Most problems involve the flow of fluid from a source area through a test area to an exhaust area. To provide a supply of new aeroelements for the source area, CASPER extracts all aeroelements from the designated exhaust area, combines them with all aeroelements currently resident in the source area, and reinitializes the entire set of aeroelements (provided it is nonnull) in the source area. This requires a complete resetting of the data base of each such aeroelement, including new position, velocity, mass, and temperature. The user is required to provide problem-specific routines that generate realistic numbers for this process. This facility can be disabled to allow closed-circuit or closed-box systems to be modeled. In this case, the user-supplied routines, if called, will simply take no action.

Note that during this relocation phase, the user has the opportunity to simulate various interesting conditions and to effect problem control adjustments. For instance, in providing information about aeroelements being relocated to the inlet, the user could model inlet distortions in both pressure and temperature. Also, the user could perform acts such as adjusting the temperatures of aeroelements in combustor flow zones to achieve or maintain a desired combustor exit temperature schedule. The possibilities for user manipulation are endless.

Flow Field Simulation Sequence

Figure 4 presents a possible sequence of CASPER module utilization to simulate a fluid flow. The figure does not represent information specific to current

- 1.0 Initialize data base and establish starting conditions.
- 2.0 Establish nearest-neighbor relationships.
- 3.0 Calculate
 - 3.1 Aeroelement volumes
 - 3.2 Aeroelement densities
 - 3.3 Aeroelement pressures
- 4.0 Establish derivative calculation matrix for each aeroelement.
- 5.0 Calculate Navier-Stokes accelerations for each aeroelement.
- 6.0 Calculate
 - 6.1 Aeroelement powers of compression
 - 6.2 Aeroelement powers of viscous distortion
 - 6.3 Aeroelement conductive heat transfers
 - 6.4 Aeroelement temperature changes
- 7.0 Adjust boundary parameters to reflect boundary conditions for next aeroelement motion period.
- 8.0 Move aeroelements through space by integrating accelerations.
- 9.0 Remove aeroelements from the exhaust zone, insert them in the inlet zone, and reinitialize inlet zone aeroelement data.
- 10.0 Go to step 2.0.

Figure 4.—Possible flow simulation sequence.

CASPER implementation but rather covers only the fundamental logic of the approach. The most striking feature of the sequence is that there is no exit. CASPER does not search for any convergence condition. Instead it continues to produce flow results without end. A settling-in period exists when problem simulation first begins; however, it is up to the user to identify the end of this period since CASPER cannot recognize it on its own.

Two additional problems intertwine themselves in CASPER problems: inducing flow, and isolating the test area from unintended inlet and exhaust area distortions. Figure 5 shows a diagram of a simple flow problem that illustrates simple solutions to both these problems.

First, a fluid does not start flowing by itself. At the very least, a pressure gradient or gravitational force must be applied to obtain continuous fluid flow. Simply placing aeroelements in a test area does not accomplish this. One could supply sufficiently massive aeroelements to the inlet zone of the example problem during each aeroelement relocation phase to maintain a given inlet plenum pressure or a given inlet pressure ratio between the inlet and exhaust plenums. This would not provide independent control of the two plenum pressures (which

could be a problem requirement). Furthermore the validity of flow-to-vacuum simulations is in some doubt. This could cause aberrations of the results upstream of the vacuum face.

A second alternative could be for a user routine to selectively remove mass from exhaust plenum aeroelements. This would provide independent control of plenum pressures. The difficulty with this approach is that the rationale for selecting the mass reductions is not nearly so clear as that for initializing aeroelements in the inlet plenum. Should all exhaust plenum aeroelements be reduced in mass or only those toward the rear of the plenum? Should a uniform pressure distribution or a pressure gradient result? Should temperature or velocity be adjusted too? Individual users may wish to assert and implement their own answers to these questions (which would be entirely possible within the existing CASPER framework); however, the author sought a third alternative.

The flow-induction alternative the author selected was to model an additional part of the apparatus that would be used in an actual experiment: a centrifugal exhauster. This approach strikes a blow both at inducing flow and at isolating poor flow simulations from the test area. In using this approach, it is necessary to admit that flows in the exhauster may not be realistic. However, the author feels that expecting flows upstream of the exhauster to be realistic is a much more comfortable idea. Furthermore there are no questions to ask about mass removal. Aeroelements are driven around in a circle by the exhauster blading until centrifugal force drags them out into the exhaust zone, where they disappear into the aeroelement relocation algorithms. Also, exhaust plenum pressure is controlled by adjusting the rotational speed of the exhauster model.

Implementation

Overview

The implementation of key CASPER modules is presented here to add corroborative detail in the absence

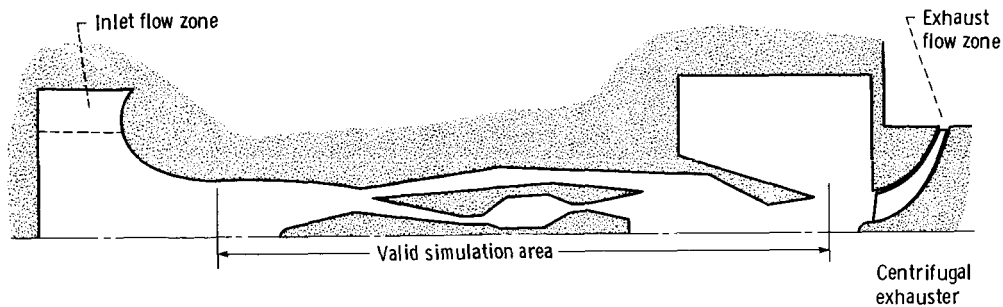


Figure 5.—Cross section of a simple flow problem for CASPER.

of computational results. The listings presented are actual, compiled CASPER code modules. The reader is cautioned that the comments contained in these listings, while generally accurate and up to date, are not guaranteed to represent the exact truth of the code presented. As always, the final arbiter of computational truth is the language statements and the interpretation thereof by the language compiler. The reader is also advised that the symbols previously used in this report are not (always) used by the CASPER codes presented in the listings. In the following discussion of the listings the symbols used by the code will be used as they appear in the listing.

Some elements of the CASPER code presented may appear confusing because of the parallel-processing nature of CASPER. For instance, because of the requirements of parallel processing, results are often stored in scratch slots for later copying back to the formal result slot. It is not within the scope of this report to provide a tutorial on parallel processing and thus these oddities will be ignored.

Finally no specifics about the use of these codes for actual computation are provided. Information such as program building instructions, program use instructions, and data preparation is beyond the scope of this report.

Calculation of Derivatives

The inversion of a Taylor series to provide derivative calculation information is provided by the CASPER module INTF presented in listing 1. This module, in turn, calls the subroutines MATRIX, DET4, and DET3 (listings 2, 3, and 4, respectively). The fundamental flow of control is to invoke the matrix construction and inversion subroutine, MATRIX, for each aeroelement in the aeroelement identification range provided to INTF (i.e., aeroelement identification numbers in the range IL to IH). If MATRIX reports a matrix singularity fault, the event is logged (by calling ERROR2, an environmental service provided by PAX), and an attempt to clear up the problem (by revising the nearest-neighbor list to provide a different matrix for inversion) is made by calling the subroutine CLNINT (which is not presented as a listing in this report).

MATRIX (listing 2) constructs the 5-by-5 matrix of spatial differentials on the basis of the proximity of the listed nearest neighbors for the identified aeroelement (lines 79 to 84). The partial inversion of the matrix proceeds in lines 85 to 105 by the transform-of-cofactor method. This method relies on the fact that the inverse of a matrix is the quotient of the transform of the cofactor matrix divided by the determinant of the matrix. This method was selected since it allows partial inversions to be calculated. Only the determinant and the cofactors of the diagonally reflected term desired need to be

calculated to determine the inverse matrix entry for any particular term.

Evaluation proceeds in MATRIX by constructing 4-by-4 matrices (and then, a 3-by-3 matrix in DET4) whose determinants are evaluated to provide the cofactors of the desired terms. The determinant of the original 5-by-5 matrix is evaluated at the first opportunity (lines 99 to 101) and a check is made to see if a singularity problem exists before any further effort is expended. If a singularity problem does exist, the aeroelement is marked as not having a current derivative calculation matrix (lines 108 and 109) and the problem is reported to the calling routine (line 107). If a singularity problem is not detected, the final construction and storage of a 3-row-by-5-column derivative calculation matrix is performed by lines 114 to 119 of the listing. This process includes clearing the derivative matrix not-available flag for the particular aeroelement.

DET4 and DET3 (listings 3 and 4) show the determinant calculation process reduced to the point where the determinant can be calculated directly by formula. Although the entire computational strategy is crude, it has the advantage of working and already being coded and debugged. If CASPER were to be continued into a computational production phase, these algorithms could be improved remarkably.

Calculation of Aeroelement Acceleration

STOK1 and STOK2, the CASPER modules that calculate aeroelement accelerations, are presented in listings 5 and 6. The computation of the accelerations must proceed in two phases since derivatives of terms involving derivatives must be calculated. This requires that the terms involving derivatives must be calculated for all aeroelements before the derivatives of the derivative terms can be determined by the application of the derivative calculation matrix. Note that each routine avoids the acceleration computation entirely if the derivative calculation matrix is not available (see line 104 of listing 5 and line 114 of listing 6). Also, note that various aeroelement information is stored in variables local to the subroutine to avoid the overhead expense of repeated access to values in shared, software-virtualized storage. Finally note that these routines calculate the contribution of all of the terms of equation (11) except the gravitational term.

The first phase of computation, STOK1 (listing 5), proceeds to calculate the derivatives of velocity and the fluid strain rate matrix by applying the derivative calculation matrix (lines 113 to 129). The full strain rate matrix is stored in the aeroelement record for use by other CASPER modules. An additional term (whose derivative must be determined in the second phase of the acceleration calculation) involving viscosity and principal

fluid strains is calculated and stored in the aeroelement record (lines 130 to 135).

The second phase of computation, STOK2 (listing 6), completes the calculation of aeroelement acceleration by the Navier-Stokes equation. A preliminary check of aeroelement density for approximate equality to zero is made (line 117) to avoid a possible divide fault (line 165). Again, a number of localizations of aeroelement information are performed to avoid shared-data access overheads. The gradients of the pressure (lines 139 to 144) and of the viscosity-and-principal-fluid-strain term (lines 145 to 150) at the aeroelement are calculated by using the standard derivative calculation procedure. An implied tensor sum of the derivatives of the product of viscosity and fluid strains is calculated by lines 151 to 163. Finally, on lines 164 to 166, these three principal terms are combined to form the aeroelement accelerations in each coordinate direction. These accelerations are then stored in the aeroelement record.

This two-phase process completes the computation of aeroelement acceleration through the Navier-Stokes equation. The only term neglected is the gravitational component. It is important to note that, given the data base available for each aeroelement, especially the derivative calculation matrix, which allows gradients to be inferred from the differences in scalar function values, the calculation of accelerations through the Navier-Stokes equation is almost trivial.

Aeroelement Positioning and Physical Boundaries

MOVEL, SURF, and SA100 (listings 7, 8, and 9) present key components of the aeroelement positioning package. Although the actual logic and programming of the aeroelement positioning process (which simply integrates acceleration and velocity to establish position) can appear to be quite involved, it must be borne in mind that underlying it all is a basically simple vision of motion through space subject to real boundaries.

Subroutine MOVEL (listing 7) is the main component of the aeroelement positioning module of CASPER. It implements the aeroelement acceleration integration algorithm and invokes the various boundary evaluation services to enforce the boundary constraints of the problem. An argument supplied to the subroutine (NINC) specifies the number of time subincrement steps to be taken to sharpen boundary edges. Again, aeroelement information is localized to minimize shared-data-access overheads.

The principal aeroelement positioning sequence occurs in lines 304 to 307 of listing 7. The internal subroutine SPC (defined by lines 459 to 482 of the listing) projects the course of the aeroelement on the basis of the current aeroelement position, velocity, and acceleration from formulas based on the classic double integration of

acceleration. The internal subroutine YNM (defined by lines 483 to 536) checks to see if the new position violates any boundaries in the problem. (Note that the subroutine establishes the flow zone of residence for the new position and then checks the position against all boundaries (1) in flow zone 1 (always) and (2) in the flow zone of residence for the new position.) Assuming that no problems have occurred in tracking the flow zone of residence (line 306), a test is performed (line 307) to see if a boundary violation has occurred. Assuming that no such violation has occurred (and that corrective measures left over from the resolution of such a violation are not pending, as determined in line 308), the time subincrement loop is repeated until all of the intermediate aeroelement positions have been determined and tested. The final aeroelement position and flow zone are stored in the aeroelement record by lines 453 to 456.

The handling of a detected boundary violation is begun with lines 375 to 445. A simple bisection loop is implemented to determine the position of violation to within a small variation (since real computations are very seldom exact). To begin this process, lines 375 to 402 are concerned with establishing points on both sides of the boundary (i.e., one point in violation and one point not in violation). Lines 404 to 423 perform a simple bisection search, where the bisected variable is time and where position is treated as parametric in time. Note that, as a safety precaution, this bisection process will always terminate after a fixed number of iterations even if the required resolution in time (line 405) has not been reached. Lines 442 to 445 effect adjustments to subroutine variables to cause the next principal position loop (lines 304 to 307) to position the aeroelement just short of the violated boundary (by adjusting the time span variable T), and to cause the course correction process to occur when (and if) that position has been successfully attained.

The course correction process is implemented by lines 309 to 355. The velocity of the aeroelement relative to the surface is established (lines 323 to 325), the velocity is adjusted by an elastic reflection method (lines 326 to 336), and the result is converted back to the absolute frame of reference (lines 337 and 338). If necessary (line 339), the component of aeroelement acceleration into the boundary (normal to the boundary, relative to the acceleration of the boundary) is set to zero by lines 340 to 350. The need to zero the normal acceleration component is determined if, during the bisection process that established the point of violation, the nonviolating point was never replaced with an updated value. Although no theoretical statement exists on this subject, this condition is presumed to indicate that the aeroelement is differentially close to the boundary already and cannot get up the necessary velocity to bounce off the boundary.

Thus, to move the aeroelement forward in time, it is necessary to disable its ability to violate the boundary by at least turning off its acceleration into the boundary.

This completes the discussion of the principal features of the aeroelement positioning process. The boundary description services have, for the most part, been submerged in calls to the YNM subroutine and in a few discrete calls to other boundary services. Listings of many of these boundary services are not included in this report since they are trivial invocations and recombinations of the fundamental boundary service features presented in listing 8.

Listing 8 presents the control point of all boundary services, the subroutine SURF. All requests to evaluate surface values, gradients, velocities, and accelerations are handled by this one, universal, fits-all routine. Control within this routine falls into three major categories: (1) specification of the desired result and transfer of control (lines 547 to 615), (2) handling of the surface truncation process (lines 622 to 719), and (3) fundamental surface evaluations (lines 724 to 752).

The desired-result-specification-and-transfer-of-control sections simply set various internal variables to turn various features of the SURF subroutine on or off. The variable ISW selects the computational results of the fundamental surface evaluation functions (of which listing 9, subroutine SA100, is an example). The variable NRTN controls the return of control from the fundamental surface evaluation section to the appropriate invoker. The surface gradient, velocity, and acceleration requests all ignore the surface truncation mechanisms and thus transfer control directly to the fundamental-surface-evaluation section and receive control directly back from that section when surface evaluation is complete. The desired-result-specification-and-transfer-of-control sections also provide a conversion from surface identification number to the surface header pointer, IP.

The fundamental-surface-evaluation section (lines 724 to 752) provides a simple calling mechanism to invoke the appropriate surface evaluation routine and to obtain the desired fundamental result (accomplished by lines 724 to 727). Once a base result is obtained, certain optional modifications may be made to it as invoked by the requesting section (lines 734 to 739). Finally control is transferred back to the invoking code section.

The surface-truncation-handling section is, by far, the most complicated area of code since it is, in fact, a recursive code written in a nonrecursive language. If a recursion of the truncation process is, in fact, occurring, lines 622 to 637 save the current surface context on a (software implemented) stack and initiate a new surface context by setting the surface description header pointer IP. If further truncations have not been inhibited (usually by selecting a result-specification-and-transfer-of-control section), a check is made to see if truncations to this

surface exist (line 640). If no truncations exist, control is transferred to the fundamental-surface-evaluation section and, upon completion of the surface evaluation, the truncation-and-surface-evaluation process is unwound.

If one or more truncations do exist, the truncation recursion process is begun at a new level. Lines 641 to 650 perform various initializations associated with the truncation process, including locating a list of truncation headers that include descriptive information about each truncation. The code then loops through each truncation header (lines 651 and 652), obtains appropriate information from each truncation header in turn (lines 653 to 665), and recursively invokes the truncation process (line 666) to establish the surface value for each truncation surface. The recursion process continues until a truncation surface is found that does not, itself, list any further truncation surfaces. Thus the mechanism of truncating truncations to build up complex truncation surfaces through spatial concatenation can occur.

When a truncation surface evaluation finally does occur, control is returned to line 672, where a final surface value modification obtained from the truncation header is applied. This allows the user to use existing surfaces by flipping them side to side. The modified truncation surface value is inspected by line 673 to determine if a truncation has occurred. Truncation occurs only if the truncation surface value is definitely less than zero. Equality with zero is not considered a truncation so that flow zones (which are defined by a primary surface and its truncations) can be defined by using common separating surfaces (one such being just the flip side of the other) without creating a locus of points that does not lie in either flow zone (by having a separating surface value of exactly zero).

If surface truncation does not occur, lines 674 to 689 skip over the truncation header and transfer control back to the truncation-header-evaluation loop. If surface truncation does occur, the recursion process is unwound to the next level (lines 695 and 696) and control is transferred either back to the desired-result-specification-and-transfer-of-control section or back to the truncation-recursion-control section. The effect of transfer back to the recursion control section is to declare that since the truncation surface was itself truncated, it is therefore nonapropos and is passed over in the process of truncating its own parent surface.

Subroutine SA100 (listing 9) is a representative fundamental surface evaluation subroutine. This is the type of routine that is invoked by subroutine SURF (listing 8) in the fundamental-surface-evaluation section. This particular subroutine provides a time-invariant sphere in space. Four results are always provided by subroutines of this class as specified by the switch variable ISW: (1) the surface value (line 91), (2) the surface gradient (line 96), (3) the surface velocity (lines 98 and 99), and (4) the surface acceleration (in this case,

since the surface is time invariant, also provided by lines 98 and 99). As can be seen by this example, fundamental surfaces are easy to describe and add to the CASPER repertoire.

The separation of surface control parameters for the fundamental-surface-evaluation functions into various groups (as commented on in lines 54 to 57 in listing 9, in the column labeled "'IV' slot") is also an important feature of the CASPER surface description system. It allows the easy repetition of groups of parameters (in this case, spheres with the same center or spheres with the same radius) simply by providing addressing information to the same actual parameter images. For spheres the economy of this is doubtful, but for more exotic surfaces (e.g., a realistic cambered and twisted fan blade that will be repeated 30 or 40 times in the same rotor) this feature can be a great help in avoiding errors in repetitive data entry.

Calculation of Thermodynamic Effects

The power of compression is calculated by subroutine POWERC, which is presented as listing 10. This routine calculates a straightforward parametric integration of the pressure-versus-volume history by passing parabolic approximations through three pressure points and three volume points (performed by lines 87 to 109) and stores the result in the aeroelement record (line 110). As it turns out, once the characteristic parametric spacings (in time, in this instance) are known, the computation can be reduced to a matrix-by-vector multiply operation to determine parabolic approximation coefficients (matrix determined by lines 87 to 94, coefficients determined by lines 96 to 107). Thus the matrix formulation can be performed once outside the actual aeroelement-by-aeroelement computation loop.

The power of viscous distortion is calculated in two phases for much the same reason as were the aeroelement accelerations—in this case derivatives of terms not yet calculated are required. Thus the appropriate term must be calculated and stored for each aeroelement before the phase involving the derivative of the term can begin. This process is carried out by subroutines WRKFLD and WRKFLE (listings 11 and 12, respectively). These subroutines are straightforward calculations of the power-of-viscous-distortion equation outlined in the theory section of this report. Lines 29 to 33 of listing 11 calculate and store the power-of-viscous-distortion result (which is the aeroelement volume times the divergence of the key term calculated in subroutine WRKFLD) by the standard derivative calculation scheme outlined previously.

The conductive heat transfer between aeroelements is calculated by subroutine WRKFLF (listing 13). The computation is a simple one implementing the conductive

heat transfer equations discussed in the theoretical section of this report. It is important to note that the heat transfer is calculated only if the nearest neighbor of the target aeroelement reciprocates with the target aeroelement (i.e., if the nearest neighbor of the target aeroelement lists the target aeroelement as one of its nearest neighbors). Since the CASPER algorithm will not modify the record of the nearest-neighbor aeroelement (for parallel-processing reasons), this reciprocity is necessary to ensure the conservation of energy. In this way, it is ensured that the same amount of energy transferred into the target aeroelement will be removed from the neighbor aeroelement (when its turn comes in the computational process) to conserve the total energy between the two aeroelements.

The cleanup hitter in the thermodynamic subroutine lineup is subroutine WRKFLG (listing 14). This routine accumulates all of the power terms for an aeroelement, multiplies the result by the time increment to obtain a net work, divides the result by the coefficient of specific heat at constant volume to determine a change in temperature, adjusts the previous aeroelement temperature by the calculated change in temperature, and stores the result in the aeroelement record.

Calculation of Aeroelement Volume and Pressure

Subroutine VOL (listing 15) estimates aeroelement volumes on the basis of the proximity of nearest neighbors to the target aeroelement. Lines 273 to 283 initialize for the solid-angle correction calculation and calculate the initial spherical volume estimate for the target aeroelement. The solid angle calculation is performed by forming a regular spherical pentagon and dividing it into three successive spherical triangles. For this process to work, the nearest neighbors must be ordered to produce a regular spherical pentagon. This is accomplished in lines 287 to 312 by establishing a spherical pole with neighbor 1, establishing a line of zero longitude with neighbor 2, and reordering neighbors 3, 4, and 5 to achieve monotonically increasing longitudinal values. Lines 318 to 363 use the reordered neighbors to calculate the solid angle of the three spherical triangles so subtended and accumulates the results to obtain the total solid angle subtended by all five nearest neighbors. Finally the original volume estimate is adjusted (on line 369) by the relationship of the calculated solid angle to the current average solid angle, and the result is stored in the target aeroelement record (on line 374).

Subroutine VSUM (listing 16) implements the volume-estimate-correction scheme described in the theoretical section of this report. The volume estimate for each aeroelement is added to a total volume value. In subroutines not included in this report this total volume estimate is compared with the known volume for the

problem and a multiplicative correction factor is produced. This factor is applied to the volume estimate for each aeroelement by subroutine VCOR (listing 17).

Subroutine RHOPRS (listing 18) calculates aeroelement density and pressure. The aeroelement density calculation is a trivial operation performed on lines 27 and 28 by dividing aeroelement mass by aeroelement volume and storing the result in the aeroelement record. The calculation of pressure is a similarly trivial process (lines 29 to 31); however, in this instance, it is performed by invoking the subroutine GASLAW (which is presented as listing 19). This allows the user to easily alter the operating gas law by the simple expedient of replacing the GASLAW subroutine. Thus any gas law relating pressure to density and temperature (and indeed any other recorded aeroelement property since the aeroelement identification number is passed to GASLAW) can be easily supported.

Finding Nearest-Neighbor Aeroelements

Only one example of a nearest-neighbor aeroelement finder is provided in this report: subroutine FNBNE (listing 20). This is the neighbor-tree-search algorithm described in the theoretical section of this report and is the most frequently used method of finding nearest neighbors in current CASPER practice. The principal advantage of this method is that the user sets the number of candidate aeroelements inspected by supplying the variable JCC in the subroutine call.

The subroutine starts out (lines 153 to 228) by constructing a candidate tree from the current neighbor tree for the target aeroelement. This is done in a two-phase process of (1) placing successive layers of the neighbor tree onto a candidate possibility stack (lines 190 to 195) and (2) removing aeroelements from the candidate possibility stack and inserting them in the candidate aeroelement tree (lines 174 to 181). This insertion process ensures that redundant entries will not occur.

The candidate-aeroelement-tree-building process continues until either enough independent aeroelement candidates have been found (i.e., more than JCC candidates have been found) or the neighbor tree fails to produce any new aeroelement candidates. In this second event the subroutine will attempt to fill out the candidate aeroelement tree by acquiring aeroelements from the flow zone of the target aeroelement (and thence from neighbor flow zones). This process is carried out by lines 207 to 228.

Once a candidate aeroelement tree of at least the requested size has been constructed, a simple center-to-center distance test is used to identify five nearest neighbors from among the candidates in the candidate aeroelement tree (lines 257 to 264 with neighbor list replacement being performed by lines 265 to 270). Note that lines 253 to 255 perform a candidate screening operation that attempts to eliminate the bogus-nearest-neighbor syndrome by requiring that each candidate aeroelement tested reside in either the flow zone of the

target aeroelement or in a flow zone that is a neighbor to the flow zone of the target aeroelement.

Flow Field Simulation Sequence

This report does not include a listing of the flow field simulation sequence since this involves PAX parallel-processing knowledge. The interested reader is referred to reference 1, which includes a listing of the current CASPER flow field simulation sequence.

Concluding Remarks

This report has detailed the theoretical basis and illustrated the implementation of CASPER. No new insight into fluid flow is involved. Rather CASPER uses a simple visualization of the fundamental physics of the problem and shifts the burden from insight to computation and management. The results of CASPER operation are a simulation of Navier-Stokes flow rather than a solution of the Navier-Stokes equation.

CASPER allows the following key features in fluid flow simulation:

- (1) Three-dimensional flow
- (2) Viscous flow
- (3) Time-varying flow
- (4) Three-dimensional boundaries
- (5) Nonsymmetric boundaries

- (6) Arbitrary, complex boundaries through the truncation and concatenation of simple boundaries
- (7) Time-varying boundaries
- (8) Boundary-flow interactions

As currently implemented, CASPER tasks can be executed asynchronously in parallel. A Parallel, Asynchronous Executive (PAX) exists to manage this feature. Details of PAX are provided in a referenced report.

Computational results (four complete iterative cycles) have been obtained from CASPER. These results are sufficient to prove the syntactical correctness of CASPER modules but do not provide the necessary base from which a technical judgment about the appropriateness of the CASPER approach can be made.

National Aeronautics and Space Administration
Lewis Research Center
Cleveland, Ohio, September 21, 1984

References

1. Jones, William H.: Parallel, Asynchronous Executive (PAX): System Concepts, Facilities, and Architecture. NASA TP-2179, 1983.
2. Li, Wen-Hsiung; and Lam, Sau-Hai: Principles of Fluid Mechanics. Addison-Wesley Publishing Co., Inc., 1964.
3. Schlichting, Hermann (J. Kestin, transl.): Boundary-Layer Theory. Sixth ed. McGraw-Hill Book Company, 1968, p. 253.

@FOR,MS CASPER2.INTFD
 FDK 4R1 E -04/13/84-15:39:41 (2,)
 >@EOF

SUBROUTINE INTF ENTRY POINT 000057

STORAGE USED: CODE(1) 000074; DATA(0) 000015; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 CHKLH
 0004 CHKTIM
 0005 MATRIX
 0006 ERROR2
 0007 CLNINT
 0010 NERR3*

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000020	116G	0001	000044	23L	0001	000046	24L	0000	I	000000	FLAG1	0000	I	000004	I
0000	I	000002	ID	0000	I	000003	IE	0000	000006	INJF*	0000	I	000001	IS		

00101	1*															000000
00101	2*															000000
00101	3*															000000
00101	4*															000000
00101	5*															000000
00101	6*															000000
00101	7*															000000
00101	8*	C														201A0010
00101	9*	C														20100020
00101	10*	C														20100030
00101	11*	C	INTF				*****	A SUBROUTINE FOR CASPER	*****							20100040
00101	12*	C					AUTHOR	WILLIAM HENRY JONES								20100050
00101	13*	C					V01-00	29 NOV 76								20100060
00101	14*	C					V01-01	23 AUG 78								20110061
00101	15*	C					V01-01A	06 FEB 79								201A0062
00101	16*	C					V01-01B	11 FEB 80								000000
00101	17*	C							SINGULAR MATRICIES TO SAFS							000000
00101	18*	C														20100080
00101	19*	C														20100090
00101	20*	C														20110233
00101	21*	C							ARGUMENTS PASSED IN SUBROUTINE CALL *****							20110234
00101	22*	C														20110235
00101	23*	C														20110236
00101	24*	C														201A0240
00101	25*	C														201A0242
00101	26*	C														201A0244
00101	27*	C														20100260
00101	28*	C														20100270
00101	29*	C														20100280
00101	30*	C														20100290
00101	31*	C														20100300
00101	32*	C														201A0310
00101	33*	C														20100320
00101	34*	C														20100330
00101	35*	C														20100340
00101	36*	C														20100350
00101	37*	C														20100360
00101	38*	C														20100370
00101	39*	C														20100380
00103	40*															20100390
00104	41*															201A0400
00106	42*															201A0405
00110	43*															201A0410
00111	44*															201A0420
00114	45*	16														201A0430
00115	46*															201A0440
00120	47*															201A0450
00121	48*															000025
00122	49*															000031
00125	50*	20														000033
00126	51*															000034
00127	52*															000040
00130	53*	23														000046
00132	54*	24														000046
00133	55*															20100480

END FOR
 >

Listing 1.—Subroutine INTF.

#FOR,MS CASPER2.MATRID
 FOR 4R1 E -04/13/84-15:41:12 (0,)
 >#EOF

SUBROUTINE MATRIX ENTRY POINT 000311

STORAGE USED: CODE(1) 000335; DATA(0) 000174; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 ISIZEC 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 X
 0005 NEI
 0006 DET4
 0007 STAT
 0010 STSTAT
 0011 STINTP
 0012 XPII
 0013 NERR3#

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000003	110G	0001	000006	113G	0001	000040	121G	0001	000052	127G	0001	000053	132G					
0001	000065	140G	0001	000075	143G	0001	000076	146G	0001	000113	154G	0001	000152	163G					
0001	000167	176G	0001	000226	203L	0001	000201	206G	0001	000234	223G	0001	000237	226G					
0001	000155	404L	0001	000200	406L	0001	000207	601L	0000	R	000000	A	0000	R	000031	COF			
0000	R	000132	DET	0006	R	000000	DET4	0000	R	000062	D4	0000	R	000102	D4I	0000	I	000126	I
0000	000152	INJP#	0003	000000	ISIZE	0000	I	000127	J	0000	I	000130	K	0000	I	000131	L		
0005	I	000000	NEI	0000	I	000133	NNN	0000	R	000134	DBET	0000	R	000135	RRR	0007	R	000000	STAT
0004	R	000000	X																

00101	1*																		000006
00101	2*																		000006
00101	3*																		000006
00101	4*																		000006
00101	5*																		000006
00101	6*																		000006
00101	7*																		000006
00101	8*	C																	000006
00101	9*	C																	000006
00101	10*	C																	000006
00101	11*	C																	000006
00101	12*	C																	000006
00101	13*	C																	000006
00101	14*	C																	000006
00101	15*	C																	000006
00101	16*	C																	000006
00101	17*	C																	000006
00101	18*	C																	000006
00101	19*	C																	000006
00101	20*	C																	000006
00101	21*	C																	000006
00101	22*	C																	000006
00101	23*	C																	000006
00101	24*	C																	000006
00101	25*	C																	000006
00101	26*	C																	000006
00101	27*	C																	000006
00101	28*	C																	000006
00101	29*	C																	000006
00101	30*	C																	000006
00101	31*	C																	000006
00101	32*	C																	000006
00101	33*	C																	000006
00101	34*	C																	000006
00101	35*	C																	000006
00101	36*	C																	000006
00101	37*	C																	000006
00101	38*	C																	000006
00101	39*	C																	000006
00101	40*	C																	000006

Listing 2.—Subroutine MATRIX.

```

00101 41* C 21100230 000006
00101 42* C FLAG1 INTEGER SCALAR SINGULAR MATRIX FLAG1=1 21100240 000006
00101 43* C 21100250 000006
00101 44* C 21100260 000006
00101 45* C DESCRIPTION: 21100270 000006
00101 46* C 21100280 000006
00101 47* C 1 MATRIX FORMS THE ARRAY (CALLED A IN THE PROGRAM) 21100290 000006
00101 48* C 21100300 000006
00101 49* C $X11 $X12 $X13 .5*$X11**2 $X12**X13 21100310 000006
00101 50* C $X21 $X22 $X23 .5*$X21**2 $X22**X23 21100320 000006
00101 51* C $X31 $X32 $X33 .5*$X31**2 $X32**X33 21100330 000006
00101 52* C $X41 $X42 $X43 .5*$X41**2 $X42**X43 21100340 000006
00101 53* C $X51 $X52 $X53 .5*$X51**2 $X52**X53 21100350 000006
00101 54* C 21100360 000006
00101 55* C WHERE $XKJ = X(NEI(I1,K),J) - X(I1,J) 21100370 000006
00101 56* C 21100380 000006
00101 57* C 2 MATRIX CALCULATES THE APPROPRIATE COFACTORS AN THE 21100390 000006
00101 58* C DETERMINANT OF A 21100400 000006
00101 59* C 21100410 000006
00101 60* C 3 IF THE DETERMINANT OF A = 0 THEN MATRIX SETS FLAG1=1, SETS 21100420 000006
00101 61* C BIT 0 OF STAT AND EXITS 21100430 000006
00101 62* C 21100440 000006
00101 63* C 4 MATRIX CALCULATES INVERSION OF A (FIRST 3 ROWS ONLY), STORES 21100450 000006
00101 64* C IT INTO INT(I1, , ), CLEARS BIT 0 OF STAT (THE INTERPOLATOR 21100460 000006
00101 65* C NOT AVAILABLE BIT), AND EXITS 21100470 000006
00101 66* C 21100480 000006
00101 67* C REQUIRED SUBROUTINES ***** 21150490 000006
00101 68* C 21150492 000006
00101 69* C 213 DET3 212 DET4 21150494 000006
00101 70* C 401 AVIRI 402 X 21150498 000006
00101 71* C 417 STSTAT 416 STAT 21150502 000006
00101 72* C 422 NEI 21150506 000006
00101 73* C 425 STINTP 24450508 000006
00101 74* C 21100520 000006
00103 75* C COMMON /ISIZEC/ISIZE 21100530 000006
00104 76* C INTEGER I1,FLAG1 21150550 000006
00105 77* C DIMENSION A(5,5),CDF(5,5),D4(4,4),D4I(5,4) 21120570 000006
00106 78* C DEFINE DX(I,J)=X(I,J) 21100580 000006
00107 79* C DO 201 I=1,5 @CALCULATE ARRAY A 21100590 000006
00112 80* C DO 201 J=1,3 21100600 000006
00115 81* C 201 A(I,J)=DX(NEI(I1,I),J)-X(I1,J) 21100610 000006
00120 82* C DO 202 I=1,5 21100620 000040
00123 83* C A(I,4)=0.5*A(I,1)*A(I,1) 21100630 000040
00124 84* C 202 A(I,5)=A(I,2)*A(I,3) 21100640 000043
00126 85* C DO 401 I=1,5 @SETUP INTERMEDIATE STORE 21120650 000053
00131 86* C DO 401 J=1,4 @ FOR FIRST PASS 21120660 000053
00134 87* C 401 D4I(I,J)=A(I,J+1) 21120670 000053
00137 88* C DO 408 J=1,3 @BEGIN COLUMN LOOP 21120680 000065
00142 89* C DO 402 K=1,4 @SETUP 4X4 MATRIX FOR FIRST 21120690 000076
00145 90* C DO 402 L=1,4 @ PASS 21120700 000076
00150 91* C 402 D4(K,L)=D4I(K+1,L) 21120710 000076
00153 92* C DO 404 I=1,5 21120720 000113
00156 93* C CDF(I,J)=DET4(D4)**((-1)**(I+J)) @CALCULATE COFACTORS 21120730 000121
00157 94* C IF (I=5) ,404, @IF I=5 SKP SETUP FOR NEXTPASS 21120740 000141
00162 95* C DO 403 L=1,4 @SETUP 4X4 FOR NEXT PASS 21120750 000152
00165 96* C 403 D4(I,L)=D4I(I,L) 21120760 000152
00167 97* C 404 CONTINUE 21120770 000157
00171 98* C IF (J=1) 406, ,406 @IF FIRST COLUMN COMPLETED 21120780 000157
00174 99* C DET=0.0 @ CALCULATE DETERMINANT * 21120790 000162
00175 100* C DO 405 K=1,5 21120800 000167
00200 101* C 405 DET=DET+A(K,J)*CDF(K,J) 21120810 000167
00202 102* C IF (ABS(DET)-1.0E-10) 601,406,406 21130820 000173
00205 103* C 406 DO 407 K=1,5 @SWAP INTERMEDIATE COLUMN 21120830 000201
00210 104* C 407 D4I(K,J)=A(K,J) 21120840 000201
00212 105* C 408 CONTINUE @EOL COLUMN LOOP 21120850 000205
00214 106* C GO TO 203 21120860 000205
00215 107* C 601 FLAG1=1 @ERROR - SET FLAG1 21120870 000207
00216 108* C NNN=OR(STAT(I1),2**0) @ SET STATUS BIT 0 21150880 000210
00217 109* C CALL STSTAT (I1,NNN) @ 21150850 000216
00220 110* C RETURN 21120890 000222
00221 111* C 203 ODET=1.0/DET 21121980 000226
00221 112* C FORM INVERSE OF MATRIX BY DIVIDING TRANSFORM OF COFACTOR 21101990 000226
00221 113* C MATRIX BY DETERMINANT 21102000 000226
00222 114* C DO 204 I=1,5 21102010 000237
00225 115* C DO 204 J=1,3 21102020 000237
00230 116* C RRR=ODET*CDF(I,J) @ 21152030 000237
00231 117* C 204 CALL STINTP (I1,J,I,RRR) @ 21152035 000242
00234 118* C NNN=AND(STAT(I1),COMPL(2**0)) @ CLR STATUS BIT 0 21152040 000257
00235 119* C CALL STSTAT (I1,NNN) @ 21152045 000265
00236 120* C RETURN 21102050 000271
00237 121* C END 21102060 000334
END FOR
>

```

Listing 2.—Concluded.

@FDR,MS CASPER2.DET4D
 FOR 4R1 E -04/13/84-15:43:57 (0,)
 >@EOF

FUNCTION DET4 ENTRY POINT 000123

STORAGE USED: CODE(1) 000135; DATA(0) 000043; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 DET3
 0004 XP11
 0005 NERR3*

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000012	105G	0001	000013	110G	0001	000031	117G	0001	000075	126G	0001	000100	203L
0003 R	000000	DET3	0000 R	000000	DET4	0000 R	000014	DE4	0000 R	000001	B3	0000 I	000012	I
0000	000021	INJP*	0000 I	000013	J									

00101	1*													000013
00101	2*													000013
00101	3*													000013
00101	4*													000013
00101	5*													000013
00101	6*													000013
00101	7*													000013
00101	8*	C	REAL FUNCTION DET4 (D4)						21200010					000013
00101	9*	C							21200020					000013
00101	10*	C							21200030					000013
00101	11*	C	***** A REAL FUNCTION FOR CASPER *****						21200040					000013
00101	12*	C	AUTHOR WILLIAM HENRY JONES						21200050					000013
00101	13*	C	DATE 13 DEC 76						21200060					000013
00101	14*	C	REVISION ORIGINAL						21200070					000013
00101	15*	C	ARGUMENT TYPE DIMENSION DESCRIPTION						21200080					000013
00101	16*	C							21200090					000013
00101	17*	C	D4 REAL 1 TO 4 ARBITRARY 4 X 4 ARRAY						21200100					000013
00101	18*	C							21200110					000013
00101	19*	C							21200120					000013
00101	20*	C	DESCRIPTION:						21200130					000013
00101	21*	C							21200140					000013
00101	22*	C	CALCULATES THE DETERMINANT OF THE INPUT MATRIX BY WEIGHTED						21200150					000013
00101	23*	C	ACCUMULATION OF FUNCTION CALLS TO DET3 (3 X 3 DETERMINANT)						21200160					000013
00101	24*	C							21200170					000013
00101	25*	C	REQUIRED SUBROUTINES:						21200180					000013
00101	26*	C							21200190					000013
00101	27*	C	REAL FUNCTION DET3 (D)						21200200					000013
00101	28*	C							21200210					000013
00101	29*	C							21200220					000013
00101	30*	C							21200230					000013
00101	31*	C							21200240					000013
00103	31*	C	REAL D4(4,4),D3(3,3)						21200250					000013
00104	32*	C	DO 201 I=-1,3						21200260					000013
00107	33*	C	DO 201 J=1,3						21200270					000013
00112	34*	201	D3(I,J)=D4(I+1,J+1) @SETUP FIRST SUBMATRIX						21200280					000013
00115	35*	C	DE4=0,0 @CLR ACCUMULATOR						21200290					000024
00116	36*	C	DO 203 J=1,4 @ENTER ACCUMULATOR LOOP						21200300					000031
00121	37*	C	DE4=DE4+DET3(D3)*D4(1,J)*((-1)**(J+1))						21200310					000042
00122	38*	C	IF (J-4) ,203, @TST FOR SKP NEXT SUBMATRIX						21200320					000064
00125	39*	C	DD 202 I=1,3 @SUBSTITUTE CHANGING COLUMN						21200330					000075
00130	40*	202	D3(I,J)=D4(I+1,J) @ FOR NEXT ACCUMULATOR PASS						21200340					000075
00132	41*	203	CONTINUE						21200350					000102
00134	42*	C	DET4=DE4						21200360					000102
00135	43*	C	RETURN						21200370					000104
00136	44*	C	END						21200380					000134

END FOR

Listing 3.—Subroutine DET4.

```

>@FDR,MS CASPER2.DET3D
FOR 4R1 E -04/13/84-15:45:11 (0,)
>@EOF

```

```

FUNCTION DET3      ENTRY POINT 000036

```

```

STORAGE USED: CODE(1) 000041; DATA(0) 000006; BLANK COMMON(2) 000000

```

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

```

0003 NERR3$

```

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

```

0000 R 000000 DET3      0000 000001 INJP$

```

```

00101      1*                               000000
00101      2*                               000000
00101      3*                               000000
00101      4*                               000000
00101      5*                               000000
00101      6*                               000000
00101      7*                               000000
00101      8*                               000000
00101      9*                               000000
00101     10*                               000000
00101     11*      C      REAL FUNCTION DET3 (D)                21300010 000000
00101     12*      C                               21300020 000000
00101     13*      C                               21300030 000000
00101     14*      C*  DET3      ***** A REAL FUNCTION FOR CASPER ***** 21300040 000000
00101     15*      C      AUTHOR      WILLIAM HENRY JONES          21300050 000000
00101     16*      C      DATE        13 DEC 76                    21300060 000000
00101     17*      C      REVISION   ORIGINAL                     21300070 000000
00101     18*      C                               21300080 000000
00101     19*      C      ARGUMENT   TYPE      DIMENSIONS      DESCRIPTION 21300090 000000
00101     20*      C      D          REAL      1 TO 3          ARBITRARY 3 X 3 ARRAY 21300110 000000
00101     21*      C                               1 TO 3          21300120 000000
00101     22*      C                               21300130 000000
00101     23*      C      DESCRIPTION: 21300140 000000
00101     24*      C                               21300150 000000
00101     25*      C      FORMS THE DETERMINANT OF AN ARBITRARY 3 X 3 ARRAY 21300160 000000
00101     26*      C                               21300170 000000
00101     27*      C      REQUIRED SUBROUTINES: 21300180 000000
00101     28*      C                               21300190 000000
00101     29*      C      NONE                                     21300200 000000
00101     30*      C                               21300210 000000
00101     31*      C                               21300220 000000
00101     32*      C                               21300230 000000
00103     33*      C      REAL D(3,3)                             21300240 000000
00104     34*      C      DET3=D(1,1)*D(2,2)*D(3,3)-D(2,3)*D(3,2))-D(2,1)*D(1,2)*D(3,3)-D(21300250 000000
00104     35*      C      11,3)*D(3,2))+D(3,1)*D(1,2)*D(2,3)-D(1,3)*D(2,2)) 21300260 000000
00105     36*      C      RETURN                                     21300270 000025
00106     37*      C      END                                       21300280 000040
END FOR
>

```

Listing 4.—Subroutine DET3.


```
#FOR,MS CASPER3.STOK1D
FOR 4R1 E -04/13/84-15:04:44 (4,)
>@EOF
```

```
SUBROUTINE STOK1 ENTRY POINT 000271
```

```
STORAGE USED: CODE(1) 000316; DATA(0) 000131; BLANK COMMON(2) 000000
```

```
EXTERNAL REFERENCES (BLOCK, NAME)
```

```
0003 STAT
0004 MU
0005 MUTHET
0006 INTP
0007 U
0010 EIJ
0011 CHKLH
0012 NEI
0013 STEIJ
0014 STMUTH
0015 CHKTIM
0016 NERR3*
```

```
STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)
```

```
0001 000017 132G      0001 000032 140G      0001 000042 144G      0001 000057 153G      0001 000072 161G
0001 000074 164G      0001 000120 172G      0001 000122 175G      0001 000124 201G      0001 000202 205L
0001 000147 210G      0001 000241 212L      0001 000152 213G      0001 000214 232G      0001 000250 701L
0000 R 000044 DELTU    0000 R 000063 DUIDXJ    0010 R 000000 EIJ      0000 I 000075 I      0000 I 000001 ID
0000 I 000002 IE      0000 000110 INJP*    0006 R 000000 INTP    0000 I 000000 IS      0000 I 000074 I1
0000 I 000076 J      0000 I 000077 K      0000 R 000033 LEIJ    0000 R 000003 LINTP   0000 R 000025 LMUTHE
0000 I 000026 LNEI    0000 R 000022 LU      0004 R 000000 MU      0005 R 000000 MUTHET   0012 I 000000 NEI
0000 R 000100 RRR      0003 I 000000 STAT    0007 R 000000 U
```

```
00101 1* 000000
00101 2* 000000
00101 3* 000000
00101 4* 000000
00101 5* 000000
00101 6* 000000
00101 7* 000000
00101 8* SUBROUTINE STOK1 (IL,IH) 301A0010 000000
00101 9* C 30100020 000000
00101 10* C 30100030 000000
00101 11* C ***** A SUBROUTINE FOR CASPER ***** 30100040 000000
00101 12* C AUTHOR WILLIAM HENRY JONES 30100050 000000
00101 13* C V01-00 28 DEC 76 30100060 000000
00101 14* C V01-01 30110061 000000
00101 15* C V01-02 30120062 000000
00101 16* C V01-03 24 AUG 78 30130063 000000
00101 17* C V01-03A 06 FEB 79 FIRST SPLIT OF 'STOK' 301A0064 000000
00101 18* C V01-03B 11 FEB 80 TIME CHECK 000000
00101 19* C V01-03C 15 SEP 80 FUNCTION TYPE STATEMENTS 000000
00101 20* C V01-03D 15 APR 83 FUNCTION TYPES, EFFICIENCY V01-03D 000000
00101 21* C 30100080 000000
00101 22* C ARGUMENTS IN CASPER 'CACHE' MEMORY ***** 30130084 000000
00101 23* C 30130086 000000
00101 24* C ARGUMENT TYPE DIMENSION DESCRIPTION 30100090 000000
00101 25* C ----- 30130100 000000
00101 26* C U REAL 1 TO ISIZE AERDELEMENT VELOCITIES 30100110 000000
00101 27* C 1 TO 3 30100120 000000
00101 28* C 30100130 000000
00101 29* C NEI INTEGER 1 TO ISIZE NEAREST NEIGHBOR LIST 30100140 000000
00101 30* C 1 TO 5 30100150 000000
00101 31* C 30100160 000000
```

Listing 5.—Subroutine STOK1.

00101	32*	C	INTP	REAL	1 TO ISIZE	INTERPOLATOR MATRICIES	30130170	000000	
00101	33*	C			1 TO 3		30100180	000000	
00101	34*	C			1 TO 5		30100190	000000	
00101	35*	C					30100200	000000	
00101	36*	C	STAT	INTEGER	1 TO ISIZE	STATUS LIST	30100210	000000	
00101	37*	C					30100220	000000	
00101	38*	C	MU	REAL	1 TO ISIZE	AEROELEMENT VISCOUSITIES	30100270	000000	
00101	39*	C			1 TO 2	1=FIRST, 2=SECOND	30100280	000000	
00101	40*	C					30100290	000000	
00101	41*	C	EIJ	REAL	1 TO ISIZE	STRAIN RATE MATRICIES	30100330	000000	
00101	42*	C			1 TO 3	EIJ(I,J)=.5*(U(I),X(J)	30100340	000000	
00101	43*	C			1 TO 3	+U(J),X(I))	30100350	000000	
00101	44*	C					30100360	000000	
00101	45*	C	MUTHET	REAL	1 TO ISIZE	SEE DESCRIPTION NOTE 3	30100370	000000	
00101	46*	C					301A0380	000000	
00101	47*	C	ARGUMENTS PASSED IN SUBROUTINE CALL *****					301A0382	000000
00101	48*	C					301A0384	000000	
00101	49*	C	ARGUMENT	TYPE	DIMENSION	DESCRIPTION	301A0386	000000	
00101	50*	C	-----	-----	-----	-----	301A0388	000000	
00101	51*	C	IL	INTEGER	SCALAR	AEROELEMENT ID LOW LIMIT	301A0390	000000	
00101	52*	C					301A0392	000000	
00101	53*	C	IH	INTEGER	SCALAR	AEROELEMENT ID HIGH LIMIT	301A0394	000000	
00101	54*	C					301A0396	000000	
00101	55*	C					301A0398	000000	
00101	56*	C	DESCRIPTION *****					301A0400	000000
00101	57*	C					301A0402	000000	
00101	58*	C	THIS SUBROUTINE PERFORMS THE FOLLOWING OPERATIONS FOR EACH					30100410	000000
00101	59*	C	AEROELEMENT IN THE RANGE 'IL' TO 'IH'.					301A0420	000000
00101	60*	C					30100430	000000	
00101	61*	C	1	A CHECK IS MADE FOR AVAILABILITY OF THE INTERPOLATOR MATRIX.			30100460	000000	
00101	62*	C		IF NOT AVAILABLE ALL SUCCEEDING OPERATIONS ARE SKIPPED FOR			30100470	000000	
00101	63*	C		THE AEROELEMENT DURING THE PASS			30100480	000000	
00101	64*	C					30100490	000000	
00101	65*	C	2	THE STRAIN RATE MATRIX IS CALCULATED (EIJ(I,J))			30100500	000000	
00101	66*	C					30100510	000000	
00101	67*	C	3	THE QUANTITY (MU'-,6666667*MU)*(EIJ(1,1)+EIJ(2,2)+EIJ(3,3)) IS			30100520	000000	
00101	68*	C		CALCULATED			30100530	000000	
00101	69*	C					30100540	000000	
00101	70*	C	REQUIRED SUBROUTINES *****					30130650	000000
00101	71*	C					30130652	000000	
00101	72*	C	401	AVIRI			30130654	000000	
00101	73*	C			404	U	30130656	000000	
00101	74*	C	407	STA			30130658	000000	
00101	75*	C			408	P	30130660	000000	
00101	76*	C	417	STSTAT	416	STAT	30130662	000000	
00101	77*	C			422	NEI	30130664	000000	
00101	78*	C			424	INTP	30130666	000000	
00101	79*	C	427	STEIJ	426	EIJ	30130668	000000	
00101	80*	C			428	MU	30130670	000000	
00101	81*	C	431	STMUTH	430	MUTHET	30130672	000000	
00101	82*	C					30100680	000000	
00101	83*	C					30100690	000000	
00101	84*	C					30100700	000000	
00103	85*	C	INTEGER IL,IH,IS,ID,IE					301A0710	000000
00104	86*	C	INTEGER STAT						000000
00105	87*	C	REAL MU,MUTHET						000000
00106	88*	C	REAL INTP				@ INTERPOLATOR MATRIX ACCESS FUNCTION	V01-03D	000000
00107	89*	C	REAL LINTP(5,3)				@ LOCAL COPY OF INTERPOLATOR	V01-03D	000000
00110	90*	C	REAL LU(3)				@ LOCAL COPY OF ELEMENT VELOCITY	V01-03D	000000
00111	91*	C	REAL LMUTHE				@ LOCAL COPY OF MUTHET FACTOR	V01-03D	000000
00112	92*	C	INTEGER LNEI(5)				@ LOCAL COPY OF NEAREST NEIGHBOR IDS	V01-03D	000000
00113	93*	C	REAL LEIJ(3,3)				@ LOCAL COPY OF STRAIN RATE MATRIX	V01-03D	000000
00114	94*	C	DATA ID/301/					301A0712	000000
00116	95*	C	DATA IE/1/					301A0714	000000
00120	96*	C	REAL DELTU(5,3),DUIDXJ(3,3)					30110750	000000
00121	97*	C	DEFINE DU(I,J)=U(I,J)					30100780	000000
00122	98*	C	DEFINE DMUTHE(I)=MUTHET(I)					30100800	000000
00123	99*	C	DEFINE DMU(I,J)=MU(I,J)					30100810	000000
00124	100*	C	DEFINE DEIJ(I,J,K)=EIJ(I,J,K)					30100820	000000
00125	101*	C	CALL CHKLNH(IL,IH,IS,ID,IE)				@ GO CHECK AEROELEMENT RANGE	301A0830	000000
00126	102*	C	IF (IS) 101,701,101				@ LEGAL RANGE ?	301A0832	000006
00131	103*	C	101	DO 213 I1=IL,IH,IS			@ YES, DO EACH AEROELEMENT	V01-03D	000010

Listing 5.—Continued.

```

00134 104*          IF (AND(STAT(I1),1)) 103,103,212 @ DO WE HAVE AN INTERPOLATOR ?V01-03D 000017
00137 105*      103 DO 107 I=1,3 @ YES, LOCALIZE V01-03D 000032
00142 106*          LU(I)=U(I,I) @ AEROELEMENT VELOCITY V01-03D 000032
00143 107*          DO 107 J=1,5 @ V01-03D 000042
00146 108*          LINTP(J,I)=INTP(I1,I,J) @ TRANSPOSE OF INTERPOLATOR V01-03D 000042
00147 109*      107 CONTINUE @ V01-03D 000057
00152 110*          DO 110 I=1,5 @ V01-03D 000057
00155 111*          LNEI(I)=NEI(I1,I) @ NEAREST NEIGHBOR LIST V01-03D 000057
00156 112*      110 CONTINUE @ V01-03D 000074
00160 113*          DO 201 I=1,5 @CALCULATE VELOCITY DIFFERENCE30100850 000074
00163 114*          DO 201 J=1,3 @ FOR ALL 5 NN IN ALL 3 30120860 000074
00166 115*      201 DELTU(I,J)=DU(LNEI(I),J)-LU(J) @ COORDINATE DIRECTIONS V01-03D 000074
00171 116*          DO 202 I=1,3 @CLR DERIVATIVE U(I),X(J) 30100880 000122
00174 117*          DO 202 J=1,3 @ STORAGE AND THEN 30100890 000122
00177 118*          DUIDXJ(I,J)=0.0 @ CALCULATE DERIVATIVE 30100900 000122
00200 119*          DO 202 K=1,5 @ BY INTERPOLATOR 30100910 000124
00203 120*      202 DUIDXJ(I,J)=DUIDXJ(I,J)+(LINTP(K,J)*DELTU(K,I)) @ V01-03D 000124
00207 121*          DO 205 I=1,3 @ CALC STRAIN RATE MATRIX V01-03D 000152
00212 122*          DO 205 J=1,3 @ V01-03D 000152
00215 123*          RRR=0.5*(DUIDXJ(I,J)+DUIDXJ(J,I)) @ 30130950 000152
00216 124*          CALL STEIJ (I1,I,J,RRR) @ 30130955 000156
00217 125*          LEIJ(I,J)=RRR @ SAVE LOCAL COPY V01-03D 000164
00220 126*          IF (I-J) 203,205,203 @ OFF-DIAGONAL ELEMENT ? V01-03D 000166
00223 127*      203 CALL STEIJ(I1,J,I,RRR) @ YES, FORCE A SYMETRIC V01-03D 000171
00224 128*          LEIJ(J,I)=RRR @ RESULT V01-03D 000177
00225 129*      205 CONTINUE @ V01-03D 000210
00230 130*          LMUTHE=0.0 @ CALC QUANTITY OF NOTE 3 V01-03D 000210
00231 131*          DO 209 I=1,3 @ V01-03D 000214
00234 132*          LMUTHE=LMUTHE+LEIJ(I,I) @ V01-03D 000214
00235 133*      209 CONTINUE @ V01-03D 000217
00237 134*          LMUTHE=LMUTHE*(MU(I1,2)-(0.666667*MU(I1,1))) @ V01-03D 000217
00240 135*          CALL STMUTH (I1,LMUTHE) @ V01-03D 000234
00241 136*      212 CALL CHKTIM (IL,IH,I1) @ KEEP AN EYE ON THE TIME V01-03D 000241
00242 137*      213 CONTINUE @ V01-03D 000250
00244 138*      701 RETURN @ BACK TO CALLER 301A1370 000250
00245 139*          END 30101380 000315
END FOR
>

```

Listing 5.—Concluded.

@FOR,MS CASPER3.STOK2D
 FOR 4R1 E -04/13/84-15:07:47 (4*)
 >@EOF

SUBROUTINE STOK2 ENTRY POINT 000424

STORAGE USED: CODE(1) 000451; DATA(0) 000214; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 STAT
 0004 MU
 0005 MUTHET
 0006 INTP
 0007 U
 0010 P
 0011 EIJ
 0012 CHKLH
 0013 RHO
 0014 STSTAT
 0015 NEI
 0016 STA
 0017 CHKTIH
 0020 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000044	107L	0001	000020	140G	0001	000062	162G	0001	000075	170G	0001	000100	173G					
0001	000116	202G	0001	000121	205G	0001	000136	214G	0001	000372	220L	0001	000160	225G					
0001	000174	232G	0001	000177	236G	0001	000211	244G	0001	000225	251G	0001	000230	255G					
0001	000243	263G	0001	000246	266G	0001	000251	271G	0001	000310	300G	0001	000311	303G					
0001	000313	307G	0001	000342	316G	0001	000344	322G	0001	000355	330G	0001	000403	701L					
0000	R	000153	DEJDXI	0000	R	000052	DELT	0000	R	000065	DELTM	0000	R	000142	DMEDXI	0000	R	000057	DPDXJ
0000	R	000062	DTDJ	0011	R	000000	EIJ	0000	I	000157	I	0000	I	000001	ID	0000	I	000002	IE
0000	I	000174	INJP\$	0006	R	000000	INTP	0000	I	000000	IS	0000	I	000156	I1	0000	I	000160	J
0000	I	000161	K	0000	R	000040	LEIJ	0000	R	000013	LINTP	0000	R	000032	LMU	0000	R	000051	LMUTHE
0000	I	000003	LNEI	0000	R	000033	LNMU	0000	R	000011	LP	0000	R	000012	LRHO	0000	I	000010	LSTAT
0004	R	000000	MU	0005	R	000000	MUTHET	0015	I	000000	NEI	0010	R	000000	P	0013	R	000000	RHO
0000	R	000162	RRR	0003	I	000000	STAT	0007	R	000000	U								

00101	1*																			000000	
00101	2*																			000000	
00101	3*																			000000	
00101	4*																			000000	
00101	5*																			000000	
00101	6*																			000000	
00101	7*																			000000	
00101	8*																			000000	
00101	9*	C																		302A0010	000000
00101	10*	C																		30100020	000000
00101	11*	C																		30100030	000000
00101	12*	C																		30100040	000000
00101	13*	C																		30100050	000000
00101	14*	C																		30100060	000000
00101	15*	C																		30110061	000000
00101	16*	C																		30120062	000000
00101	17*	C																		30130063	000000
00101	18*	C																		302A0064	000000
00101	19*	C																			000000
00101	20*	C																			000000
00101	21*	C																			000000
00101	22*	C																			000000
00101	23*	C																			000000
00101	24*	C																			000000
00101	25*	C																			000000

Listing 6.—Subroutine STOK2.

00101	26*	C	NEI	INTEGER	1 TO ISIZE	NEAREST NEIGHBOR LIST	30100140	000000	
00101	27*	C			1 TO 5		30100150	000000	
00101	28*	C					30100160	000000	
00101	29*	C	INTP	REAL	1 TO ISIZE	INTERPOLATOR MATRICIES	30130170	000000	
00101	30*	C			1 TO 3		30100180	000000	
00101	31*	C			1 TO 5		30100190	000000	
00101	32*	C					30100200	000000	
00101	33*	C	STAT	INTEGER	1 TO ISIZE	STATUS LIST	30100210	000000	
00101	34*	C					30100220	000000	
00101	35*	C	P	REAL	1 TO ISIZE	AEROELEMENT PRESSURES	30100230	000000	
00101	36*	C					30100240	000000	
00101	37*	C	RHO	REAL	1 TO ISIZE	AEROELEMENT DENSITIES	30100250	000000	
00101	38*	C					30100260	000000	
00101	39*	C	MU	REAL	1 TO ISIZE	AEROELEMENT VISCOUSITIES	30100270	000000	
00101	40*	C			1 TO 2	1=FIRST, 2=SECOND	30100280	000000	
00101	41*	C					30100290	000000	
00101	42*	C	A	REAL	1 TO ISIZE	AEROELEMENT ACCELERATION	30100300	000000	
00101	43*	C			1 TO 3		30100310	000000	
00101	44*	C					30100320	000000	
00101	45*	C	EIJ	REAL	1 TO ISIZE	STRAIN RATE MATRICIES	30100330	000000	
00101	46*	C			1 TO 3	EIJ(I,J)=.5*(U(I),X(J)	30100340	000000	
00101	47*	C			1 TO 3	+U(J),X(I))	30100350	000000	
00101	48*	C					30100360	000000	
00101	49*	C	MUTHET	REAL	1 TO ISIZE	SEE DESCRIPTION NOTE 3	30100370	000000	
00101	50*	C					302A0380	000000	
00101	51*	C	ARGUMENTS PASSED IN SUBROUTINE CALL *****					302A0382	000000
00101	52*	C					302A0384	000000	
00101	53*	C	ARGUMENT	TYPE	DIMENSION	DESCRIPTION	302A0386	000000	
00101	54*	C	-----	-----	-----	-----	302A0388	000000	
00101	55*	C	IL	INTEGER	SCALAR	AEROELEMENT ID LOW LIMIT	302A0390	000000	
00101	56*	C					302A0392	000000	
00101	57*	C	IH	INTEGER	SCALAR	AEROELEMENT ID HIGH LIMIT	302A0394	000000	
00101	58*	C					302A0396	000000	
00101	59*	C					302A0398	000000	
00101	60*	C	DESCRIPTION *****					302A0400	000000
00101	61*	C					302A0402	000000	
00101	62*	C	THIS SUBROUTINE PERFORMS THE FOLLOWING OPERATIONS FOR EACH					30100410	000000
00101	63*	C	AEROELEMENT IN THE RANGE 'IL' TO 'IH'.					302A0420	000000
00101	64*	C					30100430	000000	
00101	65*	C	1	THE DENSITY, RHO, IS CHECKED FOR APPROXIMATE EQUALITY WITH ZERO		30100570	000000		
00101	66*	C		IF SO, STATUS BIT 1 IS SET (ZERO DENSITY ERROR) AND		30100580	000000		
00101	67*	C		REMAINING CALCULATIONS ARE SKIPPED, THE CALCULATIONS ARE ALSO		302A0590	000000		
00101	68*	C		SKIPPED IF THE 'INTERPOLATOR MATRIX NOT AVAILABLE' FLAG IS SET,		302A0600	000000		
00101	69*	C				30100610	000000		
00101	70*	C	2	THE AEROELEMENT ACCELERATIONS, A, ARE CALCULATED.		30100620	000000		
00101	71*	C				30100630	000000		
00101	72*	C				30100640	000000		
00101	73*	C	REQUIRED SUBROUTINES *****					30130650	000000
00101	74*	C					30130652	000000	
00101	75*	C	401	AVIRI			30130654	000000	
00101	76*	C			404	U	30130656	000000	
00101	77*	C	407	STA			30130658	000000	
00101	78*	C			408	P	30130660	000000	
00101	79*	C	417	STSTAT	416	STAT	30130662	000000	
00101	80*	C			422	NEI	30130664	000000	
00101	81*	C			424	INTP	30130666	000000	
00101	82*	C	427	STEIJ	426	EIJ	30130668	000000	
00101	83*	C			428	MU	30130670	000000	
00101	84*	C	431	STMUTH	430	MUTHET	30130672	000000	
00101	85*	C					30100680	000000	
00101	86*	C					30100690	000000	
00101	87*	C					30100700	000000	
00103	88*	C	INTEGER IL,IH,IS,ID,IE					302A0710	000000
00104	89*	C	INTEGER STAT						000000
00105	90*	C	REAL MU,MUTHET						000000
00106	91*	C	REAL INTP	@ ACCESS TO INTERPOLATOR MATRIX			V01-03D	000000	
00107	92*	C	INTEGER LNEI(5)	@ LOCAL NEIGHBOR LIST			V01-03D	000000	
00110	93*	C	INTEGER LSTAT	@ LOCAL STATUS			V01-03D	000000	
00111	94*	C	REAL LP	@ LOCAL COPY -- PRESSURE			V01-03D	000000	
00112	95*	C	REAL LRHO	@ LOCAL COPY -- DENSITY			V01-03D	000000	
00113	96*	C	REAL LINTP(5,3)	@ LOCAL COPY -- INTERPOLATOR MATRIX			V01-03D	000000	
00114	97*	C	REAL LMU	@ LOCAL COPY -- VISCOSITY			V01-03D	000000	

Listing 6.—Continued.

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00115 98* REAL LNMU(5) @ LOCAL COPY -- NEIGHBOR VISCOUSITIES V01-03D 000000
00116 99* REAL LEIJ(3,3) @ LOCAL COPY -- STRAIN RATE MATRIX V01-03D 000000
00117 100* REAL LMUTHE @ LOCAL COPY -- MUTHET V01-03D 000000
00120 101* DATA ID/302/ 302A0712 000000
00122 102* DATA IE/1/ 302A0714 000000
00124 103* REAL DELT(5),DPDXJ(3),DTDXJ(3),DELTH(5,3,3),DMEDXI(3,3) 30100760 000000
00125 104* REAL DEJDXI(3) 30100770 000000
00126 105* DEFINE DU(I,J)=U(I,J) 30100780 000000
00127 106* DEFINE DP(I)=P(I) 30100790 000000
00130 107* DEFINE DMUTHE(I)=MUTHET(I) 30100800 000000
00131 108* DEFINE DMU(I,J)=MU(I,J) 30100810 000000
00132 109* DEFINE DEIJ(I,J,K)=EIJ(I,J,K) 30100820 000000
00133 110* CALL CHKLH(IL,IH,IS,ID,IE) @ GO CHECK AEROELEMENT RANGE 302A0990 000000
00134 111* IF (IS) 100,701,100 @ VALID RANGE ? 302A1010 000006
00137 112* 100 DO 221 I1=IL,IH,IS @ YES, DO EACH V01-03D 000010
00142 113* LSTAT=STAT(I1) @ LOCALIZE AEROELEMENT STATUS V01-03D 000020
00143 114* IF (AND(LSTAT,1)) 220,103,220 @ INTERPOLATOR AVAILABLE ? V01-03D 000023
00146 115* 103 LRHO=RHO(I1) @ YES, LOCALIZE DENSITY V01-03D 000026
00147 116* LSTAT=AND(LSTAT,COMPL(2)) @ RESET DENSITY ERROR FLAG V01-03D 000032
00150 117* IF (LRHO-1.0E-25) 106,106,107 @ DENSITY TOO SMALL ? V01-03D 000035
00153 118* 106 LSTAT=OR(LSTAT,2) @ YES, SET FLAG V01-03D 000040
00154 119* 107 CALL STSTAT (I1,LSTAT) @ REVISE STATUS IN ANY EVENT V01-03D 000044
00155 120* IF (AND(LSTAT,2)) 220,109,220 @ DENSITY OK ? V01-03D 000047
00160 121* 109 LMU=MU(I1,1) @ YES, LOCALIZE VISCOSITY V01-03D 000052
00161 122* DO 112 I=1,5 @ LOCALIZE NEIGHBOR LIST V01-03D 000062
00164 123* LNEI(I)=NEI(I1,I) @ V01-03D 000062
00165 124* 112 CONTINUE @ V01-03D 000100
00167 125* DO 116 I=1,3 @ LOCALIZE TRANSPOSE OF V01-03D 000100
00172 126* DO 116 J=1,3 @ STRAIN RATE MATRIX V01-03D 000100
00175 127* LEIJ(J,I)=EIJ(I1,I,J) @ V01-03D 000100
00176 128* 116 CONTINUE @ V01-03D 000121
00201 129* DO 120 I=1,3 @ LOCALIZE TRANSPOSE OF V01-03D 000121
00204 130* DO 120 J=1,5 @ INTERPOLATOR MATRIX V01-03D 000121
00207 131* LINTP(J,I)=INTP(I1,I,J) @ V01-03D 000121
00210 132* 120 CONTINUE @ V01-03D 000136
00213 133* DO 124 I=1,5 @ LOCALIZE NEIGHBOR'S V01-03D 000136
00216 134* J=LNEI(I) @ VISCOSITIES V01-03D 000136
00217 135* LNMU(I)=MU(J,1) @ V01-03D 000137
00220 136* 124 CONTINUE @ V01-03D 000145
00222 137* LP=P(I1) @ LOCALIZE PRESSURE V01-03D 000145
00223 138* LMUTHE=MUTHET(I1) @ LOCALIZE MUTHET V01-03D 000151
00224 139* DO 201 I=1,5 @ FORM PRESSURE DIFFERENCES V01-03D 000160
00227 140* 201 DELT(I)=DP(LNEI(I))-LP @ V01-03D 000160
00231 141* DO 207 J=1,3 @CLR DERIVATIVES OF PRESSURE 30101100 000174
00234 142* DPDXJ(J)=0.0 @ AND CALCULATE NEW BY 30101110 000174
00235 143* DO 207 K=1,5 @ INTERPOLATOR 30101120 000177
00240 144* 207 DPDXJ(J)=DPDXJ(J)+(LINTP(K,J)*DELT(K)) @ V01-03D 000177
00243 145* DO 208 I=1,5 @CALC NOTE 3 DIFFERENCES 30101140 000211
00246 146* 208 DELT(I)=DMUTHE(LNEI(I))-LMUTHE @ V01-03D 000211
00250 147* DO 209 J=1,3 @CLR NOTE 3 DERIVATIVES AND 30101160 000225
00253 148* DTDXJ(J)=0.0 @ CLACULATE NEW BY 30101170 000225
00254 149* DO 209 K=1,5 @ INTERPOLATOR 30101180 000230
00257 150* 209 DTDXJ(J)=DTDXJ(J)+(LINTP(K,J)*DELT(K)) @ V01-03D 000230
00262 151* DO 210 K=1,5 @CALC DIFFERENCE MATRIX FOR 30101200 000251
00265 152* DO 210 I=1,3 @ 2*MU*EIJ(I,J),X(I) 30101210 000251
00270 153* DO 210 J=1,3 30101220 000251
00273 154* 210 DELTH(K,I,J)=((LNMU(K)*DEIJ(LNEI(K),I,J))-(LMU*LEIJ(J,I)))*2.0 @ V01-03D 000251
00277 155* DO 211 I=1,3 @CLR DERIVATIVES AND CALC NEW 30101250 000311
00302 156* DO 211 J=1,3 @ FOR 2*MU*EIJ(I,J),X(I) 30101260 000311
00305 157* DMEDXI(I,J)=0.0 30101270 000311
00306 158* DO 211 K=1,5 30101280 000313
00311 159* 211 DMEDXI(I,J)=DMEDXI(I,J)+(LINTP(K,I)*DELTH(K,I,J)) @ V01-03D 000313
00315 160* DO 212 J=1,3 @PERFORM IMPLIED TENSOR SUM 30101300 000342
00320 161* DEJDXI(J)=0.0 @ PER NAVIER-STOKES EQUATION 30101310 000342
00321 162* DO 212 I=1,3 30101320 000344
00324 163* 212 DEJDXI(J)=DEJDXI(J)+DMEDXI(I,J) 30101330 000344
00327 164* DO 213 J=1,3 @ CALC NAVIER-STOKES EQUATION 30131340 000355
00332 165* RRR=(DTDXJ(J)+DEJDXI(J)-DPDXJ(J))/LRHO @ V01-03D 000355
00333 166* 213 CALL STA (I1,J,RRR) @ 30131355 000362
00335 167* 220 CALL CHKTIM (IL,IH,I1) @ KEEP AN EYE ON THE TIME V01-03D 000372
00336 168* 221 CONTINUE @ V01-03D 000403
00340 169* 701 RETURN 301A1370 000403
00341 170* END 30101380 000450
END FOR
>

```

Listing 6.—Concluded.

#FOR,MS CASPER9.MOVELD
 FOR 4R1 E -04/13/84-15:11:33 (12,)
 >@EOF

SUBROUTINE MOVEL ENTRY POINT 001010

STORAGE USED: CODE(1) 001544; DATA(0) 002706; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 NZNC 000001
 0004 IDUC 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0005 FZ
 0006 STAT
 0007 ZBL
 0010 IPZBL
 0011 IPLZN
 0012 LZN
 0013 CHKLH
 0014 CHKTIM
 0015 STIAES
 0016 X
 0017 U
 0020 A
 0021 STS
 0022 TOGSW
 0023 GRDBD
 0024 SURFVE
 0025 SURFAC
 0026 STSTAT
 0027 ERROR2
 0030 TSTZN
 0031 TSTRDT
 0032 NWDU\$
 0033 NID2\$
 0034 SQRT
 0035 NERR3\$
 0036 NI01\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	001333	1002L	0001	000163	101L	0001	001467	1025L	0001	001476	1028L	0001	001501	1050L				
0001	000412	106L	0001	000262	107L	0000	000243	1075F	0000	000251	1076F	0000	000261	1077F				
0000	000267	1078F	0000	000275	1079F	0000	000304	1080F	0001	001110	15L	0001	000007	175G				
0001	000007	200G	0001	000046	217G	0001	000714	219L	0001	000767	221L	0001	000071	227G				
0001	000153	250G	0001	000011	2755L	0001	000040	2796L	0001	001203	29L	0001	000264	313G				
0001	000274	322G	0001	000311	330G	0001	000324	337G	0001	000373	344G	0001	000442	3500L				
0001	000351	355G	0001	000472	3570L	0001	000503	3572L	0000	000134	3573F	0001	000514	3580L				
0001	000521	3600L	0001	000360	363G	0001	000566	3710L	0001	000371	373G	0001	000604	3760L				
0001	000615	3790L	0001	000617	3800L	0001	000633	3812L	0000	000156	3813F	0001	000644	3816L				
0001	000651	3840L	0001	000665	3852L	0000	000202	3853F	0001	000676	3856L	0001	000703	3880L				
0001	000400	400G	0001	000347	4002L	0001	000376	4010L	0001	000404	4012L	0001	001262	41L				
0001	000717	4100L	0001	000724	4101L	0000	000225	4102F	0001	000433	416G	0001	001264	42L				
0001	000216	4303L	0000	000114	4304F	0001	000227	4307L	0001	000234	4325L	0001	001272	45L				
0001	000524	454G	0001	000534	463G	0001	000575	507G	0001	000610	520G	0001	000737	572G				
0001	000735	6000L	0001	001041	610G	0001	001227	663G	0001	001372	735G	0001	001463	760G				
0020	R	000000	A	0000	R	000003	AL	0000	R	000314	ARB	0000	R	000073	B			
0005	I	000000	FZ	0000	R	000026	GB	0000	I	000054	I	0000	I	000063	IBUMP			
0000	I	000070	IDB	0000	I	000102	IDMIN	0004	I	000000	IDU	0000	I	000104	IDUM			
0000	I	000064	IFZ	0000		002610	INJP*	0000		002627	INJP*	0000		002623	INJP*			
0011	I	000000	IPLZN	0010	I	000000	IPZBL	0000	I	000314	IRB	0000	I	000002	IRBFF			
0000	I	000000	IS	0000	I	000113	IT	0000	I	000062	IZVCF	0000	I	000061	I1			
0000	I	000072	K	0012	I	000000	LZN	0000	I	000103	N	0000	I	000105	N			
0000	I	000107	NB	0000	I	000110	NC	0000	I	000075	NNN	0003	I	000000	NZN			
0000	R	000112	SV	0000	R	000071	SVMIN	0000	R	000065	T	0000	R	000077	TA			
															0000	R	000060	TE

Listing 7.—Subroutine MOVEL.

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0000 R 000056 TINC      0000 R 000057 TINCSG      0000 R 000067 TLEFT      0000 R 000076 TN      0000 R 000100 TQ
0000 R 000066 TS      0017 R 000000 U      0000 R 000045 UA      0000 R 000031 UL      0000 R 000041 UN
0000 R 000035 UQ      0000 R 000051 VBD      0016 R 000000 X      0000 R 000022 XA      0000 R 000006 XL
0000 R 000016 XN      0000 R 000012 XQ      0007 I 000000 ZBL

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00101      1*      SUBROUTINE MOVEL (IL,IH,CURTIM,GDAST,NINC)      901A0010      000000
00101      2*      C      90100030      000000
00101      3*      C      90100040      000000
00101      4*      C      MOVEL      ***** A SUBROUTINE FOR CASPER *****      90100050      000000
00101      5*      C      AUTHOR      WILLIAM HENRY JONES      90100060      000000
00101      6*      C      V02-00      14 APR 77      90100070      000000
00101      7*      C      V02-01      22 JUN 77      90110071      000000
00101      8*      C      V02-02      26 JUL 77      90120072      000000
00101      9*      C      V02-03      22 SEP 77      90130073      000000
00101     10*      C      V02-04      22 SEP 77      90140074      000000
00101     11*      C      V02-05      26 SEP 77      90150075      000000
00101     12*      C      V02-06      01 JUN 78      90160076      000000
00101     13*      C      V02-07      16 JUN 78      90170077      000000
00101     14*      C      V02-08      29 AUG 78      90180078      000000
00101     15*      C      V02-08A     13 FEB 79      901A0079      000000
00101     16*      C      V02-08B     09 MAR 79      901B0080      000000
00101     17*      C      V02-08C     13 FEB 80      INPUT/OUTPUT SEGREGATION      000000
00101     18*      C      V02-08D     15 SEP 80      FUNCTION TYPE STATEMENTS      000000
00101     19*      C      V02-08E     28 SEP 81      MOVING BOUNDARIES      V02-08E      000000
00101     20*      C      V02-08F     06 JAN 83      BAD POSITION INTEGRATION      V02-08F      000000
00101     21*      C      V02-08G     16 MAY 83      TYPE OF ZBL WRONG      V02-08G      000000
00101     22*      C      V02-08H     27 JUN 83      DEBUG MESSAGES AND HISTORY      V02-08H      000000
00101     23*      C      V02-08I     27 JUL 83      TYPOS      V02-08I      000000
00101     24*      C      V02-08J     05 AUG 83      ZERO VELOCITY COLLISIONS      V02-08J      000000
00101     25*      C      V02-08K     24 OCT 83      FLOW ZONE NOT FOUND TRAPS      V02-08K      000000
00101     26*      C      V02-08L     25 JAN 84      AVOID ENDLESS BUMPS      V02-08L      000000
00101     27*      C      90100090      000000
00101     28*      C      ARGUMENTS IN CASPER 'CACHE' MEMORY *****      90180094      000000
00101     29*      C      90180096      000000
00101     30*      C      ARGUMENT      TYPE      DIMENSION      DESCRIPTION      90100100      000000
00101     31*      C      -----      -----      -----      -----      90180110      000000
00101     32*      C      X      REAL      1 TO ISIZE      AEROELEMENT POSITION      90100120      000000
00101     33*      C      1 TO 3      COORDINATES      90100130      000000
00101     34*      C      90100140      000000
00101     35*      C      U      REAL      1 TO ISIZE      AEROELEMENT VELOCITIES      90100150      000000
00101     36*      C      1 TO 3      90100160      000000
00101     37*      C      90100170      000000
00101     38*      C      A      REAL      1 TO ISIZE      AEROELEMENT ACCELERATIONS      90100180      000000
00101     39*      C      1 TO 3      90100190      000000
00101     40*      C      90100200      000000
00101     41*      C      FZ      INTEGER      1 TO ISIZE      AEROELEMENT FLOW ZONE      90100210      000000
00101     42*      C      NUMBERS (BY AEROELEMENT)      90100220      000000
00101     43*      C      90100230      000000
00101     44*      C      STAT      INTEGER      1 TO ISIZE      AEROELEMENT STATUS LIST      90100240      000000
00101     45*      C      90100360      000000
00101     46*      C      ZBL      INTEGER      1 TO ZBLSZ      BOUNDARY LIST BY FLOW ZONES      90100370      000000
00101     47*      C      90100380      000000
00101     48*      C      IPZBL      INTEGER      1 TO NZN      ZBL CONTROL PARAMETERS LIST      90100390      000000
00101     49*      C      1 TO 2      (X,1) = STARTING POINT      90100400      000000
00101     50*      C      (X,2) = STRING LENGTH      90100410      000000
00101     51*      C      90100420      000000
00101     52*      C      90100560      000000
00101     53*      C      ARGUMENTS PASSED IN SUBROUTINE CALL *****      90180562      000000
00101     54*      C      90180564      000000
00101     55*      C      ARGUMENT      TYPE      DIMENSION      DESCRIPTION      90180566      000000
00101     56*      C      -----      -----      -----      -----      90180568      000000
00101     57*      C      IL      INTEGER      SCALAR      AEROELEMENT ID LOW LIMIT      901A0569      000000
00101     58*      C      901A0570      000000
00101     59*      C      IH      INTEGER      SCALAR      AEROELEMENT ID HIGH LIMIT      901A0571      000000
00101     60*      C      901A0572      000000
00101     61*      C      CURTIM      REAL      SCALAR      CURRENT OPENING TIME      901A0573      000000
00101     62*      C      901A0574      000000
00101     63*      C      GDAST      REAL      SCALAR      BASIC TIME INCREMENT      901A0575      000000
00101     64*      C      90180576      000000

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Listing 7.—Continued.

00101	65*	C	NINC	INTEGER	SCALAR	NUMBER OF TIME SUB-	90180578	000000	
00101	66*	C				INCREMENTS	90180580	000000	
00101	67*	C					90180582	000000	
00101	68*	C					90180584	000000	
00101	69*	C	RESULT LOCATIONS *****						000000
00101	70*	C						000000	
00101	71*	C	LOCATION	CONTENTS				000000	
00101	72*	C	-----	-----				000000	
00101	73*	C	AESCRA	FINAL FLOW ZONE ID OF AEROELEMENT				000000	
00101	74*	C						000000	
00101	75*	C	S(1)	X(1)				000000	
00101	76*	C	S(2)	X(2)				000000	
00101	77*	C	S(3)	X(3)				000000	
00101	78*	C	S(4)	U(1)				000000	
00101	79*	C	S(5)	U(2)				000000	
00101	80*	C	S(6)	U(3)				000000	
00101	81*	C						000000	
00101	82*	C						000000	
00101	83*	C	DESCRIPTION *****				90180586	000000	
00101	84*	C				90180588	000000		
00101	85*	C	MOVEL IS A SUBROUTINE WHICH, GIVEN THE POSITION, VELOCITY, AND			90100590	000000		
00101	86*	C	ACCELERATION OF INDIVIDUAL AEROELEMENTS AS WELL AS A DEFINITION			90100600	000000		
00101	87*	C	OF THE BOUNDARIES AND FLOW ZONES OF THE AIRFLOW VOLUME, WILL			90100610	000000		
00101	88*	C	REPOSITION THOSE AEROELEMENTS THAT ARE NOT RESTRICTED TO OTHER			90100620	000000		
00101	89*	C	PRESET LAWS OF MOTION (E.G. - BOUNDARY ELEMENTS FIXED IN SPACE)			90100630	000000		
00101	90*	C	ACCORDING TO THE CLASSIC INTEGRATION OF CONSTANTLY ACCELERATING			90100640	000000		
00101	91*	C	MOTION.			90100650	000000		
00101	92*	C				90100660	000000		
00101	93*	C	DURING SUCH RELOCATION EACH APPROPRIATE BOUNDARY IS CHECKED FOR			90100670	000000		
00101	94*	C	POTENTIAL VIOLATIONS BY THE AEROELEMENT. IF SUCH A VIOLATION IS			90100680	000000		
00101	95*	C	DETECTED THE POINT OF VIOLATION IS FOUND AND THE AEROELEMENT IS			90100690	000000		
00101	96*	C	ELASTICALLY BOUNCED OFF THE BOUNDARY AT THAT LOCATION. TO ENHANCE			90100700	000000		
00101	97*	C	BOUNDARY VIOLATION DETECTION A SUB-INCREMENTAL TIME STEP IS			90100710	000000		
00101	98*	C	SPECIFYABLE BY THE INTEGER ARGUMENT NINC. THIS WILL DIVIDE THE			90100720	000000		
00101	99*	C	PARABOLIC MOTION FROM X @ T TO X @ T+GDAST INTO NINC EQUAL STEPS			90100730	000000		
00101	100*	C	AND CHECK FOR BOUNDARY VIOLATIONS AT EACH OF THE INTERMEDIATE			90100740	000000		
00101	101*	C	POSITIONS, THUS LOWERING THE PROBABILITY OF AEROELEMENTS *PASSING			90100750	000000		
00101	102*	C	THROUGH* THIN BOUNDARIES SUCH AS LEADING AND TRAILING EDGES OF			90100760	000000		
00101	103*	C	AIRFOILS.			90100770	000000		
00101	104*	C				V02-08E	000000		
00101	105*	C	THE BOUNDARY BOUNCING PROCESS IS A SIMPLE REFLECTION ALGORITHM,			V02-08E	000000		
00101	106*	C	I.E., ANGLE OF INCIDENCE EQUALS ANGLE OF REFLECTION. TO DO THIS,			V02-08E	000000		
00101	107*	C	THE VELOCITY VECTOR FOR THE AEROELEMENT IS ADJUSTED AT THE TIME			V02-08E	000000		
00101	108*	C	OF BOUNCE TO GIVE THE APPROPRIATE INITIAL DIRECTION. THE			V02-08E	000000		
00101	109*	C	ACCELERATION OF THE AEROELEMENT IS NOT ADJUSTED. TO ACCOUNT			V02-08E	000000		
00101	110*	C	FOR SITUATIONS WHERE THE AEROELEMENT IS NOT MOVING AND IS HIT			V02-08E	000000		
00101	111*	C	BY A MOVING BOUNDARY, THE AEROELEMENT VELOCITY IS FIRST CONVERTED			V02-08E	000000		
00101	112*	C	TO A VELOCITY RELATIVE TO THE BOUNDARY, ADJUSTED FOR THE BOUNCE,			V02-08E	000000		
00101	113*	C	AND THEN CONVERTED BACK TO VELOCITY RELATIVE TO THE STATIONARY			V02-08E	000000		
00101	114*	C	REFERENCE FRAME.			V02-08E	000000		
00101	115*	C				90100780	000000		
00101	116*	C	SELECTED VARIABLES IN THE ARGUMENT LIST, NOTABLY LZN, ZBL, BDZN,			90100830	000000		
00101	117*	C	AND NEIZN, ARE PASSED WITH CONTROL PARAMETER LISTS IN DYNAMICALLY			90100840	000000		
00101	118*	C	VARIABLE ARRAY FORM. AS NOTED IN THE ARGUMENT DESCRIPTIONS, THE			90100850	000000		
00101	119*	C	CONTROL PARAMETERS CONSIST OF A STARTING POINT LIST AND A STRING			90100860	000000		
00101	120*	C	LENGTH LIST. THESE DYNAMICALLY VARIABLE			90180870	000000		
00101	121*	C	ARRAYS ARE ARRANGED SUCH THAT THE SUB-ARRAY RUNS FROM 1 TO THE			90100890	000000		
00101	122*	C	STRING LENGTH AND THE FIRST ELEMENT IS AT THE STARTING POINT PLUS			90100900	000000		
00101	123*	C	1. THUS, FOR LZN, THE J TH ELEMENT OF THE I TH FLOW ZONE LIST			90100910	000000		
00101	124*	C	WOULD BE LZN(IPLZN(I,1)+J) AND THE LENGTH OF THE I TH FLOW ZONE			90100920	000000		
00101	125*	C	LIST WOULD BE IPLZN(I,2).			90100930	000000		
00101	126*	C				V02-08H	000000		
00101	127*	C				V02-08H	000000		
00101	128*	C	POSITION HISTORY RING BUFFER			V02-08H	000000		
00101	129*	C				V02-08H	000000		
00101	130*	C	WITH VERSION V02-08H, A POSITION HISTORY RING BUFFER IS PROVIDED.			V02-08H	000000		
00101	131*	C	EACH TIME A NEW AEROELEMENT POSITION IS ESTABLISHED, AN ENTRY IS			V02-08H	000000		
00101	132*	C	MADE IN THE NEXT (REPLACING THE OLDEST) RING BUFFER SLOT. IF AN			V02-08H	000000		
00101	133*	C	ERROR OCCURS AND DEBUG MESSAGES ARE ENABLED, THE CONTENTS OF THE			V02-08H	000000		
00101	134*	C	RING BUFFER ARE DUMPED WITH THE ERROR MESSAGE.			V02-08H	000000		
00101	135*	C				V02-08H	000000		
00101	136*	C	THE FOLLOWING INFORMATION IS RECORDED IN EACH SLOT OF THE			V02-08H	000000		

Listing 7.—Continued.

00101	137*	C	POSITION-HISTORY RING BUFFER:		V02-08H	000000		
00101	138*	C			V02-08H	000000		
00101	139*	C	INDEX	CONTENTS	V02-08H	000000		
00101	140*	C			V02-08H	000000		
00101	141*	C	1	INFORMATION AND STATUS	V02-08H	000000		
00101	142*	C	2	AEROELEMENT ID	V02-08H	000000		
00101	143*	C	3	AEROELEMENT X(1)	V02-08H	000000		
00101	144*	C	4	AEROELEMENT X(2)	V02-08H	000000		
00101	145*	C	5	AEROELEMENT X(3)	V02-08H	000000		
00101	146*	C	6	AEROELEMENT X(4)	V02-08H	000000		
00101	147*	C	7	FLOW ZONE ID	V02-08H	000000		
00101	148*	C	8	SURFACE ID	V02-08H	000000		
00101	149*	C	9	SURFACE VALUE	V02-08H	000000		
00101	150*	C	10	SURFACE GRADIENT (1)	V02-08H	000000		
00101	151*	C	11	SURFACE GRADIENT (2)	V02-08H	000000		
00101	152*	C	12	SURFACE GRADIENT (3)	V02-08H	000000		
00101	153*	C			V02-08J	000000		
00101	154*	C			V02-08J	000000		
00101	155*	C			V02-08J	000000		
00101	156*	C			V02-08J	000000		
00101	157*	C	ZERO VELOCITY IMPACTS		V02-08J	000000		
00101	158*	C			V02-08J	000000		
00101	159*	C	ANOTHER ANOMALOUS SITUATION IS TREATED BY VERSION V02-08J. IT		V02-08J	000000		
00101	160*	C	IS POSSIBLE THAT AN AEROELEMENT MAY LIE DIFFERENTIALLY CLOSE TO		V02-08J	000000		
00101	161*	C	A BOUNDARY AND HAVE A ZERO VELOCITY NORMAL TO THE BOUNDARY WITH A		V02-08J	000000		
00101	162*	C	FINITE NORMAL ACCELERATION INTO THE BOUNDARY. IN THIS CASE, ANY		V02-08J	000000		
00101	163*	C	INCREMENTAL STEP FORWARD IN TIME WILL CARRY THE AEROELEMENT INTO		V02-08J	000000		
00101	164*	C	VIOLATION OF THE BOUNDARY. THE BOUNDARY BOUNCE OPERATION WILL		V02-08J	000000		
00101	165*	C	THEN RETURN THE AEROELEMENT TO ITS ORIGINAL POSITION IN SPACE		V02-08J	000000		
00101	166*	C	AND TIME AND MODIFY ITS VELOCITY SO THAT THERE IS (STILL) NO		V02-08J	000000		
00101	167*	C	VELOCITY COMPONENT NORMAL TO THE BOUNDARY (THE NEGATIVE OF ZERO		V02-08J	000000		
00101	168*	C	BEING ZERO). IN THIS MANNER AN INFINITE LOOP WILL FORM.		V02-08J	000000		
00101	169*	C			V02-08J	000000		
00101	170*	C	THIS SITUATION IS DETECTED BY THE SIMPLE EXPEDIENT OF OBSERVING		V02-08J	000000		
00101	171*	C	WHETHER OR NOT THE BOUNCE LOCATOR REPLACED THE ORIGINAL NON-		V02-08J	000000		
00101	172*	C	VIOLATING POINT WITH A NEW NON-VIOLATING POINT. IF SUCH A		V02-08J	000000		
00101	173*	C	REPLACEMENT WAS MADE, THEN THE ORIGINAL POINT WAS NOT DIFFER-		V02-08J	000000		
00101	174*	C	ENTIALLY CLOSE TO THE BOUNDARY SINCE (HA! HA!) A POINT BETWEEN		V02-08J	000000		
00101	175*	C	IT AND THE BOUNDARY EXISTED.		V02-08J	000000		
00101	176*	C			V02-08J	000000		
00101	177*	C	IF THIS CONDITION IS IDENTIFIED AS DESCRIBED IN THE PRECEEDING		V02-08J	000000		
00101	178*	C	PARAGRAPH, THE ACCELERATION OF THE AEROELEMENT RELATIVE TO THE		V02-08J	000000		
00101	179*	C	BOUNDARY IS EXAMINED. IF AN ACCELERATION COMPONENT INTO THE		V02-08J	000000		
00101	180*	C	BOUNDARY EXISTS, IT IS SET TO ZERO IN THE FRAME OF REFERENCE OF		V02-08J	000000		
00101	181*	C	THE BOUNDARY.		V02-08J	000000		
00101	182*	C			V02-08H	000000		
00101	183*	C			90100940	000000		
00101	184*	C			90100950	000000		
00101	185*	C			90100960	000000		
00101	186*	C			90100970	000000		
00101	187*	C			90100980	000000		
00101	188*	C			90100990	000000		
00101	189*	C			90101000	000000		
00101	190*	C			90102500	000000		
00101	191*	C	REQUIRED SUBROUTINES *****		90182510	000000		
00101	192*	C			90182512	000000		
00101	193*	C	401	AVIRI	90182514	000000		
00101	194*	C		402	X	90182516	000000	
00101	195*	C		404	U	90182518	000000	
00101	196*	C		406	A	90182520	000000	
00101	197*	C	417	STSTAT	416	STAT	90182522	000000
00101	198*	C	421	STFZ	420	FZ	90182524	000000
00101	199*	C			470	FVIRI	90182534	000000
00101	200*	C	471	ZBL			90182536	000000
00101	201*	C	475	HVIRI	476	IPZBL	90182538	000000
00101	202*	C	911	MRRM	912	TSTZN	90182540	000000
00101	203*	C					90182542	000000
00101	204*	C					90182544	000000
00101	205*	C	ERRORS REPORTED *****		90182546	000000		
00101	206*	C			90182548	000000		
00101	207*	C	1	NEITHER RESULT OF BOUNDARY SURFACE FINDER WAS	90182550	000000		
00101	208*	C		SAFE (901X3870).	90182552	000000		

Listing 7.—Continued.

00101	209*	C	2	BOUNDARY SURFACE FINDER SETUP PUSHED 'Q' BACK	90182554	000000
00101	210*	C		BEYOND ZERO TIME WITHOUT FINDING A SAFE POSITION	90182556	000000
00101	211*	C		(901X3348).	90182558	000000
00101	212*	C	3	AN AEROELEMENT FLOW PATH WAS FOUND THAT LEADS TO	901A2560	000000
00101	213*	C		BOUNDARY VIOLATION WITHOUT CROSSING A LEGITIMATE	901A2565	000000
00101	214*	C		ACTIVE BOUNDARY.	901A2570	000000
00101	215*	C	4	THE BOUNDARY INTERCEPT LOCATOR FAILED TO LOCK ON	901A2575	000000
00101	216*	C		TO AN EXISTING ACTIVE BOUNDARY.	901A2580	000000
00101	217*	C			901A2585	000000
00101	218*	C-			901A2590	000000
00103	219*			PARAMETER OURID=901 @	V02-08H	000000
00104	220*			PARAMETER IBUMPC=100 @ INITIAL BUMP COUNT	V02-08L	000000
00105	221*			PARAMETER IRBL=100 @ RING BUFFER LENGTH	V02-08H	000000
00106	222*			PARAMETER IRBIS=1 @ INFORMATION AND STATUS	V02-08H	000000
00107	223*			PARAMETER IRBAI=2 @ AEROELEMENT ID	V02-08H	000000
00110	224*			PARAMETER IRBX1=3 @ AEROELEMENT X(1)	V02-08H	000000
00111	225*			PARAMETER IRBX2=4 @ AEROELEMENT X(2)	V02-08H	000000
00112	226*			PARAMETER IRBX3=5 @ AEROELEMENT X(3)	V02-08H	000000
00113	227*			PARAMETER IRBX4=6 @ AEROELEMENT X(4)	V02-08H	000000
00114	228*			PARAMETER IRBFI=7 @ FLOW ZONE ID	V02-08H	000000
00115	229*			PARAMETER IRBSI=8 @ SURFACE ID	V02-08H	000000
00116	230*			PARAMETER IRBSV=9 @ SURFACE VALUE	V02-08H	000000
00117	231*			PARAMETER IRBG1=10 @ SURFACE GRADIENT (1)	V02-08H	000000
00120	232*			PARAMETER IRBG2=11 @ SURFACE GRADIENT (2)	V02-08H	000000
00121	233*			PARAMETER IRBG3=12 @ SURFACE GRADIENT (3)	V02-08H	000000
00122	234*			PARAMETER IRBM=12 @ SLOT LENGTH	V02-08H	000000
00123	235*			INCLUDE PGSDEF @ PAX GLOBAL STATUS DEFINITIONS	V02-08H	000000
00123	236*	C+			V02-08H	000000
00123	237*	C		POSITION RING BUFFER STATUS BITS	V02-08H	000000
00123	238*	C-			V02-08H	000000
00126	239*			PARAMETER IRBISA=1 @ AEROELEMENT ID/POSITION VALID	V02-08H	000000
00127	240*			PARAMETER IRBISF=2 @ FLOW ZONE ID VALID	V02-08H	000000
00130	241*			PARAMETER IRBISS=4 @ SURFACE ID VALID	V02-08H	000000
00131	242*			PARAMETER IRBISV=8 @ SURFACE VALUE VALID	V02-08H	000000
00132	243*			PARAMETER IRBISG=16 @ GRADIENT VALID	V02-08H	000000
00133	244*			PARAMETER LUOUP=6 @ LOGICAL UNIT FOR OUTPUT	V02-08H	000000
00134	245*			INTEGER IL,IH,IS	901A2595	000000
00135	246*			INTEGER FZ,STAT,EIPLZN,ST,EMOD,STP1,ELZN,DLZN		000000
00136	247*			COMMON /NZNC/NZN	90102620	000000
00137	248*			COMMON /IDUC/IDU	90182630	000000
00140	249*			REAL CURTIM,GDAST	90182670	000000
00141	250*			INTEGER NINC	90182680	000000
00142	251*			INTEGER ZBL	V02-08G	000000
00143	252*			INTEGER IRB(IRBM,IRBL) @ POSITION RING BUFFER	V02-08H	000000
00144	253*			INTEGER IRBPT @ POSITION RING BUFFER POINTER	V02-08H	000000
00145	254*			INTEGER IRBPP @	V02-08H	000000
00146	255*			REAL AL(3),XL(4),XQ(4),XN(4),XA(4),GB(3)	V02-08F	000000
00147	256*			REAL UL(4),UQ(4),UN(4),UA(4)	V02-08F	000000
00150	257*			REAL VBO(3)	V02-08E	000000
00151	258*			REAL ARB(IRBM,IRBL) @ POSITION RING BUFFER	V02-08H	000000
00152	259*			EQUIVALENCE (IRB(I,1),ARB(I,1)) @	V02-08H	000000
00153	260*			DATA IRBPT/0/ @	V02-08H	000000
00155	261*			DATA IRBPP/0/ @	V02-08H	000000
00157	262*			DEFINE EZBL(I)=ZBL(I)	90112715	000000
00160	263*			DEFINE DZBL(I,J)=EZBL(IPZBL(I,1)+J)	90112720	000000
00161	264*			DEFINE EIPLZN(I,J)=IPLZN(I,J)	90112725	000000
00162	265*			DEFINE ST(I)=EIPLZN(FZ(I),1)	90112730	000000
00163	266*			DEFINE NU(I)=EIPLZN(FZ(I),2)	90112740	000000
00164	267*			DEFINE EMOD(I,J)=MOD(I,J)	90112745	000000
00165	268*			DEFINE STP1(I)=EIPLZN(EMOD(FZ(I),NZN)+1,1)	90112750	000000
00166	269*			DEFINE ELZN(I)=LZN(I)	90112755	000000
00167	270*			DEFINE DLZN(I)=ELZN(ST(I)+NU(I))	90112760	000000
00170	271*			IF (IRBPT) 2751,2751,2755 @ SHALL WE INIT RING BUFFER ?	V02-08H	000000
00173	272*	2751		IRBPT=1 @ YES, RESET POINTER	V02-08H	000002
00174	273*			DO 2754 I=1,IRBL @ ZAP BUFFER	V02-08H	000007
00177	274*			DO 2754 J=1,IRBM @	V02-08H	000007
00202	275*	2754		IRB(J,I)=0 @	V02-08H	000007
00205	276*	2755		CONTINUE @	V02-08H	000011
00206	277*			TINC=GDAST/NINC @CALC SUB-INCREMENT	90102770	000011
00207	278*			TINCSQ=0.5*TINC*TINC @CALC 1/2 SQUARE SUB-INCREMENT	90112780	000015
00210	279*			TE=0.001*TINC @TOLERANCE OF BOUNCES IN TIME	90132785	000020
00211	280*			CALL CHKLH (IL,IH,IS,901,5) @ GO CHECK AEROELEMENT RANGE	901A2790	000023

Listing 7.—Continued.

00212	281*	IF (IS) 2796,2794,2796	@ VALID RANGE ?	901A2792	000032
00215	282*	2794 RETURN	@ NO	901A2794	000034
00216	283*	2796 DO 221 I=IL,IH,IS	@ IN RANGE AEROELEMENT LOOP	901A2796	000040
00221	284*	CALL CHKTIM (IL,IH,I1)	@ KEEP AN EYE ON THE TIME		000046
00222	285*	IZVCF=0	@ SHOW NO ZERO VELOCITY PROB	V02-08J	000053
00223	286*	IBUMP=IBUMPC	@ INIT BUMP COUNTER	V02-08L	000054
00224	287*	IFZ=FZ(I1)	@ LOCALIZE		000056
00225	288*	CALL STIAES (I1,IFZ)	@ OUTPUT IN CASE OF A SKIP		000062
00226	289*	DO 201 I=1,3	@ LOCALIZE		000071
00231	290*	XL(I)=X(I1,I)	@ ORIGINAL POSITION		000071
00232	291*	UL(I)=U(I1,I)	@ ORIGINAL VELOCITY		000076
00233	292*	AL(I)=A(I1,I)	@ ACCELERATION		000103
00234	293*	CALL STS (I1,I,XL(I))	@ OUTPUT POSITION AND VELOCITY		000110
00235	294*	CALL STS (I1,I+3,UL(I))	@ IN CASE OF A SKIP		000117
00236	295*	201 CONTINUE	@		000133
00240	296*	IF (AND(STAT(I1),2**9)) 221,2820,221	@ SKIP IF SPECIAL		000133
00243	297*	2820 IF (IFZ-IDU) 2830,221,2830	@ SKIP IF IN THE DOG HOUSE		000143
00246	298*	2830 XL(4)=CURTIM	@		000146
00247	299*	DO 219 I=1,NINC	@START TIME SUB-INCREMENT LOOP	90102850	000153
00252	300*	T=TINC	@SET TIME SPAN	90102860	000153
00253	301*	TS=TINCSD	@SET 1/2 SQUARE TIME SPAN	90102870	000155
00254	302*	TLEFT=0.0	@SET TIME REMAINING SUB-INC	90102880	000157
00255	303*	IDB=-1	@SET BOUNDARY NO-VIO FLAG	90102890	000160
00256	304*	101 CALL SPC (XL,UL,T)	@ POSITION AT END OF SPAN	V02-08F	000163
00257	305*	CALL YNM (XL)	@ GO CHECK ALL BOUNDARIES	901A2930	000167
00260	306*	IF (IFZ-IDU) 103,4100,103	@ LOST FLOW ZONE TRACK ?	V02-08K	000172
00263	307*	103 IF (SVMIN) 106,106,104	@ NO, 106 ON VIOLATION	V02-08K	000175
00266	308*	104 IF (IDB) 219,105,105	@CHK FOR PENDING BOUNCE	90103070	000200
00271	309*	105 IBUMP=IBUMP-1	@ ONE LESS BUMP ALLOWED	V02-08L	000203
00272	310*	IF (IBUMP) 4302,4325,4325	@ BUMPED TOO OFTEN ?	V02-08L	000206
00275	311*	4302 CALL TQGSW (PGSBUG,\$4303,\$4307)	@ YES, SHALL WE PRINT MMSG ?	V02-08L	000210
00276	312*	4303 WRITE (LUOUP,4304,END=4307,ERR=4307)	@ YES, DO SO NOW	V02-08L	000216
00300	313*	4304 FORMAT (SBHOCASPER9,MOVELD (BUG) -- AEROELEMENT BUMPED TOO MANY TIV02-08L			000224
00300	314*	1MES,/,27H HISTORY BUFFER FOLLOWS...)	@	V02-08L	000224
00301	315*	CALL RBDMP	@ DUMP THE HISTORY BUFFER	V02-08L	000224
00302	316*	4307 CALL STIAES (I1,IDU)	@ DISCARD THIS TURKEY	V02-08L	000227
00303	317*	GO TO 221	@ DON'T WORK ANY MORE ON HIM	V02-08L	000232
00304	318*	4325 CALL GRDRD (XL,IDB,GB)	@ BOUNCE -- GET GRADIENT	V02-08L	000234
00305	319*	ARB(IRBG1,IRBPP)=GB(1)	@ RECORD GRADIENT RESULT	V02-08H	000242
00306	320*	ARB(IRBG2,IRBPP)=GB(2)	@	V02-08H	000244
00307	321*	ARB(IRBG3,IRBPP)=GB(3)	@	V02-08H	000246
00310	322*	IRB(IRBIS,IRBPP)=OR(IRB(IRBIS,IRBPP),IRBIS) @		V02-08H	000250
00311	323*	CALL SURFVE (XL,IDB,VBO,\$107)	@ GET SURFACE VELOCITY	V02-08E	000253
00312	324*	107 DO 108 K=1,3	@ GET VELOCITY OF AEROELEMENT	V01-08E	000264
00315	325*	108 UL(K)=UL(K)-VBO(K)	@ RELATIVE TO SURFACE	V02-08E	000264
00317	326*	B=0.0	@CLR ACCUMULATOR	90103090	000267
00320	327*	C=0.0	@CLR ACCUMULATOR	90103100	000270
00321	328*	DO 204 K=1,3	@ACCUMULATE LENGTH SQUARED	90103110	000274
00324	329*	204 B=GB(K)**2	@ OF GRADIENT VECTOR	90103120	000274
00326	330*	B=1.0/SQRT(B)	@FAST DIVIDE LENGTH OF GRAD	90133130	000300
00327	331*	DO 205 K=1,3	@ LOOP TO	90103140	000311
00332	332*	GB(K)=B*GB(K)	@ NORMALIZE GRADIENT	90103150	000311
00333	333*	205 C=C+GB(K)*UL(K)	@ ACCUMULATE DOT PROD VELOCITY	90103160	000313
00335	334*	C=2.0*C	@ADJUST CONSTANT FOR BOUNCE	90103170	000317
00336	335*	DO 206 K=1,3	@BOUNCE! VELOCITY ANGLE INCID.	90103180	000324
00341	336*	206 UL(K)=UL(K)-C*GB(K)	@ EQUALS ANGLE OF REFLECTION	90103190	000324
00343	337*	DO 208 K=1,3	@ AEROELEMENT VELOCITY RELA-	V02-08E	000333
00346	338*	208 UL(K)=UL(K)+VBO(K)	@ TIVE TO STATIONARY FRAME	V02-08E	000333
00350	339*	IF (IZVCF) 4001,4012,4001	@ GOT A ZERO VELOCITY PROB ?	V02-08J	000336
00353	340*	4001 CALL SURFAC (XL,IDB,VBO,\$4002)	@ YES, GET SURFACE'S ACCEL	V02-08J	000340
00354	341*	4002 DO 4003 K=1,3	@ GET ACCELERATION OF ELEMENT	V02-08J	000351
00357	342*	4003 AL(K)=AL(K)-VBO(K)	@ RELATIVE TO SURFACE	V02-08J	000351
00361	343*	C=0.0	@ CALC COMPONENT OF ACCEL	V02-08J	000354
00362	344*	DO 4006 K=1,3	@ NORMAL TO THE BOUNDARY	V02-08J	000360
00365	345*	4006 C=C+(GB(K)*AL(K))	@ (GRAD HAS BEEN NORMALIZED)	V02-08J	000360
00367	346*	IF (C) 4008,4010,4010	@ ANY ACCEL INTO BOUNDARY ?	V02-08J	000364
00372	347*	4008 DO 4009 K=1,3	@ YES, REMOVE IT	V02-08J	000371
00375	348*	4009 AL(K)=AL(K)-(C*GB(K))	@	V02-08J	000371
00377	349*	4010 DO 4011 K=1,3	@ ADJUST ACCEL BACK TO	V02-08J	000400
00402	350*	4011 AL(K)=AL(K)+VBO(K)	@ STATIONARY FRAME	V02-08J	000400
00404	351*	4012 CONTINUE	@	V02-08J	000404
00405	352*	T=TLEFT	@SET TIME SPAN FOR REST OF	90103200	000404

Listing 7.—Continued.

ORIGINAL PAGE IS
OF POOR QUALITY

00406	353*	TLEFT=0.0	@CLR REMAINING TIME	90103220	000405	
00407	354*	IDB=-1	@WIPE OUT PENDING BOUNCE	90103230	000406	
00410	355*	GO TO 101	@JMP BACK - FINISH SUB-INCREMT	90103240	000410	
00410	356*	C+		901A3250	000410	
00410	357*	C	THE FOLLOWING SECTION IS ENTERED WHEN A BOUNDARY IS VIOLATED.	901A3260	000410	
00410	358*	C	IT BACKS THE PARTICLE UP ALONG ITS PATH TO LOCATE THE POINT	901A3270	000410	
00410	359*	C	AT WHICH IT FIRST PENETRATES A BOUNDARY. WHEN THIS POINT IS	901A3280	000410	
00410	360*	C	LOCATED TO WITHIN TOLERANCE 'TE' THE ID OF THE BOUNDARY	901A3290	000410	
00410	361*	C	ABOUT TO BE VIOLATED IS LOADED INTO 'IDB' AND THE TIME IS	901A3300	000410	
00410	362*	C	SUBDIVIDED TO CAUSE A STEP JUST TO THE BOUNDARY FOLLOWED BY	901A3310	000410	
00410	363*	C	A BOUNCE AND A STEP TO THE END OF THE TIME SUB-INCREMENT.	901A3320	000410	
00410	364*	C		901A3330	000410	
00410	365*	C	IN LOCATING THE NEAR-VIOLATION POINT ALL BOUNDARIES IN THE	901A3340	000410	
00410	366*	C	MANDATORY FLOW ZONE AND IN THE AEROELEMENT'S FLOW ZONE OF	901A3350	000410	
00410	367*	C	RESIDENCE ARE CHECKED TO PRODUCE A VIOLATION/NO-VIOLATION	901A3360	000410	
00410	368*	C	DECISION. THIS DECISION SHOULD BE BASED ON AT LEAST ONE	901A3370	000410	
00410	369*	C	BOUNDARY EVALUATION THAT DID NOT TRUNCATE. IF THIS IS NOT	901A3380	000410	
00410	370*	C	THE CASE ERROR #3 IS REPORTED. A PROPER CASPER PROBLEM	901A3390	000410	
00410	371*	C	SETUP MAY NOT HAVE ANY AEROELEMENT FLOW PATH THAT CROSSES	901A3400	000410	
00410	372*	C	FROM A NON-VIOLATION AREA TO A VIOLATION AREA WITHOUT	901A3410	000410	
00410	373*	C	CROSSING A DEFINED BOUNDARY SURFACE.	901A3420	000410	
00410	374*	C-		901A3430	000410	
00411	375*	106	NNN=OR(STAT(I1),2**8)	@ SET MANDATORY SIFT BIT	901A3440	000412
00412	376*		CALL STSTAT (I1,NNN)	@	901A3450	000417
00413	377*		IZVCF=IZVCF+1	@ BUMP ZERO VELOCITY FLAG	V02-08J	000423
00414	378*		TN=T	@ N IMPLIES A POINT IN	901A3460	000426
00415	379*		DO 3480 J=1,4	@ VIOLATION	901A3470	000433
00420	380*		UN(J)=UL(J)	@	V02-08F	000433
00421	381*	3480	XN(J)=XL(J)	@	901A3480	000434
00423	382*		TA=-T	@ XL BACK TO ORIGINAL SPOT	901A3490	000437
00424	383*	3500	CALL SPC (XL,UL,TA)	@	V02-08F	000442
00425	384*		CALL YNH (XL)	@ CHECK BOUNDARIES HERE	901A3510	000446
00426	385*		IF (IFZ-IDU) 3529,4100,3529	@ LOST FLOW ZONE TRACK ?	V02-08K	000451
00431	386*	3529	IF (SVMIN) 3530,3530,3600	@ NO, NON-VIOLATING ?	V02-08K	000454
00434	387*	3530	IF (XL(4)) 3570,3570,3540	@ NO, CAN WE BACK UP FURTHER ?	901A3530	000457
00437	388*	3540	TN=TN-TA	@ KEEP TRACK OF TIME SPANS	901A3540	000462
00440	389*		T=T-TA	@	901A3550	000465
00441	390*		GO TO 3500	@ GO BACK IT UP	901A3560	000470
00442	391*	3570	CALL ERROR2 (901,2)	@ CAN'T SHAKE BOUNDARY	901A3570	000472
00443	392*		CALL TOGSW (PGSEBUG,*3572,*3580)	@ SHALL WE PROVIDE A MESSAGE ?	V02-08H	000475
00444	393*	3572	WRITE (LUOUP,3573,END=3580,ERR=3580) @ YES		V02-08H	000503
00446	394*	3573	FORMAT (67HOCASPER9,NOVELD (BUG) --	UNABLE TO BACK AEROELEMENT OUT	V02-08H	000511
00446	395*		1 OF CONFLICT,/,27H HISTORY BUFFER	FOLLOWS...) @	V02-08H	000511
00447	396*		CALL RBDMP	@ DUMP THE HISTORY	V02-08H	000511
00450	397*	3580	CALL STIAES (I1,IDU)	@ THIS TURKEY GOES TO SHEOL	V02-08H	000514
00451	398*		GO TO 221	@	901A3590	000517
00452	399*	3600	TQ=0.0	@ Q IMPLIES A POINT NOT IN	901A3600	000521
00453	400*		DO 3620 J=1,4	@ VIOLATION	901A3610	000524
00456	401*		UQ(J)=UL(J)	@	V02-08F	000524
00457	402*	3620	XQ(J)=XL(J)	@	901A3620	000525
00461	403*		IE3F=0	@ ERROR 3 ABORT FLAG	901A3630	000530
00462	404*		DO 3790 J=1,15	@ BISECTION LOOP	901A3640	000534
00465	405*		IF (ABS(TN-TQ)-TE) 3800,3660,3660	@ CLOSE ENOUGH ?	901A3650	000534
00470	406*	3660	TA=0.5*(TN+TQ)	@ NO, BIJECT AGAIN	901A3660	000542
00471	407*		CALL SPC (XA,UA,TA)	@ FIND THAT POINT IN SPACE	V02-08F	000546
00472	408*		CALL YNH (XA)	@ TEST THE BOUNDARIES	901A3680	000553
00473	409*		IF (IFZ-IDU) 3664,4100,3664	@ LOST FLOW ZONE TRACK ?	V02-08K	000556
00476	410*	3664	IF (IDMIN) 3710,3710,3700	@ NO, DID ALL TRUNCATE ?	V02-08K	000561
00501	411*	3700	IE3F=IDMIN	@ NO, FLAG AN ACTIVE BOUNDARY	901B3700	000564
00502	412*	3710	IF (SVMIN) 3760,3760,3720	@ A NON-VIOLATING POINT ?	901A3710	000566
00505	413*	3720	TQ=TA	@ YES, REPLACE Q POINT	901A3720	000570
00506	414*		DO 3740 K=1,4	@	901A3730	000575
00511	415*		UQ(K)=UA(K)	@	V01-08F	000575
00512	416*	3740	XQ(K)=XA(K)	@	901A3740	000576
00514	417*		IZVCF=0	@ SHOW NO ZERO VELOCITY GLITCH	V02-08J	000601
00515	418*		GO TO 3790	@	901A3750	000602
00516	419*	3760	TN=TA	@ NO, REPLACE N POINT	901A3760	000604
00517	420*		DO 3780 K=1,4	@	901A3770	000610
00522	421*		UN(K)=UA(K)	@	V02-08F	000610
00523	422*	3780	XN(K)=XA(K)	@	901A3780	000611
00525	423*	3790	CONTINUE	@	901A3790	000617
00527	424*	3800	IF (IE3F) 3810,3810,3840	@ CONSTRUCTION PROBLEM ?	901A3800	000617

Listing 7.—Continued.

00532	425*	3810	CALL ERROR2 (901,3)	@ YES, REPORT IT	901A3810	000621
00533	426*		CALL TOGSW (PGSBUG,\$3812,\$3816)	@ PRINT A MESSAGE ?	V02-08H	000625
00534	427*	3812	WRITE (LUOUP,3813,END=3816,ERR=3816) @ YES		V02-08H	000633
00536	428*	3813	FORMAT (82HOCASPER9.MOVELD (BUG) -- A BISECTION PROCESS DID NOT ENVO2-08H			000641
00536	429*		1COUNTER A GOVERNING SURFACE,/,27H HISTORY BUFFER FOLLOWS...) @		V02-08H	000641
00537	430*		CALL RBDMP	@ PRINT HISTORY BUFFER	V02-08H	000641
00540	431*	3816	CALL STIAES (I1,IDU)	@ FORGET THIS GUY	V02-08H	000644
00541	432*		GO TO 221	@	901A3830	000647
00542	433*	3840	IF (IDMIN) 3850,3850,3880	@ ALGORITHM DIDN'T TRACK ?	901A3840	000651
00545	434*	3850	CALL ERROR2 (901,4)	@ YES, VERY ODD	901A3850	000653
00546	435*		CALL TOGSW (PGSBUG,\$3852,\$3856)	@ SHALL WE PRINT A MESSAGE ?	V02-08H	000657
00547	436*	3852	WRITE (LUOUP,3853,END=3856,ERR=3856) @ YES		V02-08H	000665
00551	437*	3853	FORMAT (71HOCASPER9.MOVELD (BUG) -- BISECTION PROCESS DID NOT FINIV02-08H			000673
00551	438*		1SH ON A BOUNDARY,/,27H HISTORY BUFFER FOLLOWS...) @		V02-08H	000673
00552	439*		CALL RBDMP	@ DUMP THIS HISTORY BUFFER	V02-08H	000673
00553	440*	3856	CALL STIAES (I1,IDU)	@ BLACK HOLE TIME	V02-08H	000676
00554	441*		GO TO 221	@	901A3870	000701
00555	442*	3880	IDB=IDMIN	@ BOUNCE OFF THIS BOUNDARY	901A3880	000703
00556	443*		TLEFT=TLEFT+T-TQ	@ TIME TO GO AFTER BOUNCE	901A3890	000704
00557	444*		T=TQ	@ TIME TO BOUNCE	901A3920	000710
00560	445*		GO TO 101	@TRY SHORTER TIME SPAN	90103960	000712
00561	446*	219	CONTINUE	@END TIME SUB-INCREMENT LOOP	90103970	000715
00563	447*		GO TO 6000	@ JOIN NORMAL CLEANUP CODE	V02-08K	000715
00564	448*	4100	CALL TOGSW (PGSBUG,\$4101,\$6000)	@ PRINT ZONE NOT FOUND MSG ?	V02-08K	000717
00565	449*	4101	WRITE (LUOUP,4102,END=6000,ERR=6000) @ YES		V02-08K	000724
00567	450*	4102	FORMAT (44HOCASPER9.MOVELD (BUG) -- FLOW ZONE NOT FOUND,/,27H HISV02-08K			000732
00567	451*		ISTORY BUFFER FOLLOWS...) @		V02-08K	000732
00570	452*		CALL RBDMP	@ DUMP THIS HISTORY BUFFER	V02-08K	000732
00571	453*	6000	DO 220 I=1,3	@ RECORD NEW POSITION AND	V02-08K	000737
00574	454*		CALL STS (I1,I,XL(I))	@ VELOCITY RESULTS IN		000737
00575	455*	220	CALL STS (I1,I+3,UL(I))	@ ASSIGNED SLOTS		000746
00577	456*		CALL STIAES (I1,IFZ)	@ RECORD FINAL FLOW ZONE		000762
00600	457*	221	CONTINUE	@END ELEMENT BY ELEMENT LOOP	90104010	000770
00602	458*		RETURN	@	90104140	000770
00603	459*		SUBROUTINE SPC (Y,Z,TI)	@	V02-08F	001021
00603	460*	C+		@	901A4160	001021
00603	461*	C	LOADS VECTOR Y WITH AEROELEMENT POSITION AT TIME 'TI' RELATIVE		901A4170	001021
00603	462*	C	TO 'XL'. CALCULATES VELOCITY AT Y AND PLACES IT IN Z.		V02-08F	001021
00603	463*	C			V02-08H	001021
00603	464*	C	BEGINNING WITH VERSION V02-08H, SPC ALSO BEGINS A NEW ENTRY IN		V02-08H	001021
00603	465*	C	THE POSITION-HISTORY RING BUFFER.		V02-08H	001021
00603	466*	C-			901A4190	001021
00606	467*		REAL Y(4),Z(3),TI	@	V02-08F	001021
00607	468*		DO 13 N=1,3	@	901A4210	001021
00612	469*		Y(N)=XL(N)+(TI*UL(N))+(0.5*TI*TI*AL(N))		V02-08F	001041
00613	470*		IDUM=IRBX1-1+N	@ FORM INDEX	V02-08H	001050
00614	471*		ARB(IDUM,IRBPT)=Y(N)	@ RECORD POSITION	V02-08I	001053
00615	472*	13	Z(N)=UL(N)+(TI*AL(N))		V02-08F	001057
00617	473*		Y(4)=XL(4)+TI		901A4230	001065
00620	474*		ARB(IRBX4,IRBPT)=Y(4)	@ RECORD TIME	V02-08H	001070
00621	475*		IRB(IRBAI,IRBPT)=I1	@ RECORD AEROELEMENT ID	V02-08H	001072
00622	476*		IRB(IRBIS,IRBPT)=IRBISA	@ SHOW INITIAL VALIDITY	V02-08H	001074
00623	477*		IRBPP=IRBPT	@ RECORD PTR FOR FURTHER USE	V02-08I	001076
00624	478*		IRBPT=IRBPT+1	@ BUMP TO NEXT SLOT SINCE	V02-08H	001100
00625	479*		IF (IRBPT-IRBL) 15,15,14	@ THIS ENTRY IS NOW 'USED'	V02-08H	001102
00630	480*	14	IRBPT=1	@ ALTHOUGH ADDITIONAL INFO	V02-08H	001105
00631	481*	15	CONTINUE	@ MAY BE ADDED LATER	V02-08H	001110
00632	482*		RETURN	@	901A4240	001110
00633	483*		SUBROUTINE YNM (Y)	@	901A5000	001142
00633	484*	C+		@	901A5010	001142
00633	485*	C	1) IDENTIFIES FLOW ZONE OF SPACE-TIME POINT 'Y' AND UPDATES		901A5020	001142
00633	486*	C	FLOW ZONE OF AEROELEMENT 'I1' IF NECESSARY.		901A5030	001142
00633	487*	C	2) CHECKS ALL APPROPRIATE BOUNDARIES TO PRODUCE 'IDMIN'/'SVMIN'.		901A5040	001142
00633	488*	C	DOES NOT CONSIDER FOR 'IDMIN'/'SVMIN' BOUNDARIES THAT ARE		901A5050	001142
00633	489*	C	SAFE BY TRUNCATION.		901A5060	001142
00633	490*	C	3) DISCONTINUES SEARCH IF 'SVMIN' GOES NEGATIVE.		901A5070	001142
00633	491*	C			V02-08H	001142
00633	492*	C	BEGINNING WITH VERSION V02-08H, YNM RECORDS IN THE POSITION-		V02-08H	001142
00633	493*	C	HISTORY RING BUFFER THE FLOW ZONE ID AND THE ID AND SURFACE		V02-08H	001142
00633	494*	C	VALUE OF THE GOVERNING SURFACE.		V02-08H	001142
00633	495*	C			V02-08K	001142
00633	496*	C			V02-08K	001142

Listing 7.—Continued.

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00633 497* C BEGINNING WITH VERSION V02-08K, THIS ROUTINE CHECKS FOR THE V02-08K 001142
00633 498* C FLOW-ZONE-NOT-FOUND ERROR AND REPORTS IT TO THE CALLER BY V02-08K 001142
00633 499* C V02-08K 001142
00633 500* C 1. SETTING THE FLOW ZONE TO THE UNUSED ZONE AND V02-08K 001142
00633 501* C V02-08K 001142
00633 502* C 2. SETTING SVMIN AND IDMIN TO -1. V02-08K 001142
00633 503* C- 901A5080 001142
00636 504* REAL Y(4) 901A5090 001142
00637 505* N=1 @ SET MANDATORY ZONE FIRST V02-08K 001142
00640 506* IDMIN=-1 @ INIT FOR SURFACE VALUE V02-08K 001146
00641 507* SVMIN=1.0E+30 @ MINIMUM SEARCH V02-08K 001150
00642 508* IRB(IRBFI,IRBP,IFZ) @ RECORD ENTERING FLOW ZONE V02-08K 001152
00643 509* IRB(IRBIS,IRBPP)=OR(IRB(IRBIS,IRBPP),IRBISF) @ MARK IT VALID V02-08K 001154
00644 510* CALL TSTZN (Y,IFZ,IFZ) @ CHECK FLOW ZONE ID V02-08K 001157
00645 511* IF (IFZ-1) 29,26,29 @ DID WE FIND A ZONE ? V02-08K 001164
00650 512* 26 IFZ=IDU @ NO, SET HIM UNUSED V02-08K 001167
00651 513* CALL STIAES (I1,IDU) @ HERE, TOO V02-08K 001171
00652 514* SVMIN=-1.0 @ SET IN VIOLATION V02-08K 001175
00653 515* RETURN @ BACK TO CALLER V02-08K 001177
00654 516* 29 IRB(IRBFI,IRBPP)=IFZ @ REVISE ZONE ID IN RING V02-08K 001203
00655 517* NA=IPZBL(N,2) @ NUMBER OF BOUNDARIES IN ZONE V02-08K 001206
00656 518* IF (NA) 42,42,31 @ SKIP NULL TESTS 901A5180 001213
00661 519* 31 NB=IPZBL(N,1) @ POINT TOWARD BOUNDARY ID 901B5190 001215
00662 520* DO 41 NC=1,NA @ DO EACH THIS ZONE 901A5200 001227
00665 521* NB=NB+1 @ POINT TO A BOUNDARY ID 901A5210 001227
00666 522* ID=ZBL(NB) @ PICKUP THE ID 901A5220 001232
00667 523* CALL TSTBDT (Y,ID,SV,IT) @ GO CHECK THIS BOUNDARY 901A5230 001236
00670 524* IF (IT) 37,37,41 @ SKIP MIN IF WE TRUNCATED 901A5240 001244
00673 525* 37 IF (SV-SVMIN) 38,38,41 @ FIND A NEW MIN ? 901A5250 001247
00676 526* 38 SVMIN=SV @ YES, RECORD IT 901A5260 001253
00677 527* IDMIN=ID @ 901A5270 001255
00700 528* IF (SVMIN) 45,45,41 @ GO INTO VIOLATION ? 901A5280 001257
00703 529* 41 CONTINUE @ NO, KEEP CHECKING 901A5290 001264
00705 530* 42 IF (N-IFZ) 43,45,43 @ JUST DO EL'S FLOW ZONE ? 901A5300 001264
00710 531* 43 N=IFZ @ NO, SWITCH TO IT 901A5310 001266
00711 532* GO TO 29 @ GO BACK AND DO IT 901A5320 001270
00712 533* 45 IRB(IRBSI,IRBPP)=IDMIN @ RECORD SURFACE ID V02-08H 001272
00713 534* ARB(IRBSV,IRBPP)=SVMIN @ RECORD SURFACE VALUE V02-08H 001275
00714 535* IRB(IRBIS,IRBPP)=OR(IRB(IRBIS,IRBPP),IRBIS+IRBSV) @ MARK IT V02-08H 001277
00715 536* RETURN @ V02-08H 001302
00716 537* SUBROUTINE RBDMP V02-08H 001326
00716 538* C+ V02-08H 001326
00716 539* C THIS SUBROUTINE DUMPS A SYMBOLIC LISTING OF THE POSITION-HISTORY V02-08H 001326
00716 540* C RING BUFFER TO UNIT LUOUP. V02-08H 001326
00716 541* C- V02-08H 001326
00721 542* I=IRBPP @ POINT TO MOST RECENT ENTRY V02-08H 001326
00722 543* IF (I) 1050,1050,1002 @ SKIP IF NO VALID ENTRIES V02-08H 001330
00725 544* 1002 IF (AND(IRB(IRBIS,I),IRBISA)) 1003,1025,1003 @ THIS ENTRY VALID ? V02-08H 001333
00730 545* 1003 WRITE (LUOUP,1075,END=1050,ERR=1050) IRB(IRBAI,I) @ YES, START V02-08H 001340
00733 546* WRITE (LUOUP,1076,END=1050,ERR=1050) (ARB(J,I),J=IRBX1,IRBX4) @ V02-08H 001357
00741 547* IF (AND(IRB(IRBIS,I),IRBISF),NE.0) WRITE (LUOUP,1077,END=1050,ERR= V02-08H 001375
00741 548* 11050) IRB(IRBFI,I) @ FLOW ZONE ID V02-08H 001375
00745 549* IF (AND(IRB(IRBIS,I),IRBIS),NE.0) WRITE (LUOUP,1078,END=1050,ERR=V02-08J 001412
00745 550* 11050) IRB(IRBSI,I) @ SURFACE ID V02-08H 001412
00751 551* IF (AND(IRB(IRBIS,I),IRBSV),NE.0) WRITE (LUOUP,1079,END=1050,ERR=V02-08H 001427
00751 552* 11050) ARB(IRBSV,I) @ SURFACE VALUE V02-08H 001427
00755 553* IF (AND(IRB(IRBIS,I),IRBISG),NE.0) WRITE (LUOUP,1080,END=1050,ERR=V02-08H 001444
00755 554* 11050) (ARB(J,I),J=IRBG1,IRBG3) @ GRADIENT V02-08H 001444
00764 555* 1025 I=I-1 @ NEXT OLDEST ENTRY V02-08H 001467
00765 556* IF (I) 1027,1027,1028 @ TIME TO WRAP AROUND ? V02-08H 001471
00770 557* 1027 I=IRBL @ YES V02-08H 001473
00771 558* 1028 IF (I-IRBPP) 1002,1050,1002 @ DONE IF BACK AT START V02-08H 001476
00774 559* 1050 RETURN @ V02-08H 001501
00775 560* 1075 FORMAT (1H0,6X,18HAEROELEMENT ID =,I13) @ 001523
00776 561* 1076 FORMAT (1H,6X,18HPOSITION =,I,4(E13.7,2X)) @ 001523
00777 562* 1077 FORMAT (1H,6X,18HFLOW ZONE ID =,I13) @ 001523
01000 563* 1078 FORMAT (1H,6X,18HSURFACE ID =,I13) @ 001523
01001 564* 1079 FORMAT (1H,6X,18HSURFACE VALUE =,IPE13.7) @ 001523
01002 565* 1080 FORMAT (1H,6X,18HGRADIENT =,I,3(E13.7,2X)) @ 001523
01003 566* END 901A9990 001523
END FOR
>

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Listing 7.—Concluded.

@FOR,MS CASPER9,SURFD
 FOR 4R1 E -04/13/84-15:22:44 (5,)
 >@EOF.

SUBROUTINE SURF ENTRY POINT 000731
 SURFTR ENTRY POINT 000747
 GRAD ENTRY POINT 000765
 SURFTI ENTRY POINT 001002
 SURFVE ENTRY POINT 001020
 SURFAC ENTRY POINT 001035

STORAGE USED: CODE(1) 001052; DATA(0) 000124; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IVSIZC 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 IBDZN
 0005 BDZN
 0006 IPBDZN
 0007 SPOPI
 0010 SPSHI
 0011 SPSHR
 0012 ADDR
 0013 SPOPR
 0014 ADR
 0015 CALSER
 0016 NERR2\$
 0017 NERR4\$
 0020 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000004	1002L	0001	000015	1010L	0001	000036	1035L	0001	000101	1101L	0001	000161	1111L					
0001	000235	1121L	0001	000261	1127L	0001	000271	1128L	0001	000275	1130L	0001	000311	1132L					
0001	000331	1135L	0001	000335	1140L	0001	000350	1144L	0001	000360	1145L	0001	000370	1146L					
0001	000412	1150L	0001	000416	1153L	0001	000427	1160L	0001	000450	1166L	0001	000517	1190L					
0001	000525	1201L	0001	000573	1218L	0001	000613	1220L	0001	000626	1222L	0001	000636	1223L					
0001	000042	1516	0001	000141	2146	0001	000463	3276	0001	000620	3566	0001	000651	3666					
0005	R	000000	BDZN	0000	R	000001	GR	0004	I	000000	IBDZN	0000	I	000101	IDUM11	0000	I	000103	IDUM12
0000	I	000073	INHIB	0000		000112	INJP\$	0000	I	000070	IP	0006	I	000000	IPBDZN	0000	I	000076	IPN
0000	I	000104	IPOS	0000	I	000077	IPT	0000	I	000071	IPTH	0000	I	000074	ISW	0000	I	000004	IV
0003	I	000000	IVSIZE	0000	I	000100	MDE	0000	I	000075	NRTN	0000	I	000102	NV	0000	R	000072	RIDCH
0000	R	000000	SV	0000	I	000067	THMDE	0000	I	000066	TRCNT								

00101	1*		SUBROUTINE SURF (XL,ID,SF,\$)			91880010	000000
00101	2*	C				91800020	000000
00101	3*	C				91800030	000000
00101	4*	C	SURF	***** A SUBROUTINE FOR CASPER *****		91800040	000000
00101	5*	C		AUTHOR WILLIAM HENRY JONES		91800050	000000
00101	6*	C		V03-00 19 APR 78		91800060	000000
00101	7*	C		V03-01 15 JUN 78		91810061	000000
00101	8*	C		V03-02 16 JUN 78		91820062	000000
00101	9*	C		V03-03 22 JUN 78		91830063	000000
00101	10*	C		V03-04 26 JUN 78		91840064	000000
00101	11*	C		V03-05 28 JUN 78		91850065	000000
00101	12*	C		V03-06 29 JUN 78		91860066	000000
00101	13*	C		V03-07 19 JUL 78		91870067	000000
00101	14*	C		V03-08 30 AUG 78		91880068	000000
00101	15*	C		V03-08A 27 OCT 80	NEW STACK ENTRY POINTS		000000
00101	16*	C		V03-08B 23 FEB 81	APPLY DC TO CALC QTY ONLY		000000
00101	17*	C		V03-08C 28 SEP 81	ADD SURFACE VELOCITIES	V03-08C	000000
00101	18*	C		V03-08D 23 APR 82	TRUNCATIONS OF TRUNCATIONS	V03-08D	000000

Listing 8.—Subroutine SURF.


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00101 19* C          V03-08E  05 AUG 83  ADD SURFACE ACCELERATIONS V03-08E  000000
00101 20* C          91800070  000000
00101 21* C          91800080  000000
00101 22* C          91800090  000000
00101 23* C ARGUMENTS PASSED IN SUBROUTINE CALL ***** 91880094  000000
00101 24* C          91880096  000000
00101 25* C ARGUMENT  TYPE      DIMENSION  DESCRIPTION  91800100  000000
00101 26* C -----  -----  -----  -----  91800110  000000
00101 27* C XL      REAL      1 TO 4      3 POSITION COORDS AND TIME 91800120  000000
00101 28* C          91800130  000000
00101 29* C ID      INTEGER   SCALAR     BOUNDARY OR FLOW ZONE 91800140  000000
00101 30* C          IDENTIFICATION NUMBER 91800150  000000
00101 31* C          91800260  000000
00101 32* C SF      REAL      SCALAR     CALCULATED SURFACE VALUE 91800270  000000
00101 33* C          91800280  000000
00101 34* C $4      N/A      RETURN LINK  TAKEN IF TRUNCATION OCCURRED 91880290  000000
00101 35* C          91800300  000000
00101 36* C GF      REAL      1 TO 3      GRADIENT, REPLACES SF IN 91800310  000000
00101 37* C          SECOND ENTRY POINT 91800320  000000
00101 38* C          91880330  000000
00101 39* C ARGUMENTS IN CASPER 'CACHE' MEMORY ***** 91880332  000000
00101 40* C          91880334  000000
00101 41* C ARGUMENT  TYPE      DIMENSION  DESCRIPTION  91880336  000000
00101 42* C -----  -----  -----  -----  91880338  000000
00101 43* C BDZN     REAL      1 TO BDZNSZ SURFACE EVALUATION ROUTINE 91880340  000000
00101 44* C          PARAMETERS LIST 91880342  000000
00101 45* C          91880344  000000
00101 46* C IBDZN    INTEGER   1 TO BDZNSZ SURFACE EVALUATION ROUTINE 91880346  000000
00101 47* C          PARAMETERS (CONTROL) LIST 91880348  000000
00101 48* C          91880350  000000
00101 49* C IPBDZN   INTEGER   1 TO NBDZN  BDZN CONTROL POINTERS LIST 91880352  000000
00101 50* C          (ID) = SDH POINTER 91880354  000000
00101 51* C          91880356  000000
00101 52* C          91880358  000000
00101 53* C          91880360  000000
00101 54* C DESCRIPTION ***** 91880362  000000
00101 55* C          91800370  000000
00101 56* C SURF HANDLES THE EVALUATION OF ALL BOUNDARIES AND TRUNCATION 91800380  000000
00101 57* C SURFACES. IT PROVIDES ALL NECESSARY LOGIC TO HANDLE TRUNCATION 91800390  000000
00101 58* C SURFACES, FIND SURFACE EVALUATION ROUTINE PARAMETER LISTS, 91800400  000000
00101 59* C AND VECTOR CONTROL TO PROPER SURFACE EVALUATION ROUTINES. 91800410  000000
00101 60* C          91800420  000000
00101 61* C ***** BDZN DATA BASE ***** 91800430  000000
00101 62* C          91800440  000000
00101 63* C SURFACE DEFINITION HEADER ***** 91800450  000000
00101 64* C          91800460  000000
00101 65* C EACH BOUNDARY AND FLOW ZONE IN CASPER IS DEFINED BY MEANS OF A 91800470  000000
00101 66* C SERIES OF NUMBERS IN THE CONTROL LIST 'BDZN'. A POINTER 91800480  000000
00101 67* C TO THESE NUMBERS CAN BE OBTAINED FROM 'IPBDZN(N)' WHERE 'N' IS 91800490  000000
00101 68* C THE ID NUMBER OF THE DESIRED BOUNDARY OR FLOW ZONE. WHAT IS 91800500  000000
00101 69* C OBTAINED IS A POINTER TO A SURFACE DEFINITION HEADER, 'SDH'. 91800510  000000
00101 70* C THE POINTER IS REFERRED TO AS 'IP'. THE HEADER APPEARS AS 91800520  000000
00101 71* C FOLLOWS. 91800530  000000
00101 72* C          91800540  000000
00101 73* C IP-5      SURFACE TYPE NUMBER 91800550  000000
00101 74* C IP-4      SURFACE PARAMETER LOCATION CONTROL (SPLC) 91800560  000000
00101 75* C IP-3      TRUNCATION HEADER LOCATION CONTROL (THLC) 91800570  000000
00101 76* C IP-2      DEFEND/CONTAIN SURFACE VALUE 91800580  000000
00101 77* C IP-1      NUMBER OF TRUNCATION HEADERS 91800590  000000
00101 78* C IP        NUMBER OF PARAMETERS FOLLOWING THIS HEADER 91800600  000000
00101 79* C          91800610  000000
00101 80* C          91800620  000000
00101 81* C SURFACE PARAMETER LOCATION CONTROL (SPLC) ***** 91800630  000000
00101 82* C          91800640  000000
00101 83* C THIS NUMBER PROVIDES THE METHOD FOR CALCULATING THE POINTER(S) 91800650  000000
00101 84* C TO THE ACTUAL NUMBERS WHICH ARE USED FOR CALCULATING THE SURFACE 91800660  000000
00101 85* C VALUE. THE METHODS ARE AS FOLLOWS. 91800670  000000
00101 86* C          91800680  000000
00101 87* C MODE      METHOD 91800690  000000
00101 88* C -----  ----- 91800700  000000
00101 89* C 1         IV = IP+1 91800710  000000
00101 90* C 2         IV = IBDZN(IP+1) 91800720  000000

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Listing 8.—Continued.

00101	91*	C	3	IV = IBDZN(IBDZN(IP+1))	91800730	000000
00101	92*	C	4	IV = IP+IBDZN(IP+1)	91800740	000000
00101	93*	C	5	IV = IBDZN(IP+IBDZN(IP+1))	91800750	000000
00101	94*	C	6	IV = IBDZN(IBDZN(IP+1)+IBDZN(IP+2))	91800760	000000
00101	95*	C	7	IV = IBDZN(IBDZN(IP+1)+IBDZN(IP+2)+IBDZN(IP+3))	91800770	000000
00101	96*	C	8	IV = IBDZN(IBDZN(IP+1)+IBDZN(IP+2)+IBDZN(2+ IOFSET))	91800780	000000
00101	97*	C			91800790	000000
00101	98*	C	9	IV = IBDZN(IBDZN(IP+1)+IBDZN(IP+2)+IBDZN(IBDZN (IP+3)+IBDZN(3+IOFSET)))	91800800	000000
00101	99*	C			91800810	000000
00101	100*	C	10	MULTIPLE MODES - FORMAT AS FOLLOWS	91800820	000000
00101	101*	C			91800830	000000
00101	102*	C		IP -> TOTAL NUMBER OF PARAMETERS FOLLOWING THIS	91800840	000000
00101	103*	C		SURFACE DEFINITION HEADER	91800850	000000
00101	104*	C		NUMBER OF ADDRESSING MODES TO BE EVALUATED	91800860	000000
00101	105*	C		FIRST SPLC	91800870	000000
00101	106*	C		(IPE 1 ->) NUMBER OF PARAMETERS FOLLOWING THIS ENTRY	91800880	000000
00101	107*	C		PARAMETER	91800890	000000
00101	108*	C		PARAMETER	91800900	000000
00101	109*	C		PARAMETER	91800910	000000
00101	110*	C		...	91800920	000000
00101	111*	C		SECOND SPLC	91800930	000000
00101	112*	C		(IPE 2 ->) NUMBER OF PARAMETERS FOLLOWING THIS ENTRY	91800940	000000
00101	113*	C		PARAMETER	91800950	000000
00101	114*	C		PARAMETER	91800960	000000
00101	115*	C		PARAMETER	91800970	000000
00101	116*	C		...	91800980	000000
00101	117*	C		...	91800990	000000
00101	118*	C		N TH SPLC	91801000	000000
00101	119*	C		(IPE N ->) NUMBER OF PARAMETERS FOLLOWING THIS ENTRY	91801010	000000
00101	120*	C		PARAMETER	91801020	000000
00101	121*	C		PARAMETER	91801030	000000
00101	122*	C		PARAMETER	91801040	000000
00101	123*	C		91801050	000000
00101	124*	C			91801060	000000
00101	125*	C		NOTE THAT THE POINTERS GENERATED POINT TO THE ACTUAL LOCATION	91801070	000000
00101	126*	C		IN BDZN OF THE FIRST PARAMETER OF ANY LIST (OR SET OF LISTS), NOT	91801080	000000
00101	127*	C		THE LOCATION BEFORE IT AS IN PREVIOUS INCARNATIONS. THUS, THE	91801090	000000
00101	128*	C		FIRST PARAMETER IS #0, NOT #1 .	91801100	000000
00101	129*	C			91801110	000000
00101	130*	C		SINCE ALL SURFACE EVALUATION ROUTINES MAY DIVIDE THE COMPLETE	91801120	000000
00101	131*	C		PARAMETER SET INTO DIFFERENT LISTS IN DIFFERENT WAYS, THE	91801130	000000
00101	132*	C		RESPONSIBILITY FOR CORRECTING POINTERS LIES WITH THESE ROUTINES.	91801140	000000
00101	133*	C		AFTER ONE OF THESE ROUTINES IS CALLED IT MUST BE ASSUMED THAT	91801150	000000
00101	134*	C		THE SUPPLIED POINTERS HAVE BEEN SO ALTERED.	91801160	000000
00101	135*	C			91801170	000000
00101	136*	C		WHEN FEWER INDEPENDENT ADDRESSING POINTERS THAN PARAMETER LISTS	91801180	000000
00101	137*	C		TO BE LOCATED ARE SUPPLIED THE UN-LOCATED LISTS ARE ASSUMED	91801190	000000
00101	138*	C		TO FOLLOW THE LAST LOCATED LIST CONTIGUOUSLY IN BDZN AND THE	91801200	000000
00101	139*	C		ASSOCIATED DEPENDENT POINTERS ARE CORRECTED ACCORDINGLY.	91801210	000000
00101	140*	C			91801220	000000
00101	141*	C			91801230	000000
00101	142*	C		TRUNCATION HEADER LOCATION CONTROL (THLC) *****	91801240	000000
00101	143*	C			91801250	000000
00101	144*	C		THIS PARAMETER SPECIFIES THE METHOD OF LOCATING THE APPROPRIATE	91801260	000000
00101	145*	C		TRUNCATION HEADERS. A TRUNCATION POINTER, 'IPT', SIMILAR TO THE	91801270	000000
00101	146*	C		SURFACE PARAMETER POINTER, 'IP', IS DEFINED AS	91801280	000000
00101	147*	C			91801290	000000
00101	148*	C		IPT = IP + 1 + IBDZN(IP) .	91801300	000000
00101	149*	C			91801310	000000
00101	150*	C		IT CAN BE SEEN THAT IBDZN(IP) CONTAINS THE NUMBER OF PARAMETERS	91801320	000000
00101	151*	C		FOLLOWING THE SURFACE DEFINITION HEADER THAT ARE ASSOCIATED WITH	91801330	000000
00101	152*	C		THE DESCRIPTION OF THE SURFACE - NOT WITH ITS TRUNCATION.	91801340	000000
00101	153*	C			91801350	000000
00101	154*	C		THE ADDRESSING MODES USED TO LOCATE TRUNCATION HEADERS ARE	91801360	000000
00101	155*	C		IDENTICAL TO THOSE USED FOR SURFACE PARAMETER LOCATION	91801370	000000
00101	156*	C		EXCEPT THAT ABSOLUTE LOCATIONS 2 AND 3 ARE REPLACED BY	91801380	000000
00101	157*	C		ABSOLUTE LOCATIONS 4 AND 5, RESPECTIVELY.	91801390	000000
00101	158*	C			91801400	000000
00101	159*	C		IBDZN(IPT) CONTAINS THE NUMBER OF PARAMETERS FOLLOWING THE 'IPT'	91801410	000000
00101	160*	C		LOCATION THAT ARE ASSOCIATED WITH THE SURFACE DEFINITION	91801420	000000
00101	161*	C		TRUNCATION. ASSUMING THAT TWO COMPLETE SURFACE DEFINITION	91801430	000000
00101	162*	C		HEADERS OCCUPY CONTIGUOUS AREAS IN BDZN/IBDZN, THE POINTER TO	91801440	000000

Listing 8.—Continued.

00101	163*	C	THE SECOND, 'IP2', CAN BE FOUND AS FOLLOWS BASED ON THE POINTER	91801450	000000
00101	164*	C	TO THE FIRST, 'IP1'.	91801460	000000
00101	165*	C		91801470	000000
00101	166*	C	IP1 = IP1 + 1 + IBDZN(IP1)	91801480	000000
00101	167*	C	IP2 = IPT1 + 6 + IBDZN(IPT1)	91801490	000000
00101	168*	C		V03-08D	000000
00101	169*	C		V03-08D	000000
00101	170*	C	TRUNCATION RECURSION *****	V03-08D	000000
00101	171*	C		V03-08D	000000
00101	172*	C	THE TRUNCATION PROCESS IS RECURSIVE. IF A TRUNCATION IS, ITSELF,	V03-08D	000000
00101	173*	C	TRUNCATED, IT NO LONGER HAS ANY EFFECT UPON ITS PARENT SURFACE.	V03-08D	000000
00101	174*	C	IF THE PARENT SURFACE IS A TRUNCATION SURFACE, IT MUST STILL BE	V03-08D	000000
00101	175*	C	EVALUATED AND MAY TRUNCATE ITS PARENT.	V03-08D	000000
00101	176*	C		V03-08D	000000
00101	177*	C	USING THIS MECHANISM, TRUNCATION SURFACES MAY BE BUILT BY THE	V03-08D	000000
00101	178*	C	CONCATENATION OF INDIVIDUAL SURFACES.	V03-08D	000000
00101	179*	C		91801500	000000
00101	180*	C		91801510	000000
00101	181*	C		91801520	000000
00101	182*	C	TRUNCATION HEADER *****	91801530	000000
00101	183*	C		91801540	000000
00101	184*	C	TRUNCATION HEADERS PROVIDE THE INFORMATION NECESSARY TO LOCATE	91801550	000000
00101	185*	C	AND MODIFY (AS APPROPRIATE) THE SURFACE DEFINITION HEADER FOR AN	91801560	000000
00101	186*	C	INDIVIDUAL TRUNCATION SURFACE. ONE TRUNCATION HEADER MUST BE	91801570	000000
00101	187*	C	SUPPLIED FOR EACH TRUNCATION LISTED BY THE PARENT SURFACE	91801580	000000
00101	188*	C	DEFINITION HEADER. IF THE SUPPLIED ADDRESSING INFORMATION	91801590	000000
00101	189*	C	DOES NOT GIVE ENOUGH INDEPENDENT POINTERS TO TRUNCATION HEADERS	91801600	000000
00101	190*	C	THE AVAILABLE N POINTERS ARE ASSUMED TO POINT TO THE FIRST	91801610	000000
00101	191*	C	N TRUNCATION HEADERS AND THE REMAINING TRUNCATION HEADERS	91801620	000000
00101	192*	C	ARE ASSUMED TO FOLLOW CONSECUTIVELY AFTER THE N TH HEADER.	91801630	000000
00101	193*	C		91801640	000000
00101	194*	C	MODIFICATION OF THE TRUNCATION SURFACE'S SURFACE DEFINITION	91801650	000000
00101	195*	C	HEADER CONSISTS SOLELY OF AN ADDITIONAL DEFEND/CONTAIN	91801660	000000
00101	196*	C	MODIFIER TO FLOP POSITIVE AND NEGATIVE SIDES OF THE SURFACE	91801670	000000
00101	197*	C	USED. THUS, ANY DEFINED SURFACE CAN BE REUSED ANY NUMBER	91801680	000000
00101	198*	C	OF TIMES TO TRUNCATE OTHER SURFACES.	91801690	000000
00101	199*	C		91801700	000000
00101	200*	C	A POINTER, 'IPTH', TO THE FIRST WORD OF THE TRUNCATION HEADER	91801710	000000
00101	201*	C	IS ASSUMED. THE TRUNCATION HEADER FORMAT IS AS FOLLOWS	91801720	000000
00101	202*	C		91801730	000000
00101	203*	C	POSITION REMARKS	91801740	000000
00101	204*	C	-----	91801750	000000
00101	205*	C	IPTH MODE NUMBER	91801760	000000
00101	206*	C	IPTH+1 DEFEND/CONTAIN MODIFIER	91801770	000000
00101	207*	C	IPTH+2 ADDITIONAL PARAMETER(S)	91801780	000000
00101	208*	C		91801790	000000
00101	209*	C	THREE MODES ARE DEFINED	91801800	000000
00101	210*	C		91801810	000000
00101	211*	C	MODE SDH LOCATION	91801820	000000
00101	212*	C	-----	91801830	000000
00101	213*	C	1 IP = IPTH + 8 -- COMPLETE SURFACE DEFINITION HEADER	91801840	000000
00101	214*	C	WITH ALL APPROPRIATE PARAMETERS AND TRUNCATION	91801850	000000
00101	215*	C	INFORMATION FOLLOWS IMMEDIATELY.	91801860	000000
00101	216*	C		91801870	000000
00101	217*	C	2 IP = IPBDZN(IBDZN(IPTH+2)) -- THE IDENTIFICATION	91801880	000000
00101	218*	C	NUMBER OF THE SURFACE IS IN IPTH+2. THIS IS	91801890	000000
00101	219*	C	A SURFACE EXTERNALLY DEFINED IN THE BOUNDARY	91801900	000000
00101	220*	C	AND FLOW ZONE POINTERS LIST, 'IPBDZN'.	91801910	000000
00101	221*	C		91801920	000000
00101	222*	C	3 IP = IBDZN(IBDZN(1)+IBDZN(IPTH+2)) -- THE	91801930	000000
00101	223*	C	IDENTIFICATION NUMBER OF THE SURFACE IS IN	91801940	000000
00101	224*	C	IPTH+2. THIS IS A SURFACE INTERNALLY DEFINED	91801950	000000
00101	225*	C	IN RDZN/IBDZN. A TABLE OF POINTERS TO THE	91801960	000000
00101	226*	C	SURFACE DEFINITION HEADERS FOR THESE SURFACES	91801970	000000
00101	227*	C	IS POINTED TO BY IBDZN(1). EXCEPT FOR THE	91801980	000000
00101	228*	C	INTERNAL/EXTERNAL DEFINITION DIFFERENCE, ALL	91801990	000000
00101	229*	C	OTHER FEATURES OF THE EXTERNALLY DEFINED SURFACE	91802000	000000
00101	230*	C	ARE AVAILABLE TO THE INTERNALLY DEFINED SURFACE.	91802010	000000
00101	231*	C		91802020	000000
00101	232*	C	NOTE -- IF THE MODE NUMBER IS NEGATIVE SUBTRUNCATIONS OF THE	91832022	000000
00101	233*	C	CITED TRUNCATION SURFACE ARE INHIBITED.	91832023	000000
00101	234*	C		91802030	000000

00101	235*	C				91802040	000000
00101	236*	C				91802050	000000
00101	237*	C				91802060	000000
00101	238*	C				91802070	000000
00101	239*	C			AS INFERRED PREVIOUSLY A NUMBER OF WORDS IN BDNZ ARE RESERVED	91802080	000000
00101	240*	C			FOR USE BY THE ADDRESSING MODE INTERPRETER, THEY ARE AS	91802090	000000
00101	241*	C			FOLLOWS --	91802100	000000
00101	242*	C	WORD	USE		91802110	000000
00101	243*	C	-----	-----		91802120	000000
00101	244*	C	1	POINTER TO BASE OF INTERNALLY IDENTIFIED SURFACE		91802130	000000
00101	245*	C		SDH POINTERS TABLE,		91802140	000000
00101	246*	C	2	POINTER TO THE TABLE OF BOUNDARY AND FLOW ZONE		91802150	000000
00101	247*	C		SURFACE TABLES,		91802160	000000
00101	248*	C	3	BELIEVE IT OR NOT, THIS IS A POINTER TO A TABLE		91802170	000000
00101	249*	C		TABLE TABLE. THIS PROVIDES A CROSS INDEXING		91802180	000000
00101	250*	C		FEATURE BETWEEN TYPES OF SURFACE. FOR INSTANCE,		91802190	000000
00101	251*	C		A SETUP USING THIS FEATURE COULD SWITCH A PROBLEM		91802200	000000
00101	252*	C		BETWEEN STATIC AND DYNAMIC BOUNDARIES OF IDENTICAL		91882210	000000
00101	253*	C		TYPES BY SIMPLY REWRITING THE TABLE TABLE.		91802220	000000
00101	254*	C		OF COURSE, YOU WOULD GO CRAZY...		91802230	000000
00101	255*	C	4 AND 5	AS 2 AND 3, RESPECTIVELY, BUT USED WHEN SEEKING		91802240	000000
00101	256*	C		TRUNCATION HEADERS,		91802250	000000
00101	257*	C				91802260	000000
00101	258*	C				91802270	000000
00101	259*	C				91802280	000000
00101	260*	C		EXAMPLE *****		91802290	000000
00101	261*	C				91802300	000000
00101	262*	C		THE FOLLOWING EXAMPLE SHOWS HOW THE FOREGOING CONVENTIONS MAY		91802310	000000
00101	263*	C		BE APPLIED TO EFFECTIVELY DESCRIBE THE ROTATING BLADES OF A		91802320	000000
00101	264*	C		TURBOJET FAN MODULE. IT IS ASSUMED THAT ALL THESE BLADES CAN		91802330	000000
00101	265*	C		BE DESCRIBED BY A SINGLE SURFACE EVALUATION ROUTINE. THIS		91802340	000000
00101	266*	C		EXAMPLE ALSO ASSUMES THAT OTHER ELEMENTS OF SUCH A FAN MODULE		91802350	000000
00101	267*	C		ARE ALSO BEING DESCRIBED AT THAT SAME TIME.		91802360	000000
00101	268*	C				91802370	000000
00101	269*	C		SURFACE EVALUATION ROUTINE *****		91802380	000000
00101	270*	C				91802390	000000
00101	271*	C		THE GENERALIZED ROUTINE WHICH SPECIFIES THE BLADES IS ASSUMED		91802400	000000
00101	272*	C		TO REQUIRE A PARAMETER LIST AS FOLLOWS --		91802410	000000
00101	273*	C				91802420	000000
00101	274*	C	REF LOC	SEG NO	REMARKS	91802430	000000
00101	275*	C	-----	-----	-----	91802440	000000
00101	276*	C	0	1	THESE 13 PARAMETERS SPECIFY A COORDINATE	91802450	000000
00101	277*	C	1	1	TRANSFORMATION AS A FUNCTION OF TIME.	91802460	000000
00101	278*	C	2	1	THEY ARE USED TO DETERMINE DISK/BLADE	91802470	000000
00101	279*	C	3	1	LOCATION AT ANY TIME.	91802480	000000
00101	280*	C	4	1		91802490	000000
00101	281*	C	5	1		91802500	000000
00101	282*	C	6	1		91802510	000000
00101	283*	C	7	1		91802520	000000
00101	284*	C	8	1		91802530	000000
00101	285*	C	9	1		91802540	000000
00101	286*	C	10	1		91802550	000000
00101	287*	C	11	1		91802560	000000
00101	288*	C	12	1		91802570	000000
00101	289*	C	13	2	ENGINE 'SPEED' PARAMETER	91802580	000000
00101	290*	C	14	3	THESE 12 PARAMETERS SPECIFY A COORDINATE	91802590	000000
00101	291*	C	15	3	TRANSFORMATION TO LOCATE THE BLADE	91802600	000000
00101	292*	C	16	3	ON THE DISK GIVEN THE RADIUS OF THE	91802610	000000
00101	293*	C	17	3	DISK AND THE BLADE NUMBER	91802620	000000
00101	294*	C	18	3		91802630	000000
00101	295*	C	19	3		91802640	000000
00101	296*	C	20	3		91802650	000000
00101	297*	C	21	3		91802660	000000
00101	298*	C	22	3		91802670	000000
00101	299*	C	23	3		91802680	000000
00101	300*	C	24	3		91802690	000000
00101	301*	C	25	3		91802700	000000
00101	302*	C	26	4	RADIUS OF DISK	91802710	000000
00101	303*	C	27	5	BLADE NUMBER ON DISK	91802720	000000
00101	304*	C	28	6	THE PARAMETERS OF GROUP 6 SPECIFY A	91802730	000000
00101	305*	C	29	6	BASIC AIRFOIL CHORDWISE THICKNESS	91802740	000000
00101	306*	C	30	6	DISTRIBUTION	91802750	000000

Listing 8.—Continued.

00101	307*	C	31	6		91802760	000000
00101	308*	C	32	6		91802770	000000
00101	309*	C	33	6		91802780	000000
00101	310*	C	34	6		91802790	000000
00101	311*	C	35	6		91802800	000000
00101	312*	C	36	6		91802810	000000
00101	313*	C	37	6		91802820	000000
00101	314*	C	38	6		91802830	000000
00101	315*	C	39	7	THE PARAMETERS OF GROUP 7 SPECIFY A	91802840	000000
00101	316*	C	40	7	RADIAL MODIFICATION OF CHORDWISE	91802850	000000
00101	317*	C	41	7	THICKNESS DISTRIBUTION	91802860	000000
00101	318*	C	42	7		91802870	000000
00101	319*	C	43	7		91802880	000000
00101	320*	C	44	7		91802890	000000
00101	321*	C	45	7		91802900	000000
00101	322*	C	46	7		91802910	000000
00101	323*	C	47	8	THE PARAMETERS OF GROUP 8 SPECIFY A	91802920	000000
00101	324*	C	48	8	RADIAL DISTRIBUTION OF THICKNESS	91802930	000000
00101	325*	C	49	8		91802940	000000
00101	326*	C	50	8		91802950	000000
00101	327*	C	51	8		91802960	000000
00101	328*	C	52	8		91802970	000000
00101	329*	C	53	9	THE PARAMETERS OF GROUP 9 SPECIFY A	91802980	000000
00101	330*	C	54	9	CAMBER FOR THE BLADE	91802990	000000
00101	331*	C	55	9		91803000	000000
00101	332*	C	56	9		91803010	000000
00101	333*	C	57	9		91803020	000000
00101	334*	C	58	9		91803030	000000
00101	335*	C	59	10	THE PARAMETERS OF GROUP 10 SPECIFY	91803040	000000
00101	336*	C	60	10	THE RADIAL STACKING OF THE BLADE	91803050	000000
00101	337*	C	61	10		91803060	000000
00101	338*	C	62	10		91803070	000000
00101	339*	C	63	10		91803080	000000
00101	340*	C	64	10		91803090	000000
00101	341*	C	65	10		91803100	000000
00101	342*	C	66	10		91803110	000000
00101	343*	C	67	10		91803120	000000
00101	344*	C	68	10		91803130	000000
00101	345*	C	69	10		91803140	000000
00101	346*	C	70	10		91803150	000000
00101	347*	C				91803160	000000
00101	348*	C			BDZN/IBDZN LIST *****	91803170	000000
00101	349*	C				91803180	000000
00101	350*	C	LOCATION	VALUE	REMARKS	91803190	000000
00101	351*	C	-----	-----	-----	91803200	000000
00101	352*	C	1			91803210	000000
00101	353*	C	2	TT	POINTER TO TABLE TABLE	91803220	000000
00101	354*	C	3			91803230	000000
00101	355*	C	4			91803240	000000
00101	356*	C	5			91803250	000000
00101	357*	C	...			91803260	000000
00101	358*	C	TT	T0	ROTOR ORIENTATIONS TABLE POINTER	91803270	000000
00101	359*	C	TT+1	T1	ROTOR SPEEDS TABLE POINTER	91803280	000000
00101	360*	C	TT+2	T2	BLADE ORIENTATIONS TABLE POINTER	91803290	000000
00101	361*	C	TT+3	T3	BLADE NUMBER TABLE POINTER	91803300	000000
00101	362*	C	TT+4	T4	BLADE MECHANICAL DESCRIPTION TABLE POINTER	91803310	000000
00101	363*	C	TT+5	T5	OTHER TABLE POINTERS	91803320	000000
00101	364*	C	TT+6	T6	'	91803330	000000
00101	365*	C	TT+7	T7	'	91803340	000000
00101	366*	C	...			91803350	000000
00101	367*	C	T0	LOWR	POINTER TO LOW ROTOR ORIENTATION	91803360	000000
00101	368*	C	T0+1	HIGHR	POINTER TO HIGH ROTOR ORIENTATION	91803370	000000
00101	369*	C	...			91803380	000000
00101	370*	C	T1	N1	POINTER TO LOW ROTOR SPEED	91803390	000000
00101	371*	C	T1+1	N2	POINTER TO HIGH ROTOR SPEED	91803400	000000
00101	372*	C	...			91803410	000000
00101	373*	C	T2	BD11	POINTER TO ORIENTER OF BLADES - FAN DISK	91803420	000000
00101	374*	C	T2+1	BD21	FAN DISK 2	91803430	000000
00101	375*	C	T2+2	BD31	FAN DISK 3	91803440	000000
00101	376*	C	T2+3	BD12	CORE DISK 1	91803450	000000
00101	377*	C	T2+4	BD22	CORE DISK 2	91803460	000000
00101	378*	C	T2+5	BD32	CORE DISK 3	91803470	000000

Listing 8.—Continued.

00101	379*	C	T2+6	BD42	CORE DISK 4	91803480	000000
00101	380*	C	T2+7	BD52	CORE DISK 5	91803490	000000
00101	381*	C	T2+8	BD62	CORE DISK 6	91803500	000000
00101	382*	C	...			91803510	000000
00101	383*	C	T3	B1	POINTERS TO BLADE NUMBERS (LARGEST	91803520	000000
00101	384*	C	T3+1	B2	NUMBER OF BLADES ON ANY DISK THIS	91803530	000000
00101	385*	C	T3+2	B3	EXAMPLE IS 120).	91803540	000000
00101	386*	C	T3+3	B4		91803550	000000
00101	387*	C	T3+4	B5		91803560	000000
00101	388*	C		91803570	000000
00101	389*	C	T3+119	B120		91803580	000000
00101	390*	C	...			91803590	000000
00101	391*	C	T4	FB1	POINTERS TO FAN BLADE (FB) AND CORE	91803600	000000
00101	392*	C	T4+1	FB2	BLADE (CB) MECHANICAL DESCRIPTIONS	91803610	000000
00101	393*	C	T4+2	FB3	FOR EACH ROTOR. (THESE POINT TO	91803620	000000
00101	394*	C	T4+3	CB1	PARAMETERS 28 TO 70 OF THE BLADE	91803630	000000
00101	395*	C	T4+4	CB2	SURFACE EVALUATION ROUTINE).	91803640	000000
00101	396*	C	T4+5	CB3		91803650	000000
00101	397*	C	T4+6	CB4		91803660	000000
00101	398*	C	T4+7	CB5		91803670	000000
00101	399*	C	T4+8	CB6		91803680	000000
00101	400*	C	...			91803690	000000
00101	401*	C	LOWOR	XXX	GROUP 1 PARAMETERS FOR BLADES OF	91803700	000000
00101	402*	C	LOWOR+1	XXX	THE LOW ROTOR	91803710	000000
00101	403*	C	LOWOR+2	XXX		91803720	000000
00101	404*	C	LOWOR+3	XXX		91803730	000000
00101	405*	C		91803740	000000
00101	406*	C	LOWOR+12	XXX		91803750	000000
00101	407*	C	...			91803760	000000
00101	408*	C	HIGHOR	XXX	GROUP 1 PARAMETERS FOR BLADES OF THE HIGH	91803770	000000
00101	409*	C	HIGHOR+1	XXX	ROTOR	91803780	000000
00101	410*	C	HIGHOR+2	XXX		91803790	000000
00101	411*	C	HIGHOR+3	XXX		91803800	000000
00101	412*	C		91803810	000000
00101	413*	C	HIGHOR+12	XXX		91803820	000000
00101	414*	C	...			91803830	000000
00101	415*	C	N1	9000	LOW ROTOR SPEED	91803840	000000
00101	416*	C	N2	12000	HIGH ROTOR SPEED	91803850	000000
00101	417*	C	...			91803860	000000
00101	418*	C	BD11	XXX	GROUP 3 PARAMETERS FOR THE BLADES OF	91803870	000000
00101	419*	C	BD11+1	XXX	FAN ROTOR 1	91803880	000000
00101	420*	C	BD11+2	XXX		91803890	000000
00101	421*	C	BD11+3	XXX		91803900	000000
00101	422*	C	...			91803910	000000
00101	423*	C	BD21	XXX	GROUP 3 PARAMETERS FOR THE BLADES OF	91803920	000000
00101	424*	C	BD21+1	XXX	FAN ROTOR 2	91803930	000000
00101	425*	C	BD21+2	XXX		91803940	000000
00101	426*	C	BD21+3	XXX		91803950	000000
00101	427*	C	...			91803960	000000
00101	428*	C	BD32	XXX	GROUP 3 PARAMETERS FOR THE BLADES OF	91803970	000000
00101	429*	C	BD32+1	XXX	CORE ROTOR 3	91803980	000000
00101	430*	C	BD32+2	XXX		91803990	000000
00101	431*	C	BD32+3	XXX		91804000	000000
00101	432*	C	...			91804010	000000
00101	433*	C	B1	1	BLADES IN THIS EXAMPLE ARE NUMBERED IN	91804020	000000
00101	434*	C	B2	2	CIRCUMFERENTIAL SEQUENCE; HOWEVER, THIS	91804030	000000
00101	435*	C	B3	3	NEED NOT BE SO WHEN USING THIS METHOD	91804040	000000
00101	436*	C	B4	4		91804050	000000
00101	437*	C	...			91804060	000000
00101	438*	C	FB1	XXX	GROUP 4 THROUGH GROUP 10 PARAMETERS	91804070	000000
00101	439*	C	FB1+1	XXX	FOR BLADES ON THE FIRST FAN DISK	91804080	000000
00101	440*	C	FB1+2	XXX		91804090	000000
00101	441*	C	FB1+3	XXX		91804100	000000
00101	442*	C	...			91804110	000000
00101	443*	C	CB2	XXX	GROUP 3 THROUGH GROUP 10 PARAMETERS	91804120	000000
00101	444*	C	CB2+1	XXX	FOR BLADES ON THE SECOND CORE DISK	91804130	000000
00101	445*	C	CB2+2	XXX		91804140	000000
00101	446*	C	CB2+3	XXX		91804150	000000
00101	447*	C	...			91804160	000000
00101	448*	C				91804170	000000
00101	449*	C			THE FOLLOWING IS THE SURFACE DEFINITION	91804180	000000
00101	450*	C			HEADER FOR BLADE 17 OF FAN ROTOR 1.	91804190	000000

Listing 8.—Continued.

00101	451*	C			THIS BLADE'S ID NUMBER IS 61.	91804200	000000
00101	452*	C	IP-5	711	BLADE SURFACE TYPE NUMBER	91804210	000000
00101	453*	C	IP-4	10	LOCATE PARAMETERS BY MULTIMODES	91804220	000000
00101	454*	C	IP-3	1	TRUNCATION HEADERS ARE IMMEDIATE	91804230	000000
00101	455*	C	IP-2	1.0	THIS IS A DEFEND SURFACE	91804240	000000
00101	456*	C	IP-1	2	THERE ARE TWO TRUNCATION HEADERS	91804250	000000
00101	457*	C	IP	24	NUMBER OF FOLLOWING PARAMETERS	91804260	000000
00101	458*	C	IP+1	6	NUMBER OF MULTIMODES TO EVALUATE	91804270	000000
00101	459*	C	IP+2	8	FIRST MULTIMODE - MODE 8	91804280	000000
00101	460*	C	IP+3	2	NUMBER OF PARAMETERS THIS MODE	91804290	000000
00101	461*	C	IP+4	0	LOW ROTOR ENTRY	91804300	000000
00101	462*	C	IP+5	0	ROTOR ORIENTATIONS TABLE	91804310	000000
00101	463*	C	IP+6	8	SECOND MULTIMODE - MODE 8	91804320	000000
00101	464*	C	IP+7	2	NUMBER OF PARAMETERS THIS MODE	91804330	000000
00101	465*	C	IP+8	0	LOW ROTOR ENTRY	91804340	000000
00101	466*	C	IP+9	1	ENGINE SPEEDS TABLE	91804350	000000
00101	467*	C	IP+10	8	THIRD MULTIMODE - MODE 8	91804360	000000
00101	468*	C	IP+11	2	NUMBER OF PARAMETERS THIS ENTRY	91804370	000000
00101	469*	C	IP+12	0	FAN DISK 1 ENTRY	91804380	000000
00101	470*	C	IP+13	2	BLADE ON DISK ORIENTATIONS TABLE	91804390	000000
00101	471*	C	IP+14	1	FOURTH MULTIMODE - MODE 1	91804400	000000
00101	472*	C	IP+15	1	NUMBER OF PARAMETERS THIS ENTRY	91804410	000000
00101	473*	C	IP+16	7.53	DISK RADIUS	91804420	000000
00101	474*	C	IP+17	8	FIFTH MULTIMODE - MODE 8	91804430	000000
00101	475*	C	IP+18	2	NUMBER OF PARAMETERS THIS ENTRY	91804440	000000
00101	476*	C	IP+19	17	BLADE 17 ENTRY	91804450	000000
00101	477*	C	IP+20	3	BLADE NUMBER TABLE	91804460	000000
00101	478*	C	IP+21	8	SIXTH MULTIMODE - MODE 8	91804470	000000
00101	479*	C	IP+22	2	NUMBER OF PARAMETERS THIS ENTRY	91804480	000000
00101	480*	C	IP+23	0	FAN DISK 1 BLADES ENTRY	91804490	000000
00101	481*	C	IP+24	4	MECHANICAL BLADE DESCRIPTIONS TABLE	91804500	000000
00101	482*	C			NOTE - THIS EXAMPLE SURFACE EVALUATION	91804510	000000
00101	483*	C			ROUTINE EXPECTS 10 GROUPS OF PARAMETERS,	91804520	000000
00101	484*	C			AND THUS 10 MULTIMODE POINTERS, SINCE	91804530	000000
00101	485*	C			ONLY 6 POINTERS ARE SUPPLIED THE STANDARD	91804540	000000
00101	486*	C			LOGIC WILL ASSUME THAT PARAMETER GROUPS	91804550	000000
00101	487*	C			7, 8, 9, AND 10 FOLLOW CONSECUTIVELY	91804560	000000
00101	488*	C			BEHIND GROUP 6, WHICH IS THE LAST	91804570	000000
00101	489*	C			GROUP POINTED TO.	91804580	000000
00101	490*	C	IP+25	6	TRUNCATION REFERENCE POSITION - # PARAM	91804590	000000
00101	491*	C	IP+26	2	FIRST TRUNCATION HEADER - OUTER CASE	91804600	000000
00101	492*	C	IP+27	1.0	DO NOT FLOP SURFACE SIDE	91804610	000000
00101	493*	C	IP+28	29	EXTERNAL ID NUMBER	91804620	000000
00101	494*	C	IP+29	2	SECOND TRUNCATION HEADER - DISK RIM	91804630	000000
00101	495*	C	IP+30	1.0	DO NOT FLOP SURFACE SIDE	91804640	000000
00101	496*	C	IP+31	32	EXTERNAL ID NUMBER	91804650	000000
00101	497*	C				91804660	000000
00101	498*	C				91804670	000000
00101	499*	C			THIS CONCLUDES THE EXAMPLE	91804680	000000
00101	500*	C				91804690	000000
00101	501*	C				91804700	000000
00101	502*	C				91804710	000000
00101	503*	C			REQUIRED SUBROUTINES *****	91804720	000000
00101	504*	C				91804730	000000
00101	505*	C	003	STACK		91804740	000000
00101	506*	C		450	BVIRI	91884750	000000
00101	507*	C	451	BDZN		91884752	000000
00101	508*	C	453	IBDZN		91884754	000000
00101	509*	C	455	CVIRI		91884756	000000
00101	510*	C		456	IPBDZN	91884758	000000
00101	511*	C	917	POINTC		91884760	000000
00101	512*	C	919	ADDR		91884762	000000
00101	513*	C		920	CALSER	91884764	000000
00101	514*	C			A COMPLETE SURFACE EVALUATION ROUTINES PACKAGE	91804770	000000
00101	515*	C				91804780	000000
00101	516*	C				91804790	000000
00101	517*	C				91804800	000000
00101	518*	C			ERRORS REPORTED *****	91804810	000000
00101	519*	C				91804820	000000
00101	520*	C			NONE	91874830	000000
00101	521*	C				91804840	000000
00101	522*	C				91804850	000000

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00101 523* C
00103 524* PARAMETER IVSIZ=50
00104 525* COMMON /IVSIZC/IVSIZE
00105 526* REAL XL(4),SV,GR(3),SF,GF(3)
00106 527* INTEGER ID
00107 528* INTEGER IV(IVSIZ),TRCNT
00110 529* INTEGER THMDE
00110 530* C
00110 531* C CARDS 918X4940 THROUGH 918X5030 DELETED BY V03-08. THE FORTRAN
00110 532* C ADDRESS MAP IS NO LONGER NEEDED SINCE CALSED HAS TAKEN OVER
00110 533* C THAT FUNCTION.
00110 534* C
00111 535* DEFINE ITYPE=IBDZN(IP-5)
00112 536* DEFINE ISPLC=IBDZN(IP-4)
00113 537* DEFINE ITHLC=IBDZN(IP-3)
00114 538* DEFINE DC=BDZN(IP-2)
00115 539* DEFINE NTRUNC=IBDZN(IP-1)
00116 540* DEFINE NPARAM=IBDZN(IP)
00117 541* DEFINE THMODE=IBDZN(IPTH)
00120 542* DEFINE THDCMD=BDZN(IPTH+1)
00121 543* DEFINE THIDNM=IBDZN(IPTH+2)
00122 544* DEFINE DIPBDZ(I)=IPBDZN(I)
00123 545* IVSIZE=IVSIZ
00124 546* DATA IVSIZE/IVSIZ/
00126 547* 1001 RIDCM=1.0 @ INTERNAL D/C MODIFIER
00127 548* 1002 INHIB=0 @ ALLOW TRUNCATIONS
00130 549* 1003 IP=IPBDZN(ID) @ SDH POINTER
00131 550* ISW=1 @ CALC SURFACE VALUES
00132 551* NRTN=1 @ SWITCH FOR SURFACES
00133 552* GO TO 1101 @ START WITH TRUNCATIONS
00134 553* 1010 SF=SV @ PASS RESULT OUT
00135 554* RETURN @ BACK TO CALLER
00135 555* C
00135 556* C SECOND ENTRY POINT - REVERSED FIRST NEST TRUNCATIONS
00135 557* C
00135 558* C
00136 559* ENTRY SURFTR (XL,ID,SF,$)
00140 560* 1020 RIDCM=-1.0 @ INTERNAL D/C MODIFIER
00141 561* GO TO 1002 @ REST OF ENTRY IS COMMON
00141 562* C
00141 563* C THIRD ENTRY - GRADIENTS
00141 564* C
00141 565* C
00142 566* ENTRY GRAD (XL,ID,GF,$)
00144 567* 1030 IP=IPBDZN(ID) @ SDH POINTER
00145 568* ISW=2 @ CALC GRADIENTS
00146 569* NRTN=3 @ SWITCH ON GRADIENTS
00147 570* GO TO 1201 @ GO STRAIGHT TO CALCS
00150 571* 1035 DO 1036 IP=1,3 @ PASS GRADIENT OUT
00153 572* 1036 GF(IP)=GR(IP) @
00155 573* RETURN @ BACK TO CALLER
00155 574* C
00155 575* C FOURTH ENTRY - INHIBIT ALL TRUNCATIONS
00155 576* C
00155 577* C
00156 578* ENTRY SURFTI (XL,ID,SF,$)
00160 579* IP=IPBDZN(ID) @ SDH POINTER
00161 580* ISW=1 @ CALC SURFACE VALUES
00162 581* NRTN=1 @ SWITCH FOR SURFACES
00163 582* GO TO 1201 @ GO DIRECT TO SURFACE
00163 583* C+
00163 584* C FIFTH ENTRY -- SURFACE VELOCITIES
00163 585* C
00163 586* C THIS ENTRY POINT INVOKES THE APPROPRIATE SURFACE EVALUTION
00163 587* C ROUTINE TO OBTAIN THE VELOCITY VECTOR FOR THE DESIGNATED SURFACE
00163 588* C AT THE POINT XL. THE VELOCITY VECTOR RESULT IS REPORTED IN GF.
00163 589* C
00163 590* C NOTE:
00163 591* C
00163 592* C THE POSITION OF A BOUNDARY IN SPACE-TIME IS INDEPENDENT OF ITS
00163 593* C DEFEND/CONTAIN VALUE. THUS, ITS VELOCITY VECTOR IS ALSO
00163 594* C INDEPENDENT OF ITS DEFEND/CONTAIN VALUE.
00163 595* C-
00164 596* ENTRY SURFVE (XL,ID,GF,$)
00166 597* IP=IPBDZN(ID) @ POINT TO SDH
00167 598* ISW=3 @ SET SER SWITCH
00170 599* NRTN=3 @ SET INTERNAL SWITCH
00171 600* GO TO 1201 @ INTERNAL CODE SERVICE

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Listing 8.—Continued.

00171	601*	C+			V03-08E	000066
00171	602*	C	SIXTH ENTRY -- SURFACE ACCELERATIONS		V03-08E	000066
00171	603*	C			V03-08E	000066
00171	604*	C	THIS ENTRY POINT INVOKES THE APPROPRIATE SURFACE EVALUATION		V03-08E	000066
00171	605*	C	ROUTINE TO OBTAIN THE ACCELERATION VECTOR FOR THE DESIGNATED		V03-08E	000066
00171	606*	C	SURFACE AT THE POINT XL. THE ACCELERATION VECTOR RESULT IS		V03-08E	000066
00171	607*	C	REPORTED IN GF. SINCE ACCELERATION IS DEPENDENT ONLY ON		V03-08E	000066
00171	608*	C	SURFACE POSITION, THE DEFEND/CONTAIN VALUE IS NOT APPLIED TO		V03-08E	000066
00171	609*	C	THE RESULT.		V03-08E	000066
00171	610*	C-			V03-08E	000066
00172	611*		ENTRY SURFAC (XL,ID,GF,*)	@	V03-08E	000067
00174	612*		IP=IPBDZN(ID)	@ POINT TO SDH	V03-08E	000067
00175	613*		ISW=4	@ SET SER SWITCH	V03-08E	000073
00176	614*		NRTN=3	@ SET INTERNAL RETURN	V03-08E	000075
00177	615*		GO TO 1201	@ JOIN COMMON SERVICE	V03-08E	000077
00177	616*	C			91805510	000077
00177	617*	C	EVALUATION OF A SURFACE BASED ON AN SDH POINTED TO BY IP STARTS		91805520	000077
00177	618*	C	HERE. IT IS RE-ENTRANT AND SHOULD FOLLOW TRUNCATIONS OUT TO		91805530	000077
00177	619*	C	A CONSIDERABLE DEPTH IF THEY ARE NOT INHIBITED BY 'INHIB'.		91805540	000077
00177	620*	C			91805550	000077
00177	621*	C			91805560	000077
00200	622*		1101 IF (NRTN-2) 1111, ,	@ SKIP SAVE ON FIRST NEST	91805570	000101
00203	623*		CALL SPOPI (IPN)	@ GET NEW SDH POINTER		000104
00204	624*		CALL SPSHI (IP)	@ SAVE CURRENT SDH POINTER	91805590	000107
00205	625*		CALL SPSHI (IPT)	@ TRUNCATION POINTER	91805600	000112
00206	626*		CALL SPSHI (IPTH)	@ TRUNCATION HEADER POINTER	91805610	000115
00207	627*		CALL SPSHI (MDE)	@ ADDRESSING MODE	91805620	000120
00210	628*		CALL SPSHI (THMDE)	@ TRUNCATION MODE	91805630	000123
00211	629*		CALL SPSHI (IDUM11)	@ TRUNCATION LOOP COUNTER	91805640	000126
00212	630*		CALL SPSHI (NV)	@ NUMBER OF MULTIMODES	91805650	000131
00213	631*		DO 1103 IDUM11=1,TRCNT	@ APPROPRIATE ADDRESS VECTORS	91805660	000141
00216	632*		IP=IV(IDUM11)	@	91805670	000141
00217	633*		1103 CALL SPSHI (IP)	@	91805680	000142
00221	634*		CALL SPSHI (TRCNT)	@ NUMBER OF TRUNCATIONS	91805690	000146
00222	635*		CALL SPSHR (RIDCM)	@ INTERNAL MODIFIER	91805700	000151
00223	636*		RIDCM=1.0	@ LOAD NEW MODIFIER	91805710	000154
00224	637*		IP=IPN	@ LOAD NEW SDH POINTER	91805720	000156
00225	638*		1111 IF (INHIB) , ,1201	@ BR IF TRUNCATIONS INHIBITED	91805730	000161
00230	639*		TRCNT=NTRUNC	@ GET NUMBER OF TRUNCATIONS	91805740	000163
00231	640*		IF (TRCNT) 1201,1201,	@ BR IF NO TRUNCATIONS ANYWAY	91805750	000172
00234	641*		IPT=IP+1+NPARAM	@ POINT TO REFERENCE SPOT	91805760	000174
00235	642*		MDE=ITHLC	@ TRUNCATION ADDRESSING MODE	91805770	000203
00236	643*		CALL ADDR (IPT,MDE,IV,NV,TRCNT)	@ FILL IN IV BASED ON ADDRESS	91885780	000212
00237	644*			@ MODE EVALUATIONS	91885790	000221
00237	645*		CALL SPSHI (INHIB)	@ SAVE INHIBIT AND	91805810	000221
00240	646*		CALL SPSHI (NRTN)	@ RETURN SWITCH INFORMATION	91805820	000224
00241	647*		NRTN=2	@ SURFACES CALLS FROM TRUNC	91805830	000227
00242	648*			@ HANDLER	91805840	000231
00242	649*		IPTH=IV(1)	@ POINT TO FIRST TRUNC HEADER	91805850	000231
00243	650*		IDUM11=0	@ CLEAR LOOP COUNTER	91805860	000233
00244	651*		1121 IDUM11=IDUM11+1	@ DO LOOP THROUGH TRUNCATIONS	91805870	000235
00245	652*		IF (IDUM11-TRCNT) , ,1190	@ BR IF LOOP FINISHED	91805880	000237
00250	653*		THMDE=THMODE	@ GET BASIC TRUNCATION HEADER	91805890	000242
00251	654*		THMDE=ABS(THMDE)	@ MODE	91805900	000246
00252	655*		INHIB=0	@ SETUP NEXT NEST LEVEL	91805910	000250
00253	656*		IF (THMODE) ,1127,1127	@ INHIBIT TRUNC CONTRL	91805920	000251
00256	657*		INHIB=1	@	91805930	000256
00257	658*		1127 GO TO (1128,1130,1132),THMDE	@ BR BY TRUNC HEADER MODE	91805940	000261
00260	659*		1128 IDUM12=IPTH+8	@ MODE 1 - SDH RIGHT HERE	91805950	000271
00261	660*		GO TO 1135	@	91805960	000273
00262	661*		1130 IDUM12=DIPBDZ(THIDNM)	@ MODE 2 - SDH DEFINED IN	91815970	000275
00263	662*		GO TO 1135	@ IPBDZN (EXTERNAL DEF)	91805980	000307
00264	663*		1132 IDUM12=THIDNM+IBDZN(1)	@ MODE 3 - SDH DEFINED IN	91805990	000311
00265	664*		IDUM12=IBDZN(IDUM12)	@ INTERNAL TABLE	91806000	000324
00266	665*		1135 CALL SPSHI (IDUM12)	@ PUT NEW SDH POINTER ON STACK	91806010	000331
00267	666*		GO TO 1101	@ GO EVALUATE THE SURFACE	91806020	000333
00267	667*	C			91806030	000333
00267	668*	C	ALL INTERNAL TRUNCATION SURFACE EVALUATIONS RETURN TO THE		91806040	000333
00267	669*	C	FOLLOWING SEGMENT OF CODE.		91806050	000333
00267	670*	C			91806060	000333
00267	671*	C			91806070	000333
00270	672*		1140 SV=SV*THDCHD*RIDCM	@ DEFEND/CONTAIN MODIFIERS	91806080	000335

00271	673*	IF (SV) 1160,	@ BR IF SURFACE TRUNCATED	91806090	000345
00274	674*	1144 IF (ITHLC-10) 1145,1153,114C	@ BR IF MULTIMODES IN EFFECT	V03-08D	000350
00277	675*	1145 GO TO (1146,1150,1150),THMDE	@ REPOINT IPTH BY TH MODE	91806110	000360
00300	676*	1146 IPTH=IPTH+8	@ MODE 1 - SKIP A STANDARD	91816120	000370
00301	677*	IPTH=IPTH+1+IBDZN(IPTH)	@ SDH	91806130	000372
00302	678*	IPTH=IPTH+1+IBDZN(IPTH)	@	91806140	000401
00303	679*	GO TO 1121	@ DO ANOTHER TRUNCATION	91806150	000410
00304	680*	1150 IPTH=IPTH+3	@ MODES 2,3 -JUST SKIP A	91806160	000412
00305	681*		@ TRUNCATION HEADER	91806170	000414
00305	682*	GO TO 1121	@ DO ANOTHER TRUNCATION	91806180	000414
00306	683*	1153 NV=NV-1	@ DOWN COUNT ACTUAL MULTIMODES	91806190	000416
00307	684*		@ LEFT	91806200	000421
00307	685*	IF (NV) 1145,1145,	@ BR IF NONE LEFT	91806210	000421
00312	686*	IPTH=IV(IDUM11+1)	@ MULTIMODE POINTERS FOR	91806220	000423
00313	687*		@ TRUNCATION HEADERS ALWAYS	91806230	000425
00313	688*		@ POINT CORRECTLY	91806240	000425
00313	689*	GO TO 1121	@ GO DO ANOTHER TRUNCATION	91806250	000425
00313	690*	C		91806260	000425
00313	691*	C CONTROL ARRIVES HERE IF A TRUNCATION OCCURS		91806270	000425
00313	692*	C		91806280	000425
00313	693*	C		91806290	000425
00314	694*	1160 SV=1.0	@ REPORT A SAFE VALUE	91806300	000427
00315	695*	CALL SPOPI (NRTN)	@ GET CALLING NEST'S SWITCHES	91806310	000430
00316	696*	CALL SPOPI (INHIB)	@	91806320	000433
00317	697*	IF (NRTN-2) 1164,1166,1164	@ ARE WE NESTED ?	V03-08D	000436
00322	698*	1164 SF=SV	@ NO, MAKE REPORT TO CALLER	V03-08D	000441
00323	699*	RETURN 4	@ VIA TRUNCATION ROUTE	V03-08D	000443
00324	700*	1166 CALL SPOPR (RIDCM)	@ YES, POP BACK TO PARENT	V03-08D	000450
00325	701*	CALL SPOPI (TRCNT)	@ SURFACE	V03-08D	000452
00326	702*	DO 1170 IDUM11=TRCNT,1,-1	@	V03-08D	000455
00331	703*	CALL SPOPI (IP)	@	V03-08D	000463
00332	704*	1170 IV(IDUM11)=IP	@	V03-08D	000465
00334	705*	CALL SPOPI (NV)	@	V03-08D	000470
00335	706*	CALL SPOPI (IDUH11)	@	V03-08D	000473
00336	707*	CALL SPOPI (THMDE)	@	V03-08D	000476
00337	708*	CALL SPOPI (MDE)	@	V03-08D	000501
00340	709*	CALL SPOPI (IPTH)	@	V03-08D	000504
00341	710*	CALL SPOPI (IPT)	@	V03-08D	000507
00342	711*	CALL SPOPI (IP)	@	V03-08D	000512
00343	712*	GO TO 1144	@ FORCE NO PARENT TRUNCATION	V03-08D	000515
00343	713*	C		91806360	000515
00343	714*	C CONTROL ARRIVES HERE IF TRUNCATION LOOP COMPLETES WITHOUT ANY		91806370	000515
00343	715*	C TRUNCATIONS OCCURING. MUST PRECEDE STATEMENT 1201 OR HAVE A GO TO		91806380	000515
00343	716*	C		91806390	000515
00343	717*	C		91806400	000515
00344	718*	1190 CALL SPOPI (NRTN)	@ LEAVING TRUNC LOOP TAKE	91806410	000517
00345	719*	CALL SPOPI (INHIB)	@ US BACK UP IN NEST	91806420	000521
00345	720*	C		91806430	000521
00345	721*	C SURFACE VALUE ROUTINE VECTORING DONE HERE.		91806440	000521
00345	722*	C		91806450	000521
00345	723*	C		91806460	000521
00346	724*	1201 MDE=ISPLC	@ GET PARAMETER ADDRESSING	91806470	000525
00347	725*	CALL ADR (IP,MDE,IV,NV)	@ MODE AND FILL IV FROM IT	91886480	000533
00350	726*	IPOS=ITYPE	@ GET SER'S NUMBER	91876490	000541
00351	727*	CALL CALSER (IPOS,XL,IV,NV,SV,GR,ISW)		91886500	000550
00352	728*		@ GO EVALUATE SURFACE	91876510	000561
00352	729*	C CARDS 918X6520 THROUGH 918X6610 DELETED BY V03-08		91876520	000561
00352	730*	C		91806620	000561
00352	731*	C SURFACE EVALUATION ROUTINES RETURN CONTROL TO THIS POINT.		91806630	000561
00352	732*	C		91806640	000561
00352	733*	C		91806650	000561
00352	734*	GO TO (1218,1220,1222,1222),ISW	@ APPLY DC AS APPROPRIATE	V03-08E	000561
00353	735*	1218 SV=SV*DC	@ APPLY DC TO SURFACE VALUE		000573
00354	736*	GO TO (1010,1223,1035),NRTN	@		000602
00355	737*	1220 DO 1221 IDUM11=1,3	@ APPLY DC TO GRADIENT		000613
00360	738*	1221 GR(IDUH11)=DC*GR(IDUH11)	@	91826680	000620
00362	739*	1222 GO TO (1010,1223,1035),NRTN	@ GO SOMEPLACE	V03-08C	000626
00363	740*	1223 CALL SPOPR (RIDCM)	@ POP THE THINGS WE	91806700	000636
00364	741*	CALL SPOPI (TRCNT)	@ STORED WHEN WE STARTED	91806710	000640
00365	742*	DO 1227 IDUM11=TRCNT,1,-1	@ TO EVALUATE THIS SURFACE	91806720	000643
00370	743*	CALL SPOPI (IP)	@	91806730	000651
00371	744*	1227 IV(IDUH11)=IP	@	91806740	000653
00373	745*	CALL SPOPI (NV)	@	91806750	000656
00374	746*	CALL SPOPI (IDUH11)	@	91806760	000661
00375	747*	CALL SPOPI (THMDE)	@	91806770	000664
00376	748*	CALL SPOPI (MDE)	@	91806780	000667
00377	749*	CALL SPOPI (IPTH)	@	91806790	000672
00400	750*	CALL SPOPI (IPT)	@	91806800	000675
00401	751*	CALL SPOPI (IP)	@	91806810	000700
00402	752*	GO TO 1140	@ GO BACK TO TRUNC HANDLER	91806820	000703
00402	753*	C CARDS 918X6830 THROUGH 918X8999 DELETED BY V03-08		91876830	000703
00403	754*	END		91809990	001051

END FOR
>

Listing 8.—Concluded.

@FOR,MS CASPER9,SA100D
 FOR 4R1 E -04/13/84-15:37:21 (2,)
 >@EOF

SUBROUTINE SA100 ENTRY POINT 000151

STORAGE USED: CODE(1) 000174; DATA(0) 000026; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 IVSIZE 000001

EXTERNAL REFERENCES (BLOCK, NAME)

0004 BDZN
 0005 POINTC
 0006 NERR2\$
 0007 SGRT
 0010 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000012	100L	0001	000056	105L	0001	000071	107L	0001	000130	114L	0001	000025	122G
0001	000110	135G	0001	000133	143G	0004	R	000000	BDZN	0000	I	000004	I	0000
000C	I	000000	IVC	0003	I	000000	IVSIZE	0000	I	000002	NC	0000	R	000003

00101	1*		SUBROUTINE SA100 (XL,IV,NV,SV,GR,ISW)	92110010	000000
00101	2*	C		92100020	000000
00101	3*	C		92100030	000000
00101	4*	C	SA100 ***** A SUBROUTINE FOR CASPER *****	92100040	000000
00101	5*	C	AUTHOR WILLIAM HENRY JONES	92100050	000000
00101	6*	C	V03-00 24 JUL 78	92100060	000000
00101	7*	C	V03-01 06 SEP 78	92110061	000000
00101	8*	C	V03-01A 28 SEP 81 ADD VELOCITY HANDLING	V03-01A	000000
00101	9*	C	V03-01B 05 AUG 83 ADD ACCELERATION SUPPORT	V03-01B	000000
00101	10*	C		90000020	000000
00101	11*	C		90000030	000000
00101	12*	C	ARGUMENTS PASSED IN SUBROUTINE CALL *****	90010034	000000
00101	13*	C		90010036	000000
00101	14*	C	ARGUMENT TYPE DIMENSION DESCRIPTION	90000040	000000
00101	15*	C	-----	90000050	000000
00101	16*	C	XL REAL 1 TO 4 THREE POSITION COORDINATES	90000060	000000
00101	17*	C		90000070	000000
00101	18*	C		90000110	000000
00101	19*	C	IV INTEGER 1 TO IVSIZE POINTER LIST TO PARAMETERS	90000120	000000
00101	20*	C		90000130	000000
00101	21*	C		90000140	000000
00101	22*	C	NV INTEGER SCALAR NUMBER OF INDEPENDENT	90000150	000000
00101	23*	C		90000160	000000
00101	24*	C		90000170	000000
00101	25*	C	SV REAL SCALAR SURFACE VALUE RETURNED	90000180	000000
00101	26*	C		90000190	000000
00101	27*	C	GR REAL 1 TO 3 GRADIENT RETURNED	90000200	000000
00101	28*	C		90000210	000000
00101	29*	C	ISW INTEGER SCALAR FUNCTION SELECTOR	90000220	000000
00101	30*	C		90000230	000000
00101	31*	C		90000240	000000
00101	32*	C		90010262	000000
00101	33*	C		90010264	000000
00101	34*	C	ARGUMENTS IN CASPER 'CACHE' MEMORY *****	90010266	000000
00101	35*	C		90010268	000000
00101	36*	C	ARGUMENT TYPE DIMENSION DESCRIPTION	90010270	000000
00101	37*	C	-----	90010272	000000
00101	38*	C	BDZN REAL 1 TO BDZNSZ SURFACE EVALUATION ROUTINE	90010274	000000
00101	39*	C		90010276	000000

Listing 9.—Subroutine SA100.

```

00101 40* C 90010278 000000
00101 41* C 90000270 000000
00101 42* C 90000280 000000
00101 43* C 90000290 000000
00101 44* C DESCRIPTION ***** 90000300 000000
00101 45* C 90000310 000000
00101 46* C SA100 DEFINES A TIME-INVARIANT SPHERE IN SPACE. 92100300 000000
00101 47* C 90000340 000000
00101 48* C 90000350 000000
00101 49* C 90000360 000000
00101 50* C PARAMETER LIST ***** 90000370 000000
00101 51* C 90000380 000000
00101 52* C REL POSIT 'IV' SLOT DESCRIPTION 90000390 000000
00101 53* C ----- 90000400 000000
00101 54* C IVP 1 X COORD OF SPHERE CENTER 92100500 000000
00101 55* C IVP+1 1 Y COORD OF SPHERE CENTER 92100510 000000
00101 56* C IVP+2 1 Z COORD OF SPHERE CENTER 92100520 000000
00101 57* C IVP+3 2 RADIUS OF SPHERE 92100530 000000
00101 58* C 90000430 000000
00101 59* C 90000440 000000
00101 60* C 90000450 000000
00101 61* C REQUIRED SUBROUTINES ***** 90000460 000000
00101 62* C 90000470 000000
00101 63* C 450 BVIRI 90010474 000000
00101 64* C 451 BDZN 90010476 000000
00101 65* C 917 POINTC 90000480 000000
00101 66* C 90000490 000000
00101 67* C 90000500 000000
00101 68* C 90000510 000000
00101 69* C ERRORS REPORTED ***** 90000520 000000
00101 70* C 90000530 000000
00101 71* C NONE 92100700 000000
00101 72* C 90000560 000000
00101 73* C 90000570 000000
00101 74* C 90000580 000000
00103 75* COMMON /IVSIZE/IVSIZE 90000600 000000
00104 76* INTEGER IV(IVSIZE),NV,ISW 90000610 000000
00105 77* REAL XL(4),SV,GR(3) 90010620 000000
00106 78* INTEGER IVC(2) 92100900 000000
00107 79* DATA NC/2/ 92100910 000000
00111 80* DATA IVC/0,3/ 92100920 000000
00113 81* DEFINE P(I)=BDZN(I) 92100930 000000
00114 82* DEFINE A(I)=F(IV(1))+I-1) 92100940 000000
00115 83* DEFINE B=F(IV(2))+3) 92100950 000000
00116 84* GO TO (100,100,114,114),ISW @ TRAP VEL AND ACCEL REQ V03-01B 000000
00117 85* 100 CALL POINTC (IV,IVC,NV,NC) @ CORRECT PARAMETER POINTERS V03-01A 000012
00120 86* R=0.0 @ CALCULATE THE RADIUS FROM 92100970 000017
00121 87* DO 102 I=1,3 @ THE CENTER OF THE SPHERE 92100980 000025
00124 88* 102 R=R+(A(I)-XL(I))**2 @ TO THE POINT IN QUESTION 92100990 000025
00126 89* R=SQRT(R) @ 92101000 000042
00127 90* GO TO (105,107),ISW @ JMP BY TASK 92101010 000046
00130 91* 105 SV=R-B @ SURFACE 92101020 000056
00131 92* RETURN @ 92101030 000065
00132 93* 107 R=AMAX1 (R,1.0E-19) @ AVOID ZERO DIVIDE 92101040 000071
00133 94* R=1.0/R @ DIVIDE BY MULTIPLYING 92101050 000076
00134 95* DO 112 I=1,3 @ DO THE GRADIENT 92101060 000110
00137 96* 112 GR(I)=R*(XL(I)-A(I)) @ 92101070 000110
00141 97* RETURN @ 92101080 000124
00142 98* 114 DO 115 I=1,3 @ TIME INVARIANT SURFACES HAVE V03-01A 000133
00145 99* 115 GR(I)=0.0 @ A ZERO VELOCITY V03-01A 000133
00147 100* RETURN @ V03-01A 000134
00150 101* END 92101090 000173
END FOR
>

```

Listing 9.—Concluded.

@FOR:MS CASPER1.POWERD
 FOR 4R1 E -04/13/84-16:03:49 (4,)
 >@EOF

SUBROUTINE POWERC ENTRY POINT 000247

STORAGE USED: CODE(1) 000315; DATA(0) 000062; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 CHKLH
 0004 WERR2
 0005 PM1
 0006 VM1
 0007 P
 0010 PM2
 0011 V
 0012 VM2
 0013 STACWD
 0014 CHKTIM
 0015 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000031	105L	0001	000035	106L	0001	000040	107L	0001	000100	147G	0001	000141	160G					
0001	000143	163G	0001	000145	167G	0000	R	000025	A1	0000	R	000026	A2	0000	R	000016	A3		
0000	R	000027	B1	0000	R	000030	B2	0000	R	000017	B3	0000	R	000020	C	0000	R	000006	DM
0000	R	000002	DMAT	0000	R	000011	EPS	0000	R	000025	F	0000	I	000021	I	0000	I	000001	IE
0000	000042	INJP\$	0000	I	000000	IS	0000	I	000022	J	0000	I	000023	K	0000	I	000024	L	
0007	R	000000	P	0005	R	000000	PM1	0010	R	000000	PM2	0000	R	000012	R	0011	R	000000	V
0006	R	000000	VM1	0012	R	000000	VM2												
00101	1*			SUBROUTINE POWERC (IL,IH,TA,TB)								12000010	000000						
00101	2*	C+																	
00101	3*	C																	
00101	4*	C	POWERC	***** A SUBROUTINE FOR CASPER *****								12000040	000000						
00101	5*	C		AUTHOR	WILLIAM HENRY JONES								12000050	000000					
00101	6*	C		V01-00	05 FEB 79								12000060	000000					
00101	7*	C		V01-00A	07 MAR 79								120A0061	000000					
00101	8*	C		V01-00B	11 FEB 80 ADD 'CHKTIM'									000000					
00101	9*	C		V01-00C	23 FEB 81 REMOVE TIME FROM COMMON									000000					
00101	10*	C		V01-00D	05 APR 83 P IS DUPLICATE NAME								V01-00D	000000					
00101	11*	C																	
00101	12*	C																	
00101	13*	C		DESCRIPTION *****								12000090	000000						
00101	14*	C																	
00101	15*	C		CALCULATES THE AVERAGE POWER OF COMPRESSION OVER THE PAST								12000100	000000						
00101	16*	C		ITERATIONS FOR ALL AEROELEMENTS IN THE RANGE 'IL' TO 'IH'.								12000120	000000						
00101	17*	C																	
00101	18*	C		THEORY *****								12000140	000000						
00101	19*	C																	
00101	20*	C		THE PRESSURE AND VOLUME HISTORIES OF EACH AEROELEMENT ARE								12000160	000000						
00101	21*	C		ASSUMED TO BE QUADRATIC IN TIME.								12000170	000000						
00101	22*	C																	
00101	23*	C																	
00101	24*	C																	
00101	25*	C																	
00101	26*	C		WE SET PRIMED TIME EQUAL TO ZERO AT THE TIME OF THE PREVIOUS								12000220	000000						
00101	27*	C		RECORDED PRESSURES AND VOLUMES (PM1 AND VM1). FURTHER, THE								12000230	000000						
00101	28*	C		CURRENT PRESSURES AND VOLUMES ARE AT RELATIVE TIME TA AND THE									000000						
00101	29*	C		SECOND PREVIOUS PRESSURES AND VOLUMES ARE AT TIME TB (WHERE									000000						
00101	30*	C		TB IS USUALLY LESS THAN ZERO, THUS,									000000						
00101	31*	C																	
00101	32*	C																	
00101	33*	C																	
00101	34*	C																	
00101	35*	C		AND															
00101	36*	C																	
00101	37*	C																	
00101	38*	C																	
00101	39*	C																	
00101	40*	C																	
00101	41*	C																	
00101	42*	C		BY SIMPLE MATRIX MANIPULATIONS, IT CAN BE SHOWN THAT									000000						

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00101 43* C
00101 44* C
00101 45* C
00101 46* C
00101 47* C
00101 48* C
00101 49* C
00101 50* C
00101 51* C
00101 52* C
00101 53* C
00101 54* C
00101 55* C
00101 56* C
00101 57* C
00101 58* C
00101 59* C
00101 60* C
00101 61* C
00101 62* C
00101 63* C
00101 64* C
00101 65* C
00101 66* C
00101 67* C
00101 68* C
00101 69* C-
00103 70*
00104 71*
00105 72*
00106 73*
00107 74*
00110 75*
00111 76*
00112 77*
00114 78*
00116 79*
00117 80*
00120 81*
00123 82*
00126 83*
00131 84*
00134 85*
00135 86*
00136 87*
00137 88*
00140 89*
00141 90*
00142 91*
00143 92*
00144 93*
00145 94*
00146 95*
00151 96*
00152 97*
00153 98*
00154 99*
00155 100*
00156 101*
00157 102*
00162 103*
00165 104*
00166 105*
00171 106*
00173 107*
00176 108*
00176 109*
00177 110*
00200 111*
00201 112*
00203 113*
00204 114*
END FOR
>

```

			A1	B1	TB	-TA	P	-PM1	V	-VM1		
			=			*						
			A2	B2	-TB**2	TA**2		PM2-PM1	VM2-VM1			
												(TA**2)*TB - TA*TB**2

```

12000350 000000
12000360 000000
12000370 000000
12000380 000000
12000390 000000
12000400 000000
12000410 000000
12000420 000000
12000430 000000
12000440 000000
12000450 000000
12000460 000000
12000470 000000
12000480 000000
12000490 000000
12000500 000000
12000510 000000
12000710 000000
12000720 000000
12000730 000000

```

```

PARAMETER OURID=120
INTEGER IL,IH,IS,IE
REAL DMAT(2,2),DM(3),EPS
REAL TA,TB,R(2,2)
REAL F(2,2),A1,B1,A2,B2,A3,B3,C
EQUIVALENCE (A1,F(1,1)),(A2,F(2,1))
EQUIVALENCE (B1,F(1,2)),(B2,F(2,2))
DATA IE/1/
DATA EPS/1.0E-20/
IE=1
CALL CHKLH (IL,IH,IS,OURID,IE)
IF (IS) 102,106,102
IF (ABS(TA-TB)-EPS) 105,103,103
IF (ABS(TA)-EPS) 105,104,104
IF (ABS(TB)-EPS) 105,107,107
CALL WERR2 (OURID,5)
RETURN
C=1.0/(TA*TB*(TA-TB))
DMAT(1,1)=C*TB
DMAT(2,1)=-C*TB*TB
DMAT(1,2)=-C*TA
DMAT(2,2)=C*TA*TA
DM(3)=0.5*TA
DM(2)=0.666667*DM(3)*TA
DM(1)=1.5*DM(2)*TA
DO 143 I=IL,IH,IS
A3=PM1(I)
B3=VM1(I)
R(1,1)=P(I)-A3
R(2,1)=PM2(I)-A3
R(1,2)=V(I)-B3
R(2,2)=VM2(I)-B3
DO 137 J=1,2
DO 137 K=1,2
F(J,K)=0.0
DO 136 L=1,2
F(J,K)=F(J,K)+DMAT(J,L)*R(L,K)
CONTINUE
C=(A1*B1*DM(1))+((2.0*A2*B1+A1*B2)*DM(2))+((2.0*A3*B1+A2*B2)*DM(3))
1)+(A3*B2)
CALL STACWD (I,C)
CALL CHKTIM (IL,IH,I)
CONTINUE
RETURN
END
12001010 000314

```

Listing 10.—Concluded.

@FOR,MS CASPER5.WRKFLD
 FOR 4R1 E -04/13/84-15:48:49 (1,)
 >@EOF

SUBROUTINE WRKFLD ENTRY POINT 000125

STORAGE USED: CODE(1) 000145; DATA(0) 000024; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 MU
 0004 MUTHET
 0005 CHKLH
 0006 CHKTIM
 0007 U
 0010 P
 0011 EIJ
 0012 STS
 0013 NERR3*

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000111	110L	0001	000017	112G	0001	000027	116G	0001	000051	122G	0011	R	000000	EIJ				
0000	I	000001	I	0000	000010	INJF*	0000	I	000000	IS	0000	I	000002	J	0000	I	000004	K	
0003	R	000000	MU	0004	R	000000	MUTHET	0010	R	000000	P	0000	R	000003	R	0007	R	000000	U

```

00101 1*          SUBROUTINE WRKFLD (IL,IH)          000000
00101 2*          C+                                000000
00101 3*          C                                  000000
00101 4*          C  WRKFLD      ***** A SUBROUTINE FOR CASPER ***** 000000
00101 5*          C          AUTHDR      WILLIAM HENRY JONES          000000
00101 6*          C          V01-00      12 FEB 80                    000000
00101 7*          C          V01-00A     15 SEP 80      FUNCTION TYPE STATEMENTS 000000
00101 8*          C                                  000000
00101 9*          C                                  000000
00101 10*         C  DESCRIPTION ***** 000000
00101 11*         C                                  000000
00101 12*         C  THIS ROUTINE IS PART OF A PATCH TO THE POWER OF DISTORTION 000000
00101 13*         C  SECTION OF CASPER WORK FLOW CALCULATION.  IT LOADS INTO THE 000000
00101 14*         C  SCRATCH STRING OF EACH ELEMENT IN THE RANGE 'IL' TO 'IH' THE 000000
00101 15*         C  QUANTITY 000000
00101 16*         C                                  000000
00101 17*         C  S(I) = U(J)*(-P*D(I,J)+MUTHET*D(I,J)+2*MU*E(I,J)), I=1,3, J=1,3 000000
00101 18*         C                                  000000
00101 19*         C  PER THE DERIVATION IN THE CASPER THEORETICAL REPORT. 000000
00101 20*         C                                  000000
00101 21*         C                                  000000
00101 22*         C-                                000000
00103 23*         C  PARAMETER OURID=504 000000
00104 24*         C  REAL MU,MUTHET 000000
00105 25*         C  CALL CHKLH (IL,IH,IS,OURID,1) @ GO VALIDATE DO LOOP RANGE 000000
00106 26*         C  IF (IS) 102,110,102 @ IS IT VALID ? 000006
00111 27*         C  DO 109 I=IL,IH,IS @ YES, DO IT 000010
00114 28*         C  CALL CHKTIM (IL,IH,I) @ KEEP AN EYE ON THE TIME 000017
00115 29*         C  DO 108 J=1,3 @ 000027
00120 30*         C  R=U(I,J)*(MUTHET(I)-P(I)) @ DO KRONECKER DELTA TERM 000027
00121 31*         C  DO 107 K=1,3 @ 000051
00124 32*         C  R=R+2.0*U(I,K)*MU(I,1)*EIJ(I,J,K) @ ACCUMULATE SHEAR TERM 000051
00126 33*         C  CALL STS (I,J,R) @ STORE RESULT 000077
00130 34*         C  CONTINUE @ 000111
00132 35*         C  RETURN @ 000111
00133 36*         C  END @ 000144
END FOR.
>

```

Listing 11.—Subroutine WRKFLD.

@FOR,MS CASPERS,WRKFED
 FOR 4R1 E -04/13/84-15:50:03 (0,)
 >@EOF

SUBROUTINE WRKFLE ENTRY POINT 000153

STORAGE USED: CODE(1) 000174; DATA(0) 000046; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 CHKLH
 0004 CHKTIM
 0005 NEI
 0006 S
 0007 INTF
 0010 V
 0011 STS
 0012 NERR3*

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000017	112G	0001	000030	116G	0001	000136	118L	0001	000040	122G	0001	000054	130G					
0001	000056	133G	0001	000074	142G	0001	000077	145G	0000	R	000000	B	0000	R	000024	D			
0000	I	000021	I	0000	000032	INJP*	0007	I	000000	INTP	0000	I	000017	IS	0000	I	000020	I1	
0000	I	000022	J	0000	I	000023	K	0005	I	000000	NEI	0006	R	000000	S	0010	R	000000	V

```

00101      1*          SUBROUTINE WRKFLE (IL,IH)                                000000
00101      2*      C+                                                                    000000
00101      3*      C                                                                    000000
00101      4*      C      WRKFLE          ***** A SUBROUTINE FOR CASPER *****  000000
00101      5*      C              AUTHOR          WILLIAM HENRY JONES            000000
00101      6*      C              V01-00          12 FEB 80                      000000
00101      7*      C                                                                    000000
00101      8*      C                                                                    000000
00101      9*      C      DESCRIPTION *****                                       000000
00101     10*      C                                                                    000000
00101     11*      C      THIS ROUTINE COMPLETES THE POWER OF DISTORTION PATCH BY  000000
00101     12*      C      CALCULATING THE DIVERGENCE OF THE VECTORS CALCULATED BY  000000
00101     13*      C      WRKFELD.                                                 000000
00101     14*      C                                                                    000000
00101     15*      C                                                                    000000
00101     16*      C-                                                                    000000
00103     17*          PARAMETER OURID=505                                          @          000000
00104     18*          REAL B(3,5)                                                  @          000000
00105     19*          CALL CHKLH (IL,IH,IS,OURID,1)                                @ CHECK RANGE LIMITS  000000
00106     20*          IF (IS) 102,118,102                                          @ VALID RANGE ?      000006
00111     21*      102 DO 117 I1=IL,IH,IS                                          @ YES, USE IT        000010
00114     22*          CALL CHKTIM (IL,IH,I1)                                       @ KEEP AN EYE ON THE TIME  000017
00115     23*          DO 107 I=1,5                                                @ PICKUP VALUES FROM THE  000030
00120     24*          J=NEI(I1,I)                                                  @ NEIGHBORS          000030
00121     25*          DO 107 K=1,3                                                @                      000040
00124     26*      107 B(K,I)=S(J,K)                                               @                      000040
00127     27*          DO 110 I=1,5                                                @ FORM DIFFERENCES     000056
00132     28*          DO 110 J=1,3                                                @                      000056
00135     29*      110 B(J,I)=B(J,I)-S(I1,J)                                       @                      000056
00140     30*          D=0.0                                                        @ INIT ACCUMULATOR    000067
00141     31*          DO 114 I=1,3                                                @ ACCUMULATE DIVERGENCE  000077
00144     32*          DO 114 J=1,5                                                @ (WORK PER UNIT VOLUME) 000077
00147     33*      114 D=D+INTP(I1,I,J)*B(I,J)                                     @                      000077
00152     34*          D=D*(I1)                                                    @ WORK DONE ON THE ELEMENT 000121
00153     35*          CALL STS (I1,4,D)                                           @ SAVE IN SCRATCH SLOT 4  000126
00154     36*      117 CONTINUE                                                    @                      000136
00156     37*      118 RETURN                                                       @                      000136
00157     38*          END                                                         @                      000173
END FOR

```

Listing 12.—Subroutine WRKFLE.


```

@FOR,MS CASPERS.WRKFFD
FOR 4R1 E -04/13/84-15:51:27 (1,)
>EOF

```

```

SUBROUTINE WRKFLF ENTRY POINT 000220

```

```

STORAGE USED: CODE(1) 000243; DATA(0) 000043; BLANK COMMON(2) 000000

```

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

```

0003 CHKLH
0004 ASCH
0005 T
0006 V
0007 X
0010 NEI
0011 STS
0012 CHKTIM
0013 XPRR
0014 SQRT
0015 NERR3$

```

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

```

0001 000017 112G      0001 000047 121G      0001 000103 125L      0001 000061 126G      0001 000161 131L
0001 000071 132G      0001 000203 136L      0001 000106 144G      0004 R 000000 ASCH      0000 R 000000 B
0000 R 000001 C        0000 R 000002 D        0000 R 000003 E        0000 I 000013 I        0000 000025 INJP$
0000 I 000011 IS      0000 I 000012 I1       0000 I 000014 J        0000 I 000015 K        0010 I 000000 NEI
0000 R 000004 R        0000 R 000005 S        0005 R 000000 T        0006 R 000000 V        0007 R 000000 X
0000 R 000006 X1
00101 1*          SUBROUTINE WRKFLF (IL,IH,GDAST)          000000
00101 2*          C+                                     000000
00101 3*          C                                     000000
00101 4*          C   WRKFLF      ***** A SUBROUTINE FOR CASPER ***** 000000
00101 5*          C   AUTHOR      WILLIAM HENRY JONES          000000
00101 6*          C   X01.00      12 FEB 80                    000000
00101 7*          C   X01.00A    06 OCT 81      DISTANCE INTO HEAT FLOW X01.00A 000000
00101 8*          C                                     000000
00101 9*          C                                     000000
00101 10*         C   DESCRIPTION *****                    000000
00101 11*         C                                     000000
00101 12*         C   THIS ROUTINE CALCULATES THE HEAT FLOW BETWEEN NEAREST 000000
00101 13*         C   NEIGHBORS. IT IS CALCULATED AS THE AVERAGE COEFFICIENT 000000
00101 14*         C   OF HEAT TRANSFER BETWEEN THE NEIGHBORS TIMES THE DIFFERENCE 000000
00101 15*         C   IN TEMPERATURE TIMES THE TIME DURATION OF HEAT FLOW TIMES THE X01.00A 000000
00101 16*         C   AVERAGE CROSS-SECTIONAL AREA OF THE HEAT-EXCHANGING ELEMENTS X01.00A 000000
00101 17*         C   AND DIVIDED BY THE DISTANCE BETWEEN THE ELEMENTS.      X01.00A 000000
00101 18*         C                                     000000
00101 19*         C   CALCULATIONS ARE RECORDED ONLY FOR TARGET AEROELEMENTS 000000
00101 20*         C   IN THE RANGE 'IL' TO 'IH'. NEIGHBORS MUST RECIPROCATE 000000
00101 21*         C   (THE NEIGHBOR MUST LIST THE TARGET AEROELEMENT AS A 000000
00101 22*         C   NEIGHBOR) FOR THE CALCULATIONS BETWEEN THE PAIRING TO 000000
00101 23*         C   BE CARRIED OUT.                                     000000
00101 24*         C                                     000000
00101 25*         C                                     000000
00101 26*         C-                                     000000
00103 27*         C   PARAMETER OURID=506                      000000
00104 28*         C   REAL B,C,D,E,R,S,X1(3)                  @          X01.00A 000000
00105 29*         C   CALL CHKLH (IL,IH,IS,OURID,1)          @ CHECK RANGE LIMITS 000000
00106 30*         C   IF (IS) 102,136,102                    @ VALID RANGE ?     X01.00A 000006
00111 31*         C   DO 135 I1=IL,IH,IS                      @ YES, USE IT       X01.00A 000010
00114 32*         C   B=0.0                                    @ CLEAR ACCUMULATOR X01.00A 000017
00115 33*         C   C=ASCH(I1)                              @ TARGET COEFFICIENT, X01.00A 000020
00116 34*         C   D=T(I1)                                 @ TEMPERATURE,     X01.00A 000024

```

```

00117 35*      E=3.141592653*(ABS(7.9577471E-02*V(I1))**0.6666667) @ AREA,      X01.00A  000030
00120 36*      DO 108 I=1,3 @ POSITION X01.00A  000047
00123 37* 108  X1(I)=X(I1,I) @ X01.00A  000047
00125 38*      DO 131 I=1,5 @ DO EACH NEAREST NEIGHBOR X01.00A  000061
00130 39*      J=NEI(I1,I) @ GET NEIGHBOR ID X01.00A  000061
00131 40*      DO 113 K=1,5 @ X01.00A  000071
00134 41*      IF (NEI(J,K)-I1) 113,125,113 @ DOES NEIGHBOR RECIPROCATATE ? X01.00A  000071
00137 42* 113  CONTINUE @ NO, NOT YET ANYWAY X01.00A  000101
00141 43*      GO TO 131 @ NO, NOT AT ALL X01.00A  000101
00142 44* 125  R=0.0 @ CALC DISTANCE BETWEEN X01.00A  000103
00143 45*      DO 127 K=1,3 @ NEIGHBORS X01.00A  000106
00146 46* 127  R=R+(X(J,K)-X1(K))**2 @ X01.00A  000106
00150 47*      R=SQRT(R) @ X01.00A  000120
00151 48*      S=3.141592653*(ABS(7.9577471E-02*V(J))**0.6666667) @ CALC AREA X01.00A  000124
00152 49*      B=B+((ASCH(J)+C)*(T(J)-D)*(S+E))/R @ UN-NORMALIZED HEAT EXCHANGE X01.00A  000140
00153 50* 131  CONTINUE @ X01.00A  000162
00155 51*      B=B*0.25*GDAST @ NORMALIZE HEAT EXCHANGE X01.00A  000162
00156 52*      CALL STS (I1,5,B) @ SAVE IN SCRATCH AREA X01.00A  000166
00157 53*      CALL CHKTIH (IL,IH,I1) @ KEEP AN EYE ON THE TIME X01.00A  000173
00160 54* 135  CONTINUE @ X01.00A  000203
00162 55* 136  RETURN @ X01.00A  000203
00163 56*      END @ X01.00A  000242
END FOR
>

```

Listing 13.—Concluded.

```

@FOR,MS CASPER5.WRKFGD
FOR 4R1 E -04/13/84-15:53:01 (1,)
>@EOF

```

```

SUBROUTINE WRKFLG ENTRY POINT 000106

```

```

STORAGE USED: CODE(1) 000125; DATA(0) 000020; BLANK COMMON(2) 000000

```

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

```

0003 STAT
0004 CHKLH
0005 CHKTIM
0006 S
0007 ACWDT
0010 ASCV
0011 GDACT
0012 STT
0013 NERR3$

```

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

```

0001 000054 107L 0001 000075 110L 0001 000017 113G 0007 R 000000 ACWDT 0010 R 000000 ASCV
0000 R 000000 B 0011 R 000000 GDACT 0000 000007 INJP$ 0000 I 000001 IS 0000 I 000002 I1
0006 R 000000 S 0003 I 000000 STAT

```

```

00101 1* SUBROUTINE WRKFLG (IL,IH,GDAST) 000000
00101 2* C+ 000000
00101 3* C 000000
00101 4* C WRKFLG ***** A SUBROUTINE FOR CASPER ***** 000000
00101 5* C AUTHOR WILLIAM HENRY JONES 000000
00101 6* C V01-00 12 FEB 80 000000
00101 7* C V01-00A 15 SEP 80 FUNCTION TYPE STATEMENT 000000
00101 8* C 000000
00101 9* C 000000
00101 10* C DESCRIPTION ***** 000000
00101 11* C 000000
00101 12* C THIS ROUTINE REVISES THE CURRENT TEMPERATURE OF EACH ELEMENT 000000
00101 13* C IN THE RANGE 'IL' TO 'IH' BASED ON THE FOLLOWING INFORMATION: 000000
00101 14* C 1) THE CURRENT TEMPERATURE COPY IN GDACT, 2) THE POWER OF 000000
00101 15* C COMPRESSION IN ACWDT, 3) THE VISCOUS DISTORTION WORK IN 000000
00101 16* C S(4), AND 4) THE HEAT TRANSFERED BY CONDUCTION IN S(5). 000000
00101 17* C 000000
00101 18* C 000000
00101 19* C- 000000
00103 20* PARAMETER DURID=507 000000
00104 21* INTEGER STAT 000000
00105 22* REAL B 000000
00106 23* CALL CHKLH (IL,IH,IS,DURID,1) @ CHECK RANGE LIMITS 000000
00107 24* IF (IS) 102,110,102 @ VALID RANGE ? 000006
00112 25* 102 DO 109 I1=IL,IH,IS @ YES, USE IT 000010
00115 26* CALL CHKTIM (IL,IH,I1) @ KEEP AN EYE ON THE TIME 000017
00116 27* B=S(I1,4)+S(I1,5) @ DISTORTION + CONDUCTION 000024
00117 28* IF (AND(STAT(I1),2**2)) 107,106,107 @ IS THERE A COMPRESSION TERM? 000037
00122 29* 106 B=B+GDAST*ACWDT(I1) @ YES, CONVERT IT TO WORK 000045
00123 30* 107 B=(B/ASCV(I1))+GDACT(I1) @ CONVERT TO TEMPERATURE 000054
00124 31* CALL STT (I1,B) @ REVISE ELEMENT'S TEMP 000066
00125 32* 109 CONTINUE @ 000075
00127 33* 110 RETURN @ 000075
00130 34* END @ 000124
END FOR
>

```

```

@FOR,MS CASPER1.VOLD
FOR 4R1 E -04/17/84-12:49:01 (5,)
>@EOF

```

```

SUBROUTINE VOL ENTRY POINT 001017

```

```

STORAGE USED: CODE(1) 001040; DATA(0) 000145; BLANK COMMON(2) 000000

```

```

COMMON BLOCKS:

```

```

0003 ISIZEC 000001

```

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

```

0004 STAT
0005 CHKLH
0006 SPSHI
0007 PAAI
0010 SPSHR
0011 REQSFA
0012 SPOPI
0013 ERROR2
0014 X
0015 NEI
0016 NORMM
0017 CROSS
0020 NORM
0021 DOT
0022 CROSSM
0023 ABSARC
0024 STV
0025 CHKTIM
0026 NERR2*
0027 ACOS
0030 TAN
0031 SIN
0032 SQRT
0033 COS
0034 ASIN
0035 EXP
0036 NERR3*

```

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

```

0001 000110 101L      0001 000250 118L      0001 000307 126L      0001 000021 15L       0001 000112 154G
0001 000125 161G      0001 000135 165G      0001 000030 17L       0001 000153 174G      0001 000175 203G
0001 000217 211G      0001 000053 22L       0001 000263 226G      0001 000267 232G      0001 000322 245G
0001 000331 254G      0001 000526 255L      0001 000342 260G      0001 000550 260L      0001 000352 267G
0001 000073 27L       0001 000572 275L      0001 000716 300L      0001 000721 600L      0001 000771 707L
0000 R 000104 A        0000 R 000103 ARNM      0000 R 000102 AROM      0000 R 000101 B        0000 R 000100 C
0000 R 000070 CD       0000 R 000061 CURAV      0000 I 000063 I        0000 I 000056 ID       0000 I 000057 IE
0000 I 000074 IJK      0000 000131 INJP*        0000 R 000001 IPAV      0000 I 000055 IS       0000 I 000050 ISEN
0003 000000 ISIZE      0000 I 000060 ISW        0000 I 000062 I1       0000 I 000064 J        0000 I 000065 K
0000 I 000076 M        0000 I 000000 MIN      0000 I 000075 N        0015 I 000000 NEI      0000 R 000073 OM
0000 R 000005 P        0000 R 000077 PHI1      0000 R 000067 R        0000 R 000066 RAD      0000 R 000105 RRR
0000 R 000071 SI       0004 I 000000 STAT      0000 R 000072 TH       0000 R 000043 THETA    0014 R 000000 X
0000 R 000002 XL       0000 R 000024 Z

```

```

00101 1*          SUBROUTINE VOL (IL,IH,PAV,ACAV)          115A0010 000000
00101 2*          C          11500020 000000
00101 3*          C          11500030 000000
00101 4*          C          VOL          ***** A SUBROUTINE FOR CASPER ***** 11500040 000000
00101 5*          C          AUTHOR          WILLIAM HENRY JONES          11500050 000000
00101 6*          C          V01-00          06 APR 78          11500060 000000
00101 7*          C          V01-01          30 AUG 78          11510061 000000

```

Listing 15.—Subroutine VOL.

00101	8*	C	V01-01A	06 FEB 79		115A0062	000000	
00101	9*	C	V01-01B	08 FEB 80	PAX PROTOCOL ADJUSTMENTS		000000	
00101	10*	C	V01-01C	15 SEP 80	FUNCTION TYPE STATEMENT		000000	
00101	11*	C	V01-01D	20 APR 83	LITTLE FIXES	V01-01D	000000	
00101	12*	C	V01-01E	29 APR 83	LITTLE TYPO	V01-01E	000000	
00101	13*	C				11500070	000000	
00101	14*	C	ARGUMENTS IN CASPER 'CACHE' MEMORY *****				11510074	000000
00101	15*	C				11510076	000000	
00101	16*	C	ARGUMENT	TYPE	DIMENSION	DESCRIPTION	11500080	
00101	17*	C	-----	-----	-----	-----	11510090	
00101	18*	C	X	REAL	1 TO ISIZE	AEROELEMENT POSITIONS	11500100	
00101	19*	C			1 TO 3		11500110	
00101	20*	C					11500120	
00101	21*	C	NEI	INTEGER	1 TO ISIZE	NEAREST NEIGHBOR LIST	11500130	
00101	22*	C			1 TO 5		11500140	
00101	23*	C					11500150	
00101	24*	C	V	REAL	1 TO ISIZE	AEROELEMENT VOLUMES	11510160	
00101	25*	C				-- THESE WILL BE REPLACED	11500170	
00101	26*	C				WITH ADJUSTED VOLUME	11500180	
00101	27*	C				ESTIMATES	11500190	
00101	28*	C	STAT	INTEGER	1 TO ISIZE	AEROELEMENT STATUS LIST	11510192	
00101	29*	C					11510194	
00101	30*	C					11500200	
00101	31*	C					11510202	
00101	32*	C	ARGUMENTS PASSED IN SUBROUTINE CALL *****				11510203	000000
00101	33*	C					11510204	
00101	34*	C	ARGUMENT	TYPE	DIMENSION	DESCRIPTION	11510205	
00101	35*	C	-----	-----	-----	-----	11510206	
00101	36*	C	IL	INTEGER	SCALAR	LOW AEROELEMENT ID LIMIT	115A0210	
00101	37*	C					115A0212	
00101	38*	C	IH	INTEGER	SCALAR	HIGH AEROELEMENT ID LIMIT	115A0214	
00101	39*	C					115A0216	
00101	40*	C	PAV	REAL	SCALAR	PREVIOUS AEROELEMENT SOLID	115A0218	
00101	41*	C				ANGLE AVERAGE	115A0220	
00101	42*	C					115A0222	
00101	43*	C	ACAV	REAL	SCALAR	ACCUMULATION SLOT FOR ALL	115A0224	
00101	44*	C				SOLID ANGLES CALCULATED	115A0226	
00101	45*	C				BY THE EXECUTION OF THIS	115A0228	
00101	46*	C				ROUTINE	115A0230	
00101	47*	C					11500250	
00101	48*	C					11500260	
00101	49*	C					11500270	
00101	50*	C	DESCRIPTION				11500280	000000
00101	51*	C					11500290	
00101	52*	C	THIS ROUTINE CALCULATES NEW ESTIMATED VOLUMES FOR ALL AEROELEMENTS				11500300	000000
00101	53*	C	ACCORDING TO FIXED RULES, THE VOLUME ESTIMATES WILL NOT (IN ALL				11500310	000000
00101	54*	C	PROBABILITY) ADD UP TO EQUAL THE TOTAL VOLUME OF THE PROBLEM AND				11500320	000000
00101	55*	C	MUST BE ADJUSTED FOR THIS OUTSIDE THIS ROUTINE.				11500330	000000
00101	56*	C					11500340	
00101	57*	C	THE VOLUMES CALCULATED BY THIS ROUTINE ARE BASED ON A SPHERE				11500350	000000
00101	58*	C	WHOSE RADIUS IS EQUAL TO THE AVERAGE DISTANCE TO THE AEROELEMENT'S				11500360	000000
00101	59*	C	FIVE NEAREST NEIGHBORS, THIS ESTIMATE IS ADJUSTED BY THE SOLID				11500370	000000
00101	60*	C	ANGLE SUBTENDED BY THE FIVE NEAREST NEIGHBORS, THE ADJUSTMENT				11500380	000000
00101	61*	C	GIVES MORE VOLUME TO AEROELEMENTS WHOSE SOLID ANGLE RESULTS ARE				11500390	000000
00101	62*	C	LESS THAN AVERAGE.				11500400	000000
00101	63*	C					11510401	
00101	64*	C	IF A PARTICULAR AEROELEMENT IS IDENTIFIED AS A 'BOUNDARY'				11510402	000000
00101	65*	C	AEROELEMENT (BIT #11 OF STATUS WORD SET) THE FOLLOWING				11510403	000000
00101	66*	C	ADJUSTMENTS ARE MADE. ITS SOLID ANGLE RESULT WILL AUTOMATICALLY				11510404	000000
00101	67*	C	BE DOUBLED (SINCE IT HAS ONLY HALF A HORIZON FOR NEIGHBORS)				11510405	000000
00101	68*	C	AND ITS VOLUME ESTIMATE IS HALVED (SINCE IT HAS ONLY HALF A				11510406	000000
00101	69*	C	SPHERE TO RESIDE IN, THIS PUTS BOUNDARY ELEMENTS ON EQUAL				11510407	000000
00101	70*	C	FOOTING WITH NORMAL ELEMENTS PROVIDED THE BOUNDARY IS QUASI-				11510408	000000
00101	71*	C	FLAT AT THE BOUNDARY ELEMENT SITE WHEN VIEWED IN THE SCALE				11510409	000000
00101	72*	C	OF THE BOUNDARY ELEMENT.				11510410	000000
00101	73*	C					11510411	
00101	74*	C	DURING THE EXECUTION OF THE SUBROUTINE THE SUM OF ALL SOLID				115A0420	000000
00101	75*	C	ANGLES CALCULATED (FOR AEROELEMENTS IN THE RANGE 'IL' TO 'IH')				115A0425	000000
00101	76*	C	IS ACCUMULATED, ON EXIT THE SUM IS LOADED INTO SLOT 'ACAV'				115A0430	000000
00101	77*	C	TO AID THE CALLER IN MAKING ANY NECESSARY ADJUSTMENTS IN 'PAV'.				115A0435	000000
00101	78*	C					11500450	
00101	79*	C					11500460	

```

00101 80* C
00101 81* C THE CALCULATION OF SOLID ANGLE 11500470 000000
00101 82* C V01-01D 000000
00101 83* C V01-01D 000000
00101 84* C THE SOLID ANGLE SUBTENDED BY THE FIVE NEAREST NEIGHBORS IS V01-01D 000000
00101 85* C CALCULATED BY SUMMING THE CONTRIBUTIONS OF SPHERICAL TRIANGLES. V01-01D 000000
00101 86* C THREE SPHERICAL TRIANGLES ARE IDENTIFIED: ONE SUBTENDED BY V01-01D 000000
00101 87* C NEIGHBORS 1, 2, AND 3; ONE SUBTENDED BY NEIGHBORS 1, 3, AND V01-01D 000000
00101 88* C 4, AND ONE SUBTENDED BY NEIGHBORS 1, 4, AND 5. THE SPHERICAL V01-01D 000000
00101 89* C TRIANGLES ARE PROJECTED ONTO A SPHERE OF UNIT RADIUS AND ARE V01-01D 000000
00101 90* C IDENTIFIED THROUGH A NEAREST NEIGHBOR LIST THAT HAS BEEN RE- V01-01D 000000
00101 91* C ORDERED TO MAKE A MONOTONICALLY INCREASING ORIENTATION OF NEIGH- V01-01D 000000
00101 92* C BORS WHEN VIEWED FROM A POLE ESTABLISHED BY THE FIRST NEIGHBOR. V01-01D 000000
00101 93* C THE AREA OF EACH SPHERICAL TRIANGLE IS ESTABLISHED BY DECOM- V01-01D 000000
00101 94* C POSING IT INTO TWO SPHERICAL RIGHT TRIANGLES. IT CAN BE SHOWN V01-01D 000000
00101 95* C THAT THE AREA OF A SPHERICAL RIGHT TRIANGLE OF BASE THETA.1 AND V01-01D 000000
00101 96* C HEIGHT PHI.1 IS THE INTEGRAL V01-01D 000000
00101 97* C
00101 98* C 
$$\text{AREA} = \int_0^{\text{THETA.1}} \frac{A * \text{SIN}(\text{THETA})}{\sqrt{1 + (A * \text{SIN}(\text{THETA}))^2}} D.\text{THETA}$$
 V01-01D 000000
00101 99* C V01-01D 000000
00101 100* C V01-01D 000000
00101 101* C V01-01D 000000
00101 102* C 
$$\text{WHERE } A = \frac{\text{TAN}(\text{PHI.1})}{\text{SIN}(\text{THETA.1})}$$
 V01-01D 000000
00101 103* C V01-01D 000000
00101 104* C V01-01D 000000
00101 105* C V01-01D 000000
00101 106* C V01-01D 000000
00101 107* C THIS CAN BE INTEGRATED BY THE SUBSTITUTION V01-01D 000000
00101 108* C V01-01D 000000
00101 109* C 
$$X = B * \text{COS}(\text{THETA})$$
 V01-01D 000000
00101 110* C V01-01D 000000
00101 111* C 
$$\text{WHERE } B = \sqrt{(A^2) / (1 + (A^2))}$$
 V01-01D 000000
00101 112* C V01-01D 000000
00101 113* C V01-01D 000000
00101 114* C THIS INTEGRATION GIVES THE RESULT V01-01D 000000
00101 115* C V01-01D 000000
00101 116* C 
$$\text{AREA} = \text{ASIN}(B) - \text{ASIN}(B * \text{COS}(\text{THETA.1}))$$
 V01-01D 000000
00101 117* C V01-01D 000000
00101 118* C V01-01D 000000
00101 119* C AN ANOMALLY OF COMPUTATION EXISTS AS PHI.1 APPROACHES PI/2. V01-01D 000000
00101 120* C IN THIS EVENT, B IS SET TO THE LIMIT OF 1.0. ALTHOUGH A TENDS V01-01D 000000
00101 121* C TO INFINITY AS THETA.1 TENDS TO PI, A COMPUTATIONAL ANOMALLY IS V01-01D 000000
00101 122* C AVOIDED BY CALCULATING B AS V01-01D 000000
00101 123* C V01-01D 000000
00101 124* C 
$$B = \sqrt{\left( \frac{\text{TAN}(\text{PHI.1})^2}{(\text{SIN}(\text{THETA.1})^2) + (\text{TAN}(\text{PHI.1})^2)} \right)}$$
 V01-01D 000000
00101 125* C V01-01D 000000
00101 126* C V01-01D 000000
00101 127* C V01-01D 000000
00101 128* C V01-01D 000000
00101 129* C V01-01D 000000
00101 130* C THE CALCULATION OF A SPHERICAL TRIANGLE PROCEEDS IN THE FOLLOWING V01-01D 000000
00101 131* C MANNER. V01-01D 000000
00101 132* C V01-01D 000000
00101 133* C 1. A VECTOR TO THE FIRST NEIGHBOR, V.N1, IS ESTABLISHED. THIS V01-01D 000000
00101 134* C VECTOR DEFINES AN ARBITRARY X' AXIS AND THE LOCATION OF AN V01-01D 000000
00101 135* C ARBITRARY 0 LONGITUDE, 0 LATITUDE POINT ON THE UNIT SPHERE. V01-01D 000000
00101 136* C V01-01D 000000
00101 137* C 2. A VECTOR TO NEIGHBOR N (N=2, 3, 4), V.NN, IS ESTABLISHED. V01-01D 000000
00101 138* C V01-01D 000000
00101 139* C 3. A NORTH POLE (Z' AXIS) IS ESTABLISHED AS V01-01D 000000
00101 140* C V01-01D 000000
00101 141* C 
$$V.NP = \frac{V.N1 \times V.NN}{\text{MAG}(V.N1 \times V.NN)}$$
 V01-01D 000000
00101 142* C V01-01D 000000
00101 143* C V01-01D 000000
00101 144* C V01-01D 000000
00101 145* C 4. THE EAST LONGITUDE OF NEIGHBOR N IS ESTABLISHED AS V01-01D 000000
00101 146* C V01-01D 000000
00101 147* C 
$$\text{THETA.N} = \text{ACOS}(V.N1 \cdot V.NN)$$
 V01-01D 000000
00101 148* C V01-01D 000000
00101 149* C 5. A VECTOR TO NEIGHBOR M (M=N+1), V.NM, IS ESTABLISHED. V01-01D 000000
00101 150* C V01-01D 000000
00101 151* C 6. THE HEIGHT OF THE SPHERICAL TRIANGLES IS ESTABLISHED AS V01-01D 000000

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Listing 15.—Continued.

00101	152*	C			V01-01D	000000
00101	153*	C		PSI.1 = ACOS (V.NP * V.NM)	V01-01D	000000
00101	154*	C		PHI.1 = ABS (PI/2 - PSI.1)	V01-01D	000000
00101	155*	C			V01-01D	000000
00101	156*	C	7.	THE VECTOR TO NEIGHBOR M IS PROJECTED INTO THE EQUATORIAL	V01-01D	000000
00101	157*	C		(X-Y) PLANE AS	V01-01D	000000
00101	158*	C			V01-01D	000000
00101	159*	C		V.EM = V.NP X (V.NM X V.NP)	V01-01D	000000
00101	160*	C			V01-01D	000000
00101	161*	C		AND IS NORMALIZED.	V01-01D	000000
00101	162*	C			V01-01D	000000
00101	163*	C	8.	THE LENGTH OF A RIGHT SPHERICAL TRIANGLE (WHOSE BASE IS THE	V01-01D	000000
00101	164*	C		EQUATOR) RUNNING FROM 0 LONGITUDE TO NEIGHBOR M IS FOUND AS	V01-01D	000000
00101	165*	C			V01-01D	000000
00101	166*	C		THETA.M = ACOS (V.N1 * V.EM)	V01-01D	000000
00101	167*	C			V01-01D	000000
00101	168*	C	9.	THE LENGTH OF A RIGHT SPHERICAL TRIANGLE (WHOSE BASE IS THE	V01-01D	000000
00101	169*	C		EQUATOR) RUNNING FROM NEIGHBOR N TO NEIGHBOR M IS FOUND AS	V01-01D	000000
00101	170*	C			V01-01D	000000
00101	171*	C		THETA.NM = ACOS (V.EM * V.NN)	V01-01D	000000
00101	172*	C			V01-01D	000000
00101	173*	C	10.	THE SENSE OF THE ROTATIONS FROM 0 LONGITUDE TO NEIGHBOR N,	V01-01D	000000
00101	174*	C		FROM 0 LONGITUDE TO NEIGHBOR M, AND FROM NEIGHBOR N TO	V01-01D	000000
00101	175*	C		NEIGHBOR M IS ESTABLISHED AS	V01-01D	000000
00101	176*	C			V01-01D	000000
00101	177*	C		SENSE.ON = SIGN (V.NP * (V.N1 X V.NN))	V01-01D	000000
00101	178*	C		SENSE.OM = SIGN (V.NP * (V.N1 X V.EM))	V01-01D	000000
00101	179*	C		SENSE.NM = SIGN (V.NP * (V.NN X V.EM))	V01-01D	000000
00101	180*	C			V01-01D	000000
00101	181*	C	11.	THE AREA (SOLID ANGLE) OF TWO SPHERICAL RIGHT TRIANGLES IS	V01-01D	000000
00101	182*	C		CALCULATED USING THE FORMULATION PREVIOUSLY DESCRIBED. THE	V01-01D	000000
00101	183*	C		FIRST TRIANGLE RUNS FROM 0 LONGITUDE TO NEIGHBOR M AND THE	V01-01D	000000
00101	184*	C		SECOND TRIANGLE RUNS FROM NEIGHBOR N TO NEIGHBOR M. THE	V01-01D	000000
00101	185*	C		BASE OF EACH TRIANGLE RUNS ALONG THE EQUATOR. THUS,	V01-01D	000000
00101	186*	C			V01-01D	000000
00101	187*	C		AR.OM = AREA (THETA.M, PHI.1)	V01-01D	000000
00101	188*	C		AR.NM = AREA (THETA.NM, PHI.1)	V01-01D	000000
00101	189*	C			V01-01D	000000
00101	190*	C	12.	THE SOLID ANGLE CONTRIBUTION SUBTENDED BY NEIGHBORS N AND	V01-01D	000000
00101	191*	C		M IS CALCULATED ACCORDING TO THE FOLLOWING RULES.	V01-01D	000000
00101	192*	C			V01-01D	000000
00101	193*	C		IF SENSE.OM AND SENSE.NM ARE OF THE SAME SIGN, THEN	V01-01D	000000
00101	194*	C			V01-01D	000000
00101	195*	C		ANGLE = ABS (AR.OM - AR.NM)	V01-01D	000000
00101	196*	C			V01-01D	000000
00101	197*	C		ELSE	V01-01D	000000
00101	198*	C			V01-01D	000000
00101	199*	C		IF SENSE.ON AND SENSE.NM ARE OF THE SAME SIGN, THEN	V01-01D	000000
00101	200*	C			V01-01D	000000
00101	201*	C		ANGLE = ABS (2*PI - (AR.OM + AR.NM))	V01-01D	000000
00101	202*	C			V01-01D	000000
00101	203*	C		ELSE	V01-01D	000000
00101	204*	C			V01-01D	000000
00101	205*	C		ANGLE = ABS (AR.OM + AR.NM)	V01-01D	000000
00101	206*	C			V01-01D	000000
00101	207*	C		END. IF	V01-01D	000000
00101	208*	C			V01-01D	000000
00101	209*	C		END. IF	V01-01D	000000
00101	210*	C			V01-01D	000000
00101	211*	C			V01-01D	000000
00101	212*	C			V01-01D	000000
00101	213*	C			V01-01D	000000
00101	214*	C			V01-01D	000000
00101	215*	C		REQUIRED SUBROUTINES	11500480	000000
00101	216*	C			11500490	000000
00101	217*	C	010	ABSARC	11500500	000000
00101	218*	C	020	CROSSM	11500510	000000
00101	219*	C	021	CROSSM	11500520	000000
00101	220*	C	023	DOT1	11500530	000000
00101	221*	C	025	NORM1M	11500540	000000
00101	222*	C			11500550	000000
00101	223*	C			11500560	000000

00101	224*	C			11500570	000000
00101	225*	C	ERRORS		11500580	000000
00101	226*	C			11500590	000000
00101	227*	C	NONE		11500600	000000
00101	228*	C			11500610	000000
00101	229*	C			11500620	000000
00101	230*	C			11500630	000000
00103	231*		COMMON /ISIZEC/ISIZE		11500640	000000
00104	232*		REAL PAV,ACAV		115A0680	000000
00105	233*		REAL IPAV	@	V01-01D	000000
00106	234*		REAL XL(3)	@	V01-01D	000000
00107	235*		REAL P(3,5)	@	V01-01D	000000
00110	236*		REAL Z(3,5)	@	V01-01D	000000
00111	237*		REAL THETA(5)	@	V01-01D	000000
00112	238*		INTEGER ISEN(5)	@ ROTATION SENSE VALUES	V01-01D	000000
00113	239*		INTEGER IL,IH,IS,ID,IE		115A0682	000000
00114	240*		INTEGER STAT			000000
00115	241*		DATA ID/115/		115A0684	000000
00117	242*		DATA IE/1/		115A0686	000000
00121	243*		ISW=1	@ INTERNAL RETURN SWITCH	11500710	000000
00122	244*		CURAV=0.0	@ NEXT AVERAGE ACCUMULATOR	11500720	000001
00123	245*		IPAV=1.0/PAV	@ FAST DIVIDES	11500730	000002
00124	246*		CALL CHKLH (IL,IH,IS,ID,IE)	@ GO CHECK ID RANGE	115A0740	000005
00125	247*		IF (IS) 14,17,14	@ VALID ID RANGE ?	115A0745	000014
00130	248*	14	I1=IL-IS	@ YES, INIT ID DO LOOP	115A0750	000016
00131	249*	15	I1=I1+IS	@ NEXT AEROELEMENT ID	115A0755	000021
00132	250*		IF (IS*(I1-IH)) 101,101,17	@ END OF LOOP YET ?	115A0760	000023
00135	251*	17	ACAV=CURAV	@ YES, END OF ROUTINE	115A0765	000030
00136	252*		CALL SPSHI (0)	@ END-OF-ARGUMENTS FOR SAF		000031
00137	253*		CALL SPSHI (0)	@ REQUEST		000034
00140	254*		CALL PAAI (4,I)	@ PAX SUPPLIED ACCUMULATOR		000037
00141	255*		GO TO (22,27),I	@ IS IT NON-LITERAL ?		000043
00142	256*	22	CALL SPSHR (CURAV)	@ YES, SEND OUR SUB-TOTAL		000053
00143	257*		CALL SPSHI (1)	@		000055
00144	258*		CALL SPSHI (7)	@ LENGTH OF PACKAGE		000060
00145	259*		CALL REQSAF (115,1)	@ ASK FOR OUR ONLY SAF		000063
00146	260*		RETURN	@ DONE		000067
00147	261*	27	CALL SPOPI (I)	@ OOPS, PAX MUST GIVE A		000073
00150	262*		CALL SPOPI (I)	@ NON-LITERAL		000075
00151	263*		CALL ERROR2 (115,5)	@		000100
00152	264*		RETURN	@	115A0770	000104
00152	265*	C			11500790	000104
00152	266*	C	ENTRY TO VOLUME, SOLID ANGLE CALCULATOR		11500800	000104
00152	267*	C			11500810	000104
00152	268*	C	I1 MUST BE A LEGAL AEROELEMENT ID.		11500820	000104
00152	269*	C	ISW MUST BE A LEGAL INTERNAL JUMP SWITCH.		11500830	000104
00152	270*	C	IPAV MUST BE THE AVERAGE (DATUM) SOLID ANGLE INVERSE.		11500840	000104
00152	271*	C			11500850	000104
00152	272*	C			11500860	000104
00153	273*	101	DO 102 I=1,3	@ PICKUP TARGET ELEMENT'S	V01-01D	000112
00156	274*	102	XL(I)=X(I1,I)	@ POSITION IN SPACE	V01-01D	000112
00160	275*		DO 104 I=1,5	@ MAKE AND SAVE VECTORS TO	V01-01D	000125
00163	276*		J=NEI(I1,I)	@ NEAREST NEIGHBORS REFERENCE	11500880	000125
00164	277*		DO 104 K=1,3	@ TO BASE AEROELEMENT	11500890	000135
00167	278*	104	P(K,I)=X(J,K)-XL(K)	@	V01-01D	000135
00172	279*		RAD=0.0	@	11500910	000147
00173	280*		DO 108 I=1,5	@ NORMALIZE VECTORS, ACCUM	11500920	000153
00176	281*		CALL NORHM (P(1,I),R)	@ MAGNITUDES	V01-01E	000153
00177	282*	108	RAD=RAD+R	@	11500940	000160
00201	283*		RAD=4.1887902*(0.5*RAD)**3	@ CALC VOLUME ESTIMATE	V01-01D	000164
00201	284*	C			11500960	000164
00201	285*	C	NON-FOLDBACK ORDERING STARTS HERE		11500970	000164
00201	286*	C			11500980	000164
00202	287*		DO 112 I=2,5	@ CREATE THE ORDERING	11500990	000175
00205	288*		CALL CROSS (P(1,I),P(1,I),Z(1,I))	@ VECTORS AND NORMALIZE	V01-01D	000175
00206	289*	112	CALL NORH (Z(1,I))	@ THEM	V01-01D	000205
00210	290*		DO 119 I=3,5	@ CALCULATE RELATIVE ROTATIONS	11501010	000217
00213	291*		CALL DOT (Z(1,2),Z(1,I),CO)	@ OF Z3 TO Z5 REFERENCED TO	V01-01D	000217
00214	292*		CALL CROSSM (Z(1,2),Z(1,I),Z(1,1),SI)	@ Z2 AND STORE IN THETA	V01-01D	000225
00215	293*		CALL DOT (P(1,1),Z(1,1),TH)	@	V01-01D	000235
00216	294*		IF (TH) ,118,118	@	11501050	000242
00221	295*		SI=-SI	@	11501060	000245
00222	296*	118	CALL ABSARC (TH,SI,CO)	@	11501070	000250
00223	297*	119	THETA(I)=TH	@	11501080	000254
00225	298*		DO 130 I=1,3	@ REORDER VECTORS IN INCREASE	-11501090	000263
00230	299*		MIN=10000.0	@ ING VALUES OF THETA BY A	11501100	000263
00231	300*		DO 126 J=3,5	@ SIMPLE MINIMUM SEARCH	11501110	000267
00234	301*		IF (THETA(J)-MIN) , ,126	@	11501120	000267
00237	302*		MIN=THETA(J)	@	11501130	000275
00240	303*		K=J	@	11501140	000304
00241	304*	126	CONTINUE	@	11501150	000310
00243	305*		THETA(K)=10001.0	@ DON'T PICK THIS AGAIN	11501160	000310

Listing 15.—Continued.


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00244 306* DO 129 J=1,3 @ TRANSFER THE VECTOR 11501170 000313
00247 307* 129 Z(J,I)=F(J,K) @ 001-01D 000322
00251 308* 130 CONTINUE @ 11501190 000331
00253 309* DO 134 I=1,3 @ PUT VECTORS BACK IN NEW 11501200 000331
00256 310* K=I+2 @ ORDER 11501210 000331
00257 311* DO 134 J=1,3 @ 11501220 000334
00262 312* 134 P(J,K)=Z(J,I) @ 001-01D 000342
00262 313* C 11501240 000342
00262 314* C THIS SECTION CALCULATES THE SOLID ANGLE, OM, SUBTENDED BY THE 11501250 000342
00262 315* C FIVE NEAREST NEIGHBORS. THE FIRST NEAREST NEIGHBOR IS USED AS 11501260 000342
00262 316* C A POLE POSITION. 11501270 000342
00262 317* C 11501280 000342
00265 318* OM=0.0 @ SEE TEXT FOR THEORY 11501290 000346
00266 319* DO 600 IJK=2,4 @ ACCUMULATE SOLID ANGLE 001-01D 000352
00271 320* N=IJK @ CONTRIBUTION FROM EACH OF 001-01D 000352
00272 321* M=IJK+1 @ THREE SPHERICAL TRIANGLES 001-01D 000354
00273 322* CALL CROSS (P(1,1),P(1,N),Z(1,1)) @ ESTABLISH A NORMALIZED 001-01D 000356
00274 323* CALL NORM (Z(1,1)) @ NORTH POLE IN Z,1 001-01D 000370
00275 324* CALL DOT (P(1,1),P(1,N),CO) @ CALCULATE EAST LONGITUDE 001-01D 000373
00276 325* THETA(N)=ACOS(CO) @ OF NEIGHBOR N 001-01D 000403
00277 326* CALL DOT (Z(1,1),P(1,M),CO) @ CALCULATE THE HEIGHT OF THE 001-01D 000410
00300 327* PHI1=ABS(1.5707963-ACOS(CO)) @ SPHERICAL TRIANGLES 001-01D 000422
00301 328* IF (ABS(PHI1-1.5707963)-1.0E-03) 500,500,225 @ ANOMALLY ? 001-01D 000430
00304 329* 225 CALL CROSS (P(1,M),Z(1,1),Z(1,5)) @ NO, PROJECT VECTOR TO 001-01D 000435
00305 330* CALL CROSS (Z(1,1),Z(1,5),Z(1,2)) @ NEIGHBOR M INTO EQUATORIAL 001-01D 000445
00306 331* CALL NORM (Z(1,2)) @ PLANE AND NORMALIZE IT 001-01D 000452
00307 332* CALL DOT (P(1,1),Z(1,2),CO) @ LONGITUDE (EAST OR WEST) OF 001-01D 000455
00310 333* THETA(M)=ACOS(CO) @ NEIGHBOR M 001-01D 000462
00311 334* CALL DOT (P(1,N),Z(1,2),CO) @ LONGITUDE FROM NEIGHBOR N 001-01D 000467
00312 335* THETA(1)=ACOS(CO) @ TO NEIGHBOR M 001-01D 000476
00313 336* ISEN(1)=1 @ ESTABLISH ROTATIONAL SENSE 001-01D 000502
00314 337* CALL CROSS (P(1,N),Z(1,2),Z(1,4)) @ FROM NEIGHBOR N TO 001-01D 000504
00315 338* CALL DOT (Z(1,1),Z(1,4),CO) @ NEIGHBOR M 001-01D 000513
00316 339* IF (CO) 254,255,255 @ 001-01D 000520
00321 340* 254 ISEN(1)=-1 @ 001-01D 000523
00322 341* 255 ISEN(N)=1 @ ESTABLISH ROTATIONAL SENSE 001-01D 000526
00323 342* CALL CROSS (P(1,1),P(1,2),Z(1,4)) @ FROM 0 LONGITUDE TO 001-01D 000530
00324 343* CALL DOT (Z(1,1),Z(1,4),CO) @ NEIGHBOR N 001-01D 000535
00325 344* IF (CO) 259,260,260 @ 001-01D 000542
00330 345* 259 ISEN(N)=-1 @ 001-01D 000545
00331 346* 260 ISEN(M)=1 @ ESTABLISH ROTATIONAL SENSE 001-01D 000550
00332 347* CALL CROSS (P(1,1),Z(1,2),Z(1,4)) @ FROM 0 LONGITUDE TO 001-01D 000552
00333 348* CALL DOT (Z(1,1),Z(1,4),CO) @ NEIGHBOR M 001-01D 000557
00334 349* IF (CO) 264,275,275 @ 001-01D 000564
00337 350* 264 ISEN(M)=-1 @ 001-01D 000567
00340 351* 275 C=(TAN(PHI1))**2 @ COMMON TO BOTH TRIANGLES 001-01D 000572
00341 352* B=SQRT(C/((SIN(THETA(M))**2)+C)) @ AREA FROM 0 LONGITUDE TO 001-01D 000576
00342 353* AROM=ABS(ASIN(B)-ASIN(B*COS(THETA(M)))) @ NEIGHBOR M 001-01D 000615
00343 354* B=SQRT(C/((SIN(THETA(1))**2)+C)) @ AREA FROM NEIGHBOR N TO 001-01D 000636
00344 355* ARNM=ABS(ASIN(B)-ASIN(B*COS(THETA(1)))) @ NEIGHBOR M 001-01D 000652
00345 356* A=ABS(AROM-ARNM) @ ASSUME SIMPLEST CASE 001-01D 000671
00346 357* IF (ISEN(1)*ISEN(M)) 302,600,600 @ GOOD ASSUMPTION ? 001-01D 000674
00351 358* 302 A=ABS(AROM+ARNM) @ NO, WE WILL NEED THIS 001-01D 000700
00352 359* IF (ISEN(1)*ISEN(N)) 600,304,304 @ GOING OVER THE POLE ? 001-01D 000704
00355 360* 304 A=ABS(6.2831854-A) @ YES, WE CALC'D COMPLEMENT 001-01D 000711
00356 361* GO TO 600 @ JOIN AFTER ANOMALLY HANDLER 001-01D 000714
00357 362* 500 A=ABS(THETA(N)) @ PROPORTION OF HEMISPHERE 001-01D 000716
00360 363* 600 OM=OM+A @ ACCUMULATE SOLID ANGLE 001-01D 000721
00360 364* C 11501580 000721
00360 365* C ACCUMULATE AVERAGE AND STORE REVISED VOLUME ESTIMATE 11501590 000721
00360 366* C 11501600 000721
00362 367* OM=ABS(OM) @ RECOGNIZE ALWAYS POSITIVE 11501610 000725
00363 368* CURAV=CURAV+OM @ ACCUM AVERAGE FOR NEXT TIME 11501620 000727
00364 369* RRR=RAD*EXP(1.0-OM*IPAV) @ ADJUST VOLUME BY HORIZON 11511630 000731
00365 370* IF (AND(STAT(I1),2048)) 704,707,704 @ BR IF NOT BOUNDARY ELEMENT 001-01D 000742
00370 371* 704 CURAV=CURAV+OM @ PUT BOUNDARY ELEMENTS ON 001-01D 000750
00371 372* OM=OM+OM @ EQUAL TERMS 11511636 000753
00372 373* RRR=0.5*RRR*EXP(1.0-OM*IPAV) @ REVISE VOLUME ESTIMATE 11511640 000756
00373 374* 707 CALL STV (I1,RRR) @ SAVE VOLUME ESTIMATE 001-01D 000771
00374 375* CALL CHKTIM (IL,IH,I1) @ KEEP AN EYE ON THE TIME 001-01D 000774
00375 376* GO TO 15 @ NO ALTERNATE RETURNS YET 115A1650 001001
00376 377* END 11501660 001037
END FOR
>

```

Listing 15.—Concluded.

@FOR,MS CASPER1.VSUMD
 FOR 4R1 E -04/17/84-12:56:31 (1,)
 >@EOF

SUBROUTINE VSUM ENTRY POINT 000121

STORAGE USED: CODE(1) 000143; DATA(0) 000021; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 CHKLH
 0004 CHKTIM
 0005 V
 0006 SPSHI
 0007 PAAI
 0010 SPSHR
 0011 REQSFAF
 0012 SPOPI
 0013 ERROR2
 0014 NERR2\$
 0015 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000020 1176 0001 000056 24L 0001 000076 29L 0001 000110 32L 0000 I 000003 I
 0000 I 000001 ID 0000 I 000002 IE 0000 000012 INJF\$ 0000 I 000000 IS 0005 R 000000 V

```

00101 1*          SUBROUTINE VSUM (IL,IH,VL)                10000010  000000
00101 2*          C+                                       10000020  000000
00101 3*          C                                       10000030  000000
00101 4*          C  VSUM      ***** A SUBROUTINE FOR CASPER ***** 10000040  000000
00101 5*          C          AUTHOR      WILLIAM HENRY JONES          10000050  000000
00101 6*          C          V01-00      02 FEB 79                    10000060  000000
00101 7*          C          V01-00A     06 FEB 80      PAX PROTOCOL ADJUSTMENTS 000000
00101 8*          C                                       10000070  000000
00101 9*          C                                       10000080  000000
00101 10*         C  DESCRIPTION ***** 10000090  000000
00101 11*         C                                       10000100  000000
00101 12*         C  SUMS UP THE VOLUME ESTIMATES OF ALL THE AERDELEMENTS BETWEEN 10000110  000000
00101 13*         C  'IL' AND 'IH'. 10000120  000000
00101 14*         C                                       10000130  000000
00101 15*         C- 10000140  000000
00103 16*         C  INTEGER IL,IH,IS,ID,IE 10000150  000000
00104 17*         C  REAL VL 10000160  000000
00105 18*         C  DATA ID/100/ 10000170  000000
00107 19*         C  DATA IE/1/ 10000180  000000
00111 20*         C  CALL CHKLH (IL,IH,IS,ID,IE) @ CHECK AERDELEMENT RANGE 10000190  000000
00112 21*         C  IF (IS) 17,32,17 @ VALIC RANGE ? 10000200  000006
00115 22*         C  17 VL=0,0 @ YES, DO THE SUMATION 10000210  000010
00116 23*         C  DO 19 I=IL,IH,IS @ 10000220  000020
00121 24*         C  CALL CHKTIM (IL,IH,I) @ KEEP AN EYE ON THE TIME 000020
00122 25*         C  19 VL=VL+V(I) @ 10000230  000025
00124 26*         C  CALL SPSHI (0) @ PUT END-OF-ARGUMENTS ON 000034
00125 27*         C  CALL SPSHI (0) @ THE STACK 000037
00126 28*         C  CALL PAAI (3,I) @ USE 'VL' AS MASTER ACCUM 000042
00127 29*         C  GO TO (24,29),I @ PAX GIVE US VALID 'VL' ? 000046
00130 30*         C  24 CALL SPSHR (VL) @ YES, LOAD OUR SUB-TOTAL 000056
00131 31*         C  CALL SPSHI (1) @ AS A LITERAL 000060
00132 32*         C  CALL SPSHI (7) @ ITEMS ON STACK 000063
00133 33*         C  CALL REQSFAF (100,1) @ LET PAX ADD THE SUB-TOTALS 000066
00134 34*         C  RETURN @ 000072
00135 35*         C  29 CALL SPOPI (I) @ CLEAN UP STACK 000076
00136 36*         C  CALL SPOPI (I) @ 000100
00137 37*         C  CALL ERROR2 (100,5) @ REPORT BAD ARGUMENT ERROR 000103
00140 38*         C  32 RETURN @ 000110
00141 39*         C  END 10000250  000142
END FOR
>

```

Listing 16.—Subroutine VSUM..

```

@FOR,MS CASPER1,VCOR
FOR 4R1 E -04/17/84-12:48:11 (1,)
>@EOF

```

```

SUBROUTINE VCOR      ENTRY POINT 000051

```

```

STORAGE USED: CODE(1) 000070; DATA(0) 000015; BLANK COMMON(2) 000000

```

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

```

0003  CHKLH
0004  CHKTIM
0005  V
0006  STAESC
0007  NERR3$

```

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

```

0001  000017 116G      0001  000040 20L      0000 I 000004 I      0000 I 000001 ID      0000 I 000002 IE
0000  000005 INJ$     0000 I 000000 IS      0000 R 000003 R      0005 R 000000 V

```

```

00101  1*          SUBROUTINE VCOR (IL,IH,VL)                13200010  000000
00101  2*          C+                                       13200020  000000
00101  3*          C                                       13200030  000000
00101  4*          C      VCOR      ***** A SUBROUTINE FOR CASPER *****  13200040  000000
00101  5*          C      AUTHOR      WILLIAM HENRY JONES                13200050  000000
00101  6*          C      V01-00      02 FEB 79                          13200060  000000
00101  7*          C      V01-00A     08 FEB 80      SEPARATES INPUTS AND OUTPUT  000000
00101  8*          C                                       13200070  000000
00101  9*          C                                       13200080  000000
00101 10*          C      DESCRIPTION *****                            13200090  000000
00101 11*          C                                       13200100  000000
00101 12*          C      APPLIES A SUPPLIED MULTIPLICATIVE CORRECTION TO THE VOLUME  13200110  000000
00101 13*          C      ESTIMATES OF ALL AEROELEMENTS IN THE RANGE 'IL' TO 'IH'.    13200120  000000
00101 14*          C                                       13200130  000000
00101 15*          C-                                       13200140  000000
00103 16*          C      INTEGER IL,IH,IS,ID,IE                        13200150  000000
00104 17*          C      REAL VL,R                                       13200160  000000
00105 18*          C      DATA ID/132/                                       13200170  000000
00107 19*          C      DATA IE/1/                                       13200180  000000
00111 20*          C      CALL CHKLH (IL,IH,IS,ID,IE)                @ CHECK AEROELEMENT RANGE  13200190  000000
00112 21*          C      IF (IS) 17,20,17                                @ VALID RANGE ?          13200200  000006
00115 22*          17 DO 19 I=IL,IH,IS                                @ YES, APPLY CORRECTION  13200210  000010
00120 23*          C      CALL CHKTIM (IL,IH,I)                            @ KEEP AN EYE ON THE TIME  000017
00121 24*          C      R=VL*V(I)                                         @                               13200220  000024
00122 25*          19 CALL STAESC (I,R)                                       @ RESULT TO SCRATCH SLOT  000031
00124 26*          20 RETURN                                                @                               13200240  000040
00125 27*          C      END                                               @                               13200250  000067
END FOR
>

```

```

@FOR,MS CASPER1,RHOPRD
FOR 4R1 E -04/13/84-16:06:31 (2,)
>@EOF

```

```

SUBROUTINE RHOPRS ENTRY POINT 000073

```

```

STORAGE USED: CODE(1) 000110; DATA(0) 000017; BLANK COMMON(2) 000000

```

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

```

0003 M
0004 CHKLH
0005 CHKTIM
0006 V
0007 STRHD
0010 T
0011 GASLAW
0012 STP
0013 NERR3#

```

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

```

0001 000017 116G 0001 000062 22L 0000 R 000004 DENS 0000 I 000003 I 0000 I 000001 ID
0000 I 000002 IE 0000 000007 INJP* 0000 I 000000 IS 0003 R 000000 M 0000 R 000006 PRES
0010 R 000000 T 0000 R 000005 TEMP 0006 R 000000 V

```

```

00101 1* SUBROUTINE RHOPRS (IL,IH) 17600010 000000
00101 2* C+ 17600020 000000
00101 3* C 17600030 000000
00101 4* C RHOPRS ***** A SUBROUTINE FOR CASPER ***** 17600040 000000
00101 5* C AUTHOR WILLIAM HENRY JONES 17600050 000000
00101 6* C V01-00 02 FEB 79 17600060 000000
00101 7* C V01-00A 11 FEB 80 ADD TIME CHECK 000000
00101 8* C V01-00B 15 SEP 80 FUNCTION TYPE STATEMENT 000000
00101 9* C 17600070 000000
00101 10* C 17600080 000000
00101 11* C DESCRIPTION ***** 17600090 000000
00101 12* C 17600100 000000
00101 13* C FOR ALL AEROELEMENTS IN THE RANGE 'IL' TO 'IH', 1) CALCULATES 17600110 000000
00101 14* C DENSITY BASED ON MASS AND VOLUME, AND 2) CALCULATES PRESSURE 17600120 000000
00101 15* C BASED ON TEMPERATURE AND DENSITY AND A CALL TO SUBROUTINE 17600130 000000
00101 16* C 'GASLAW' (WHICH MAY BE USER SUPPLIED). 17600140 000000
00101 17* C 17600150 000000
00101 18* C- 17600160 000000
00103 19* INTEGER IL,IH,IS,ID,IE 17600170 000000
00104 20* REAL M 000000
00105 21* DATA ID/176/ 17600180 000000
00107 22* DATA IE/1/ 17600190 000000
00111 23* CALL CHKLH (IL,IH,IS,ID,IE) @ CHECK AEROELEMENT RANGE 17600200 000000
00112 24* IF (IS) 16,22,16 @ VALID RANGE ? 17600210 000006
00115 25* 16 DO 21 I=IL,IH,IS @ YES, DO THEM 17600220 000010
00120 26* CALL CHKTIM (IL,IH,I) @ KEEP AN EYE ON THE TIME 000017
00121 27* DENS=M(I)/V(I) @ CALC DENSITY 17600230 000024
00122 28* CALL STRHD (I,DENS) @ UPDATE DATA BASE 17600240 000035
00123 29* TEMP=T(I) @ TEMPERATURE 17600250 000041
00124 30* CALL GASLAW (PRES, DENS, TEMP, I) @ USE SOMEBODY'S GAS LAW 17600260 000045
00125 31* 21 CALL STP (I,PRES) @ UPDATE DATA BASE 17600270 000053
00127 32* 22 RETURN @ 17600280 000062
00130 33* END 17600290 000107
END FOR
>

```

Listing 18.—Subroutine RHOPRS.

```

@FOR,MS CASPER1,GASLAD
FOR 4R1 E -04/17/84-12:58:57 (0,)
>@EOF

```

```

SUBROUTINE GASLAW ENTRY POINT 000012

```

```

STORAGE USED: CODE(1) 000016; DATA(0) 000004; BLANK COMMON(2) 000000

```

```

COMMON BLOCKS:

```

```

0003 GASCON 000001

```

```

EXTERNAL REFERENCES (BLOCK, NAME)

```

```

0004 NERR3$

```

```

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

```

```

0000 000000 INJP$ 0003 R 000000 R

```

```

00101 1* SUBROUTINE GASLAW (PR,RH,TP,ID) 000000
00101 2* C+ 000000
00101 3* C 000000
00101 4* C GASLAW ***** A SUBROUTINE FOR CASPER ***** 000000
00101 5* C AUTHOR WILLIAM HENRY JONES 000000
00101 6* C V01-00 22 OCT 80 000000
00101 7* C 000000
00101 8* C 000000
00101 9* C DESCRIPTION ***** 000000
00101 10* C 000000
00101 11* C THIS ROUTINE CALCULATES THE IDEAL GAS LAW. 000000
00101 12* C 000000
00101 13* C PR PRESSURE 000000
00101 14* C RH DENSITY 000000
00101 15* C TP TEMPERATURE 000000
00101 16* C ID ELEMENT ID (IGNORED) 000000
00101 17* C 000000
00101 18* C THUS 000000
00101 19* C 000000
00101 20* C PR = RH * TP * R 000000
00101 21* C 000000
00101 22* C WHERE R IS THE IDEAL GAS CONSTANT. THE FOLLOWING ARE APPROPRIATE 000000
00101 23* C CONSTANTS FOR VARIOUS UNITS OF MEASURE: 000000
00101 24* C 000000
00101 25* C 53.352000 (FT-LBF)/(LBM-DEGREES R) 000000
00101 26* C 1716.5473 (FT-LBF)/(SLUG-DEGREES R) 000000
00101 27* C 88.595808 (NT-M)/(KG-DEGRESS K) 000000
00101 28* C 000000
00101 29* C 000000
00101 30* C THIS ROUTINE IS INITIALIZED FOR (NT-M)/(KG-DEGRESS K); HOWEVER, 000000
00101 31* C THIS MAY BE ALTERED BY THE PAX/CASPER WORKER STARTUP 000000
00101 32* C INITIALIZATION PROCESS. 000000
00101 33* C 000000
00101 34* C- 000000
00103 35* COMMON /GASCON/R @ FOR EASY INITIALIZATION 000000
00104 36* REAL PR,RH,TP,R @ SO EASY I ONLY HAD TO TRY 000000
00105 37* DATA R/88.595808/ @ 3 TIMES TO GET IT RIGHT 000000
00107 38* PR=RH*TP*R @ 000000
00110 39* RETURN @ 000003
00111 40* END @ 000015
END FOR
>

```

Listing 19.—Subroutine GASLAW.

@FOR,MS CASPER1,FNBNE
 FOR 4R1 E -04/13/84-16:24:54 (2,)
 >@EOF

SUBROUTINE FNBNE ENTRY POINT 000707

STORAGE USED: CODE(1) 000736; DATA(0) 030116; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003 ELNK
 0004 FZ
 0005 PNEIZN
 0006 CHKLN
 0007 WERR2
 0010 TREE2
 0011 X
 0012 NEI
 0013 IPLZN
 0014 NEIZN
 0015 STNEI
 0016 CHKTIM
 0017 NERR2\$
 0020 SQRT
 0021 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000047	1000L	0001	000110	1010L	0001	000147	1025L	0001	000152	1050L	0001	000200	1055L
0001	000207	1075L	0001	000267	1088L	0001	000276	1100L	0001	000324	1300L	0001	000345	1303L
0001	000402	1311L	0001	000410	1400L	0001	000055	170G	0001	000432	2000L	0001	000473	2012L
0001	000512	2025L	0001	000542	2032L	0001	000112	204G	0001	000600	2040L	0001	000615	2044L
0001	000623	2046L	0001	000124	212G	0001	000023	225L	0001	000035	228L	0001	000225	245G
0001	000245	255G	0001	000356	312G	0001	000434	340G	0001	000476	363G	0001	000521	373G
0001	000533	400G	0001	000551	412G	0001	000567	421G	0001	000610	434G	0001	000627	446G
0001	000656	7L	0000	R 006405	AET	0003	I 000000	ELNK	0004	I 000000	FZ	0000	I 006367	I
0000	I 006362	ICC	0000	I 006370	IEP	0000	I 006371	IERC	0000	I 006373	IFZBAS	0000	030074	INJP\$
0013	I 000000	IFLZN	0000	I 006363	IST	0000	I 006365	ITAR	0000	I 006364	ITARG	0000	I 006402	IZEP
0000	I 006401	IZLC	0000	I 006400	IZLP	0000	I 006371	J	0000	I 006372	JECNT	0000	I 006375	JENEP
0000	I 006374	JENEW	0000	I 000000	JES	0000	I 006366	JESP	0000	I 006405	JET	0000	I 006200	JZS
0000	I 006403	JZSF	0000	I 006376	K	0000	I 006377	L	0000	I 006344	LNEI	0012	I 000000	NEI
0014	I 000000	NEIZN	0005	I 000000	PNEIZN	0000	R 006404	R	0000	R 006354	RNEI	0011	R 000000	X
0000	R 006351	XBAS												

00101	1*		SUBROUTINE FNBNE (ILO,IHI,JCC,IR)	000000
00101	2*	C+		000000
00101	3*	C		000000
00101	4*	C	FNBNE ***** A SUBROUTINE FOR CASPER *****	000000
00101	5*	C	AUTHOR WILLIAM HENRY JONES	000000
00101	6*	C	1015 X01.00 28 JAN 83	000000
00101	7*	C	X01.00A 15 FEB 83 TYPD X01.00A	000000
00101	8*	C	X01.00B 17 MAR 83 INDEX TYPD X01.00B	000000
00101	9*	C		000000
00101	10*	C		000000
00101	11*	C	DESCRIPTION *****	000000
00101	12*	C		000000
00101	13*	C	FNBNE (FIND BY NEIGHBOR ELEMENTS) UPDATES THE NEAREST NEIGHBORS	000000
00101	14*	C	LIST FOR EACH AEROELEMENT IN THE RANGE ILO TO IHI. NEAREST	000000
00101	15*	C	NEIGHBOR CANDIDATES ARE TAKEN FROM THE TARGET ELEMENT'S LISTED	000000
00101	16*	C	NEIGHBORS, THE NEIGHBORS OF THE NEIGHBORS, AND SO ON, UNTIL AT	000000
00101	17*	C	LEAST JCC (CANDIDATE COUNT) INDEPENDENT (NON-REDUNDANT) ELEMENTS	000000
00101	18*	C	HAVE BEEN CONSIDERED.	000000
00101	19*	C		000000
00101	20*	C	IT IS POSSIBLE THAT THE NEIGHBORS-OF-NEIGHBORS-OF-NEIGHBORS	000000
00101	21*	C	SCHEME WILL FAIL TO PRODUCE JCC CANDIDATE ELEMENTS. IN THIS	000000

Listing 20.—Subroutine FNBNE.

```

00101 22* C EVENT, CANDIDATE ELEMENTS ARE DRAWN FROM THE TARGET ELEMENT'S 000000
00101 23* C FLOW ZONE AND, THEN, FROM THAT FLOW ZONE'S NEIGHBORS. IF 000000
00101 24* C THIS IS NECESSARY, THE REQUIREMENT FOR JCC CANDIDATE ELEMENTS 000000
00101 25* C IS WAIVED, 000000
00101 26* C 000000
00101 27* C 000000
00101 28* C 000000
00101 29* C 000000
00101 30* C INPUT INFORMATION ***** 000000
00101 31* C 000000
00101 32* C QUANTITY TYPE DIMENSION DESCRIPTION 000000
00101 33* C -----
00101 34* C X REAL 1 TO ISIZE AEROELEMENT POSITION IN 000000
00101 35* C 1 TO 3 SPACE 000000
00101 36* C 000000
00101 37* C NEI INTEGER 1 TO ISIZE AEROELEMENT NEAREST 000000
00101 38* C 1 TO 5 NEIGHBOR LIST 000000
00101 39* C 000000
00101 40* C ELNK INTEGER 1 TO ISIZE AEROELEMENT LINKAGES 000000
00101 41* C 1 TO 3 ( ,1) POINTER TO NEXT 000000
00101 42* C ELEMENT IN FLOW 000000
00101 43* C ZONE 000000
00101 44* C 000000
00101 45* C IPLZN INTEGER 1 TO NZN FLOW ZONE RESIDENT ELEMENT 000000
00101 46* C 1 TO 6 LINKAGE HEAD 000000
00101 47* C ( ,4) PTR TO FIRST ELEMENT 000000
00101 48* C ( ,5) NUMBER OF ELEMENTS 000000
00101 49* C ( ,6) PTR TO LAST ELEMENT 000000
00101 50* C 000000
00101 51* C FZ INTEGER 1 TO ISIZE FLOW ZONE OF ELEMENT 000000
00101 52* C 000000
00101 53* C NEIZN INTEGER 1 TO NEIZSZ FLOW ZONE NEIGHBOR LISTS 000000
00101 54* C 000000
00101 55* C PNEIZN INTEGER 1 TO NZN NEIZN CONTROL INFO 000000
00101 56* C ( ,1) STARTING POINT 000000
00101 57* C ( ,2) NUMBER OF NEIGHBORS 000000
00101 58* C 000000
00101 59* C 000000
00101 60* C 000000
00101 61* C 000000
00101 62* C ERRORS REPORTED BY THIS ROUTINE 000000
00101 63* C 000000
00101 64* C CODE ERROR 000000
00101 65* C -----
00101 66* C 1 ILO <1 000000
00101 67* C 000000
00101 68* C 2 ILO >ISIZE 000000
00101 69* C 000000
00101 70* C 3 IHI <1 000000
00101 71* C 000000
00101 72* C 4 IHI >ISIZE 000000
00101 73* C 000000
00101 74* C 5 CANDIDATE COUNT TOO LOW (OPERATION CONTINUES) 000000
00101 75* C 000000
00101 76* C 6 CANDIDATE COUNT TOO HIGH (OPERATION CONTINUES) 000000
00101 77* C 000000
00101 78* C 7 COULD NOT INSERT TARGET AEROELEMENT IN AEROELEMENT 000000
00101 79* C TREE (TREE MECHANISMS FAULT), 000000
00101 80* C 000000
00101 81* C 000000
00101 82* C 000000
00101 83* C 000000
00101 84* C DEFINED RETURN SWITCH (IR) VALUES 000000
00101 85* C 000000
00101 86* C VALUE MEANING 000000
00101 87* C -----
00101 88* C 1 SUCCESS 000000
00101 89* C 2 FAILURE 000000
00101 90* C 000000
00101 91* C FORMAT OF AEROELEMENT TREE 000000
00101 92* C 000000
00101 93* C A BINARY TREE IS CONSTRUCTED FOR THE PURPOSE OF ELIMINATING 000000

```

```

00101  94*  C  REDUNDANT ELEMENTS. ITS FORMAT IS AS FOLLOWS: 000000
00101  95*  C  000000
00101  96*  C  INDEX      CONTENTS 000000
00101  97*  C  ----- 000000
00101  98*  C  1          LENGTH OF AN ENTRY 000000
00101  99*  C  2          POINTER TO FIRST FREE ENTRY 000000
00101  100* C  3          NUMBER OF FREE ENTRIES REMAINING 000000
00101  101* C  4          COMPARISON CONTROL CODE 000000
00101  102* C  5          POINTER TO FIRST ENTRY, IPTR, 0 => NONE 000000
00101  103* C  ... 000000
00101  104* C  IPTR -> < BRANCH POINTER, 0 => NONE 000000
00101  105* C  +1      > BRANCH POINTER, 0 => NONE 000000
00101  106* C  +2      PREVIOUS ENTRY POINTER, 0 => NONE 000000
00101  107* C  +3      INFORMATION WORD 000000
00101  108* C  +4      ELEMENT ID 000000
00101  109* C  +5      ELEMENT X( ,1) 000000
00101  110* C  +6      ELEMENT X( ,2) 000000
00101  111* C  +7      ELEMENT X( ,3) 000000
00101  112* C  +8      ELEMENT'S FLOW ZONE ID 000000
00101  113* C  000000
00101  114* C  000000
00101  115* C- 000000
00103  116*  PARAMETER OURID=106 @ CASPER CATALOG ID 000000
00104  117*  PARAMETER NNNEI=5 @ NUMBER OF NEAREST NEIGHBORS 000000
00105  118*  INCLUDE TREE @ 000000
00120  119*  PARAMETER NNNEIM=NNNEI-1 @ 000000
00121  120*  PARAMETER ERCCL=5 @ ERROR -- CANDIDATE COUNT TOO LOW 000000
00122  121*  PARAMETER ERCCH=6 @ ERROR -- CANDIDATE COUNT TOO HIGH 000000
00123  122*  PARAMETER JETNE=1000 @ ELEMENT TREE -- NUMBER OF ENTRIES 000000
00124  123*  PARAMETER JETFF=6 @ ELEMENT TREE -- FIRST FREE ENTRY 000000
00125  124*  PARAMETER JETLE=9 @ ELEMENT TREE -- LENGTH OF ENTRY 000000
00126  125*  PARAMETER JETAL=(JETNE*JETLE)+JETFF-1 @ LENGTH OF JET ARRAY 000000
00127  126*  PARAMETER JESAL=3200 @ SIZE OF ELEMENT STACK 000000
00130  127*  PARAMETER JZSAL=100 @ TEMPORARY ZONE STORAGE 000000
00131  128*  INTEGER JET(JETAL) @ ELEMENT TREE TABLE 000000
00132  129*  INTEGER JES(JESAL) @ ELEMENT STACK 000000
00133  130*  INTEGER JZS(JZSAL) @ 000000
00134  131*  INTEGER ELNK @ 000000
00135  132*  INTEGER LNEI(NNNEI) @ LOCAL NEAREST NEIGHBORS LIST 000000
00136  133*  INTEGER FZ @ 000000
00137  134*  INTEGER PNEIZN @ 000000
00140  135*  REAL XBAS(3) @ TARGET AEROELEMENT'S POSITION 000000
00141  136*  REAL RNEI(NNNEI) @ LOCAL NEAREST NEIGHBOR RADIAL DISTANCES 000000
00142  137*  REAL AET(JETAL) @ REAL ACCESS TO JET 000000
00143  138*  EQUIVALENCE (JET(1),AET(1)) @ 000000
00144  139*  IERC=1 @ INIT ERROR COUNTER 000000
00145  140*  IR=1 @ ASSUME SUCCESS 000001
00146  141*  ICC=JCC @ DUMMY UP 000002
00147  142*  CALL CHKLH (ILO,IHI,IST,OURID,IERC) @ CHECK DO-LOOP RANGE 000004
00150  143*  IERC=1 @ RESET ERROR COUNTER 000013
00151  144*  IF (IST)225,202,225 @ ANY ERROR ? 000015
00154  145* 202 RETURN @ YES 000017
00155  146* 225 IF (ICC=6) 226,228,228 @ ENFORCE A MINIMUM CANDIDATE 000023
00160  147* 226 ICC=6 @ COUNT 000026
00161  148*  CALL WERR2 (OURID,ERCCL) @ 000030
00162  149* 228 IF (ICC+1-JETNE) 1000,1000,229 @ ALWAYS LEAVE SPACE IN TREE 000035
00165  150* 229 ICC=JETNE-1 @ FOR TARGET ELEMENT ENTRY TO 000040
00166  151*  CALL WERR2 (OURID,ERCCH) @ AVERT TARGET-TO-TARGET 000042
00167  152* 1000 DO 2100 ITARG=ILO,IHI,IST @ DO EACH ELEMENT IN RANGE 000047
00172  153*  ITAR=ITARG @ DUMMY UP FOR DEC 000055
00173  154*  JET(IETLE)=JETLE @ INIT TREE -- ENTRY LENGTH 000057
00174  155*  JET(IETFF)=JETFF @ FIRST FREE ENTRY 000061
00175  156*  JET(IETFC)=JETNE @ FREE ENTRY COUNT 000063
00176  157*  JET(IETCC)=-1 @ COMPARE BY INTEGERS 000065
00177  158*  JET(IETVE)=0 @ NO ENTRIES YET 000067
00200  159*  JESP=0 @ RESET ELEMENT STACK 000070
00201  160*  CALL TREE2 (I,IEP,ITAR,JET) @ ENTER TARGET ELEMENT 000071
00202  161*  GO TO (1010,1010,7),I @ CHECK RESULT JUST IN CASE 000077
00203  162* 1010 DO 1012 I=1,3 @ PICK UP AEROELEMENT'S 000112
00206  163*  XBAS(I)=X(ITAR,I) @ POSITION X01,00B 000112
00207  164* 1012 CONTINUE @ 000124
00211  165*  DO 1017 I=1,5 @ PICK UP AEROELEMENT'S 000124

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Listing 20.—Continued.

00214	166*	J=I	@ NEAREST NEIGHBORS AND PUT	000124
00215	167*	JESP=JESP+1	@ ON POSSIBILITY STACK	000126
00216	168*	JES(JESP)=NEI(ITAR,J)	@	000131
00217	169*	1017 CONTINUE	@	000141
00221	170*	JECNT=0	@ CLEAR ENTRY COUNT	000141
00222	171*	IFZBAS=FZ(ITAR)	@ RECORD TARGET'S FLOW ZONE	000142
00223	172*	1025 JENEW=0	@ CLEAR NEW ENTRY COUNT	000147
00224	173*	JENEP=JET(IETFF)	@ POINT TO FIRST NEW ENTRY	000147
00225	174*	1050 IF (JESP) 1075,1075,1051	@ ANYTHING ON STACK ?	000152
00230	175*	1051 I=JES(JESP)	@ YES, POP ELEMENT POSSIBILITY	000155
00231	176*	JESP=JESP-1	@ ID OFF THE STACK	000157
00232	177*	CALL TREE2 (J,IEP,I,JET)	@ INSERT IN THE TREE IF NEW	000161
00233	178*	GO TO (1050,1055,2000),J	@ WAS IT A NEW ENTRY ?	000167
00234	179*	1055 JENEW=JENEW+1	@ YES, BUMP COUNT OF NEW	000200
00235	180*	JECNT=JECNT+1	@ BUMP OVERALL COUNT, TOO	000202
00236	181*	GO TO 1050	@	000205
00237	182*	1075 IF (JENEW) 1100,1100,1076	@ ANY NEW ELEMENTS LEFT ?	000207
00242	183*	1076 I=JENEP+IEVA	@ YES, POINT TO ELEMENT ID	000211
00243	184*	J=JET(I)	@ GET ELEMENT ID	000216
00244	185*	DO 1081 K=1,3	@ GET ELEMENT'S POSITION	000225
00247	186*	L=K	@ AND RECORD IN THE ENTRY	000225
00250	187*	AET(I+K)=X(J,L)	@	000227
00251	188*	1081 CONTINUE	@	000236
00253	189*	JET(I+4)=FZ(J)	@ RECORD ZONE, TOO	000236
00254	190*	DO 1087 K=1,5	@ TRANSFER THE ELEMENT'S	000245
00257	191*	L=K	@ NEIGHBORS TO THE CANDIDATE	000245
00260	192*	IF (JESP-JESAL) 1085,1088,1088	@ STACK (UNTIL THE STACK	000247
00263	193*	1085 JESP=JESP+1	@ FILLS UP, VERY UNLIKELY)	000253
00264	194*	JES(JESP)=NEI(J,L)	@	000256
00265	195*	1087 CONTINUE	@	000267
00267	196*	1088 JENEW=JENEW-1	@ ONE LESS 'NEW' ENTRY	000267
00270	197*	JENEP=JENEP+JET(IETLE)	@ POINT TO NEXT ENTRY	000271
00271	198*	GO TO 1075	@ GO THROUGH ALL 'NEW' ENTRIES	000274
00272	199*	1100 IF (JECNT-ICC) 1101,2000,2000	@ ENOUGH CANDIDATES ?	000276
00275	200*	1101 IF (JESP) 1200,1200,1025	@ NO, PROCESS STACK IF NONNULL	000301
00275	201*	C+		000301
00275	202*	C	THIS SECTION LOCATES CANDIDATE ELEMENTS BY SEARCHING FLOW ZONE	000301
00275	203*	C	RESIDENT LISTS. THE FIRST FLOW ZONE USED IS THE TARGET ELEMENT'S	000301
00275	204*	C	FLOW ZONE OF RESIDENCE. THEN A FLOW ZONE NEIGHBORS OF NEIGHBORS	000301
00275	205*	C	OF NEIGHBORS SCHEME IS USED TO LOCATE ADDITIONAL FLOW ZONES.	000301
00275	206*	C-		000301
00300	207*	1200 IZLF=PNEIZN(IFZBAS,1)	@ INIT ZONE'S NEIGHBOR CONTROL	000304
00301	208*	IZLC=PNEIZN(IFZBAS,2)	@	000311
00302	209*	IZEP=IPLZN(IFZBAS,4)	@ POINT TO ZONE'S FIRST EL	000316
00303	210*	1300 IF (IZEP) 1400,1400,1301	@ GOT AN ELEMENT ?	000324
00306	211*	1301 CALL TREE2 (J,I,IZEP,JET)	@ YES, PUT IT IN THE TREE	000326
00307	212*	GO TO (1311,1303,2000),J	@ A NEW TREE ENTRY ?	000334
00310	213*	1303 J=I+IEVA	@ YES	000345
00311	214*	DO 1307 K=1,3	@ TRANSFER ITS POSITION TO	000347
00314	215*	L=K	@ THE TREE ENTRY	000356
00315	216*	AET(J+K)=X(IZEP,L)	@	000360
00316	217*	1307 CONTINUE	@	000367
00320	218*	JET(J+4)=FZ(IZEP)	@ RECORD ZONE, TOO	000367
00321	219*	JECNT=JECNT+1	@ BUMP ENTRY COUNT	000373
00322	220*	IF (JECNT-ICC) 1311,2000,2000	@ ENOUGH ENTRIES ?	000376
00325	221*	1311 IZEP=ELNK(IZEP,1)	@ NO, LOOK FOR NEXT ELEMENT	000402
00326	222*	GO TO 1300	@	000406
00327	223*	1400 IF (IZLC) 2000,2000,1401	@ ANY MORE NEIGHBOR ZONES ?	000410
00332	224*	1401 IZLC=IZLC-1	@ YES, ONE LESS NOW	000412
00333	225*	I=NEIZN(IZLP)	@ GET NEIGHBOR'S ID	000414
00334	226*	IZLP=IZLP+1	@ POINT TO NEXT	000420
00335	227*	IZEP=IPLZN(I,4)	@ POINT TO FIRST ELEMENT	000423
00336	228*	GO TO 1300	@	000430
00336	229*	C+		000430
00336	230*	C	THE FOLLOWING CODE DOES THE FINAL SELECTION OF NEAREST NEIGHBORS	000430
00336	231*	C	FROM THE POPULATION IN THE ELEMENT TREE.	000430
00336	232*	C-		000430
00337	233*	2000 DO 2003 I=1,NNNEI	@ INIT LOCAL NEIGHBOR	000434
00342	234*	LNEI(I)=I	@ SELECTION TABLES	000434
00343	235*	RNEI(I)=1.0E+30	@	000436
00344	236*	2003 CONTINUE	@	000442
00346	237*	JENEP=JETFF+JETLE	@ SKIP OVER TARGET'S ENTRY	000442

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00347 238*      JZSP=1                @ PUT TARGET AERDELEMENT'S      000444
00350 239*      JZS(JZSP)=IFZBAS          @ FLOW ZONE OR ZONE STACK      000447
00351 240*      J=PNEIZN(IFZBAS,1)     @ PUT AS MANY NEIGHBORS OF    000451
00352 241*      K=PNEIZN(IFZBAS,2)     @ THAT ZONE ON THE STACK      000456
00353 242*      IF (K) 2025,2025,2010 @ AS WILL FIT                  000463
00356 243*      2010 IF (K-JZSAL) 2012,2011,2011 @                             000465
00361 244*      2011 K=JZSAL-1         @                             000470
00362 245*      2012 DO 2016 L=1,K     @                             000473
00365 246*      JZSP=JZSP+1           @                             000476
00366 247*      JZS(JZSP)=NEIZN(I)    @                             000500
00367 248*      I=I+1                 @                             000505
00370 249*      2016 CONTINUE          @                             000512
00372 250*      2025 DO 2046 I=1,JECNT @ LOOK AT EACH CANDIDATE      000512
00375 251*      J=JENEP+IEVA          @ POINTER CANDIDATE'S ID      000521
00376 252*      JENEP=JENEP+JETLE     @ POINT TO NEXT ENTRY         000524
00377 253*      DO 2030 K=1,JZSP      @ CANDIDATE MUST BE IN A GOOD 000533
00402 254*      IF (JZS(K)-JET(J+4)) 2030,2032,2030 @ FLOW ZONE TO BE CONSIDERED 000533
00405 255*      2030 CONTINUE          @                             000540
00407 256*      GO TO 2046            @ OOPS, CLOSE YOUR EYES, MARY 000540
00410 257*      2032 R=0.0            @ ZAF RADIAL DISTANCE        000542
00411 258*      DO 2034 K=1,3         @ CALC DISTANCE FROM TARGET    000542
00414 259*      2034 R=R+((AET(J+K)-XBAS(K))*#2) @ TO CANDIDATE                000552
00416 260*      R=SQRT(R)             @                             000556
00417 261*      L=NNNEI+1             @ L BECOMES POSITION NUMBER OF 000562
00420 262*      DO 2039 K=NNNEI,1,-1  @ CLOSEST NEIGHBOR BESTED BY 000567
00423 263*      IF (R-RNEI(K)) 2039,2039,2040 @ THE CANDIDATE POSITION        000567
00426 264*      2039 L=K              @                             000573
00430 265*      2040 IF (L-NNNEI) 2041,2044,2046 @ ANY REPLACEMENT ?           000600
00433 266*      2041 DO 2043 K=NNNEIM,L,-1 @ YES, LEFT FURTHER NEIGHBORS 000603
00436 267*      LNEI(K+1)=LNEI(K)     @ UP ONE                       000610
00437 268*      2043 RNEI(K+1)=RNEI(K) @                             000611
00441 269*      2044 LNEI(L)=JET(J)   @ SLIP NEW NEIGHBOR INTO      000615
00442 270*      RNEI(L)=R             @ POSITION                       000620
00443 271*      2046 CONTINUE          @                             000627
00445 272*      DO 2053 I=1,5         @ TRANSFER RESULTS TO TARGET   000627
00450 273*      J=I                   @ ELEMENT'S STORAGE AREA      000627
00451 274*      CALL STNEI (ITAR,J,LNEI(J)) @                             000631
00452 275*      2053 CONTINUE          @                             000643
00454 276*      CALL CHKTIM (ILO,IHI,ITAR) @ KEEP AN EYE ON THE TIME     000643
00455 277*      2100 CONTINUE         @ END OF TARGET LOOP          000652
00457 278*      RETURN                @ THAT'S ALL !!               000652
00457 279*      C+                    @                             000652
00457 280*      C ERROR REPORTING     @                             000652
00457 281*      C-                    @                             000652
00460 282*      7 IERC=IERC+6          @ FAILED TO INSERT TARGET ELEMENT 000656
00461 283*      IR=2                   @ SET FAILURE RETURN          000660
00462 284*      CALL WERR2 (OURID,IERC) @ REPORT ERROR                 000662
00463 285*      RETURN                 @                             000666
00464 286*      END                     @                             000735
END FOR
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Listing 20.—Concluded.

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16. Abstract The Combined Aerodynamic and Structural Dynamic Problem Emulating Routines (CASPER) is a collection of data-base modification computer routines that can be used to simulate Navier-Stokes flow through realistic, time-varying internal flow fields. The Navier-Stokes equation used involves calculations in all three dimensions and retains all viscous terms. The only term neglected in the current implementation is the gravitational term. The solution approach is of an iterative, time-marching nature. Calculations are based on Lagrangian aerodynamic elements (aeroelements). It is assumed that the relationships between a particular aeroelement and its five nearest neighbor aeroelements are sufficient to make a valid simulation of Navier-Stokes flow on a small scale and that the collection of all small-scale simulations makes a valid simulation of a large-scale flow. In keeping with these assumptions, it must be noted that CASPER produces an imitation or simulation of Navier-Stokes flow rather than a strict numerical solution of the Navier-Stokes equation. CASPER is written to operate under the Parallel, Asynchronous Executive (PAX), which is described in a separate report.					
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