THE TURBULENT BOUNDARY LAYER ON A POROUS PLATE: AN EXPERIMENTAL STUDY OF THE HEAT TRANSFER BEHAVIOR WITH ADVERSE PRESSURE GRADIENTS

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Report No. HMT-16

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ABSTRACT

An experimental investigation of the heat transfer behavior of the near equilibrium transpired turbulent boundary layer with adverse pressure gradient has been carried out. Stanton numbers were measured by an energy balance on electrically heated plates that form the bottom wall of the wind tunnel. Mean temperature profiles were measured by a 0.003 inch diameter Chromel/constantan thermocouple probe.

Two adverse pressure gradients of the form $u_\infty \sim x^m$ $(m < 0)$ were studied. Two types of transpiration boundary conditions were investigated: (1) constant $F = \dot{m}''/\rho_\infty u_\infty$ and (2) constant $B_h = F/St$. The concept of an equilibrium thermal boundary layer was introduced. It was found that Stanton number as a function of enthalpy thickness Reynolds number is essentially unaffected by adverse pressure gradient with no transpiration.

Shear stress, heat flux, and turbulent Prandtl number profiles were computed from mean temperature and velocity profiles. It was concluded that the turbulent Prandtl number is greater than unity in near the wall and decreases continuously to approximately 0.5 at the free stream. In the log-region, the turbulent Prandtl number was found to be a function primarily of the pressure gradient; transpiration has relatively little influence. Increasing the adverse pressure gradient decreases the turbulent Prandtl number in the log-region.

Prediction of selected experimental runs was accomplished by a finite difference computer program. The turbulent Prandtl number model for the inner region was

$$Pr_t = C_1 \frac{\phi}{1-e^{-\phi}} \quad , \quad \phi = \frac{C_2}{\frac{\varepsilon_m}{\nu} Pr}$$

while the outer region model was

$$Pr_t = 0.5 + b_1[1 - (y/\delta)^2] \quad .$$

Mean velocity field closure was accomplished by van Driest's mixing length model.

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NOMENCLATURE

a, a_1	constants
A	van Driest length scale
A_h^+	non-dimensional heat transfer sublayer thickness, see Equation (7-18)
b, b_1	constants
B_f	$= F/(C_f/2)$, momentum blowing parameter
B_h	$= F/St$, heat transfer blowing parameter
C_1	see Equation (7-5)
C_2	see Equation (7-9)
$C_f/2$	$= \tau_0/\rho_\infty u_\infty^2$, skin friction coefficient
$(C_f/2)_{cp}$	constant property value of $C_f/2$
c_p	specific heat at constant pressure
D	see Equation (6-11)
E	$= u_\infty^2/2g_c J(T_0-T_\infty)$, Eckert number
f, f_1	functional relationship
F	$= \dot{m}''/\rho_\infty u_\infty$, blowing fraction
F_1	see Equation (2-22)
g_c	$= 32.174$ ft-lbm/(lbf-sec^2)
G_f	$= \frac{1}{\Delta_c} \int_0^\infty \left(\frac{u_\infty - u_\tau}{u_\tau}\right)^2 dy$, Clauser shape factor
G_h	$= \Delta_4/\Delta_3$, defect enthalpy shape factor

H	$= \delta_1/\theta$, velocity shape factor
i	static enthalpy
i_o	static enthalpy at wall
i_∞	static enthalpy at free-stream
I	$= i + u^2/2 - (i_\infty + u_\infty^2/2)$, stagnation enthalpy referenced to free-stream value
I_o	$= i_o - (i_\infty + u_\infty^2/2)$, value of I at wall
I^+	$= \left(1 - \frac{I}{I_o}\right) \sqrt{\frac{C_f/2}{\rho_\infty/\rho_o}} \frac{1}{St}$
I_d^+	$= I_\infty^+ - I^+$
J	= 778 ft-lbf/Btu
k	thermal conductivity
K	$= \frac{\nu}{u_\infty^2} \frac{du_\infty}{dx}$
ℓ	mixing length
ℓ_h^+	non-dimensional heat transfer mixing length, see Equation (7-17)
m	exponent in Equation (2-11)
m_F	exponent in Equation (2-13)
$\dot{m}''$	$= \rho_o v_o$, mass injection at the wall
n	exponent in Equation (3-1)
P	static pressure
Pe_t	$= Pr\varepsilon_m/\nu$, turbulent Peclet number

Pr = ν/α , molecular Prandtl number

Pr_t = $\varepsilon_m/\varepsilon_h$, turbulent Prandtl number

$(Pr_t)_\ell$ average value of Pr_t in log-region

$\dot{q}''$ heat flux

$\dot{q}_o''$ wall heat flux

Q^+ = $\dot{q}''/\dot{q}_o''$

Q_c^+, Q_1^+, Q_2^+ see Equation (6-8)

r = $(Pr)^{1/3}$, recovery factor

$Re_{\Delta 2}$ = $\dfrac{\rho_\infty u_\infty \Delta 2}{\nu_\infty}$, enthalpy thickness Reynolds number

Re_θ = $\dfrac{\rho_\infty u_\infty \theta}{\nu_\infty}$, momentum thickness Reynolds number

St = $\dot{q}_o''/\rho_\infty u_\infty I_o$, Stanton number

T mean temperature

T_o wall temperature

T_∞ free stream temperature

T' fluctuating temperature

T^+ = $\overline{T}\sqrt{\dfrac{C_f/2}{\rho_\infty/\rho_o}}\ \dfrac{1}{St}$

T^* = $\overline{T}\sqrt{\dfrac{St}{\rho_\infty/\rho_o}}$

$\overline{T}$ = $(T-T_o)/(T_\infty-T_o)$

u,v,w components of mean velocity

u',v',w' components of fluctuating velocity

u_∞ free-stream velocity

u_τ $= \sqrt{\tau_o/\rho_o}$, shear velocity

u^+ $= u/u_\tau$

v_o blowing velocity

x streamwise coordinate

x_o, x_1 see Equations (2-21) and (2-22)

y coordinate normal to the wall

y^+ $= y\, u_\tau/\nu_o$

y^* $= \dfrac{y\, u_\infty}{\nu_o} \sqrt{St\ \rho_\infty/\rho_o}$

z transverse coordinate

Greek

α $= k/\rho c_p$, thermal diffusivity

$\alpha_1, \alpha_2, \alpha_3$ curve fit constants

β $= \dfrac{\delta_1}{\tau_o} \dfrac{dp}{dx}$

γ $= K \times 10^3\, Re_\theta/(H-1)$

δ momentum boundary layer thickness ($u/u_\infty = 0.99$)

δ_1 $= \displaystyle\int_0^\infty \left(1 - \frac{\rho u}{\rho_\infty u_\infty}\right) dy$, displacement thickness

Δ thermal boundary layer thickness ($\overline{T} = 0.99$)

$\Delta_c = \int_0^\infty \frac{u_\infty - u}{u_\tau} dy$

$\Delta_2 = \int_0^\infty \frac{\rho u I}{\rho_\infty u_\infty I_o} dy$, enthalpy thickness

Δ_3 see Equation (2-7)

Δ_4 see Equation (2-8)

ΔE see Equation (3-5)

ΔSt see Equation (3-6)

ε_m eddy viscosity, see Equation (6-13)

$\varepsilon_m^+ = \varepsilon_m/\nu$

ε_h eddy diffusivity, see Equation (6-14)

$\varepsilon_h^+ = \varepsilon_h/\nu$

$\kappa = 0.41$, von Kármán constant

κ_h heat transfer constant analogous to κ

λ computational value of ℓ/δ in outer region

μ dynamic viscosity

ν kinematic viscosity

ρ density

ρ_o wall value of ρ

τ shear stress

τ_o wall value of τ

τ^+ $= \tau/\tau_o$

ϕ see Equation (7-9)

θ $= \int_0^\infty \frac{\rho u}{\rho_\infty u_\infty}\left(1 - \frac{u}{u_\infty}\right)dy$, momentum thickness

θ' see Equation (7-5)

CHAPTER 1

INTRODUCTION

In recent years, the transpired* turbulent boundary layer has aroused considerable technical interest. It has been well established that blowing is an effective means of protecting a body from a hot fluid environment. Examples of this are found in turbine blades and rocket nozzles. Suction can be used to provide boundary layer control on high lift devices. Aside from the many important practical applications of the transpired turbulent boundary layer, any information that leads to a better understanding of the transpired turbulent boundary layer will be a significant scientific contribution.

Since 1967, the Heat and Mass Transfer Group at Stanford University has been actively engaged in an experimental and analytical program to study the transpired turbulent boundary layer. Simpson [1] reported on the hydrodynamic behavior of the constant pressure layers, and Moffat [2] and Whitten [3] reported on the heat transfer behavior of the same flows; Julien [4] and Loyd [5] studied the hydrodynamics of accelerating flows, and Thielbahr [6] and Kearney [7] studied the heat transfer behavior of the same flows. The above work has been summarized by Kays [8]. The present study is concerned with the heat transfer behavior of decelerating, or adverse pressure gradient, transpired turbulent boundary layers, and is a logical extension of the earlier work done by the Heat and Mass Transfer Group at Stanford. Coincident with this work, Andersen [9] studied the hydrodynamics of adverse pressure gradient flows.

Only one experimental study of the transpired turbulent boundary layer with adverse pressure gradients has been reported in the literature. McLean [10] investigated strong adverse pressure gradients with blowing, with primary emphasis on the onset of separation. McLean's [10] initial velocity was 155 ft/sec with a linear decrease in the streamwise direction.

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* The term transpiration is used to indicate that the normal component of velocity at the wall is non-zero; blowing and suction indicate mass injection into and out of the main flow, respectively.

Velocity profiles were measured with a pitot probe and skin friction was determined from Stevenson's [11] law of the wall. Stanton numbers were measured but no temperature profiles were taken. Seban [27], Moretti [28], Perry [12], and Hatton [13] reported Stanton numbers for adverse pressure gradient flows but with no transpiration. None of the above heat transfer studies drew any conclusions about the effect of pressure gradient and/or transpiration on the turbulent Prandtl number.

The objectives of the present study are as follows:

1. Provide Stanton number and temperature profile data for near equilibrium flow conditions that would serve as a standard of comparison for future turbulent boundary layer prediction methods.
2. Ascertain the influence of the combined effects of adverse pressure gradient and transpiration on the Stanton number for the turbulent boundary layer.
3. Determine turbulent Prandtl number variation in the boundary layer (from mean profile measurements), and ascertain the influence of adverse pressure gradient and transpiration on the turbulent Prandtl number.
4. Develop a turbulent Prandtl number model that would allow one to predict heat transfer to the turbulent boundary layer under the influence of adverse pressure gradient and transpiration boundary conditions.

CHAPTER 2

BOUNDARY CONDITIONS: SURFACE TEMPERATURE, FREE STREAM VELOCITY AND TRANSPIRATION RATE

In designing a heat transfer experiment which is not directly related to a particular hardware application, the experimenter must choose the boundary conditions he would like to investigate. Boundary conditions in this sense refer to the streamwise variations of surface temperature, free stream velocity and transpiration rate. There exists an infinite number of possible choices for each of the above three boundary conditions, and the experimenter must choose carefully in order to gain the maximum amount of information from his experiment.

The outer 90% of the boundary layer responds slowly to changes in boundary conditions. Consequently the influence of a change in boundary conditions would be felt far downstream from where the change occurred. This slow response of the boundary layer would make interpretation of the data more difficult and might mask some of the more important results. On this basis, boundary conditions which produce rapid changes (over short distances) in Stanton number and mean temperature profiles were rejected, including: step changes in surface temperature, free stream velocity and transpiration rate as well as adverse pressure gradients strong enough to cause separation.

The thermal boundary layer is directly influenced by the mean velocity profile and the fluctuating velocity v' through the term $\overline{T'v'}$. Hence, it seems natural to consider the momentum boundary layer first in designing a meaningful heat transfer experiment. Since the outer 90% of an equilibrium momentum boundary layer has defect-similarity, it was decided to restrict this study to <u>equilibrium</u> (or at least near-equilibrium) flows. The problem of how to construct an equilibrium momentum boundary layer and an equilibrium thermal boundary layer will be discussed in subsequent sections.

2.1 Velocity Defect Similarity

Clauser [14] first introduced the concept of an equilibrium momentum boundary layer. He defined this as a layer in which the defect velocity is an unique function of y/δ, i.e.,

$$\frac{u_\infty - u}{u_\tau} = f_1(y/\delta) \quad . \tag{2-1}$$

Since the momentum boundary layer thickness is ill-defined, Clauser [14] replaced δ by a new thickness parameter Δ_c defined by

$$\Delta_c = \delta \int_0^1 \frac{u_\infty - u}{u_\tau} \, d(y/\delta) \quad . \tag{2-2}$$

Therefore, (2-1) can be equivalently written as

$$\frac{u_\infty - u}{u_\tau} = f_1(y/\Delta_c) \quad . \tag{2-3}$$

A shape factor describing the defect velocity profile was defined as

$$G_f = \frac{\delta}{\Delta_c} \int_0^1 \left(\frac{u_\infty - u}{u_\tau} \right)^2 d(y/\delta) \quad . \tag{2-4}$$

From (2-3) and (2-4) it follows that an equilibrium momentum boundary layer has a constant value of G_f. It should be noted that G_f is only approximately constant for an equilibrium flow, since the inner 5-10% of the momentum boundary layer does not have defect similarity.

2.2 Temperature (Enthalpy) Defect Similarity

Equation (2-1) can also be written as

$$u_\infty^+ - u^+ = f_1(y/\delta) \quad . \tag{2-5}$$

By analogy with (2-5), let us propose a defect temperature law of the form

$$T_\infty^+ - T^+ = f_2(y/\Delta) \quad , \tag{2-6}$$

where Δ is the thermal boundary layer thickness. The validity of this proposed defect temperature law must be verified experimentally, and this will be done in CHAPTER 5. In order for this defect temperature law to be valid for high velocity flows or flows with chemical reactions, a more general defect enthalpy law is proposed.

$$I_d^+ = I_\infty^+ - I^+ = f_2(y/\Delta) \quad . \tag{2-6a}$$

Following Clauser [14] one can define two thickness parameters that are related to the defect enthalpy profile by

$$\Delta_3 = \Delta \int_0^1 (I_\infty^+ - I^+) d(y/\Delta) \tag{2-7}$$

and

$$\Delta_4 = \Delta \int_0^1 (I_\infty^+ - I^+)^2 d(y/\Delta) \quad . \tag{2-8}$$

It can be shown that the relationship between T^+ and I^+ is

$$I^+ = \frac{1}{1 - E/2} \left(T^+ - \frac{E}{2} \frac{\rho_\infty}{\rho_o} \frac{(C_f/2)^{3/2}}{St} u^{+2} \right) \quad . \tag{2-9}$$

For the range of velocities considered in this study, T^+ and I^+ are essentially identical.

From (2-7), it is obvious that one can replace the ill-defined thermal boundary layer thickness with a more useful thickness parameter Δ_3. In this study, all defect enthalpy profiles will be shown as a function of y/Δ_3.

A defect enthalpy profile shape factor can be defined as

$$G_h = \frac{\Delta_4}{\Delta_3} \quad . \tag{2-10}$$

If outer layer similarity exists for the defect enthalpy, then G_h should be approximately constant. In this study, the equilibrium turbulent thermal boundary layer is defined as a boundary layer for which the defect enthalpy is a function of y/Δ_3, in the outer part of the layer.

2.3 Surface Temperature Variation

The surface temperature was kept at a constant value (for a given run) within the limits of the experimental apparatus. The temperature difference across the boundary layer varied from one run to the next but was kept in the range 20-30°F in order to minimize the influence of temperature-dependent properties.

2.4 Free Stream Velocity Variation

When Clauser [14] established his equilibrium momentum boundary layer, a long trial and error procedure was necessary. Bradshaw [15] concluded, from his own experiments and the earlier data of Clauser [14], that an adverse equilibrium momentum boundary layer would be experimentally established if the free stream velocity varied in the manner

$$u_\infty \sim x^m , \quad m < 0 . \tag{2-11}$$

Neither Clauser [14] nor Bradshaw [15] considered the effects of transpiration. In a companion study to the present work, done by Andersen [9], it was concluded that an equilibrium momentum boundary layer with transpiration could be experimentally established if the free stream velocity were given by (2-11), and if the transpiration fraction F is proportional to x^{m_F}, $m_F < 0$. It should be noted that m_F is a function of m, and this will be discussed in greater detail in the next section.

2.5 Transpiration Rate for Equilibrium Flows

For two-dimensional incompressible constant property flow, the momentum integral equation can be written in the form:

$$\frac{d}{dx}(\theta u_\infty^2) = \frac{\tau_o}{\rho}(1 + \beta + B_f) , \tag{2-12}$$

where $B_f = \rho v_o u_\infty / \tau_o$ is a momentum transfer blowing parameter. Andersen [9] demonstrated that if both β and B_f were constant, then G_f was also a constant and equilibrium flow was established. He also showed that if one makes three assumptions:

(a) $$u_\infty = u_1 x^m \quad ,$$

where u_1 and $m < 0$ are constants,

(b) $$(C_f/2)_o = a\, Re_\theta^{-b} \quad ,$$

where a and b are constants and $(C_f/2)_o$ is the skin friction for the non-transpired flow corresponding to (a), and

(c) $$\left(\frac{C_f}{C_{f_o}}\right)_{m,Re_\theta} = f(B_f) \quad ,$$

then the transpiration fraction F must vary according to

$$F \sim x^{m_F}, \quad m_F = -(1 + m)\frac{b}{1 + b} \tag{2-13}$$

We will now go through a similar analysis for the heat transfer problem. The energy integral equation for two-dimensional flow with negligible density fluctuation can be written as

$$\frac{d}{dx}(\rho_\infty u_\infty I_o \Delta_2) = \dot{q}_o''(1 + B_h) \quad , \tag{2-14}$$

where $B_h = \rho_o v_o I_o / \dot{q}_o''$ is a heat transfer blowing parameter. Physically, B_h represents the ratio of the transpiration energy flux to the wall heat flux. In comparing (2-12) and (2-14), note the absence of an explicit pressure gradient term analogous to β for the heat transfer problem. This leads one to suspect that the Stanton number behavior will be quite different from the skin friction behavior for adverse pressure gradient flows.

The analysis of Andersen [9] for the momentum transfer problem leads one to suspect that if we are able to experimentally establish a flow for which B_h is a constant, then G_h might also be constant. With this idea in mind, we will now proceed to determine the variation in transpiration rate necessary to experimentally establish a constant B_h flow.

In the analysis that follows, it will be necessary to make the following assumptions:

(a) $$u_\infty = u_1 x^m \quad ,$$

where u_1 is constant,

(b) $$St_o = a_1 \, Re_{\Delta_2}^{-b_1} \quad ,$$

where a_1 and b_1 are constants and St_o is the Stanton number for the free stream velocity variation given by (a) but for no transpiration, and

(c) $$\left(\frac{St}{St_o}\right)_{m,Re_{\Delta_2}} = f_1(B_h) \quad .$$

Assumption (c) implies that for a given pressure gradient, i.e., given $m < 0$, the ratio of St for the transpired flow to St for the non-transpired flow at the same enthalpy thickness Reynolds number Re_{Δ_2}, is a function of the heat transfer blowing parameter B_h only. This assumption was verified experimentally by Whitten [3] for the special case of $m = 0$ and will be verified for $m < 0$ in CHAPTER 4.

If we further assume constant properties and constant wall temperature, (2-14) can be written as

$$\frac{d\, Re_{\Delta_2}}{dx} = \frac{u_\infty}{\nu} St(1 + B_h) \quad . \tag{2-15}$$

Applying assumptions (a)-(c), (2-15) becomes

$$\frac{d\, Re_{\Delta_2}}{dx} = a_1 \frac{u_1}{\nu} f_1(B_h)(1 + B_h) x^m \, Re_{\Delta_2}^{-b_1} \quad . \tag{2-16}$$

The solution to (2-16), subject to the initial condition $Re_{\Delta_2} = 0$ at $x = 0$, is

$$Re_{\Delta_2} = \left[a_1 \frac{u_1}{\nu} f_1(B_h)(1 + B_h) \frac{b_1 + 1}{m + 1}\right] x^{\left(\frac{1+m}{1+b_1}\right)} \quad . \tag{2-17}$$

From the definition of B_h and assumption (b), one can write

$$F = B_h f_1(B_h) a_1 Re_{\Delta_2}^{-b_1} \quad . \tag{2-18}$$

Substituting for Re_{Δ_2} in (2-18), one finds that the transpiration rate variation necessary to maintain a constant B_h flow is given by

$$F \sim x^{m_F} \quad , \quad m_F = -b_1 \left(\frac{1 + m}{1 + b_1} \right) \quad . \tag{2-19}$$

On comparing (2-13) and (2-19), one concludes that the variation in the transpiration fraction F necessary to produce a constant B_f flow will also produce a constant B_h flow provided that b and b_1 are the same. Physically, b and b_1 are the slopes of a log-log plot of $(C_f/2)_o$ vs. Re_θ and $(St)_o$ vs. Re_{Δ_2}, respectively. From the data of Andersen [9] and the data to be reported in CHAPTER 4, $b = b_1 = 0.25$. Zero pressure gradient $(m = 0)$ is a special case of (2-19), and this case was studied experimentally by Simpson [1] and Whitten [3].

In conclusion, the boundary conditions that will yield a constant B_h flow will be taken to be

$$u_\infty \sim x^m \quad , \quad F \sim x^{m_F} \quad , \quad m_F = -b \left(\frac{1 + m}{1 + b} \right) \quad . \tag{2-20}$$

Establishing these boundary conditions should produce an equilibrium thermal boundary layer.

Before turning to the details of the boundary conditions established in this study, it should be pointed out that in developing these relationships, it has been assumed that the boundary layer, the pressure gradient, and the transpiration rate all have a common origin at $x = 0$. In this study, the origin of the momentum boundary layer was slightly upstream of the thermal boundary layer. Also, $x = 0$ corresponds to an infinite free-stream velocity and transpiration rate, both of which are physically impossible. Consequently, the actual conditions did not exactly match the desired ones near the beginning of the test section. The influence of the entrance effects should not drastically alter the

test results far downstream. This point will be discussed in greater detail in CHAPTER 5.

2.6 Actual u_∞ and F Variations

Three different nominal free stream velocity variations were established in this study. They each may be approximately represented by an equation of the form:

$$u_\infty = u_1 \left(\frac{x - x_o}{x_1 - x_o} \right)^m \quad . \tag{2-21}$$

The nominal constants in (2-21) for the three different pressure gradients of this study are tabulated in Table 2-1.

m	u_1(ft/sec)	x_o(in)	x_1(in)
0.00	31.1	-	-
-0.15	29.2	-3	4
-0.20	29.2	-2	4

Table 2-1: Nominal constants for free stream velocity variation

The transpiration boundary conditions considered in this study can be expressed in the form

$$F = F_1 \left(\frac{x - x_o}{x_1 - x_o} \right)^{m_F} \quad . \tag{2-22}$$

In addition to the B_h = constant flows, a series of F = constant flows were also established. The combinations of pressure gradient and transpiration rate considered are tabulated in Table 2-2.

m	F_1	m_F
0.00	0.000	-
-0.15	0.000	-
	±0.001	
	±0.002	0.00 and
	±0.004	-0.17
-0.20	0.000	-

Table 2-2: Nominal pressure gradient and transpiration rates studied

The zero pressure gradient ($m = 0$), no transpiration case was part of a series of qualification tests. Most of this study was concerned with the pressure gradient $m = -0.15$ for a wide range of transpiration rates.

2.7 Identification of the Boundary Conditions

From the previous section, it is obvious that the three parameters (m, F_1, m_F) nominally describe the pressure gradient and transpiration boundary conditions. Therefore, each run will be identified by these three parameters. For example, the run designation (-0.15, -0.004, -0.17) will indicate $u_\infty \sim x^{-0.15}$, $F_1 = -0.004$, and $F \sim x^{-0.17}$. For the runs with F constant, the third parameter m_F is not necessary. The run designation (-0.20, 0.000) indicates $u_\infty \sim x^{-0.20}$ and $F_1 = 0.000$ everywhere. For the constant B_h runs, a three-parameter designation is necessary, while only two are necessary for the constant F runs.

CHAPTER 3

EXPERIMENTAL APPARATUS, INSTRUMENTATION, AND QUALIFICATION TESTS

The basic apparatus used in this study was an open-end wind tunnel. The apparatus was first described by Moffat [2], and a description of subsequent modifications can be found in References [1] and [3]-[7]. A schematic diagram of the wind tunnel is shown in Figure 3-1.

The wind tunnel was originally designed for zero pressure gradient studies of the transpired turbulent boundary layer. Subsequent studies were concerned with accelerating flows. This heat transfer study and a parallel hydrodynamics study by Andersen [9] were concerned with adverse pressure gradient effects on the transpired turbulent boundary layer. Consequently, the only major modification of the basic apparatus was to design a new upper surface for the test channel used to create the pressure gradient. The adverse pressure gradient is created by a series of adjustable slots on the top wall which removes the boundary layer that forms along this upper surface.

Since the apparatus has been adequately described in the above references, only a brief description will be given below, along with a detailed description of any major modifications made for this study.

3.1 Main Air Flow

Referring to Figure 3-1, the main air flow enters the filter box, with the filter material being 0.7 micron retention felt-type material. The main air blower is of the centrifugal type and has a 2000 scfm capacity at 30 inches of water. The flow-turning header was designed to provide a uniform velocity at the heat exchanger. Honeycomb is placed both upstream and downstream of the main flow heat exchanger. This heat exchanger is supplied with cooling water from the Stanford University water system. During peak water-usage periods, considerable fluctuations were noted in the incoming water supply. Since this heat exchanger has a very high effectiveness, the fluctuating cooling water temperature caused a

fluctuating main air temperature. In order to damp these fluctuations, the cooling water is first passed through two large tanks in series, each with a capacity of approximately 5000 gal. The nominal cooling water flow rate was 40 gal/min.

After leaving the heat exchanger, the main flow air passes through 1-1/2 inch thick honeycomb with 3/16 inch cell size. Following the honeycomb and located in a constant area section 23 x 23 inches are six 32 x 32 mesh stainless steel screens. The function of this set of screens is to remove any non-uniformities in dynamic pressure. During the preliminary stages of this study, it was found that the last screen which the air passes through had a slight crease in it. This slight crease considerably affected the uniformity of the potential core in the test section and the screen had to be replaced.

Following the screen pack, the flow enters a 4:1 contraction (over 26 inches) nozzle. The nozzle provides an almost two-dimensional contraction from the 23 x 23 inch inlet to the 6 x 20 inch outlet. The nozzle is symmetric about both a vertical plane and a horizontal plane, with the contraction taking place primarily in the vertical plane. In the preliminary stages of this study, it was concluded that a separation occurred at the inlet of the nozzle. Consequently, the basic shape of the nozzle was modified to incorporate an initial contracting angle of approximately 5° downstream of the last screen.

At the exit of the nozzle, a 3/16 inch wide slot was cut across the bottom and side walls of the nozzle. Since the static pressure in the tunnel is slightly above atmospheric, this suction slot removes the boundary layer that develops in the nozzle. To insure a fully turbulent profile at the first test plate, a 1/32 inch high by 1/4 inch wide boundary layer trip is located 6 inches upstream of first test plate. There were no trips on the side or top walls.

3.2 Test Section

The test section consists of a 6 x 20 inch rectangular cross section duct 8 feet in length. The side walls are 1/2 inch plexiglass, the top is 5/16 inch aluminum tool plate, and the bottom wall (the actual test surface) is porous sintered bronze.

One of the side walls contains static pressure taps, which are used in conjunction with Kiel probes for total pressure. Free stream velocity variations can be deduced from these pressures. The side wall static pressure taps are 0.040 inch diameter with a sharp edge and are spaced two inches apart in the streamwise direction. The distance above the bottom wall test surface is 1 inch. Every 12 inches in the streamwise direction four additional pressure taps are provided at 2, 3, 4, and 5 inches above the test surface, on both side walls. The function of these vertical columns of pressure taps was to check the static pressure uniformity in the vertical and transverse directions. The side-to-side static pressure variation was found to be less than 0.002 inches of water. The pressure variation in the vertical direction was less than 0.001 inches of water, which is also the accuracy of the pressure measuring system. The static pressure taps are evident in Figure 3.2.

The bottom wall of the test section consists of 24 individual porous test plates, and they are mounted in four separate aluminum base castings. Each plate is thermally isolated from the base casting and the neighboring plates. The physical characteristics of the plates are as follows:

Material - sintered porous bronze

Dimensions - 18.0 x 3.975 x 0.25 inches

Particles - spherical, varying in diameter in the range 0.002-0.007 inches

Porosity - Approximately 40%, uniform within ±6% in center 6-inch section

Roughness - maximum of 200 microinches (RMS) measured with a stylus of 0.0005 inch radius

Thermal conductivity - 6.5 Btu/hr-ft-F, minimum

Surface emittance - 0.37 average.

Plate temperatures are monitored by five Iron/constantan thermocouples, each located 0.040 inches below the surface. The spacing of the plate thermocouples is shown in Figure 3.3. Each plate is electrically heated by nichrome wires which are located in grooves on the underside of the plate. Separate AC power supplies, both stabilized, are available for plates 1-12 and 13-24. In addition, the power supplied to each plate

is individually controlled by a rheostat. This allows one to vary the power to each plate individually to maintain a uniform surface temperature.

The upper wall of the test section is used to control the pressure gradient. It consists of a series of 24, 5/16 inch thick by 3.5 inches wide aluminum plates. These plates are arranged on top of the side walls such that there is a 1/2 inch space (in the flow direction) between adjacent plates. Each of the 23 resulting 1/2 inch wide slots is partially covered by two 1/2 inch thick aluminum bars. One of the above two bars is permanently fixed to the 3.5 inch plate, while the other bar is allowed to move relative to the fixed bar. The result is to form a slot whose width can be varied between 0 and 0.4 inches. A side view of the tunnel with the slot arrangement is shown in Figure 3-4. A feeler gauge allows the slot widths to be set to within 0.001 inches. Wing nuts are used to keep the movable bar in place once the slot width has been set and can be seen in Figure 3-2.

The test section is extended 14 inches past the last heated plate. A movable gate which slides up and down vertically is across this extension piece. This gate valve and a throttle valve at the main stream air blower are used to control the main stream air flow rate. The function of this extension is to insure that influence of the sliding gate valve is not appreciably felt at the last test station.

3.3 Transpiration Air System

The transpiration air system is quite similar to the main air system. The main difference is that after leaving the transpiration blower, the air goes to a header and then to 24 individually calibrated rotameters. Actually, the air supplied to a given plate can be routed to one of two rotameters, depending on the magnitude of the flow rate. By using the two rotameters in parallel, flow rates in the range of 0.5 to 18 scfm can be measured. Each of these 48 rotameters was individually calibrated by Kearney [7]. A typical transpiration compartment and plate assembly is shown in Figure 3-5.

3.4 Pressure Measurements

All pressure measurements were made with a STATHAM type PM-97 unbonded strain gauge differential pressure transducer for pressures in the range 0-1.4 inches of H_2O. The Wheatstone bridge was excited by a stable Hewlett-Packard model 6213A DC power supply. The output voltage from the pressure transducer was read by a Vidar 5206 D-DAS data acquisition system employing a digital PDP 8/L computer. The integration time was in the range of 6-10 seconds for each pressure measurement.

The pressure transducer was calibrated with a Meriam model 34FB2 micromanometer, and was found to be linear within ±0.001 inches of H_2O.

3.5 Velocity Measurements

The free stream velocity was determined by a Kiel probe, side wall static pressure taps, the pressure transducer, and Bernoulli's equation. The technique by which the slots were adjusted to obtain a given free stream velocity variation is described by Andersen [9]. The mean velocity profiles used in this thesis were taken from the parallel hydrodynamics study by Andersen [9], and were measured using a linearized constant temperature hot-wire anemometer. In general, the y-locations at which the velocity was measured differed from the y-locations at which the temperature was measured. Consequently, it was necessary to interpolate in the velocity profile to obtain data at the corresponding temperature y-locations. The interpolation scheme used was an average of two three-point Lagrangian interpolations, centered about the data point in question.

The data of Andersen [9] was taken under isothermal conditions. The corresponding data of this study was taken with a boundary layer temperature difference of 20-30°F. Consequently, some care must be exercised in using isothermal hydrodynamics data with the slightly variable density data of this study. Typically, the density ratio ρ_∞/ρ_0 was of the order 1.04. Thielbahr [6] investigated, both experimentally and numerically by a computer solution of the boundary layer equations, the question of which one of the following quantities would most nearly be preserved: a) u/u_∞, b) $\rho u/\rho_\infty u_\infty$, or c) $\rho u^2/\rho_\infty u_\infty^2$. He found that, under similar free-stream conditions, the minimum error in the computation of integral parameters

by mixing isothermal and non-isothermal data was achieved by assuming the preservation of u/u_∞. The same procedure was followed in this study.

3.6 Skin Friction

The skin friction reported in this study is taken directly from the parallel study of Andersen [9]. Kays [16] reports that the effect of variable properties on skin friction can be approximately correlated by

$$\frac{C_f}{(C_f)_{cp}} = \left(\frac{T_o}{T_\infty}\right)^n , \qquad (3\text{-}1)$$

where the exponent $n = -0.5$ is valid for this study. This indicates that the variable property skin friction should be approximately 2% lower than the corresponding constant property skin friction. Since the data of Andersen [9] are not accurate to within 2%, it was concluded that this correction was not justified.

3.7 Mean Temperature Profile Measurements

Considerable time was spent in developing a boundary layer temperature probe that would have acceptable conduction losses when used near the wall. The final probe design is shown in Figure 3-6. The sensing element of the probe is a Chromel/constantan thermocouple of 0.003 inch diameter wire. The thermocouple junction is formed by butt welding the two thermoelectric elements together. After welding, the wire was rolled between two pieces of flat steel in order to remove any kinks. The sensing element was supported between two 22 gauge stainless steel hypodermic needles with the teflon-coated wire being inside the hypodermic needle. This teflon coating was burned off the part of the thermocouple that was exposed to the air stream. Consequently, contact between the bare wire and the hypodermic needle occurred only at the end of the hypodermic needle. Since the two hypodermic needles were electrically insulated from each other, this contact did not introduce any error. The shape of the hypodermic needles was such as to give some spring to the probe assembly when in contact with the wall. The span between the probe prongs was approximately 0.5 inches, with the junction in the middle of the span.

APPENDIX A presents an analysis of the expected temperature distribution in the probe and the approximate temperature error.

After the probe was assembled, an optical comparator was used to insure that both prongs would touch the wall at approximately the same time. This was accomplished to within 0.0015 inches. From the experimental temperature profiles, a difference in y-location of 0.0015 inches, in very near the wall, might cause the two ends of the probe to be at temperatures that differ by 0.3°F for the strongest blowing run to 1.5°F for the strongest suction run. Consequently, it should be expected that the probe performance in near the wall would be the worst for the suction runs. Therefore, it was decided that the first data point greater than $y^+ = 3 - 9$ (depending on the transpiration rate and pressure gradient) would be forced to match the laminar sublayer equation. This was accomplished by shifting all of the y-locations (for a given profile) by a fixed amount. Typically, this shift was ±0.0015 inches.

The boundary layer temperature probe was mounted in a micrometer-traversing mechanism that was adjustable to the nearest 0.001 inch.

The temperature probe should measure a temperature somewhere between the local static and the stagnation temperature. In this study, it was assumed that the static temperature is related to the indicated probe temperature by the relationship

$$T = T_{probe} - r \frac{u^2}{2g_c J c_p} , \qquad (3\text{-}2)$$

where r, the recovery factor, was taken to be $(Pr)^{1/3}$. The maximum value of the quantity $u^2/2g_c J c_p$ for this study was about 0.08°F. Hence, the actual value of the recovery factor was not significant for the velocities of this study.

3.8 Stanton Number

The Stanton number reported in this study is defined through the relationship

$$St = \frac{\dot{q}''_o}{\rho_\infty u_\infty I_o} , \qquad (3\text{-}3)$$

where $\dot{q}_o''$ is the wall heat flux and I_o is the stagnation enthalpy at the wall referenced to the free stream stagnation enthalpy. The static enthalpy was calculated from the static temperature by

$$i = c_p T \quad ,$$

where the specific heat c_p was assumed to be independent of temperature but did depend on the water vapor present in the air. The relative humidity was determined with a sling psychrometer and the mass fraction of water vapor was computed using the data of Keenan [17].

The wall heat flux $\dot{q}_o''$ was determined by performing an energy balance on the center six-inch section of each test plate. This energy balance can be written symbolically as

$$\text{Power} = \text{Convection} + \text{Transpiration} + \text{Losses} \quad , \qquad (3\text{-}4)$$

where

Power - electrical power used to heat the plates

Convection - wall heat flux $\dot{q}_o''$

Transpiration - energy flux due to mass injection

Losses - heat transfer to the surroundings by radiation from the top and bottom of the plate and conduction from the plate to its supports.

The mathematical model for the loss terms is the same as that used by Kearney [7] and will not be discussed here. The thermocouples in the plates and a thermocouple in the underbody of the transpiration compartment were used to measure the temperature of the transpiration air. The electrical power was measured by a Singer model DW precision watt meter.

3.9 Qualification of the Apparatus

A series of tests was performed to qualify the basic characteristics of the apparatus. These tests consisted of (1) transpiration energy balances, (2) transverse uniformity of the mean temperature and velocity

profiles, (3) boundary layer energy balances, and (4) repeatability of earlier zero pressure gradient, zero transpiration studies of Moffat [2], Whitten [3], Theilbahr [6], and Kearney [7].

3.9.1 Transpiration Energy Balances

If there is no main stream flow in the wind tunnel, the Convection term in the energy balance Equation (3-4) is identically zero.* Consequently, the left and right hand sides of (3-4) can be evaluated independently. Any discrepancy between the left and right hand sides of (3-4) will be an energy imbalance. Let us define an energy imbalance term as

$$\Delta E = \text{Power} - (\text{Transpiration} + \text{Losses}) \quad . \tag{3-5}$$

Since we are more concerned with the effects of this energy imbalance on the Stanton number under actual operating conditions, let us define

$$\Delta St = \frac{\Delta E}{\rho_\infty u_\infty I_0} \quad . \tag{3-6}$$

Since the term in the denominator of (3-6) may depend on the particular run as well as the x-location of a given run, the denominator was given the nominal value of

$$\rho_\infty u_\infty I_0 = (0.075 \text{ lbm/ft}^3)(25 \text{ ft/sec})(64.8 \text{ Btu/lbm}) \quad . \tag{3-7}$$

The results of the blowing and suction energy balance tests are shown in Figures 3-7 and 3-8, respectively. The range of blowing and suction considered in these tests span the nominal range of blowing and suction considered in the runs with main air flow. The majority of the plates show an energy imbalance within 0.0001 Stanton number units. This is consistent with the earlier findings of Kearney [7].

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* In the suction mode, the energy balance control volume must be extended to $+\infty$ in the y-direction in order for this to be true.

3.9.2 Inlet Velocity and Temperature Uniformity

Velocity and temperature profiles were taken at nine transverse locations corresponding to an x-location of 10 inches; $Z = -8, -6, \ldots, 6, 8,$ inches. The results are shown in Figures 3-9 through 3-12. Both velocity and temperature profiles are very uniform, especially over the central portion of the test section. As was expected, the velocity profiles at $z = \pm 8$ inches show the greatest deviation, due to the side wall boundary layer. The same problem does not exist with the temperature profile. For additional comments on the velocity uniformity, see Andersen [9].

3.9.3 Boundary Layer Energy Balances

The Stanton number was determined experimentally without making use of any of the temperature or velocity profile data. However, any heat transfer at the wall must be distributed within the thermal boundary layer. Consequently, the measured temperature profiles must be consistent with the measured heat flux at the wall. This consistency can be examined with the aid of the energy integral equation. Anticipating that any real flow such as the ones studied here has some amount of three-dimensionality, let us develop the energy integral equation for a flow in which the convective motion is three-dimensional but the shear stress and heat flux have only one component. The continuity and energy equations can be written as

$$\frac{\partial}{\partial x}(\rho u) + \frac{\partial}{\partial y}(\rho v) + \frac{\partial}{\partial z}(\rho w) = 0 \quad , \tag{3-8}$$

$$\frac{\partial}{\partial x}(\rho u I) + \frac{\partial}{\partial y}(\rho v I) + \frac{\partial}{\partial z}(\rho w I) = -\frac{\partial \dot{q}''}{\partial y} + \frac{\partial}{\partial y}(\tau u) \quad . \tag{3-9}$$

Integrating (3-9) with respect to y between the wall and infinity, one obtains

$$St + F = \frac{1}{\rho_\infty u_\infty I_0}\frac{d}{dx}(\rho_\infty u_\infty I_0 \Delta_2) + 3\text{-D} \quad , \tag{3-10}$$

where the three-dimensional term is given by

$$3\text{-}D = \frac{1}{\rho_\infty u_\infty I_0} \frac{d}{dz} \int_0^\infty \rho w I dy \quad . \tag{3-11}$$

Insight can be gained into the 3-D term by restricting the analysis to flow in a convergent or divergent channel where the streamlines all originate from a single point. Following Schlichting [18], we have

$$\frac{w}{u} = \frac{z}{x + a} \quad , \quad \left.\frac{\partial w}{\partial z}\right)_{z=0} = \frac{u}{x + a} \quad . \tag{3-12}$$

Substituting (3-12) into (3-11), we obtain

$$3\text{-}D = \frac{1}{\rho_\infty u_\infty I_0} \frac{d}{dz} \left(\frac{z}{x + z} \rho_\infty u_\infty I_0 \Delta_2 \right) \quad . \tag{3-13}$$

Since the primary temperature and velocity profiles were taken along the center line $(z = 0)$ of the wind tunnel, it seems reasonable to restrict (3-13) to $z = 0$. Consequently,

$$3\text{-}D)_{z=0} = \frac{\Delta_2}{x + a} \quad . \tag{3-14}$$

Diverging streamlines correspond to $x + a > 0$, while converging streamlines correspond to $x + a < 0$.

If plate energy balances were not available, one could compute the Stanton number from the temperature profiles and the energy integral equation. However, it would be necessary to evaluate the 3-D term. Consequently, we will use the energy integral equation to tell us something about the magnitude of the 3-D effects.

Let us define a two-dimensional Stanton number through the relationship

$$(St)_{2\text{-}D} = \frac{1}{\rho_\infty u_\infty I_0} \frac{d}{dx} (\rho_\infty u_\infty I_0 \Delta_2) - F \quad . \tag{3-15}$$

The two-dimensional Stanton number and the actual plate Stanton number are then related by

$$St = (St)_{2\text{-}D} + 3\text{-}D \quad . \tag{3-16}$$

From (3-16), and the physical situation, we conclude that

$$\begin{aligned} St &> (St)_{2\text{-}D}, \quad \text{diverging streamlines} \quad , \\ St &< (St)_{2\text{-}D}, \quad \text{converging streamlines} \quad . \end{aligned} \tag{3-17}$$

For all the data presented in this study, the term $(St)_{2\text{-}D}$ was calculated. The results are presented in the data tabulation, CHAPTER 9. In general, the flow exhibited a slight amount of streamline divergence. The exception was the high blowing runs which had streamline divergence at the beginning of the test section but streamline convergence at the end of the test section. In computing the derivative in (3-13), a least-squares curve fit of the form

$$\rho_\infty u_\infty \Delta_2 = \alpha_1 (x + \alpha_2)^{\alpha_3} \tag{3-18}$$

was generated and the derivative evaluated analytically. The I_o term was omitted under the assumption of constant wall temperature.

3.9.4 Zero Pressure Gradient, Zero Transpiration Flow

The zero pressure gradient, zero transpiration turbulent boundary layer has been studied by many investigators. Therefore, this flow provides a good test of the wind tunnel and data-reduction system.

All of the Stanton number data for this study will be presented in the form of Stanton number vs. enthalpy thickness Reynolds number. Stanton numbers were measured for each of the 24 test plates, but the data from plates 1, 2, and 24 will not be presented because of entrance and exit effects and conduction losses. Boundary layer measurements of enthalpy thickness Reynolds numbers are available only for the x-locations where temperature and velocity profiles were measured (8 or 9 stations). Kearney [7] obtained Re_{Δ_2} for the centerline of each plate by solving (3-10) for Δ_2 and neglecting the 3-D term.

$$\rho_\infty u_\infty I_0 \Delta_2 = (\rho_\infty u_\infty I_0 \Delta_2)\Big|_{x_0} + \int_{x_0}^{x} \rho_\infty u_\infty I_0 (St + F)dx \quad . \qquad (3\text{-}19)$$

This approach has the disadvantage that the Re_{Δ_2} computed from (3-19) can differ considerably from Re_{Δ_2} obtained from profile measurements because of streamline convergence or divergence. Since this is a cumulative effect, the error will increase with x. It was felt that a better approach would be to least-squares curve-fit the profile enthalpy thickness Reynolds number in the form

$$Re_{\Delta_2} = \alpha_1 (x + \alpha_3)^{\alpha_2} \qquad (3\text{-}20)$$

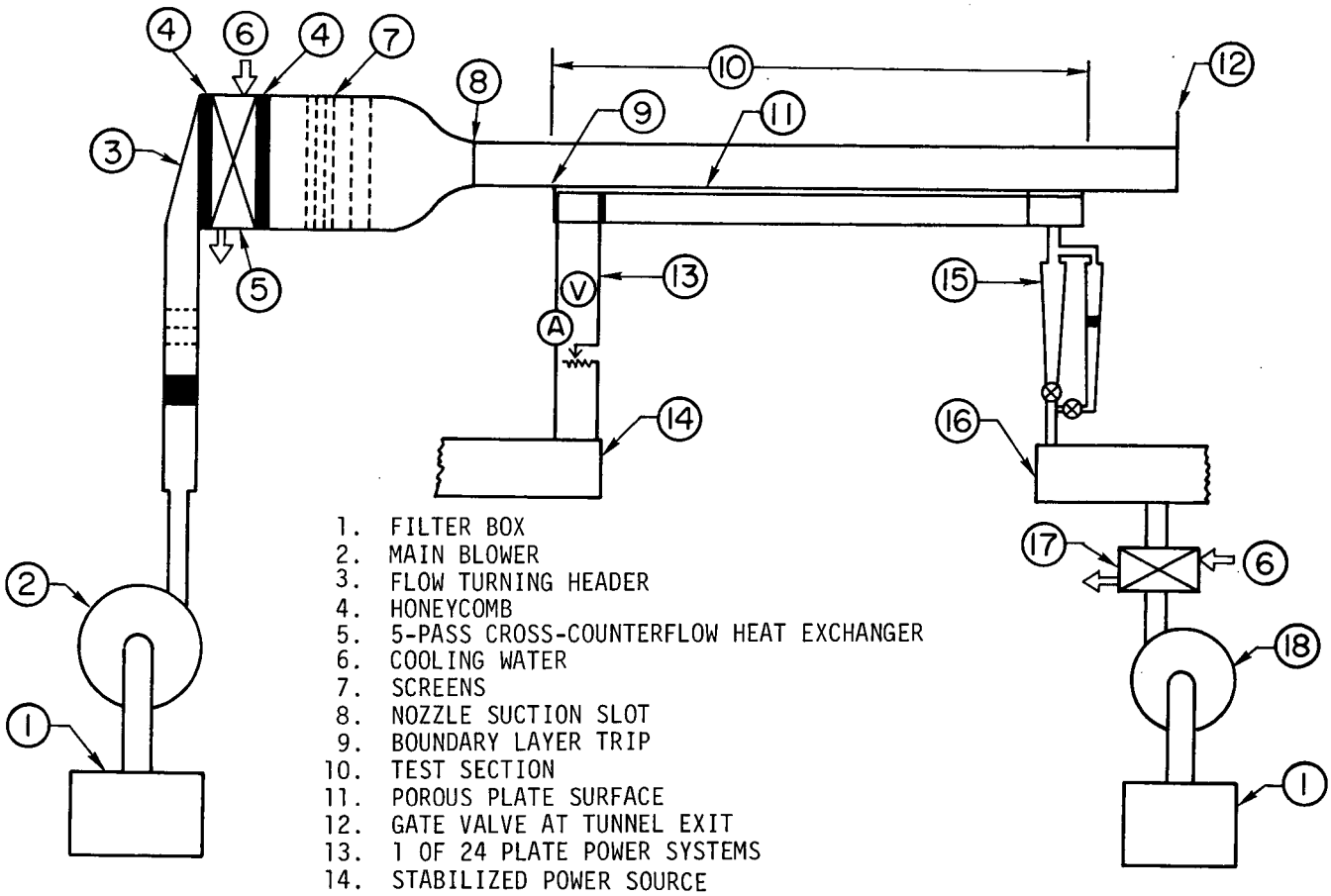
and then evaluate the curve fit at the plate centerline x-locations. Equation (3-20) was found to be a very good representation for all of the data presented in this study. All of the values of Re_{Δ_2} that are tabulated in CHAPTER 9 under the heading of Stanton number results were obtained from (3-20). The actual values of Re_{Δ_2} computed from the profile measurements are tabulated in the temperature profile results section of CHAPTER 9.

Figure 3-13 shows a comparison of the zero pressure gradient, zero transpiration data of this study with the earlier data of Kearney [7]. The comparison is very good, with the worst deviation occurring at the higher Reynolds numbers. This discrepancy can be explained by the different manner in which Re_{Δ_2} was computed. Kearney [7] indicated that a slight streamline divergence was present in his flat plate data. This effect indicates that his Re_{Δ_2} computed from (3-19) would be larger than the corresponding profile measurements. If Kearney's data are shifted to the left in Figure 3-13 to account for this streamline divergence, the agreement would be even better.

Using the step function solution presented by Reynolds [20], it can be shown that the effects of an unheated starting length for the zero pressure gradient turbulent boundary layer can be approximately accounted for by the relationship

$$St = (St)_{eq} \left(Pr^{0.4} \frac{Re_{\Delta_2}}{Re_\theta} \right)^{5/36} , \quad \frac{Re_{\Delta_2}}{Re_\theta} < 1 , \qquad (3\text{-}21)$$

where $(St)_{eq}$ denotes the value of Stanton number that would have existed if both boundary layers had a common origin. The closed symbols in Figure 3-13 have been moved upward according to (3-21). The solid line in Figure 3-13 was taken from Moffat [19]. The agreement is quite good.



1. FILTER BOX
2. MAIN BLOWER
3. FLOW TURNING HEADER
4. HONEYCOMB
5. 5-PASS CROSS-COUNTERFLOW HEAT EXCHANGER
6. COOLING WATER
7. SCREENS
8. NOZZLE SUCTION SLOT
9. BOUNDARY LAYER TRIP
10. TEST SECTION
11. POROUS PLATE SURFACE
12. GATE VALVE AT TUNNEL EXIT
13. 1 OF 24 PLATE POWER SYSTEMS
14. STABILIZED POWER SOURCE
15. 1 OF 24 TRANSPIRATION ROTAMETERS
16. TRANSPIRATION HEADER
17. TRANSPIRATION HEAT EXCHANGER
18. TRANSPIRATION BLOWER

Figure 3-1 Schematic of test apparatus

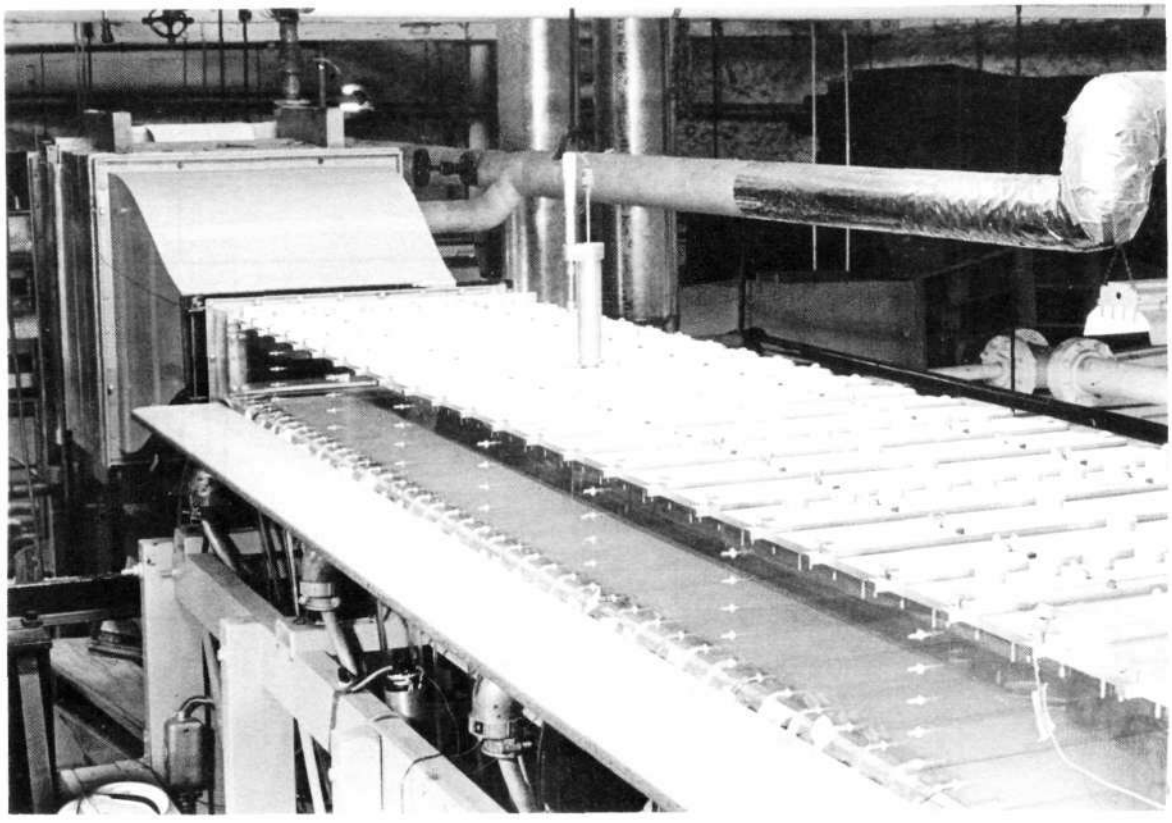


Figure 3-2 Photograph of test section with traversing mechanism in position

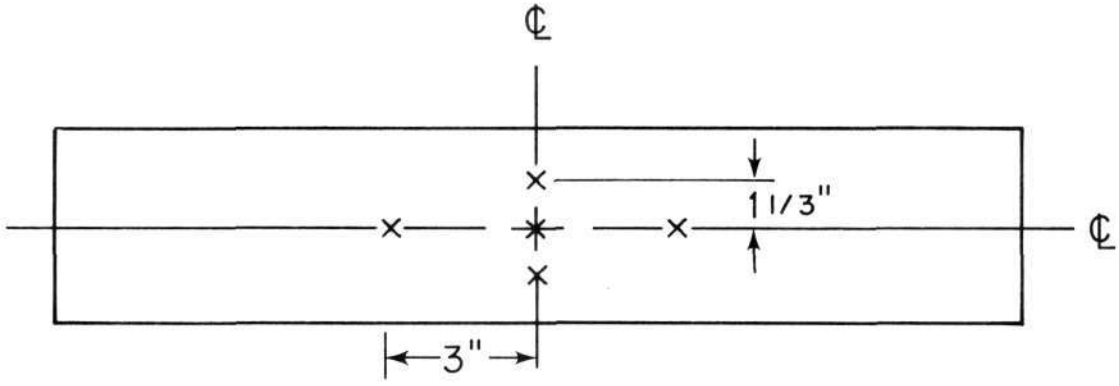


Figure 3-3 Spacing of plate thermocouples

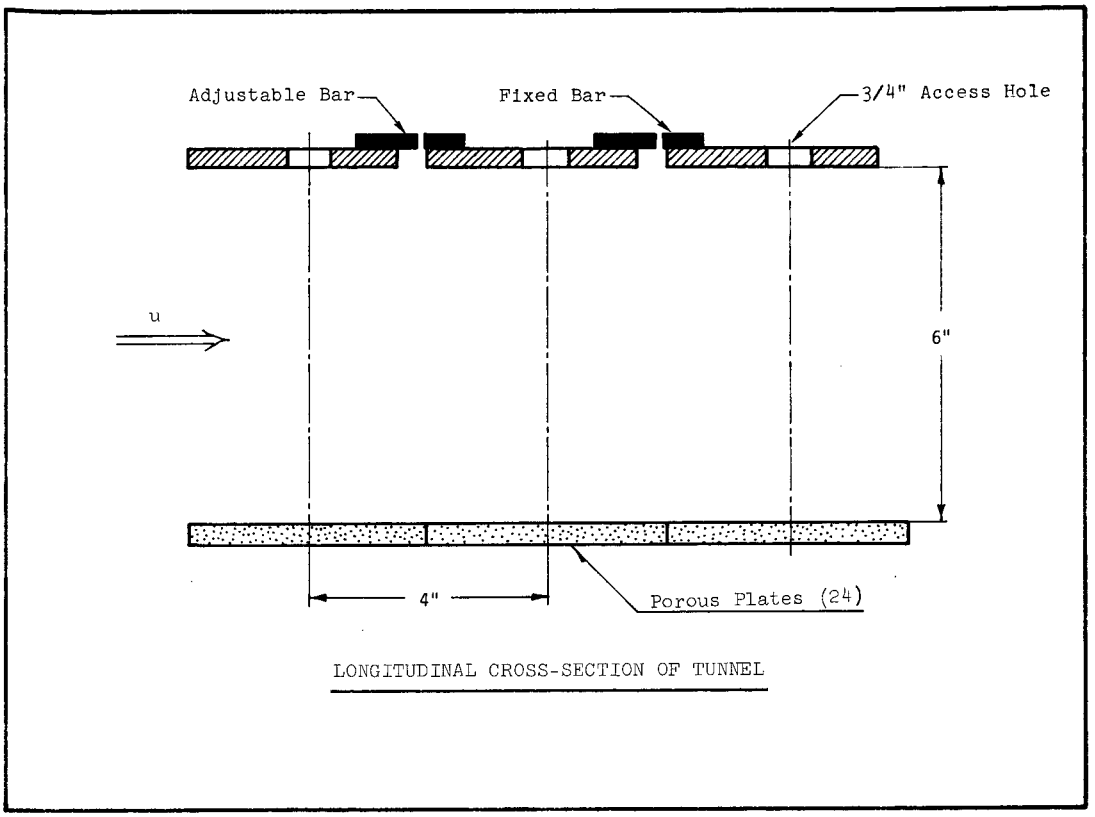
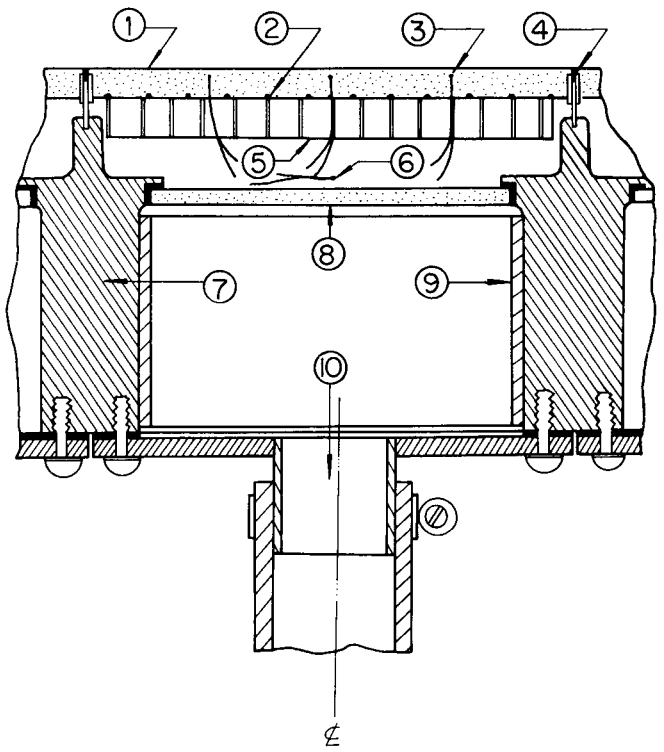


Figure 3-4 Longitudinal cross section of tunnel test section



1. Porous plate
2. Heater wires
3. Thermocouples
4. Support webs
5. Honeycomb
6. Thermocouple
7. Base casting
8. Pre-plate
9. Balsa insulation
10. Delivery tube

Figure 3-5 Cross section view of typical compartment

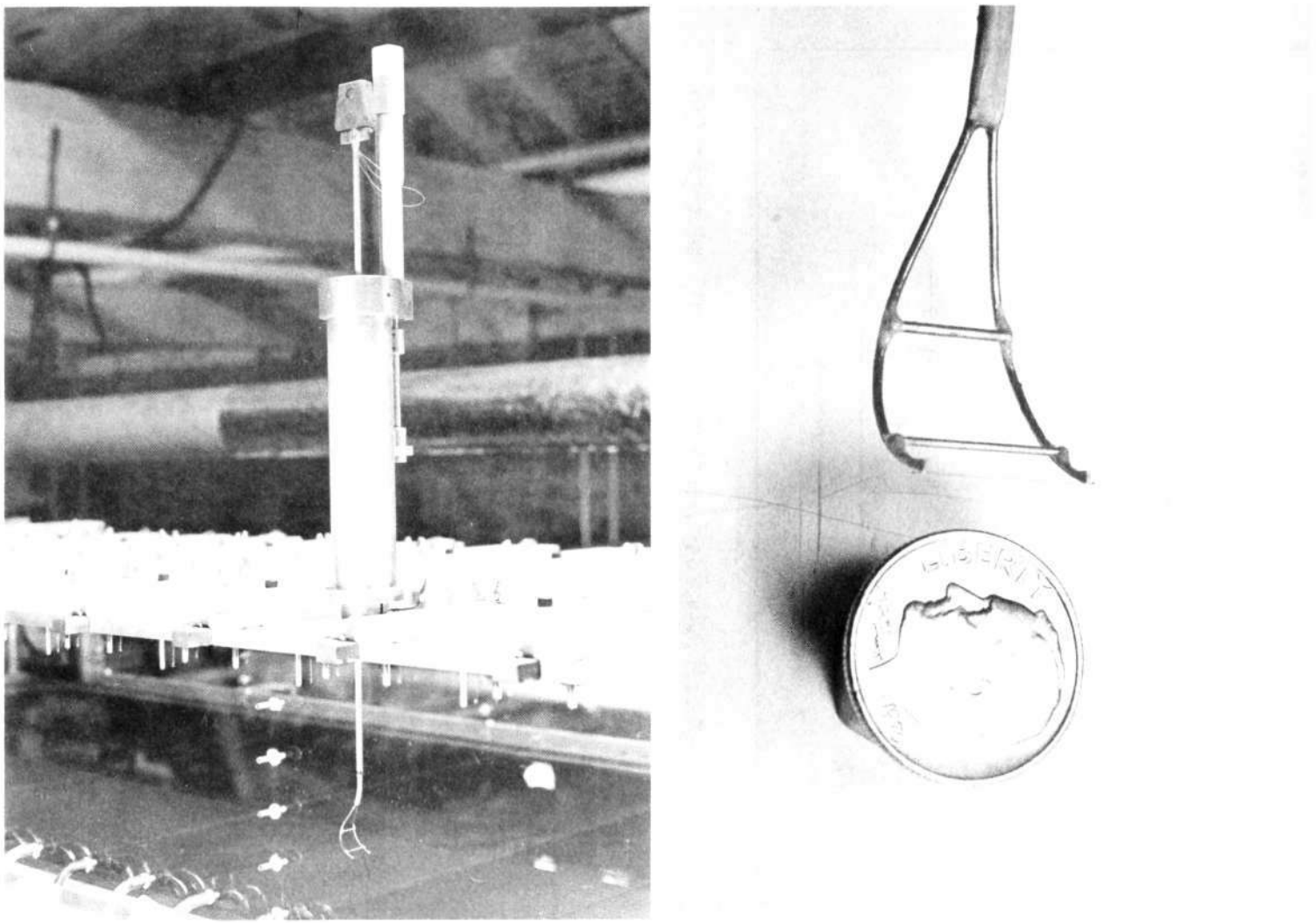


Figure 3-6 Photograph of traversing mechanism and temperature probe

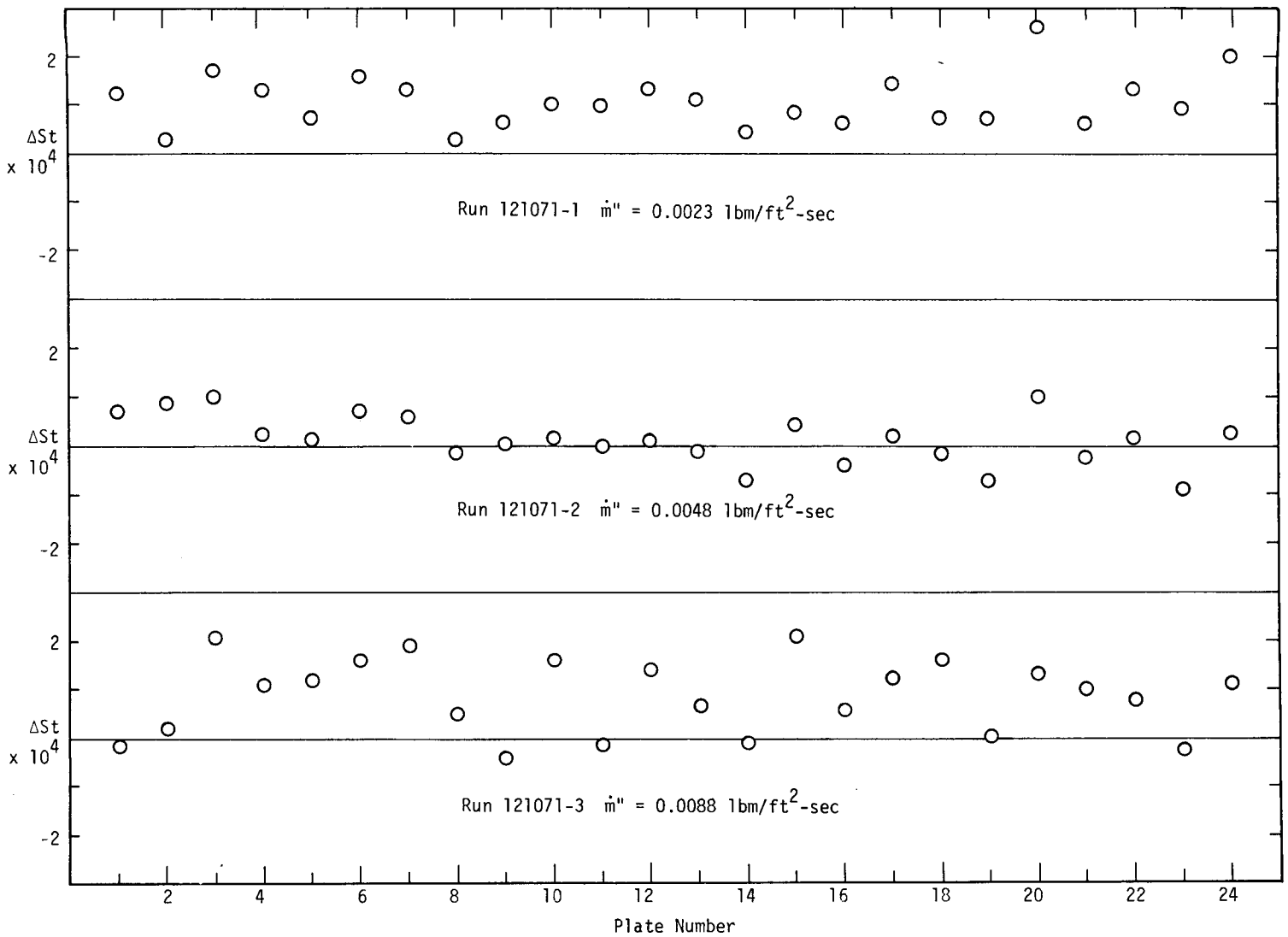


Figure 3-7 Transpiration energy balances for blowing mode

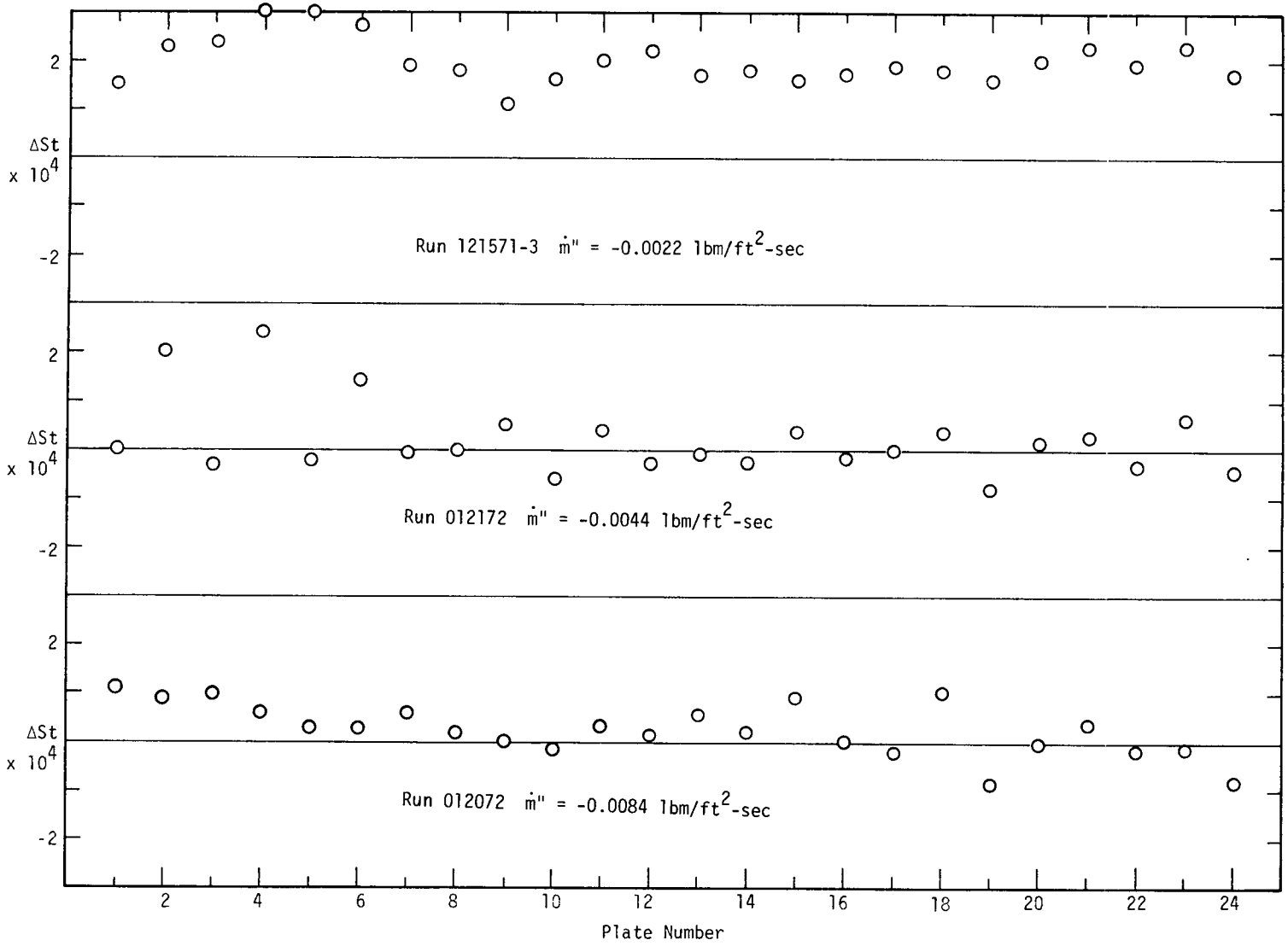


Figure 3-8 Transpiration energy balances for suction mode

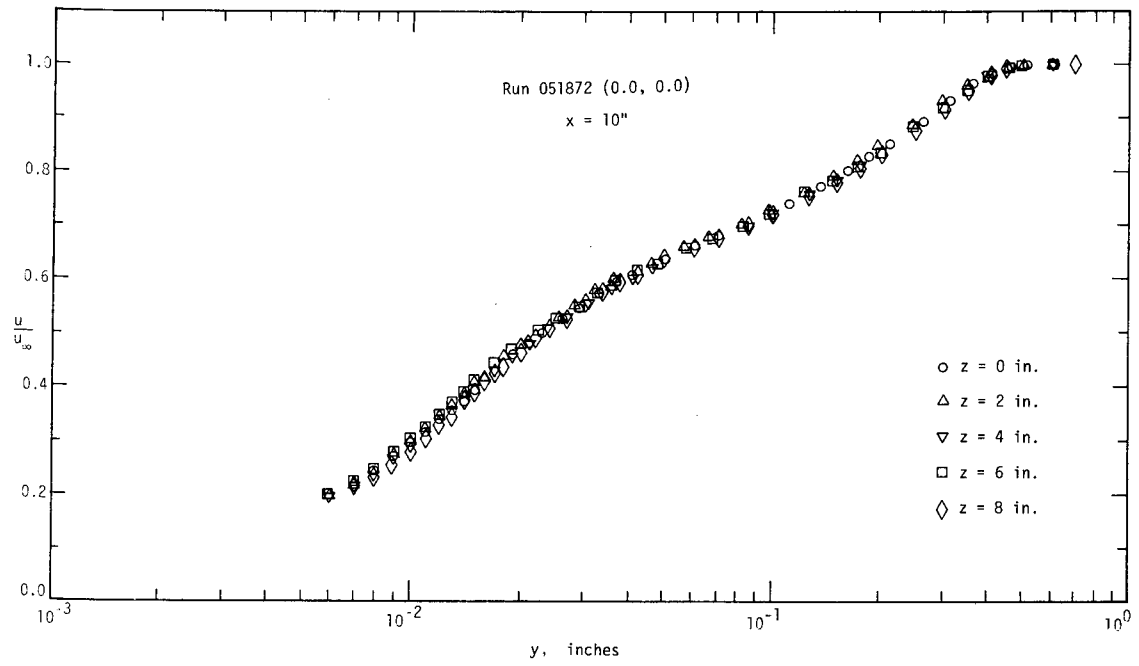


Figure 3-9 Transverse velocity profiles, $z > 0$, $x = 10$ inches

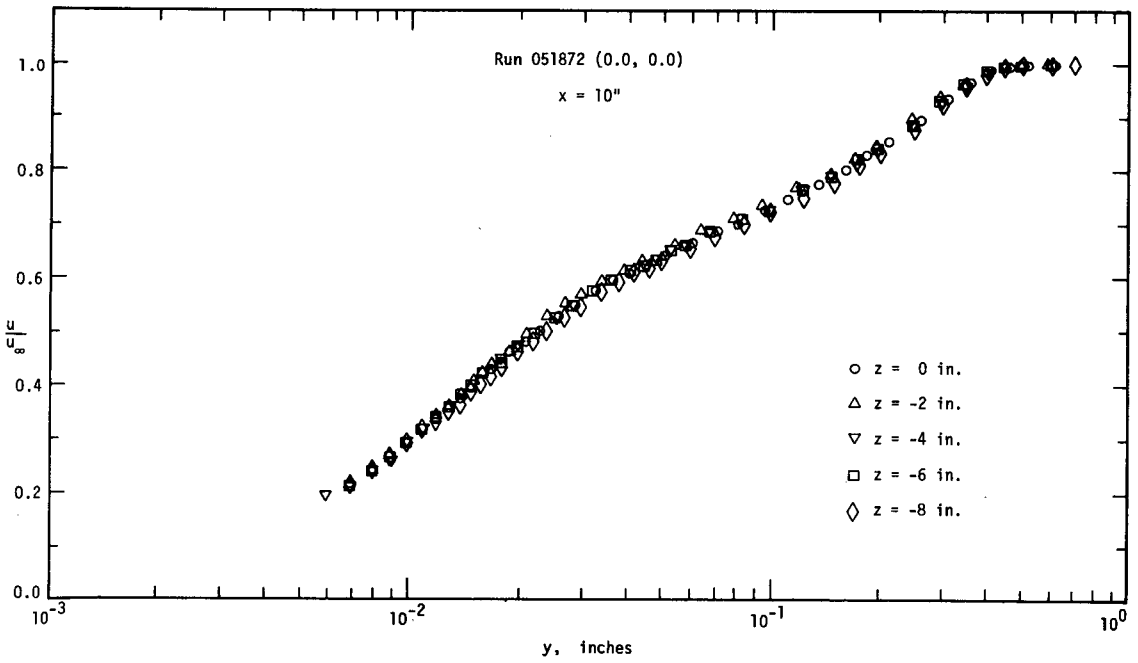


Figure 3-10 Transverse velocity profiles, $z < 0$, $x = 10$ inches

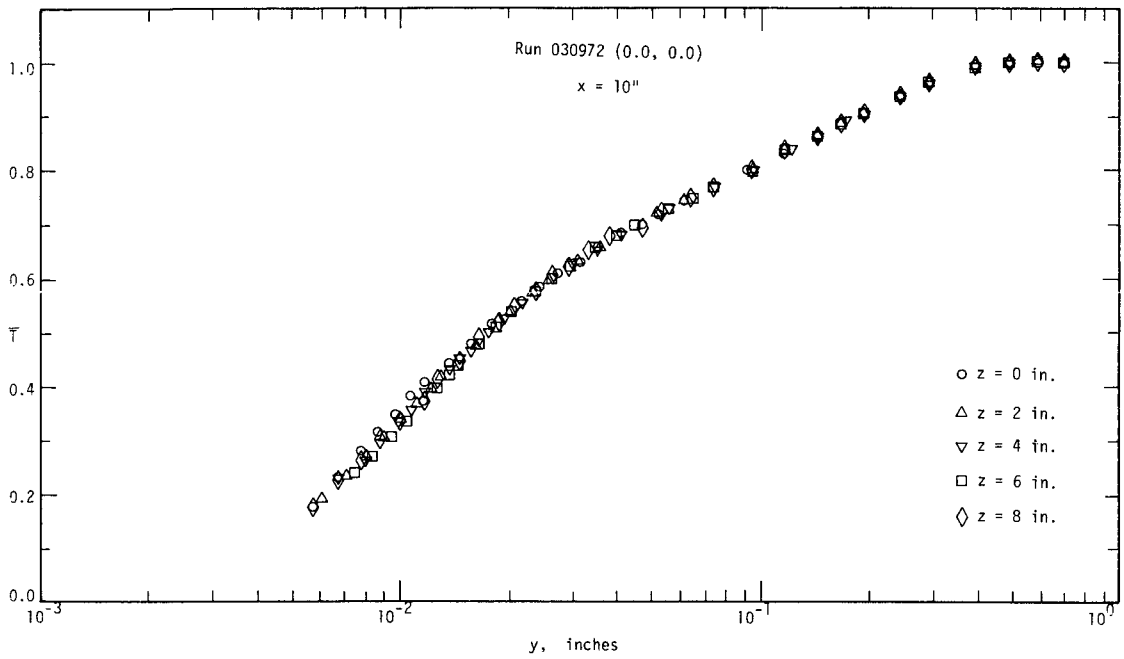


Figure 3-11 Transverse temperature profiles, $z > 0$, $x = 10$ inches

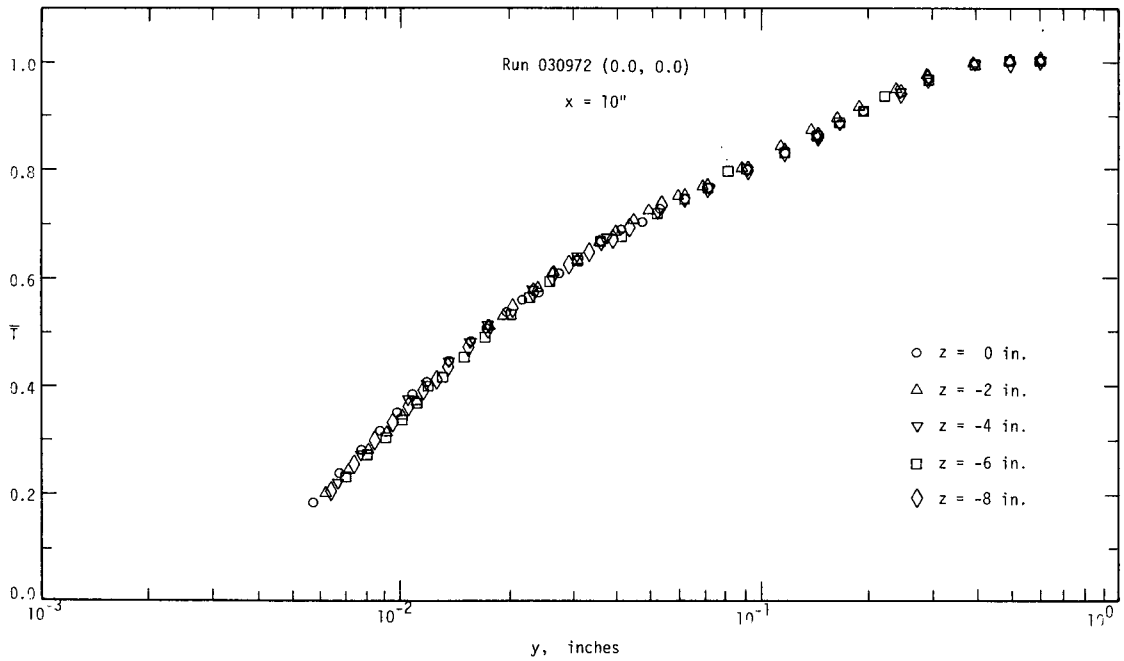


Figure 3-12 Transverse temperature profiles, $z < 0$, $x = 10$ inches

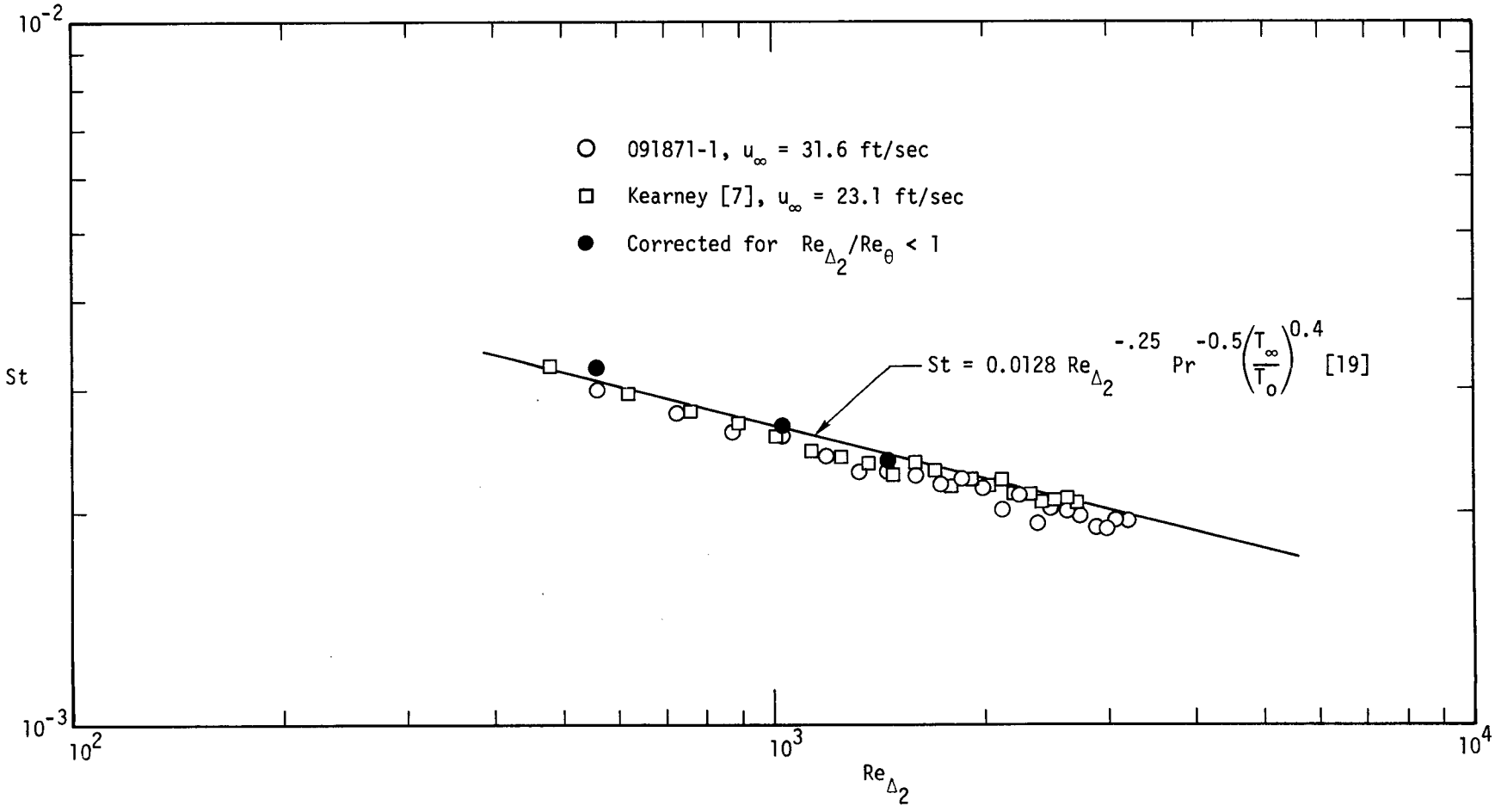


Figure 3-13 Zero pressure gradient, zero transpiration Stanton number data

CHAPTER 4

PRESENTATION OF EXPERIMENTAL STANTON NUMBER DATA

In this study, a total of 15 different combinations of pressure gradient and transpiration boundary conditions were investigated experimentally. The various boundary conditions will be divided into three categories: (1) no transpiration, (2) constant F with $m = -0.15$, and (3) constant $B_h \triangleq F/St$ with $m = -0.15$. Strictly speaking, the zero transpiration runs have constant $B_h = 0$ but they will still be treated as a separate case. The assumptions made in Section 2.5 as to how one would generate a constant B_h flow will also be verified.

For a given set of boundary conditions, the Stanton number data were taken twice; once before the temperature profiles were taken and once after. This provides a check on the repeatability of the data. In this chapter, only the first run will be presented. By checking the Stanton number data tabulation in CHAPTER 9, one can verify that the repeatability of the data was quite good. Using the methods of Kline [33] and the computer program of Kearney [7], the Stanton number uncertainty was estimated to be within 0.0001 Stanton number units.

4.1 Stanton Numbers for No Transpiration Flows

Figure 4-1 shows the influence of pressure gradient on the Stanton number for no transpiration. Within the uncertainty of the data, the two adverse pressure gradient flows have the same $St = f(Re_{\Delta_2})$ relationship as the zero pressure gradient. In contrast, the skin friction data of Andersen [9] for the same three flows shows that increasing adverse pressure gradient causes a decrease in skin friction for a given value of momentum thickness Reynolds number. This indicates that the Reynolds analogy between heat and momentum transfer is definitely not valid for adverse pressure gradient flows.

If the Stanton number data is plotted as a function of x, the streamwise distance, increasing adverse pressure gradient causes an increase in Stanton number for a given value of x. The enthalpy

thickness Reynolds number decreases with increasing adverse pressure gradient, for a given value of x. For skin friction, adverse pressure gradient yields the opposite trend.

Even though the data in Figure 4-1 indicates no influence of adverse pressure gradient (within the uncertainty of the data), it is felt that a slight increase in Stanton number actually does occur. This was concluded by least-square curve-fitting St vs Re_{Δ_2} in the form

$$St = a\, Re_{\Delta_2}^{b} \tag{4-1}$$

and evaluating the curve fit. The curve fit coefficients are tabulated in Table 4-1.

m	a	b
0.0	0.0144	-0.25
-0.15	0.0147	-0.25
-0.20	0.0161	-0.26

Table 4-1: Curve fit coefficients for non-transpired flows

4.2 Constant F Flows, m = -0.15

The Stanton number data for all of the constant F boundary conditions with $m = -0.15$ is shown in Figure 4-2. As was expected, blowing decreases the Stanton number while suction increases the Stanton number.

4.3 Constant B_h Flows, m = -0.15, m_F = -0.17

The Stanton number data for the constant B_h boundary conditions is shown in Figure 4-3. The constant B_h flows show the same trends with blowing and suction as the constant F flows. Note that the St vs Re_{Δ_2} curves for the constant B_h flows are approximately parallel.

As stated previously, two sets of Stanton data were taken for each set of boundary conditions. A "best interpretation" of these two runs was obtained by least-square curve-fitting the two runs together by an equation of the form

$$St = a(x + b)^c \qquad (4\text{-}2)$$

and evaluating the resulting curve-fit at the x-locations corresponding to the plate centerline. The results for the $m = -0.15$ data are shown in Figure 4-4. The constant F runs (solid curve) have the nominal value of F on the left of each curve; the constant B_h runs have the nominal value of B_h on the right of each curve. The data tabulated under the heading STNA in CHAPTER 9 was obtained from (4-2).

In Section 2.5, it was assumed that the ratio of Stanton number to the non-transpired Stanton number, for a given pressure gradient and enthalpy thickness Reynolds number, is a unique function of the transpiration parameter $B_h = F/St$. This assumption was expressed in the form

$$\left.\frac{St}{St_o}\right)_{m,Re_{\Delta 2}} = f_1(B_h) \qquad (4\text{-}3)$$

All of the Stanton number data was plotted in the form of (4-3) and is shown in Figure 4-5. This figure not only verifies (4-3) for the constant B_h flows, but it also shows that if $\dot{m}''$ varies slowly (as was the case for the F = constant runs) the Stanton number ratio is a unique function of B_h , for a given pressure gradient. This fact might prove useful in an integral method for predicting heat transfer.

4.4 Comparison of Adverse Pressure Gradient Stanton Numbers With Zero Pressure Gradient Data

Since most people are more familiar with Stanton number data for zero pressure gradient, it will be useful to compare the adverse pressure gradient data of this study with the earlier zero pressure gradient data of Moffat [2]. Figure 4-6 compares selected constant F runs of this study with the corresponding data of Moffat. The zero pressure gradient, no transpiration data is shown in order to have a reference. (The (-0.15, 0.000) flow could also have been shown but the data in Figure 4-1 indicates that it is extremely close to the (0.00, 0.000) flow). The data sets are arranged in the order of increasing F . For small values of $|F|$

(blowing and suction), the mild adverse pressure gradient of this study does not appreciably alter the $St = f(Re_{\Delta 2})$ relationship, when compared to the zero pressure gradient data. For the larger values of $|F|$, the effect of adverse pressure gradient is to decrease St for a given $Re_{\Delta 2}$. The run where the pressure gradient has the most effect was the strongest blowing rate. Part of this difference is possibly due to the uncertainty in the data. It was estimated that the uncertainty was ± 0.0001 Stanton number units. In this case, the uncertainty band for each of the two runs is almost overlapping.

4.5 Asymptotic Suction Layer for $u_\infty \sim x^m$ Flows

The constant property, constant wall temperature energy integral equation can be written as

$$\frac{d\Delta_2}{dx} = St + F - m\frac{\Delta_2}{x-x_o} \quad , m < 0 \qquad (4\text{-}5)$$

The term $\Delta_2/(x-x_o)$ should approach zero for large values of x because Δ_2 is approaching a constant value. Therefore, we conclude that for the type of adverse pressure gradients of this study, an asymptotic suction layer exists where $St = -F$. However, it should be emphasized that even though both zero and adverse pressure gradient have the same asymptotic suction limit for a given constant F, Stanton number as a function of streamwise distance x will be quite different for the two pressure gradients.

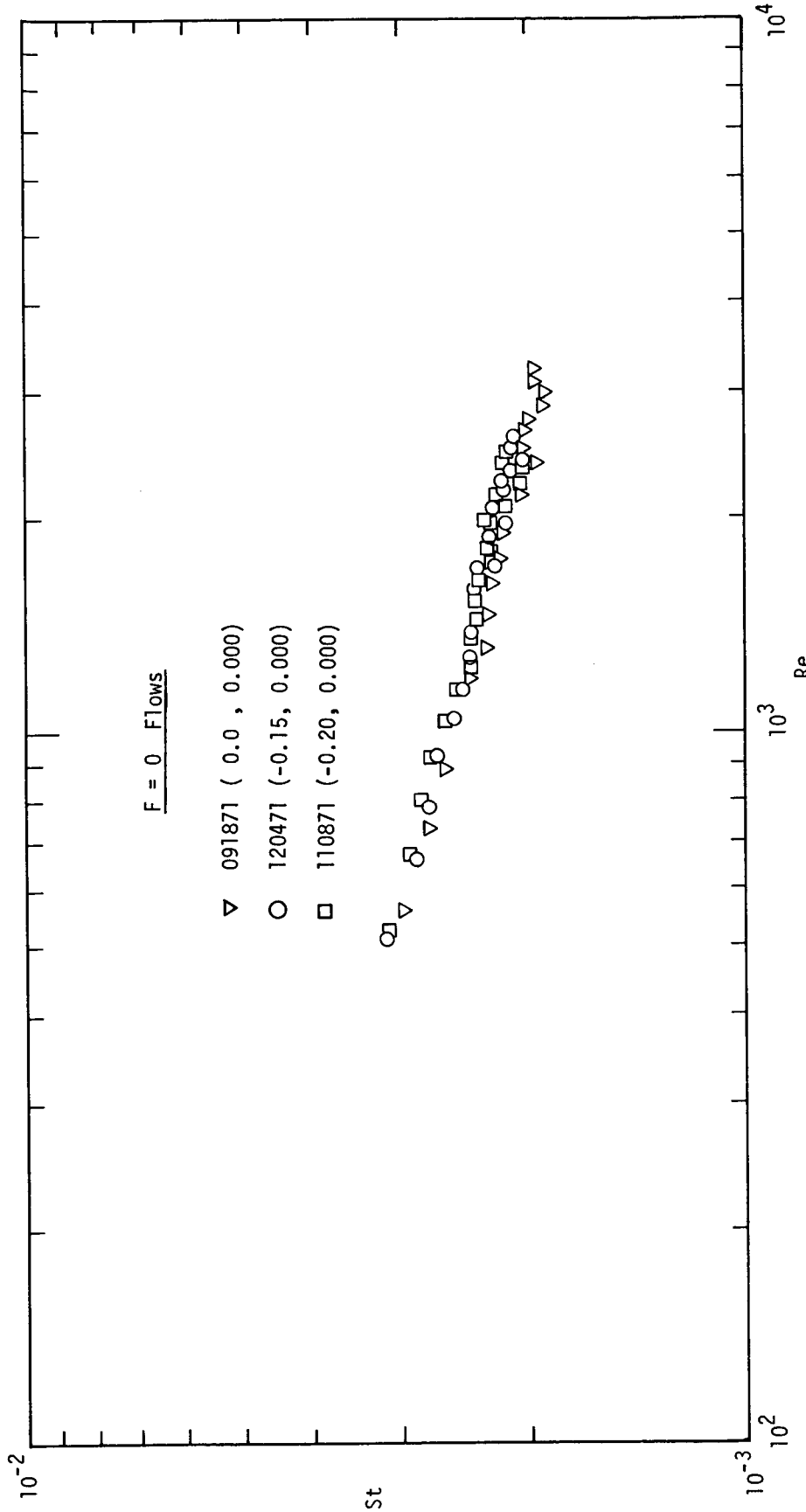


Figure 4-1 Influence of pressure gradient with zero transpiration on Stanton number

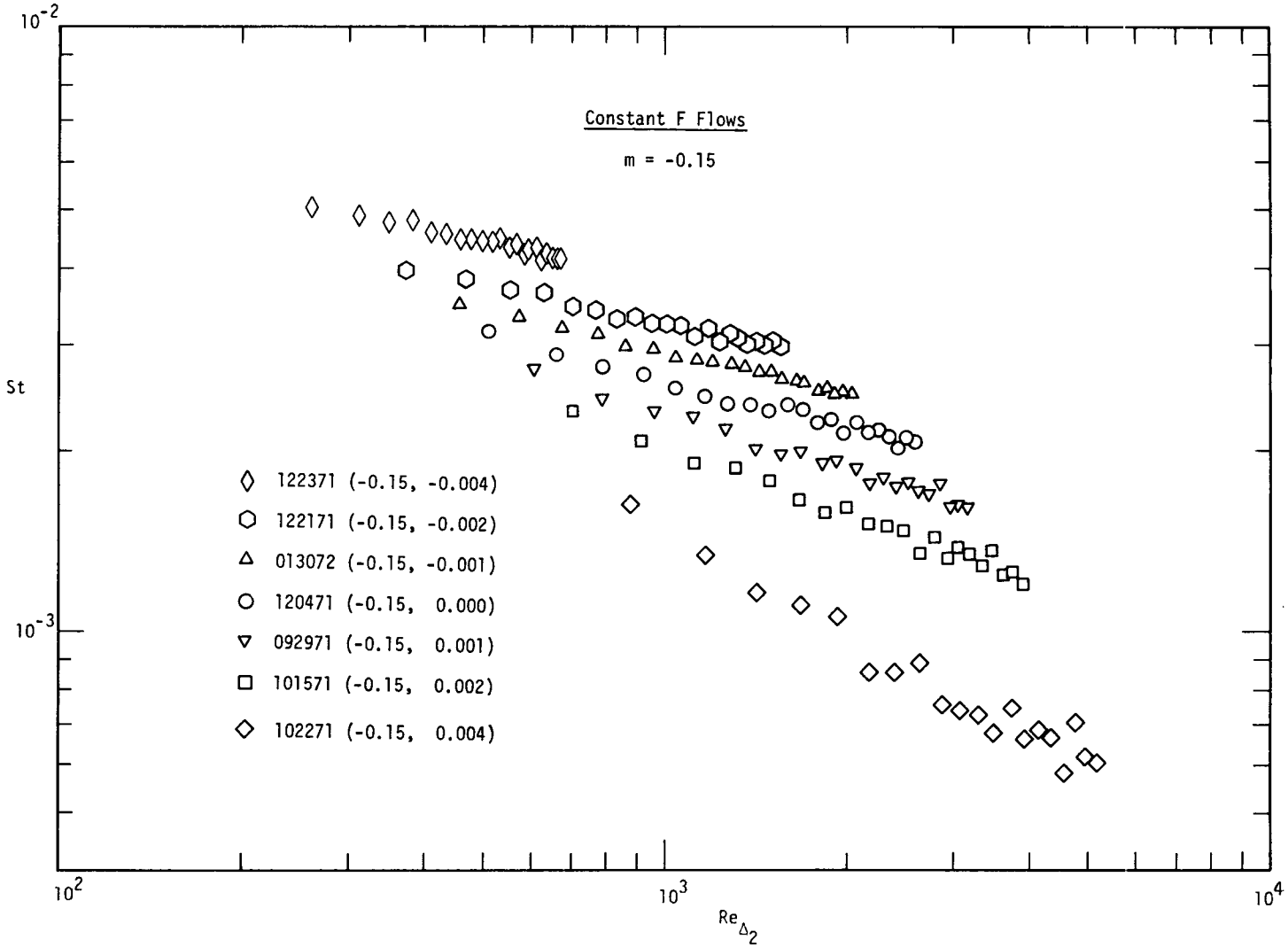


Figure 4-2 Stanton number data for m = -0.15 and constant F boundary conditions

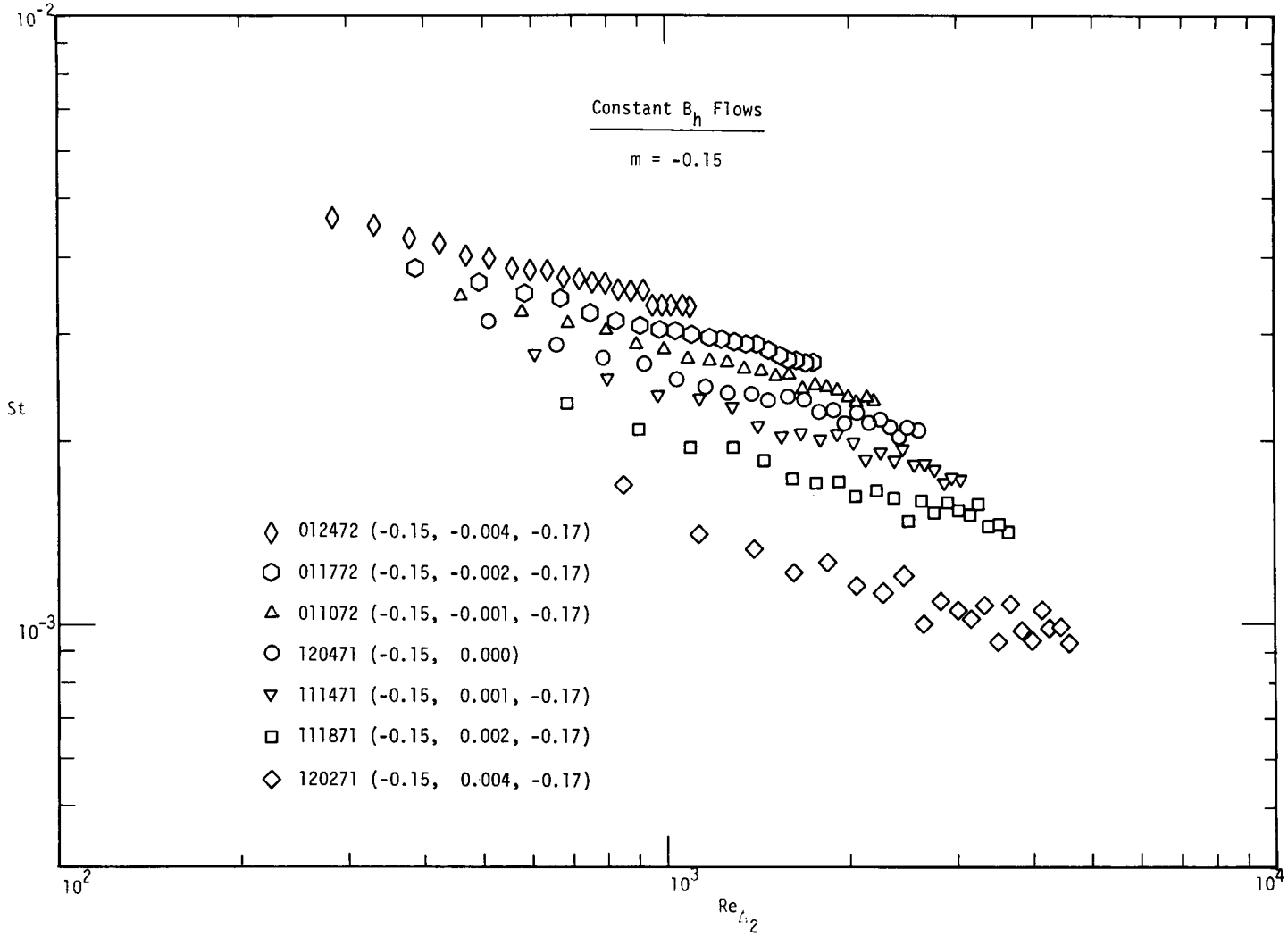


Figure 4-3 Stanton number data for m = -0.15 and constant B_h boundary conditions

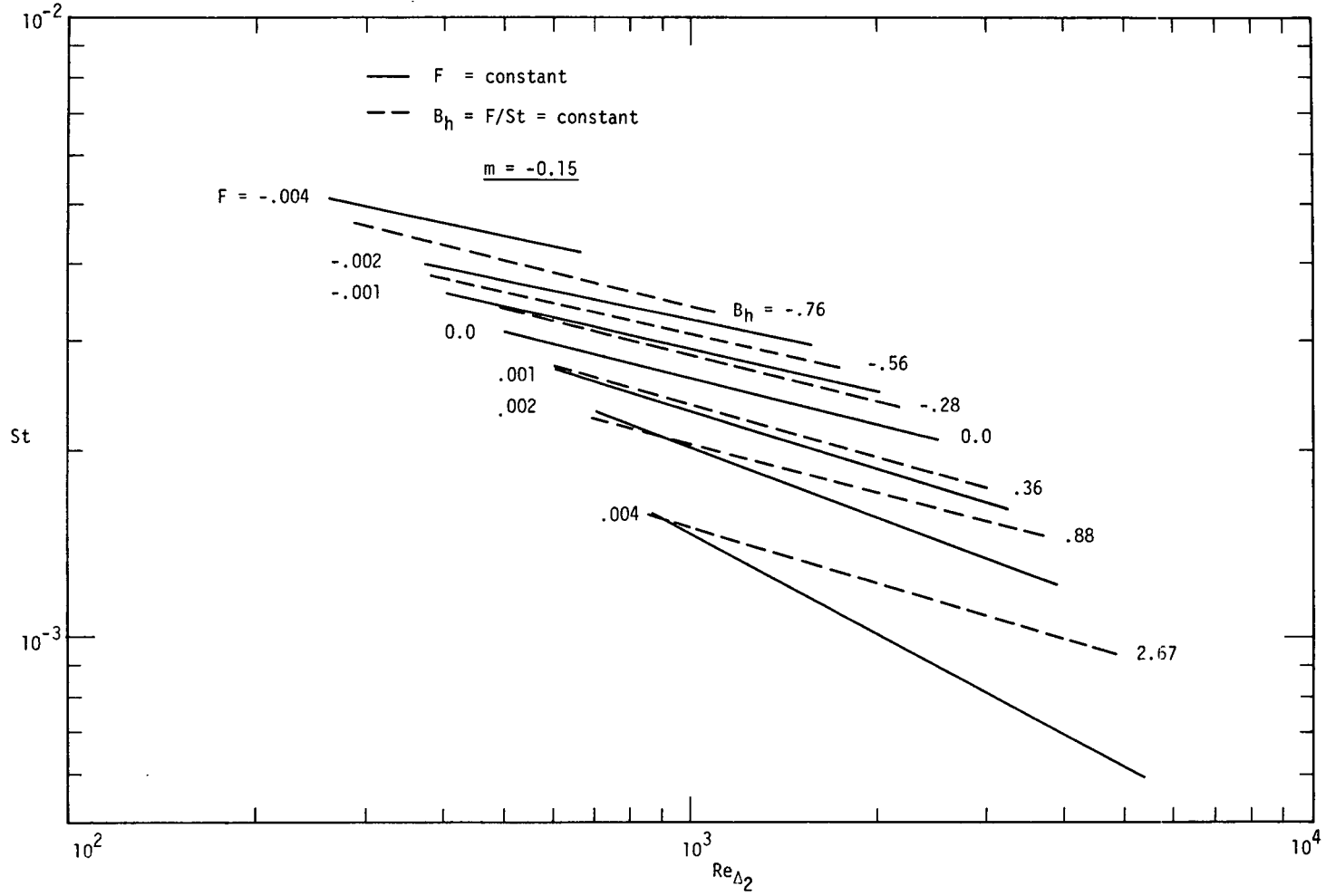


Figure 4-4 Summary of all Stanton number data for m = -0.15

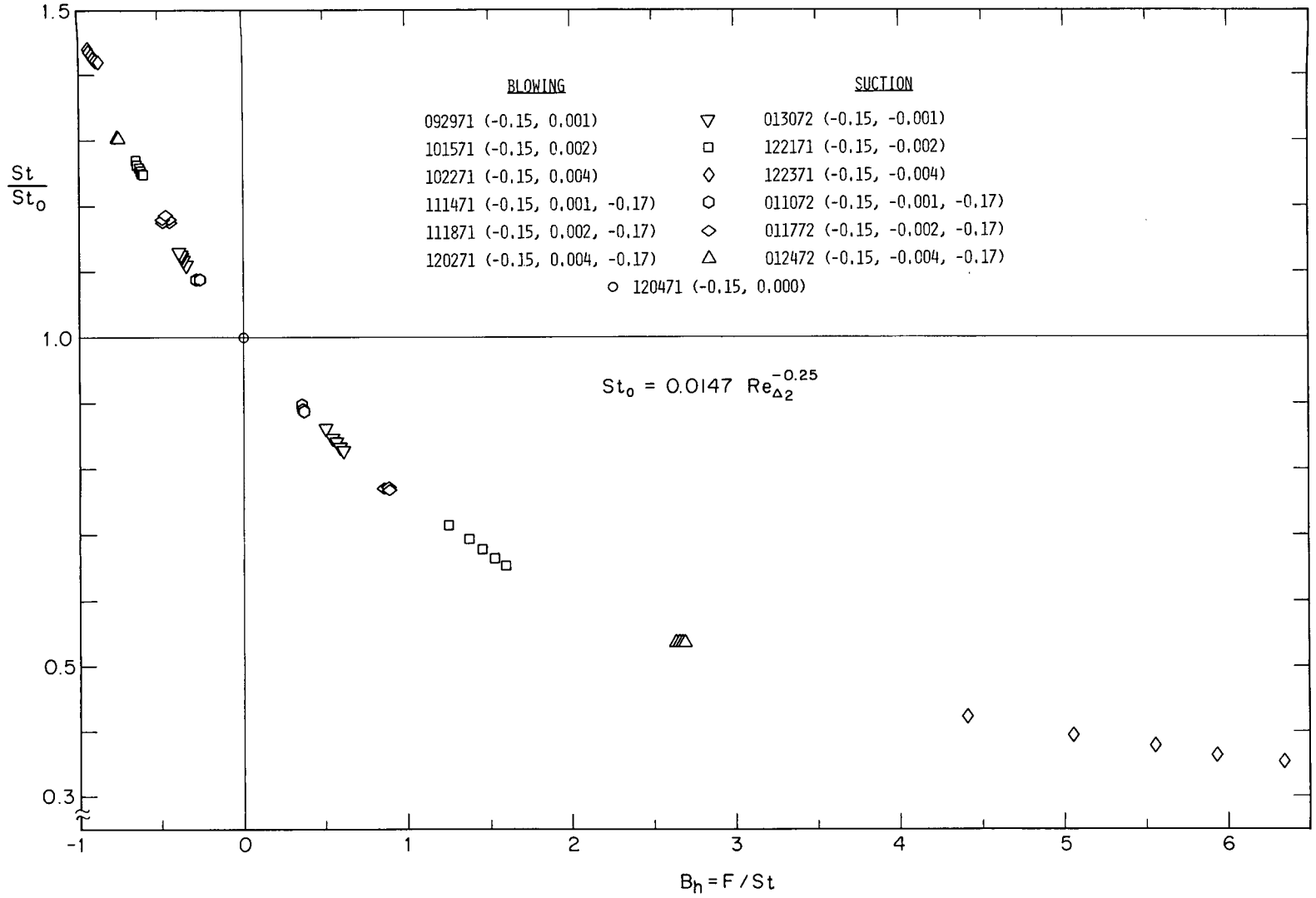


Figure 4-5 Stanton number ratio for all m = -0.15 flows

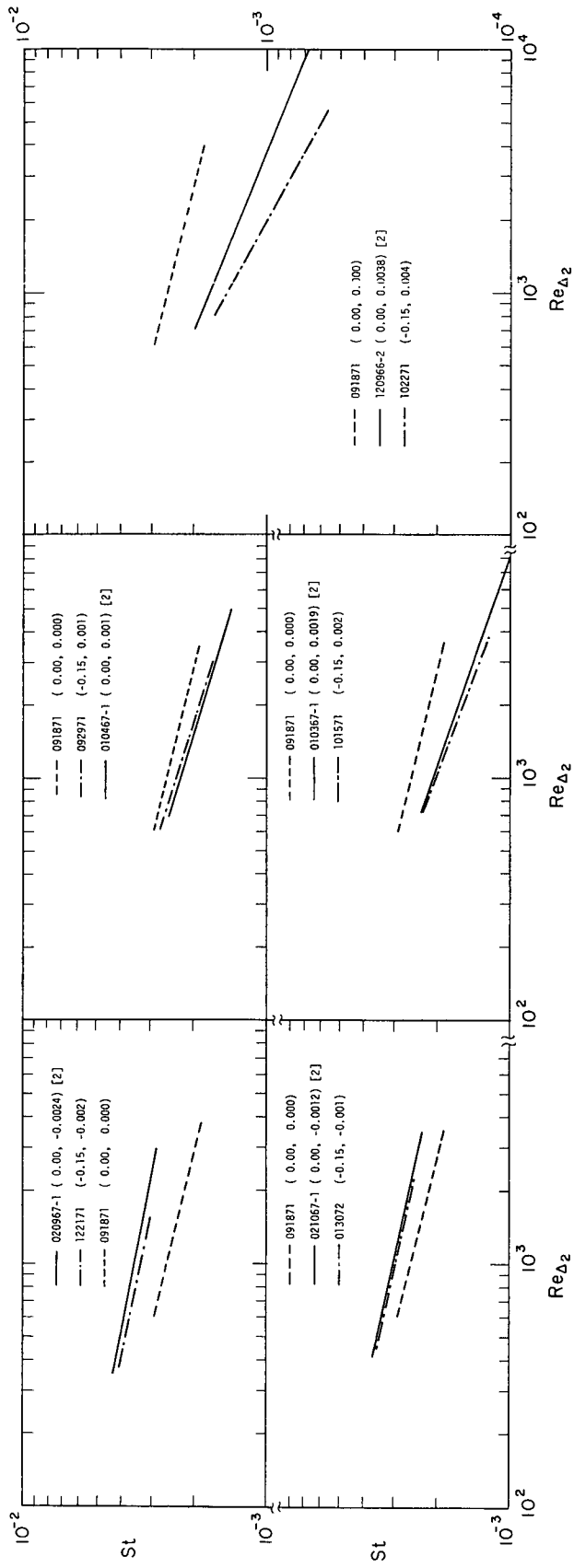


Figure 4-6 Comparison of selected adverse pressure gradient runs with zero pressure gradient data of Moffat [2]

CHAPTER 5

MEAN TEMPERATURE PROFILE DATA

For each of the 15 different runs listed in Table 2-2, mean temperature profiles were measured using the boundary layer temperature probe described in Section 3.7. A total of 132 temperature profiles are reported in this study with each profile consisting of 30-45 data points. With this large a number of temperature profiles, only those profiles that bring out a significant point will be presented. All of the temperature profiles of this study are tabulated in CHAPTER 9. The estimated uncertainty in the profile temperature was $0.2^{o}F$.

5.1 Mean Temperature Profiles in Wall Coordinates

It has been well established that a "law of the wall" exists for the velocity boundary layer for adverse pressure gradients and no transpiration. However, the same is not true of the thermal boundary layer. This fact is shown by the data in Figure 5-1. Although all of the temperature profiles in Figure 5-1 exhibit a logarithmic region, the slope of this region decreases with increasing adverse pressure gradient. This fact was also reported by Perry [12]. Due to the fact that the skin friction is markedly decreased by adverse pressure gradients while the Stanton number is essentially unaffected, it is apparent that a "temperature law of the wall" should not exist. The data in Figure 5-1 also indicates that any type of "Reynolds analogy" between skin friction and Stanton number for adverse pressure gradient flows is definitely not valid.

From the definition of T^+ and y^+, both depend on $\sqrt{C_f/2}$. It is not obvious that skin friction should appear in the temperature and distance scales, at least very near the wall. For momentum transfer, it is well accepted that u^+ is a function of y^+, for no transpiration and close to the wall. The wall variables u^+ and y^+ can be written as (for constant property flow)

$$u^+ = \frac{u}{u_\infty} \frac{1}{\sqrt{C_f/2}} \quad , \quad y^+ = \frac{y\, u_\infty}{\nu} \sqrt{C_f/2} \tag{5-1}$$

For heat transfer, $(T-T_0)/(T_\infty-T_0)$ is analogous to u/u_∞ and St is analogous to $C_f/2$. Using (5-1) as a guide and the above analogies, let us define new temperature and distance variables as

$$T^* = \overline{T} \cdot \frac{1}{\sqrt{St}} \quad , \quad y^* = \frac{y\, u_\infty}{\nu} \sqrt{St} \tag{5-2}$$

In order to account for variable density flow, we should define T^* and y^* as

$$T^* = \overline{T} \frac{1}{\sqrt{St\ \rho_\infty/\rho_0}} \tag{5-3}$$

and

$$y^* = \frac{y\, u_\infty}{\nu} \sqrt{\frac{\rho_\infty}{\rho_0} St} \tag{5-4}$$

Figure 5-2 presents T^* vs y^* for the three no transpiration runs of this study. On comparing the data in Figure 5-2 with the (T^+,y^+) data of Figure 5-1 for the same runs, it appears that (T^*,y^*) collapse the inner part $(y^* < 20)$ of the boundary layer much better than (T^+,y^+), and does a fair job at collapsing the logarithmic region.

The (T^*,y^*) variables are also suggested by the laminar sublayer equation for temperature. For low velocity, constant property flow, this sublayer equation is

$$T^+ = Pr\ y^+ \tag{5-5}$$

From definitions, (5-5) can be written as

$$\overline{T}\,\frac{\sqrt{C_f/2}}{St} = Pr\,\frac{y\,u_\infty}{\nu}\,\sqrt{C_f/2} \qquad (5\text{-}6)$$

Since $\sqrt{C_f/2}$ appears on both sides of (5-6), it can be cancelled out. Hence, (5-6) becomes

$$\overline{T}\,\frac{1}{\sqrt{St}} = Pr\,\frac{y\,u_\infty}{\nu}\,\sqrt{St} \qquad (5\text{-}7)$$

or,

$$T^* = Pr\,y^* \qquad (5\text{-}8)$$

We conclude that the form of the laminar sublayer equation is the same for both (T^+,y^+) and (T^*,y^*).

Figure 5-3 shows the influence of transpiration on the mean temperature profiles for $m = -0.15$. From this figure, it can be concluded that blowing produces a large wake while suction suppresses the wake. These same conclusions were also drawn by Whitten [3] in his constant free stream velocity study.

5.2 Mean Temperature Profiles in Outer Region Coordinates

The coordinates chosen to present the temperature profiles in the outer part of the boundary layer are $-I_d^+$ vs y/Δ_3, where I_d^+ and Δ_3 are defined by Equations (2-6a) and (2-7), respectively. Figure 5-4 presents the defect enthalpy profile for the zero pressure gradient, no transpiration run. Only the profiles at the $x = 34$, 58, and 82 inch locations are presented; profiles at other x locations are tabulated in CHAPTER 9. For $x < 34$ inches, the flow is not in equilibrium because the momentum boundary layer originates upstream of the thermal boundary layer. In this figure, $y/\Delta = 0.1$ corresponds approximately to $y/\Delta_3 = 0.03$. Hence, the outer 90% of the thermal boundary layer is similar in terms of defect coordinates; it is apparent that the inner 10% of the thermal boundary layer is not similar in defect coordinates.

Figures 5-5 thru 5-8 show defect enthalpy profiles for other selected runs. Again, the outer 90% of the thermal boundary layer is similar in defect coordinates. However, the defect profile shape changes considerably from one run to the next.

5.3 Enthalpy Defect Profile Shape Factors

In Section 2.2, a defect enthalpy profile shape factor G_h was introduced and is formally defined by Equation (2-10). This shape factor G_h is directly analogous to the defect velocity shape factor introduced by Clauser [14]. Figure 5-9 shows the influence of pressure gradient with no transpiration on G_h. All three of the runs shown in Figure 5-9 approach a constant value of G_h for large values of x, and hence are equilibrium thermal layers. The primary reason that G_h varies for small values of x is that the momentum boundary layer originates upstream of the thermal boundary layer. The equilibrium flat plate value of G_h is approximately 5.75. The effect of increasing adverse pressure gradient is to decrease G_h. Andersen [9] reports the opposite effect of adverse pressure gradient on the defect velocity shape factor G_f.

Figure 5-10 shows the influence of transpiration on G_h for all of the $m = -0.15$ flows. Blowing increases G_h while suction decreases G_h. All of the constant B_h flows approach a constant value of G_h for large values of x. All of the constant F flows approach a constant value of G_h with the exception of the most extreme blowing run ($F = 0.004$). This indicates that if the transpiration rate $\dot{m}''$ changes sufficiently slowly with x, then the outer part of the thermal boundary layer is able to respond sufficiently fast to maintain an equilibrium state.

5.4 Reynolds Number Ratio

As was pointed out earlier, the momentum boundary layer originates upstream of the thermal boundary layer. The effect of this different virtual origin is that the defect enthalpy shape factor G_h is different from what it would have been if the origin of both boundary layers had

been coincident. Another effect is that the enthalpy thickness Reynolds number is smaller than it would have been if the two origins were coincident. This latter effect is shown in Figure 5-11, where the enthalpy thickness Reynolds number has been normalized by the momentum thickness Reynolds number. This starting length effect is the most pronounced for the zero pressure gradient run because the asymptotic value of Re_{Δ_2}/Re_θ is the largest of all the flows reported in this study. Using the zero pressure gradient case for a standard of comparison, one concludes that increasing adverse pressure gradient causes a decrease in the asymptotic Reynolds number ratio. This is due to the fact that increasing adverse pressure gradient causes a decrease in Re_{Δ_2} but an increase in Re_θ, for a given value of x. Figures 5-12 and 5-13 show the same data for the constant B_h and constant F flows respectively. Blowing decreases this Reynolds number ratio while suction increases it.

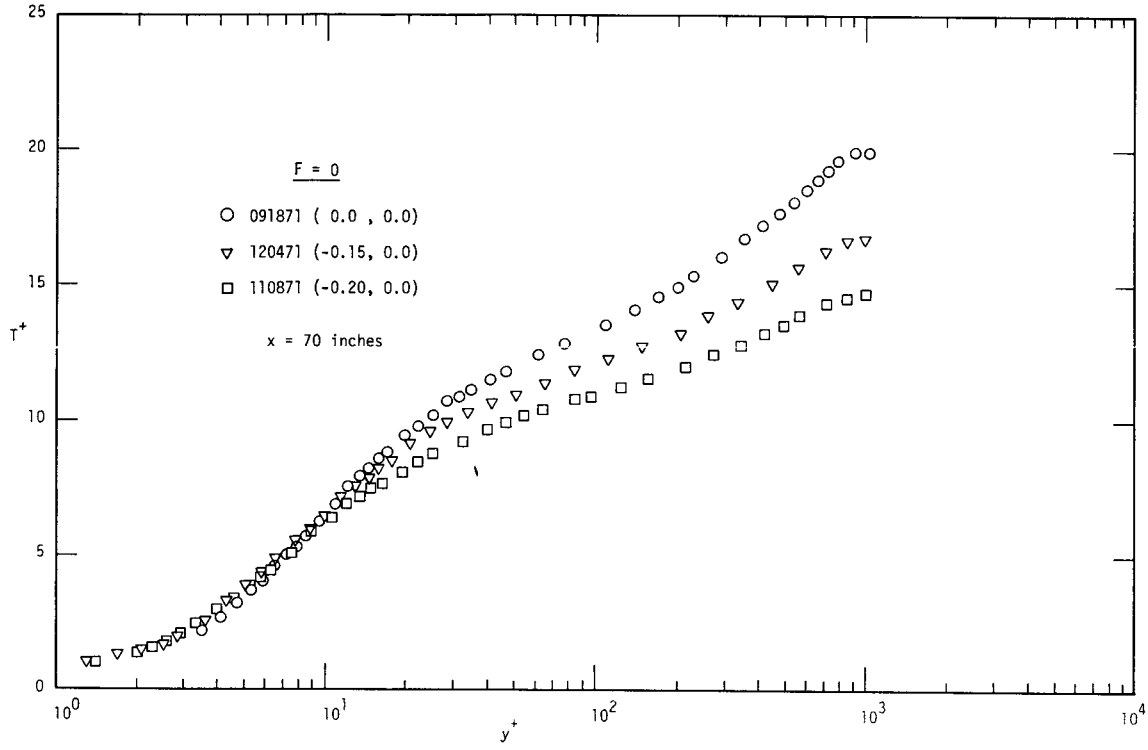


Figure 5-1 Influence of pressure gradient on non-dimensional temperature profiles, wall coordinates

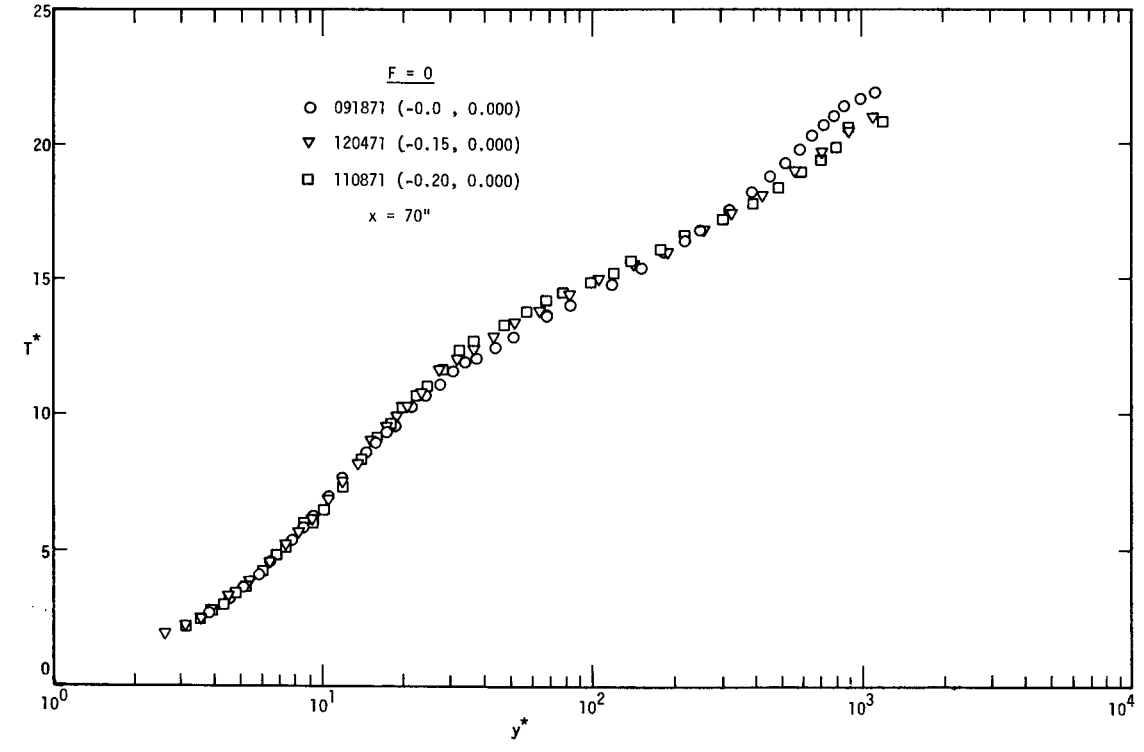


Figure 5-2 Influence of pressure gradient on non-dimensional temperature profiles, wall coordinates

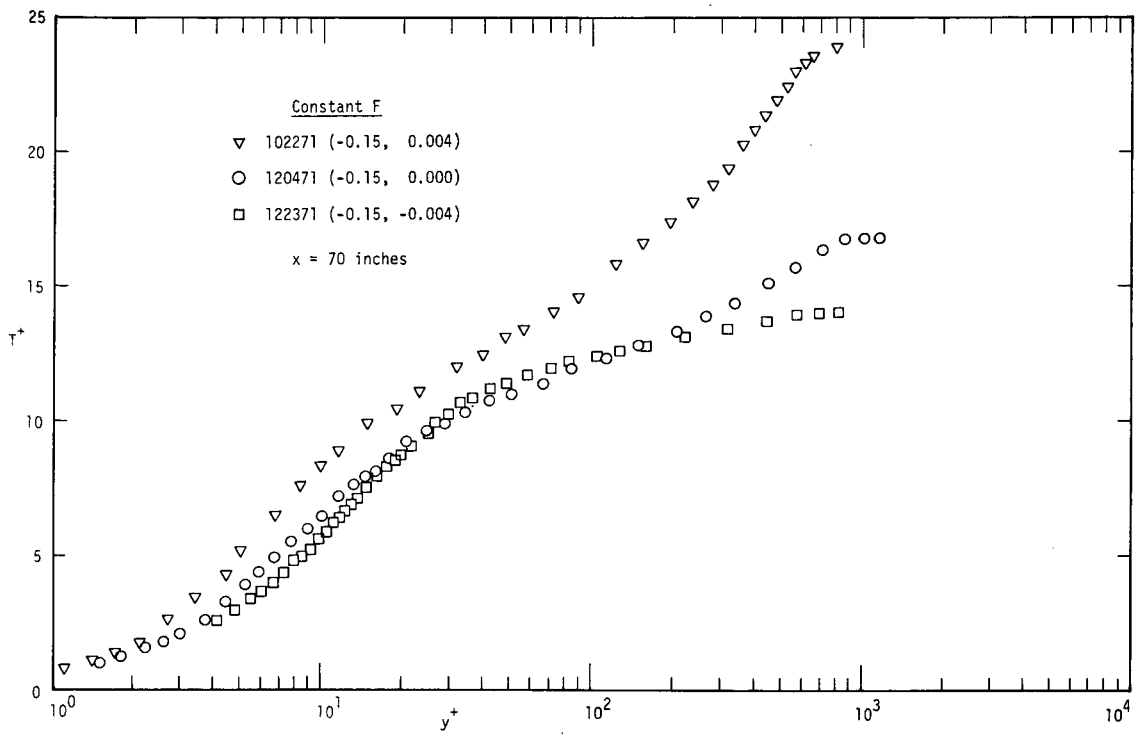


Figure 5-3 Influence of transpiration on non-dimensional temperature profiles, wall coordinates

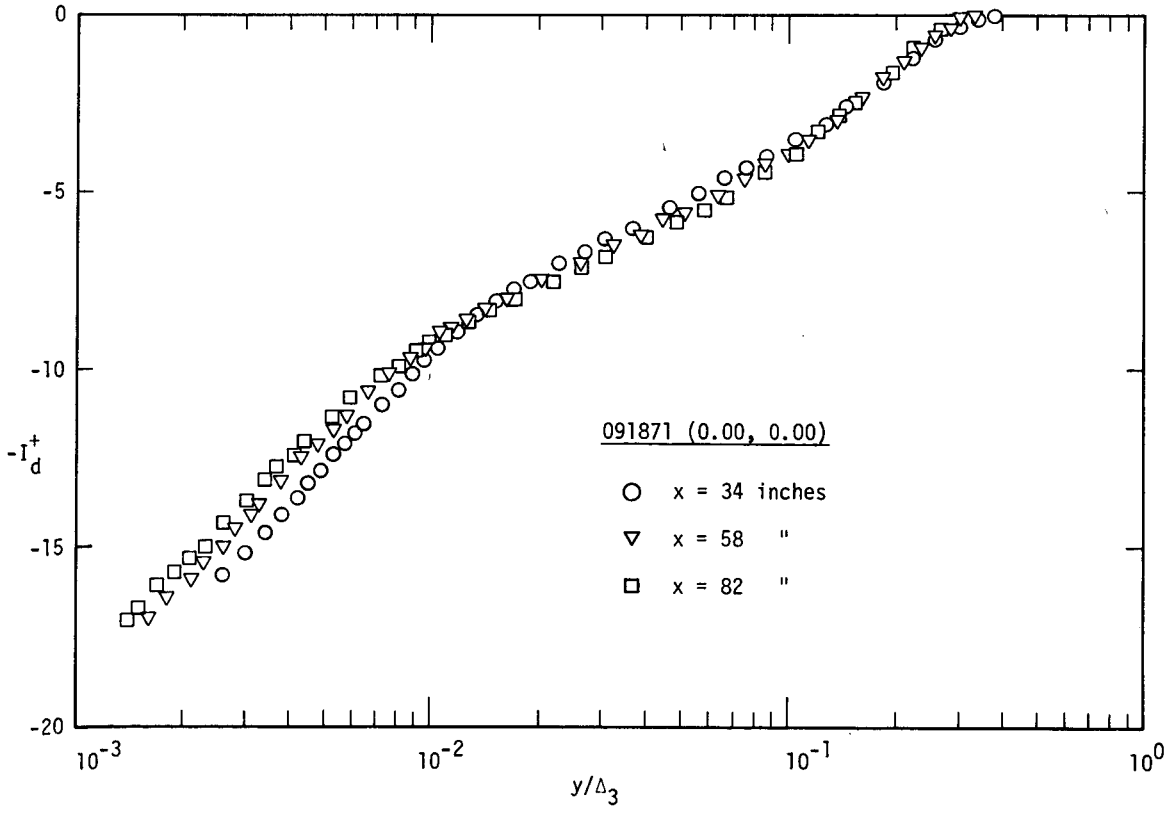


Figure 5-4 Defect enthalpy profiles, run 091871

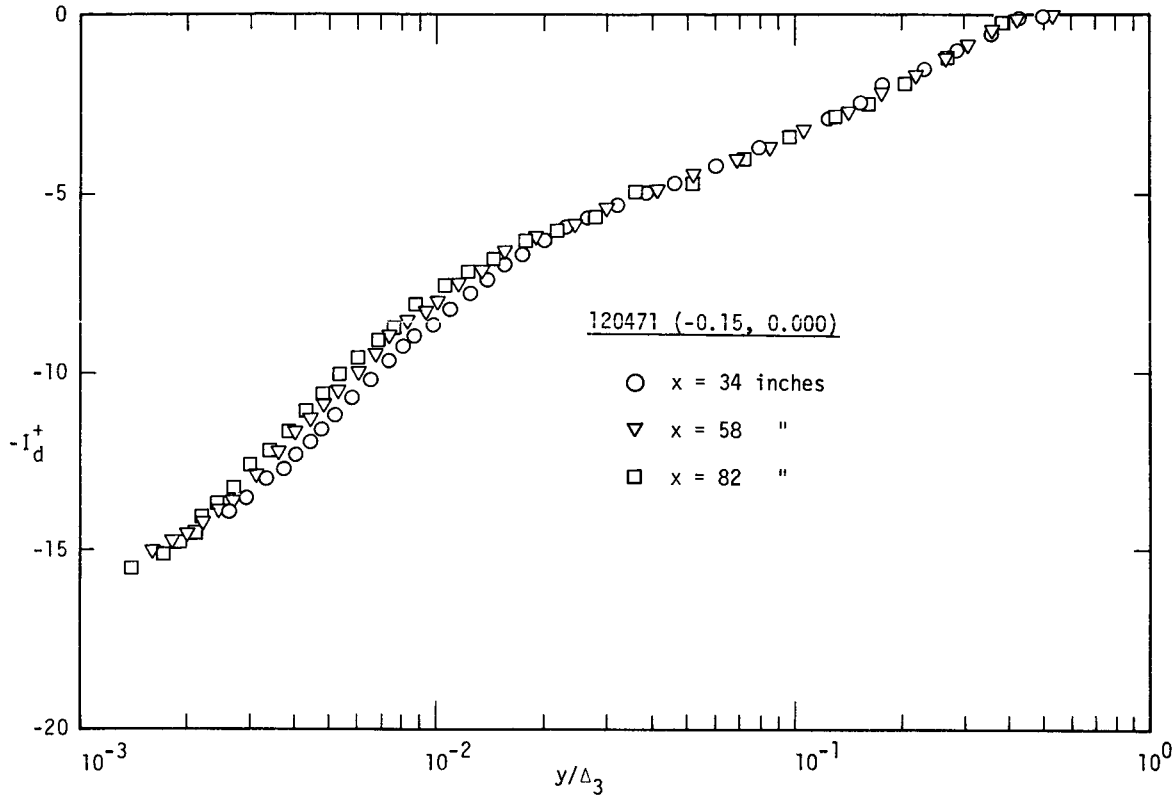


Figure 5-5 Defect enthalpy profiles, run 120471

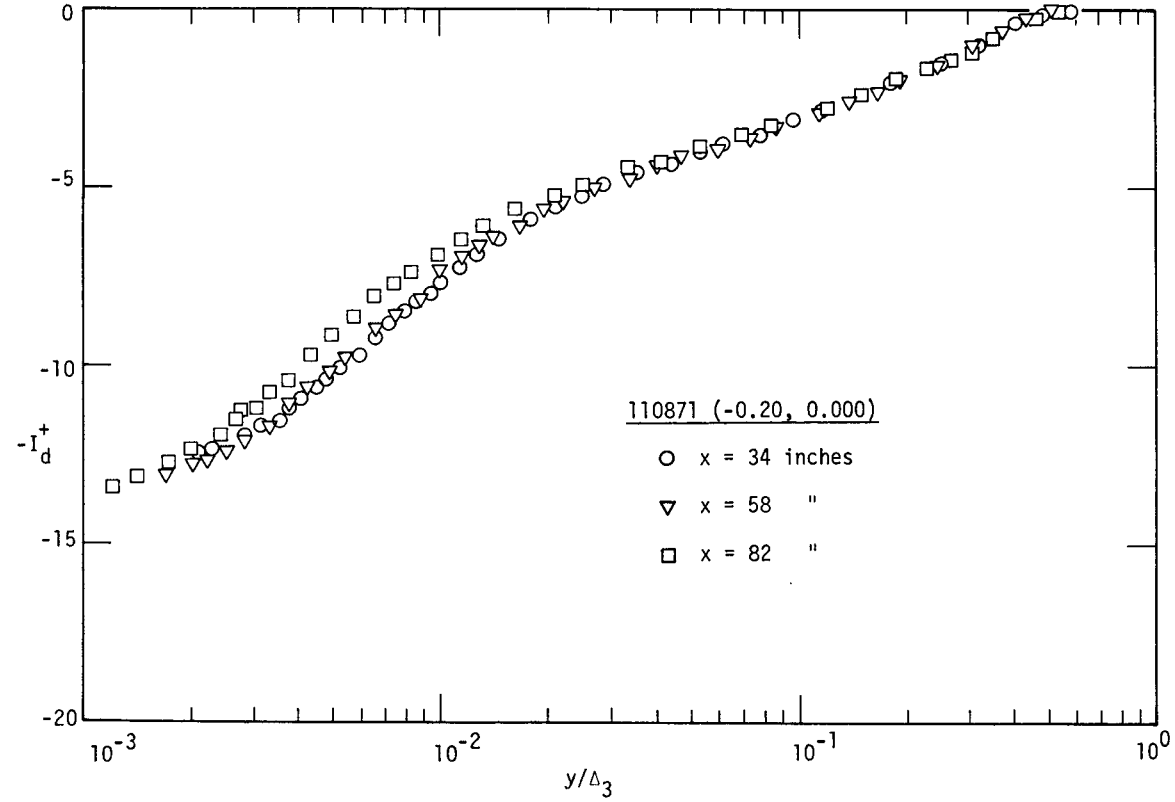


Figure 5-6 Defect enthalpy profiles, run 110871

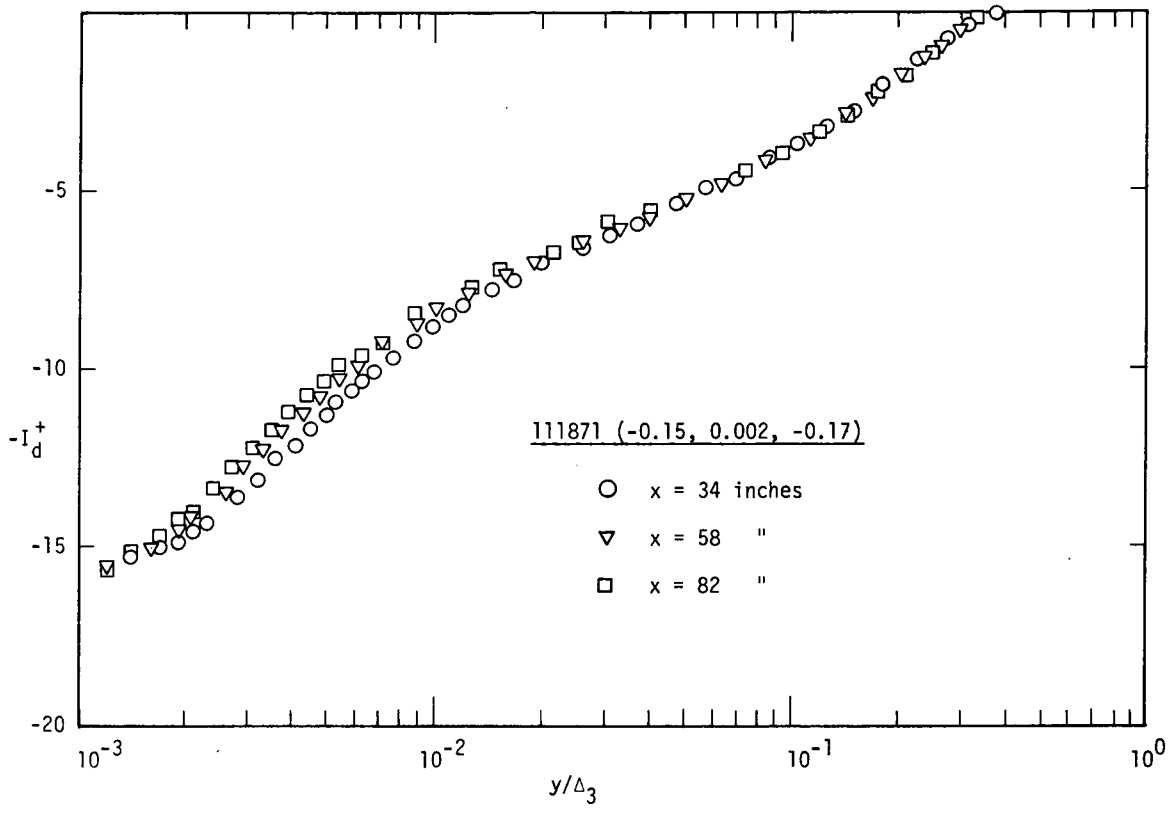


Figure 5-7 Defect enthalpy profiles, run 111871

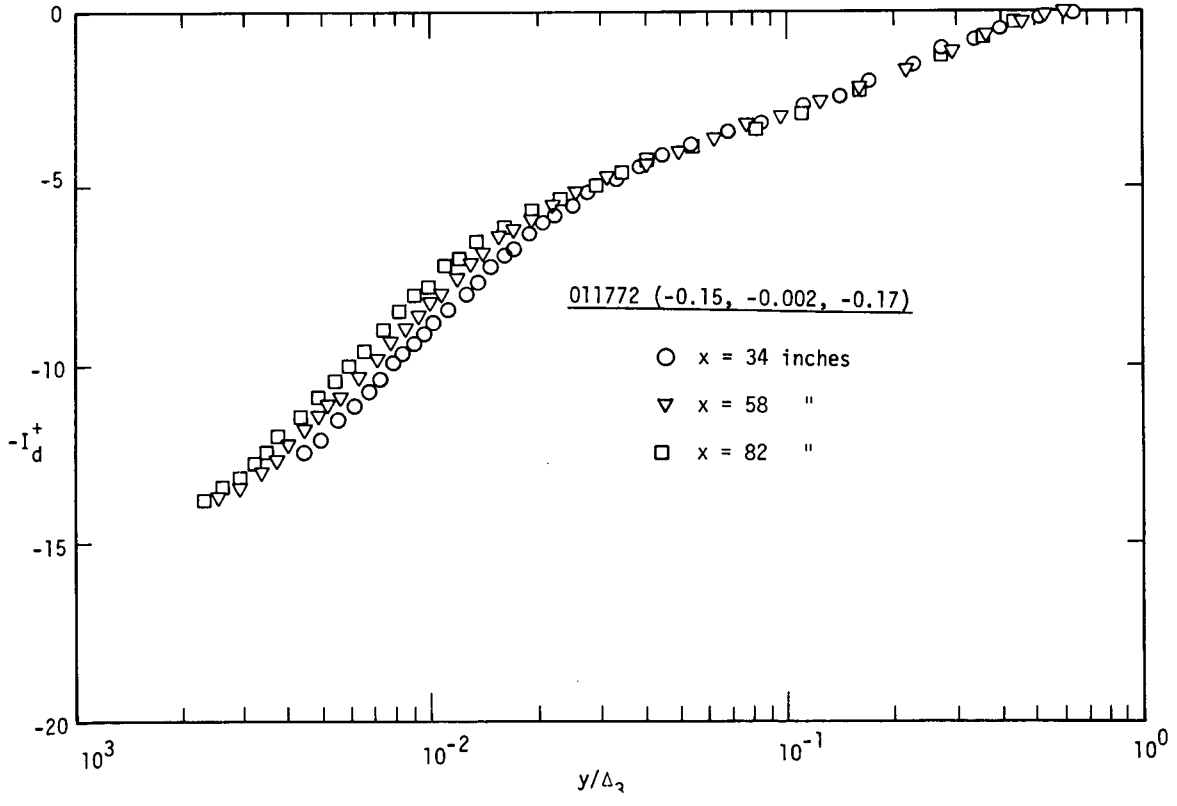


Figure 5-8 Defect enthalpy profiles, run 011772

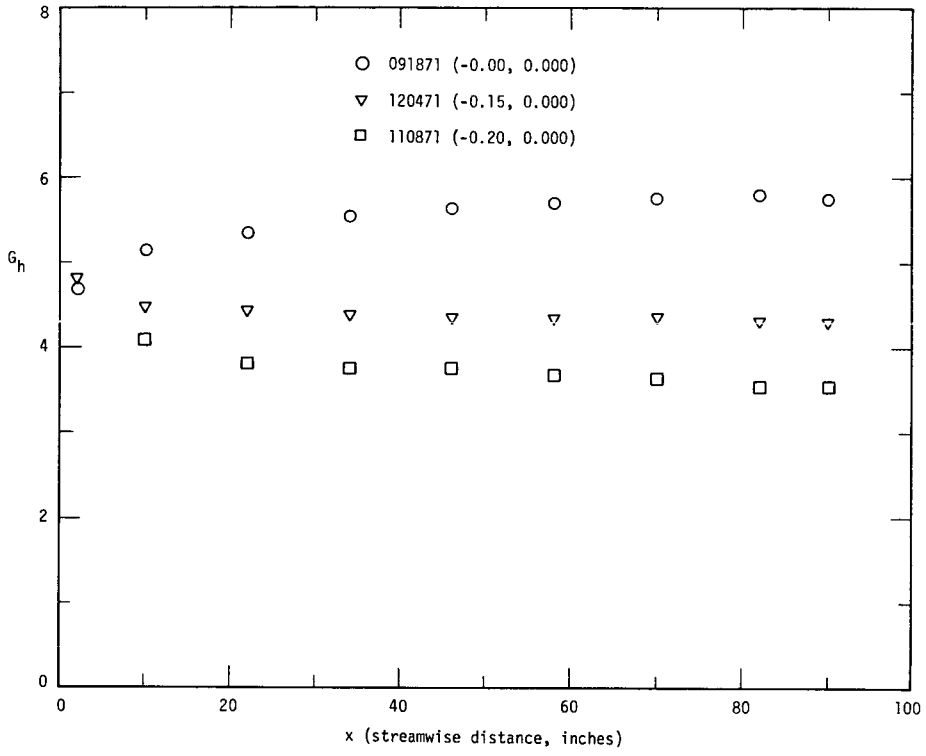


Figure 5-9 Influence of pressure gradient on defect enthalpy shape factor

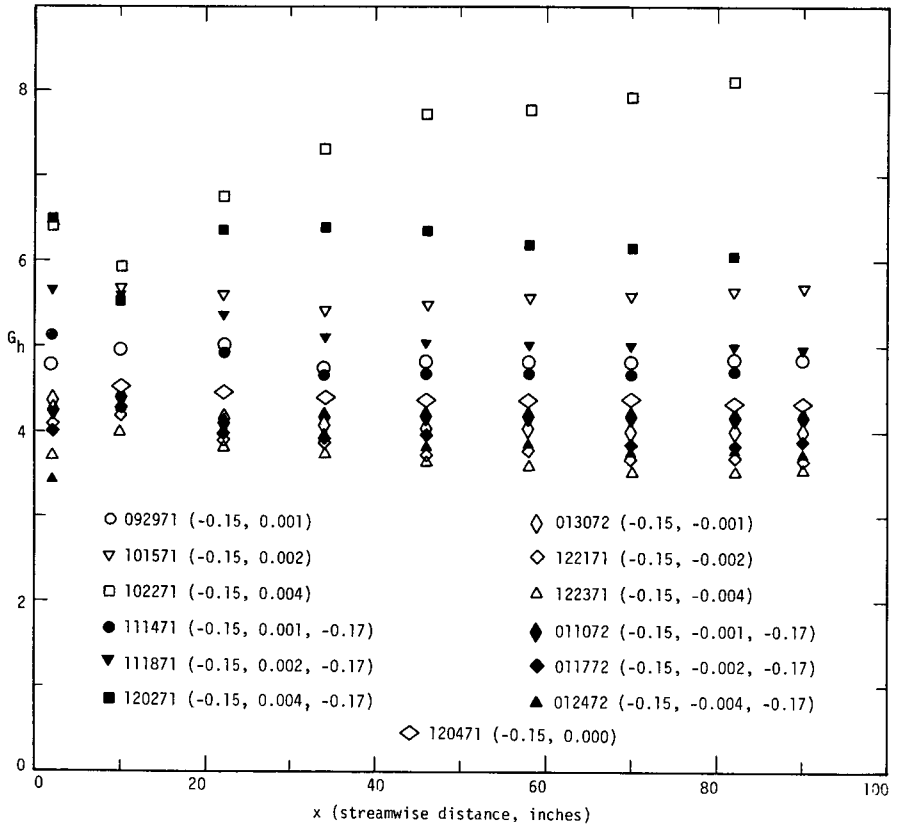


Figure 5-10 Influence of transpiration on defect enthalpy shape factor

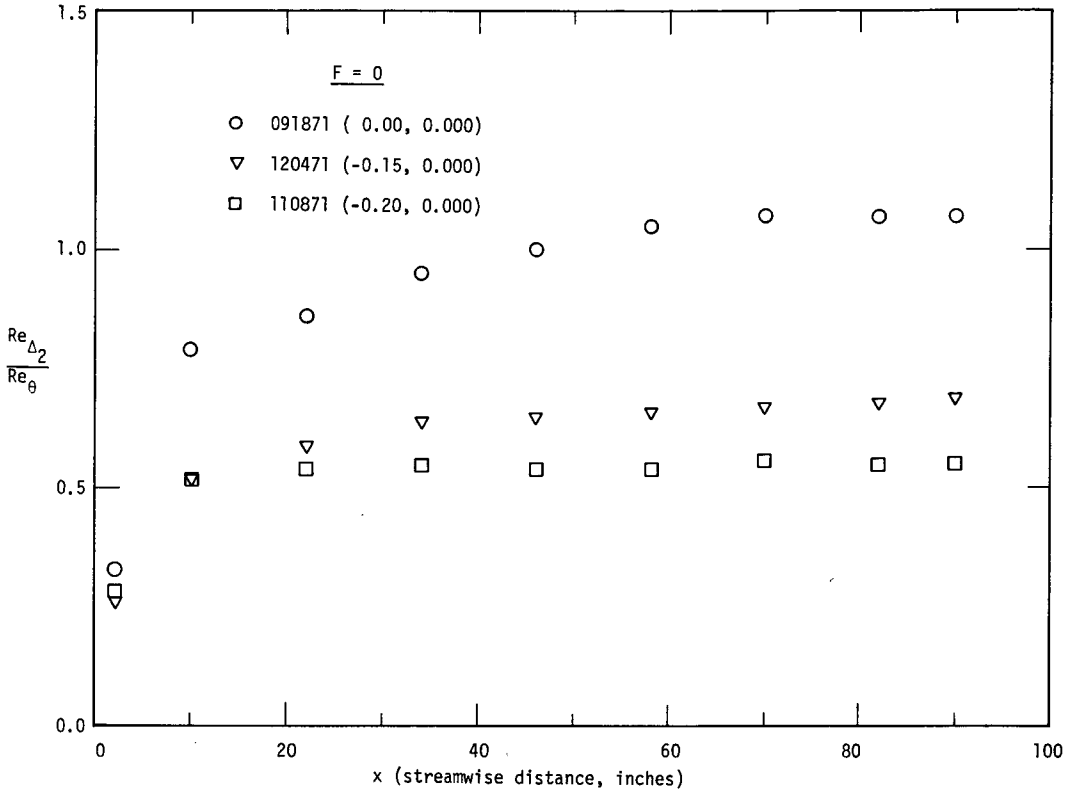


Figure 5-11 Influence of pressure gradient on Reynolds number ratio, F = 0

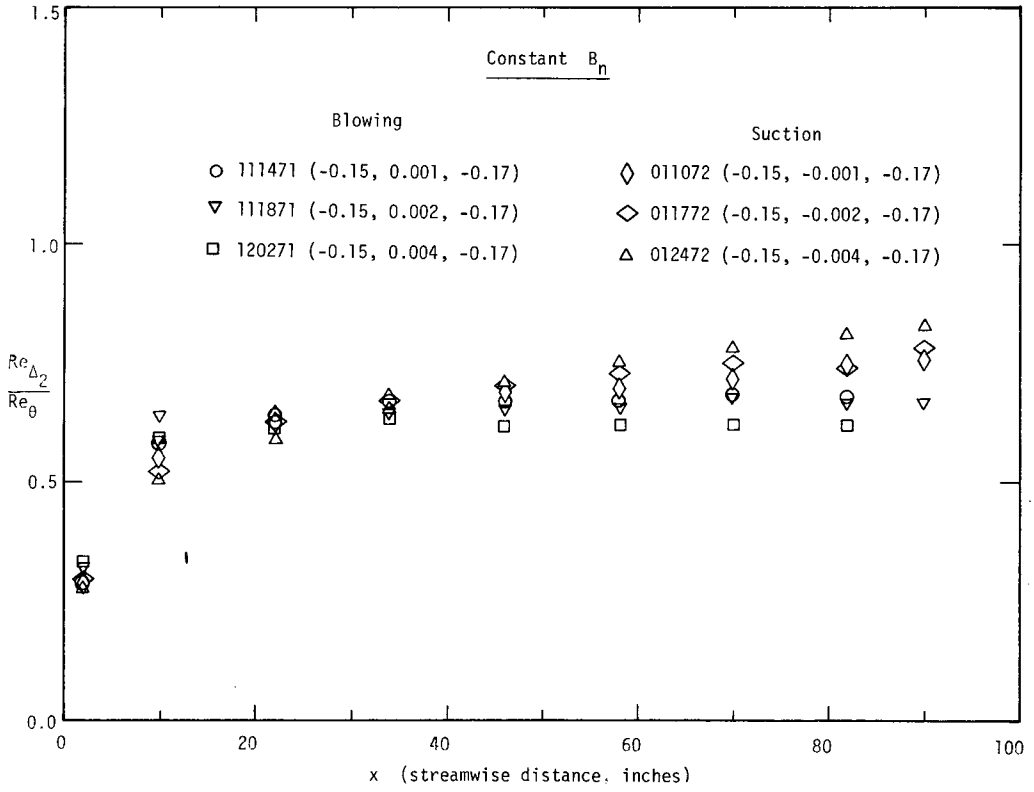


Figure 5-12 Influence of transpiration on Reynolds number ratio, B_h = constant

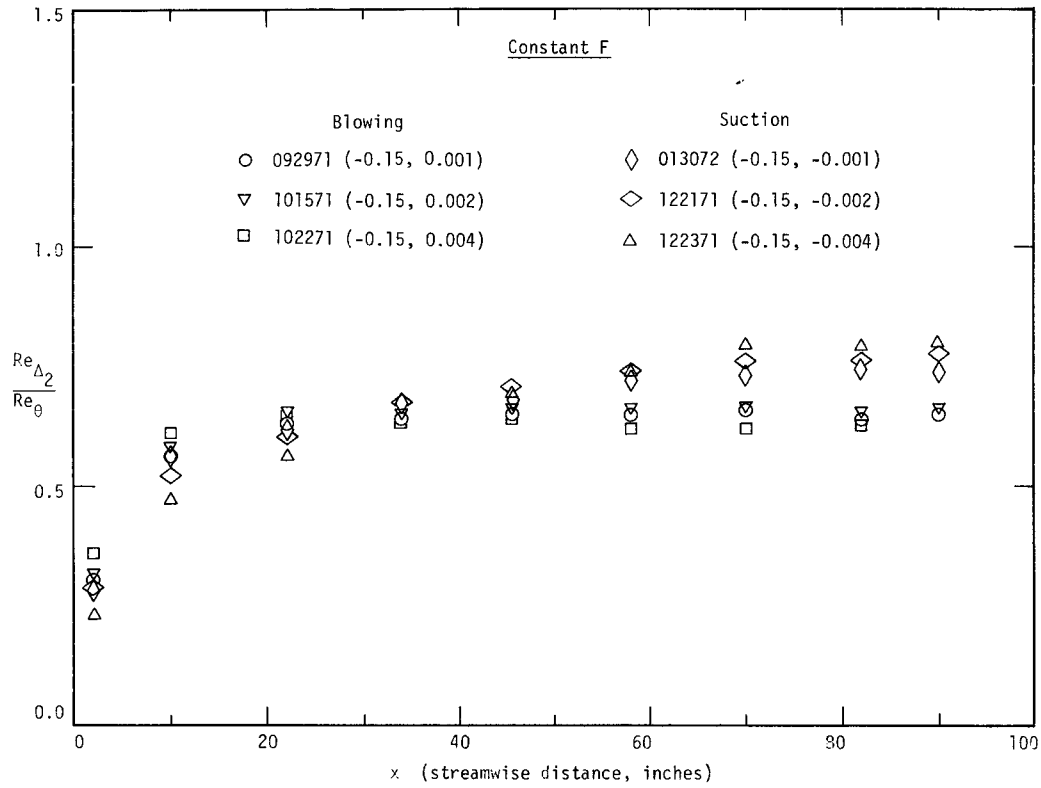


Figure 5-13 Influence of transpiration on Reynolds number ratio, F = constant

CHAPTER 6

HEAT FLUX AND TURBULENT PRANDTL NUMBER PROFILES

In recent years considerable heat transfer research has been directed toward experimentally obtaining the turbulent Prandtl number variation in a boundary layer. This is an extremely difficult problem since one must know not only the mean temperature and velocity profiles but also the heat flux and shear stress profiles. This chapter will outline the previous experimental turbulent Prandtl number studies, the method used to compute the heat flux profiles from mean temperature and velocity profiles will be outlined, and the computed turbulent Prandtl number results will be presented.

6.1 Previous Experimental Turbulent Prandtl Number Studies

Most previous experimental studies of the turbulent Prandtl number were concerned with fully developed pipe and channel flow. One reason for this is that the heat flux and shear stress profiles are known from theoretical considerations for those flow conditions. Blom [31] reviewed the status of experimental turbulent Prandtl number studies up through 1968 and, of the numerous references presented, only the data of Johnson [32] was concerned with the external turbulent boundary layer. Both Blom [31] and Johnson [32] experimentally studied the constant free stream velocity turbulent boundary layer, and measured $\overline{T'v'}$ downstream of an unheated starting length by means of a hot wire. The data of Johnson [32] exhibited considerable scatter with no definite trend. The data of Blom [31] indicated that Pr_t increased with y^+ close to the wall, reached a maximum of 0.8 - 1.2 in the range $y^+ = 50 - 80$, and then decreased with increasing y^+. This maximum was not indicated by the data of Simpson [26] who studied the transpired turbulent boundary layer with constant free stream velocity. Simpson [26] concluded that for air, Pr_t was greater than unity close to the wall, and decreased to approximately 0.5 at the free stream. Kearney [7] presented turbulent Prandtl numbers for the accelerating transpired turbulent boundary layer, and found that acceleration increases Pr_t in the log-region. While

his data exhibited more scatter than the data of Simpson [26], both data sets had the same general trend: Pr_t greater than unity near the wall, and decreasing with increasing y^+. A more recent study by Meier [30] for supersonic flow of air over a flat plate and for a supersonic nozzle is consistent with the trend of Simpson's [26] data. At this point in time, the bulk of the experimental data indicates that for the equilibrium external turbulent boundary layer in air, the turbulent Prandtl number is greater than unity close to the wall and decreases with increasing y. The data of this study will be additional evidence to support this belief.

6.2 Computation of Heat Flux Profiles

The two-dimensional continuity and energy equations of the boundary layer can be written as

$$\frac{\partial}{\partial x}(\rho u) + \frac{\partial}{\partial y}(\rho v) = 0 \tag{6-1}$$

$$\frac{\partial}{\partial x}(\rho u I) + \frac{\partial}{\partial y}(\rho v I) = -\frac{\partial \dot{q}''}{\partial y} + \frac{\partial}{\partial y}(\tau u) \tag{6-2}$$

Integrating (6-1) and (6-2) from the wall to any arbitrary y-location in the boundary layer, one obtains

$$Q^+ = 1 + \frac{\tau u}{\dot{q}''_o} + \frac{F}{St}\left(1 - \frac{I}{I_o}\right) + \frac{I}{\dot{q}''_o}\int_o^y \frac{\partial}{\partial x}(\rho u)dy - \frac{1}{\dot{q}''_o}\int_o^y \frac{\partial}{\partial x}(\rho u I)dy \tag{6-3}$$

If we let $y \to \infty$, then we obtain the energy integral equation (3-10) with $3\text{-}D = 0$. The first three terms of (6-3) represent the Couette-flow approximation to the local heat flux. The term $\tau u/\dot{q}''_o$ represents the ratio of the local viscous dissipation to the wall heat flux and is quite small for the low velocities of this study. However, this term was retained in all of the computations of this study.

The two integral terms in (6-3) are not important very near the wall, but they become dominant in the outer region of the boundary layer. In fact, Q^+ goes to zero at the outer edge of the boundary layer and the Couette-flow terms should balance these two integral terms. In practice, the Q^+ computed from (6-3) will not be identically zero at the free stream due to three dimensionality of the flow and the inability to evaluate the two integral terms very precisely. Since the streamwise derivative terms will be difficult to evaluate precisely, let us attempt to write the equations in a form where their significance becomes smaller. For example, derivatives of terms like $\partial(\rho u/\rho_\infty u_\infty)/\partial x$ and $\partial(\rho uI/\rho_\infty u_\infty I_o)/\partial x$ should be small in the outer part of the boundary layer because of approximate similarity. With the above ideas in mind, the two integral terms in (6-3) can be written as

$$\int_0^y \frac{\partial}{\partial x}(\rho u)dy = \frac{d}{dx}(\rho_\infty u_\infty) \int_0^y \frac{\rho u}{\rho_\infty u_\infty} dy + \rho_\infty u_\infty \int_0^y \frac{\partial}{\partial x}\left(\frac{\rho u}{\rho_\infty u_\infty}\right) dy \qquad (6\text{-}4)$$

and

$$\int_0^y \frac{\partial}{\partial x}(\rho uI)dy = \frac{d}{dx}(\rho_\infty u_\infty I_o) \int_0^y \frac{\rho uI}{\rho_\infty u_\infty I_o} dy + \rho_\infty u_\infty I_o \int_0^y \frac{\partial}{\partial x}\left(\frac{\rho uI}{\rho_\infty u_\infty I_o}\right)dy \qquad (6\text{-}5)$$

Note that the x-derivatives must be evaluated at a constant y. They can be converted to derivatives at constant $\eta = y/\Delta$ by the chain rule

$$\left.\frac{\partial}{\partial x}\right)_y = \left.\frac{\partial}{\partial x}\right)_\eta - \frac{\eta}{\Delta}\frac{d\Delta}{dx}\left.\frac{\partial}{\partial \eta}\right)_x \qquad (6\text{-}6)$$

Applying (6-4) - (6-6) to (6-3), one obtains

$$Q^+ = Q_c^+ + Q_1^+ + Q_2^+ \tag{6-7}$$

where

$$Q_c^+ = 1 + \frac{\tau u}{\dot{q}''} + \frac{F}{St}\left(1 - \frac{I}{I_o}\right) \tag{6-8a}$$

$$Q_1 \frac{St}{\Delta}\frac{I_o}{I} = \frac{d}{dx}[\ell n(\rho_\infty u_\infty \Delta)] \int_0^\eta \frac{\rho u}{\rho_\infty u_\infty} d\eta + \int_0^\eta \frac{\partial}{\partial x}\left(\frac{\rho u}{\rho_\infty u_\infty}\right) d\eta \tag{6-8b}$$

$$-Q_2 \frac{St}{\Delta} = \frac{d}{dx}[\ell n(\rho_\infty u_\infty \Delta)] \int_0^\eta \frac{\rho u I}{\rho_\infty u_\infty I_o} d\eta + \int_0^\eta \frac{\partial}{\partial x}\left(\frac{\rho u I}{\rho_\infty u_\infty I_o}\right) d\eta \tag{6-8c}$$

Note that the streamwise derivatives in (6-8) are now evaluated at <u>constant η</u> . These derivatives were evaluated by the three-point centered derivative formula

$$\left.\frac{\partial f}{\partial x}\right)_n = \frac{f_{n+1} - (1 - R^2)f_n - R^2 f_{n-1}}{x_{n+1} - x_n + R^2(x_n - x_{n-1})}, \quad R = \frac{x_{n+1} - x_n}{x_{n-1} - x_n} \tag{6-9}$$

The derivatives of $\rho_\infty u_\infty \Delta$ were evaluated by first determining a least squares curve fit of the form

$$\rho_\infty u_\infty \Delta = a(x-b)^c \tag{6-10}$$

and evaluating the derivative analytically.

When the temperature and velocity profiles were measured, it was impossible to ensure that the profile points for adjacent profiles were at the same values of η . Consequently, it was necessary to interpolate

in the upstream and downstream temperature and velocity profiles when evaluating the streamwise derivatives.

Computational experiments showed that $Q^+(\infty)$ evaluated from (6-8) was consistently closer to zero than that obtained from (6-3). However, the results from (6-8) were not identically zero. It was assumed that this discrepancy was solely due to the inability to evaluate the two integral terms accurately. In order to force the computed Q^+ profiles to satisfy the free stream boundary condition, a factor D was introduced, defined by

$$Q^+ = Q_c^+ + D(Q_1^+ + Q_2^+) \tag{6-11}$$

Evaluating (6-11) at the free stream, we obtain

$$D = - \frac{Q_c^+(\infty)}{Q_1^+(\infty) + Q_2^+(\infty)} \tag{6-12}$$

In the inner part of the boundary layer, both Q_1^+ and Q_2^+ are very small. Consequently, the D factor affects the Q^+ profiles only in the outer region. In general, it was found that $|D| < 0.1$ with many of the profiles having $|D| < 0.05$.

Figure (6-1) shows the influence of pressure gradient with no transpiration on the computed heat flux profiles. In the inner part of the boundary layer, the local value of Q^+ is essentially <u>independent</u> of pressure gradient. In contrast, the corresponding shear stress profiles* for the same three runs are shown in Figure (6-2). The shear stress profiles are strongly dependent on the pressure gradient. One would expect the above behavior, at least in the inner region, as a result of inspecting the Couette-flow expressions for Q^+ and τ^+ .

Figure (6-3) shows the influence of blowing and suction on the heat flux profiles. For blowing, the maximum heat flux occurs well away from

*The shear stress profiles were interpolated from the parallel study of Andersen [9].

the wall whereas the maximum heat flux for suction occurs at the wall (assuming no viscous dissipation). The uncertainty in computing Q^+ is zero at the wall and increases further away from the wall. Since Q^+ goes to zero at the free stream, the relative uncertainty goes to infinity. The Couette flow assumption for Q^+ was accurate to within 2% for $y^+ < 70$, as shown by the data in Figure (6-4).

6.3 Turbulent Prandtl Number Profiles

The eddy viscosity and eddy diffusivity are defined through the relationships

$$\tau = \rho(\varepsilon_m + \nu) \frac{\partial u}{\partial y} \tag{6-13}$$

$$\dot{q}'' = - \rho c_p(\varepsilon_h + \alpha) \frac{\partial T}{\partial y} \tag{6-14}$$

In terms of wall variables, (6-13) and (6-14) can be written as

$$\tau^+ = \frac{\mu}{\mu_o}(\varepsilon_m^+ + 1) \frac{\partial u^+}{\partial y^+} \tag{6-15}$$

and

$$Q^+ = \frac{\mu}{\mu_o} \frac{\varepsilon_h^+ + 1/Pr}{1 - E/2} \frac{\partial T^+}{\partial y^+} \tag{6-16}$$

Solving (6-15) and (6-16) for ε_m^+ and ε_h^+ respectively, one obtains

$$\varepsilon_m^+ = \frac{\frac{\mu_o}{\mu} \tau^+}{\partial u^+/\partial y^+} - 1 \tag{6-17}$$

and

$$\varepsilon_h^+ = \frac{\frac{\mu_o}{\mu}(1 - E/2)Q^+}{\partial T^+/\partial y^+} - \frac{1}{Pr} \qquad (6\text{-}18)$$

The turbulent Prandtl number is defined as

$$Pr_t = \frac{\varepsilon_m^+}{\varepsilon_h^+} \qquad (6\text{-}19)$$

The critical experimental data necessary to calculate Pr_t are τ^+, Q^+, $\partial u^+/\partial y^+$, and $\partial T^+/\partial y^+$. The computation of both τ^+ and Q^+ was discussed in Section 6.1. As is well known, it is extremely difficult to differentiate experimental data such as velocity and temperature profiles, with any degree of certainty. After considerable numerical experimentation, the above derivatives were evaluated by curve-fitting a least-squares parabola through seven points, of the form (u^+, T^+) vs $\ell n\ y^+$, and evaluating the derivative at the center point; the end points had to be treated as special cases. Near the wall where the temperature and velocity gradients are the steepest, one would expect considerable difficulty in evaluating the derivatives accurately. Also, since both derivatives approach zero at the free stream, the relative uncertainty there approaches infinity. Consequently, the uncertainty of the derivatives is the smallest in the "middle" portion of the boundary layer. The turbulent Prandtl number calculations in the outer region are additionally hampered by the large uncertainty in both τ^+ and Q^+.

Figure (6-5) shows the influence of pressure gradient with no transpiration on the turbulent Prandtl number. It must be emphasized that the data in the inner region is quite uncertain; however, the data does have the consistent trend of being greater than unity very near the wall, and decreasing with increasing y^+. The pronounced dip in Run 110871 is thought to be due to numerical difficulties associated with evaluating $\partial u^+/\partial y^+$ and $\partial T^+/\partial y^+$. In the logarithmic region where the turbulent

Prandtl number data is the most certain, an adverse pressure gradient produces a decrease in turbulent Prandtl number.

Figures (6-6) and (6-7) show the effects of blowing on Pr_t for the $m = -0.15$ flows. Again, the data is consistently above unity close to the wall, but there does not appear to be a consistent trend with blowing, for either the constant F or B_h flows.

Figures (6-8) and (6-9) show the effects of suction on the turbulent Prandtl number. Again, it is high near the wall with no consistent trend with suction as one moves away from the wall.

In the log-region, Pr_t appears to be strongly dependent on the pressure gradient. The parameter $K = \frac{\nu}{u_\infty^2}\frac{du_\infty}{dx}$ is one means of characterizing the pressure gradient. This might suggest that Pr_t in the log-region could be correlated as a function of K. However, the Pr_t data in the log-region for a given set of boundary conditions was relatively independent of x while K was a strong function of x. Therefore, to correlate $(Pr_t)_\ell$ we need a pressure gradient parameter that is approximately constant for a given run. Since $|K|$ decreases with x while Re_θ increases with x, their product might not vary with x. It was found that the parameter $KRe_\theta/(H-1)$ correlated the $(Pr_t)_\ell$ data reasonably well. This correlation is shown in Figure 6-10. Also shown in Figure 6-10 is one data point for a strongly accelerated flow taken from the data of Kearney [7]. This data point is consistent with the trend of this study; deceleration produces a decrease in the turbulent Prandtl number in the log-region.

Figures 6-11 thru 6-15 present one turbulent Prandtl number profile in outer region coordinates for each of the runs of this study. Data for $y/\delta > 0.7 - 0.8$ is not presented because of the high degree of uncertainty. All of the data shows a decrease in Pr_t with increasing y/δ. Also, it appears that a limit of $Pr_t = 0.5$ at the outer edge of the boundary layer would be reasonable.

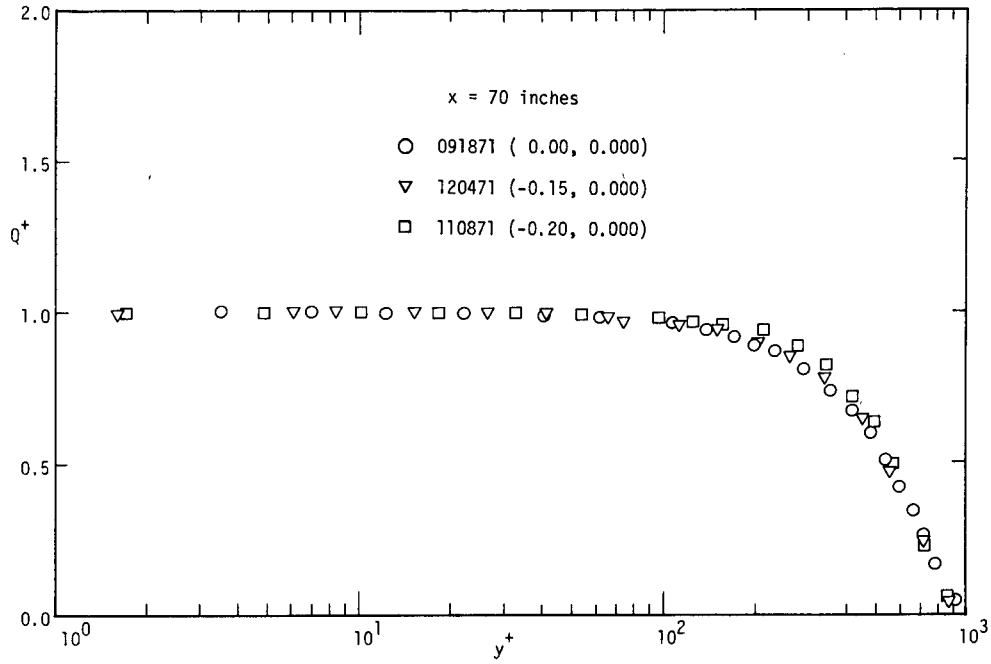


Figure 6-1 Influence of pressure gradient on heat flux profiles, F = 0

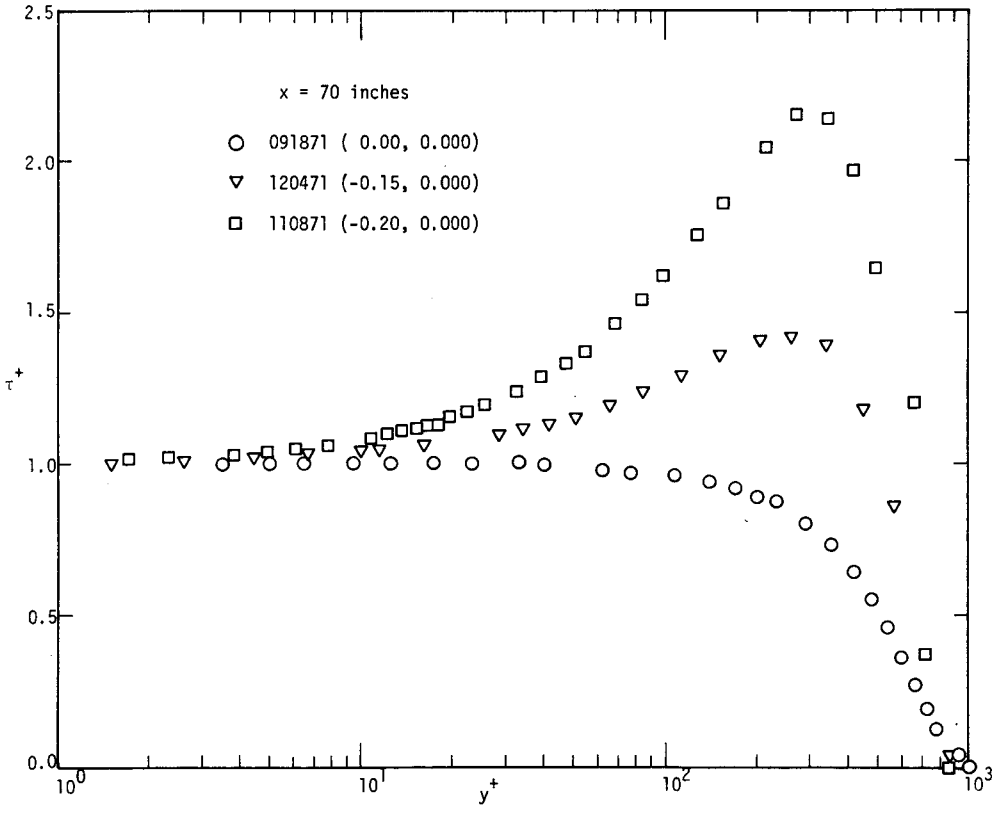


Figure 6-2 Influence of pressure gradient on shear stress profiles, F = 0

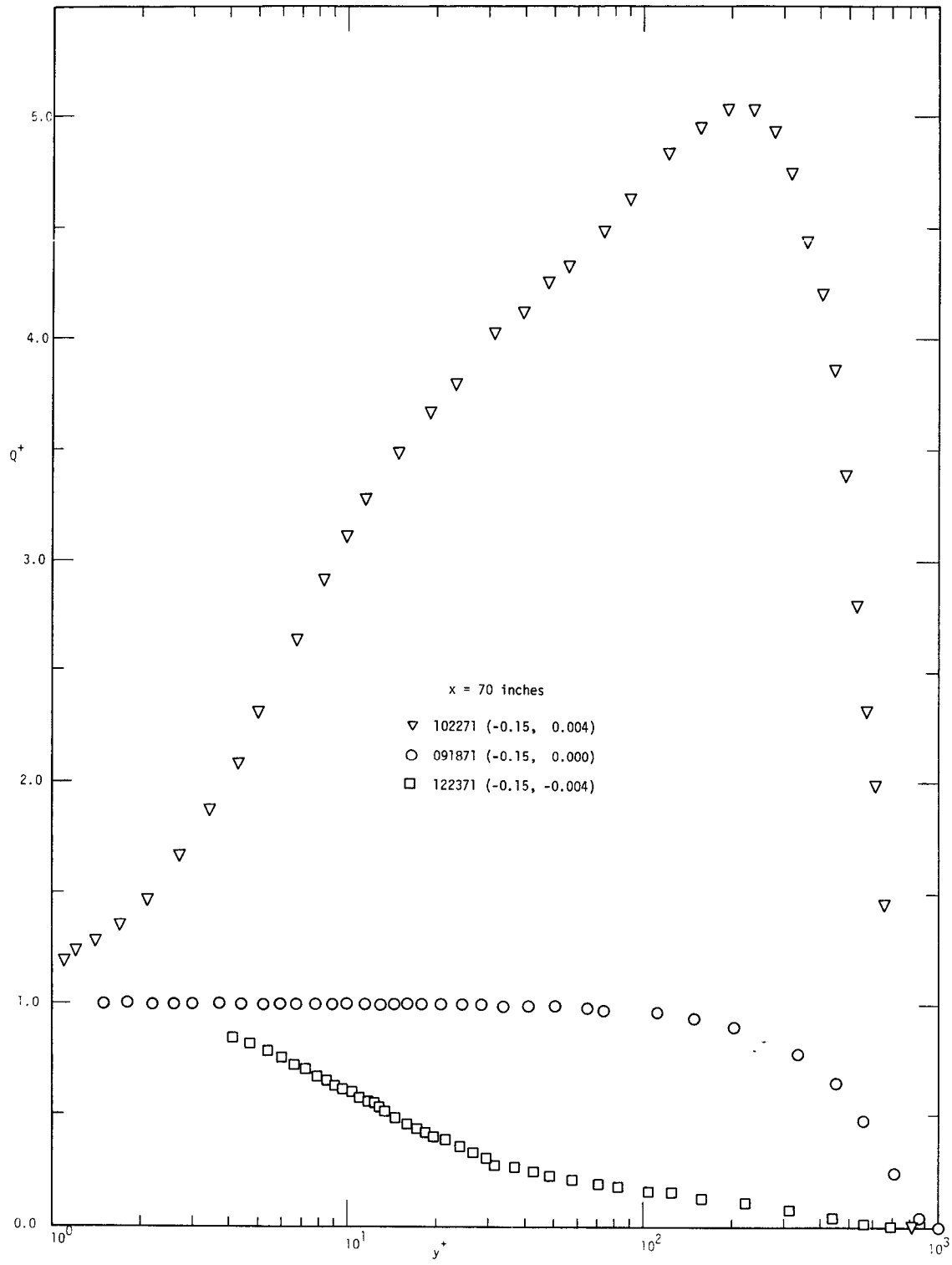


Figure 6-3 Influence of transpiration on heat flux profiles, m = -0.15

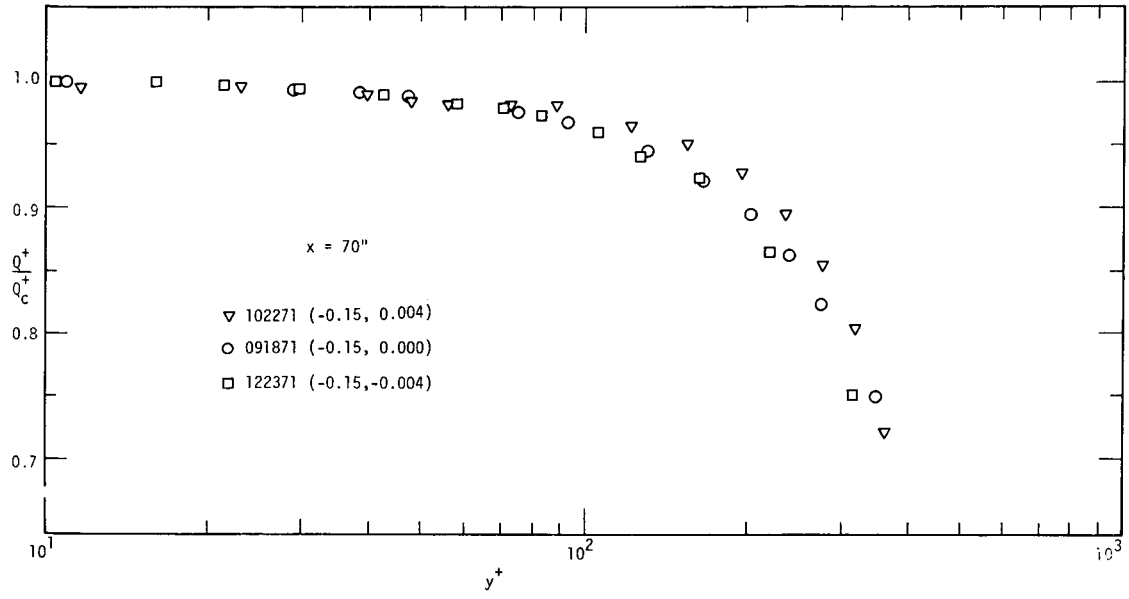


Figure 6-4 Validity of Couette flow assumption for computing heat flux profiles

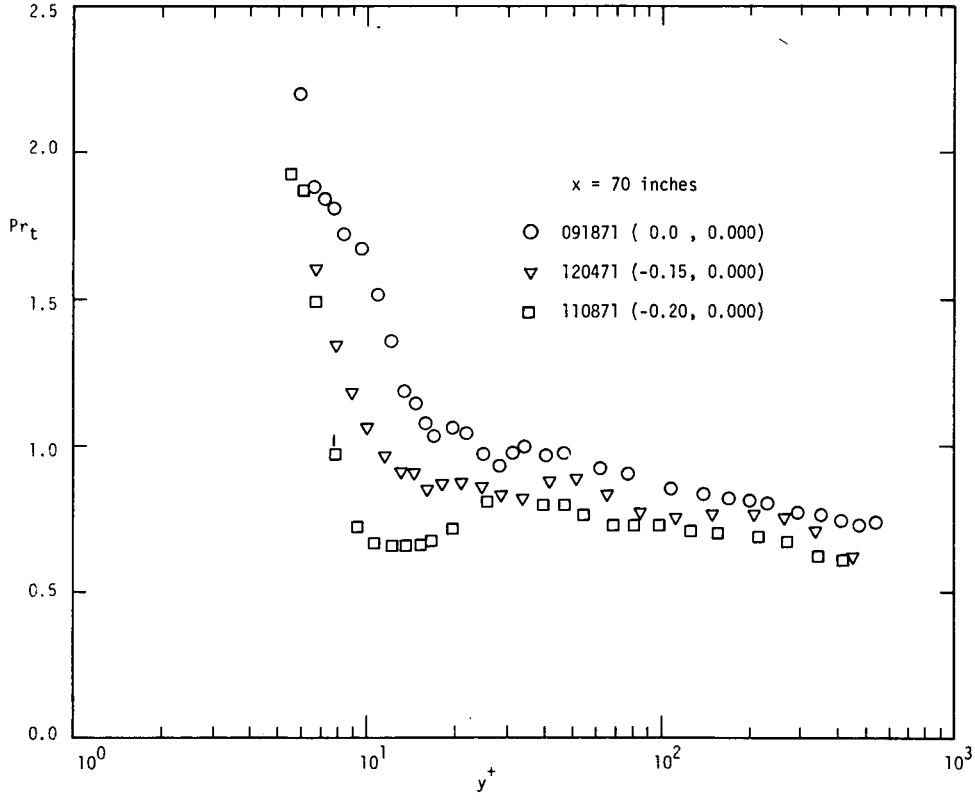


Figure 6-5 Influence of pressure gradient on turbulent Prandtl number profiles, x = 70 inches

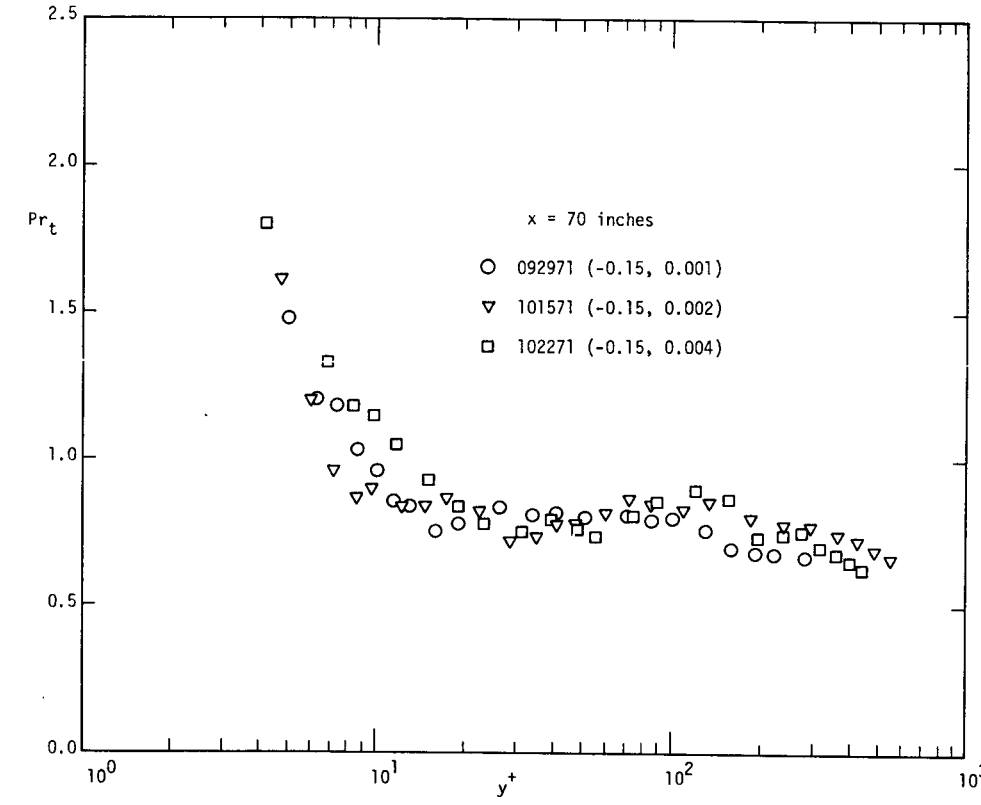


Figure 6-6 Influence of blowing on turbulent Prandtl number profiles, x = 70 inches

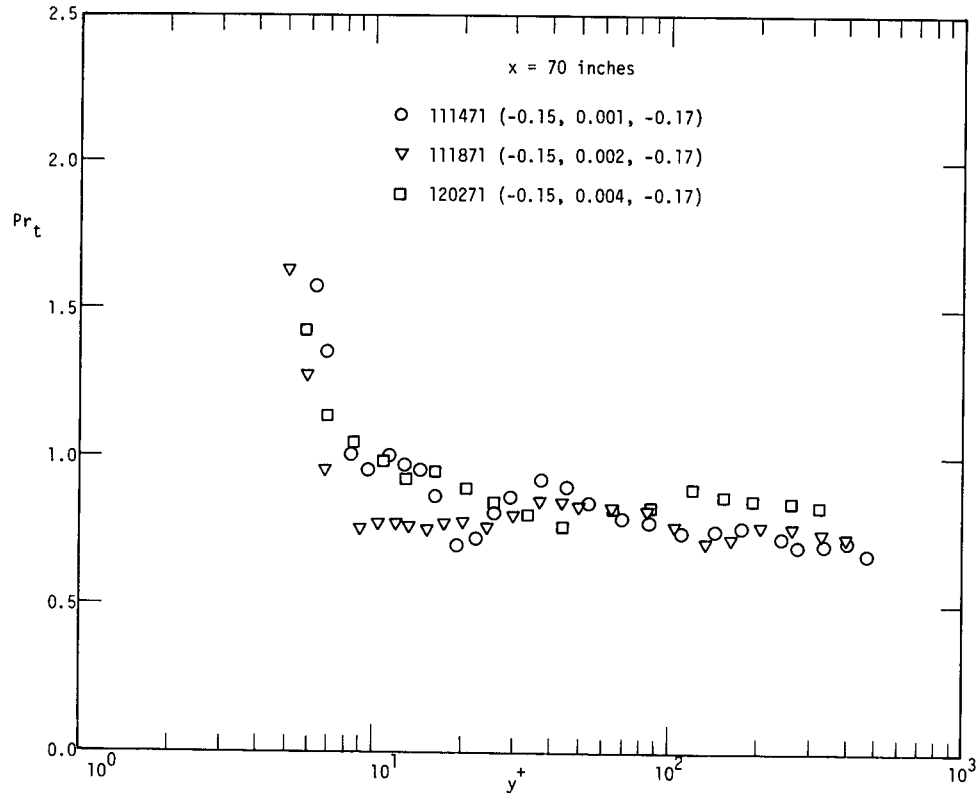


Figure 6-7 Influence of blowing on turbulent Prandtl number profiles, x = 70 inches

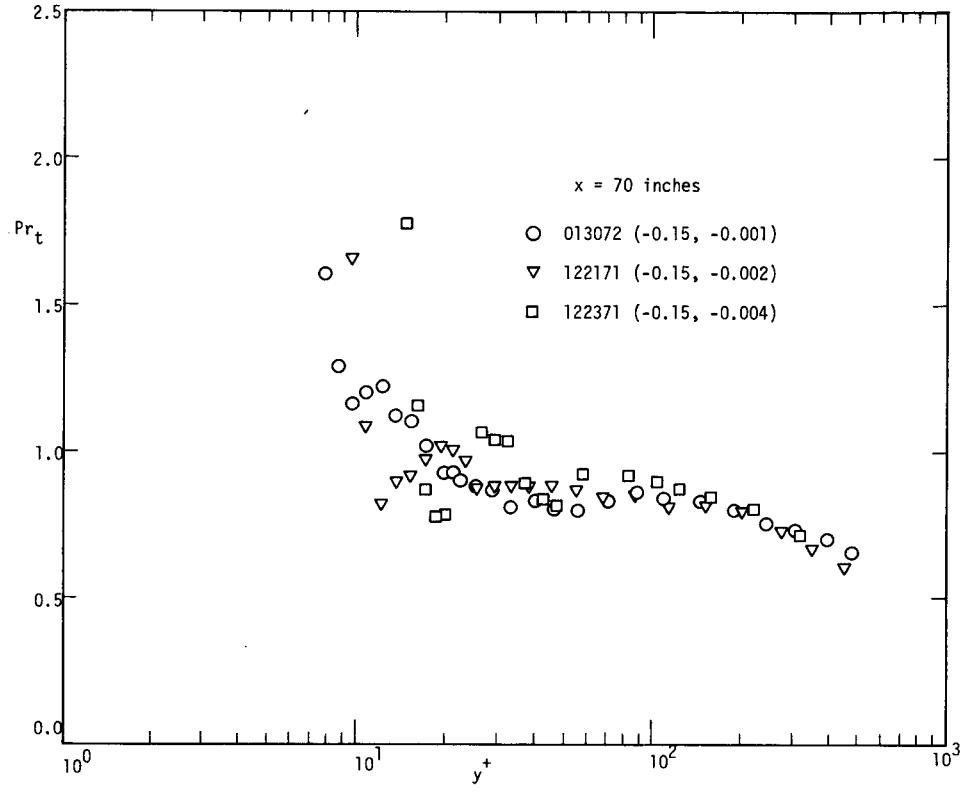


Figure 6-8 Influence of suction on turbulent Prandtl number profiles, x = 70 inches

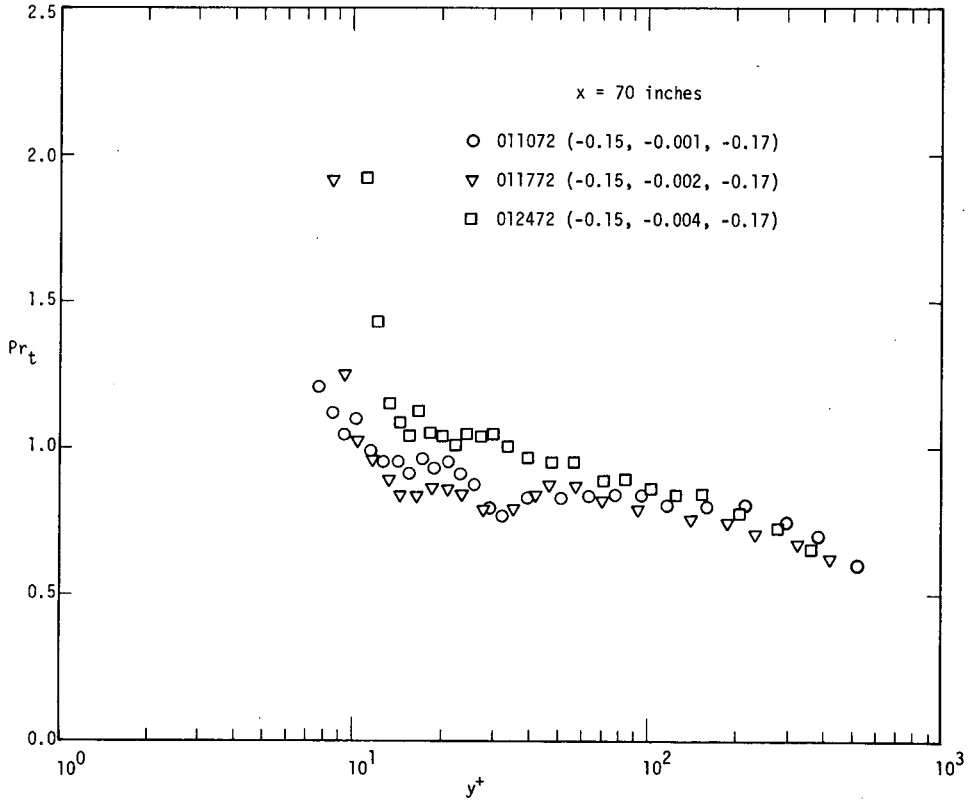


Figure 6-9 Influence of suction on turbulent Prandtl number profiles, x = 70 inches

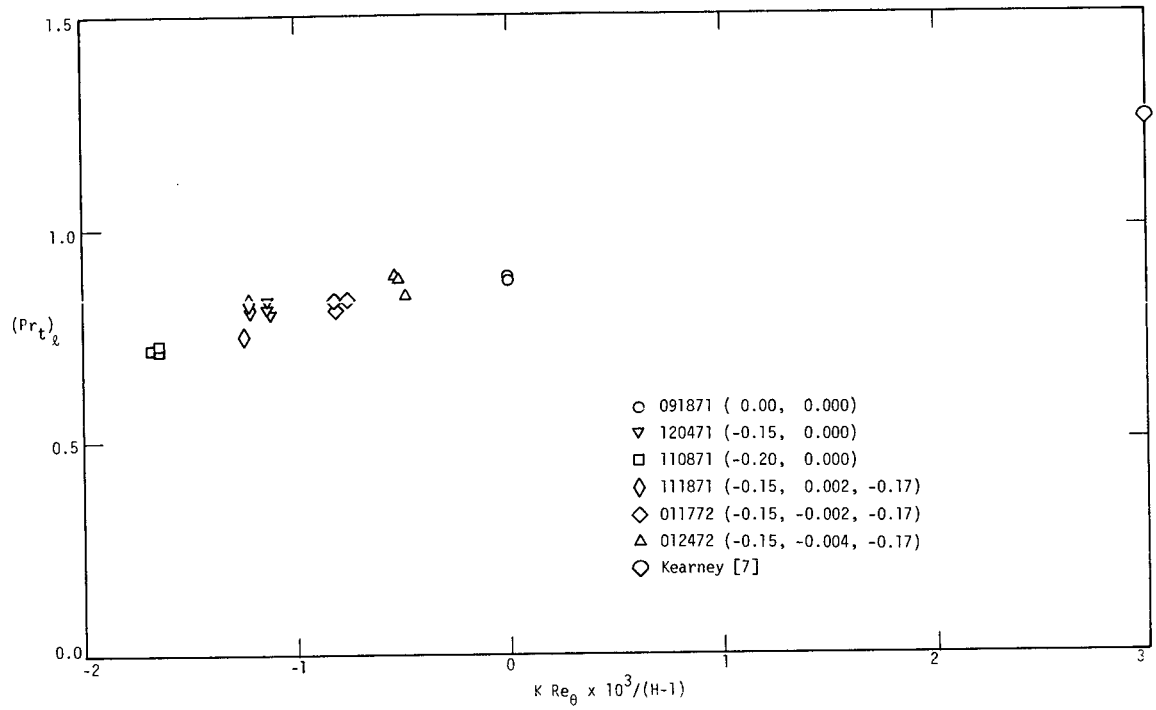


Figure 6-10 Variation of turbulent Prandtl number in log-region

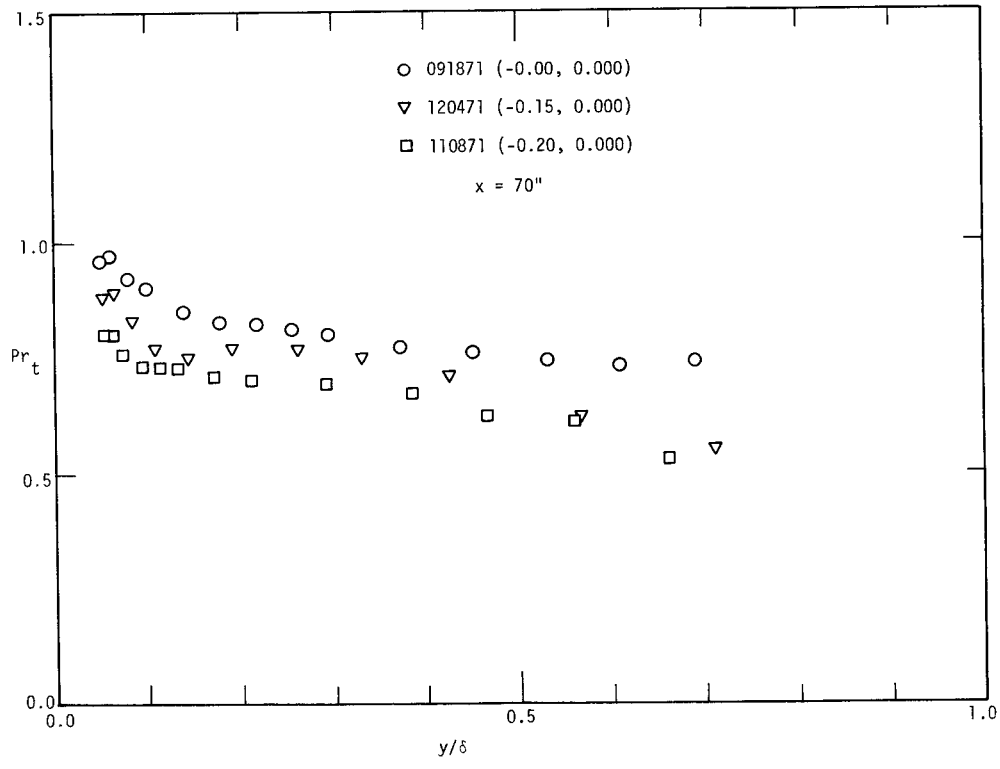


Figure 6-11 Influence of pressure gradient on turbulent Prandtl number profiles, x = 70 inches

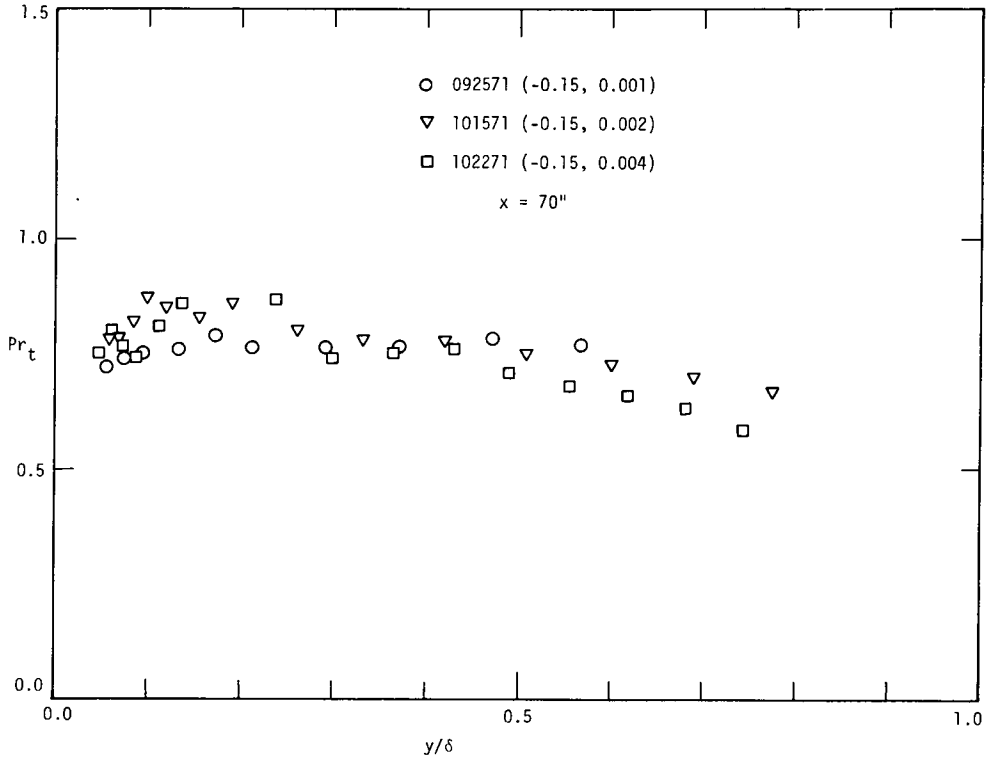


Figure 6-12 Influence of blowing on turbulent Prandtl number profiles, x = 70 inches

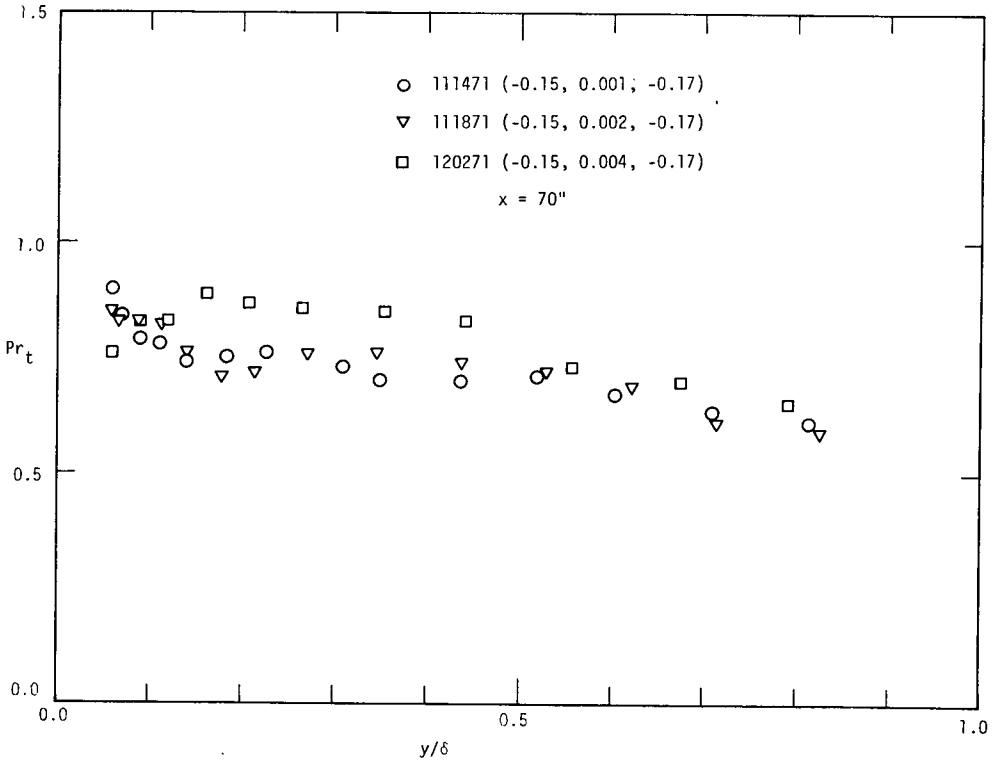


Figure 6-13 Influence of blowing on turbulent Prandtl number profiles, x = 70 inches

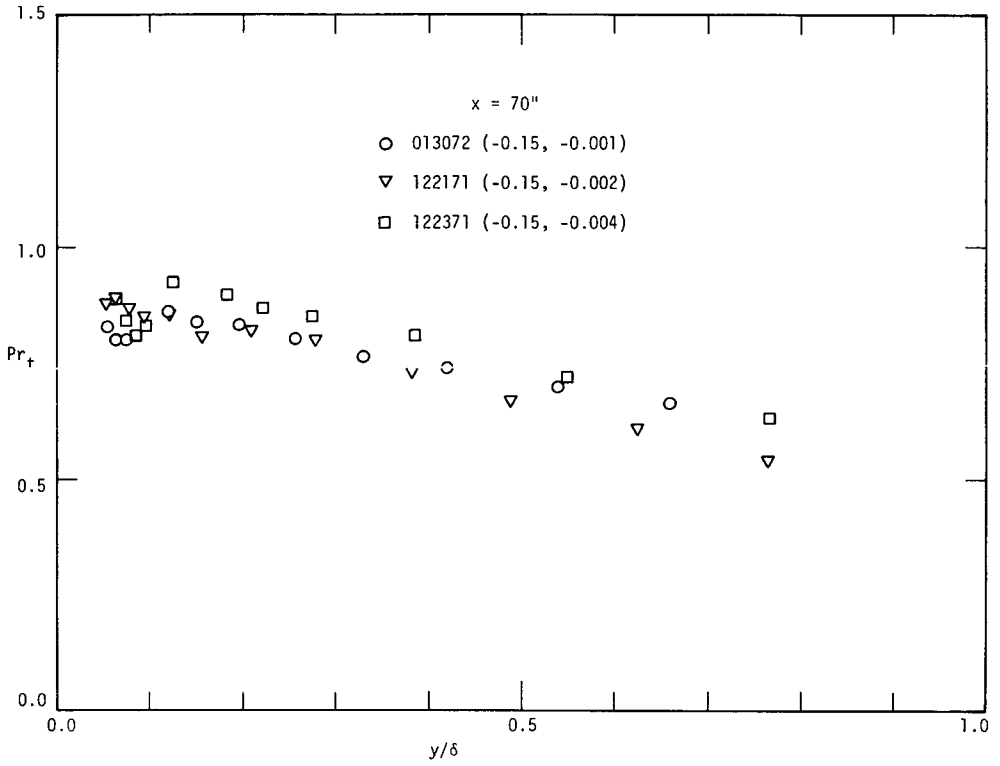


Figure 6-14 Influence of suction on turbulent Prandtl number profiles, x = 70 inches

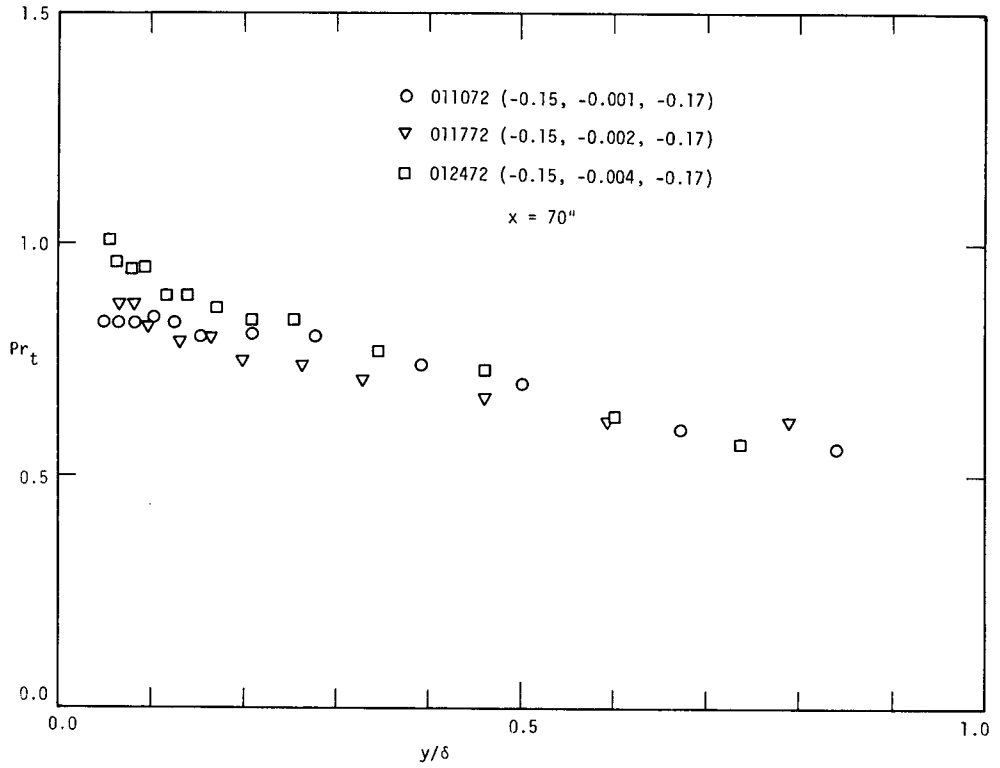


Figure 6-15 Influence of suction on turbulent Prandtl number profiles, x = 70 inches

CHAPTER 7

A TURBULENT PRANDTL NUMBER MODEL AND PREDICTION OF SELECTED RUNS

The turbulent Prandtl number has long been a useful concept in modeling turbulent heat transfer processes, even though the eddy diffusivity does not fully describe the events that occur in a turbulent boundary layer. Historically, the turbulent Prandtl number was first assumed to be unity. As more data became available, various analysts assumed that Pr_t was a constant but somewhat less than unity (for air). Beginning with Jenkins [21], a series of analysts have proposed turbulent Prandtl number models based on the idea that an "eddy" loses energy by molecular processes during its trajectory. Other examples of this type of eddy conduction model can be found in [22] - [24]. In the sections that follow, an analysis will be presented which is similar to that of Deissler's [22] for the turbulent Prandtl number variation in the inner region. In addition, an empirical correlation for Pr_t in the outer region will be shown, along with a comparison between experimental data and predictions using these models.

7.1 Turbulent Prandtl Number Model for Inner Region

The analysis that follows is quite similar to the analysis presented by Deissler [22]; consequently, only the more important points will be repeated here. Let us assume that an eddy originates at some distance y_1 from the wall and is convected upward with a characteristic velocity v. At this location y_1, the eddy is at a temperature T_1 equal to the mean temperature of the surrounding fluid. During the trajectory of this eddy, it is continuously losing energy to the surrounding fluid by molecular conduction. (It should be noted that the momentum transfer problem has no analogous loss mechanism, as opposed to the model of Jenkins [21]). When the eddy has traveled a distance ℓ in the vertical direction, it breaks up and mixes with the surrounding fluid. The eddy temperature at this new location $y_2 = y_1 + \ell$ is T_2', which is dif-

ferent from the mean fluid temperature T_2 at y_2. The energy transfer due to the turbulent mixing at the location y_2 is assumed to be given by

$$\dot{q}''_t = \rho c_p v(T'_2 - T_2) \tag{7-1}$$

Assuming that the mixing length ℓ is small, (7-1) can be written as

$$\dot{q}''_t = -\rho c_p v \ell \left[\frac{T'_2 - T_2}{T_1 - T_2}\right] \frac{\partial T}{\partial y} \tag{7-2}$$

The eddy diffusivity for heat transfer is defined through the relationship

$$\dot{q}''_t = -\rho c_p \varepsilon_h \frac{\partial T}{\partial y} \tag{7-3}$$

From (7-2) and (7-3), we obtain

$$\varepsilon_h = v\ell \left[\frac{T'_2 - T_2}{T_1 - T_2}\right] \tag{7-4}$$

But the product $v\ell$ should be proportional to the eddy viscosity ε_m. Consequently, the turbulent Prandtl number can be written as

$$Pr_t = \frac{\varepsilon_m}{\varepsilon_h} = C_1 \frac{T_1 - T_2}{T'_2 - T_2} = C_1 \theta' \tag{7-5}$$

Equation (7-5) is the same as that derived by Deissler [22], except that Deissler set $C_1 = 1$. As we shall see later, the constant C_1 can be significantly different from unity.

With (7-5) as the basic model for the turbulent Prandtl number, the problem remaining is to evaluate the eddy temperature during its trajectory. Various investigators have proposed eddy conduction models of varying degrees of sophistication. Three of the models that are available in the literature are:

Deissler [22],

$$\theta' = \frac{\phi}{1 - e^{-\phi}} \tag{7-6}$$

Jenkins [21]*,

$$\theta' = \frac{\phi}{1 - \frac{90}{\pi^4}\sum_{n=1}^{\infty}\frac{1}{n^4}\exp(-\frac{n^2\pi^2}{15}\phi)} \tag{7-7}$$

and, Lykoudis [23]

$$\theta' = \frac{\pi^2/6}{\sum_{n=1}^{\infty}\frac{1}{n^2}\exp(-\frac{n^2\pi^2}{15}\phi)} \tag{7-8}$$

where the parameter ϕ is given by

$$\phi = \frac{C_2}{\frac{\varepsilon_m}{\nu}\,Pr} \tag{7-9}$$

In the above analyses, the significant parameter is the turbulent Peclet number $Pe_t = Pr\ \varepsilon_m/\nu$. However, it should be noted that Pe_t is independent of the molecular viscosity. Figure 7-1 presents a comparison of the three different eddy conduction models. The Deissler [22] and Jenkins [21] models are quite similar. Although the Lykoudis [23] model appears quite different, the yet unspecified constant C_2 for this model would be quite different from the C_2 for the other two models. All

*When (7-7) is used in conjunction with (7-5) for a Pr_t model, the result is quite different from that proposed originally by Jenkins [21].

three models have a common asymptote of unity for large values of eddy viscosity ε_m .

The Deissler [22] model is essentially a lumped parameter analysis. Since it is the simplest of the three model presented here, it was adopted for this study. It is felt that any of the above three models would prove adequate for prediction purposes provided the constants were chosen in a consistent manner. The turbulent Prandtl number model used for the remainder of this study was*

$$Pr_t = C_1 \frac{\phi}{1 - e^{-\phi}}, \quad \phi = \frac{C_2}{\frac{\varepsilon_m}{\nu} Pr} \tag{7-10}$$

Equation (7-10) has two free constants; in reality, C_1 and C_2 are probably not universal constants and must be empirically correlated for each class of data. For large values of ε_m , (7-10) approaches $Pr_t = C_1$. Therefore, C_1 should be approximately equal to the turbulent Prandtl number in the log-region. The constant C_2 controls the portion of the boundary layer where a rapid decrease in Pr_t occurs. The limiting case of $C_2 = 0$ would correspond to $Pr_t = C_1$ throughout the inner portion of the boundary layer.

The problem we are faced with now is how to evaluate C_1 and C_2 . Computational experiments showed that a computed temperature profile is much more sensitive to changes in C_1 than in C_2 . Therefore, based on these computational experiments, a nominal value of $C_2 = 0.5$ was chosen. Since C_1 is essentially the turbulent Prandtl number in the log-region, the data in Figure 6-10 could be taken as representing C_1 . However, due to the experimental uncertainty in the Pr_t calculations, it was decided to integrate the equations from the wall out to the log-

*(7-10) is essentially the same as a limiting case of the analysis presented by Tokuro [24]. However, the values of C_1 and C_2 for this study are quite different from those proposed by Tokuro.

region and vary the constant C_1 (with $C_2 = 0.5$) until the computed temperature matched the experimental temperature at a particular point. The y^+ location where the matching occurred varied with pressure gradient and transpiration but was always in the log-region. The computational procedure was to integrate (6-16) numerically using the computed heat flux profiles discussed in CHAPTER 6 and (7-10) for the turbulent Prandtl number model.

$$\frac{dT^+}{dy^+} = \frac{\frac{\mu_o}{\mu}(1 - E/2)}{\frac{\varepsilon_m^+}{Pr_t} + \frac{1}{Pr}} Q^+ \qquad (7\text{-}11)$$

The eddy viscosity model for ε_m^+ was that proposed by Andersen [9]. The results of this series of computational experiments is shown in Figure 7-2, and are adequately represented by the empirical equation

$$C_1 = 0.8(\gamma + 2)^{0.17} \qquad (7\text{-}12)$$

where γ is defined as

$$\gamma = K \times 10^3 \, Re_\theta/(H\text{-}1) \qquad (7\text{-}13)$$

For the origin of γ, see Section 6.2. The data in Figure 7-2 is consistent with the data in Figure 6-10 and has less scatter.

7.2 Turbulent Prandtl Number Model for Outer Region

Rotta [25] proposed that the turbulent Prandtl number in the outer region be correlated by

$$Pr_t = 0.95 - 0.45(y/\delta)^2 \qquad (7\text{-}14)$$

Equation (7-14) also fits the zero pressure gradient data of Simpson [26] quite well. Note that this equation has a limit of 0.5 at the outer edge of the boundary layer, which is consistent with the data in Figures 6-11 thru 6-15. Since we have already established that the turbulent Prandtl number in the log-region depends on parameter γ, (7-14) will

not be adequate for the data of this study. Using (7-14) as a guide, it is proposed that Pr_t in the outer region be modeled by

$$Pr_t = 0.5 + b_1[1 - (y/\delta)^2] \tag{7-15}$$

The constant b_1 was determined by requiring that (7-15) agree with (7-10) at some point in the boundary layer. The match point for these two expressions was at $y/\delta = \lambda/\kappa$, which is commonly used as the dividing point between the inner and outer part of a mixing length model for momentum transfer. The values of λ and κ were taken from Andersen [9]. Matching these two expressions yields

$$b_1 = \frac{C_1 - 0.5}{1 - \left(\frac{\lambda}{\kappa}\right)^2} \tag{7-16}$$

Since the computed turbulent Prandtl numbers in the outer region are quite uncertain, it is difficult to judge the validity of (7-15) using only the Pr_t data of CHAPTER 6. However, one check will be to use (7-15) with a finite-difference boundary layer prediction program. This will be discussed in subsequent sections.

7.3 Comparison of Predicted Stanton Numbers With Experimental Data

In order to verify the turbulent Prandtl number model proposed in Section 7.2, the model was used in conjunction with a version of the Patankar-Spalding [29] computational procedure for solving the boundary layer equations. The mean velocity field closure was accomplished with the model proposed by Andersen [9]. This mixing-length model is given by

$$\ell = \begin{cases} \kappa y[1 - \exp(-y/A)], & y \leq \lambda\delta/\kappa \\ \lambda\delta, & y > \lambda\delta/\kappa \end{cases} \tag{7-17}$$

The length scale, A, in this van Driest type model was obtained from

$$A = \frac{A_o}{\sqrt{\tau^+(3A)}} \tag{7-18}$$

The parameter λ showed a weak dependence on F and Re_θ ; for the details of this, see Andersen [9]. Four runs were selected as test cases. These runs cover a wide range of transpiration boundary conditions and for two of the pressure gradients of this study. In all cases, the experimental velocity and temperature profiles at $x = 2$ inches were used as the starting profiles.

Figure 7-3 presents a comparison of experimental Stanton numbers with predictions for the zero pressure gradient, no transpiration run. The experimental data presented for all of the Stanton number comparisons was the "best interpretation" of runs 1 and 2 (see Section 4.3). The agreement is excellent. Figure 7-4 presents the Stanton number comparison for the adverse pressure gradient $u_\infty \sim x^{-0.15}$ with no transpiration. The agreement is within 5%. Figures 7-5 and 7-6 present the Stanton number comparisons for the strongest suction and strongest blowing boundary conditions respectively, where B_h was held constant. The strong blowing run shows the largest discrepancy with the predicted values as much as 12% high. However, the predictions are within the experimental uncertainty.

Andersen [9] presented a comparison of experimental data with predictions for the hydrodynamics of some of the same flows presented here. He concluded that his mixing length model performed worst for the case of strongest blowing. Since the turbulent Prandtl number model proposed in this study depends on Andersen's [9] mixing length model, it is not possible to ascertain whether the relatively poor Stanton number predictions for strong blowing could be blamed on the mixing length model, turbulent Prandtl number model, or the experimental uncertainty in determining Stanton number.

7.4 Comparison of Predicted Temperature Profiles With Experimental Data

In this section, a predicted temperature profile will be compared with an experimental profile for each of the four runs discussed in Section 7.3. In all cases, the x-location for comparison was chosen to be 70 inches. This x-location was chosen because the flow should be in equilibrium this far downstream. Figure 7-7 presents the temperature profile comparison for the zero pressure gradient, no transpiration run. The agreement is quite good. Figures 7-7 - 7-10 present the temperature profile comparisons for the other three runs. Again, the agreement is quite good. In fact, the temperature profile agreement is better than the Stanton number agreement (except for the zero pressure gradient, no transpiration run). This raises the question of how the temperature profiles could agree better than the Stanton numbers. The particular computer program used computes the wall heat flux by evaluating the temperature gradient at the wall numerically. The Stanton number data might be improved by using an energy integral equation to evaluate the Stanton number from the predicted rate of growth of the boundary layer, but this has not been attempted.

7.5 Some Comments on a Heat Transfer Mixing Length Model

Meier [30] proposed that the turbulent heat transfer processes in the inner part of the boundary layer could be modeled using a heat transfer mixing-length. This proposed model takes the form

$$\varepsilon_h^+ = \ell_h^{+2} \frac{\partial u^+}{\partial y^+} \tag{7-19}$$

where the non-dimensional heat transfer mixing length is given by

$$\ell_h^+ = \kappa_h y^+ [1 - \exp(-y^+/A_h^+)] \tag{7-20}$$

where κ_h is a heat transfer parameter analogous to the von Kármán constant κ and A_h^+ is a measure of the thermal boundary layer sublayer thickness. If one uses a momentum transfer mixing length model similar to (7-20), then the turbulent Prandtl number in the log-region (large y^+)

is given by

$$Pr_t = \left(\frac{\kappa}{\kappa_h}\right)^2 \quad , \quad y^+ \text{ large} \tag{7-21}$$

Meier [30] proposed that $(\kappa/\kappa_h)^2 = 0.86$ for air. It will be shown in this section that if $\kappa = 0.41$ (as used by Andersen [9] and many other investigators), then κ_h must be a function of pressure gradient (and possibly transpiration rate).

If one plots ℓ_h^+/y^+ as a function of y^+/A_h^+, (7-20) indicates that the limit in the log-region should be κ_h. Figure 7-11 shows the influence of pressure gradient with no transpiration on the heat transfer mixing length ℓ_h^+. This data clearly indicates that κ_h increases in an adverse pressure gradient. This is consistent with the fact that the turbulent Prandtl number in the log-region decreases in an adverse pressure gradient. The conclusion is that if one attempted to extend Meier's [30] model to heat transfer with adverse pressure gradient, one must correlate κ_h as a function of pressure gradient.

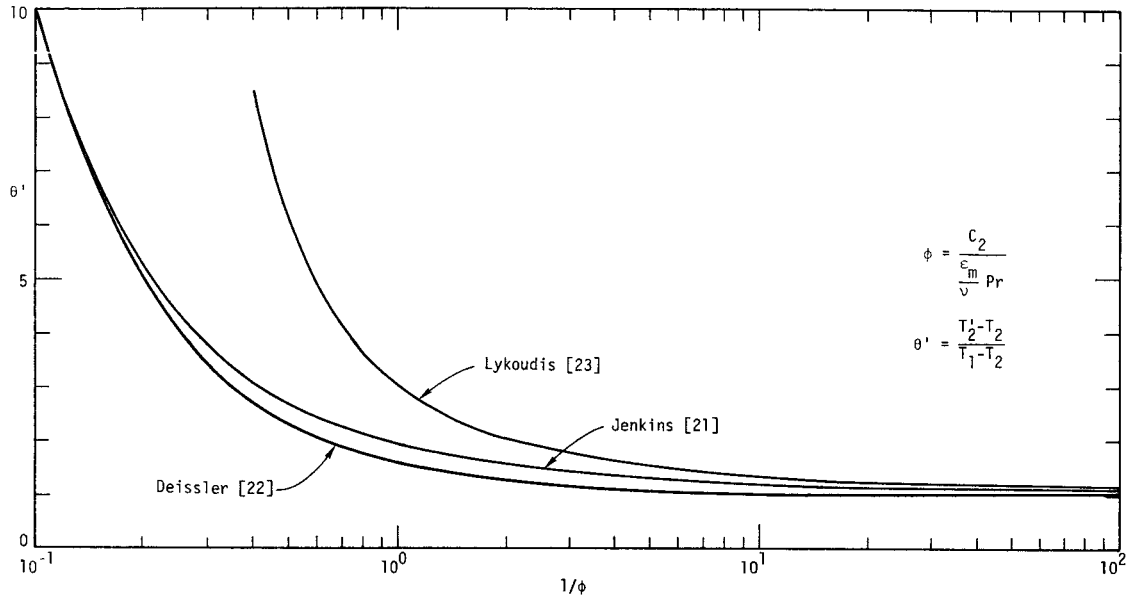


Figure 7-1 Comparison of different eddy heat transfer models

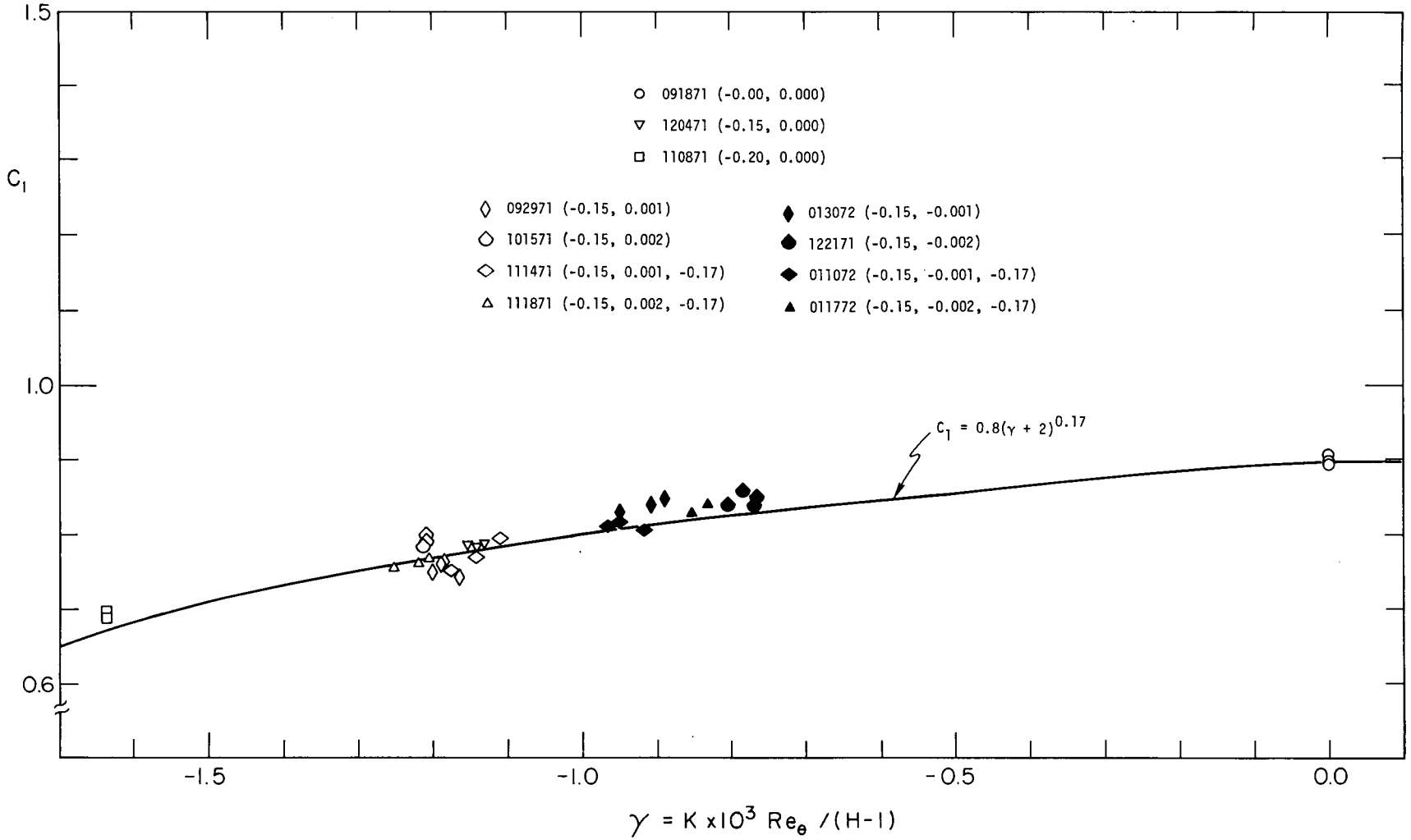


Figure 7-2 Variation of C_1 in the turbulent Prandtl number model

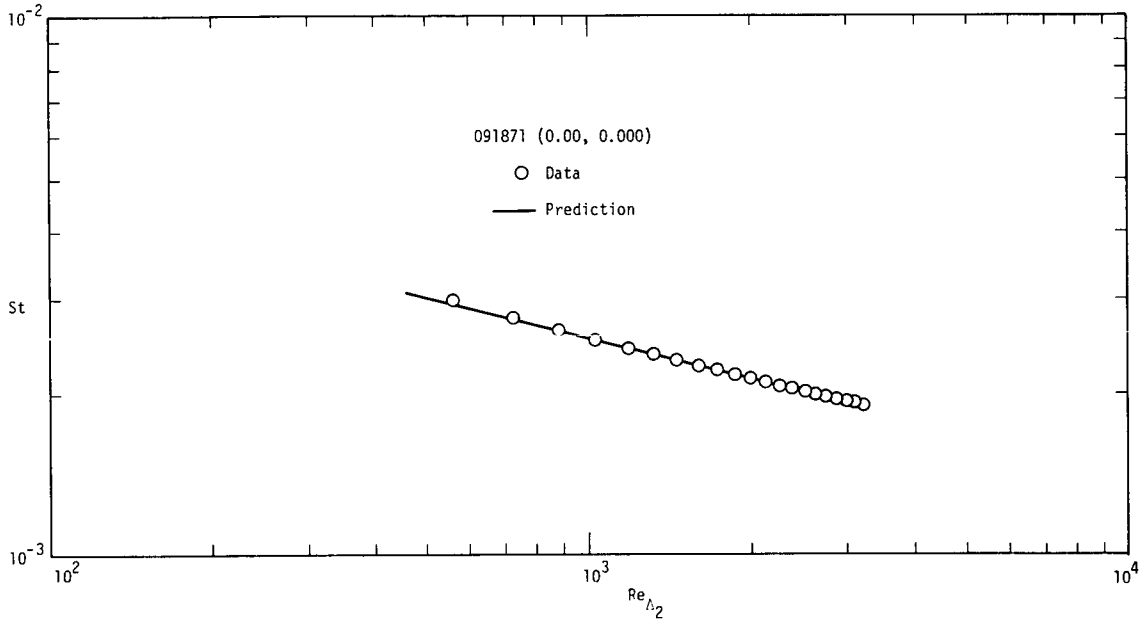


Figure 7-3 Comparison of predicted Stanton numbers with experimental data, run 091871

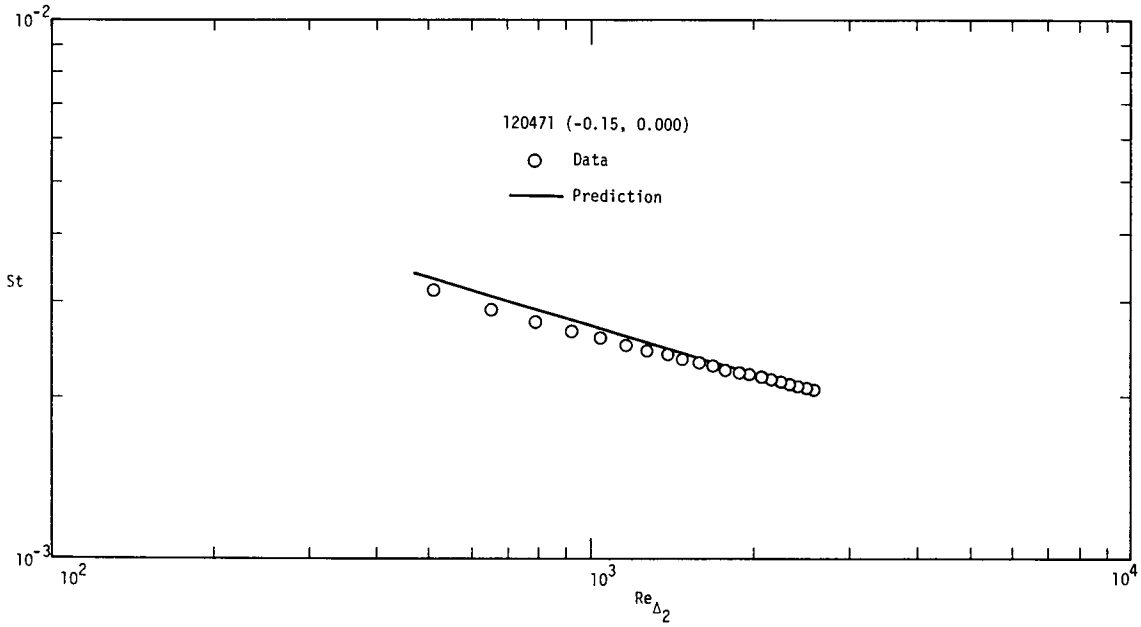


Figure 7-4 Comparison of predicted Stanton numbers with experimental data, run 120471

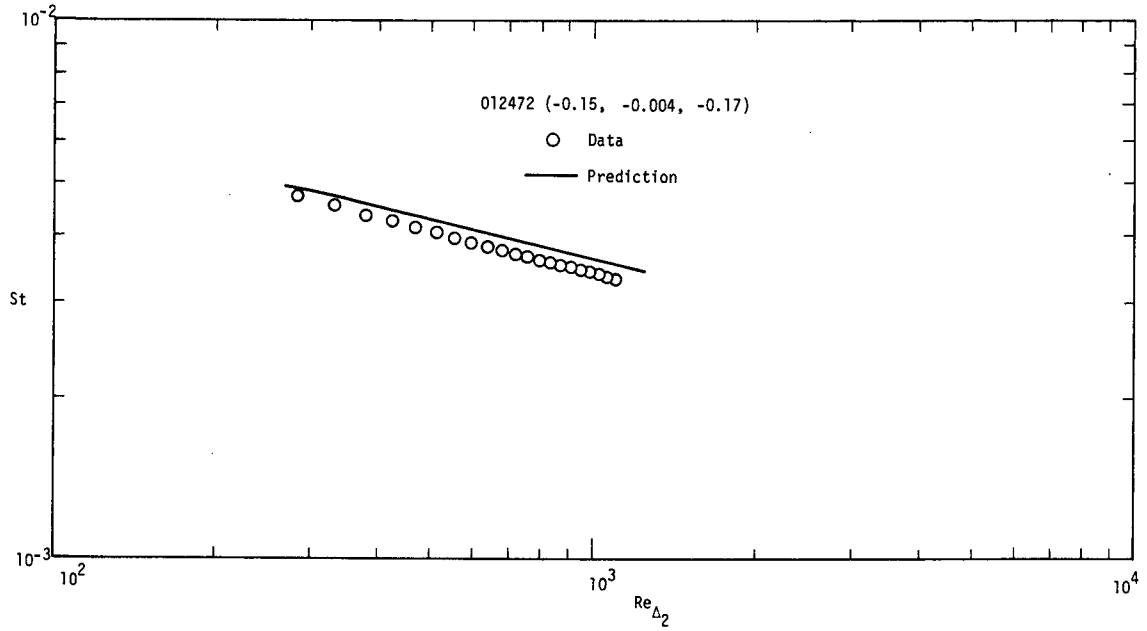


Figure 7-5 Comparison of predicted Stanton numbers with experimental data, run 012472

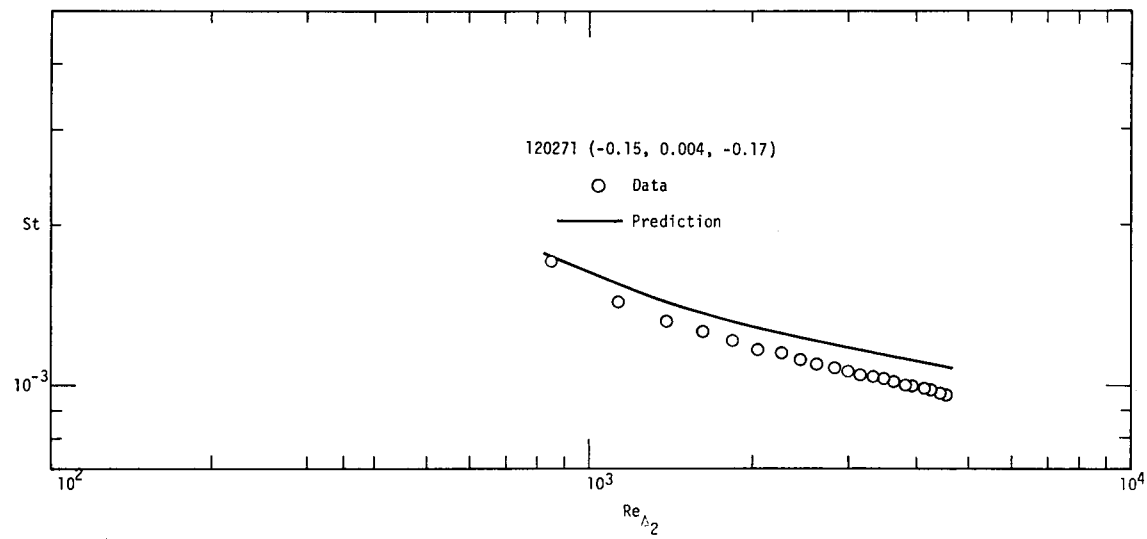


Figure 7-6 Comparison of predicted Stanton numbers with experimental data, run 120271

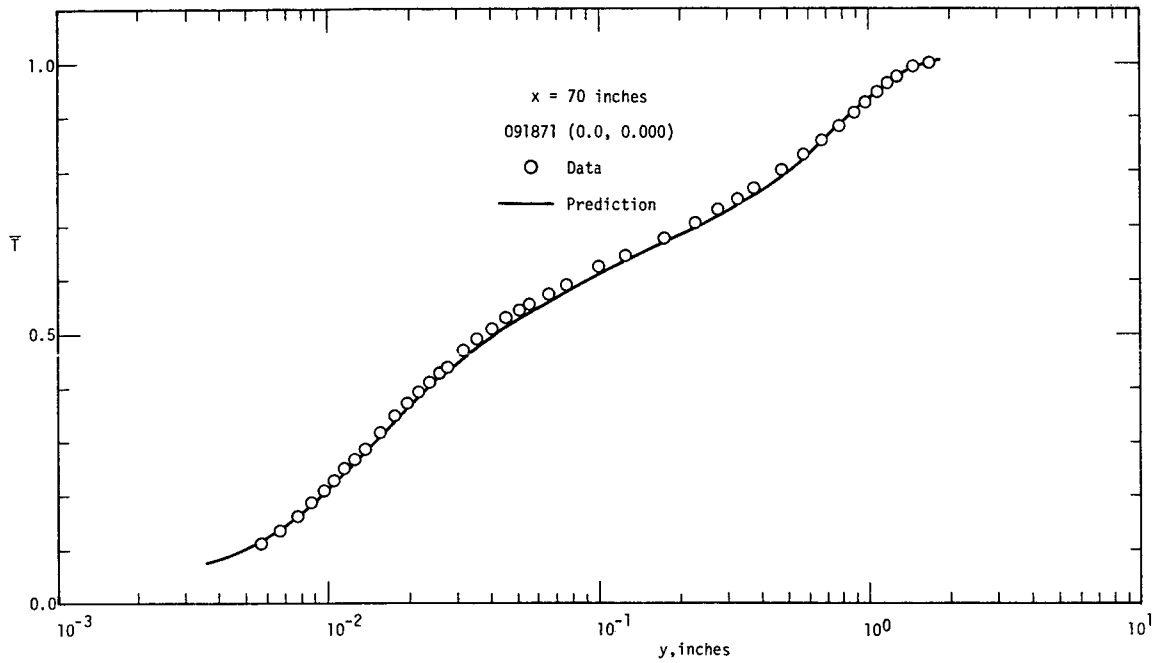


Figure 7-7 Comparison of predicted temperature profile with experimental data, run 091871

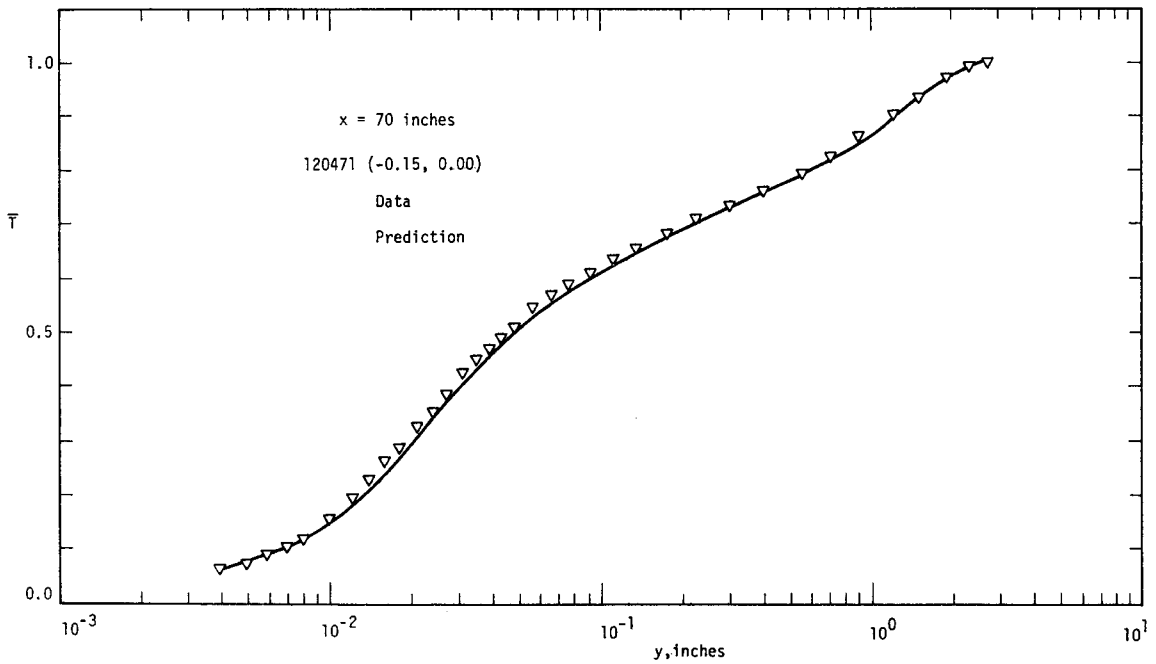


Figure 7-8 Comparison of predicted temperature profile with experimental data, run 120471

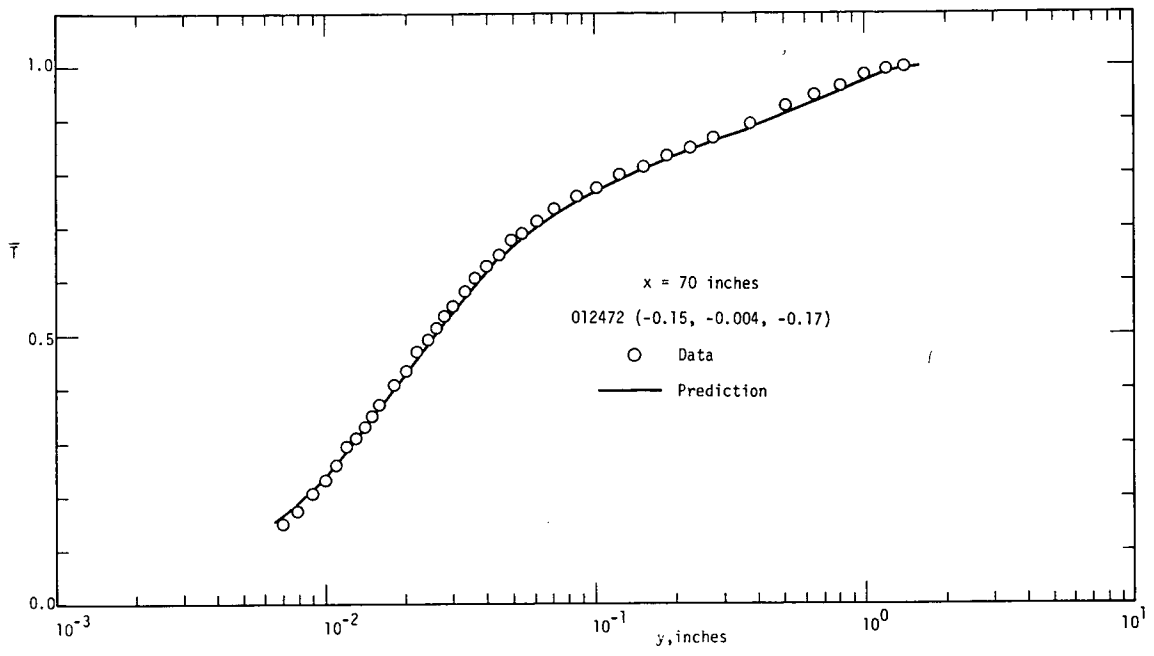


Figure 7-9 Comparison of predicted temperature profile with experimental data, run 012472

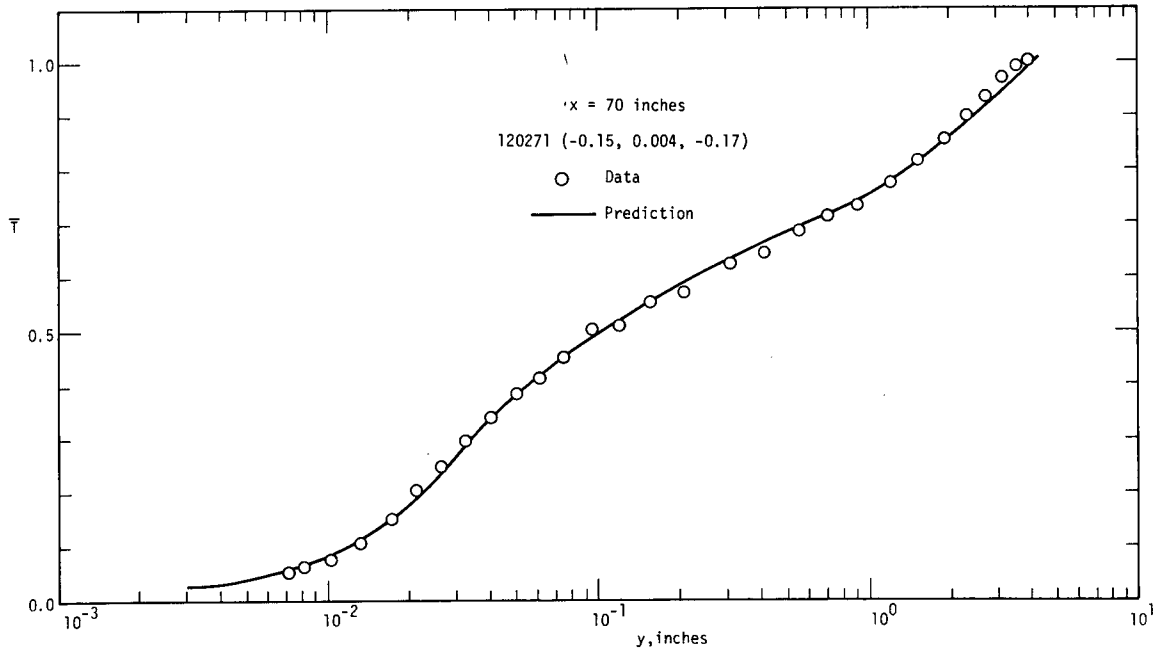


Figure 7-10 Comparison of predicted temperature profile with experimental data, run 120271

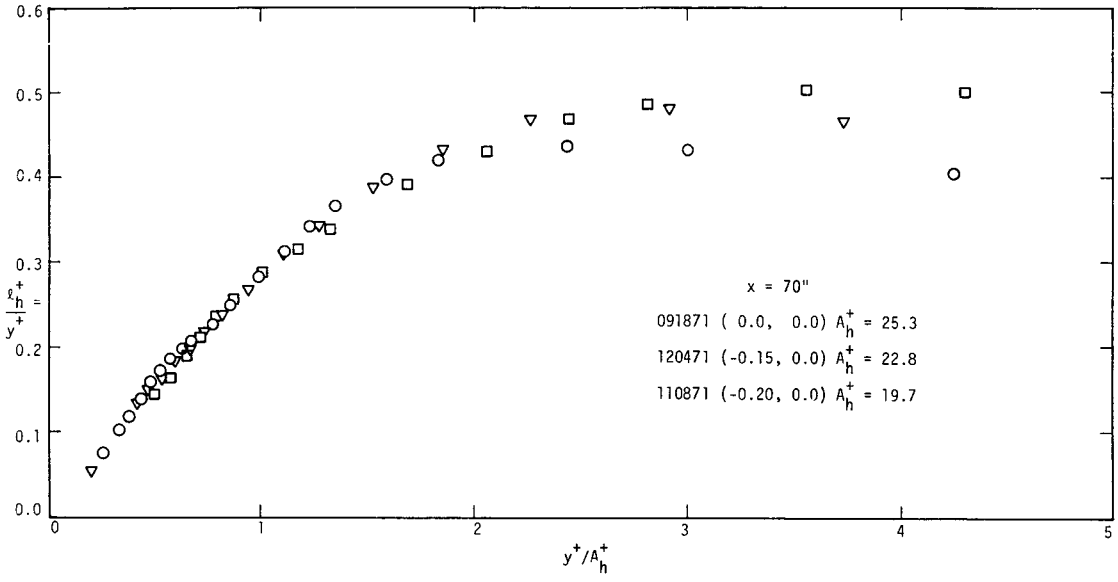


Figure 7-11 Influence of pressure gradient on heat transfer mixing length

CHAPTER 8

SUMMARY

The heat transfer behavior of the near equilibrium transpired turbulent boundary layer in an adverse pressure gradient has been studied experimentally using a total of 15 different combinations of pressure gradient and transpiration boundary conditions. Stanton numbers were measured by an energy balance technique while mean temperature profiles were measured by a 0.003 inch diameter Chromel/constantan thermocouple. The free stream velocity and transpiration boundary conditions of this study can be characterized by:

$$u_\infty \sim x^m \quad , \quad m < 0 \tag{8-1}$$

and

$$F \sim F_1 x^{m_F} \quad , \quad m_F = m_F(m) \tag{8-2}$$

The values of (m, F_1, m_F) are tabulated in Table 2-2. It was experimentally determined that for a given m and $m_F \neq 0$, the heat transfer parameter $B_h = F/St$ was a constant for a given run.

By comparing the adverse pressure gradient data of this study with the zero pressure gradient data of Moffat [2], it was concluded that mild adverse pressure gradients do not substantially alter the Stanton number-enthalpy thickness Reynolds number relationship (for a given transpiration rate). The extreme blowing and suction runs showed the greatest difference between zero pressure gradient and adverse pressure gradient. If the transpiration rate changes slowly as in this study, then the Stanton number for a given adverse pressure gradient (i.e. given m) is a function of B_h only. This functional relationship is of the form

$$\frac{St}{St_o} = f(B_h) \tag{8-3}$$

where St_o is the Stanton number at the same value of m and Re_{Δ_2} but with $F = 0$.

Various investigators have reported that a law-of-the-wall exists for the velocity boundary layer with adverse pressure gradients and no transpiration. The data of this study indicates that an analogous law-of-the-wall for the thermal boundary layer does not exist.

The concept of an equilibrium thermal boundary layer was introduced in CHAPTER 2. It is characterized by outer layer similarity in terms of $I_\infty^+ - I^+$ as a function of y/Δ_3 where Δ_3 is an integral thickness of the thermal layer. A shape factor that characterizes this outer layer enthalpy defect similarity was introduced and is defined by

$$G_h = \frac{\int_0^\infty (I_\infty^+ - I^+)^2 \, dy}{\int_0^\infty (I_\infty^+ - I^+) \, dy} \tag{8-4}$$

For all of the flows studied, G_h was approximately constant for a given run except for the profiles close to the beginning of the test section. This was attributed to the fact that the momentum boundary layer originated upstream of the thermal boundary layer.

Shear stress, heat flux and turbulent Prandtl number profiles were computed from mean velocity and temperature profiles. It was concluded that the turbulent Prandtl number is greater than unity close to the wall and decreases continuously to approximately 0.5 at the free stream. Adverse pressure gradient has more of an effect on the turbulent Prandtl number than does transpiration. An adverse pressure gradient decreases the turbulent Prandtl number in the log-region.

A turbulent Prandtl number model was proposed and used in a finite difference computer program that solves the continuity, momentum, and energy equations. The inner region Pr_t model was

$$Pr_t = C_1 \frac{\phi}{1 - e^{-\phi}} \quad , \quad \phi = \frac{0.5}{\frac{\varepsilon_m}{\nu} Pr} \tag{8-5}$$

where

$$C_1 = 0.8(\gamma + 2)^{0.17} \quad , \quad \gamma = K \times 10^3 Re_\theta/(H-1) \tag{8-6}$$

while the outer region model was

$$Pr_t = 0.5 + b_1[1 - (y/\delta)^2] \tag{8-7}$$

with the constant b_1 being determined from continuity of (8-5) and (8-7). Four representative cases were predicted using the above turbulent Prandtl number model and a mixing-length momentum transfer model proposed by Andersen [9]. In all cases, the Stanton number predictions were within the experimental uncertainty of the data.

CHAPTER 9

TABULATION OF EXPERIMENTAL DATA

All the experimental Stanton numbers and mean temperature profiles of this study are tabulated in this chapter. The Stanton number data will be presented in Section 9.1 and the mean temperature profiles in Section 9.2. The order in which the runs are tabulated (in both sections) is given in Table 9.1.

Date	m	F_1	m_F
	F = 0		
091871	0.00	0.000	0.00
120471	-0.15	0.000	0.00
110871	-0.20	0.000	0.00
	F > 0		
092972	-0.15	0.001	0.00
101571	-0.15	0.002	0.00
102271	-0.15	0.004	0.00
111471	-0.15	0.001	-0.17
111871	-0.15	0.002	-0.17
120271	-0.15	0.004	-0.17
	F < 0		
013072	-0.15	-0.001	0.00
122171	-0.15	-0.002	0.00
122371	-0.15	-0.004	0.00
011072	-0.15	-0.001	-0.17
011772	-0.15	-0.002	-0.17
012472	-0.15	-0.004	-0.17

Table 9-1: Order of data tabulation

9.1 Experimental Stanton Number Tabulation

As pointed out in Section 4.3, two different Stanton number runs were taken. Both runs are tabulated in this section under the heading Run 1 and Run 2. With the aid of the nomenclature below, the data tabulation should be self explanatory.

Special Nomenclature

Symbol	Explanation	Units
BH	= F/STNA (B_h = F/St)	-
F	= $\dot{m}''/\rho_\infty u_\infty$	-
PBAR	barometric pressure	in Hg
PL	plate number	-
RE	Re_{Δ_2} , enthalpy thickness Reynolds number (see Eq. 3-20)	-
RHUM	relative humidity	-
SBH	= F/STNO (b_h = F/St_o)	-
STN	experimental Stanton no.	-
STNA	average Stanton number (see Sec. 4.3 and Eq. 4-2)	-
STNE	Stanton number from energy integral equation	-
STNO	Stanton number for m = -.15 , F = 0 , $St_o = 0.0147\ Re_{\Delta_2}^{-0.25}$	-
TAMB	ambient temperature	°F
TBASE	casting base temperature	°F
TCOV	wind tunnel cover (top) temperature	°F

Symbol	Explanation	Units
TGAS	free stream static temperature at x = 10 inches	°F
TO	plate temperature	°F
UINF	u_∞ , free stream velocity	ft/sec
X	x-location	in

DATE = 091871 (0.00, 0.000)

RUN 1

TAMB = 83.6 TBASE = 79.4 TGAS = 74.2

TCOV = 77.7 PBAR = 29.93 RHUM = .38

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	SH	SBH	STN	F	TO	UINF	X	PL
3	10	31.53	99.1	0.00000	.00298	.00299	559	.00269	.991	0.000	0.000	.00296	0.00000	99.1	31.54	10	3
4	14	31.66	99.0	0.00000	.00275	.00276	724	.00254	.975	0.000	0.000	.00286	0.00000	99.1	31.65	14	4
5	18	31.51	99.1	0.00000	.00261	.00261	852	.00244	.969	0.000	0.000	.00262	0.00000	99.0	31.50	18	5
6	22	31.54	99.1	0.00000	.00256	.00251	1034	.00236	.967	0.000	0.000	.00254	0.00000	99.1	31.52	22	6
7	26	31.69	99.0	0.00000	.00241	.00242	1151	.00229	.966	0.000	0.000	.00240	0.00000	98.9	31.60	26	7
8	30	31.62	99.1	0.00000	.00229	.00235	1324	.00224	.965	0.000	0.000	.00233	0.00000	99.2	31.57	30	8
9	34	31.64	99.0	0.00000	.00228	.00229	1464	.00219	.966	0.000	0.000	.00227	0.00000	99.0	31.60	34	9
10	38	31.64	99.0	0.00000	.00226	.00225	1601	.00214	.966	0.000	0.000	.00224	0.00000	99.0	31.63	38	10
11	42	31.63	99.0	0.00000	.00220	.00220	1736	.00211	.967	0.000	0.000	.00217	0.00000	99.1	31.65	42	11
12	46	31.65	99.1	0.00000	.00224	.00216	1869	.00207	.968	0.000	0.000	.00221	0.00000	99.0	31.66	46	12
13	50	31.66	99.0	0.00000	.00218	.00213	1999	.00204	.969	0.000	0.000	.00217	0.00000	99.0	31.67	50	13
14	54	31.65	99.1	0.00000	.00203	.00210	2128	.00202	.970	0.000	0.000	.00209	0.00000	99.2	31.68	54	14
15	58	31.66	99.1	0.00000	.00211	.00207	2256	.00199	.970	0.000	0.000	.00209	0.00000	99.1	31.68	58	15
16	62	31.62	99.0	0.00000	.00194	.00204	2381	.00197	.971	0.000	0.000	.00197	0.00000	99.1	31.64	62	16
17	66	31.63	98.9	0.00000	.00204	.00202	2506	.00195	.972	0.000	0.000	.00206	0.00000	99.2	31.66	66	17
18	70	31.64	99.0	0.00000	.00202	.00200	2629	.00193	.973	0.000	0.000	.00201	0.00000	99.2	31.62	70	18
19	74	31.66	98.9	0.00000	.00199	.00198	2750	.00191	.974	0.000	0.000	.00198	0.00000	99.1	31.67	74	19
20	78	31.65	99.0	0.00000	.00190	.00196	2871	.00189	.975	0.000	0.000	.00196	0.00000	99.2	31.63	78	20
21	82	31.67	99.0	0.00000	.00190	.00194	2991	.00188	.976	0.000	0.000	.00189	0.00000	99.2	31.65	82	21
22	86	31.67	99.1	0.00000	.00196	.00192	3109	.00186	.976	0.000	0.000	.00195	0.00000	99.2	31.63	86	22
23	90	31.63	99.0	0.00000	.00195	.00191	3227	.00185	.977	0.000	0.000	.00193	0.00000	99.1	31.58	90	23

DATE = 120471 (-0.15, 0.000)

RUN 1

TAMB = 60.8 TBASE = 66.7 TGAS = 64.6

TCOV = 65.3 PBAR = 30.14 RHUM = .68

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	SH	SBH	STN	F	TO	UINF	X	PL
3	10	26.52	89.5	0.00000	.00316	.00316	519	.00279	1.022	0.000	0.000	.00317	0.00000	89.4	26.55	10	3
4	14	25.57	89.5	0.00000	.00288	.00295	657	.00263	.999	0.000	0.000	.00289	0.00000	89.4	25.60	14	4
5	18	24.74	89.4	0.00000	.00275	.00275	792	.00254	.992	0.000	0.000	.00275	0.00000	89.3	24.76	18	5
6	22	24.15	89.5	0.00000	.00269	.00264	920	.00246	.989	0.000	0.000	.00269	0.00000	89.5	24.19	22	6
7	26	23.70	89.5	0.00000	.00254	.00256	1041	.00239	.988	0.000	0.000	.00253	0.00000	89.5	23.72	26	7
8	30	23.24	89.6	0.00000	.00247	.00249	1157	.00234	.988	0.000	0.000	.00247	0.00000	89.5	23.26	30	8
9	34	22.93	89.5	0.00000	.00240	.00244	1269	.00231	.989	0.000	0.000	.00239	0.00000	89.4	22.96	34	9
10	38	22.46	89.6	0.00000	.00240	.00239	1377	.00227	.990	0.000	0.000	.00238	0.00000	89.7	22.48	38	10
11	42	22.12	89.4	0.00000	.00234	.00235	1483	.00225	.991	0.000	0.000	.00226	0.00000	89.5	22.16	42	11
12	46	21.83	89.5	0.00000	.00239	.00231	1585	.00222	.992	0.000	0.000	.00238	0.00000	89.5	21.85	46	12
13	50	21.54	89.6	0.00000	.00235	.00228	1686	.00220	.993	0.000	0.000	.00234	0.00000	89.5	21.55	50	13
14	54	21.29	89.6	0.00000	.00223	.00225	1783	.00218	.994	0.000	0.000	.00222	0.00000	89.5	21.33	54	14
15	58	21.05	89.6	0.00000	.00225	.00222	1879	.00216	.996	0.000	0.000	.00224	0.00000	89.6	21.11	58	15
16	62	20.85	89.5	0.00000	.00215	.00220	1974	.00214	.997	0.000	0.000	.00211	0.00000	89.5	20.88	62	16
17	66	20.66	89.6	0.00000	.00223	.00218	2066	.00213	.998	0.000	0.000	.00224	0.00000	89.3	20.69	66	17
18	70	20.49	89.6	0.00000	.00215	.00215	2157	.00211	.999	0.000	0.000	.00214	0.00000	89.4	20.53	70	18
19	74	20.36	89.4	0.00000	.00217	.00214	2247	.00209	1.000	0.000	0.000	.00217	0.00000	89.4	20.37	74	19
20	78	20.19	89.5	0.00000	.00211	.00212	2335	.00208	1.001	0.000	0.000	.00212	0.00000	89.4	20.21	78	20
21	82	20.05	89.7	0.00000	.00212	.00210	2423	.00206	1.002	0.000	0.000	.00201	0.00000	89.6	20.10	82	21
22	86	19.92	89.6	0.00000	.00211	.00208	2509	.00205	1.003	0.000	0.000	.00209	0.00000	89.6	19.94	86	22
23	90	19.75	89.6	0.00000	.00209	.00207	2591	.00204	1.004	0.000	0.000	.00205	0.00000	89.5	19.78	90	23

DATE = 110971 (-0.20, 0.000)

RUN 1

TAMB = 65.5 TBASE = 70.1 TGAS = 67.2

TCOV = 69.0 PBAR = 30.01 RHUM = .60

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	SH	SBH	STN	F	TO	UINF	X	PL
3	10	25.86	91.6	0.00000	.00317	.00320	527	.00280	1.043	0.000	0.000	.00319	0.00000	91.7	25.83	10	3
4	14	24.51	91.6	0.00000	.00293	.00293	668	.00266	1.013	0.000	0.000	.00294	0.00000	91.6	24.48	14	4
5	18	23.35	91.7	0.00000	.00280	.00277	798	.00259	1.003	0.000	0.000	.00282	0.00000	91.7	23.33	18	5
6	22	22.49	91.6	0.00000	.00273	.00268	918	.00253	.998	0.000	0.000	.00272	0.00000	91.7	22.46	22	6
7	26	21.83	91.6	0.00000	.00259	.00258	1033	.00247	.995	0.000	0.000	.00258	0.00000	91.8	21.81	26	7
8	30	21.21	91.6	0.00000	.00249	.00251	1141	.00244	.994	0.000	0.000	.00249	0.00000	91.7	21.19	30	8
9	34	20.71	91.6	0.00000	.00242	.00246	1246	.00240	.994	0.000	0.000	.00241	0.00000	91.8	20.69	34	9
10	38	20.25	91.7	0.00000	.00240	.00241	1347	.00237	.994	0.000	0.000	.00231	0.00000	91.9	20.23	38	10
11	42	19.86	91.7	0.00000	.00236	.00237	1444	.00235	.995	0.000	0.000	.00234	0.00000	91.9	19.84	42	11
12	46	19.53	91.5	0.00000	.00238	.00234	1539	.00232	.995	0.000	0.000	.00239	0.00000	91.7	19.51	46	12
13	50	19.23	91.6	0.00000	.00236	.00230	1631	.00230	.996	0.000	0.000	.00234	0.00000	91.7	19.21	50	13
14	54	18.97	91.6	0.00000	.00222	.00227	1721	.00228	.997	0.000	0.000	.00221	0.00000	91.6	18.95	54	14
15	58	18.73	91.6	0.00000	.00227	.00225	1809	.00226	.997	0.000	0.000	.00226	0.00000	91.7	18.71	58	15
16	62	18.52	91.6	0.00000	.00216	.00222	1896	.00224	.998	0.000	0.000	.00206	0.00000	91.7	18.50	62	16
17	66	18.33	91.6	0.00000	.00232	.00220	1980	.00222	.999	0.000	0.000	.00232	0.00000	91.6	18.31	66	17
18	70	18.14	91.6	0.00000	.00217	.00218	2063	.00220	1.000	0.000	0.000	.00217	0.00000	91.6	18.13	70	18
19	74	17.98	91.6	0.00000	.00221	.00216	2145	.00218	1.000	0.000	0.000	.00220	0.00000	91.6	17.96	74	19
20	78	17.80	91.5	0.00000	.00209	.00214	2225	.00217	1.001	0.000	0.000	.00214	0.00000	91.6	17.78	78	20
21	82	17.63	91.7	0.00000	.00205	.00213	2304	.00216	1.002	0.000	0.000	.00204	0.00000	91.7	17.61	82	21
22	86	17.40	91.6	0.00000	.00216	.00211	2382	.00215	1.003	0.000	0.000	.00214	0.00000	91.7	17.38	86	22
23	90	17.19	91.7	0.00000	.00215	.00209	2459	.00215	1.003	0.000	0.000	.00214	0.00000	91.7	17.17	90	23

DATE = 092971 (-0.15, 0.001)

RUN 1

TAMB = 75.5 TBASE = 76.2 TGAS = 72.8

TCOV = 75.4 PBAR = 29.79 RHUM = .47

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.81	97.5	.00099	.00273	.00272	604	.00257	.920	.367
4	14	25.80	97.6	.00101	.00245	.00250	791	.00234	.901	.406
5	18	24.97	97.4	.00100	.00232	.00235	958	.00222	.889	.428
6	22	24.38	97.5	.00100	.00228	.00224	1115	.00212	.880	.449
7	26	23.93	97.6	.00101	.00219	.00215	1264	.00201	.873	.474
8	30	23.49	97.6	.00101	.00202	.00208	1407	.00195	.867	.488
9	34	23.11	97.6	.00100	.00197	.00202	1545	.00193	.862	.500
10	38	22.74	97.7	.00101	.00200	.00197	1678	.00195	.858	.515
11	42	22.43	97.6	.00100	.00192	.00193	1807	.00192	.854	.525
12	46	22.15	97.5	.00101	.00194	.00189	1933	.00177	.850	.541
13	50	21.87	97.6	.00100	.00187	.00185	2056	.00175	.847	.546
14	54	21.65	97.7	.00101	.00177	.00182	2176	.00172	.845	.558
15	58	21.43	97.7	.00099	.00181	.00179	2293	.00171	.842	.559
16	62	21.22	97.6	.00101	.00175	.00178	2409	.00167	.840	.576
17	66	21.04	97.7	.00100	.00178	.00174	2522	.00165	.837	.581
18	70	20.90	97.6	.00100	.00172	.00171	2633	.00163	.835	.586
19	74	20.76	97.6	.00099	.00170	.00169	2743	.00162	.833	.588
20	78	20.62	97.5	.00100	.00176	.00167	2851	.00158	.832	.604
21	82	20.50	97.6	.00100	.00161	.00165	2958	.00156	.830	.608
22	86	20.32	97.6	.00100	.00162	.00164	3063	.00155	.828	.614
23	90	20.21	97.7	.00100	.00162	.00162	3167	.00154	.827	.620

RUN 2

TAMB = 64.7 TBASE = 74.1 TGAS = 72.0

TCOV = 72.8 PBAR = 29.79 RHUM = .52

SBH	STN	F	TO	UINF	X	PL
.338	.00275	.00101	95.9	26.75	10	3
.366	.00249	.00102	95.9	25.79	14	4
.380	.00233	.00101	95.9	24.97	18	5
.395	.00228	.00101	96.0	24.38	22	6
.414	.00219	.00103	96.0	23.90	26	7
.423	.00203	.00102	96.1	23.45	30	8
.431	.00197	.00102	96.0	23.06	34	9
.442	.00201	.00102	96.2	22.72	38	10
.443	.00192	.00102	95.9	22.41	42	11
.460	.00196	.00103	95.9	22.14	46	12
.463	.00196	.00102	95.9	21.90	50	13
.472	.00175	.00102	96.0	21.65	54	14
.471	.00179	.00101	96.0	21.42	58	15
.484	.00174	.00102	95.9	21.22	62	16
.487	.00178	.00102	96.0	21.04	66	17
.490	.00169	.00101	96.0	20.91	70	18
.490	.00169	.00100	95.9	20.77	74	19
.502	.00174	.00102	96.0	20.62	78	20
.504	.00160	.00101	96.0	20.51	82	21
.509	.00160	.00101	96.0	20.37	86	22
.513	.00160	.00101	96.1	20.21	90	23

DATE = 101571 (-0.15, 0.002)

RUN 1

TAMB = 71.0 TBASE = 70.7 TGAS = 67.8

TCOV = 70.4 PBAR = 29.81 RHUM = .47

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.82	91.0	.00199	.00234	.00231	701	.00212	.807	.870
4	14	25.79	91.2	.00199	.00209	.00209	917	.00195	.782	.958
5	18	25.02	91.0	.00197	.00191	.00194	1119	.00184	.763	1.024
6	22	24.40	91.2	.00198	.00189	.00183	1310	.00174	.748	1.094
7	26	23.95	91.3	.00197	.00179	.00174	1493	.00167	.736	1.144
8	30	23.47	91.1	.00196	.00166	.00167	1669	.00163	.725	1.184
9	34	23.09	91.1	.00199	.00158	.00161	1839	.00156	.716	1.245
10	38	22.71	91.2	.00195	.00163	.00156	2005	.00156	.708	1.264
11	42	22.38	91.3	.00199	.00151	.00151	2167	.00144	.701	1.328
12	46	22.12	91.0	.00200	.00150	.00147	2325	.00144	.694	1.371
13	50	21.85	91.1	.00197	.00148	.00143	2479	.00144	.688	1.384
14	54	21.59	91.2	.00199	.00135	.00140	2631	.00140	.683	1.434
15	58	21.37	91.1	.00197	.00144	.00137	2780	.00140	.678	1.447
16	62	21.17	91.1	.00199	.00133	.00135	2927	.00136	.673	1.487
17	66	20.97	91.2	.00197	.00138	.00132	3071	.00136	.669	1.499
18	70	20.83	91.2	.00197	.00135	.00130	3214	.00134	.665	1.526
19	74	20.69	91.2	.00195	.00129	.00128	3354	.00133	.661	1.539
20	78	20.56	91.2	.00196	.00137	.00126	3493	.00131	.657	1.567
21	82	20.41	91.1	.00196	.00125	.00124	3630	.00129	.654	1.591
22	86	20.29	91.2	.00197	.00126	.00122	3765	.00126	.651	1.626
23	90	20.13	91.2	.00198	.00120	.00120	3899	.00123	.648	1.660

RUN 2

TAMB = 70.4 TBASE = 71.8 TGAS = 68.3

TCOV = 69.8 PBAR = 29.81 RHUM = .50

SBH	STN	F	TO	UINF	X	PL
.702	.00229	.00202	91.1	26.83	10	3
.749	.00206	.00201	91.2	25.90	14	4
.781	.00191	.00200	91.1	25.04	18	5
.819	.00187	.00202	91.1	24.41	22	6
.841	.00175	.00201	91.2	23.97	26	7
.859	.00156	.00199	91.1	23.49	30	8
.891	.00156	.00201	91.0	23.11	34	9
.894	.00161	.00198	91.1	22.72	38	10
.931	.00146	.00202	91.0	22.39	42	11
.952	.00146	.00203	91.0	22.13	46	12
.953	.00145	.00200	91.1	21.86	50	13
.979	.00133	.00203	91.1	21.59	54	14
.981	.00137	.00200	90.9	21.38	58	15
1.001	.00127	.00201	91.0	21.18	62	16
1.003	.00134	.00199	91.1	20.99	66	17
1.014	.00127	.00199	91.0	20.84	70	18
1.017	.00126	.00198	90.9	20.70	74	19
1.030	.00130	.00198	91.0	20.57	78	20
1.040	.00120	.00198	91.1	20.42	82	21
1.059	.00120	.00200	91.0	20.30	86	22
1.075	.00113	.00202	91.0	20.14	90	23

DATE = 112271 (-0.15, 0.004)

RUN 1

TAMB = 71.2 TBASE = 73.4 TGAS = 69.2

TCOV = 71.3 PBAR = 30.06 RHUM = .53

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.72	92.3	.00396	.00164	.00165	890	.00130	.610	2.791
4	14	25.75	92.5	.00395	.00134	.00136	1159	.00119	.538	2.908
5	18	24.92	92.3	.00396	.00116	.00119	1424	.00113	.498	3.315
6	22	24.33	92.4	.00395	.00112	.00108	1680	.00109	.471	3.640
7	26	23.85	92.6	.00394	.00107	.00100	1927	.00105	.452	3.920
8	30	23.40	92.4	.00395	.00096	.00094	2169	.00101	.437	4.194
9	34	23.01	92.3	.00394	.00086	.00089	2404	.00101	.424	4.407
10	38	22.64	92.5	.00396	.00089	.00085	2634	.00096	.414	4.664
11	42	22.34	92.3	.00396	.00076	.00081	2861	.00095	.405	4.854
12	46	22.05	92.4	.00398	.00074	.00078	3084	.00093	.397	5.049
13	50	21.79	92.5	.00397	.00073	.00076	3304	.00092	.390	5.234
14	54	21.58	92.5	.00395	.00069	.00073	3520	.00092	.384	5.376
15	58	21.36	92.4	.00396	.00075	.00071	3734	.00090	.378	5.550
16	62	21.16	92.5	.00397	.00067	.00069	3945	.00088	.373	5.718
17	66	20.99	92.5	.00396	.00069	.00068	4154	.00087	.369	5.851
18	70	20.85	92.4	.00392	.00067	.00066	4361	.00090	.364	5.932
19	74	20.71	92.5	.00395	.00057	.00064	4566	.00085	.360	6.120
20	78	20.56	92.5	.00395	.00071	.00063	4769	.00085	.357	6.244
21	82	20.42	92.5	.00394	.00062	.00062	4970	.00086	.353	6.338
22	86	20.28	92.4	.00392	.00061	.00061	5169	.00086	.350	6.435
23	90	20.14	92.5	.00394	.00053	.00060	5367	.00084	.347	6.570

RUN 2

TAMB = 70.3 TBASE = 71.8 TGAS = 68.9

TCOV = 70.8 PBAR = 30.06 RHUM = .58

SBH	STN	F	TO	UINF	X	PL
1.460	.00166	.00392	91.3	26.78	10	3
1.564	.00133	.00393	91.6	25.82	14	4
1.651	.00120	.00394	91.3	24.97	18	5
1.716	.00112	.00393	91.5	24.37	22	6
1.771	.00109	.00392	91.7	23.89	26	7
1.831	.00090	.00394	91.2	23.44	30	8
1.870	.00089	.00391	91.2	23.04	34	9
1.930	.00094	.00396	91.3	22.68	38	10
1.965	.00080	.00394	91.3	22.36	42	11
2.005	.00078	.00393	91.3	22.08	46	12
2.042	.00072	.00395	91.3	21.82	50	13
2.065	.00067	.00393	91.3	21.61	54	14
2.101	.00078	.00394	91.2	21.40	58	15
2.135	.00072	.00395	91.2	21.20	62	16
2.157	.00071	.00394	91.2	21.03	66	17
2.162	.00077	.00390	91.1	20.86	70	18
2.206	.00069	.00394	91.2	20.72	74	19
2.227	.00069	.00393	91.3	20.59	78	20
2.239	.00067	.00390	91.2	20.44	82	21
2.252	.00063	.00389	91.1	20.38	86	22
2.280	.00057	.00389	91.4	20.23	90	23

DATE = 111471 (-0.15, 0.001, -0.17)

RUN 1

TAMB = 64.7 TBASE = 69.2 TGAS = 68.1

TCOV = 68.6 PBAR = 30.20 RHUM = .68

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	SH
3	10	26.59	91.6	.00091	.00278	.00276	698	.00285	.932	.330
4	14	25.64	91.5	.00086	.00253	.00254	900	.00253	.919	.339
5	18	24.84	91.6	.00083	.00238	.00240	972	.00235	.912	.346
6	22	24.25	91.5	.00081	.00236	.00239	1129	.00221	.907	.352
7	26	23.79	91.6	.00079	.00228	.00222	1276	.00211	.903	.355
8	30	23.34	91.6	.00077	.00211	.00218	1415	.00203	.901	.357
9	34	22.95	91.6	.00075	.00205	.00211	1547	.00198	.899	.356
10	38	22.58	91.6	.00075	.00207	.00206	1674	.00192	.897	.362
11	42	22.27	91.6	.00073	.00202	.00202	1796	.00188	.895	.361
12	46	21.96	91.5	.00071	.00206	.00199	1915	.00185	.894	.358
13	50	21.69	91.6	.00071	.00199	.00195	2029	.00181	.892	.363
14	54	21.44	91.6	.00071	.00186	.00193	2141	.00177	.891	.369
15	58	21.24	91.7	.00070	.00192	.00190	2250	.00174	.890	.368
16	62	21.05	91.7	.00069	.00186	.00188	2356	.00172	.889	.368
17	66	20.86	91.7	.00067	.00195	.00185	2460	.00170	.888	.367
18	70	20.70	91.7	.00066	.00184	.00182	2561	.00169	.887	.360
19	74	20.55	91.6	.00067	.00194	.00181	2661	.00165	.887	.369
20	78	20.38	91.7	.00065	.00190	.00180	2759	.00164	.886	.364
21	82	20.24	91.7	.00065	.00171	.00178	2855	.00162	.885	.365
22	86	20.14	91.7	.00065	.00175	.00176	2949	.00160	.885	.369
23	90	20.00	91.7	.00063	.00174	.00175	3042	.00160	.884	.363

RUN 2

TAMB = 65.8 TBASE = 70.0 TGAS = 69.0

TCOV = 69.1 PBAR = 30.20 RHUM = .68

S9H	STN	F	TO	UINF	X	PL
.307	.00276	.00091	92.3	26.62	10	3
.311	.00252	.00086	92.4	25.70	14	4
.315	.00236	.00083	92.3	24.86	18	5
.319	.00235	.00081	92.4	24.29	22	6
.321	.00226	.00079	92.4	23.83	26	7
.321	.00209	.00077	92.4	23.37	30	8
.320	.00203	.00075	92.4	22.98	34	9
.324	.00208	.00074	92.4	22.63	38	10
.323	.00201	.00073	92.4	22.29	42	11
.319	.00206	.00071	92.4	22.01	46	12
.324	.00199	.00071	92.5	21.73	50	13
.329	.00188	.00071	92.5	21.49	54	14
.328	.00192	.00070	92.4	21.27	58	15
.327	.00186	.00069	92.5	21.05	62	16
.326	.00193	.00069	92.5	20.86	66	17
.319	.00183	.00066	92.5	20.70	70	18
.327	.00184	.00067	92.4	20.56	74	19
.323	.00183	.00066	92.5	20.41	78	20
.323	.00171	.00065	92.3	20.29	82	21
.326	.00175	.00065	92.4	20.15	86	22
.321	.00173	.00064	92.4	20.02	90	23

DATE = 111871 (-0.15, 3.002, -0.17)

RUN 1

TAMB = 68.3 TBASE = 70.2 TGAS = 65.4

TCOV = 68.1 PBAR = 30.10 RHUM = .62

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	SH
3	10	26.53	91.5	.00182	.00232	.00232	693	.00222	.509	.785
4	14	25.61	91.6	.00171	.00210	.00211	903	.00207	.787	.813
5	18	24.72	91.4	.00168	.00196	.00199	1097	.00195	.778	.847
6	22	24.18	91.5	.00163	.00196	.00190	1278	.00188	.774	.856
7	26	23.68	91.7	.00158	.00186	.00184	1450	.00183	.772	.859
8	30	23.23	91.6	.00153	.00174	.00179	1614	.00180	.771	.859
9	34	22.82	91.4	.00152	.00172	.00175	1772	.00175	.770	.874
10	38	22.46	91.5	.00151	.00171	.00171	1925	.00172	.770	.881
11	42	22.15	91.6	.00145	.00162	.00168	2074	.00173	.770	.864
12	46	21.84	91.5	.00145	.00169	.00165	2218	.00169	.770	.882
13	50	21.58	91.6	.00142	.00162	.00162	2359	.00168	.770	.877
14	54	21.36	91.6	.00147	.00148	.00160	2497	.00160	.771	.921
15	58	21.12	91.6	.00140	.00160	.00158	2632	.00164	.771	.888
16	62	20.90	91.6	.00141	.00145	.00156	2765	.00160	.771	.908
17	66	20.73	91.7	.00136	.00158	.00155	2895	.00164	.771	.876
18	70	20.57	91.6	.00134	.00155	.00153	3023	.00163	.772	.876
19	74	20.44	91.6	.00134	.00152	.00152	3149	.00160	.772	.884
20	78	20.30	91.7	.00132	.00159	.00150	3272	.00159	.773	.882
21	82	20.15	91.7	.00131	.00145	.00149	3395	.00159	.773	.880
22	86	20.01	91.6	.00130	.00145	.00148	3515	.00158	.773	.881
23	90	19.86	91.6	.00129	.00142	.00146	3634	.00158	.774	.881

RUN 2

TAMB = 68.2 TBASE = 70.2 TGAS = 65.3

TCOV = 67.8 PBAR = 30.20 RHUM = .50

S9H	STN	F	TO	UINF	X	PL
.635	.00232	.00182	91.2	26.47	10	3
.640	.00210	.00172	91.1	25.49	14	4
.660	.00199	.00169	91.0	24.65	18	5
.663	.00196	.00163	91.1	24.09	22	6
.663	.00189	.00158	91.3	23.63	26	7
.662	.00172	.00154	91.3	23.17	30	8
.673	.00172	.00153	91.1	22.79	34	9
.679	.00175	.00150	91.1	22.44	38	10
.666	.00169	.00145	91.3	22.11	42	11
.679	.00169	.00146	91.1	21.84	46	12
.676	.00166	.00143	91.2	21.57	50	13
.709	.00154	.00148	91.2	21.33	54	14
.685	.00163	.00141	91.2	21.13	58	15
.700	.00155	.00143	91.1	20.92	62	16
.676	.00160	.00135	91.2	20.74	66	17
.676	.00155	.00134	91.2	20.58	70	18
.683	.00154	.00134	91.2	20.44	74	19
.682	.00161	.00133	91.2	20.29	78	20
.680	.00147	.00131	91.2	20.15	82	21
.681	.00146	.00130	91.2	20.00	86	22
.681	.00145	.00129	91.3	19.84	90	23

DATE = 120271 (-0.15, 0.004, -0.17)

RUN 1

TAMB = 65.5 TBASE = 68.5 TGAS = 65.6

TCOV = 66.6 PBAR = 30.10 RHUM = .70

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	SH
3	10	26.70	87.8	.00362	.00170	.00171	950	.00182	.628	2.118
4	14	25.74	88.0	.00344	.00141	.00143	1132	.00153	.565	2.408
5	18	24.90	87.8	.00332	.00134	.00132	1307	.00139	.550	2.511
6	22	24.32	88.1	.00322	.00122	.00126	1622	.00129	.543	2.560
7	26	23.85	88.2	.00313	.00127	.00121	1844	.00122	.540	2.589
8	30	23.39	87.9	.00308	.00116	.00117	2054	.00114	.538	2.631
9	34	22.99	87.8	.00301	.00113	.00115	2256	.00113	.537	2.625
10	38	22.64	87.9	.00294	.00121	.00112	2450	.00111	.536	2.628
11	42	22.31	87.9	.00293	.00100	.00110	2637	.00105	.536	2.664
12	46	22.01	87.9	.00286	.00110	.00108	2819	.00105	.536	2.654
13	50	21.74	87.9	.00285	.00106	.00107	2996	.00102	.536	2.675
14	54	21.51	87.9	.00278	.00103	.00105	3169	.00103	.536	2.646
15	58	21.31	87.9	.00277	.00109	.00104	3338	.00099	.537	2.674
16	62	21.09	88.0	.00275	.00094	.00103	3502	.00096	.537	2.691
17	66	20.92	87.9	.00271	.00111	.00101	3664	.00097	.537	2.680
18	70	20.75	87.8	.00269	.00098	.00100	3823	.00095	.537	2.677
19	74	20.61	87.8	.00263	.00094	.00100	3979	.00097	.538	2.647
20	78	20.46	87.9	.00264	.00106	.00099	4132	.00093	.538	2.676
21	82	20.33	87.8	.00263	.00099	.00098	4283	.00091	.538	2.688
22	86	20.20	87.9	.00259	.00099	.00097	4431	.00092	.539	2.674
23	90	20.02	87.9	.00257	.00093	.00096	4578	.00092	.539	2.673

RUN 2

TAMB = 64.5 TBASE = 68.2 TGAS = 65.8

TCOV = 66.5 PBAR = 30.10 RHUM = .70

S9H	STN	F	TO	UINF	X	PL
1.330	.00172	.00362	87.5	26.70	10	3
1.361	.00142	.00346	87.6	25.73	14	4
1.380	.00134	.00333	87.5	24.89	18	5
1.390	.00132	.00322	87.8	24.30	22	6
1.397	.00129	.00314	87.9	23.84	26	7
1.415	.00106	.00310	87.6	23.39	30	8
1.411	.00112	.00301	87.6	22.98	34	9
1.409	.00120	.00295	87.6	22.61	38	10
1.428	.00104	.00293	87.7	22.30	42	11
1.423	.00109	.00288	87.7	21.98	46	12
1.434	.00106	.00285	87.5	21.75	50	13
1.419	.00097	.00278	87.6	21.53	54	14
1.435	.00108	.00278	87.5	21.29	58	15
1.444	.00098	.00277	87.6	21.10	62	16
1.434	.00110	.00271	87.6	20.92	66	17
1.439	.00097	.00269	87.5	20.76	70	18
1.424	.00093	.00264	87.5	20.62	74	19
1.440	.00109	.00264	87.4	20.47	78	20
1.447	.00101	.00263	87.5	20.33	82	21
1.440	.00100	.00260	87.4	20.19	86	22
1.441	.00091	.00258	87.5	20.04	90	23

DATE = 013072 (-0.15, -0.001)

RUN 1

TAMB = 67.9 TBASE = 80.9 TGAS = 66.4

TCOV = 72.0 PBAR = 30.26 RHUM = .70

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.90	91.1	-.00099	.00348	.00349	456	.00314	1.097	-.284
4	14	25.94	91.2	-.00099	.00333	.00332	570	.00301	1.103	-.298
5	18	25.03	91.2	-.00100	.00320	.00319	675	.00295	1.107	-.323
6	22	24.38	91.2	-.00100	.00312	.00309	774	.00288	1.110	-.323
7	26	23.89	91.2	-.00099	.00299	.00302	867	.00282	1.113	-.328
8	30	23.43	91.1	-.00099	.00294	.00295	956	.00278	1.116	-.336
9	34	23.00	91.2	-.00100	.00285	.00289	1042	.00276	1.118	-.346
10	38	22.64	91.2	-.00099	.00284	.00284	1125	.00272	1.120	-.348
11	42	22.34	91.3	-.00099	.00282	.00280	1205	.00269	1.121	-.354
12	46	22.05	91.2	-.00099	.00279	.00276	1283	.00267	1.123	-.359
13	50	21.79	91.3	-.00100	.00276	.00272	1359	.00265	1.124	-.367
14	54	21.58	91.3	-.00099	.00270	.00269	1433	.00262	1.126	-.366
15	58	21.37	91.3	-.00098	.00269	.00266	1505	.00259	1.127	-.368
16	62	21.20	91.3	-.00099	.00263	.00263	1576	.00258	1.128	-.374
17	66	21.02	91.3	-.00098	.00261	.00261	1646	.00256	1.129	-.376
18	70	20.86	91.3	-.00099	.00260	.00258	1714	.00255	1.130	-.381
19	74	20.73	91.2	-.00099	.00252	.00256	1782	.00254	1.131	-.387
20	78	20.54	91.2	-.00099	.00255	.00254	1848	.00253	1.132	-.390
21	82	20.39	91.2	-.00099	.00248	.00252	1913	.00251	1.133	-.391
22	86	20.21	91.2	-.00099	.00251	.00250	1977	.00250	1.134	-.396
23	90	20.07	91.3	-.00100	.00249	.00248	2041	.00251	1.135	-.403

RUN 2

TAMB = 66.2 TBASE = 82.0 TGAS = 67.8

TCOV = 72.2 PBAR = 30.26 RHUM = .60

S9H	STN	F	TO	UINF	X	PL
-.311	.00348	-.00099	91.5	26.96	10	3
-.329	.00334	-.00099	91.6	25.97	14	4
-.347	.00319	-.00100	91.6	25.07	18	5
-.359	.00313	-.00100	91.6	24.42	22	6
-.365	.00298	-.00099	91.6	23.94	26	7
-.374	.00292	-.00099	91.5	23.45	30	8
-.386	.00284	-.00100	91.6	23.04	34	9
-.390	.00284	-.00099	91.6	22.70	38	10
-.397	.00281	-.00099	91.7	22.38	42	11
-.403	.00277	-.00099	91.7	22.08	46	12
-.413	.00275	-.00100	91.7	21.84	50	13
-.412	.00269	-.00098	91.7	21.65	54	14
-.415	.00267	-.00098	91.6	21.46	58	15
-.422	.00259	-.00098	91.8	21.26	62	16
-.425	.00262	-.00098	91.8	21.09	66	17
-.431	.00260	-.00098	91.8	20.92	70	18
-.438	.00252	-.00099	91.6	20.79	74	19
-.442	.00255	-.00099	91.6	20.59	78	20
-.443	.00251	-.00098	91.6	20.47	82	21
-.449	.00248	-.00099	91.6	20.28	86	22
-.457	.00251	-.00100	91.7	20.12	90	23

DATE 122171 (-0.15, -0.002)

RUN 1

TAMB = 63.6 TBASE = 78.7 TGAS = 63.8

TCOV = 64.7 PBAR = 29.76 RHUM = .77

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	27.10	91.3	-.00199	.00399	.00403	372	.00383	1.205	-.495
4	14	26.08	91.5	-.00198	.00386	.00383	468	.00365	1.212	-.518
5	18	25.16	91.4	-.00199	.00371	.00369	553	.00355	1.218	-.539
6	22	24.52	91.4	-.00198	.00367	.00359	630	.00346	1.224	-.551
7	26	24.01	91.4	-.00198	.00349	.00351	703	.00340	1.229	-.566
8	30	23.53	91.4	-.00200	.00342	.00344	771	.00336	1.234	-.581
9	34	23.15	91.4	-.00198	.00331	.00338	835	.00331	1.238	-.586
10	38	22.79	91.4	-.00199	.00334	.00333	897	.00328	1.242	-.598
11	42	22.47	91.3	-.00199	.00327	.00329	956	.00325	1.245	-.606
12	46	22.20	91.5	-.00198	.00327	.00325	1014	.00321	1.248	-.610
13	50	21.96	91.4	-.00198	.00323	.00322	1069	.00318	1.251	-.616
14	54	21.76	91.4	-.00199	.00310	.00318	1122	.00317	1.254	-.625
15	58	21.56	91.3	-.00199	.00320	.00316	1175	.00315	1.257	-.631
16	62	21.36	91.3	-.00199	.00302	.00313	1225	.00313	1.259	-.638
17	66	21.19	91.3	-.00199	.00314	.00310	1275	.00311	1.261	-.641
18	70	21.03	91.4	-.00199	.00310	.00308	1323	.00309	1.264	-.646
19	74	20.89	91.3	-.00199	.00300	.00306	1371	.00308	1.266	-.651
20	78	20.72	91.3	-.00197	.00305	.00304	1417	.00310	1.268	-.668
21	82	20.59	91.4	-.00199	.00299	.00302	1462	.00306	1.270	-.661
22	86	20.40	91.4	-.00199	.00303	.00300	1507	.00304	1.271	-.663
23	90	20.22	91.4	-.00199	.00298	.00298	1551	.00304	1.273	-.669

RUN 2

TAMB = 62.9 TBASE = 78.6 TGAS = 63.4

TCOV = 64.8 PBAR = 29.73 RHUM = .82

S9H	STN	F	TO	UINF	X	PL
-.596	.00401	-.00200	90.8	27.05	10	3
-.628	.00387	-.00199	91.0	26.04	14	4
-.656	.00371	-.00199	90.9	25.11	18	5
-.675	.00368	-.00198	91.0	24.46	22	6
-.695	.00348	-.00199	91.0	23.98	26	7
-.717	.00342	-.00200	90.9	23.52	30	8
-.726	.00329	-.00199	90.9	23.11	34	9
-.743	.00334	-.00200	91.0	22.77	38	10
-.755	.00331	-.00200	91.0	22.43	42	11
-.762	.00328	-.00199	91.1	22.16	46	12
-.770	.00323	-.00198	91.0	21.93	50	13
-.784	.00318	-.00199	90.9	21.72	54	14
-.793	.00322	-.00199	90.9	21.53	58	15
-.803	.00305	-.00200	90.8	21.33	62	16
-.809	.00315	-.00199	90.9	21.16	66	17
-.816	.00311	-.00199	90.9	21.01	70	18
-.824	.00302	-.00199	90.9	20.88	74	19
-.847	.00307	-.00209	90.8	20.71	78	20
-.839	.00302	-.00200	91.0	20.57	82	21
-.843	.00303	-.00199	91.0	20.39	86	22
-.852	.00302	-.00200	90.9	20.19	90	23

DATE = 122371 (-0.15, -0.004)

RUN 1

TAMB = 62.8 TBASE = 82.5 TGAS = 64.0

TCOV = 65.7 PBAR = 30.18 RHUM = .87

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.87	91.4	-.00397	.00509	.00509	260	.00499	1.391	-.777
4	14	25.91	91.4	-.00397	.00496	.00491	310	.00475	1.402	-.806
5	18	25.05	91.4	-.00396	.00480	.00479	348	.00463	1.408	-.825
6	22	24.38	91.6	-.00397	.00482	.00470	381	.00456	1.413	-.843
7	26	23.89	91.5	-.00398	.00460	.00463	409	.00450	1.417	-.857
8	30	23.42	91.5	-.00398	.00453	.00457	434	.00446	1.420	-.868
9	34	23.02	91.3	-.00398	.00448	.00452	457	.00443	1.423	-.878
10	38	22.63	91.4	-.00398	.00449	.00448	478	.00440	1.425	-.887
11	42	22.31	91.3	-.00397	.00445	.00444	498	.00438	1.427	-.894
12	46	22.02	91.5	-.00399	.00442	.00441	516	.00437	1.429	-.903
13	50	21.75	91.5	-.00399	.00450	.00438	534	.00434	1.431	-.907
14	54	21.56	91.3	-.00398	.00434	.00435	550	.00432	1.433	-.913
15	58	21.34	91.5	-.00399	.00441	.00432	566	.00432	1.434	-.920
16	62	21.15	91.3	-.00397	.00426	.00430	580	.00429	1.435	-.921
17	66	20.97	91.4	-.00399	.00431	.00428	595	.00430	1.437	-.932
18	70	20.81	91.4	-.00398	.00435	.00426	608	.00429	1.438	-.936
19	74	20.67	91.4	-.00396	.00415	.00424	622	.00426	1.439	-.935
20	78	20.49	91.5	-.00397	.00424	.00422	634	.00426	1.440	-.940
21	82	20.33	91.5	-.00399	.00418	.00420	647	.00426	1.441	-.947
22	86	20.16	91.6	-.00398	.00419	.00418	658	.00425	1.442	-.949
23	90	19.99	91.6	-.00400	.00419	.00417	670	.00426	1.443	-.957

RUN 2

TAMB = 63.1 TBASE = 83.4 TGAS = 64.1

TCOV = 66.7 PBAR = 30.18 RHUM = .87

S9H	STN	F	TO	UINF	X	PL
-1.081	.00505	-.00394	91.6	26.87	10	3
-1.130	.00493	-.00395	91.6	25.91	14	4
-1.162	.00477	-.00395	91.6	25.05	18	5
-1.192	.00479	-.00396	91.7	24.38	22	6
-1.215	.00458	-.00396	91.7	23.89	26	7
-1.233	.00454	-.00396	91.6	23.42	30	8
-1.249	.00435	-.00396	91.7	23.03	34	9
-1.265	.00444	-.00397	91.6	22.63	38	10
-1.276	.00444	-.00397	91.4	22.31	42	11
-1.291	.00439	-.00397	91.6	22.02	46	12
-1.298	.00448	-.00395	91.5	21.75	50	13
-1.308	.00432	-.00396	91.4	21.56	54	14
-1.319	.00438	-.00396	91.6	21.34	58	15
-1.322	.00418	-.00395	91.6	21.15	62	16
-1.339	.00429	-.00398	91.7	20.97	66	17
-1.346	.00432	-.00399	91.6	20.81	70	18
-1.345	.00412	-.00396	91.6	20.67	74	19
-1.354	.00424	-.00396	91.6	20.49	78	20
-1.365	.00419	-.00397	91.5	20.34	82	21
-1.368	.00417	-.00396	91.6	20.17	86	22
-1.381	.00417	-.00398	91.7	19.99	90	23

DATE = 011072 (-0.15, -0.001, -0.17)

RUN 1

TAMB = 66.1 TBASE = 80.0 TGAS = 67.8

TCOV = 68.8 PBAR = 30.33 RHUM = .78

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.83	91.5	-.00090	.00348	.00348	458	.00313	1.095	-.259
4	14	25.89	91.3	-.00085	.00326	.00327	579	.00298	1.092	-.261
5	18	25.03	91.4	-.00083	.00313	.00313	691	.00289	1.091	-.265
6	22	24.38	91.4	-.00079	.00305	.00302	796	.00281	1.090	-.264
7	26	23.89	91.4	-.00078	.00289	.00293	897	.00275	1.090	-.267
8	30	23.35	91.6	-.00076	.00283	.00286	995	.00270	1.089	-.267
9	34	22.99	91.5	-.00075	.00274	.00279	1088	.00266	1.089	-.269
10	38	22.63	91.5	-.00074	.00272	.00273	1179	.00263	1.089	-.271
11	42	22.30	91.5	-.00073	.00270	.00268	1268	.00260	1.089	-.272
12	46	22.01	91.5	-.00071	.00265	.00264	1354	.00256	1.089	-.269
13	50	21.77	91.6	-.00071	.00262	.00260	1439	.00254	1.089	-.273
14	54	21.57	91.5	-.00069	.00255	.00256	1522	.00250	1.089	-.269
15	58	21.36	91.5	-.00070	.00259	.00253	1603	.00249	1.089	-.277
16	62	21.15	91.4	-.00068	.00245	.00250	1683	.00246	1.089	-.272
17	66	21.00	91.5	-.00067	.00249	.00247	1761	.00243	1.089	-.271
18	70	20.84	91.5	-.00067	.00246	.00245	1838	.00242	1.089	-.274
19	74	20.69	91.5	-.00067	.00243	.00242	1914	.00241	1.089	-.277
20	78	20.50	91.5	-.00066	.00236	.00240	1989	.00239	1.089	-.275
21	82	20.36	91.5	-.00065	.00234	.00238	2063	.00237	1.090	-.274
22	86	20.18	91.6	-.00066	.00237	.00236	2136	.00237	1.090	-.280
23	90	20.01	91.5	-.00065	.00234	.00234	2208	.00236	1.090	-.278

RUN 2

TAMB = 65.3 TBASE = 79.4 TGAS = 64.2

TCOV = 68.7 PBAR = 30.33 RHUM = .76

SBH	STN	F	TO	UINF	X	PL
-.283	.00348	-.00090	91.8	26.84	10	3
-.295	.00327	-.00086	91.6	25.90	14	4
-.289	.00316	-.00083	91.6	25.04	18	5
-.287	.00306	-.00080	91.7	24.39	22	6
-.290	.00288	-.00078	91.7	23.89	26	7
-.290	.00283	-.00076	91.9	23.40	30	8
-.293	.00283	-.00075	91.7	23.00	34	9
-.295	.00272	-.00074	91.7	22.63	38	10
-.296	.00271	-.00073	91.7	22.31	42	11
-.293	.00265	-.00071	91.8	22.01	46	12
-.297	.00263	-.00071	91.7	21.78	50	13
-.293	.00252	-.00069	91.7	21.57	54	14
-.301	.00258	-.00070	91.7	21.37	58	15
-.296	.00247	-.00068	91.6	21.16	62	16
-.295	.00248	-.00067	91.7	21.01	66	17
-.298	.00246	-.00067	91.7	20.84	70	18
-.301	.00244	-.00067	91.6	20.69	74	19
-.300	.00234	-.00066	91.6	20.50	78	20
-.298	.00236	-.00065	91.6	20.36	82	21
-.305	.00239	-.00066	91.7	20.18	86	22
-.303	.00236	-.00065	91.6	20.02	90	23

DATE = 011772 (-0.15, -0.002, -0.17)

RUN 1

TAMB = 63.0 TBASE = 81.8 TGAS = 64.0

TCOV = 69.2 PBAR = 30.03 RHUM = .80

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.87	91.5	-.00178	.00382	.00384	388	.00371	1.158	-.464
4	14	25.95	91.5	-.00170	.00365	.00363	490	.00350	1.163	-.469
5	18	25.03	91.5	-.00165	.00350	.00349	583	.00338	1.166	-.476
6	22	24.40	91.6	-.00161	.00343	.00338	669	.00326	1.169	-.477
7	26	23.89	91.6	-.00155	.00324	.00329	751	.00315	1.171	-.471
8	30	23.41	91.5	-.00152	.00315	.00321	828	.00305	1.173	-.474
9	34	23.04	91.5	-.00149	.00310	.00315	903	.00301	1.175	-.473
10	38	22.67	91.6	-.00148	.00307	.00310	975	.00297	1.176	-.478
11	42	22.37	91.6	-.00144	.00305	.00305	1044	.00291	1.178	-.474
12	46	22.07	91.6	-.00141	.00300	.00300	1111	.00286	1.179	-.471
13	50	21.85	91.7	-.00140	.00297	.00296	1176	.00282	1.180	-.473
14	54	21.62	91.6	-.00143	.00293	.00293	1240	.00284	1.181	-.490
15	58	21.41	91.6	-.00138	.00293	.00289	1302	.00276	1.182	-.477
16	62	21.20	91.7	-.00137	.00287	.00286	1363	.00274	1.183	-.479
17	66	21.02	91.6	-.00135	.00288	.00283	1423	.00271	1.184	-.478
18	70	20.86	91.7	-.00134	.00282	.00281	1482	.00268	1.185	-.477
19	74	20.72	91.6	-.00132	.00276	.00278	1539	.00264	1.186	-.474
20	78	20.55	91.6	-.00130	.00273	.00276	1596	.00262	1.187	-.473
21	82	20.42	91.6	-.00129	.00271	.00274	1651	.00259	1.187	-.471
22	86	20.27	91.6	-.00129	.00269	.00272	1706	.00258	1.188	-.475
23	90	20.09	91.7	-.00128	.00270	.00270	1760	.00256	1.189	-.474

RUN 2

TAMB = 60.4 TBASE = 91.6 TGAS = 64.1

TCOV = 68.8 PBAR = 30.03 RHUM = .80

SBH	STN	F	TO	UINF	X	PL
-.537	.00382	-.00178	91.5	26.87	10	3
-.544	.00367	-.00170	91.6	25.95	14	4
-.555	.00350	-.00167	91.5	25.02	18	5
-.557	.00344	-.00161	91.5	24.39	22	6
-.552	.00325	-.00155	91.6	23.89	26	7
-.557	.00317	-.00153	91.5	23.41	30	8
-.556	.00312	-.00149	91.5	23.04	34	9
-.563	.00309	-.00148	91.5	22.66	38	10
-.559	.00308	-.00145	91.5	22.37	42	11
-.556	.00302	-.00142	91.6	22.07	46	12
-.558	.00300	-.00140	91.6	21.85	50	13
-.579	.00293	-.00144	91.6	21.61	54	14
-.564	.00294	-.00138	91.6	21.41	58	15
-.566	.00283	-.00137	91.6	21.20	62	16
-.566	.00287	-.00136	91.7	21.02	66	17
-.566	.00285	-.00134	91.5	20.85	70	18
-.562	.00277	-.00132	91.6	20.72	74	19
-.561	.00275	-.00131	91.6	20.55	78	20
-.559	.00272	-.00129	91.5	20.42	82	21
-.564	.00271	-.00129	91.6	20.27	86	22
-.564	.00271	-.00128	91.6	20.09	90	23

DATE = 012472 (-0.15, -0.004, -0.17)

RUN 1

TAMB = 63.9 TBASE = 84.7 TGAS = 64.0

TCOV = 70.5 PBAR = 30.13 RHUM = .70

PL	X	UINF	TO	F	STN	STNA	RE	STNE	STNA/STNO	BH
3	10	26.84	91.6	-.00356	.00469	.00473	282	.00445	1.319	-.753
4	14	25.82	91.7	-.00342	.00452	.00451	331	.00431	1.309	-.758
5	18	24.95	91.8	-.00329	.00432	.00435	378	.00415	1.303	-.759
6	22	24.31	91.8	-.00318	.00426	.00421	423	.00409	1.300	-.757
7	26	23.84	91.7	-.00311	.00403	.00410	468	.00399	1.299	-.756
8	30	23.36	91.7	-.00304	.00400	.00401	511	.00393	1.298	-.759
9	34	22.96	91.7	-.00299	.00397	.00393	554	.00388	1.297	-.762
10	38	22.60	91.7	-.00294	.00391	.00386	596	.00381	1.297	-.760
11	42	22.28	91.7	-.00291	.00391	.00380	637	.00379	1.298	-.766
12	46	21.97	91.7	-.00286	.00371	.00374	677	.00374	1.298	-.765
13	50	21.74	91.6	-.00286	.00370	.00369	717	.00368	1.298	-.761
14	54	21.52	91.7	-.00277	.00364	.00364	757	.00363	1.299	-.758
15	58	21.32	91.7	-.00276	.00364	.00360	796	.00364	1.300	-.770
16	62	21.12	91.7	-.00273	.00358	.00356	834	.00359	1.300	-.766
17	66	20.96	91.6	-.00268	.00353	.00352	872	.00355	1.301	-.761
18	70	20.80	91.7	-.00267	.00353	.00348	910	.00353	1.302	-.765
19	74	20.68	91.7	-.00263	.00336	.00345	947	.00349	1.303	-.762
20	78	20.50	91.7	-.00261	.00337	.00342	984	.00347	1.304	-.762
21	82	20.38	91.8	-.00257	.00336	.00339	1021	.00343	1.304	-.759
22	86	20.22	91.8	-.00256	.00336	.00336	1057	.00342	1.305	-.762
23	90	20.10	91.8	-.00254	.00334	.00334	1093	.00340	1.306	-.761

RUN 2

TAMB = 64.5 TBASE = 83.5 TGAS = 62.8

TCOV = 69.8 PBAR = 30.13 RHUM = .70

SBH	STN	F	TO	UINF	X	PL
-.994	.00473	-.00357	90.2	26.81	10	3
-.992	.00458	-.00342	90.3	25.80	14	4
-.988	.00435	-.00330	90.3	24.92	18	5
-.984	.00431	-.00320	90.5	24.29	22	6
-.982	.00407	-.00310	90.5	23.81	26	7
-.985	.00402	-.00305	90.2	23.33	30	8
-.988	.00390	-.00300	90.3	22.94	34	9
-.986	.00397	-.00293	90.4	22.57	38	10
-.994	.00382	-.00291	90.4	22.26	42	11
-.993	.00374	-.00286	90.3	21.94	46	12
-.988	.00373	-.00281	90.3	21.71	50	13
-.985	.00361	-.00275	90.3	21.49	54	14
-1.001	.00368	-.00278	90.3	21.30	58	15
-.996	.00352	-.00272	90.3	21.10	62	16
-.991	.00353	-.00268	90.3	20.94	66	17
-.996	.00355	-.00266	90.4	20.77	70	18
-.993	.00339	-.00263	90.3	20.66	74	19
-.993	.00345	-.00260	90.4	20.47	78	20
-.999	.00339	-.00258	90.4	20.36	82	21
-.995	.00339	-.00257	90.4	20.20	86	22
-.994	.00336	-.00254	90.4	20.09	90	23

9.2 Mean Temperature Profile Tabulation

Special Nomenclature

Symbol	Explanation	Units
BETA	β	-
CF/2	$C_f/2$	-
DEL2	Δ_2	in
DEL3	Δ_3	in
DEL4	Δ_4	in
DELH	Δ	in
DELM	δ	in
GAM	$\gamma = - K \times 10^3 \, Re_\theta/(H-1)$	-
GH	G_h	-
H	H	-
-ID	$- I_d^+$	-
K(E06)	$K \times 10^6$	-
PLATE	plate number	-
Q+	Q^+	-
REH	$Re_{\Delta 2}$	-
REM	Re_θ	-
STNA	St (see Section 9.1)	-
T	T	°F
T+	T^+	-
TAU+	τ^+	-

Symbol	Explanation	Units
T RUN	date of temperature run	-
U	u	ft/sec
U+	u^+	-
UINF	u_∞	ft/sec
V RUN	date of velocity run	-
X	x	in
Y	y	in
Y+	y^+	-

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00428 DELM = .199 REM = 170.0
V RUN = 120771-1 CF/2 = .00249 DELM = .287 REM = 515.0
PLATE = 1 UINF = 31.6 DEL2 = .0107 DEL3 = .257
X(IN) = 2.00 GM = 4.702 THETA = .0324 DEL4 = 1.228
K(E06) = .0014 GAM = .001 BETA = -.000 H = 1.563

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-11.4	0.0000	0.00	99.20
2	2.9	3.0	2.1	.0148	-9.4	.0039	4.82	94.85
3	3.7	3.7	2.6	.0186	-9.0	.0049	6.01	93.77
4	4.4	4.4	3.1	.0224	-8.3	.0059	7.16	92.27
5	5.2	5.1	3.7	.0262	-7.7	.0069	8.25	90.89
6	5.9	5.7	4.2	.0308	-7.2	.0079	9.16	89.77
7	6.7	6.3	4.7	.0338	-6.7	.0089	10.17	88.74
8	7.4	6.9	5.0	.0376	-6.3	.0099	11.20	87.85
9	8.2	7.5	5.4	.0414	-5.9	.0109	12.03	86.96
10	8.9	7.9	5.8	.0452	-5.6	.0119	12.77	86.25
11	9.7	8.4	6.1	.0490	-5.3	.0129	13.60	85.54
12	10.4	8.9	6.4	.0528	-5.0	.0139	14.41	84.92
13	11.2	9.3	6.6	.0566	-4.8	.0149	15.04	84.41
14	12.6	10.0	7.1	.0642	-4.3	.0169	16.12	83.20
15	14.1	10.5	7.5	.0717	-3.8	.0189	16.98	82.28
16	15.6	10.9	7.9	.0793	-3.5	.0209	17.61	81.44
17	17.1	11.3	8.2	.0869	-3.2	.0229	18.31	80.79
18	18.6	11.7	8.4	.0965	-2.9	.0249	18.87	80.25
19	21.6	12.2	8.8	.1097	-2.5	.0289	19.75	79.36
20	24.6	12.7	9.2	.1249	-2.2	.0329	20.49	78.61
21	28.3	13.2	9.5	.1439	-1.9	.0379	21.35	77.98
22	32.1	13.6	9.7	.1629	-1.6	.0429	21.96	77.33
23	35.8	13.9	9.9	.1819	-1.4	.0479	22.45	76.85
24	39.6	14.2	10.1	.2009	-1.3	.0529	22.92	76.49
25	47.0	14.7	10.4	.2388	-1.0	.0629	23.66	75.86
26	54.5	15.1	10.6	.2768	-.8	.0729	24.33	75.39
27	65.7	15.6	10.8	.3338	-.6	.0879	25.20	74.87
28	84.4	16.4	11.1	.4287	-.3	.1129	26.41	74.33
29	103.1	17.0	11.2	.5236	-.2	.1379	27.49	74.03
30	121.8	17.6	11.3	.6186	-.1	.1629	28.46	73.81
31	159.1	18.6	11.4	.8085	-.0	.2129	29.96	73.66
32	196.5	19.2	11.4	.9983	.0	.2629	30.97	73.59
33	233.9	19.5	11.4	1.1882	.0	.3129	31.47	73.59
34	271.3	19.6	11.4	1.3781	.0	.3629	31.60	73.59
35	285.9	19.6	11.4	1.4526	.0	.3825	31.61	73.59
36	323.3	19.6	11.4	1.6425	.0	.4325	31.61	73.59

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00299 DELM = .334 REM = 560.0
V RUN = 120771-1 CF/2 = .00222 DELM = .422 REM = 816.0
PLATE = 3 UINF = 31.6 DEL2 = .0393 DEL3 = .988
X(IN) = 10.00 GM = 5.145 THETA = .0514 DEL4 = 4.528
K(E06) = .0012 GAM = .002 BETA = -.001 H = 1.531

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.4	0.0000	0.00	99.34	1.000	1.000
2	4.0	4.1	2.6	.0064	-12.7	.0057	6.17	94.85	1.000	1.002
3	4.7	4.7	3.1	.0075	-12.1	.0067	7.17	93.85	1.000	1.002
4	5.4	5.3	3.9	.0086	-11.5	.0077	8.11	92.83	1.000	1.001
5	6.1	5.9	4.4	.0097	-11.0	.0087	8.98	92.06	1.000	1.001
6	6.8	6.5	4.8	.0108	-10.5	.0097	9.81	91.24	.999	1.000
7	7.5	7.0	5.7	.0120	-10.1	.0107	10.55	90.53	.999	1.000
8	8.2	7.4	5.7	.0131	-9.7	.0117	11.30	89.85	.999	.999
9	8.9	7.9	6.0	.0142	-9.4	.0127	11.95	89.26	.998	.998
10	9.7	8.3	6.4	.0153	-9.0	.0137	12.54	88.64	.998	.997
11	10.4	8.6	6.7	.0164	-8.7	.0147	13.09	88.14	.997	.997
12	11.1	8.9	7.0	.0175	-8.4	.0157	13.59	87.61	.997	.995
13	11.8	9.2	7.3	.0186	-8.1	.0167	14.05	87.16	.996	.994
14	12.5	9.5	7.5	.0197	-7.9	.0177	14.47	86.79	.995	.993
15	13.9	10.0	7.9	.0219	-7.4	.0197	15.28	86.07	.993	.991
16	15.3	10.5	8.3	.0242	-7.1	.0217	15.92	85.48	.991	.989
17	16.7	10.8	8.7	.0264	-6.7	.0237	16.42	84.89	.989	.987
18	19.5	11.4	9.2	.0308	-6.2	.0277	17.38	83.93	.986	.981
19	22.3	12.0	9.7	.0353	-5.7	.0317	18.27	83.13	.980	.975
20	25.8	12.6	10.1	.0408	-5.2	.0367	19.11	82.39	.974	.969
21	29.4	13.0	10.5	.0464	-4.9	.0417	19.69	81.85	.967	.962
22	32.9	13.2	10.8	.0519	-4.6	.0467	20.13	81.32	.960	.953
23	36.4	13.8	11.0	.0574	-4.4	.0517	20.51	80.96	.952	.945
24	43.4	14.0	11.5	.0685	-3.9	.0617	21.32	80.22	.936	.923
25	50.5	14.4	11.7	.0796	-3.7	.0717	21.90	79.74	.918	.903
26	57.5	14.7	12.1	.0907	-3.3	.0817	22.36	79.20	.899	.875
27	68.0	15.2	12.4	.1074	-3.0	.0967	23.07	78.63	.869	.836
28	85.6	15.8	12.9	.1351	-2.5	.1217	23.98	77.80	.812	.761
29	103.2	16.4	13.1	.1629	-2.1	.1467	24.93	77.08	.751	.681
30	120.8	17.0	13.7	.1906	-1.7	.1717	25.78	76.49	.684	.599
31	156.0	17.9	14.3	.2461	-1.1	.2217	27.26	75.49	.544	.437
32	191.2	18.6	14.7	.3015	-.7	.2717	28.59	74.77	.406	.292
33	226.3	19.6	15.0	.3570	-.4	.3217	29.72	74.26	.284	.195
34	261.5	20.1	15.2	.4125	-.2	.3717	30.56	73.92	.199	.087
35	296.7	20.5	15.3	.4680	-.1	.4217	31.17	73.74	.123	.037
36	321.9	20.7	15.4	.5235	-.0	.4717	31.42	73.62	.072	.000
37	367.0	20.7	15.4	.5789	-.0	.5217	31.51	73.62	.036	.002
38	402.2	20.7	15.4	.6344	-.0	.5717	31.52	73.62	.009	.002
39	420.9	20.7	15.4	.6639	-.0	.5983	31.52	73.62	.000	.002
40	473.7	20.7	15.4	.7471	-.0	.6733	31.50	73.62	.000	.000

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00251 DELM = .636 REM = 1930.0
V RUN = 120771-1 CF/2 = .00202 DELM = .624 REM = 1204.0
PLATE = 6 UINF = 31.6 DEL2 = .0648 DEL3 = 1.726
X(IN) = 22.00 GM = 5.353 THETA = .0758 DEL4 = 9.242
K(E06) = .0009 GAM = .002 BETA = -.001 H = 1.534

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.5	0.0000	0.00	98.99	1.000	1.000
2	3.5	3.7	2.5	.0029	-15.3	.0052	5.45	95.79	.999	1.001
3	4.2	4.2	3.0	.0035	-14.7	.0062	6.17	94.94	.999	1.001
4	4.9	4.7	3.4	.0041	-14.2	.0072	6.88	94.18	.999	1.001
5	5.5	5.2	3.9	.0046	-13.6	.0082	7.58	93.30	.999	1.001
6	6.2	5.7	4.5	.0052	-13.0	.0092	8.25	92.53	.998	1.001
7	6.9	6.2	4.9	.0058	-12.6	.0102	9.02	91.86	.998	1.001
8	7.6	6.7	5.4	.0063	-12.1	.0112	9.75	91.21	.998	1.001
9	8.2	7.2	5.8	.0069	-11.7	.0122	10.51	90.65	.998	1.001
10	8.9	7.7	6.1	.0075	-11.3	.0132	11.19	90.09	.997	1.000
11	9.6	8.2	6.5	.0080	-11.0	.0142	11.85	89.56	.997	1.000
12	10.3	8.5	6.9	.0086	-10.6	.0152	12.41	89.06	.997	1.000
13	10.9	8.9	7.1	.0092	-10.4	.0162	12.99	88.73	.997	.999
14	12.3	9.5	7.5	.0103	-9.9	.0182	13.74	88.05	.996	.999
15	13.6	10.0	8.0	.0114	-9.5	.0202	14.59	87.37	.996	.998
16	15.0	10.5	8.5	.0126	-9.0	.0222	15.25	86.72	.995	.997
17	16.3	10.9	8.8	.0137	-8.7	.0242	15.81	86.19	.994	.996
18	19.0	11.5	9.4	.0160	-8.1	.0282	16.67	85.42	.992	.994
19	21.7	11.9	9.9	.0182	-7.6	.0322	17.27	84.65	.990	.991
20	24.4	12.3	10.2	.0205	-7.3	.0362	17.69	84.20	.988	.989
21	27.1	12.7	10.5	.0228	-7.0	.0402	18.42	83.73	.986	.986
22	29.8	13.0	10.8	.0250	-6.7	.0442	18.83	83.40	.983	.984
23	32.5	13.2	11.0	.0273	-6.5	.0482	19.16	83.04	.981	.981
24	35.9	13.5	11.3	.0301	-6.2	.0532	19.57	82.66	.977	.976
25	39.2	13.7	11.5	.0329	-6.0	.0582	19.96	82.27	.974	.970
26	46.0	14.1	11.9	.0386	-5.6	.0682	20.50	81.73	.967	.961
27	52.7	14.4	12.2	.0443	-5.3	.0782	20.94	81.35	.959	.952
28	62.8	14.8	12.5	.0528	-5.0	.0932	21.59	80.84	.946	.936
29	79.7	15.5	13.1	.0669	-4.4	.1182	22.46	80.03	.922	.903
30	96.5	16.0	13.5	.0811	-4.0	.1432	23.19	79.44	.894	.871
31	113.3	16.4	13.9	.0952	-3.6	.1682	23.84	78.87	.862	.833
32	130.2	16.8	14.2	.1094	-3.2	.1932	24.48	78.33	.825	.791
33	147.0	17.3	14.5	.1235	-3.0	.2182	25.08	77.91	.790	.752
34	163.9	17.6	14.8	.1377	-2.7	.2432	25.62	77.49	.748	.708
35	180.7	18.0	15.1	.1518	-2.4	.2682	26.15	77.14	.703	.666
36	214.4	18.7	15.6	.1801	-1.9	.3182	27.19	76.42	.606	.569
37	248.1	19.4	16.0	.2084	-1.5	.3682	28.17	75.85	.504	.478
38	281.8	20.0	16.3	.2367	-1.2	.4182	29.01	75.30	.401	.378
39	315.5	20.5	16.6	.2650	-.9	.4682	29.75	74.85	.306	.287
40	349.2	20.9	16.9	.2933	-.6	.5182	30.44	74.46	.224	.200
41	382.9	21.3	17.1	.3216	-.4	.5682	30.94	74.16	.155	.129
42	450.2	21.7	17.4	.3782	-.1	.6682	31.45	73.74	.055	.022
43	517.6	21.7	17.5	.4348	-.0	.7682	31.61	73.65	.000	.000
44	585.0	21.7	17.5	.4914	-.0	.8682	31.60	73.62	.000	.000
45	652.4	21.7	17.5	.5480	-.0	.9682	31.60	73.62	.000	.000

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00229 DELM = .828 REM = 1458.0
V RUN = 120771-1 CF/2 = .00190 DELM = .785 REM = 1534.0
PLATE = 9 UINF = 31.6 DEL2 = .0916 DEL3 = 2.495
X(IN) = 34.00 GM = 5.528 THETA = .0964 DEL4 = 13.819
K(E06) = .0006 GAM = .002 BETA = -.001 H = 1.526

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-18.6	0.0000	0.00	98.96	1.000	1.000
2	4.3	4.5	3.1	.0026	-15.8	.0067	6.32	95.15	1.000	1.002
3	5.0	4.9	3.5	.0030	-15.2	.0077	6.90	94.33	1.000	1.002
4	5.7	5.4	4.0	.0034	-14.6	.0087	7.63	93.56	1.000	1.002
5	6.3	5.9	4.5	.0038	-14.1	.0097	8.36	92.86	1.000	1.002
6	7.0	6.4	4.9	.0042	-13.6	.0107	9.03	92.24	1.000	1.002
7	7.6	6.8	5.3	.0045	-13.2	.0117	9.64	91.71	1.000	1.002
8	8.3	7.2	5.8	.0049	-12.8	.0127	10.22	91.12	.999	1.002
9	8.9	7.7	6.2	.0053	-12.4	.0137	10.81	90.59	.999	1.002
10	9.6	8.1	6.5	.0057	-12.1	.0147	11.39	90.09	.999	1.001
11	10.2	8.5	6.8	.0061	-11.8	.0157	11.96	89.76	.999	1.001
12	10.9	8.9	7.1	.0065	-11.5	.0167	12.48	89.29	.999	1.001
13	12.2	9.5	7.6	.0073	-11.0	.0187	13.34	88.67	.999	1.001
14	13.5	9.9	8.0	.0081	-10.6	.0207	13.96	88.05	.998	1.000
15	14.8	10.4	8.4	.0088	-10.1	.0227	14.68	87.49	.997	1.000
16	16.1	10.8	8.8	.0096	-9.7	.0247	15.26	86.96	.996	.999
17	17.4	11.1	9.2	.0104	-9.4	.0267	15.69	86.51	.996	.998
18	20.0	11.6	9.6	.0120	-8.9	.0307	16.41	85.86	.994	.997
19	22.6	12.1	10.1	.0135	-8.5	.0347	17.06	85.21	.992	.995
20	25.3	12.5	10.5	.0151	-8.1	.0387	17.64	84.73	.991	.993
21	28.5	12.9	10.8	.0171	-7.8	.0437	18.25	84.26	.989	.990
22	31.8	13.3	11.1	.0190	-7.5	.0487	18.74	83.87	.987	.988
23	36.3	13.8	11.5	.0229	-7.0	.0587	19.43	83.25	.981	.983
24	44.9	14.1	11.9	.0269	-6.7	.0687	19.90	82.77	.976	.977
25	51.4	14.4	12.3	.0308	-6.3	.0787	20.35	82.27	.970	.969
26	61.2	14.9	12.6	.0366	-6.0	.0937	20.95	81.85	.962	.960
27	77.5	15.4	13.1	.0464	-5.4	.1187	21.70	81.11	.946	.939
28	93.9	15.9	13.6	.0562	-5.0	.1437	22.38	80.51	.928	.913
29	110.2	16.3	13.9	.0660	-4.6	.1687	23.01	80.03	.909	.898
30	126.5	16.7	14.2	.0758	-4.3	.1937	23.56	79.61	.888	.873
31	142.9	17.1	14.5	.0856	-4.0	.2187	24.05	79.20	.866	.847
32	175.6	17.7	15.1	.1052	-3.5	.2687	24.97	78.45	.817	.789
33	208.2	18.3	15.5	.1247	-3.1	.3187	25.85	77.89	.760	.733
34	240.9	18.9	16.0	.1443	-2.6	.3687	26.68	77.22	.695	.660
35	306.2	20.0	16.7	.1835	-1.9	.4687	28.16	76.26	.545	.527
36	371.6	20.9	17.3	.2226	-1.2	.5687	29.45	75.36	.384	.374
37	436.9	21.6	17.8	.2618	-.7	.6687	30.40	74.70	.231	.240
38	502.3	22.1	18.3	.3009	-.3	.7687	31.15	74.10	.118	.105
39	567.6	22.4	18.5	.3401	-.1	.8687	31.55	73.77	.046	.022
40	633.0	22.4	18.6	.3792	.0	.9687	31.69	73.66	.004	.000
41	698.3	22.4	18.6	.4184	.0	1.0687	31.61	73.65	.000	.000
42	763.7	22.4	18.6	.4576	.0	1.1687	31.61	73.65	.000	.001
43	829.0	22.4	18.6	.4967	.0	1.2687	31.61	73.65	.000	.005

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00216 DELM = 1.037 REM = 1970.0
V RUN = 120771-1 CF/2 = .00181 DELM = .959 REM = 1862.0
PLATE = 12 UINF = 31.6 DEL2 = .1175 DEL3 = 3.264
X(IN) = 46.00 GH = 5.633 THETA = .1170 DEL4 = 16.388
K(E06) = .0801 GAM = .001 BETA = -.000 H = 1.505

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-19.2	0.0000	0.00	98.89	1.000	1.000
2	2.8	3.1	2.0	.0013	-17.5	.0044	4.33	96.64	1.000	1.001
3	3.5	3.6	2.4	.0016	-17.0	.0054	4.94	96.00	1.000	1.001
4	4.1	4.1	2.9	.0019	-16.5	.0064	5.71	95.39	1.000	1.001
5	4.7	4.7	3.3	.0022	-16.0	.0074	6.41	94.65	.999	1.001
6	5.4	5.1	3.8	.0025	-15.5	.0084	7.05	93.97	.999	1.002
7	6.0	5.7	4.2	.0028	-15.0	.0094	7.78	93.36	.999	1.002
8	6.6	6.1	4.7	.0031	-14.5	.0104	8.46	92.65	.999	1.002
9	7.3	6.6	5.1	.0034	-14.1	.0114	9.03	92.15	.999	1.002
10	7.9	7.0	5.5	.0037	-13.7	.0124	9.61	91.59	.999	1.002
11	8.6	7.4	5.9	.0040	-13.4	.0134	10.19	91.18	.999	1.002
12	9.2	7.8	6.2	.0043	-13.0	.0144	10.74	90.74	.999	1.002
13	9.8	8.2	6.5	.0046	-12.7	.0154	11.22	90.30	.998	1.002
14	11.1	8.8	7.0	.0052	-12.2	.0174	12.10	89.62	.998	1.002
15	12.4	9.4	7.5	.0058	-11.7	.0194	12.87	88.97	.998	1.002
16	13.7	9.9	8.1	.0064	-11.1	.0214	13.56	88.26	.997	1.001
17	14.9	10.3	8.4	.0070	-10.8	.0234	14.14	87.79	.997	1.001
18	16.2	10.6	8.8	.0076	-10.4	.0254	14.55	87.31	.996	1.000
19	17.5	10.9	9.0	.0082	-10.2	.0274	15.01	87.02	.996	1.000
20	20.0	11.6	9.6	.0094	-9.6	.0314	15.92	86.26	.996	.999
21	22.6	12.0	10.0	.0106	-9.2	.0354	16.57	85.71	.995	.998
22	25.8	12.5	10.4	.0121	-8.8	.0404	17.15	85.21	.993	.997
23	29.0	12.8	10.7	.0136	-8.5	.0454	17.62	84.76	.991	.995
24	35.4	13.4	11.3	.0166	-7.9	.0554	18.39	84.02	.988	.991
25	41.7	13.8	11.7	.0196	-7.5	.0654	19.02	83.46	.984	.987
26	48.1	14.2	12.1	.0226	-7.1	.0754	19.54	82.98	.980	.982
27	57.7	14.6	12.5	.0271	-6.7	.0904	20.15	82.48	.974	.975
28	73.6	15.2	12.9	.0346	-6.3	.1154	20.87	81.91	.962	.965
29	89.6	15.6	13.3	.0420	-6.0	.1404	21.50	81.34	.950	.950
30	105.5	16.1	13.7	.0495	-5.5	.1654	22.11	80.81	.936	.933
31	121.5	16.5	14.0	.0570	-5.2	.1904	22.69	80.42	.920	.917
32	137.4	16.8	14.3	.0645	-4.9	.2154	23.18	80.03	.903	.897
33	169.3	17.5	14.9	.0795	-4.4	.2654	24.04	79.39	.865	.858
34	201.2	18.1	15.3	.0944	-3.9	.3154	24.84	78.75	.823	.816
35	233.1	18.6	15.7	.1094	-3.5	.3654	25.54	78.21	.775	.770
36	296.9	19.5	16.4	.1393	-2.8	.4654	26.89	77.25	.662	.669
37	360.8	20.4	17.1	.1692	-2.1	.5654	28.10	76.41	.533	.559
38	424.6	21.2	17.8	.1992	-1.6	.6654	29.15	75.66	.395	.443
39	488.4	21.9	18.1	.2291	-1.1	.7654	30.07	75.00	.265	.323
40	552.2	22.4	18.6	.2590	-.6	.8654	30.86	74.43	.151	.207
41	616.0	22.8	18.9	.2890	-.3	.9654	31.34	74.01	.069	.111
42	679.8	22.9	19.1	.3189	-.1	1.0654	31.56	73.74	.022	.042
43	743.6	23.0	19.2	.3488	.0	1.1654	31.62	73.59	.002	.000
44	807.4	23.0	19.2	.3787	.0	1.2654	31.63	73.56	.000	.000
45	871.2	23.0	19.2	.4087	.0	1.3654	31.62	73.56	.000	.000
46	935.0	23.0	19.2	.4386	.0	1.4654	31.63	73.56	.000	.000

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00207 DELM = 1.215 REM = 2272.0
V RUN = 120771-1 CF/2 = .00174 DELM = 1.136 REM = 2124.0
PLATE = 18 UINF = 31.7 DEL2 = .1427 DEL3 = 4.000
X(IN) = 58.00 GH = 5.702 THETA = .1392 DEL4 = 22.810
K(E06) = -.0003 GAM = -.002 BETA = .001 H = 1.498

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-19.7	0.0000	0.00	98.58	1.000	1.000
2	4.1	4.0	2.9	.0016	-17.0	.0066	5.46	95.15	1.000	1.001
3	4.8	4.5	3.4	.0018	-16.4	.0076	6.13	94.39	1.000	1.002
4	5.4	5.1	3.8	.0021	-15.9	.0086	6.91	93.77	1.000	1.002
5	6.0	5.6	4.3	.0023	-15.4	.0096	7.60	93.12	1.000	1.002
6	6.7	6.0	4.7	.0026	-15.0	.0106	8.18	92.62	1.000	1.002
7	7.3	6.5	5.2	.0028	-14.5	.0116	8.76	92.01	1.000	1.002
8	7.9	6.9	5.6	.0031	-14.1	.0126	9.38	91.56	1.000	1.002
9	8.5	7.4	5.8	.0033	-13.8	.0136	10.00	91.18	1.000	1.002
10	9.0	8.3	6.5	.0036	-13.1	.0156	11.26	90.27	1.000	1.002
11	11.1	9.1	7.1	.0043	-12.5	.0176	12.32	89.53	1.000	1.002
12	12.3	9.6	7.6	.0048	-12.1	.0196	12.99	88.94	.999	1.002
13	13.6	10.1	7.9	.0053	-11.7	.0216	13.66	88.52	.999	1.002
14	14.8	10.6	8.4	.0058	-11.3	.0236	14.35	87.96	.999	1.001
15	17.3	11.2	9.0	.0067	-10.6	.0276	15.14	87.10	.998	1.000
16	19.9	11.6	9.5	.0077	-10.1	.0316	15.76	86.48	.997	1.000
17	22.4	12.2	9.9	.0087	-9.7	.0356	16.46	85.95	.996	.999
18	24.9	12.6	10.3	.0097	-9.4	.0396	17.02	85.50	.996	.998
19	27.4	12.9	10.7	.0106	-8.9	.0436	17.42	84.97	.995	.996
20	29.9	13.1	10.9	.0116	-8.8	.0476	17.73	84.76	.994	.995
21	33.0	13.3	11.1	.0128	-8.6	.0526	18.04	84.47	.993	.994
22	36.2	13.6	11.3	.0141	-8.3	.0576	18.39	84.17	.991	.993
23	42.5	14.1	11.7	.0165	-8.0	.0676	19.03	83.75	.988	.990
24	51.9	14.5	12.2	.0202	-7.5	.0826	19.66	83.10	.983	.984
25	67.6	15.1	12.7	.0263	-7.0	.1076	20.45	82.45	.973	.974
26	83.3	15.6	13.2	.0324	-6.5	.1326	21.07	81.82	.962	.961
27	99.0	16.0	13.5	.0385	-6.2	.1576	21.63	81.46	.951	.952
28	114.7	16.4	13.8	.0446	-5.8	.1826	22.13	81.02	.939	.939
29	130.4	16.7	14.1	.0507	-5.6	.2076	22.58	80.72	.925	.927
30	161.8	17.3	14.6	.0629	-5.1	.2576	23.38	80.09	.896	.899
31	193.2	17.8	15.0	.0751	-4.6	.3076	24.14	79.49	.864	.867
32	224.6	18.3	15.5	.0873	-4.2	.3576	24.81	78.93	.829	.830
33	256.0	18.8	15.8	.0996	-3.9	.4076	25.45	78.51	.790	.797
34	287.4	19.3	16.1	.1118	-3.5	.4576	26.06	78.06	.748	.757
35	350.2	20.1	16.8	.1362	-2.9	.5576	27.17	77.26	.654	.675
36	413.0	20.9	17.4	.1606	-2.3	.6576	28.23	76.53	.551	.581
37	475.8	21.5	17.8	.1851	-1.8	.7576	29.14	75.90	.440	.486
38	538.6	22.1	18.3	.2095	-1.3	.8576	29.96	75.30	.327	.385
39	601.4	22.7	18.7	.2339	-.9	.9576	30.70	74.76	.223	.280
40	664.2	23.1	19.1	.2584	-.6	1.0576	31.21	74.31	.134	.181
41	727.0	23.3	19.4	.2828	-.3	1.1576	31.52	73.95	.070	.096
42	789.8	23.4	19.6	.3072	-.1	1.2576	31.68	73.71	.029	.034
43	852.6	23.5	19.7	.3316	.0	1.3576	31.73	73.59	.008	.000
44	915.4	23.5	19.7	.3961	.0	1.4576	31.73	73.56	.000	.000
45	978.3	23.4	19.7	.3805	.0	1.5576	31.72	73.56	.000	.000
46	1041.1	23.4	19.7	.4049	.0	1.6576	31.71	73.56	.001	.000
47	1071.8	23.4	19.7	.4169	.0	1.7065	31.72	73.56	.000	.000

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00200 DELM = 1.417 REM = 2648.0
V RUN = 120771-1 CF/2 = .00168 DELM = 1.276 REM = 2481.0
PLATE = 18 UINF = 31.6 DEL2 = .1665 DEL3 = 4.715
X(IN) = 70.00 GH = 5.750 THETA = .1560 DEL4 = 27.114
K(E06) = -.0009 GAM = -.005 BETA = .002 H = 1.490

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-20.0	0.0000	0.00	98.68	1.000	1.000
2	3.5	3.5	2.5	.0012	-17.8	.0057	4.61	95.94	1.000	1.001
3	4.1	4.0	2.9	.0014	-17.3	.0067	5.29	95.29	1.000	1.001
4	4.7	4.7	3.3	.0016	-16.8	.0077	6.29	94.62	1.000	1.002
5	5.3	5.4	3.8	.0018	-16.3	.0087	7.15	94.00	1.000	1.002
6	5.9	5.9	4.2	.0020	-15.8	.0097	7.84	93.44	1.000	1.002
7	6.6	6.4	4.6	.0022	-15.4	.0107	8.46	92.89	1.000	1.002
8	7.2	6.8	5.0	.0024	-15.0	.0117	9.07	92.45	1.000	1.002
9	7.8	7.3	5.3	.0026	-14.7	.0127	9.68	92.00	1.000	1.002
10	8.4	7.7	5.7	.0028	-14.3	.0137	10.26	91.56	1.000	1.002
11	9.6	8.4	6.3	.0032	-13.7	.0157	11.14	90.74	1.000	1.002
12	10.9	8.9	6.9	.0036	-13.1	.0177	11.82	89.97	1.000	1.002
13	12.1	9.4	7.5	.0041	-12.6	.0197	12.49	89.35	.999	1.002
14	13.3	9.9	7.9	.0045	-12.1	.0217	13.08	88.79	.999	1.002
15	14.6	10.3	8.2	.0049	-11.8	.0237	13.61	88.38	.998	1.002
16	15.8	10.6	8.6	.0053	-11.5	.0257	14.01	87.96	.998	1.002
17	17.0	10.8	8.8	.0057	-11.2	.0277	14.37	87.67	.997	1.002
18	19.5	11.5	9.4	.0065	-10.6	.0317	15.24	86.87	.997	1.001
19	21.9	12.0	9.8	.0074	-10.2	.0357	15.95	86.36	.996	1.000
20	25.0	12.5	10.2	.0084	-9.8	.0407	16.59	85.89	.995	.999
21	28.1	12.8	10.7	.0094	-9.4	.0457	17.00	85.33	.994	.998
22	31.2	13.1	10.9	.0105	-9.1	.0507	17.30	85.06	.993	.997
23	34.2	13.3	11.1	.0115	-8.9	.0557	17.63	84.76	.992	.996
24	40.4	13.8	11.5	.0136	-8.5	.0657	18.38	84.29	.990	.993
25	46.5	14.2	11.8	.0157	-8.2	.0757	18.88	83.84	.988	.991
26	61.9	14.7	12.5	.0208	-7.5	.1007	19.46	83.04	.981	.984
27	77.3	15.2	12.9	.0260	-7.1	.1257	20.21	82.56	.974	.978
28	108.1	16.1	13.6	.0364	-6.4	.1757	21.32	81.64	.957	.959
29	138.8	16.8	14.1	.0467	-5.9	.2257	22.21	80.99	.937	.940
30	169.6	17.3	14.6	.0571	-5.4	.2757	22.97	80.33	.916	.915
31	200.3	17.9	15.0	.0675	-5.0	.3257	23.68	79.85	.892	.894
32	231.1	18.4	15.4	.0778	-4.6	.3757	24.33	79.37	.865	.867
33	292.6	19.1	16.1	.0986	-4.0	.4757	25.37	78.57	.800	.811
34	354.1	20.0	16.7	.1193	-3.3	.5757	26.45	77.79	.727	.743
35	415.6	20.7	17.2	.1400	-2.8	.6757	27.43	77.13	.644	.674
36	477.1	21.3	17.7	.1607	-2.3	.7757	28.27	76.53	.554	.598
37	538.6	21.9	18.1	.1814	-1.9	.8757	29.07	75.96	.460	.513
38	600.1	22.5	18.6	.2022	-1.4	.9757	29.83	75.39	.364	.419
39	661.6	23.0	18.9	.2229	-1.1	1.0757	30.49	74.97	.272	.341
40	723.2	23.3	19.3	.2436	-.8	1.1757	30.94	74.55	.190	.255
41	784.7	23.6	19.6	.2643	-.4	1.2757	31.31	74.16	.125	.166
42	907.7	23.8	19.9	.3058	-.1	1.4757	31.60	73.71	.038	.045
43	1030.7	23.9	20.0	.3472	.0	1.6757	31.64	73.59	.002	.000
44	1153.7	23.8	20.0	.3887	.0	1.8757	31.60	73.59	.000	.000
45	1276.7	23.9	20.0	.4301	.0	2.0757	31.62	73.59	.000	.000

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00194 DELM = 1.598 REM = 3008.0
V RUN = 120771-1 CF/2 = .00163 DELM = 1.461 REM = 2809.0
PLATE = 21 UINF = 31.6 DEL2 = .1891 DEL3 = 5.406
X(IN) = 82.00 GH = 5.795 THETA = .1766 DEL4 = 31.331
K(E06) = -.0015 GAM = -.009 BETA = .004 H = 1.479

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-20.3	0.0000	0.00	95.72	1.000	1.000
2	4.6	4.5	3.3	.0014	-17.1	.0077	5.93	94.74	1.000	1.001
3	5.2	5.0	3.7	.0015	-16.7	.0087	6.49	94.18	1.000	1.001
4	5.9	5.4	4.2	.0017	-16.1	.0097	7.00	93.56	1.001	1.001
5	6.5	5.8	4.7	.0019	-15.7	.0107	7.61	92.95	1.001	1.001
6	7.1	6.3	5.0	.0021	-15.3	.0117	8.22	92.50	1.001	1.001
7	7.7	6.8	5.3	.0023	-15.0	.0127	8.82	92.12	1.001	1.001
8	8.9	7.6	6.0	.0026	-14.3	.0147	9.87	91.30	1.001	1.001
9	10.1	8.3	6.6	.0030	-13.7	.0167	10.77	90.53	1.001	1.001
10	11.3	8.9	7.2	.0034	-13.1	.0187	11.61	89.85	1.001	1.001
11	12.5	9.5	7.6	.0037	-12.7	.0207	12.38	89.29	1.001	1.001
12	13.7	10.0	8.0	.0041	-12.4	.0227	13.04	88.85	1.000	1.001
13	14.9	10.4	8.4	.0044	-12.0	.0247	13.64	88.38	1.000	1.001
14	17.4	11.0	8.9	.0052	-11.4	.0287	14.41	87.67	.999	1.001
15	19.8	11.6	9.5	.0059	-10.8	.0327	15.20	87.02	.999	1.001
16	22.2	12.1	9.9	.0066	-10.5	.0367	15.83	86.54	.999	1.001
17	24.6	12.5	10.1	.0073	-10.2	.0407	16.32	86.19	.998	1.001
18	27.7	12.9	10.5	.0082	-9.9	.0457	16.98	85.80	.998	1.001
19	30.7	13.3	10.8	.0091	-9.5	.0507	17.31	85.36	.997	1.001
20	33.7	13.5	11.1	.0100	-9.2	.0557	17.64	85.00	.996	1.000
21	36.8	13.7	11.3	.0110	-9.0	.0607	17.95	84.76	.995	1.000
22	42.8	14.1	11.7	.0128	-8.7	.0707	18.45	84.35	.993	1.000
23	48.9	14.4	12.1	.0146	-8.3	.0807	18.86	83.84	.992	.998
24	58.0	14.8	12.4	.0173	-8.0	.0957	19.34	83.46	.990	.996
25	73.1	15.3	12.9	.0218	-7.5	.1207	20.01	82.86	.986	.989
26	88.3	15.8	13.2	.0263	-7.1	.1457	20.57	82.44	.984	.984
27	103.4	16.1	13.5	.0308	-6.8	.1707	20.97	82.03	.980	.979
28	133.7	16.7	14.0	.0399	-6.3	.2207	21.85	81.43	.967	.970
29	164.0	17.3	14.5	.0489	-5.8	.2707	22.64	80.81	.950	.957
30	194.3	17.7	14.9	.0580	-5.5	.3207	23.12	80.36	.931	.942
31	224.6	18.2	15.3	.0670	-5.1	.3707	23.75	79.88	.913	.925
32	285.2	19.0	15.9	.0851	-4.4	.4707	24.77	79.09	.872	.885
33	345.8	19.7	16.5	.1031	-3.9	.5707	25.77	78.39	.827	.838
34	406.3	20.5	17.0	.1212	-3.3	.6707	26.70	77.73	.769	.763
35	466.9	21.1	17.5	.1393	-2.8	.7707	27.52	77.10	.693	.713
36	527.5	21.6	17.9	.1574	-2.4	.8707	28.26	76.62	.607	.649
37	588.1	22.1	18.7	.1935	-1.6	1.0707	29.62	75.60	.427	.483
38	769.9	23.5	19.4	.2297	-.9	1.2707	30.68	74.76	.253	.310
39	891.0	24.0	20.0	.2658	-.4	1.4707	31.31	74.10	.120	.145
40	1012.2	24.2	20.2	.3020	-.1	1.6707	31.55	73.74	.045	.039
41	1133.4	24.2	20.3	.3381	-.0	1.8707	31.61	73.62	.011	.000
42	1254.6	24.2	20.3	.3743	-.0	2.0707	31.61	73.62	.000	.000
43	1375.7	24.2	20.3	.4105	-.0	2.2707	31.59	73.62	.022	.000

DATE = 091871 (0.00, 0.000)

T RUN = 91871-1 STNA = .00191 DELH = 1.683 REM = 3180.0
W RUN = 120771-1 CF/2 = .00161 DELM = 1.581 REM = 2971.0
PLATE = 23 UINF = 31.5 DEL2 = .2003 DEL3 = 5.742
X(IN) = 90.00 GW = 5.749 THETA = .1871 DEL4 = 33.006
K(E06) = -.0020 GAM = -.012 BETA = .006 M = 1.470

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-20.5	0.0000	0.00	98.61
2	3.4	3.4	2.4	.0010	-19.4	.0056	4.44	96.00
3	4.0	4.0	2.8	.0011	-17.9	.0066	5.19	95.41
4	4.6	4.6	3.2	.0013	-17.4	.0076	5.92	94.82
5	5.2	5.1	3.7	.0015	-16.9	.0086	6.62	94.15
6	5.8	5.8	4.1	.0016	-16.4	.0096	7.16	93.56
7	6.4	6.2	4.6	.0018	-15.9	.0106	8.04	93.00
8	7.0	6.7	4.9	.0020	-15.6	.0116	8.71	92.57
9	7.6	7.1	5.3	.0022	-15.2	.0126	9.12	92.06
10	8.2	7.4	5.7	.0023	-14.8	.0135	9.54	91.65
11	8.8	7.7	6.0	.0025	-14.5	.0146	10.02	91.27
12	10.0	8.6	6.6	.0028	-14.0	.0166	11.07	90.56
13	11.2	9.0	7.1	.0032	-13.4	.0196	11.70	89.88
14	12.4	9.5	7.6	.0035	-12.9	.0205	12.28	89.32
15	13.6	9.9	8.1	.0039	-12.4	.0226	12.84	88.67
16	14.8	10.3	8.5	.0042	-12.1	.0246	13.32	88.23
17	17.2	11.0	9.0	.0049	-11.5	.0286	14.27	87.52
18	20.2	11.7	9.7	.0057	-10.8	.0336	15.19	86.72
19	23.2	12.4	10.2	.0066	-10.3	.0386	16.01	86.17
20	29.2	13.0	10.9	.0083	-9.6	.0486	16.77	85.27
21	35.2	13.6	11.4	.0100	-9.1	.0586	17.54	84.65
22	41.2	14.1	11.7	.0117	-8.8	.0686	18.22	84.20
23	56.2	14.7	12.4	.0159	-8.2	.0936	18.95	83.43
24	71.2	15.3	12.8	.0202	-7.7	.1186	19.79	82.92
25	86.3	15.8	13.2	.0244	-7.3	.1436	20.40	82.36
26	101.3	16.0	13.5	.0287	-7.0	.1686	20.70	82.00
27	116.3	16.3	13.9	.0330	-6.7	.1936	21.13	81.64
28	131.3	16.7	14.1	.0372	-6.4	.2186	21.54	81.25
29	161.3	17.2	14.6	.0457	-6.0	.2686	22.24	80.75
30	191.3	17.7	14.9	.0542	-5.6	.3186	22.92	80.30
31	221.4	18.2	15.3	.0627	-5.2	.3686	23.55	79.79
32	251.4	18.6	15.6	.0712	-4.9	.4186	24.01	79.40
33	281.4	19.0	15.9	.0798	-4.6	.4686	24.52	79.04
34	341.5	19.7	16.5	.0968	-4.0	.5686	25.52	78.36
35	401.5	20.3	17.0	.1138	-3.5	.6686	26.31	77.73
36	461.6	20.9	17.4	.1308	-3.1	.7686	27.02	77.19
37	521.6	21.5	17.9	.1479	-2.7	.8686	27.77	76.69
38	641.7	22.5	18.6	.1819	-1.9	1.0686	29.15	75.72
39	761.8	23.4	19.3	.2159	-1.2	1.2686	30.23	74.99
40	881.9	24.0	19.9	.2500	-.6	1.4686	31.00	74.19
41	1002.1	24.3	20.3	.2840	-.2	1.6686	31.42	73.69
42	1122.2	24.3	20.6	.3180	-.0	1.8686	31.45	73.44
43	1242.3	24.3	20.5	.3521	-.0	2.0686	31.43	73.41
44	1362.4	24.3	20.5	.3861	-.0	2.2686	31.45	73.41
45	1482.5	24.3	20.5	.4201	-.0	2.4686	31.45	73.41
46	1566.4	24.3	20.5	.4439	-.0	2.6084	31.45	73.41
47	1686.5	24.4	20.5	.4780	-.0	2.8084	31.50	73.41
48	1806.7	24.4	20.5	.5120	-.0	3.0084	31.50	73.41

DATE = 120471 (-0.13, 0.000)

T RUN = 120471-1 STNA = .00446 DELH = .144 REM = 144.0
W RUN = 71571-5 CF/2 = .00271 DELM = .309 REM = 944.0
PLATE = 1 UINF = 29.4 DEL2 = .0094 DEL3 = .245
X(IN) = 2.00 GW = 4.806 THETA = .0354 DEL4 = 1.178
K(E06) = -.4800 GAM = -.437 BETA = .146 M = 1.578

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-11.5	0.0000	0.00	89.68
2	3.1	3.5	2.2	.0169	-9.4	.0041	5.54	88.23
3	3.9	4.0	2.7	.0205	-8.9	.0051	6.29	84.07
4	4.6	4.6	3.2	.0245	-8.2	.0061	7.14	82.56
5	5.4	5.6	3.9	.0295	-7.6	.0071	8.77	81.11
6	6.1	6.1	4.4	.0324	-7.0	.0081	9.54	79.99
7	6.9	6.4	4.9	.0364	-6.5	.0091	10.07	78.92
8	7.6	6.6	5.3	.0404	-6.2	.0101	10.39	78.01
9	8.4	7.1	5.7	.0444	-5.8	.0111	11.10	77.19
10	9.1	7.5	6.1	.0484	-5.4	.0121	11.41	76.34
11	9.9	7.9	6.3	.0524	-5.1	.0131	12.38	75.72
12	10.6	8.2	6.6	.0564	-4.8	.0141	12.92	75.09
13	11.4	8.6	6.9	.0604	-4.6	.0151	13.47	74.55
14	12.2	8.9	7.1	.0644	-4.4	.0161	13.98	74.04
15	12.9	9.2	7.3	.0683	-4.1	.0171	14.45	73.56
16	14.4	9.7	7.7	.0763	-3.8	.0191	15.17	72.72
17	15.9	10.0	8.1	.0843	-3.4	.0211	15.74	71.91
18	17.4	10.4	8.4	.0923	-3.1	.0231	16.24	71.25
19	18.9	10.7	8.6	.1003	-2.9	.0251	16.76	70.83
20	21.2	11.2	9.9	.1122	-2.6	.0281	17.50	70.14
21	23.5	11.6	9.2	.1242	-2.3	.0311	18.13	69.48
22	25.7	11.9	9.4	.1362	-2.1	.0341	18.65	69.03
23	28.7	12.3	9.6	.1521	-1.8	.0381	19.21	68.49
24	32.5	12.6	9.8	.1721	-1.6	.0431	19.77	67.97
25	36.3	12.9	10.1	.1920	-1.4	.0481	20.18	67.52
26	41.6	13.2	10.3	.2199	-1.2	.0551	20.76	66.98
27	47.6	13.6	10.5	.2519	-.9	.0631	21.37	66.50
28	55.1	14.1	10.7	.2917	-.7	.0731	22.07	66.07
29	62.7	14.5	10.9	.3316	-.6	.0831	22.69	65.74
30	74.2	15.0	11.1	.3914	-.4	.0981	23.46	65.29
31	89.1	15.4	11.2	.4712	-.2	.1181	24.46	64.95
32	104.1	16.1	11.3	.5510	-.1	.1381	25.22	64.74
33	123.8	16.6	11.4	.6507	-.1	.1631	26.07	64.58
34	141.8	17.1	11.4	.7504	-.0	.1881	26.87	64.52
35	179.5	18.0	11.5	.9499	-.0	.2381	28.15	64.45
36	217.2	18.5	11.5	1.1493	-.0	.2881	28.96	64.45
37	225.1	18.5	11.5	1.1911	-.0	.2986	29.06	64.45
38	244.0	18.6	11.5	1.2908	-.0	.3236	29.21	64.45
39	262.8	18.7	11.5	1.3905	-.0	.3486	29.33	64.45
40	281.7	18.7	11.5	1.4903	-.0	.3736	29.37	64.45
41	300.5	18.8	11.5	1.5900	-.0	.3986	29.35	64.45
42	319.4	18.8	11.5	1.6897	-.0	.4236	29.40	64.45
43	338.2	18.8	11.5	1.7894	-.0	.4486	29.40	64.45

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00316 DELH = .449 REM = 511.0
W RUN = 71571-5 CF/2 = .00198 DELM = .515 REM = 985.0
PLATE = 3 UINF = 26.5 DEL2 = .0369 DEL3 = .912
X(IN) = 10.00 GW = 4.492 THETA = .0711 DEL4 = 4.099
K(E06) = -.8670 GAM = -1.374 BETA = .681 M = 1.622

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.8	0.0000	0.00	89.68	1.000	1.000
2	2.1	2.2	1.4	.0038	-12.3	.0035	2.62	87.12	1.022	1.000
3	2.6	2.8	1.9	.0048	-12.0	.0045	3.38	86.53	1.028	1.001
4	3.2	3.4	2.3	.0059	-11.6	.0055	4.11	85.82	1.045	1.001
5	3.8	4.0	2.7	.0070	-11.1	.0065	4.84	84.87	1.050	1.000
6	4.4	4.5	3.1	.0081	-10.6	.0075	5.45	83.96	1.056	1.000
7	5.0	4.9	3.6	.0091	-10.2	.0085	5.92	83.13	1.061	1.000
8	5.6	5.3	4.0	.0102	-9.8	.0095	6.37	82.41	1.067	1.000
9	6.1	5.7	4.4	.0113	-9.3	.0105	6.83	81.61	1.073	.999
10	6.7	6.0	4.8	.0123	-8.9	.0115	7.27	80.93	1.078	.999
11	7.3	6.4	5.1	.0134	-8.6	.0125	7.69	80.31	1.083	.999
12	7.9	6.7	5.4	.0145	-8.3	.0135	8.09	79.77	1.088	.999
13	9.0	7.4	6.0	.0166	-7.7	.0155	8.88	78.73	1.097	.998
14	10.2	8.0	6.5	.0188	-7.3	.0175	9.63	77.86	1.106	.998
15	11.3	8.5	6.8	.0209	-6.9	.0195	10.28	77.27	1.115	.998
16	12.5	9.0	7.2	.0231	-6.5	.0215	10.86	76.49	1.122	.996
17	14.2	9.6	7.6	.0263	-6.1	.0245	11.63	75.83	1.133	.996
18	16.0	10.2	8.0	.0295	-5.8	.0275	12.31	75.15	1.143	.995
19	18.3	10.7	8.3	.0336	-5.4	.0315	12.94	74.49	1.154	.995
20	20.6	11.1	9.7	.0380	-5.1	.0355	13.42	73.83	1.162	.992
21	23.0	11.5	9.0	.0423	-4.8	.0395	13.86	73.35	1.170	.990
22	25.3	11.8	9.1	.0466	-4.6	.0435	14.25	73.02	1.177	.989
23	27.6	12.1	9.3	.0509	-4.4	.0475	14.60	72.72	1.183	.987
24	31.7	12.5	9.7	.0584	-4.1	.0545	15.12	72.09	1.191	.979
25	36.3	12.9	10.0	.0669	-3.8	.0625	15.56	71.52	1.197	.968
26	42.1	13.3	10.2	.0777	-3.5	.0725	16.07	71.04	1.200	.956
27	50.8	13.8	10.6	.0937	-3.1	.0875	16.70	70.32	1.198	.928
28	59.5	14.3	10.9	.1098	-2.9	.1025	17.23	69.84	1.197	.900
29	71.2	14.8	11.2	.1312	-2.5	.1225	17.88	69.24	1.165	.854
30	85.7	15.5	11.6	.1580	-2.2	.1475	18.68	68.55	1.122	.787
31	100.2	16.0	11.9	.1847	-1.8	.1725	19.37	67.97	1.063	.716
32	129.2	17.2	12.4	.2383	-1.3	.2225	20.75	67.01	.921	.565
33	158.3	18.2	12.8	.2918	-.9	.2725	22.03	66.26	.758	.426
34	201.8	19.7	13.3	.3721	-.5	.3475	23.75	65.46	.531	.229
35	245.4	20.9	13.6	.4524	-.2	.4225	25.20	64.95	.377	.081
36	289.0	21.7	13.7	.5327	-.1	.4975	26.14	64.70	.292	.000
37	347.0	22.0	13.8	.6398	-.0	.5975	26.50	64.61	.025	.000
38	405.1	22.0	13.8	.7468	-.0	.6975	26.51	64.61	.000	.000
39	463.2	22.0	13.8	.8539	-.0	.7975	26.51	64.61	.000	.000

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00264 DELH = .820 REM = 909.0
W RUN = 71571-5 CF/2 = .00169 DELM = .961 REM = 1545.0
PLATE = 6 UINF = 24.1 DEL2 = .0721 DEL3 = 1.947
X(IN) = 22.00 GW = 4.452 THETA = .1225 DEL4 = 8.226
K(E06) = -.4850 GAM = -1.241 BETA = .760 M = 1.604

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.2	0.0000	0.00	89.68	1.000	1.000
2	2.4	3.1	1.7	.0025	-13.8	.0045	3.39	87.30	1.020	1.001
3	2.9	3.3	2.0	.0031	-13.5	.0055	3.93	86.80	1.024	1.000
4	3.3	3.5	2.4	.0036	-13.0	.0065	3.56	86.12	1.027	1.000
5	3.9	3.8	2.7	.0041	-12.6	.0075	3.86	85.44	1.031	1.000
6	4.3	4.2	3.1	.0046	-12.1	.0085	4.21	84.64	1.034	1.000
7	4.8	4.6	3.5	.0052	-11.7	.0095	4.64	83.94	1.038	1.000
8	5.3	5.0	3.9	.0057	-11.3	.0105	5.07	83.24	1.041	1.000
9	5.8	5.4	4.3	.0062	-10.9	.0115	5.50	82.56	1.044	1.000
10	6.3	5.8	4.6	.0068	-10.6	.0125	5.89	82.15	1.048	1.000
11	6.8	6.2	4.9	.0073	-10.3	.0135	6.24	81.58	1.051	1.000
12	7.2	6.5	5.2	.0078	-9.9	.0145	6.55	81.05	1.054	.999
13	8.2	7.1	5.9	.0089	-9.4	.0168	7.18	80.07	1.060	.999
14	9.2	7.6	6.3	.0099	-8.9	.0188	7.73	79.32	1.066	.999
15	10.2	8.1	6.7	.0110	-8.5	.0209	8.26	78.73	1.072	.998
16	11.1	8.7	7.1	.0120	-8.1	.0228	8.79	77.99	1.078	.997
17	12.1	9.1	7.3	.0131	-7.9	.0249	9.22	77.69	1.083	.997
18	13.1	9.4	7.6	.0142	-7.6	.0269	9.56	77.13	1.089	.997
19	14.6	9.9	7.9	.0157	-7.3	.0298	10.01	76.64	1.096	.996
20	16.0	10.3	8.2	.0173	-7.0	.0328	10.49	76.19	1.104	.995
21	19.0	11.0	8.6	.0205	-6.6	.0388	11.18	75.57	1.115	.995
22	19.9	11.2	9.0	.0216	-6.2	.0408	11.34	74.94	1.122	.991
23	21.9	11.5	9.2	.0237	-6.0	.0448	11.61	74.52	1.130	.989
24	24.3	11.9	9.4	.0263	-5.7	.0498	11.93	74.13	1.140	.985
25	27.7	12.2	9.9	.0300	-5.4	.0568	12.35	73.56	1.154	.984
26	31.6	12.7	10.1	.0343	-5.1	.0648	12.86	73.14	1.168	.981
27	36.5	13.1	10.3	.0395	-4.9	.0748	13.26	72.69	1.185	.977
28	43.5	13.5	10.6	.0475	-4.6	.0898	13.67	72.19	1.206	.970
29	51.2	13.9	10.9	.0554	-4.2	.1048	14.10	71.68	1.225	.959
30	60.9	14.4	11.3	.0660	-3.9	.1248	14.60	71.14	1.248	.945
31	70.7	14.8	11.5	.0766	-3.6	.1448	15.01	70.69	1.264	.930
32	82.9	15.2	11.9	.0898	-3.4	.1698	15.43	70.29	1.278	.912
33	107.3	16.0	12.2	.1162	-2.9	.2198	16.19	69.54	1.297	.869
34	131.7	16.8	12.7	.1427	-2.5	.2699	17.00	68.85	1.272	.815
35	168.3	17.9	13.2	.1823	-2.0	.3448	18.13	67.95	1.197	.719
36	217.1	19.3	13.9	.2352	-1.4	.4448	19.59	67.04	1.010	.589
37	265.9	20.6	14.3	.2881	-.9	.5448	20.94	66.23	.794	.439
38	314.6	21.9	14.6	.3410	-.6	.6445	22.18	65.62	.605	.296
39	387.8	23.2	15.0	.4203	-.2	.7948	23.57	64.95	.391	.106
40	485.4	23.8	15.2	.5261	.0	.9948	24.12	64.65	.104	.000
41	487.3	23.8	15.2	.5281	.0	.9986	24.12	64.65	.103	.000
42	536.1	23.8	15.2	.5810	.0	1.0986	24.12	64.65	.000	.001
43	584.9	23.8	15.2	.6338	.0	1.1986	24.12	64.65	.000	.001

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00244 DELH = 1.166 REH = 1276.0
V RUN = 71571-5 CF/2 = .00153 DELM = 1.175 REM = 2008.0
PLATE = 9 UINF = 22.9 DEL2 = .1268 DEL3 = 2.714
X(IN) = 34.00 GM = 4.381 THETA = .1691 DEL4 = 11.859
K(E06) = -.3480 GAM = -1.200 BETA = .721 H = 1.582

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.7	0.0000	0.00	89.72	1.000	1.000
2	2.4	3.0	1.7	.0019	-14.2	.0055	2.77	87.33	1.015	1.001
3	2.9	3.3	2.0	.0024	-13.9	.0065	2.98	86.85	1.018	1.001
4	3.3	3.6	2.3	.0026	-13.5	.0075	3.30	86.26	1.021	1.001
5	3.8	3.9	2.6	.0031	-13.0	.0085	3.62	85.52	1.023	1.001
6	4.2	4.2	3.0	.0035	-12.7	.0095	3.87	84.90	1.026	1.001
7	4.6	4.5	3.4	.0038	-12.3	.0105	4.11	84.31	1.028	1.001
8	5.1	4.8	3.7	.0042	-12.0	.0115	4.38	83.79	1.031	1.001
9	5.5	5.1	4.1	.0045	-11.6	.0125	4.66	83.22	1.033	1.001
10	6.0	5.4	4.4	.0049	-11.2	.0135	4.95	82.62	1.036	1.001
11	6.8	6.1	5.0	.0056	-10.7	.0155	5.59	81.70	1.040	1.000
12	7.7	6.8	5.4	.0063	-10.2	.0175	6.24	80.99	1.045	1.000
13	8.6	7.5	6.0	.0071	-9.7	.0195	6.84	80.19	1.049	1.000
14	9.5	8.1	6.4	.0078	-9.3	.0215	7.38	79.53	1.054	1.000
15	10.4	8.8	6.8	.0085	-9.0	.0235	7.93	79.12	1.059	1.000
16	11.7	9.1	7.0	.0096	-8.7	.0265	8.38	78.52	1.064	1.000
17	13.0	9.6	7.5	.0107	-8.2	.0295	8.82	77.75	1.070	.998
18	14.8	10.2	7.9	.0121	-7.8	.0335	9.38	77.15	1.078	.998
19	16.5	10.8	8.3	.0135	-7.4	.0375	9.88	76.46	1.086	.996
20	18.8	11.3	8.7	.0153	-7.0	.0425	10.36	75.78	1.095	.995
21	21.0	11.7	8.9	.0171	-6.7	.0475	10.72	75.42	1.103	.995
22	24.0	12.1	9.3	.0197	-6.3	.0545	11.12	74.79	1.115	.993
23	27.6	12.5	9.6	.0225	-6.0	.0625	11.48	74.25	1.128	.990
24	32.0	12.9	10.0	.0261	-5.7	.0725	11.87	73.63	1.143	.986
25	35.6	13.5	10.4	.0315	-5.3	.0875	12.36	72.06	1.165	.979
26	47.4	14.0	10.6	.0357	-5.0	.1075	12.85	72.70	1.192	.975
27	56.2	14.4	11.0	.0459	-4.7	.1275	13.22	72.16	1.216	.966
28	73.9	15.1	11.5	.0603	-4.2	.1675	13.83	71.35	1.259	.948
29	96.0	16.0	11.9	.0743	-3.7	.2175	14.63	70.60	1.305	.921
30	119.0	16.5	12.3	.0963	-3.4	.2675	15.15	70.00	1.334	.890
31	151.1	17.4	12.7	.1233	-2.9	.3425	16.00	69.30	1.356	.844
32	184.2	18.2	13.2	.1503	-2.5	.4175	16.69	68.64	1.337	.789
33	228.3	19.3	13.6	.1863	-2.0	.5175	17.67	67.89	1.278	.707
34	283.4	20.7	14.2	.2313	-1.5	.6425	18.94	66.98	1.133	.579
35	349.6	22.1	14.6	.2853	-1.0	.7925	20.30	66.26	.867	.444
36	437.8	23.9	15.2	.3573	-.5	.9925	21.97	65.39	.508	.237
37	526.1	24.8	15.6	.4293	-.1	1.1925	22.73	64.81	.235	.069
38	614.3	25.0	15.7	.5012	-.0	1.3925	22.90	64.62	.045	.000
39	702.5	25.0	15.7	.5732	-.0	1.5925	22.91	64.62	.000	.000

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00231 DELH = 1.532 REH = 1602.0
V RUN = 71571-5 CF/2 = .00145 DELM = 1.503 REM = 2460.0
PLATE = 12 UINF = 21.8 DEL2 = .1404 DEL3 = 3.631
X(IN) = 46.00 GM = 4.373 THETA = .2156 DEL4 = 15.878
K(E06) = -.2740 GAM = -1.193 BETA = .734 H = 1.585

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.1	0.0000	0.00	89.68	1.000	1.000
2	2.3	3.3	1.6	.0014	-14.7	.0056	2.52	87.44	1.020	1.000
3	2.7	3.6	1.9	.0017	-14.4	.0066	3.02	87.00	1.022	1.000
4	3.1	3.9	2.2	.0021	-14.1	.0076	3.26	86.53	1.024	1.000
5	3.5	4.2	2.5	.0022	-13.7	.0086	3.43	86.00	1.026	1.001
6	3.9	4.3	2.9	.0025	-13.3	.0096	3.66	85.35	1.028	1.001
7	4.3	4.6	3.1	.0029	-13.0	.0106	3.85	84.79	1.030	1.001
8	4.7	4.9	3.6	.0032	-12.5	.0116	4.14	84.10	1.032	1.001
9	5.1	5.2	3.9	.0033	-12.3	.0126	4.41	83.75	1.033	1.001
10	6.0	5.9	4.4	.0040	-11.7	.0146	5.04	82.83	1.037	1.001
11	6.8	6.7	4.9	.0045	-11.2	.0166	5.66	82.03	1.041	1.001
12	7.6	7.2	5.3	.0049	-10.7	.0186	6.14	81.35	1.045	1.000
13	8.4	7.7	5.8	.0056	-10.3	.0206	6.56	80.68	1.049	1.000
14	9.2	8.2	6.2	.0060	-9.9	.0226	6.94	80.01	1.052	1.000
15	10.0	8.6	6.5	.0065	-9.6	.0246	7.30	79.56	1.055	1.000
16	11.3	9.2	7.1	.0075	-9.0	.0276	7.75	78.64	1.060	.999
17	12.5	9.6	7.3	.0083	-8.7	.0306	8.17	78.22	1.065	.999
18	14.1	10.1	7.7	.0092	-8.4	.0346	8.61	77.66	1.071	.999
19	16.2	10.8	8.2	.0107	-7.8	.0396	9.17	76.82	1.079	.998
20	18.2	11.3	8.6	.0119	-7.5	.0446	9.64	76.26	1.086	.997
21	21.1	11.7	9.1	.0138	-7.0	.0515	9.97	75.54	1.096	.996
22	24.4	12.1	9.4	.0161	-6.7	.0596	10.28	75.02	1.106	.995
23	25.4	12.7	9.7	.0168	-6.4	.0696	10.76	74.61	1.120	.995
24	34.6	13.3	10.1	.0228	-6.0	.0846	11.32	73.89	1.140	.992
25	42.8	13.8	10.5	.0282	-5.6	.1046	11.76	73.27	1.165	.986
26	55.0	14.4	11.0	.0362	-5.1	.1346	12.22	72.59	1.197	.979
27	69.3	14.9	11.4	.0457	-4.6	.1696	12.68	71.83	1.231	.967
28	100.0	15.9	12.0	.0658	-4.0	.2446	13.54	70.90	1.289	.943
29	130.7	16.6	12.4	.0860	-3.7	.3196	14.15	70.39	1.324	.921
30	171.5	17.7	13.0	.1129	-3.1	.4196	15.04	69.46	1.354	.867
31	222.7	18.9	13.5	.1465	-2.6	.5446	16.06	68.61	1.349	.800
32	284.0	20.2	14.1	.1869	-2.0	.6946	17.14	67.74	1.267	.701
33	365.8	21.8	14.7	.2407	-1.4	.8946	18.54	66.80	1.059	.554
34	447.5	23.3	15.2	.2945	-.9	1.0946	19.81	65.99	.762	.390
35	529.3	24.6	15.6	.3483	-.5	1.2946	20.92	65.32	.490	.226
36	652.0	25.6	16.0	.4290	-.1	1.5946	21.74	64.89	.179	.035
37	774.6	25.7	16.1	.5097	.0	1.8946	21.92	64.57	.000	.000
38	855.2	25.7	16.1	.5627	.0	2.0916	21.92	64.57	.000	.000

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00222 DELH = 1.824 REH = 1972.0
V RUN = 71571-5 CF/2 = .00140 DELM = 1.787 REM = 2917.0
PLATE = 15 UINF = 21.1 DEL2 = .1700 DEL3 = 4.410
X(IN) = 58.00 GM = 4.364 THETA = .2559 DEL4 = 19.245
K(E06) = -.2280 GAM = -1.160 BETA = .724 H = 1.563

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.5	0.0000	0.00	89.75	1.000	1.000
2	2.1	2.2	1.5	.0013	-15.0	.0056	1.51	87.56	1.010	1.000
3	2.5	2.6	1.8	.0015	-14.7	.0065	2.12	87.12	1.012	1.000
4	2.9	3.0	2.0	.0017	-14.5	.0075	2.46	86.71	1.014	1.000
5	3.3	3.4	2.3	.0019	-14.2	.0085	2.71	86.26	1.016	1.001
6	3.7	3.8	2.6	.0021	-13.8	.0095	3.10	85.73	1.018	1.001
7	4.1	4.2	3.0	.0024	-13.5	.0105	3.41	85.20	1.021	1.001
8	4.8	5.0	3.6	.0028	-12.8	.0125	4.00	84.19	1.024	1.001
9	5.6	5.6	4.2	.0033	-12.2	.0145	4.55	83.25	1.027	1.001
10	6.4	6.2	4.8	.0037	-11.7	.0165	5.05	82.47	1.030	1.001
11	7.2	6.8	5.2	.0041	-11.3	.0185	5.51	81.82	1.034	1.001
12	8.0	7.4	5.8	.0046	-10.9	.0205	5.98	81.26	1.037	1.001
13	8.7	7.9	6.0	.0050	-10.5	.0225	6.40	80.63	1.040	1.001
14	9.9	8.5	6.5	.0057	-10.0	.0255	6.93	79.83	1.044	1.001
15	11.1	9.0	7.0	.0064	-9.5	.0285	7.28	79.09	1.044	1.001
16	12.2	9.5	7.4	.0070	-9.0	.0315	7.69	78.43	1.052	1.001
17	13.8	10.2	7.9	.0079	-8.6	.0355	8.21	77.72	1.057	1.000
18	15.3	10.7	8.1	.0088	-8.3	.0395	8.63	77.33	1.062	1.001
19	16.9	11.1	8.5	.0097	-8.0	.0435	8.98	76.76	1.068	1.000
20	19.6	11.6	8.9	.0112	-7.5	.0505	9.34	76.08	1.075	1.000
21	22.7	12.1	9.3	.0130	-7.1	.0585	9.78	75.48	1.085	.999
22	26.6	12.7	9.8	.0152	-6.6	.0695	10.27	74.70	1.096	.997
23	32.5	13.4	10.2	.0185	-6.2	.0835	10.81	74.10	1.113	.995
24	42.2	14.0	10.6	.0241	-5.9	.1085	11.33	73.60	1.137	.990
25	51.9	14.4	11.0	.0296	-5.4	.1335	11.67	72.85	1.161	.989
26	71.3	15.1	11.5	.0407	-4.9	.1835	12.22	72.10	1.199	.981
27	90.8	15.7	12.0	.0518	-4.5	.2335	12.68	71.47	1.233	.968
28	119.9	16.4	12.3	.0684	-4.1	.3085	13.27	70.67	1.277	.949
29	149.1	17.1	12.7	.0850	-3.7	.3835	13.79	70.27	1.318	.926
30	188.0	17.9	13.3	.1071	-3.2	.4835	14.47	69.49	1.354	.896
31	246.3	19.1	13.7	.1404	-2.7	.6335	15.42	68.76	1.360	.833
32	304.6	20.2	14.2	.1736	-2.2	.7835	16.15	68.01	1.320	.759
33	382.4	21.7	14.8	.2179	-1.7	.9835	17.07	67.17	1.195	.646
34	460.2	23.0	15.3	.2622	-1.2	1.1835	18.61	66.36	.981	.508
35	537.9	24.2	15.7	.3065	-.8	1.3835	19.83	65.91	.700	.385
36	635.1	25.4	16.1	.3619	-.4	1.6335	20.52	65.14	.397	.286
37	732.4	26.0	16.4	.4173	-.1	1.8835	21.03	64.72	.171	.069
38	926.8	26.1	16.5	.5280	.0	2.3835	21.10	64.57	.000	.000
39	932.1	26.1	16.5	.5311	.0	2.3973	21.12	64.57	.000	.000

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00215 DELH = 2.150 REH = 2165.0
V RUN = 71571-5 CF/2 = .00136 DELM = 2.121 REM = 3229.0
PLATE = 18 UINF = 20.5 DEL2 = .2022 DEL3 = 5.297
X(IN) = 70.00 GM = 4.376 THETA = .3015 DEL4 = 23.180
K(E06) = -.1960 GAM = -1.137 BETA = .735 H = 1.557

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.8	0.0000	0.00	89.61	1.000	1.000
2	1.5	1.5	1.0	.0008	-15.7	.0039	1.19	88.01	1.006	1.000
3	1.8	1.9	1.3	.0009	-15.5	.0049	1.49	87.71	1.008	1.000
4	2.2	2.3	1.6	.0011	-15.3	.0059	1.80	87.39	1.009	1.000
5	2.6	2.7	1.9	.0013	-15.0	.0069	2.10	87.03	1.011	1.000
6	3.0	3.1	2.1	.0015	-14.8	.0079	2.40	86.62	1.012	1.000
7	3.7	3.9	2.6	.0019	-14.1	.0099	2.98	85.67	1.017	1.000
8	4.4	4.6	3.3	.0022	-13.4	.0119	3.54	84.67	1.021	1.000
9	5.2	5.2	3.9	.0026	-12.9	.0139	4.07	83.97	1.024	1.000
10	5.9	5.9	4.4	.0030	-12.4	.0159	4.56	83.04	1.027	1.000
11	6.7	6.5	4.9	.0033	-11.9	.0179	5.00	82.33	1.030	1.000
12	7.8	7.2	5.5	.0039	-11.3	.0209	5.59	81.41	1.034	1.000
13	8.9	7.8	6.0	.0044	-10.8	.0239	6.01	80.69	1.038	1.000
14	10.0	8.4	6.5	.0050	-10.3	.0269	6.47	79.92	1.043	1.000
15	11.5	9.1	7.2	.0057	-9.6	.0309	7.07	78.94	1.048	.999
16	13.0	9.8	7.6	.0065	-9.2	.0349	7.60	78.31	1.053	.999
17	14.5	10.3	7.9	.0072	-8.9	.0389	7.96	77.54	1.058	.999
18	16.0	10.6	8.2	.0080	-8.5	.0429	8.24	77.36	1.063	.998
19	17.9	11.1	8.6	.0089	-8.1	.0479	8.57	76.76	1.068	.997
20	20.8	11.7	9.2	.0103	-7.6	.0559	9.04	75.90	1.077	.996
21	24.6	12.4	9.6	.0122	-7.2	.0659	9.56	75.33	1.089	.996
22	28.3	12.8	9.9	.0140	-6.9	.0759	9.90	74.91	1.099	.995
23	33.9	13.2	10.3	.0168	-6.5	.0909	10.25	74.31	1.113	.993
24	41.3	13.8	10.7	.0205	-6.1	.1109	10.71	73.66	1.131	.989
25	50.6	14.4	11.0	.0251	-5.7	.1359	11.10	73.18	1.154	.987
26	65.5	14.7	11.4	.0325	-5.3	.1759	11.35	72.52	1.186	.982
27	84.1	15.2	11.9	.0417	-4.9	.2259	11.77	71.96	1.227	.973
28	112.1	16.2	12.3	.0555	-4.5	.3009	12.55	71.26	1.285	.955
29	149.3	17.1	12.8	.0740	-4.0	.4009	13.21	70.57	1.346	.937
30	205.2	18.2	13.3	.1016	-3.4	.5509	14.07	69.70	1.407	.903
31	261.0	19.1	13.9	.1293	-2.9	.7009	14.75	68.92	1.424	.857
32	335.5	20.5	14.4	.1662	-2.3	.9009	15.84	68.07	1.385	.783
33	447.2	22.2	15.1	.2215	-1.7	1.2009	17.20	67.03	1.182	.652
34	559.0	23.9	15.7	.2769	-1.0	1.5009	18.52	66.17	.857	.478
35	707.9	25.7	16.3	.3506	-.4	1.9009	19.86	65.27	.346	.241
36	856.9	26.5	16.7	.4244	-.1	2.3009	20.48	64.69	.068	.046
37	1005.9	26.5	16.8	.4982	-0.0	2.7009	20.90	64.60	.000	.000
38	1154.8	26.5	16.8	.5720	-0.0	3.1009	20.90	64.60	.000	.000

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00210 DELM = 2.479 REM = 2422.0
V RUN = 71571-5 CF/2 = .00133 DELM = 2.404 REM = 3543.0
PLATE = 21 UINF = 20.1 DEL2 = .2310 DEL3 = 6.922
X(IN) = 82.00 GM = 4.314 THETA = .3378 DEL4 = 25.976
K(E06) = -.1740 GAM = -1.142 BETA = .732 M = 1.540

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.0	0.0000	0.00	89.79	1.000	1.000
2	2.2	2.4	1.6	.0010	-15.5	.0062	1.77	87.65	1.009	1.000
3	2.6	2.7	1.8	.0012	-15.3	.0072	2.08	87.30	1.010	1.000
4	3.0	3.1	2.1	.0013	-15.0	.0082	2.32	86.91	1.011	1.000
5	3.3	3.5	2.3	.0015	-14.7	.0092	2.61	86.38	1.013	1.000
6	3.7	3.8	2.6	.0017	-14.4	.0102	2.85	85.91	1.015	1.000
7	4.0	4.2	3.0	.0018	-14.0	.0112	3.15	85.41	1.017	1.000
8	4.4	4.5	3.2	.0020	-13.7	.0122	3.41	84.96	1.019	1.000
9	5.1	5.2	3.8	.0023	-13.2	.0142	3.91	84.19	1.022	1.000
10	5.9	5.8	4.3	.0026	-12.6	.0162	4.37	83.33	1.024	1.000
11	6.6	6.4	4.8	.0030	-12.2	.0182	4.79	82.66	1.027	1.000
12	7.7	7.2	5.4	.0035	-11.6	.0212	5.37	81.76	1.031	1.000
13	8.7	7.9	5.9	.0039	-11.1	.0242	5.91	81.02	1.034	1.001
14	9.8	8.5	6.4	.0044	-10.6	.0272	6.40	80.31	1.038	1.001
15	10.9	9.1	6.9	.0049	-10.1	.0302	6.81	79.59	1.042	1.001
16	12.3	9.6	7.4	.0056	-9.6	.0342	7.23	78.79	1.046	1.000
17	14.2	10.3	7.8	.0064	-9.1	.0392	7.76	78.19	1.051	1.001
18	16.0	10.8	8.2	.0072	-8.8	.0442	8.12	77.60	1.055	1.001
19	18.8	11.5	8.9	.0085	-8.1	.0522	8.66	76.67	1.062	1.001
20	22.5	12.2	9.4	.0101	-7.5	.0622	9.14	75.81	1.074	1.000
21	26.1	12.7	9.9	.0117	-7.2	.0722	9.52	75.27	1.084	.999
22	31.5	13.3	10.2	.0142	-6.8	.0872	9.99	74.70	1.099	.999
23	36.7	13.9	10.7	.0174	-6.3	.1072	10.44	73.93	1.118	.999
24	47.7	14.4	11.0	.0215	-6.0	.1322	10.81	73.51	1.140	.993
25	60.4	14.9	11.4	.0271	-5.6	.1672	11.15	72.91	1.172	.990
26	78.4	15.4	11.9	.0352	-5.1	.2172	11.55	72.19	1.217	.983
27	114.5	16.4	12.7	.0515	-4.7	.3172	12.30	71.59	1.291	.981
28	159.6	17.2	13.0	.0717	-4.0	.4422	12.93	70.51	1.352	.959
29	213.8	18.3	13.5	.0961	-3.4	.5922	13.73	69.73	1.411	.921
30	286.0	19.4	14.1	.1285	-2.8	.7922	14.59	68.93	1.457	.868
31	355.2	20.7	14.5	.1609	-2.5	.9922	15.52	68.25	1.445	.784
32	448.4	22.0	15.1	.2015	-1.9	1.2422	16.48	67.41	1.321	.681
33	592.6	23.9	15.8	.2664	-1.2	1.6422	17.97	66.39	.958	.499
34	719.2	25.5	16.3	.3232	-.7	1.9922	19.10	65.63	.550	.322
35	845.5	26.5	16.7	.3799	-.2	2.3422	19.86	64.97	.214	.135
36	985.9	26.8	16.9	.4407	-.0	2.7172	20.15	64.66	.017	.023
37	1044.1	26.8	17.0	.4691	-.0	2.8922	20.15	64.60	.001	.000
38	1125.3	26.8	17.0	.5056	.0	3.1172	20.12	64.60	.000	.000
39	1152.8	26.8	17.0	.5180	.0	3.1935	20.12	64.60	.000	.000

DATE = 120471 (-0.15, 0.000)

T RUN = 120471-1 STNA = .00207 DELM = 2.696 REM = 2578.0
V RUN = 71571-5 CF/2 = .00131 DELM = 2.570 REM = 3734.0
PLATE = 23 UINF = 19.6 DEL2 = .2497 DEL3 = 6.922
X(IN) = 90.00 GM = 4.311 THETA = .3617 DEL4 = 28.118
K(E06) = -.1700 GAM = -1.185 BETA = .765 M = 1.936

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-17.1	0.0000	0.00	89.72
2	1.8	1.9	1.3	.0006	-15.8	.0051	1.39	87.86
3	2.2	2.3	1.5	.0009	-15.6	.0061	1.66	87.50
4	2.5	2.8	1.8	.0011	-15.3	.0071	1.93	87.15
5	2.9	3.0	2.0	.0012	-15.1	.0081	2.20	86.85
6	3.2	3.4	2.3	.0014	-14.8	.0091	2.47	86.35
7	3.6	3.7	2.6	.0015	-14.5	.0101	2.73	85.88
8	3.9	4.1	2.9	.0017	-14.2	.0111	2.99	85.49
9	4.6	4.7	3.4	.0020	-13.6	.0131	3.48	84.67
10	5.3	5.4	3.9	.0023	-13.1	.0151	3.95	83.93
11	6.0	5.9	4.6	.0026	-12.5	.0171	4.35	82.98
12	6.7	6.4	4.9	.0029	-12.2	.0191	4.69	82.50
13	7.4	6.8	5.3	.0032	-11.8	.0211	5.00	81.94
14	8.2	7.2	5.8	.0035	-11.3	.0231	5.32	81.17
15	8.9	7.7	6.1	.0038	-11.0	.0251	5.62	80.72
16	9.9	8.3	6.5	.0042	-10.6	.0281	6.06	80.16
17	11.0	8.8	7.0	.0047	-10.1	.0311	6.46	79.41
18	12.4	9.4	7.4	.0053	-9.7	.0351	6.87	78.82
19	14.9	10.2	8.1	.0063	-9.0	.0421	7.49	77.81
20	17.3	11.0	8.6	.0074	-8.4	.0491	8.08	77.00
21	20.2	11.7	9.1	.0086	-8.0	.0571	8.62	76.38
22	23.7	12.4	9.6	.0100	-7.5	.0671	9.11	75.66
23	29.0	13.0	10.0	.0123	-7.0	.0821	9.57	74.97
24	36.0	13.7	10.5	.0153	-6.6	.1021	10.07	74.34
25	44.9	14.3	10.9	.0190	-6.2	.1271	10.47	73.66
26	57.2	14.8	11.4	.0243	-5.7	.1621	10.82	73.03
27	74.9	15.3	11.8	.0318	-5.3	.2121	11.26	72.40
28	101.3	16.1	12.3	.0430	-4.8	.2871	11.90	71.69
29	136.6	16.8	12.7	.0580	-4.3	.3871	12.34	70.99
30	171.9	17.5	13.1	.0730	-4.0	.4871	12.85	70.49
31	224.9	18.5	13.6	.0954	-3.5	.6371	13.57	69.79
32	277.8	19.3	13.9	.1179	-3.1	.7871	14.19	69.22
33	348.4	20.4	14.5	.1478	-2.6	.9871	15.00	68.47
34	454.3	21.8	15.1	.1928	-2.0	1.2871	16.01	67.53
35	560.2	23.3	15.6	.2377	-1.5	1.5871	17.13	66.84
36	666.0	24.7	16.1	.2827	-1.0	1.8871	18.10	66.11
37	807.2	26.2	16.6	.3426	-.5	2.2871	19.19	65.33
38	948.4	26.9	16.9	.4025	-.1	2.6871	19.73	64.82
39	1089.6	27.0	17.1	.4624	-.0	3.0871	19.84	64.60
40	1131.8	27.0	17.1	.4803	-0.0	3.2068	19.83	64.60
41	1237.7	27.0	17.1	.5253	.0	3.5068	19.81	64.60
42	1343.6	27.0	17.1	.5702	.0	3.8068	19.80	64.60

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00446 DELM = .148 REM = 149.0
V RUN = 110971-1 CF/2 = .00269 DELM = .306 REM = 540.0
PLATE = 1 UINF = 29.4 DEL2 = .0098 DEL3 = .262
X(IN) = 2.00 GM = 4.738 THETA = .0356 DEL4 = 1.195
K(E06) = -.6990 GAM = -.647 BETA = .222 M = 1.584

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-11.4	0.0000	0.00	91.79
2	2.9	3.6	2.1	.0154	-9.5	.0039	5.65	87.65
3	3.7	4.0	2.6	.0192	-8.9	.0049	6.24	86.41
4	4.4	4.5	3.1	.0231	-8.2	.0059	7.07	84.96
5	5.1	5.1	3.7	.0270	-7.7	.0069	7.96	83.75
6	5.9	5.6	4.2	.0309	-7.1	.0079	8.74	82.56
7	6.6	6.1	4.6	.0348	-6.7	.0089	9.53	81.67
8	7.4	6.7	5.1	.0387	-6.3	.0099	10.39	80.63
9	8.1	7.2	5.5	.0425	-5.9	.0109	11.18	79.93
10	8.9	7.5	5.8	.0464	-5.5	.0119	11.78	79.05
11	9.6	7.9	6.1	.0503	-5.3	.0129	12.35	78.42
12	10.3	8.3	6.4	.0542	-5.0	.0139	13.03	77.80
13	11.1	8.6	6.7	.0581	-4.7	.0149	13.66	77.17
14	11.8	9.1	6.9	.0619	-4.5	.0159	14.14	76.77
15	13.3	9.6	7.3	.0697	-4.0	.0179	14.92	75.77
16	14.8	10.0	7.6	.0775	-3.8	.0199	15.58	75.17
17	16.3	10.4	8.0	.0852	-3.4	.0219	16.19	74.39
18	17.8	10.7	8.3	.0930	-3.1	.0239	16.64	73.67
19	19.3	10.9	8.5	.1008	-2.9	.0259	16.98	73.26
20	20.7	11.2	8.7	.1085	-2.7	.0279	17.43	72.81
21	23.7	11.7	9.0	.1241	-2.3	.0319	18.25	72.06
22	27.4	12.2	9.4	.1435	-2.0	.0369	18.96	71.28
23	31.1	12.6	9.6	.1629	-1.7	.0419	19.60	70.73
24	34.8	12.9	9.9	.1822	-1.5	.0469	20.11	70.25
25	38.6	13.1	10.0	.2017	-1.3	.0519	20.49	69.83
26	46.0	13.6	10.3	.2405	-1.1	.0619	21.17	69.23
27	53.4	14.0	10.6	.2792	-.9	.0719	21.87	68.72
28	72.0	14.9	10.9	.3764	-.6	.0969	23.26	67.90
29	90.5	15.6	11.1	.4734	-.2	.1219	24.42	67.45
30	109.1	16.3	11.2	.5705	-.1	.1469	25.44	67.20
31	127.7	16.9	11.3	.6675	-.1	.1719	26.31	67.05
32	146.2	17.4	11.3	.7646	-.0	.1969	27.17	66.98
33	164.8	17.8	11.4	.8616	-.0	.2219	27.79	66.95
34	201.9	18.4	11.4	1.0557	-.0	.2719	28.76	66.95
35	239.0	18.7	11.4	1.2498	-.0	.3219	29.22	66.95
36	265.6	18.8	11.4	1.3883	-.0	.3576	29.35	66.95
37	302.7	18.8	11.4	1.5824	-.0	.4076	29.40	66.95
38	339.8	18.8	11.4	1.7765	-.0	.4576	29.40	66.95

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00320 DELM = .474 REM = 526.0
V RUN = 110971-1 CF/2 = .00174 DELM = .537 REM = 1018.0
PLATE = 3 UINF = 25.9 DEL2 = .0364 DEL3 = .909
X(IN) = 10.00 GM = 4.096 THETA = .0762 DEL4 = 3.722
K(E06) = -1.2700 GAM = -2.008 BETA = 1.177 M = 1.644

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-12.7	0.0000	0.00	91.75	1.000	1.000
2	3.0	3.4	2.1	.0061	-10.8	.0057	3.76	88.06	1.064	1.001
3	3.5	3.8	2.5	.0072	-10.4	.0067	4.25	87.27	1.074	1.001
4	4.0	4.3	2.9	.0082	-9.9	.0077	4.72	86.32	1.085	1.001
5	4.6	4.7	3.2	.0093	-9.5	.0087	5.22	85.46	1.095	1.001
6	5.1	5.2	3.6	.0104	-9.1	.0097	5.74	84.67	1.105	1.001
7	5.6	5.6	4.0	.0115	-8.8	.0107	6.21	84.01	1.115	1.001
8	6.2	6.0	4.3	.0126	-8.4	.0117	6.63	83.16	1.125	1.001
9	6.7	6.4	4.6	.0136	-8.1	.0127	7.05	82.66	1.134	1.001
10	7.2	6.8	5.0	.0147	-7.8	.0137	7.49	82.09	1.143	1.001
11	8.3	7.5	5.4	.0169	-7.4	.0157	8.28	81.28	1.160	1.001
12	9.3	8.1	5.8	.0190	-6.9	.0177	8.92	80.45	1.175	1.001
13	10.4	8.5	6.2	.0212	-6.6	.0197	9.45	79.74	1.190	1.001
14	11.4	9.0	6.5	.0233	-6.2	.0217	9.96	79.05	1.204	1.000
15	12.5	9.5	6.8	.0255	-6.0	.0237	10.53	78.58	1.219	1.000
16	13.5	10.0	7.0	.0276	-5.8	.0257	11.00	78.16	1.230	1.000
17	14.6	10.2	7.2	.0298	-5.5	.0277	11.30	77.66	1.242	.998
18	16.7	10.8	7.6	.0341	-5.2	.0317	11.94	77.00	1.264	.998
19	19.1	11.4	7.9	.0394	-4.8	.0367	12.61	76.25	1.289	.995
20	21.9	11.8	8.2	.0448	-4.5	.0417	13.06	75.68	1.310	.993
21	24.6	12.2	8.5	.0502	-4.3	.0467	13.51	75.23	1.329	.991
22	27.2	12.6	8.7	.0556	-4.0	.0517	13.88	74.82	1.346	.988
23	32.5	13.1	9.0	.0663	-3.7	.0617	14.52	74.16	1.375	.980
24	37.7	13.6	9.3	.0771	-3.4	.0717	14.99	73.62	1.396	.969
25	43.0	13.9	9.5	.0878	-3.2	.0817	15.39	73.14	1.412	.955
26	56.1	14.7	10.0	.1147	-2.7	.1067	16.27	72.24	1.429	.913
27	69.3	15.4	10.4	.1416	-2.4	.1317	17.07	71.52	1.422	.861
28	82.5	16.1	10.7	.1685	-2.0	.1567	17.76	70.89	1.394	.802
29	95.6	16.8	11.0	.1953	-1.8	.1817	18.45	70.38	1.355	.741
30	121.9	18.0	11.4	.2491	-1.3	.2317	19.88	69.47	1.224	.608
31	148.2	19.2	11.8	.3029	-.9	.2817	21.21	68.72	1.077	.488
32	174.6	20.2	12.1	.3566	-.6	.3317	22.37	68.15	.923	.340
33	200.9	21.2	12.3	.4104	-.4	.3817	23.46	67.69	.801	.220
34	227.2	22.1	12.5	.4641	-.2	.4317	24.39	67.36	.707	.123
35	253.5	22.7	12.6	.5179	-.1	.4817	25.14	67.11	.624	.062
36	279.9	23.2	12.7	.5717	-.0	.5317	25.62	66.99	.523	.026
37	306.1	23.4	12.7	.6254	-.0	.5817	25.84	66.93	.371	.000
38	332.4	23.4	12.7	.6792	.0	.6317	25.91	66.90	.195	.000
39	358.7	23.4	12.7	.7329	.0	.6817	25.92	66.90	.039	.000
40	367.1	23.4	12.7	.7500	.0	.6976	25.92	66.90	.000	.000
41	419.7	23.4	12.7	.8575	.0	.7976	25.92	66.90	.000	.000

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00266 DELM = .979 REM = 923.0
V RUN = 110971-1 CF/2 = .00129 DELM = .954 REM = 1718.0
PLATE = 6 UINF = 22.5 DEL2 = .0765 DEL3 = 1.874
X(IN) = 22.00 GM = 3.812 THETA = .1460 DEL4 = 7.143
K(E06)= -.7020 GAM = -1.732 BETA = 1.481 H = 1.696

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.2	0.0000	0.00	91.72	1.000	1.000
2	2.1	2.2	1.5	.0028	-11.9	.0054	1.84	89.21	1.034	1.000
3	2.5	2.6	1.8	.0033	-11.6	.0064	2.18	88.71	1.040	1.000
4	2.9	3.0	2.1	.0039	-11.2	.0074	2.52	87.98	1.047	1.000
5	3.3	3.5	2.3	.0044	-10.9	.0084	2.85	87.42	1.053	1.000
6	3.7	3.8	2.6	.0049	-10.6	.0094	3.19	86.82	1.060	1.000
7	4.1	4.2	2.9	.0054	-10.3	.0104	3.50	86.29	1.066	1.001
8	4.5	4.6	3.2	.0060	-10.0	.0114	3.81	85.76	1.071	1.001
9	4.9	5.0	3.5	.0065	-9.6	.0124	4.11	85.08	1.077	1.001
10	5.3	5.3	3.7	.0070	-9.3	.0134	4.39	84.52	1.082	1.001
11	5.7	5.6	4.1	.0075	-9.1	.0144	4.66	84.13	1.088	1.001
12	6.1	6.0	4.3	.0080	-8.9	.0154	4.93	83.69	1.093	1.001
13	6.5	6.3	4.5	.0086	-8.6	.0164	5.20	83.21	1.099	1.001
14	7.3	6.9	5.0	.0096	-8.2	.0184	5.74	82.38	1.109	1.001
15	8.0	7.6	5.4	.0106	-7.8	.0204	6.25	81.67	1.120	1.000
16	8.8	8.1	5.7	.0117	-7.5	.0224	6.69	81.14	1.130	1.000
17	9.6	8.5	6.0	.0127	-7.2	.0244	7.04	80.54	1.140	1.000
18	11.2	9.2	6.4	.0148	-6.8	.0284	7.64	79.71	1.159	1.000
19	12.0	9.6	6.6	.0159	-6.6	.0304	7.92	79.32	1.168	1.000
20	13.6	10.3	7.0	.0180	-6.2	.0344	8.49	78.58	1.186	.999
21	15.1	10.8	7.3	.0200	-5.9	.0384	8.95	78.01	1.204	.999
22	17.1	11.3	7.6	.0226	-5.6	.0434	9.31	77.45	1.223	.998
23	21.0	11.9	8.1	.0279	-5.1	.0534	9.87	76.55	1.259	.997
24	25.0	12.6	8.4	.0331	-4.8	.0634	10.46	75.99	1.295	.996
25	30.9	13.2	8.8	.0409	-4.4	.0784	10.90	75.21	1.339	.992
26	40.7	14.0	9.2	.0540	-4.0	.1034	11.57	74.46	1.406	.986
27	50.6	14.6	9.6	.0670	-3.6	.1284	12.03	73.83	1.461	.976
28	70.2	15.6	10.0	.0931	-3.2	.1784	12.91	72.96	1.546	.951
29	89.9	16.6	10.4	.1192	-2.8	.2284	13.72	72.25	1.594	.919
30	109.6	17.4	10.7	.1453	-2.5	.2784	14.42	71.62	1.600	.880
31	129.3	18.3	11.0	.1713	-2.2	.3284	15.10	71.07	1.573	.835
32	149.0	19.2	11.3	.1974	-1.9	.3784	15.86	70.53	1.526	.782
33	168.7	20.1	11.5	.2235	-1.7	.4284	16.59	70.14	1.449	.734
34	208.0	21.6	12.0	.2757	-1.2	.5284	17.87	69.33	1.215	.611
35	247.4	23.2	12.3	.3278	-.9	.6284	19.15	68.67	1.015	.479
36	286.8	24.7	12.6	.3800	-.6	.7284	20.45	68.09	.893	.338
37	365.5	26.8	13.0	.4844	-.2	.9284	22.18	67.36	.631	.119
38	444.3	27.2	13.2	.5887	-.0	1.1284	22.52	67.03	.073	.000
39	523.0	27.2	13.2	.6931	-.0	1.3284	22.51	67.03	.000	.087

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00246 DELM = 1.386 REM = 1263.0
V RUN = 110971-1 CF/2 = .00119 DELM = 1.353 REM = 2316.0
PLATE = 9 UINF = 20.7 DEL2 = .1182 DEL3 = 2.840
X(IN) = 34.00 GM = 3.766 THETA = .2168 DEL4 = 10.702
K(E06)= -.5040 GAM = -1.685 BETA = 1.554 H = 1.693

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.7	0.0000	0.00	91.75	1.000	1.000
2	1.9	2.0	1.3	.0019	-12.5	.0055	1.44	89.60	1.024	1.000
3	2.2	2.3	1.6	.0022	-12.3	.0065	1.71	89.18	1.029	1.000
4	2.6	2.7	1.8	.0026	-12.0	.0075	1.97	88.68	1.033	1.000
5	2.9	3.1	2.1	.0029	-11.7	.0085	2.22	88.21	1.038	1.000
6	3.3	3.4	2.3	.0033	-11.5	.0095	2.49	87.71	1.042	1.000
7	3.6	3.8	2.6	.0036	-11.2	.0105	2.75	87.27	1.049	1.000
8	4.0	4.1	2.8	.0039	-10.9	.0115	3.00	86.77	1.055	1.000
9	4.3	4.4	3.1	.0043	-10.6	.0125	3.24	86.15	1.059	1.000
10	4.7	4.8	3.3	.0046	-10.4	.0135	3.48	85.76	1.063	1.000
11	5.0	5.1	3.6	.0050	-10.1	.0145	3.71	85.26	1.069	1.000
12	5.7	5.7	4.0	.0057	-9.7	.0165	4.17	84.49	1.076	1.000
13	6.4	6.3	4.5	.0064	-9.2	.0185	4.57	83.63	1.083	1.000
14	7.1	6.7	4.9	.0070	-8.8	.0205	4.91	82.95	1.092	.999
15	7.8	7.2	5.2	.0077	-8.5	.0225	5.20	82.35	1.100	.999
16	8.5	7.8	5.5	.0084	-8.2	.0245	5.67	81.91	1.107	.999
17	9.2	8.3	5.8	.0091	-7.9	.0265	6.07	81.35	1.115	.999
18	9.9	8.8	6.0	.0098	-7.7	.0285	6.42	80.93	1.123	.999
19	11.3	9.6	6.4	.0112	-7.3	.0325	6.98	80.16	1.137	.998
20	12.7	10.0	6.8	.0125	-6.9	.0365	7.34	79.47	1.151	.997
21	14.4	10.4	7.2	.0143	-6.5	.0415	7.63	78.79	1.167	.996
22	16.2	10.9	7.6	.0160	-6.1	.0465	7.93	78.16	1.183	.995
23	17.9	11.3	7.9	.0177	-5.9	.0515	8.28	77.66	1.200	.994
24	21.4	12.1	8.2	.0211	-5.5	.0615	8.85	77.00	1.232	.993
25	24.8	12.6	8.5	.0246	-5.2	.0715	9.22	76.49	1.261	.991
26	28.3	12.9	8.8	.0280	-4.9	.0815	9.40	75.93	1.289	.987
27	35.3	13.5	9.1	.0349	-4.6	.1015	9.86	75.39	1.347	.984
28	44.0	14.0	9.4	.0435	-4.3	.1265	10.24	74.79	1.413	.978
29	52.6	14.5	9.7	.0521	-4.0	.1515	10.57	74.31	1.475	.972
30	61.3	14.9	9.9	.0607	-3.8	.1765	10.91	73.95	1.535	.965
31	78.7	15.6	10.2	.0779	-3.5	.2265	11.37	73.33	1.638	.949
32	96.1	16.3	10.6	.0951	-3.1	.2765	11.94	72.76	1.731	.930
33	113.5	16.9	10.8	.1123	-2.9	.3265	12.35	72.31	1.797	.909
34	148.2	18.2	11.3	.1467	-2.4	.4265	13.28	71.50	1.881	.859
35	183.0	19.5	11.6	.1811	-2.1	.5265	14.22	70.87	1.888	.805
36	252.5	22.0	12.2	.2500	-1.5	.7265	16.04	69.72	1.692	.659
37	322.0	24.4	12.7	.3188	-1.0	.9265	17.80	68.88	1.271	.504
38	408.9	26.9	13.3	.4048	-.4	1.1765	19.65	67.82	.790	.240
39	495.8	28.2	13.6	.4908	-.1	1.4265	20.57	67.22	.364	.054
40	582.8	28.4	13.7	.5768	.0	1.6765	20.72	67.07	.000	.000
41	624.0	28.3	13.7	.6177	.0	1.7952	20.71	67.07	.000	.001

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00234 DELM = 1.809 REM = 1530.0
V RUN = 110971-1 CF/2 = .00114 DELM = 1.804 REM = 2825.0
PLATE = 12 UINF = 19.5 DEL2 = .1516 DEL3 = 3.713
X(IN) = 46.00 GM = 3.750 THETA = .2802 DEL4 = 13.925
K(E06)= -.3960 GAM = -1.639 BETA = 1.554 H = 1.693

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.1	0.0000	0.00	91.69	1.000	1.000
2	1.7	1.8	1.2	.0014	-13.1	.0053	1.18	89.86	1.018	1.000
3	2.0	2.1	1.4	.0017	-12.8	.0063	1.41	89.45	1.022	1.000
4	2.3	2.4	1.6	.0019	-12.6	.0073	1.62	89.10	1.025	1.000
5	2.7	2.8	1.9	.0022	-12.4	.0083	1.86	88.65	1.029	1.000
6	3.0	3.1	2.1	.0025	-12.1	.0093	2.08	88.24	1.032	1.000
7	3.6	3.7	2.6	.0030	-11.7	.0113	2.52	87.42	1.039	1.000
8	4.3	4.4	3.0	.0035	-11.1	.0133	2.94	86.44	1.046	1.000
9	4.9	5.0	3.5	.0040	-10.6	.0153	3.34	85.52	1.054	1.000
10	5.5	5.5	3.9	.0046	-10.2	.0173	3.71	84.84	1.059	1.000
11	6.2	6.1	4.3	.0051	-9.8	.0193	4.08	84.13	1.075	1.000
12	7.5	7.0	5.1	.0062	-9.0	.0233	4.70	82.80	1.088	.999
13	8.7	7.6	5.5	.0072	-8.6	.0273	5.12	82.03	1.101	.999
14	10.3	8.6	6.1	.0085	-7.9	.0323	5.79	80.96	1.115	.999
15	11.9	9.3	6.7	.0098	-7.4	.0373	6.29	80.07	1.131	.998
16	13.6	10.0	7.1	.0112	-7.0	.0423	6.75	79.38	1.147	.998
17	15.2	10.6	7.4	.0125	-6.7	.0473	7.16	78.72	1.161	.997
18	16.8	11.0	7.7	.0138	-6.4	.0523	7.43	78.25	1.175	.997
19	20.0	11.5	8.1	.0164	-5.9	.0623	7.75	77.49	1.201	.996
20	23.2	12.1	8.4	.0190	-5.6	.0723	8.17	76.94	1.228	.995
21	26.4	12.7	8.7	.0217	-5.4	.0823	8.57	76.55	1.255	.995
22	32.8	13.3	9.1	.0269	-5.0	.1023	8.97	75.87	1.306	.994
23	40.8	13.8	9.4	.0335	-4.7	.1273	9.33	75.24	1.368	.991
24	48.8	14.3	9.7	.0401	-4.4	.1523	9.66	74.73	1.428	.987
25	56.8	14.7	9.9	.0467	-4.1	.1773	9.92	74.34	1.489	.984
26	72.9	15.4	10.2	.0598	-3.9	.2273	10.35	73.64	1.602	.979
27	88.9	15.9	10.5	.0730	-3.6	.2773	10.74	73.33	1.702	.970
28	104.9	16.3	10.8	.0862	-3.3	.3273	11.01	72.88	1.793	.957
29	137.0	17.4	11.1	.1125	-2.9	.4273	11.73	72.25	1.956	.932
30	169.1	18.3	11.5	.1388	-2.6	.5273	12.32	71.59	2.072	.893
31	201.1	19.5	11.8	.1651	-2.3	.6273	13.11	71.05	2.146	.851
32	233.2	20.4	12.1	.1914	-2.0	.7273	13.75	70.60	2.196	.808
33	297.3	22.4	12.6	.2441	-1.5	.9273	15.09	69.73	2.209	.696
34	377.5	24.8	13.1	.3099	-1.0	1.1773	16.71	69.85	1.689	.542
35	457.6	26.7	13.5	.3757	-.6	1.4273	17.98	68.13	1.011	.370
36	537.8	28.2	13.9	.4415	-.2	1.6773	19.01	67.49	.534	.164
37	617.9	28.9	14.0	.5073	-.0	1.9273	19.50	67.16	.296	.030
38	698.1	29.0	14.1	.5731	-.0	2.1773	19.53	67.10	.056	.000
39	778.2	29.0	14.1	.6389	.0	2.4273	19.51	67.07	.000	.000
40	858.4	29.0	14.1	.7047	.0	2.6773	19.53	67.07	.000	.000

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00225 DELM = 2.169 REM = 1769.0
V RUN = 110971-1 CF/2 = .00118 DELM = 2.174 REM = 3258.0
PLATE = 15 UINF = 18.7 DEL2 = .1830 DEL3 = 4.467
X(IN) = 56.00 GM = 3.676 THETA = .3369 DEL4 = 16.423
K(E06)= -.3280 GAM = -1.628 BETA = 1.539 H = 1.652

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.4	0.0000	0.00	91.65	1.000	1.000
2	1.9	2.0	1.3	.0014	-13.3	.0063	1.25	89.71	1.018	1.000
3	2.2	2.3	1.6	.0016	-13.1	.0073	1.45	89.42	1.021	1.000
4	2.5	2.6	1.8	.0018	-12.8	.0083	1.65	88.95	1.024	1.000
5	2.8	2.9	2.0	.0020	-12.6	.0093	1.85	88.60	1.027	1.000
6	3.1	3.2	2.2	.0022	-12.4	.0103	2.04	88.18	1.029	1.000
7	3.4	3.5	2.4	.0025	-12.1	.0113	2.24	87.74	1.032	1.000
8	3.7	3.8	2.6	.0027	-11.9	.0123	2.42	87.33	1.035	1.000
9	4.3	4.4	3.0	.0031	-11.4	.0143	2.80	86.52	1.041	1.000
10	4.9	5.0	3.4	.0036	-11.0	.0163	3.15	85.79	1.047	1.000
11	5.5	5.5	3.9	.0040	-10.5	.0183	3.48	85.05	1.062	1.000
12	6.1	6.0	4.3	.0044	-10.1	.0203	3.79	84.37	1.066	1.000
13	7.6	7.3	5.2	.0059	-9.2	.0293	4.60	82.36	1.090	1.000
14	9.2	8.2	5.8	.0066	-8.6	.0303	5.21	81.73	1.094	.999
15	10.7	9.2	6.4	.0077	-8.0	.0353	5.82	80.75	1.119	.999
16	12.2	10.0	6.8	.0088	-7.6	.0403	6.32	79.98	1.122	.999
17	13.7	10.4	7.2	.0099	-7.2	.0453	6.62	79.36	1.135	.999
18	15.2	10.7	7.5	.0110	-6.9	.0503	6.91	78.88	1.148	.998
19	16.7	11.0	7.8	.0121	-6.6	.0553	7.00	78.37	1.160	.997
20	19.7	11.7	8.3	.0143	-6.1	.0653	7.43	77.54	1.185	.995
21	22.6	12.3	8.6	.0165	-5.8	.0753	7.83	76.91	1.209	.994
22	25.8	12.9	8.9	.0187	-5.5	.0853	8.17	76.47	1.232	.992
23	28.8	13.2	9.1	.0208	-5.2	.0953	8.39	76.11	1.255	.991
24	36.4	13.8	9.5	.0263	-4.9	.1203	8.75	75.45	1.311	.990
25	43.9	14.3	9.8	.0318	-4.6	.1453	9.09	75.00	1.366	.989
26	51.5	14.8	10.0	.0373	-4.4	.1703	9.39	74.64	1.417	.989
27	66.6	15.5	10.3	.0482	-4.1	.2203	9.92	74.02	1.514	.985
28	81.7	15.9	10.6	.0591	-3.8	.2703	10.08	73.57	1.605	.981
29	96.8	16.4	10.9	.0701	-3.6	.3203	10.41	73.21	1.697	.977
30	111.9	17.0	11.0	.0810	-3.4	.3703	10.77	72.91	1.786	.972
31	127.0	17.4	11.2	.0920	-3.2	.4203	11.05	72.61	1.869	.964
32	157.2	18.2	11.5	.1138	-2.9	.5203	11.57	72.04	2.017	.945
33	187.4	18.9	11.8	.1357	-2.6	.6203	11.98	71.53	2.119	.919
34	217.6	19.6	12.0	.1576	-2.3	.7203	12.42	71.11	2.185	.888
35	278.1	21.2	12.5	.2014	-1.9	.9203	13.42	70.39	2.237	.817
36	353.6	23.2	13.0	.2561	-1.4	1.1703	14.74	69.55	2.078	.701
37	429.1	25.2	13.4	.3108	-1.0	1.4203	15.99	68.85	1.718	.564
38	504.7	26.9	13.7	.3655	-.7	1.6703	17.05	68.25	1.217	.412
39	580.2	28.4	14.0	.4202	-.4	1.9203	18.01	67.71	.768	.246
40	655.7	29.2	14.3	.4749	-.1	2.1703	18.53	67.35	.359	.106
41	731.2	29.5	14.4	.5296	-.0	2.4203	18.71	67.13	.061	.000
42	806.8	29.5	14.4	.5843	.0	2.6703	18.74	67.07	.000	.000
43	849.0	29.5	14.4	.6149	.0	2.8100	18.73	67.07	.000	.000

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00218 DELM = 2.687 REM = 2055.0
V RUN = 110971-1 CF/2 = .00107 DELM = 2.567 REM = 3659.0
PLATE = 18 UINF = 19.2 DEL2 = .2194 DEL3 = 5.325
X(IN) = 70.00 GM = 3.645 THETA = .3986 DEL4 = 19.407
K(E06) = -.2820 GAM = -1.637 BETA = 1.527 M = 1.630

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.7	0.0000	0.00	91.59	1.000	1.000
2	1.7	1.8	1.2	.0011	-13.7	.0060	1.05	89.95	1.015	1.000
3	2.0	2.1	1.4	.0013	-13.5	.0070	1.28	89.71	1.017	1.000
4	2.3	2.4	1.6	.0015	-13.3	.0080	1.46	89.33	1.020	1.000
5	2.6	2.7	1.8	.0016	-13.1	.0090	1.64	88.92	1.022	1.000
6	2.9	3.0	2.1	.0018	-12.9	.0100	1.82	88.60	1.024	1.000
7	3.2	3.3	2.3	.0020	-12.6	.0110	2.00	88.09	1.027	1.000
8	3.8	3.9	2.7	.0024	-12.1	.0130	2.35	87.39	1.032	1.000
9	4.4	4.4	3.0	.0027	-11.7	.0150	2.69	86.65	1.037	1.000
10	4.9	4.9	3.4	.0031	-11.3	.0170	3.01	85.97	1.042	1.000
11	5.5	5.5	3.8	.0035	-10.8	.0190	3.32	85.26	1.046	1.000
12	6.1	5.9	4.2	.0038	-10.5	.0210	3.61	84.64	1.049	1.001
13	6.7	6.4	4.5	.0042	-10.1	.0230	3.87	84.07	1.054	1.001
14	7.9	7.1	5.2	.0049	-9.5	.0270	4.35	83.01	1.064	1.001
15	9.3	8.1	5.9	.0059	-8.8	.0320	4.90	81.91	1.075	1.001
16	10.7	9.0	6.4	.0068	-8.3	.0370	5.46	80.99	1.086	1.001
17	12.2	9.9	6.9	.0077	-7.8	.0420	6.02	80.25	1.097	1.001
18	13.6	10.5	7.2	.0086	-7.5	.0470	6.42	79.69	1.105	1.001
19	15.1	10.9	7.5	.0095	-7.2	.0520	6.64	79.24	1.114	1.001
20	16.5	11.1	7.7	.0105	-7.0	.0570	6.79	79.02	1.120	1.001
21	19.4	11.8	8.1	.0123	-6.6	.0670	7.16	78.10	1.150	1.001
22	22.3	12.4	8.5	.0141	-6.2	.0770	7.53	77.57	1.171	1.001
23	25.2	12.8	8.7	.0160	-5.9	.0870	7.82	77.12	1.191	1.080
24	32.5	13.7	9.3	.0206	-5.4	.1120	8.34	76.20	1.240	.997
25	39.7	14.2	9.7	.0251	-5.0	.1370	8.66	75.67	1.286	.994
26	47.0	14.6	9.9	.0297	-4.7	.1621	8.89	75.15	1.329	.993
27	54.2	14.9	10.2	.0343	-4.5	.1873	9.06	74.76	1.372	.991
28	69.7	15.5	10.5	.0435	-4.2	.2378	9.45	74.23	1.455	.987
29	83.2	16.0	10.8	.0527	-3.9	.2878	9.77	73.81	1.537	.983
30	97.7	16.5	10.9	.0619	-3.7	.3378	10.04	73.51	1.615	.981
31	126.7	17.4	11.3	.0802	-3.4	.4378	10.62	72.94	1.758	.972
32	155.7	18.1	11.6	.0986	-3.1	.5378	11.01	72.40	1.857	.957
33	213.7	19.5	12.0	.1353	-2.6	.7378	11.86	71.68	2.043	.935
34	271.7	20.9	12.5	.1721	-2.2	.9378	12.71	70.99	2.149	.892
35	344.2	22.5	12.9	.2180	-1.8	1.1878	13.72	70.30	2.137	.827
36	416.8	24.2	13.3	.2639	-1.4	1.4378	14.71	69.58	1.971	.721
37	489.3	25.8	13.6	.3098	-1.1	1.6878	15.74	69.12	1.649	.635
38	561.8	27.3	13.9	.3557	-.8	1.9378	16.61	68.58	1.292	.503
39	706.8	29.3	14.4	.4475	-.3	2.4378	17.98	67.74	.372	.229
40	851.9	29.9	14.6	.5393	-.0	2.9378	18.23	67.38	.000	.061
41	996.8	29.9	14.7	.6311	-.0	3.4378	18.23	67.32	.000	.000

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00213 DELM = 3.125 REM = 2289.0
V RUN = 110971-1 CF/2 = .00103 DELM = 2.979 REM = 4139.0
PLATE = 21 UINF = 17.7 DEL2 = .2516 DEL3 = 6.076
X(IN) = 52.00 GM = 3.545 THETA = .4549 DEL4 = 21.542
K(E06) = -.2490 GAM = -1.665 BETA = 1.585 M = 1.619

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.7	0.0000	0.00	91.75	1.000	1.000
2	1.5	1.6	1.1	.0009	-13.7	.0056	.91	90.13	1.012	1.000
3	1.8	1.9	1.3	.0011	-13.5	.0066	1.08	89.90	1.014	1.000
4	2.1	2.1	1.5	.0012	-13.4	.0076	1.25	89.48	1.016	1.000
5	2.4	2.4	1.7	.0014	-13.1	.0086	1.41	89.13	1.019	1.000
6	2.9	3.0	2.1	.0017	-12.7	.0106	1.74	88.45	1.023	1.000
7	3.5	3.5	2.5	.0020	-12.3	.0126	2.06	87.77	1.027	1.000
8	4.0	4.1	2.8	.0024	-11.9	.0146	2.37	87.09	1.032	1.000
9	4.6	4.6	3.2	.0027	-11.5	.0166	2.68	86.41	1.036	1.000
10	5.1	5.1	3.6	.0030	-11.1	.0186	2.96	85.76	1.040	1.000
11	5.7	5.6	4.0	.0033	-10.7	.0206	3.24	85.14	1.045	1.000
12	6.2	6.0	4.4	.0037	-10.4	.0226	3.49	84.52	1.050	1.000
13	7.3	6.9	5.1	.0043	-9.7	.0266	4.01	83.39	1.059	1.000
14	8.5	7.8	5.6	.0049	-9.1	.0306	4.51	82.47	1.069	1.000
15	9.8	8.7	6.2	.0057	-8.6	.0356	5.09	81.55	1.085	1.000
16	11.2	9.6	6.6	.0065	-8.1	.0406	5.61	80.78	1.072	1.000
17	12.6	10.3	7.0	.0074	-7.7	.0456	5.99	80.13	1.079	1.000
18	14.0	10.8	7.3	.0082	-7.4	.0506	6.25	79.65	1.086	1.000
19	16.7	11.5	7.8	.0098	-6.9	.0606	6.68	78.88	1.101	1.000
20	19.5	12.2	8.3	.0114	-6.5	.0706	7.10	78.10	1.115	1.001
21	22.3	12.7	8.6	.0130	-6.1	.0806	7.36	77.54	1.129	1.001
22	29.2	13.6	9.2	.0170	-5.6	.1056	7.90	76.61	1.159	1.001
23	36.1	14.3	9.6	.0210	-5.2	.1306	8.30	75.96	1.188	1.000
24	43.0	14.7	9.8	.0250	-4.9	.1556	8.54	75.51	1.217	.997
25	56.9	15.3	10.2	.0331	-4.4	.2056	8.87	74.76	1.276	.988
26	70.7	16.0	10.4	.0411	-4.1	.2556	9.23	74.49	1.335	.984
27	91.4	16.6	10.9	.0532	-3.8	.3306	9.66	73.75	1.402	.970
28	119.1	17.1	11.2	.0693	-3.5	.4306	9.96	73.27	1.465	.957
29	146.7	17.9	11.4	.0854	-3.3	.5306	10.43	72.45	1.536	.944
30	202.1	19.1	11.9	.1176	-2.8	.7306	11.07	72.01	1.644	.903
31	257.4	20.5	12.3	.1497	-2.4	.9306	11.90	71.35	1.735	.860
32	326.5	21.7	12.7	.1900	-2.0	1.1806	12.61	70.79	1.711	.515
33	395.7	23.3	13.1	.2302	-1.7	1.4306	13.53	70.19	1.654	.744
34	464.8	24.6	13.4	.2704	-1.4	1.6806	14.32	69.67	1.517	.659
35	533.9	26.1	13.6	.3106	-1.1	1.9306	15.15	69.22	1.326	.566
36	603.1	27.4	13.9	.3509	-.9	2.1806	15.93	68.76	1.045	.462
37	672.2	28.6	14.1	.3911	-.6	2.4306	16.62	68.40	.732	.367
38	810.5	30.1	14.5	.4715	-.2	2.9306	17.52	67.77	.215	.167
39	948.5	30.5	14.7	.5520	-.0	3.4306	17.73	67.47	.000	.035
40	1087.1	30.5	14.7	.6324	-.0	3.9306	17.74	67.41	.000	.000

DATE = 110871 (-0.20, 0.000)

T RUN = 110871-1 STNA = .00209 DELM = 2.499 REM = 2511.0
V RUN = 110971-1 CF/2 = .00101 DELM = 3.367 REM = 4533.0
PLATE = 23 UINF = 17.2 DEL2 = .2537 DEL3 = 6.979
X(IN) = 90.00 GM = 3.548 THETA = .5122 DEL4 = 24.622
K(E06) = -.2420 GAM = -1.737 BETA = 1.720 M = 1.632

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-14.9	0.0000	0.00	91.75
2	1.5	1.6	1.1	.0008	-14.0	.0056	.87	90.39
3	1.8	1.8	1.2	.0010	-13.9	.0066	1.02	90.10
4	2.0	2.1	1.4	.0011	-13.8	.0075	1.16	89.74
5	2.6	2.7	1.8	.0014	-13.3	.0096	1.49	89.16
6	3.1	3.2	2.2	.0017	-12.8	.0116	1.79	88.42
7	3.6	3.7	2.6	.0020	-12.4	.0136	2.09	87.85
8	4.2	4.3	2.9	.0022	-12.0	.0156	2.38	87.20
9	4.7	4.8	3.3	.0025	-11.5	.0176	2.66	86.72
10	5.2	5.2	3.6	.0028	-11.2	.0196	2.93	85.82
11	5.8	5.7	4.0	.0031	-10.8	.0216	3.18	85.17
12	6.8	6.5	4.7	.0036	-10.1	.0256	3.63	84.02
13	8.2	7.5	5.4	.0043	-9.5	.0306	4.17	82.95
14	9.5	8.2	6.1	.0051	-8.8	.0356	4.57	81.82
15	10.8	8.9	6.7	.0058	-8.5	.0406	4.96	81.35
16	12.1	9.6	6.9	.0065	-8.0	.0456	5.35	80.52
17	14.8	10.7	7.5	.0079	-7.4	.0555	5.96	79.50
18	17.5	11.4	8.0	.0093	-6.9	.0656	6.38	78.67
19	20.1	12.0	8.4	.0107	-6.5	.0756	6.70	78.05
20	26.8	12.8	9.0	.0142	-5.9	.1006	7.18	77.06
21	33.4	13.5	9.4	.0177	-5.5	.1256	7.54	76.35
22	40.1	14.3	9.7	.0213	-5.2	.1506	8.02	75.90
23	46.7	14.8	9.8	.0248	-5.0	.1756	8.27	75.66
24	60.0	15.2	10.3	.0318	-4.6	.2256	8.62	74.94
25	73.4	15.7	10.5	.0389	-4.3	.2756	8.75	74.53
26	86.7	16.0	10.8	.0459	-4.1	.3256	8.94	74.11
27	113.3	16.6	11.1	.0600	-3.8	.4256	9.26	73.63
28	139.9	17.4	11.4	.0741	-3.5	.5256	9.73	73.12
29	193.1	19.5	11.8	.1023	-3.1	.7256	10.36	72.46
30	246.3	19.7	12.2	.1304	-2.6	.9256	11.03	71.74
31	312.9	21.0	12.6	.1657	-2.2	1.1756	11.76	71.09
32	379.4	22.5	12.9	.2009	-2.0	1.4256	12.57	70.66
33	445.9	23.8	13.2	.2361	-1.8	1.6756	13.25	70.06
34	512.5	25.3	13.5	.2713	-1.4	1.9256	14.16	69.67
35	645.5	27.5	14.0	.3418	-.9	2.4256	15.35	69.83
36	778.6	29.7	14.4	.4122	-.4	2.9256	16.54	68.13
37	911.6	30.6	14.7	.4827	-.2	3.4256	17.09	67.68
38	1044.7	30.8	14.8	.5531	-.0	3.9256	17.20	67.47
39	1177.7	30.8	14.9	.6236	-.0	4.4256	17.20	67.41

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00420 DELM = .162 REM = 166.0
V RUN = 91771-2 CF/2 = .00249 DELM = .319 REM = 556.0
PLATE = 1 UINF = 29.7 DEL2 = .0111 DEL3 = .291
X(IN) = 2.00 GM = 4.800 THETA = .0372 DEL4 = 1.398
K(E06) = -.4670 GAM = -.416 BETA = .169 M = 1.624

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-11.6	0.0000	0.00	97.72
2	2.7	3.3	2.0	.0129	-9.7	.0039	9.04	93.56
3	3.4	3.7	2.5	.0162	-9.1	.0049	9.64	92.36
4	4.1	4.2	3.1	.0196	-8.5	.0059	6.12	91.04
5	4.8	4.7	3.6	.0229	-8.1	.0069	7.12	89.98
6	5.6	5.3	4.1	.0263	-7.5	.0079	7.98	88.88
7	6.2	5.8	4.5	.0296	-7.1	.0089	8.74	88.00
8	6.9	6.2	4.9	.0330	-6.7	.0099	9.47	87.00
9	7.6	6.7	5.3	.0363	-6.3	.0109	10.16	86.28
10	9.0	7.5	5.9	.0430	-5.7	.0129	11.35	84.87
11	10.4	8.2	6.4	.0497	-5.2	.0149	12.48	83.68
12	11.9	8.9	6.9	.0564	-4.7	.0169	13.54	82.79
13	13.3	9.5	7.2	.0631	-4.4	.0189	14.42	81.97
14	14.7	9.9	7.6	.0698	-4.0	.0209	14.97	81.13
15	17.5	10.7	8.1	.0832	-3.5	.0249	16.16	79.99
16	21.0	11.4	8.7	.1000	-2.9	.0299	17.24	78.83
17	24.5	11.9	9.1	.1167	-2.5	.0349	18.06	77.91
18	28.0	12.4	9.4	.1335	-2.2	.0399	18.82	77.25
19	31.5	12.7	9.7	.1502	-1.9	.0449	19.31	76.59
20	38.6	13.3	10.1	.1837	-1.5	.0549	20.15	75.75
21	45.6	13.9	10.4	.2172	-1.2	.0649	21.09	75.10
22	52.6	14.3	10.6	.2507	-1.0	.0749	21.72	74.67
23	59.6	14.7	10.8	.2842	-.8	.0849	22.37	74.11
24	70.2	15.3	11.1	.3345	-.5	.0999	23.28	73.62
25	87.7	16.2	11.3	.4182	-.3	.1249	24.53	73.05
26	105.3	16.9	11.4	.5020	-.2	.1499	25.58	72.75
27	122.9	17.5	11.5	.5857	-.1	.1749	26.51	72.57
28	140.4	18.0	11.6	.6695	-.0	.1999	27.29	72.47
29	158.0	18.4	11.6	.7533	-.0	.2249	27.95	72.44
30	175.6	18.8	11.6	.8370	-.0	.2499	28.51	72.41
31	193.1	19.1	11.6	.9208	-.0	.2749	28.94	72.41
32	219.5	19.4	11.6	1.0465	.0	.3124	29.38	72.40
33	254.6	19.5	11.6	1.2140	-.0	.3624	29.62	72.40
34	289.7	19.6	11.6	1.3815	-.0	.4124	29.78	72.40
35	342.4	19.6	11.6	1.6328	-.0	.4874	29.91	72.40
36	395.1	19.6	11.6	1.8840	-.0	.5624	29.91	72.40

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00272 DELH = .513 REH = 609.0
V RUN = 91771-2 CF/2 = .00173 DELH = .593 REH = 1079.0
PLATE = 3 UINF = 26.8 DEL2 = .0452 DEL3 = 1.236
X(IN) = 10.00 GH = 4.973 THETA = .0800 DEL4 = 6.147
K(E06) = -.8720 GAM = -1.358 BETA = .883 H = 1.693

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.9	0.0000	0.00	97.44	1.000	1.000
2	2.6	3.1	1.9	.0038	-13.2	.0049	3.54	94.59	1.027	1.042
3	3.1	3.5	2.3	.0046	-12.8	.0059	3.95	93.80	1.043	1.054
4	3.6	3.8	2.7	.0054	-12.3	.0069	4.38	92.98	1.059	1.065
5	4.2	4.2	3.2	.0062	-11.8	.0079	4.77	92.16	1.075	1.077
6	4.7	4.6	3.6	.0070	-11.3	.0089	5.21	91.39	1.091	1.088
7	5.2	5.0	4.0	.0078	-10.9	.0099	5.72	90.68	1.209	1.098
8	5.8	5.5	4.3	.0096	-10.6	.0109	6.24	90.13	1.226	1.106
9	6.6	6.3	5.0	.0102	-10.0	.0129	7.16	89.06	1.259	1.121
10	7.5	7.0	5.6	.0117	-9.4	.0149	7.94	88.08	1.287	1.139
11	8.9	7.6	6.1	.0133	-8.9	.0169	8.62	87.26	1.317	1.146
12	10.0	8.1	6.5	.0149	-8.4	.0189	9.24	86.52	1.336	1.156
13	11.1	8.5	6.9	.0165	-8.0	.0209	9.74	85.81	1.356	1.165
14	12.1	8.9	7.2	.0181	-7.7	.0229	10.16	85.31	1.373	1.171
15	13.2	9.2	7.6	.0196	-7.4	.0249	10.52	84.89	1.389	1.178
16	15.7	9.8	8.0	.0225	-7.0	.0289	11.20	84.07	1.417	1.187
17	17.4	10.2	9.4	.0260	-6.5	.0329	11.79	83.33	1.443	1.195
18	20.0	10.9	8.8	.0299	-6.2	.0379	12.49	82.67	1.472	1.201
19	22.7	11.5	9.1	.0339	-5.8	.0429	13.08	82.08	1.496	1.206
20	25.3	11.8	9.4	.0378	-5.5	.0479	13.50	81.60	1.514	1.208
21	28.0	12.1	9.7	.0418	-5.2	.0529	13.84	81.22	1.529	1.210
22	33.3	12.6	10.0	.0497	-4.9	.0629	14.40	80.59	1.548	1.209
23	38.6	13.1	10.4	.0576	-4.5	.0729	14.89	79.97	1.562	1.202
24	43.8	13.4	10.6	.0655	-4.3	.0829	15.32	79.58	1.569	1.194
25	57.1	14.2	11.3	.0852	-3.7	.1079	16.30	78.54	1.568	1.155
26	70.3	15.1	11.7	.1050	-3.2	.1329	17.19	77.76	1.545	1.105
27	83.5	15.7	12.1	.1247	-2.8	.1579	17.91	77.10	1.490	1.046
28	96.7	16.4	12.5	.1445	-2.5	.1829	18.66	76.47	1.427	.976
29	110.0	17.0	12.8	.1643	-2.2	.2079	19.44	76.00	1.357	.910
30	123.2	17.6	13.1	.1840	-1.9	.2329	20.11	75.49	1.267	.932
31	149.6	18.8	13.5	.2235	-1.4	.2829	21.45	74.68	1.085	.679
32	176.1	20.0	14.0	.2630	-1.0	.3329	22.81	73.98	.939	.520
33	202.5	21.0	14.3	.3026	-.7	.3829	24.01	73.41	.807	.370
34	229.0	21.9	14.6	.3421	-.4	.4329	25.03	72.99	.705	.243
35	281.8	23.2	14.9	.4211	-.1	.5329	26.44	72.48	.520	.062
36	334.7	23.5	14.9	.5001	-.0	.6329	26.78	72.33	.211	.000
37	387.6	23.5	14.9	.5792	-.0	.7329	26.82	72.33	.000	.001
38	425.4	23.5	14.9	.6357	-.0	.8044	26.82	72.33	.000	.000

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00224 DELH = .944 REH = 1112.0
V RUN = 91771-2 CF/2 = .00136 DELH = .949 REH = 1778.0
PLATE = 6 UINF = 24.4 DEL2 = .0967 DEL3 = 2.592
X(IN) = 22.00 GH = 5.010 THETA = .1449 DEL4 = 12.986
K(E06) = -.4900 GAM = -1.227 BETA = 1.025 H = 1.710

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.2	0.0000	0.00	97.31	1.000	1.000
2	2.2	3.2	1.6	.0020	-14.7	.0051	2.97	95.06	1.129	1.041
3	2.6	3.4	1.9	.0024	-14.4	.0061	3.16	94.53	1.138	1.050
4	3.1	3.7	2.2	.0027	-14.1	.0071	3.46	94.03	1.151	1.059
5	3.5	4.1	2.5	.0031	-13.7	.0081	3.78	93.49	1.165	1.069
6	3.9	4.4	2.9	.0035	-13.3	.0091	4.11	92.93	1.179	1.081
7	4.4	4.8	3.3	.0039	-12.9	.0101	4.42	92.24	1.192	1.091
8	4.8	5.1	3.7	.0042	-12.5	.0111	4.72	91.63	1.205	1.102
9	5.2	5.4	4.1	.0046	-12.1	.0121	5.03	91.01	1.218	1.113
10	5.6	5.8	4.3	.0050	-11.9	.0131	5.37	90.71	1.232	1.119
11	6.1	6.1	4.5	.0054	-11.7	.0141	5.70	90.30	1.246	1.126
12	6.5	6.5	4.8	.0058	-11.4	.0151	6.01	89.86	1.259	1.134
13	7.4	7.0	5.3	.0065	-10.9	.0171	6.54	89.09	1.282	1.147
14	8.2	7.5	5.9	.0073	-10.3	.0191	6.96	88.27	1.302	1.161
15	9.1	7.9	6.2	.0080	-10.0	.0211	7.34	87.74	1.320	1.170
16	10.8	8.7	6.9	.0095	-9.3	.0251	8.09	86.73	1.355	1.188
17	12.5	9.4	7.4	.0110	-8.8	.0291	8.70	85.85	1.387	1.202
18	14.7	10.0	7.9	.0129	-8.3	.0341	9.25	85.11	1.420	1.214
19	16.8	10.5	8.4	.0148	-7.8	.0391	9.77	84.39	1.449	1.225
20	19.0	11.0	8.7	.0167	-7.5	.0441	10.22	83.92	1.475	1.233
21	21.1	11.4	8.9	.0186	-7.3	.0491	10.61	83.58	1.500	1.239
22	25.4	12.0	9.5	.0223	-6.7	.0591	11.12	82.70	1.536	1.248
23	29.7	12.3	9.8	.0261	-6.4	.0691	11.46	82.17	1.566	1.254
24	34.1	12.6	10.1	.0299	-6.1	.0791	11.72	81.67	1.594	1.257
25	44.5	13.8	10.7	.0393	-5.5	.1041	12.83	80.80	1.676	1.295
26	55.6	14.3	11.2	.0487	-5.1	.1291	13.27	80.12	1.718	1.252
27	66.3	14.8	11.5	.0582	-4.7	.1541	13.68	79.64	1.752	1.244
28	77.1	15.3	11.8	.0676	-4.4	.1791	14.20	79.17	1.785	1.231
29	98.6	16.2	12.3	.0865	-3.9	.2291	15.00	78.30	1.812	1.192
30	120.2	17.0	12.7	.1053	-3.5	.2791	15.80	77.70	1.811	1.150
31	141.7	17.8	13.1	.1242	-3.1	.3291	16.55	77.05	1.769	1.092
32	163.2	18.7	13.5	.1430	-2.7	.3791	17.36	76.48	1.703	1.028
33	184.7	19.6	13.8	.1619	-2.4	.4291	18.16	75.97	1.607	.959
34	227.8	21.2	14.4	.1996	-1.8	.5291	19.67	75.10	1.353	.808
35	270.9	22.7	14.9	.2373	-1.3	.6291	21.07	74.29	1.111	.630
36	313.9	24.1	15.4	.2750	-.8	.7291	22.35	73.69	.916	.445
37	356.9	25.2	15.8	.3127	-.5	.8291	23.47	73.03	.777	.267
38	400.0	26.0	16.0	.3504	-.2	.9291	24.10	72.61	.568	.116
39	486.1	26.3	16.2	.4258	-.0	1.1291	24.43	72.33	.061	.000
40	572.2	26.3	16.2	.5013	-.0	1.3291	24.42	72.33	.000	.003

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00262 DELH = 1.363 REH = 1536.0
V RUN = 91771-2 CF/2 = .00189 DELH = 1.367 REH = 2394.0
PLATE = 9 UINF = 23.0 DEL2 = .1327 DEL3 = 3.667
X(IN) = 34.00 GH = 4.766 THETA = .2065 DEL4 = 17.958
K(E06) = -.3520 GAM = -1.222 BETA = 1.256 H = 1.690

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.0	0.0000	0.00	97.78	1.000	1.000
2	2.2	2.3	1.6	.0016	-14.6	.0060	1.80	95.21	1.094	1.043
3	2.5	2.7	1.8	.0019	-14.3	.0070	2.11	94.74	1.110	1.053
4	2.9	3.1	2.1	.0022	-14.0	.0080	2.42	94.30	1.126	1.062
5	3.2	3.5	2.4	.0024	-13.6	.0090	2.73	93.64	1.147	1.074
6	3.6	3.9	2.7	.0027	-13.3	.0100	3.04	93.21	1.166	1.083
7	4.0	4.3	2.9	.0030	-13.0	.0110	3.34	92.77	1.181	1.092
8	4.3	4.7	3.2	.0032	-12.8	.0120	3.63	92.36	1.194	1.101
9	4.7	5.0	3.5	.0035	-12.4	.0130	3.91	91.89	1.209	1.112
10	5.4	5.7	4.1	.0040	-11.9	.0150	4.44	91.01	1.235	1.126
11	6.1	6.3	4.6	.0046	-11.4	.0170	4.91	90.24	1.259	1.143
12	6.6	6.8	5.0	.0051	-11.0	.0190	5.28	89.51	1.280	1.157
13	7.6	7.2	5.3	.0056	-10.7	.0210	5.62	89.06	1.301	1.167
14	8.3	7.7	5.7	.0062	-10.2	.0230	5.98	88.39	1.322	1.180
15	9.7	8.7	6.3	.0073	-9.7	.0270	6.77	87.50	1.365	1.198
16	11.5	9.8	6.9	.0086	-9.1	.0320	7.66	86.56	1.414	1.216
17	13.3	10.5	7.4	.0099	-8.6	.0370	8.17	85.82	1.450	1.231
18	15.1	11.0	7.7	.0113	-8.2	.0420	8.56	85.25	1.479	1.241
19	16.9	11.4	8.1	.0126	-7.9	.0470	8.95	84.72	1.503	1.251
20	20.5	12.2	8.7	.0153	-7.3	.0570	9.52	83.77	1.546	1.266
21	24.2	12.9	9.0	.0180	-6.9	.0670	9.95	83.21	1.598	1.275
22	27.8	13.1	9.4	.0207	-6.6	.0770	10.19	82.62	1.627	1.284
23	36.8	14.3	10.0	.0274	-6.0	.1020	11.15	81.75	1.719	1.294
24	45.8	14.8	10.3	.0341	-5.7	.1270	11.49	81.22	1.775	1.298
25	54.8	15.4	10.6	.0408	-5.4	.1520	11.93	80.80	1.835	1.299
26	63.8	15.7	11.0	.0475	-4.9	.1770	12.24	80.09	1.885	1.292
27	81.9	16.7	11.4	.0608	-4.6	.2270	12.97	79.52	1.994	1.262
28	99.9	17.6	11.7	.0742	-4.2	.2770	13.64	79.06	2.061	1.265
29	117.9	18.1	12.1	.0876	-3.9	.3270	14.06	78.39	2.103	1.242
30	154.0	19.5	12.7	.1144	-3.3	.4270	15.12	77.50	2.162	1.186
31	190.0	20.9	13.2	.1412	-2.8	.5270	16.24	76.66	2.156	1.103
32	226.1	22.2	13.7	.1680	-2.3	.6270	17.27	75.94	2.080	1.007
33	262.2	23.5	14.1	.1948	-1.9	.7270	18.27	75.31	1.987	.903
34	298.2	24.8	14.4	.2216	-1.5	.8270	19.25	74.74	1.858	.789
35	334.3	26.0	14.8	.2484	-1.2	.9270	20.17	74.17	1.395	.653
36	406.4	28.0	15.4	.3020	-.6	1.1270	21.76	73.27	.936	.384
37	478.5	29.3	15.8	.3556	-.2	1.3270	22.74	72.61	.598	.128
38	550.6	29.6	16.0	.4092	-.0	1.5270	23.01	72.34	.232	.000
39	622.8	29.6	16.0	.4628	-.0	1.7270	22.99	72.31	.274	.000
40	694.9	29.6	16.0	.5164	-.0	1.9270	22.99	72.31	.274	.000

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00189 DELH = 1.811 REH = 1949.0
V RUN = 91771-2 CF/2 = .00102 DELH = 1.766 REH = 2978.0
PLATE = 12 UINF = 22.1 DEL2 = .1751 DEL3 = 4.916
X(IN) = 46.00 GH = 4.818 THETA = .2676 DEL4 = 23.647
K(E06) = -.2760 GAM = -1.201 BETA = 1.309 H = 1.685

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.5	0.0000	0.00	97.27	1.000	1.000
2	1.3	1.4	.9	.0008	-15.6	.0038	.98	95.88	1.054	1.029
3	1.6	1.7	1.2	.0010	-15.4	.0048	1.24	95.56	1.069	1.036
4	2.0	2.1	1.4	.0012	-15.1	.0058	1.50	95.18	1.083	1.044
5	2.3	2.5	1.7	.0014	-14.9	.0068	1.77	94.83	1.098	1.051
6	2.6	2.8	1.9	.0016	-14.7	.0078	2.04	94.45	1.113	1.059
7	3.0	3.2	2.2	.0018	-14.3	.0088	2.30	93.98	1.127	1.069
8	3.3	3.6	2.4	.0020	-14.1	.0098	2.57	93.65	1.142	1.076
9	3.6	3.9	2.8	.0022	-13.7	.0108	2.83	93.07	1.157	1.088
10	4.3	4.6	3.3	.0026	-13.2	.0128	3.34	92.30	1.184	1.104
11	5.0	5.3	3.7	.0029	-12.8	.0148	3.82	91.60	1.215	1.119
12	5.6	5.9	4.3	.0033	-12.2	.0168	4.26	90.80	1.238	1.136
13	6.3	6.5	4.8	.0037	-11.8	.0188	4.67	90.07	1.260	1.151
14	7.7	7.5	5.3	.0045	-11.2	.0228	5.41	89.21	1.305	1.169
15	9.3	8.5	6.1	.0055	-10.4	.0278	6.14	88.00	1.350	1.194
16	11.0	9.2	6.9	.0065	-9.6	.0328	6.68	86.85	1.387	1.217
17	12.7	10.0	7.4	.0075	-9.1	.0378	7.20	86.05	1.422	1.233
18	14.4	10.8	7.8	.0085	-8.9	.0428	7.79	85.67	1.460	1.241
19	17.7	11.5	8.3	.0105	-8.2	.0528	8.72	84.66	1.506	1.260
20	21.1	12.2	8.7	.0125	-7.8	.0628	8.81	84.13	1.549	1.271
21	24.4	12.6	9.0	.0145	-7.5	.0728	9.10	83.60	1.583	1.279
22	32.8	13.5	9.7	.0194	-6.8	.0978	9.76	82.50	1.662	1.295
23	41.2	14.4	10.1	.0244	-6.4	.1228	10.39	81.93	1.731	1.303
24	49.6	15.0	10.6	.0294	-5.9	.1478	10.92	81.22	1.801	1.308
25	58.0	15.4	10.9	.0344	-5.7	.1728	11.14	80.80	1.856	1.310
26	74.7	16.1	11.2	.0443	-5.3	.2228	11.63	80.27	1.954	1.309
27	91.5	16.8	11.6	.0542	-4.9	.2728	12.11	79.67	2.039	1.300
28	108.2	17.5	11.9	.0642	-4.6	.3228	12.65	79.23	2.119	1.291
29	141.8	18.7	12.6	.0840	-3.9	.4228	13.52	78.16	2.240	1.254
30	175.3	19.9	13.0	.1039	-3.6	.5228	14.36	77.62	2.318	1.222
31	208.8	20.9	13.4	.1238	-3.1	.6228	15.12	76.99	2.337	1.172
32	242.4	22.0	13.7	.1437	-2.8	.7228	15.89	76.42	2.304	1.112
33	309.4	24.1	14.4	.1834	-2.1	.9228	17.44	75.37	2.075	.963
34	393.2	26.6	15.2	.2331	-1.4	1.1728	19.22	74.26	1.556	.736
35	477.1	28.7	15.8	.2828	-.8	1.4228	20.76	73.36	.999	.478
36	560.9	30.1	16.2	.3325	-.3	1.6728	21.72	72.67	.540	.220
37	644.7	30.5	16.4	.3822	-.1	1.9228	22.06	72.31	.216	.054
38	728.5	30.6	16.5	.4319	-.0	2.1728	22.11	72.22	.032	.000
39	812.3	30.6	16.5	.4816	-.0	2.4228	22.09	72.22	.067	.000

C

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .30179 DELM = 2.190 REM = 2287.0
W RUN = 91771-2 CF/2 = .00096 DELM = 2.173 REM = 3510.0
PLATE = 15 UINF = 21.4 DEL2 = .2122 DEL3 = 6.044
X(IN) = 58.00 GM = 4.830 THETA = .3257 DEL4 = 29.191
K(E06) = -.2270 GAM = -1.191 BETA = 1.345 M = 1.869

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.9	0.0000	0.00	97.00	1.000	1.000
2	1.5	1.7	1.1	.0008	-15.8	.0049	1.12	95.35	1.067	1.037
3	1.9	2.0	1.3	.0010	-15.6	.0059	1.39	95.06	1.081	1.043
4	2.2	2.4	1.6	.0011	-15.4	.0069	1.60	94.71	1.095	1.051
5	2.5	2.7	1.8	.0013	-15.1	.0079	1.84	94.33	1.109	1.059
6	2.8	3.1	2.0	.0014	-14.9	.0089	2.06	93.98	1.123	1.067
7	3.1	3.4	2.3	.0016	-14.6	.0099	2.32	93.59	1.137	1.076
8	3.4	3.8	2.5	.0018	-14.4	.0109	2.55	93.27	1.151	1.083
9	4.1	4.4	3.2	.0021	-13.8	.0129	3.01	92.33	1.183	1.104
10	4.7	5.1	3.6	.0024	-13.3	.0149	3.45	91.65	1.214	1.118
11	5.3	5.7	4.1	.0027	-12.8	.0169	3.96	90.92	1.242	1.135
12	6.0	6.2	4.5	.0031	-12.4	.0189	4.24	90.33	1.266	1.144
13	6.6	6.7	4.9	.0034	-12.0	.0209	4.56	89.74	1.287	1.161
14	8.2	8.0	5.7	.0042	-11.2	.0259	5.42	88.56	1.341	1.187
15	9.7	9.0	6.3	.0050	-10.6	.0309	6.05	87.65	1.386	1.207
16	11.3	9.8	7.0	.0058	-10.0	.0359	6.62	86.73	1.425	1.227
17	12.9	10.4	7.4	.0066	-9.5	.0409	7.09	86.02	1.460	1.242
18	16.1	11.3	8.0	.0082	-8.9	.0509	7.69	85.20	1.513	1.260
19	19.2	12.1	8.7	.0099	-8.3	.0609	8.21	84.22	1.560	1.278
20	22.4	12.6	8.9	.0115	-8.0	.0709	8.58	83.89	1.601	1.286
21	30.3	13.8	9.6	.0155	-7.2	.0959	9.32	82.93	1.694	1.305
22	33.1	14.4	10.3	.0196	-6.7	.1209	9.74	81.85	1.769	1.319
23	46.0	14.9	10.6	.0236	-6.3	.1459	10.11	81.34	1.830	1.327
24	53.9	15.4	10.8	.0276	-6.1	.1709	10.43	81.01	1.892	1.333
25	69.7	16.2	11.2	.0357	-5.7	.2209	11.01	80.51	2.011	1.332
26	85.4	16.8	11.5	.0438	-5.4	.2709	11.43	79.97	2.113	1.332
27	101.2	17.4	12.0	.0519	-5.0	.3209	11.77	79.35	2.205	1.328
28	172.8	18.4	12.4	.0851	-4.5	.4209	12.50	78.72	2.371	1.322
29	164.3	19.5	12.9	.0842	-4.1	.5209	13.26	78.04	2.497	1.296
30	227.4	21.3	13.6	.1156	-3.3	.7209	14.48	76.93	2.572	1.219
31	290.5	23.1	14.3	.1489	-2.7	.9209	15.69	75.98	2.473	1.115
32	369.3	25.4	14.9	.1894	-2.0	1.1709	17.23	74.96	2.148	.944
33	448.2	27.4	15.5	.2298	-1.4	1.4209	18.57	74.09	1.896	.734
34	527.0	29.2	16.0	.2702	-.9	1.6709	19.75	73.37	.939	.516
35	605.9	30.5	16.4	.3106	-.5	1.9209	20.64	72.74	.767	.289
36	684.7	31.3	16.8	.3511	-.2	2.1709	21.22	72.26	.054	.085
37	763.6	31.6	16.9	.3915	-.1	2.4209	21.42	72.08	.000	.000
38	842.4	31.6	16.9	.4319	-.0	2.6709	21.44	72.05	.026	.000
39	921.3	31.6	16.9	.4724	-.0	2.9209	21.42	72.05	.213	.007
40	949.1	31.6	16.9	.4866	-.0	3.0090	21.43	72.05	.000	.012

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00171 DELM = 2.597 REM = 2669.0
W RUN = 91771-2 CF/2 = .00091 DELM = 2.527 REM = 4014.0
PLATE = 18 UINF = 20.9 DEL2 = .2538 DEL3 = 7.274
X(IN) = 76.00 GM = 4.921 THETA = .3816 DEL4 = 35.067
K(E06) = -.1930 GAM = -1.167 BETA = 1.383 M = 1.664

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.2	0.0000	0.00	96.86	1.000	1.000
2	1.4	1.5	1.0	.0006	-16.3	.0046	.96	95.44	1.061	1.034
3	1.7	1.8	1.2	.0007	-16.1	.0056	1.18	95.15	1.075	1.041
4	2.0	2.2	1.4	.0009	-15.8	.0066	1.39	94.93	1.089	1.049
5	2.3	2.5	1.7	.0010	-15.6	.0076	1.61	94.56	1.103	1.059
6	2.6	2.8	1.9	.0012	-15.4	.0085	1.83	94.18	1.117	1.064
7	2.9	3.2	2.1	.0013	-15.2	.0096	2.05	93.86	1.131	1.072
8	3.2	3.5	2.3	.0014	-14.9	.0106	2.27	93.51	1.144	1.080
9	3.8	4.2	2.9	.0017	-14.4	.0126	2.70	92.71	1.172	1.099
10	4.4	4.8	3.3	.0020	-13.9	.0146	3.11	92.10	1.198	1.113
11	5.0	5.4	3.8	.0022	-13.5	.0166	3.50	91.42	1.218	1.129
12	6.2	6.5	4.5	.0028	-12.7	.0206	4.19	90.33	1.267	1.155
13	7.4	7.4	5.1	.0033	-11.9	.0246	4.78	89.18	1.302	1.182
14	8.6	8.2	5.9	.0038	-11.4	.0286	5.32	88.39	1.344	1.200
15	10.1	9.1	6.7	.0045	-10.5	.0336	6.01	87.15	1.392	1.229
16	11.5	10.1	7.3	.0052	-9.9	.0386	6.51	86.25	1.427	1.247
17	13.1	10.6	7.5	.0059	-9.7	.0436	6.83	86.05	1.452	1.255
18	16.1	11.7	8.2	.0072	-9.0	.0536	7.31	84.98	1.496	1.279
19	19.1	12.0	8.6	.0085	-8.7	.0636	7.77	84.60	1.537	1.299
20	26.6	13.7	9.6	.0119	-7.7	.0886	8.69	83.19	1.621	1.321
21	34.1	14.2	9.9	.0153	-7.3	.1136	9.15	82.59	1.690	1.336
22	41.6	14.8	10.4	.0186	-6.8	.1386	9.39	81.79	1.740	1.350
23	56.6	15.7	10.9	.0253	-6.2	.1886	10.15	81.16	1.858	1.359
24	71.6	16.4	11.3	.0321	-5.9	.2386	10.57	80.51	1.950	1.362
25	86.6	17.0	11.7	.0388	-5.6	.2886	10.95	80.03	2.037	1.365
26	101.6	17.6	12.0	.0455	-5.2	.3385	11.35	79.60	2.125	1.367
27	131.6	18.7	12.5	.0589	-4.7	.4386	12.02	78.81	2.279	1.363
28	161.6	19.3	12.9	.0724	-4.3	.5386	12.46	78.22	2.397	1.348
29	191.6	20.1	13.3	.0858	-4.0	.6386	13.00	77.71	2.479	1.325
30	221.6	21.0	13.6	.0992	-3.7	.7386	13.54	77.29	2.546	1.301
31	281.6	22.6	14.1	.1261	-3.1	.9386	14.57	76.48	2.599	1.239
32	356.6	24.5	14.7	.1597	-2.5	1.1886	15.99	75.56	2.529	1.117
33	431.6	26.5	15.3	.1933	-1.9	1.4386	17.12	74.79	2.269	.964
34	506.6	28.2	15.8	.2269	-1.4	1.6886	18.22	74.06	1.755	.778
35	581.6	29.8	16.3	.2605	-.9	1.9386	19.22	73.47	1.245	.561
36	656.6	31.0	16.7	.2941	-.6	2.1886	20.01	72.80	.767	.354
37	731.6	31.9	16.9	.3277	-.3	2.4386	20.59	72.39	.424	.175
38	806.6	32.4	17.1	.3613	-.1	2.6886	20.91	72.11	.197	.045
39	881.6	32.5	17.2	.3949	-.0	2.9386	20.97	72.02	.029	.000
40	956.6	32.5	17.2	.4285	.0	3.1886	20.95	71.96	.000	.000
41	1031.7	32.5	17.2	.4621	.0	3.4386	20.95	71.96	.000	.000

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00165 DELM = 2.682 REM = 2915.0
W RUN = 91771-2 CF/2 = .00088 DELM = 2.903 REM = 4561.0
PLATE = 21 UINF = 20.5 DEL2 = .2825 DEL3 = 9.242
X(IN) = 82.00 GM = 4.843 THETA = .4402 DEL4 = 49.912
K(E06) = -.1690 GAM = -1.168 BETA = 1.416 M = 1.646

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.6	0.0000	0.00	96.76	1.000	1.000
2	1.6	1.7	1.1	.0006	-16.5	.0054	1.04	95.21	1.068	1.038
3	1.9	2.0	1.3	.0007	-16.3	.0064	1.23	94.91	1.081	1.045
4	2.1	2.3	1.6	.0009	-16.1	.0074	1.43	94.62	1.094	1.053
5	2.4	2.6	1.8	.0010	-15.9	.0084	1.62	94.39	1.107	1.058
6	2.7	2.9	2.0	.0011	-15.6	.0094	1.83	94.01	1.120	1.068
7	3.3	3.6	2.4	.0013	-15.1	.0114	2.23	93.33	1.146	1.084
8	3.9	4.2	2.9	.0016	-14.7	.0134	2.62	92.71	1.172	1.100
9	4.5	4.8	3.4	.0018	-14.1	.0154	3.00	91.92	1.197	1.119
10	5.0	5.4	3.8	.0021	-13.7	.0174	3.35	91.33	1.219	1.133
11	5.6	5.9	4.2	.0023	-13.4	.0194	3.69	90.56	1.238	1.145
12	6.8	6.9	4.8	.0028	-12.8	.0234	4.27	90.04	1.277	1.166
13	8.2	8.1	5.7	.0034	-11.9	.0284	5.05	88.82	1.332	1.196
14	9.7	9.1	6.3	.0039	-11.3	.0334	5.63	87.94	1.372	1.217
15	11.1	9.7	7.0	.0045	-10.8	.0384	6.04	86.88	1.402	1.243
16	12.6	10.2	7.4	.0051	-10.1	.0434	6.34	86.29	1.427	1.257
17	15.5	11.4	8.2	.0063	-9.2	.0534	7.11	85.17	1.484	1.282
18	18.4	11.9	8.5	.0075	-8.8	.0634	7.39	84.72	1.512	1.294
19	21.3	12.4	9.0	.0087	-8.5	.0734	7.79	84.04	1.545	1.309
20	24.1	13.1	9.3	.0099	-8.2	.0834	8.15	83.63	1.562	1.319
21	31.4	13.9	10.1	.0128	-7.6	.1084	8.68	82.53	1.644	1.341
22	38.6	14.7	10.3	.0158	-7.3	.1334	9.11	82.29	1.717	1.348
23	45.9	15.2	10.9	.0188	-6.7	.1584	9.47	81.52	1.751	1.354
24	53.1	15.7	11.0	.0217	-6.6	.1834	9.76	81.25	1.796	1.353
25	67.6	16.4	11.3	.0277	-6.2	.2334	10.23	80.81	1.852	1.355
26	82.0	17.1	11.7	.0336	-5.9	.2834	10.63	80.27	1.962	1.359
27	96.5	17.6	12.1	.0395	-5.5	.3334	10.97	79.77	2.035	1.361
28	125.5	18.6	12.6	.0514	-5.0	.4334	11.58	79.05	2.159	1.355
29	154.4	19.4	12.9	.0632	-4.7	.5334	12.07	78.60	2.259	1.342
30	212.3	20.8	13.5	.0870	-4.0	.7334	12.92	77.71	2.402	1.291
31	270.2	22.2	14.2	.1107	-3.4	.9334	13.79	76.78	2.502	1.202
32	342.6	23.9	14.7	.1403	-2.9	1.1834	14.85	76.07	2.498	1.120
33	414.9	25.5	15.3	.1700	-2.3	1.4334	15.84	75.29	2.344	1.015
34	487.3	27.0	15.7	.1996	-1.8	1.6834	16.82	74.60	2.112	.898
35	559.7	28.6	16.1	.2293	-1.4	1.9334	17.78	74.03	1.794	.777
36	632.1	30.0	16.6	.2589	-1.0	2.1834	18.66	73.43	1.396	.599
37	704.4	31.3	16.9	.2886	-.7	2.4334	19.45	72.95	.981	.429
38	776.8	32.2	17.2	.3182	-.4	2.6834	20.04	72.53	.606	.260
39	849.2	32.8	17.5	.3479	-.1	2.9334	20.39	72.20	.314	.087
40	921.5	33.0	17.5	.3775	-.1	3.1834	20.52	72.08	.197	.000
41	993.9	33.0	17.6	.4072	-.0	3.4334	20.54	72.02	.000	.000
42	1066.3	33.0	17.6	.4368	-.0	3.6834	20.53	72.02	.000	.000
43	1138.7	33.0	17.6	.4664	-.0	3.9334	20.54	72.02	.000	.000

DATE = 092971 (-0.15, 0.001)

T RUN = 92971-1 STNA = .00162 DELM = 3.265 REM = 3173.0
W RUN = 91771-2 CF/2 = .00086 DELM = 3.164 REM = 4875.0
PLATE = 23 UINF = 20.1 DEL2 = .3127 DEL3 = 9.132
X(IN) = 90.00 GM = 4.846 THETA = .4803 DEL4 = 44.254
K(E06) = -.1640 GAM = -1.243 BETA = 1.510 M = 1.643

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-17.7	0.0000	0.00	96.65
2	1.4	1.5	1.0	.0006	-16.8	.0051	.92	95.38
3	1.7	1.8	1.2	.0007	-16.6	.0061	1.11	95.12
4	2.0	2.2	1.4	.0008	-16.3	.0071	1.30	94.77
5	2.3	2.5	1.6	.0009	-16.1	.0081	1.49	94.47
6	2.6	2.8	1.9	.0010	-15.9	.0091	1.69	94.18
7	2.9	3.1	2.1	.0011	-15.6	.0101	1.87	93.77
8	3.4	3.7	2.5	.0013	-15.2	.0121	2.24	93.18
9	4.0	4.3	3.0	.0016	-14.7	.0141	2.61	92.54
10	4.5	4.9	3.4	.0018	-14.3	.0161	2.97	91.89
11	5.1	5.5	4.0	.0020	-13.7	.0181	3.30	91.16
12	6.2	6.5	4.7	.0024	-13.0	.0221	3.90	90.13
13	7.3	7.3	5.3	.0028	-12.4	.0261	4.42	89.27
14	8.7	8.4	5.8	.0034	-11.9	.0311	5.03	88.56
15	10.1	9.2	6.6	.0039	-11.1	.0361	5.53	87.56
16	11.5	9.9	7.2	.0044	-10.5	.0411	6.00	86.70
17	12.9	10.5	7.6	.0050	-10.2	.0461	6.34	86.26
18	14.3	10.8	7.9	.0055	-9.8	.0511	6.49	85.76
19	15.7	10.9	9.1	.0060	-9.6	.0561	6.59	85.37
20	17.1	11.4	9.5	.0066	-9.2	.0611	6.86	84.93
21	18.5	11.8	8.7	.0071	-9.0	.0661	7.14	84.66
22	21.4	12.7	9.0	.0082	-8.7	.0761	7.69	84.25
23	24.2	13.2	9.3	.0093	-8.4	.0861	7.97	83.80
24	28.4	13.8	9.6	.0109	-8.1	.1011	8.32	83.30
25	35.4	14.5	10.3	.0135	-7.4	.1261	8.71	82.38
26	42.4	14.9	10.4	.0162	-7.3	.1511	8.98	82.20
27	56.4	16.0	11.0	.0216	-6.8	.2011	9.62	81.49
28	70.5	16.7	11.4	.0269	-6.3	.2511	10.09	80.84
29	91.5	17.4	11.9	.0350	-5.8	.3261	10.52	80.15
30	119.6	18.2	12.5	.0457	-5.2	.4261	10.97	79.35
31	147.6	19.1	12.8	.0564	-4.8	.5261	11.52	78.93
32	203.9	20.5	13.4	.0776	-4.3	.7261	12.15	78.10
33	259.9	21.9	13.9	.0992	-3.8	.9261	13.20	77.38
34	330.0	23.4	14.6	.1260	-3.1	1.1761	14.11	76.46
35	400.2	24.9	15.1	.1527	-2.7	1.4261	15.21	75.86
36	470.3	26.5	15.6	.1795	-2.1	1.6761	15.96	75.06
37	540.5	28.0	16.0	.2062	-1.7	1.9261	16.87	74.51
38	660.8	30.6	16.7	.2598	-1.0	2.4261	18.42	73.52
39	821.1	32.6	17.3	.3133	-.4	2.9261	19.67	72.65
40	961.4	33.3	17.6	.3668	-.1	3.4261	20.07	72.26
41	1101.7	33.3	17.7	.4204	-.0	3.9261	20.10	72.14

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00376 DELH = .163 REH = 181.0
V RUN = 101371-2 CF/2 = .00228 DELM = .321 REM = 587.0
PLATE = 1 UINF = 29.7 DEL2 = .0120 DEL3 = .336
X(IN) = 2.00 GH = 5.168 THETA = .0387 DEL4 = 1.735
K(E06) = -.4540 GAM = -.421 BETA = .151 M = 1.633

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T
1	.0	0.0	.0	0.0000	-12.4	0.0000	0.00	91.38
2	2.8	3.6	2.1	.0120	-10.4	.0041	9.19	87.56
3	3.5	4.1	2.6	.0149	-9.8	.0051	9.87	86.47
4	4.2	4.5	3.1	.0178	-9.3	.0061	6.58	85.46
5	4.9	5.1	3.7	.0209	-8.7	.0071	7.34	84.40
6	5.6	5.6	4.2	.0237	-8.2	.0081	8.10	83.54
7	6.2	6.1	4.7	.0266	-7.8	.0091	8.81	82.65
8	6.9	6.5	5.1	.0295	-7.4	.0101	9.48	81.91
9	7.6	7.0	5.4	.0324	-7.0	.0111	10.14	81.19
10	8.3	7.4	5.9	.0354	-6.6	.0121	10.78	80.54
11	9.0	7.9	6.1	.0383	-6.3	.0131	11.40	79.97
12	10.4	8.5	6.6	.0441	-5.8	.0151	12.27	78.99
13	11.7	9.0	7.1	.0500	-5.3	.0171	13.09	78.10
14	13.1	9.6	7.5	.0558	-4.9	.0191	13.95	77.29
15	14.5	10.1	8.0	.0616	-4.4	.0211	14.61	76.49
16	15.8	10.5	8.3	.0675	-4.2	.0231	15.25	75.99
17	17.2	10.8	8.5	.0733	-3.9	.0251	15.68	75.56
18	20.0	11.3	8.9	.0850	-3.5	.0291	16.32	74.78
19	22.7	11.9	9.3	.0967	-3.1	.0331	17.04	74.06
20	26.1	12.3	9.7	.1112	-2.7	.0381	17.92	73.34
21	29.6	12.8	10.0	.1258	-2.4	.0431	18.54	72.74
22	33.0	13.1	10.2	.1404	-2.2	.0481	19.04	72.38
23	36.4	13.4	10.5	.1550	-2.0	.0531	19.48	71.87
24	43.7	14.0	10.9	.1842	-1.6	.0631	20.34	71.15
25	50.1	14.6	11.1	.2134	-1.3	.0731	21.12	70.61
26	60.4	15.2	11.5	.2572	-.9	.0881	22.06	69.92
27	77.6	16.2	11.9	.3302	-.5	.1131	23.51	69.16
28	94.7	17.1	12.2	.4031	-.3	.1381	24.75	68.74
29	111.9	17.8	12.3	.4761	-.1	.1631	25.81	68.46
30	129.0	18.4	12.4	.5491	-.1	.1881	26.70	68.34
31	146.2	19.0	12.4	.6220	-.0	.2131	27.52	68.25
32	180.5	19.9	12.4	.7680	-.0	.2631	28.85	68.24
33	214.7	20.3	12.4	.9139	-.0	.3131	29.37	68.24
34	248.3	20.4	12.4	1.0228	-.0	.3504	29.59	68.24
35	267.3	20.5	12.4	1.1795	-.0	.3904	29.69	68.24
36	299.8	20.5	12.4	1.2709	-.0	.4354	29.71	68.24
37	332.9	20.5	12.4	1.4168	-.0	.4854	29.71	68.24

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00231 DELH = .549 REH = 699.0
V RUN = 101371-2 CF/2 = .00152 DELM = .577 REM = 1198.0
PLATE = 3 UINF = 26.9 DEL2 = .0510 DEL3 = 1.598
X(IN) = 10.00 GH = 5.668 THETA = .0874 DEL4 = 8.957
K(E06) = -.8550 GAM = -1.376 BETA = 1.100 M = 1.745

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.5	0.0000	0.00	91.37	1.000	1.000
2	2.4	3.2	1.9	.0030	-14.9	.0048	3.52	89.15	1.238	1.086
3	2.9	3.6	2.2	.0036	-14.5	.0058	3.87	88.54	1.264	1.109
4	3.4	4.0	2.5	.0042	-14.0	.0068	4.32	87.86	1.294	1.135
5	3.9	4.5	3.0	.0048	-13.5	.0078	4.81	87.15	1.327	1.161
6	4.4	5.0	3.5	.0054	-13.0	.0088	5.31	86.52	1.360	1.186
7	4.9	5.4	4.0	.0061	-12.5	.0098	5.77	85.88	1.391	1.209
8	5.5	5.7	4.4	.0067	-12.1	.0108	6.13	85.29	1.416	1.231
9	6.0	6.0	4.9	.0073	-11.7	.0118	6.44	84.72	1.438	1.252
10	6.5	6.3	5.1	.0079	-11.4	.0128	6.72	84.25	1.459	1.270
11	7.5	6.9	5.7	.0092	-10.8	.0148	7.35	83.48	1.505	1.299
12	8.5	7.5	6.2	.0104	-10.3	.0168	8.00	82.80	1.548	1.324
13	9.5	7.9	6.6	.0116	-9.9	.0188	8.51	82.17	1.585	1.347
14	10.5	8.2	7.0	.0129	-9.5	.0208	8.94	81.61	1.617	1.367
15	11.5	8.7	7.4	.0141	-9.1	.0228	9.33	81.08	1.647	1.386
16	14.1	9.5	8.1	.0172	-8.4	.0278	10.20	80.09	1.712	1.422
17	16.6	10.2	8.7	.0203	-7.8	.0328	11.00	79.29	1.772	1.449
18	19.1	10.8	9.1	.0234	-7.3	.0378	11.62	78.69	1.819	1.469
19	21.7	11.2	9.4	.0265	-7.1	.0428	12.04	78.34	1.851	1.482
20	24.2	11.6	9.8	.0296	-6.7	.0478	12.40	77.83	1.877	1.495
21	29.3	12.2	10.2	.0358	-6.2	.0578	13.04	77.17	1.921	1.511
22	34.9	12.9	10.8	.0451	-5.6	.0728	13.96	76.34	1.969	1.518
23	49.6	13.9	11.5	.0606	-5.0	.0978	14.92	75.35	2.002	1.504
24	62.2	14.8	12.1	.0761	-4.3	.1228	15.74	74.54	1.997	1.465
25	74.9	15.6	12.7	.0916	-3.8	.1478	16.66	73.82	1.957	1.409
26	87.6	16.3	13.1	.1071	-3.4	.1728	17.41	73.25	1.889	1.345
27	100.3	17.0	13.4	.1225	-3.0	.1978	18.18	72.71	1.809	1.269
28	112.9	17.7	13.9	.1380	-2.6	.2228	18.91	72.17	1.711	1.181
29	139.3	19.0	14.5	.1690	-2.0	.2728	20.34	71.30	1.507	1.001
30	163.6	20.3	15.0	.2000	-1.5	.3228	21.74	70.55	1.291	.805
31	189.0	21.6	15.4	.2310	-1.0	.3729	23.09	69.94	1.132	.612
32	214.3	22.7	15.8	.2619	-.7	.4228	24.34	69.43	1.028	.425
33	239.7	23.7	16.1	.2929	-.4	.4728	25.36	69.04	.923	.264
34	265.1	24.4	16.3	.3239	-.2	.5228	26.14	68.76	.807	.137
35	315.9	25.1	16.5	.3858	.0	.6228	26.85	68.49	.405	.000
36	366.6	25.1	16.5	.4478	.0	.7229	26.92	68.46	.000	.000
37	417.2	25.1	16.5	.5098	.0	.8228	26.91	68.46	.000	.000

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00161 DELH = 1.044 REH = 1324.0
V RUN = 101371-2 CF/2 = .00103 DELM = 1.038 REM = 2048.0
PLATE = 6 UINF = 24.4 DEL2 = .1063 DEL3 = 3.338
X(IN) = 22.00 GH = 5.595 THETA = .1645 DEL4 = 19.675
K(E06) = -.4770 GAM = -1.250 BETA = 1.540 M = 1.791

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.2	0.0000	0.00	91.13	1.000	1.000
2	1.4	1.6	1.0	.0011	-16.2	.0038	1.26	90.89	1.123	1.061
3	1.9	2.0	1.3	.0014	-15.9	.0048	1.61	89.48	1.157	1.081
4	2.2	2.5	1.6	.0017	-15.7	.0058	1.98	89.16	1.192	1.097
5	2.6	2.9	1.9	.0020	-15.3	.0068	2.35	88.68	1.227	1.120
6	2.9	3.4	2.2	.0023	-14.9	.0078	2.72	88.21	1.291	1.143
7	3.3	3.9	2.6	.0026	-14.6	.0088	3.08	87.74	1.350	1.166
8	4.1	4.7	3.2	.0032	-14.0	.0108	3.75	86.91	1.407	1.207
9	4.9	5.6	3.9	.0038	-13.3	.0128	4.45	86.06	1.458	1.249
10	5.6	6.3	4.5	.0043	-12.7	.0148	5.04	85.27	1.515	1.290
11	6.4	6.9	4.9	.0049	-12.2	.0168	5.54	84.64	1.565	1.319
12	7.1	7.5	5.4	.0055	-11.8	.0188	5.97	84.10	1.608	1.346
13	7.9	7.9	5.9	.0061	-11.4	.0208	6.34	83.57	1.647	1.371
14	9.4	8.7	6.5	.0073	-10.7	.0248	6.97	82.65	1.718	1.416
15	10.9	9.4	7.0	.0084	-10.1	.0288	7.54	81.88	1.780	1.453
16	12.8	9.9	7.5	.0099	-9.7	.0338	7.94	81.26	1.835	1.482
17	14.7	10.3	8.0	.0114	-9.1	.0388	8.24	80.57	1.878	1.514
18	16.6	10.6	8.5	.0128	-8.7	.0438	8.47	80.04	1.916	1.539
19	18.5	11.2	8.7	.0143	-8.5	.0488	8.82	79.74	1.973	1.553
20	22.3	12.1	9.2	.0172	-7.9	.0588	9.69	79.02	2.075	1.583
21	26.0	12.8	9.6	.0202	-7.5	.0688	10.20	78.52	2.153	1.602
22	35.6	13.8	10.4	.0275	-6.8	.0938	11.07	77.60	2.297	1.635
23	45.0	14.7	10.9	.0349	-6.4	.1188	11.73	77.03	2.402	1.656
24	63.9	15.8	11.6	.0495	-5.8	.1688	12.66	75.89	2.558	1.647
25	82.9	17.0	12.2	.0642	-5.0	.2188	13.58	75.17	2.658	1.628
26	101.8	18.0	12.7	.0788	-4.5	.2688	14.36	74.52	2.702	1.596
27	120.8	19.1	13.1	.0935	-4.0	.3188	15.25	73.92	2.714	1.548
28	139.7	20.0	13.6	.1082	-3.6	.3688	16.02	73.32	2.665	1.485
29	158.6	21.1	14.0	.1229	-3.2	.4188	16.97	72.61	2.576	1.416
30	196.5	22.8	14.7	.1522	-2.5	.5188	18.22	71.91	2.202	1.250
31	234.4	24.7	15.3	.1816	-1.9	.6188	19.74	71.12	1.849	1.054
32	272.3	26.4	15.8	.2109	-1.4	.7188	21.14	70.44	1.535	.828
33	310.2	28.1	16.2	.2402	-.9	.8188	22.44	69.80	1.318	.598
34	348.1	29.4	16.7	.2696	-.5	.9188	23.49	69.25	1.116	.356
35	385.9	30.2	17.0	.2989	-.2	1.0188	24.12	68.86	.817	.160
36	423.8	30.5	17.1	.3283	-.1	1.1188	24.36	68.69	.377	.057
37	461.7	30.5	17.2	.3576	.0	1.2188	24.41	68.59	.000	.000
38	499.6	30.5	17.2	.3870	.0	1.3188	24.40	68.59	.000	.000
39	537.5	30.5	17.2	.4163	.0	1.4188	24.40	68.59	.000	.000

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00161 DELH = 1.512 REH = 1939.0
V RUN = 101371-2 CF/2 = .00078 DELM = 1.503 REM = 2914.0
PLATE = 9 UINF = 23.1 DEL2 = .1557 DEL3 = 4.799
X(IN) = 34.00 GH = 5.431 THETA = .2385 DEL4 = 28.067
K(E06) = -.3420 GAM = -1.232 BETA = 2.015 M = 1.791

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.0	0.0000	0.00	91.03	1.000	1.000
2	1.3	1.5	1.0	.0009	-16.0	.0043	.98	89.71	1.132	1.074
3	1.7	1.9	1.2	.0011	-15.8	.0053	1.22	89.42	1.165	1.090
4	2.0	2.2	1.5	.0013	-15.5	.0063	1.47	89.10	1.198	1.108
5	2.3	2.6	1.7	.0015	-15.3	.0073	1.73	88.80	1.232	1.125
6	2.6	3.0	2.0	.0017	-15.0	.0083	1.98	88.42	1.266	1.147
7	2.9	3.4	2.2	.0019	-14.8	.0093	2.24	88.09	1.300	1.165
8	3.5	4.2	2.8	.0023	-14.2	.0113	2.75	87.33	1.367	1.209
9	4.2	4.9	3.3	.0027	-13.7	.0133	3.23	86.65	1.432	1.246
10	4.8	5.6	3.9	.0031	-13.1	.0152	3.68	85.95	1.516	1.291
11	5.4	6.2	4.4	.0035	-12.6	.0173	4.10	85.26	1.565	1.324
12	6.0	6.8	4.7	.0040	-12.2	.0193	4.48	84.78	1.607	1.351
13	6.7	7.3	5.2	.0044	-11.8	.0213	4.83	84.19	1.648	1.384
14	7.3	7.8	5.4	.0048	-11.5	.0233	5.16	83.84	1.697	1.403
15	8.5	8.8	6.1	.0056	-10.9	.0273	5.77	83.01	1.797	1.449
16	10.1	9.8	6.6	.0066	-10.4	.0323	6.43	82.32	1.894	1.485
17	11.6	10.4	7.1	.0076	-9.9	.0373	6.83	81.67	1.961	1.524
18	13.2	10.8	7.5	.0086	-9.5	.0423	7.14	81.14	2.017	1.553
19	16.3	12.1	8.1	.0107	-8.9	.0523	7.98	80.30	2.151	1.598
20	21.0	13.1	9.0	.0137	-8.2	.0673	9.64	79.41	2.284	1.644
21	28.8	14.4	9.4	.0188	-7.6	.0923	9.48	78.61	2.465	1.683
22	36.6	15.1	10.0	.0239	-7.0	.1173	9.92	77.96	2.591	1.713
23	44.4	15.7	10.4	.0291	-6.5	.1423	10.37	77.21	2.715	1.734
24	60.0	17.1	10.7	.0393	-6.2	.1923	11.29	76.85	2.950	1.744
25	67.8	17.6	11.0	.0444	-5.9	.2173	11.58	76.46	3.035	1.750
26	83.5	18.4	11.5	.0546	-5.5	.2673	12.11	75.83	3.189	1.753
27	99.1	19.4	12.1	.0648	-4.9	.3173	12.78	75.09	3.345	1.742
28	114.7	20.2	12.4	.0750	-4.6	.3673	13.31	74.67	3.476	1.728
29	130.3	20.9	12.7	.0852	-4.3	.4172	13.74	74.25	3.580	1.707
30	161.5	22.6	13.3	.1056	-3.7	.5173	14.86	73.47	3.569	1.639
31	192.7	24.0	13.8	.1260	-3.1	.6173	15.88	72.75	3.501	1.547
32	223.9	25.6	14.3	.1464	-2.7	.7173	16.84	72.12	3.355	1.436
33	255.2	27.2	14.7	.1668	-2.2	.8172	17.94	71.55	3.133	1.305
34	286.4	28.7	15.2	.1872	-1.8	.9173	18.91	70.98	2.866	1.165
35	345.8	31.4	15.8	.2260	-1.1	1.1173	20.72	70.10	1.955	.828
36	411.3	33.7	16.4	.2689	-.5	1.3173	22.18	69.29	1.356	.446
37	473.7	34.8	16.8	.3097	-.1	1.5173	22.92	68.77	.743	.135
38	536.2	35.1	17.0	.3505	.0	1.7173	23.11	68.59	.156	.000
39	598.6	35.1	17.0	.3913	.0	1.9173	23.11	68.56	.000	.000

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00147 DELM = 2.006 REM = 2314.0
V RUN = 101371-2 CF/2 = .00071 DELM = 1.941 REM = 3827.0
PLATE = 12 UINF = 22.2 DEL2 = .2047 DEL3 = 6.520
X(IN) = 46.00 GM = 5.500 THETA = .3120 DEL4 = 35.961
K(E06) = -.2660 GAM = -1.214 BETA = 2.174 M = 1.778

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.8	0.0000	0.00	90.82	1.000	1.000
2	1.2	1.3	.9	.0006	-17.0	.0041	.78	89.83	1.119	1.061
3	1.5	1.6	1.1	.0007	-16.8	.0051	.98	89.57	1.148	1.077
4	1.7	2.0	1.3	.0009	-16.5	.0061	1.19	89.24	1.179	1.095
5	2.0	2.3	1.5	.0010	-16.3	.0071	1.40	89.01	1.210	1.112
6	2.3	2.7	1.7	.0012	-16.1	.0081	1.62	88.68	1.242	1.132
7	2.9	3.4	2.3	.0015	-15.5	.0101	2.05	87.95	1.306	1.177
8	3.5	4.1	2.7	.0018	-15.0	.0121	2.48	87.39	1.370	1.212
9	4.0	4.8	3.2	.0021	-14.6	.0141	2.89	86.82	1.443	1.247
10	4.6	5.4	3.8	.0024	-14.0	.0161	3.28	86.06	1.506	1.294
11	5.8	6.6	4.6	.0030	-13.2	.0201	3.97	85.05	1.595	1.356
12	6.9	7.6	5.2	.0036	-12.5	.0241	4.58	84.28	1.694	1.403
13	8.1	8.6	5.8	.0042	-12.0	.0281	5.19	83.60	1.793	1.445
14	9.5	9.4	6.3	.0049	-11.4	.0331	5.70	82.89	1.878	1.485
15	10.9	10.1	6.9	.0057	-10.8	.0381	6.10	82.19	1.947	1.533
16	13.8	11.2	7.7	.0072	-10.0	.0481	6.75	81.11	2.067	1.595
17	16.6	11.8	8.4	.0087	-9.4	.0581	7.15	80.23	2.152	1.645
18	19.5	12.6	8.7	.0102	-9.0	.0681	7.61	79.86	2.245	1.670
19	26.7	14.1	9.5	.0139	-8.3	.0931	8.51	79.01	2.434	1.726
20	33.9	14.9	9.9	.0177	-7.8	.1181	9.02	78.34	2.576	1.757
21	41.0	15.5	10.5	.0215	-7.2	.1431	9.34	77.63	2.684	1.789
22	48.2	16.0	10.7	.0252	-7.0	.1681	9.64	77.36	2.788	1.801
23	62.5	17.2	11.1	.0327	-6.6	.2181	10.38	76.85	3.039	1.825
24	76.8	18.1	11.6	.0402	-6.1	.2681	10.91	76.19	3.190	1.850
25	91.1	18.8	12.2	.0477	-5.8	.3181	11.35	75.57	3.345	1.865
26	119.5	20.0	12.7	.0628	-5.1	.4181	12.05	74.94	3.597	1.970
27	148.4	21.7	13.1	.0778	-4.7	.5181	13.08	74.37	3.929	1.952
28	205.7	24.1	14.1	.1078	-3.7	.7181	14.57	73.14	3.992	1.751
29	263.0	26.7	14.8	.1379	-3.0	.9181	16.12	72.24	3.877	1.608
30	334.6	29.7	15.6	.1755	-2.1	1.1681	17.94	71.19	3.306	1.336
31	406.2	32.4	16.4	.2130	-1.4	1.4181	19.59	70.25	2.356	.989
32	477.8	34.9	17.0	.2506	-.8	1.6681	21.06	69.47	1.530	.615
33	549.4	36.4	17.5	.2881	-.3	1.9181	21.96	68.87	.977	.252
34	621.0	36.8	17.7	.3257	-.1	2.1681	22.21	68.57	.238	.030
35	692.6	36.8	17.8	.3633	-.0	2.4181	22.21	68.54	.000	.000
36	764.2	36.8	17.8	.4009	-.0	2.6681	22.22	68.54	.000	.000
37	835.8	36.8	17.8	.4384	-.0	2.9181	22.22	68.54	.000	.002

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00137 DELM = 2.476 REM = 2762.0
V RUN = 101371-2 CF/2 = .00066 DELM = 2.274 REM = 4172.0
PLATE = 19 UINF = 21.4 DEL2 = .2529 DEL3 = 9.232
X(IN) = 56.00 GM = 5.582 THETA = .3521 DEL4 = 45.956
K(E06) = -.2220 GAM = -1.211 BETA = 2.261 M = 1.769

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-19.4	0.0000	0.00	90.54	1.000	1.000
2	1.5	1.7	1.1	.0007	-17.2	.0056	.93	89.19	1.134	1.081
3	1.8	2.0	1.3	.0008	-17.0	.0066	1.11	88.95	1.163	1.107
4	2.0	2.3	1.5	.0009	-16.8	.0076	1.25	88.71	1.213	1.123
5	2.3	2.6	1.7	.0010	-16.6	.0086	1.48	88.45	1.247	1.140
6	2.8	3.3	2.2	.0013	-16.2	.0106	1.85	87.92	1.304	1.176
7	3.4	4.0	2.6	.0015	-15.7	.0126	2.22	87.38	1.365	1.213
8	3.9	4.6	3.0	.0018	-15.3	.0146	2.59	86.91	1.424	1.244
9	4.4	5.2	3.5	.0020	-14.8	.0166	2.93	86.29	1.441	1.285
10	5.5	6.3	4.5	.0025	-13.9	.0206	3.56	85.11	1.555	1.364
11	6.5	7.3	5.2	.0029	-13.2	.0246	4.09	84.34	1.672	1.415
12	7.6	8.1	5.7	.0034	-12.7	.0286	4.54	83.72	1.767	1.457
13	8.9	9.1	6.4	.0040	-11.9	.0336	5.11	82.80	1.867	1.518
14	10.3	10.0	6.9	.0046	-11.5	.0386	5.63	82.10	1.952	1.552
15	11.6	10.6	7.4	.0052	-11.0	.0436	5.98	81.67	2.011	1.594
16	12.9	11.1	7.7	.0058	-10.7	.0486	6.21	81.35	2.065	1.615
17	15.6	12.1	8.3	.0070	-10.1	.0586	6.78	80.57	2.179	1.667
18	18.3	12.7	8.9	.0082	-9.5	.0686	7.13	79.99	2.259	1.711
19	24.9	14.0	9.6	.0112	-8.5	.0936	7.94	79.06	2.435	1.765
20	31.6	14.9	10.2	.0141	-8.2	.1186	8.35	78.31	2.576	1.812
21	38.3	15.5	10.4	.0171	-8.0	.1436	8.67	77.10	2.649	1.823
22	44.9	16.1	10.7	.0201	-7.7	.1686	9.03	77.72	2.804	1.846
23	58.2	17.3	11.3	.0260	-7.0	.2186	9.71	76.97	3.024	1.879
24	71.6	18.2	11.9	.0320	-6.4	.2686	10.19	76.25	3.210	1.907
25	84.9	18.8	12.1	.0379	-6.2	.3186	10.61	76.01	3.368	1.918
26	111.5	20.1	12.6	.0498	-5.7	.4186	11.27	75.38	3.659	1.921
27	138.2	21.2	13.1	.0617	-5.2	.5186	11.84	74.76	3.853	1.904
28	191.4	23.4	14.0	.0855	-4.4	.7186	13.10	73.77	4.197	1.861
29	244.7	25.6	14.7	.1093	-3.7	.9186	14.35	72.90	4.255	1.769
30	309.0	27.7	15.3	.1331	-3.0	1.1186	15.54	72.15	4.227	1.642
31	351.3	29.6	15.8	.1570	-2.5	1.3186	16.62	71.52	3.914	1.494
32	404.6	31.7	16.4	.1808	-1.9	1.5186	17.77	70.80	3.435	1.271
33	457.9	33.6	16.9	.2046	-1.5	1.7186	18.83	70.26	2.774	1.065
34	511.1	35.2	17.3	.2284	-1.0	1.9186	19.75	69.74	2.022	.816
35	577.7	36.9	17.8	.2581	-.5	2.1686	20.72	69.14	1.238	.473
36	644.3	37.9	18.2	.2879	-.2	2.4186	21.27	68.75	.647	.212
37	710.9	38.2	18.3	.3176	-.0	2.6686	21.42	68.54	.177	.050
38	777.5	38.2	18.4	.3474	.0	2.9186	21.44	68.48	.000	.000
39	828.7	38.2	18.4	.3703	.0	3.1105	21.44	68.48	.000	.084

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00130 DELM = 2.905 REM = 3156.0
V RUN = 101371-2 CF/2 = .00062 DELM = 2.624 REM = 4823.0
PLATE = 18 UINF = 20.9 DEL2 = .2990 DEL3 = 9.845
X(IN) = 70.00 GM = 5.601 THETA = .4529 DEL4 = 55.218
K(E06) = -.1590 GAM = -1.210 BETA = 2.401 M = 1.754

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-18.8	0.0000	0.00	90.54	1.000	1.000
2	1.4	1.6	1.0	.0006	-17.7	.0056	.84	89.33	1.147	1.084
3	1.7	1.9	1.2	.0007	-17.6	.0066	1.00	89.13	1.175	1.099
4	1.9	2.2	1.4	.0008	-17.3	.0076	1.16	88.87	1.204	1.119
5	2.2	2.5	1.6	.0009	-17.1	.0086	1.32	88.62	1.232	1.134
6	2.7	3.1	2.0	.0011	-16.7	.0106	1.66	88.15	1.291	1.166
7	3.2	3.8	2.6	.0012	-16.2	.0126	1.99	87.47	1.349	1.214
8	3.7	4.4	3.0	.0014	-15.7	.0146	2.32	86.97	1.406	1.249
9	4.7	5.5	3.9	.0018	-14.9	.0186	2.94	85.94	1.515	1.320
10	6.0	6.8	4.7	.0023	-14.1	.0236	3.61	85.02	1.634	1.384
11	7.2	7.8	5.7	.0028	-13.1	.0286	4.15	83.84	1.737	1.466
12	8.5	8.7	6.3	.0033	-12.5	.0336	4.61	83.10	1.835	1.518
13	9.7	9.5	6.7	.0038	-12.0	.0386	5.03	82.59	1.912	1.553
14	12.3	11.0	7.6	.0048	-11.2	.0486	5.83	81.61	2.061	1.620
15	14.8	12.1	8.2	.0058	-10.6	.0586	6.42	80.90	2.153	1.668
16	17.3	12.8	8.9	.0068	-9.9	.0686	6.90	80.07	2.272	1.724
17	22.4	14.0	9.5	.0088	-9.3	.0886	7.41	79.35	2.423	1.772
18	25.7	14.9	10.0	.0113	-8.7	.1136	7.91	74.73	2.567	1.812
19	35.0	15.5	10.6	.0138	-8.2	.1386	8.23	78.04	2.682	1.851
20	41.3	16.0	10.6	.0162	-8.2	.1636	8.49	78.04	2.786	1.852
21	47.6	16.5	10.9	.0187	-7.8	.1886	8.78	77.66	2.891	1.874
22	60.2	17.7	11.5	.0237	-7.3	.2386	9.38	77.00	3.102	1.910
23	72.8	18.8	11.9	.0287	-6.9	.2886	9.97	76.52	3.307	1.929
24	85.4	19.2	12.1	.0336	-6.6	.3386	10.21	76.25	3.439	1.932
25	110.6	19.7	12.8	.0436	-6.0	.4386	10.48	75.51	3.642	1.940
26	135.8	21.2	13.1	.0535	-5.6	.5386	11.25	75.06	3.947	1.941
27	186.3	23.0	14.0	.0734	-4.8	.7386	12.23	74.04	4.332	1.907
28	236.7	24.9	14.5	.0933	-4.2	.9386	13.22	73.41	4.551	1.872
29	299.8	27.4	15.3	.1181	-3.4	1.1886	14.57	72.45	4.654	1.754
30	362.8	29.5	15.9	.1430	-2.9	1.4386	15.69	71.79	4.372	1.630
31	425.9	31.8	16.5	.1678	-2.3	1.6886	16.87	71.07	3.947	1.434
32	488.9	33.8	17.1	.1927	-1.7	1.9386	17.96	70.41	3.264	1.192
33	552.0	35.6	17.5	.2175	-1.3	2.1886	18.92	69.90	2.397	.962
34	615.0	37.5	18.0	.2424	-.8	2.4386	19.98	69.35	1.682	.666
35	678.1	38.7	18.4	.2672	-.4	2.6886	20.54	68.90	.986	.380
36	741.1	39.2	18.6	.2928	-.2	2.9386	20.85	68.60	.434	.164
37	804.2	39.4	18.7	.3169	-.0	3.1886	20.93	68.45	.090	.039
38	867.3	39.4	18.8	.3417	-.0	3.4386	20.92	68.42	.000	.000
39	910.2	39.4	18.8	.3587	-.0	3.6090	20.93	68.42	.000	.000

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00124 DELM = 3.261 REM = 3616.0
V RUN = 101371-2 CF/2 = .00058 DELM = 3.069 REM = 5499.0
PLATE = 21 UINF = 20.5 DEL2 = .3462 DEL3 = 11.452
X(IN) = 82.00 GM = 5.627 THETA = .5266 DEL4 = 64.552
K(E06) = -.1650 GAM = -1.247 BETA = 2.554 M = 1.728

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-19.0	0.0000	0.00	90.36	1.000	1.000
2	1.2	1.3	.9	.0004	-18.8	.0049	.65	89.16	1.125	1.085
3	1.4	1.6	1.0	.0005	-17.9	.0059	.79	89.04	1.152	1.097
4	1.7	1.9	1.2	.0006	-17.8	.0069	.94	88.89	1.180	1.105
5	1.9	2.2	1.4	.0006	-17.7	.0079	1.08	88.71	1.208	1.118
6	2.1	2.4	1.6	.0007	-17.4	.0089	1.23	88.46	1.236	1.137
7	2.4	2.7	1.9	.0008	-17.1	.0099	1.38	88.12	1.269	1.162
8	2.9	3.4	2.2	.0010	-16.8	.0119	1.69	87.74	1.327	1.190
9	3.3	4.0	2.6	.0012	-16.4	.0139	1.99	87.24	1.350	1.227
10	3.8	4.5	3.0	.0013	-16.0	.0159	2.29	86.92	1.437	1.259
11	4.8	5.6	4.0	.0017	-15.0	.0199	2.85	85.67	1.543	1.344
12	5.7	6.6	4.6	.0020	-14.4	.0239	3.37	84.99	1.638	1.394
13	6.7	7.5	5.1	.0024	-13.7	.0279	3.76	84.19	1.709	1.454
14	7.6	8.2	5.9	.0027	-13.2	.0319	4.12	83.54	1.825	1.503
15	8.8	9.0	6.5	.0031	-12.5	.0369	4.52	82.80	1.876	1.553
16	11.2	10.7	7.1	.0040	-11.9	.0469	5.41	82.09	2.062	1.612
17	13.6	12.0	7.9	.0048	-11.1	.0569	6.05	81.17	2.203	1.679
18	19.6	13.7	9.2	.0070	-9.9	.0819	6.90	79.74	2.421	1.781
19	25.6	14.7	9.8	.0091	-9.2	.1069	7.41	78.94	2.573	1.834
20	31.6	15.6	10.2	.0113	-8.9	.1319	7.84	78.52	2.711	1.862
21	43.5	16.8	10.4	.0155	-8.2	.1819	8.48	77.81	2.945	1.912
22	55.5	17.8	11.4	.0198	-7.6	.2319	8.97	77.15	3.141	1.960
23	67.5	18.6	11.9	.0241	-7.2	.2819	9.38	76.64	3.312	1.992
24	79.5	19.2	12.3	.0284	-7.0	.3319	9.67	76.43	3.462	2.006
25	103.4	20.1	12.6	.0369	-6.5	.4319	10.13	75.74	3.759	2.035
26	127.3	21.3	13.1	.0455	-5.9	.5319	10.74	75.19	4.045	2.043
27	151.3	22.4	13.3	.0540	-5.7	.6319	11.26	74.91	4.220	2.041
28	175.2	23.1	13.9	.0626	-5.3	.7319	11.61	74.40	4.368	2.024
29	223.1	24.8	14.4	.0797	-4.6	.9319	12.48	73.62	4.644	1.971
30	282.9	27.1	15.1	.1011	-3.9	1.1819	13.63	72.81	4.791	1.899
31	342.8	28.7	15.7	.1225	-3.4	1.4319	14.45	72.21	4.709	1.843
32	402.6	30.9	16.3	.1439	-2.8	1.6819	15.58	71.52	4.623	1.740
33	462.5	32.8	16.7	.1652	-2.4	1.9319	16.51	71.04	4.124	1.656
34	522.3	34.6	17.2	.1866	-1.8	2.1819	17.44	70.41	3.508	1.510
35	582.2	36.3	17.6	.2080	-1.4	2.4319	18.26	69.96	2.570	1.204
36	642.1	37.6	18.0	.2294	-1.0	2.6819	19.07	69.48	1.577	.982
37	701.9	39.1	18.4	.2508	-.7	2.9319	19.68	69.06	.949	.760
38	761.8	40.0	18.7	.2722	-.4	3.1819	20.16	68.72	.434	.486
39	821.6	40.5	18.9	.2936	-.2	3.4319	20.48	68.48	.095	.252
40	881.5	40.6	19.0	.3150	-.1	3.6819	20.48	68.36	.000	.105
41	941.3	40.7	19.0	.3364	-.0	3.9319	20.50	68.33	.000	.000
42	1003.9	40.7	19.0	.3766	-.0	4.4022	20.50	68.33	.000	.080

DATE = 101571 (-0.15, 0.002)

T RUN = 101571-2 STNA = .00120 DELH = 3.806 REM = 3966.0
V RUN = 101371-2 CF/2 = .00357 DELM = 3.614 REM = 5904.0
PLATE = 23 UINF = 20.1 DEL2 = .3955 DEL3 = 12.919
X(IN) = 90.00 GM = 5.679 THETA = .5737 DEL4 = 73.371
K(E06) = -.1590 GAM = -1.293 BETA = 2.499 H = 1.726

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-19.5	0.0000	0.00	90.23
2	1.3	1.5	1.0	.0304	-15.6	.0056	.71	89.19
3	1.5	1.7	1.1	.0305	-18.3	.0066	.85	88.92
4	1.8	2.0	1.3	.0006	-15.2	.0076	.99	88.74
5	2.0	2.3	1.5	.0006	-14.1	.0086	1.17	88.60
6	2.2	2.6	1.8	.0007	-17.7	.0096	1.28	88.21
7	2.7	3.2	2.1	.0009	-17.4	.0116	1.57	87.83
8	3.2	3.8	2.5	.0010	-17.0	.0136	1.86	87.42
9	3.6	4.4	3.1	.0012	-16.4	.0156	2.15	86.74
10	4.1	4.9	3.6	.0013	-15.9	.0176	2.42	86.17
11	5.0	6.0	4.2	.0016	-15.3	.0216	2.93	85.49
12	6.0	6.9	5.0	.0019	-14.5	.0256	3.38	84.58
13	7.1	7.9	5.7	.0023	-13.8	.0296	3.85	83.72
14	9.4	9.4	7.0	.0031	-12.5	.0376	4.59	82.24
15	10.6	9.9	7.2	.0034	-12.3	.0456	4.97	82.09
16	12.9	11.1	7.9	.0042	-11.6	.0555	5.46	81.29
17	15.3	12.3	8.4	.0050	-11.1	.0656	6.05	80.66
18	17.6	13.3	9.0	.0057	-10.5	.0756	6.52	79.95
19	23.4	14.3	9.6	.0076	-9.9	.1006	6.98	79.27
20	29.2	15.2	10.2	.0095	-9.3	.1256	7.46	78.67
21	40.9	16.7	11.0	.0133	-8.5	.1756	8.16	77.72
22	52.5	17.4	11.5	.0171	-8.0	.2256	8.50	77.14
23	64.2	18.1	12.0	.0209	-7.5	.2756	8.89	76.52
24	75.8	19.1	12.1	.0247	-7.4	.3256	9.35	76.40
25	99.1	20.1	12.5	.0323	-6.7	.4256	9.94	75.63
26	122.4	20.9	13.1	.0398	-6.4	.5256	10.22	75.30
27	169.9	22.6	13.8	.0550	-5.7	.7256	11.09	74.52
28	215.5	24.2	14.4	.0702	-5.0	.9256	11.85	73.77
29	273.7	26.0	15.2	.0891	-4.3	1.1756	12.76	72.96
30	331.9	28.2	15.8	.1081	-3.7	1.4256	13.91	72.24
31	390.1	29.9	16.3	.1270	-3.2	1.6755	14.66	71.64
32	448.3	31.6	16.9	.1460	-2.7	1.9255	15.50	71.07
33	506.5	33.5	17.2	.1650	-2.3	2.1756	16.40	70.62
34	564.7	34.9	17.6	.1839	-1.9	2.4256	17.12	70.20
35	622.9	36.7	18.0	.2029	-1.5	2.6756	18.00	69.72
36	681.1	38.3	18.5	.2218	-1.1	2.9256	18.78	69.21
37	739.3	39.5	18.7	.2408	-.8	3.1756	19.33	68.87
38	797.6	40.2	19.0	.2597	-.5	3.4256	19.71	68.57
39	855.8	40.8	19.2	.2787	-.3	3.6756	19.97	68.33
40	914.0	40.9	19.4	.2977	-.2	3.9256	20.03	68.18
41	1030.4	40.9	19.5	.3356	-.0	4.4256	20.03	68.03

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00280 DELH = .167 REM = 224.0
V RUN = 102171-1 CF/2 = .00194 DELM = .339 REM = 627.0
PLATE = 1 UINF = 29.6 DEL2 = .0148 DEL3 = .515
X(IN) = 2.00 GM = 6.419 THETA = .0414 DEL4 = 3.305
K(E06) = -.4550 GAM = -.404 BETA = .251 H = 1.706

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-15.4	0.0000	0.00	91.96
2	3.8	4.0	2.4	.0092	-13.0	.0048	5.33	88.42
3	3.7	4.5	3.0	.0111	-12.4	.0058	5.95	87.50
4	4.3	4.9	3.5	.0130	-11.9	.0068	6.51	86.77
5	4.9	5.3	4.2	.0149	-11.1	.0078	7.07	85.64
6	5.6	5.8	4.9	.0168	-10.6	.0088	7.69	84.78
7	6.2	6.2	5.4	.0187	-10.0	.0098	9.32	83.98
8	6.8	6.8	5.8	.0206	-9.6	.0108	9.03	83.30
9	7.5	7.3	6.3	.0225	-9.1	.0118	9.66	82.59
10	8.1	7.6	6.7	.0244	-8.7	.0128	10.14	81.97
11	8.7	7.9	7.0	.0263	-8.4	.0138	10.53	81.49
12	10.0	8.5	7.7	.0301	-7.7	.0158	11.38	80.54
13	11.3	9.2	8.2	.0339	-7.2	.0178	12.22	79.79
14	12.5	9.8	8.7	.0377	-6.7	.0198	12.65	79.05
15	13.8	10.2	9.1	.0415	-6.3	.0218	13.64	78.42
16	15.1	10.6	9.4	.0453	-5.9	.0238	14.10	77.89
17	16.3	10.9	9.8	.0491	-5.6	.0258	14.52	77.41
18	18.9	11.5	10.3	.0568	-5.1	.0298	15.26	76.57
19	21.4	11.9	10.8	.0644	-4.6	.0338	15.89	75.92
20	24.6	12.5	11.3	.0739	-4.1	.0388	16.66	75.20
21	27.7	12.9	11.7	.0834	-3.7	.0438	17.21	74.51
22	30.9	13.4	12.0	.0929	-3.4	.0488	17.78	74.03
23	34.0	13.7	12.1	.1024	-3.2	.0538	18.27	73.85
24	40.4	14.4	12.7	.1214	-2.7	.0638	19.14	73.04
25	46.7	14.9	13.1	.1405	-2.2	.0738	19.51	72.38
26	53.0	15.5	13.5	.1595	-1.9	.0838	20.60	71.81
27	59.4	16.0	13.8	.1795	-1.5	.0938	21.35	71.33
28	65.7	16.6	14.1	.1975	-1.3	.1038	22.05	70.91
29	78.3	17.5	14.6	.2356	-.8	.1238	23.26	70.24
30	90.2	18.5	14.9	.2831	-.5	.1488	24.60	69.70
31	110.0	19.3	15.2	.3307	-.2	.1738	25.71	69.36
32	125.8	20.0	15.3	.3782	-.1	.1988	26.67	69.15
33	141.6	20.6	15.4	.4256	-.1	.2238	27.48	69.09
34	173.3	21.5	15.4	.5209	-.0	.2738	28.64	69.02
35	204.9	22.0	15.4	.6160	-.0	.3239	29.29	69.02
36	213.4	22.1	15.4	.6416	-.0	.3373	29.35	69.02
37	241.9	22.2	15.4	.7272	-.0	.3823	29.56	69.02
38	273.6	22.2	15.4	.8223	-.0	.4323	29.60	69.02
39	321.0	22.2	15.4	.9650	-.0	.5073	29.60	69.02

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00165 DELH = .624 REM = 880.0
V RUN = 102171-1 CF/2 = .00073 DELM = .649 REM = 1440.0
PLATE = 3 UINF = 26.6 DEL2 = .0640 DEL3 = 2.075
X(IN) = 10.00 GM = 5.926 THETA = .1048 DEL4 = 12.294
K(E06) = -.8590 GAM = -1.361 BETA = 2.861 H = 1.900

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.0	0.0000	0.00	92.00	1.000	1.000
2	1.3	1.5	1.0	.0017	-15.1	.0035	1.12	90.69	1.289	1.190
3	1.6	2.0	1.3	.0022	-14.9	.0046	1.48	90.27	1.378	1.185
4	2.0	2.5	1.5	.0027	-14.5	.0056	1.85	89.83	1.471	1.232
5	2.3	3.0	1.9	.0032	-14.1	.0066	2.22	89.27	1.565	1.292
6	2.7	3.5	2.3	.0036	-13.8	.0075	2.61	88.77	1.660	1.345
7	3.0	4.0	2.6	.0041	-13.4	.0085	2.99	88.24	1.754	1.402
8	3.4	4.5	2.9	.0046	-13.1	.0095	3.36	87.80	1.872	1.449
9	3.7	5.0	3.4	.0050	-12.6	.0105	3.71	87.18	1.974	1.515
10	4.1	5.5	3.7	.0055	-12.3	.0115	4.04	86.68	2.060	1.569
11	4.8	6.3	4.3	.0065	-11.7	.0135	4.65	85.89	2.216	1.655
12	5.5	7.0	4.8	.0074	-11.2	.0155	5.15	85.14	2.377	1.734
13	6.2	7.7	5.2	.0083	-10.8	.0175	5.68	84.58	2.513	1.795
14	6.9	8.3	5.5	.0093	-10.5	.0196	6.15	84.07	2.636	1.850
15	7.6	8.9	5.5	.0102	-10.2	.0216	6.58	83.66	2.744	1.895
16	9.4	10.1	6.5	.0126	-9.5	.0266	7.49	82.71	2.991	1.998
17	11.1	11.1	7.0	.0149	-9.0	.0316	8.18	82.00	3.187	2.073
18	12.9	11.9	7.5	.0173	-8.6	.0366	8.77	81.34	3.354	2.142
19	14.7	12.6	7.9	.0197	-8.1	.0416	9.30	80.75	3.506	2.201
20	18.2	13.5	8.4	.0244	-7.6	.0516	9.96	80.03	3.699	2.271
21	21.7	14.3	8.8	.0291	-7.2	.0616	10.61	79.38	3.882	2.325
22	25.2	15.2	9.2	.0338	-6.8	.0716	11.27	78.87	4.056	2.361
23	28.7	15.8	9.5	.0385	-6.6	.0816	11.72	78.49	4.161	2.381
24	32.3	16.4	9.9	.0433	-6.1	.0916	12.30	77.99	4.235	2.408
25	37.6	17.2	10.2	.0503	-5.8	.1066	12.78	77.44	4.340	2.413
26	46.4	18.3	10.7	.0621	-5.3	.1316	13.52	76.67	4.480	2.408
27	55.2	19.5	11.2	.0739	-4.8	.1566	14.40	75.95	4.636	2.359
28	64.0	20.5	11.7	.0857	-4.4	.1816	15.15	75.35	4.770	2.301
29	72.8	21.6	12.1	.0975	-3.9	.2066	15.96	74.75	4.878	2.231
30	81.6	22.6	12.4	.1093	-3.6	.2316	16.73	74.24	4.952	2.147
31	99.2	24.6	13.1	.1329	-2.9	.2816	18.20	73.25	5.025	1.960
32	116.8	26.6	13.7	.1565	-2.3	.3316	19.65	72.41	5.011	1.699
33	134.4	28.4	14.3	.1801	-1.8	.3816	21.03	71.63	5.238	1.421
34	152.0	30.3	14.7	.2037	-1.3	.4316	22.43	70.96	5.193	1.132
35	169.6	32.1	15.1	.2273	-.9	.4816	23.76	70.39	5.215	.868
36	187.2	33.6	15.4	.2509	-.6	.5316	24.87	69.94	5.188	.590
37	222.4	35.7	15.9	.2981	-.1	.6316	26.36	69.27	2.795	.142
38	257.6	36.2	16.0	.3453	.0	.7316	26.80	69.09	1.437	.000
39	292.8	36.3	16.0	.3924	.0	.8316	26.82	69.09	.000	.010
40	328.1	36.3	16.0	.4396	.0	.9316	26.82	69.09	.000	.017

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00108 DELH = 1.287 REM = 1672.0
V RUN = 102171-1 CF/2 = .00042 DELM = 1.276 REM = 2700.0
PLATE = 6 UINF = 24.4 DEL2 = .1338 DEL3 = 5.261
X(IN) = 22.00 GM = 6.753 THETA = .2180 DEL4 = 35.525
K(E06) = -.4700 GAM = -1.215 BETA = 5.155 H = 2.044

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-18.6	0.0000	0.00	91.79	1.000	1.083
2	1.1	1.4	.9	.0009	-17.7	.0047	.71	90.75	1.344	1.172
3	1.4	1.7	1.1	.0010	-17.5	.0057	.89	90.51	1.427	1.212
4	1.6	2.1	1.3	.0012	-17.3	.0067	1.07	90.22	1.513	1.259
5	1.9	2.5	1.5	.0014	-17.1	.0077	1.24	90.01	1.602	1.294
6	2.1	2.8	1.8	.0016	-16.8	.0087	1.45	89.63	1.692	1.357
7	2.4	3.2	2.0	.0018	-16.6	.0097	1.65	89.33	1.783	1.406
8	2.8	4.0	2.6	.0022	-16.0	.0117	2.02	88.65	1.963	1.519
9	3.3	4.7	3.1	.0025	-15.4	.0137	2.40	87.98	2.136	1.629
10	3.8	5.4	3.8	.0029	-14.8	.0157	2.75	87.15	2.299	1.766
11	4.3	6.0	4.2	.0033	-14.4	.0177	3.06	86.74	2.450	1.833
12	4.8	6.6	4.5	.0037	-14.1	.0197	3.35	86.35	2.563	1.895
13	5.9	7.5	5.2	.0044	-13.3	.0237	3.85	85.41	2.814	2.052
14	6.7	8.4	5.9	.0051	-12.7	.0277	4.27	84.70	3.102	2.169
15	8.0	9.3	6.3	.0061	-12.2	.0327	4.74	84.07	3.400	2.272
16	9.2	10.2	6.9	.0070	-11.7	.0377	5.22	83.45	3.619	2.373
17	11.6	11.7	7.6	.0089	-11.0	.0477	5.96	82.59	4.046	2.512
18	14.0	12.6	8.1	.0107	-10.4	.0577	6.44	81.91	4.352	2.620
19	16.5	13.6	8.6	.0126	-10.0	.0677	6.93	81.32	4.655	2.712
20	18.9	14.3	9.0	.0145	-9.6	.0777	7.33	80.87	4.916	2.781
21	25.0	15.7	9.7	.0191	-8.9	.1027	8.00	80.01	5.404	2.905
22	31.1	16.8	10.1	.0238	-8.5	.1277	8.56	79.53	5.816	2.986
23	37.2	17.8	10.6	.0284	-8.0	.1527	9.11	78.94	6.201	3.037
24	43.2	18.6	10.9	.0331	-7.7	.1777	9.49	78.58	6.457	3.073
25	49.3	19.2	11.3	.0377	-7.2	.2027	9.82	78.01	6.675	3.122
26	55.4	20.1	11.6	.0424	-7.0	.2277	10.28	77.68	6.935	3.142
27	67.6	21.8	12.1	.0517	-6.4	.2777	11.13	77.06	7.377	3.164
28	79.7	23.1	12.7	.0610	-5.9	.3277	11.76	76.40	7.560	3.165
29	91.9	24.6	13.1	.0703	-5.5	.3777	12.56	75.86	7.724	3.142
30	104.1	25.9	13.6	.0796	-5.0	.4277	13.24	75.29	7.869	3.098
31	125.4	29.1	14.4	.0982	-4.2	.5277	14.84	74.31	7.420	2.951
32	152.7	31.9	15.1	.1168	-3.4	.6277	16.27	73.41	6.641	2.731
33	177.0	35.0	15.8	.1355	-2.8	.7277	17.88	72.59	6.157	2.442
34	201.4	38.1	16.4	.1541	-2.2	.8277	19.44	71.87	5.807	2.101
35	225.7	40.7	17.0	.1727	-1.6	.9277	20.76	71.15	5.320	1.682
36	274.4	43.4	17.9	.2099	-.7	1.1277	23.18	70.00	4.937	.823
37	323.0	47.6	18.5	.2472	-.1	1.3277	24.30	69.31	2.724	.144
38	371.7	47.8	18.6	.2844	.0	1.5277	24.42	69.19	.000	.000
39	420.3	47.8	18.6	.3216	.0	1.7277	24.42	69.19	.000	.012
40	469.0	47.8	18.6	.3589	.0	1.9277	24.42	69.19	.000	.023

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00089 DELM = 1.922 REM = 2410.0
V RUN = 102171-1 CF/2 = .00035 DELM = 1.920 REM = 3808.0
PLATE = 9 UINF = 23.0 DEL2 = .2041 DEL3 = 9.827
X(IN) = 34.00 GM = 7.316 THETA = .3225 DEL4 = 64.591
K(E06) = -.3310 GAM = -1.185 BETA = 5.144 M = 2.264

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-20.6	0.0000	0.00	91.65	1.000	1.000
2	1.3	1.6	1.0	.0006	-19.7	.0062	.70	90.63	1.419	1.205
3	1.5	1.9	1.2	.0008	-19.4	.0072	.84	90.39	1.494	1.253
4	1.7	2.2	1.4	.0009	-19.2	.0082	.98	90.16	1.579	1.299
5	2.1	2.9	1.8	.0011	-18.8	.0102	1.27	89.66	1.746	1.389
6	2.5	3.6	2.3	.0013	-18.3	.0122	1.57	89.19	1.915	1.476
7	3.0	4.2	2.8	.0015	-17.8	.0142	1.85	88.57	2.081	1.559
8	3.4	4.8	3.7	.0018	-17.3	.0162	2.13	88.03	2.240	1.726
9	3.9	5.4	3.7	.0020	-16.8	.0192	2.39	87.56	2.390	1.820
10	4.2	6.0	4.0	.0022	-16.5	.0202	2.62	87.24	2.531	1.884
11	5.1	6.9	5.1	.0026	-15.8	.0242	3.05	86.09	2.797	2.114
12	5.9	7.8	5.5	.0031	-15.1	.0282	3.41	85.70	3.012	2.192
13	6.9	8.6	6.3	.0036	-14.3	.0332	3.80	84.91	3.261	2.369
14	9.0	10.1	7.2	.0047	-13.4	.0432	4.42	83.78	3.686	2.597
15	11.1	11.2	9.0	.0059	-12.6	.0532	4.90	82.95	3.995	2.736
16	16.4	13.3	9.1	.0086	-11.5	.0782	5.85	81.71	4.721	2.973
17	21.6	14.7	9.8	.0114	-10.7	.1032	6.45	80.91	5.237	3.128
18	26.8	15.6	12.3	.0142	-10.2	.1282	6.84	80.37	5.647	3.224
19	32.1	16.1	10.5	.0170	-9.8	.1532	7.09	79.96	5.976	3.311
20	47.9	18.7	11.8	.0253	-8.8	.2282	8.21	78.79	7.145	3.479
21	53.0	19.6	12.0	.0280	-8.5	.2532	8.62	78.49	7.537	3.521
22	58.3	20.4	12.3	.0308	-8.2	.2782	8.95	78.25	7.967	3.553
23	68.7	21.2	12.7	.0364	-7.8	.3282	9.32	77.74	8.917	3.609
24	79.2	22.4	13.1	.0419	-7.4	.3782	9.82	77.33	9.925	3.645
25	89.7	23.4	13.5	.0475	-7.1	.4282	10.28	76.94	9.256	3.670
26	110.6	25.4	14.2	.0586	-6.7	.5282	11.16	76.13	9.929	3.691
27	131.6	27.9	14.9	.0697	-6.7	.6282	12.24	75.45	13.547	3.670
28	152.5	30.1	15.4	.0808	-6.1	.7282	13.21	74.92	13.441	3.603
29	194.4	34.7	16.9	.1029	-4.0	.9282	15.22	73.59	10.576	3.332
30	236.3	38.9	17.5	.1251	-3.1	1.1282	17.09	72.57	9.159	2.931
31	278.2	43.3	15.4	.1473	-2.2	1.3282	19.01	71.57	7.514	2.367
32	321.1	47.2	19.2	.1695	-1.3	1.5282	20.76	70.67	6.386	1.594
33	362.0	50.3	19.9	.1917	-.6	1.7282	22.11	69.89	5.795	.961
34	403.8	51.9	20.4	.2139	-.2	1.9282	22.82	69.37	5.635	.319
35	456.2	52.4	20.6	.2416	.0	2.1782	23.01	69.16	.957	.000
36	505.6	52.4	20.6	.2694	.0	2.4282	23.01	69.16	.000	.000
37	522.1	52.4	20.6	.2766	.0	2.4930	23.00	69.16	.000	.000

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00078 DELM = 2.636 REM = 5114.0
V RUN = 102171-1 CF/2 = .00031 DELM = 2.630 REM = 4497.0
PLATE = 12 UINF = 22.1 DEL2 = .2751 DEL3 = 12.649
X(IN) = 46.00 GM = 7.715 THETA = .4321 DEL4 = 87.579
K(E06) = -.2560 GAM = -1.185 BETA = 6.873 M = 2.559

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-22.1	0.0000	0.00	91.62	1.000	1.000
2	1.1	1.3	.9	.0004	-21.3	.0057	.82	90.83	1.356	1.191
3	1.3	1.6	1.0	.0005	-21.2	.0067	.82	90.69	1.428	1.213
4	1.6	2.1	1.3	.0006	-20.9	.0057	.95	90.27	1.670	1.310
5	2.0	2.7	1.7	.0008	-20.4	.0107	1.09	89.86	1.738	1.404
6	2.4	3.3	2.1	.0010	-20.0	.0127	1.33	89.48	1.899	1.491
7	3.2	4.5	3.0	.0013	-19.1	.0167	1.81	88.67	2.215	1.699
8	3.9	5.6	3.9	.0016	-18.2	.0207	2.23	87.85	2.524	1.910
9	4.9	6.9	5.1	.0020	-17.2	.0257	2.69	86.97	2.820	2.180
10	5.8	7.7	5.7	.0023	-16.5	.0307	3.08	86.26	3.097	2.342
11	6.8	8.6	6.1	.0027	-15.8	.0357	3.41	85.35	3.331	2.437
12	7.7	9.2	6.8	.0031	-15.2	.0407	3.69	84.73	3.544	2.575
13	9.6	10.5	7.6	.0039	-14.6	.0507	4.18	83.96	3.931	2.785
14	11.5	11.4	8.3	.0047	-13.8	.0607	4.54	83.19	4.251	2.929
15	13.4	12.2	8.8	.0054	-13.3	.0707	4.86	82.64	4.543	3.044
16	15.3	12.9	9.0	.0062	-13.1	.0807	5.14	82.47	4.688	3.092
17	20.0	14.3	9.9	.0082	-12.2	.1057	5.67	81.58	5.430	3.290
18	24.8	15.5	10.4	.0101	-11.7	.1307	6.11	80.98	5.948	3.423
19	34.2	17.8	11.4	.0140	-10.7	.1807	7.07	79.84	6.782	3.643
20	43.7	19.6	12.0	.0179	-10.1	.2307	7.84	79.34	7.217	3.769
21	53.2	19.5	12.5	.0217	-9.6	.2807	7.73	78.88	7.755	3.860
22	62.6	21.0	13.0	.0256	-9.1	.3307	8.34	78.42	8.428	3.932
23	81.6	22.5	13.7	.0333	-8.4	.4307	8.95	77.86	9.288	4.041
24	100.6	24.3	14.3	.0411	-7.7	.5307	9.65	77.20	10.131	4.126
25	119.5	26.1	14.9	.0488	-7.2	.6307	10.37	76.49	10.879	4.173
26	138.4	27.6	15.8	.0565	-6.6	.7307	10.98	75.91	11.392	4.142
27	176.3	31.4	16.4	.0720	-5.7	.9307	12.46	74.96	12.319	4.144
28	223.7	35.3	17.6	.0914	-4.6	1.1807	14.02	73.85	12.874	3.960
29	271.0	40.4	18.4	.1107	-3.7	1.4307	16.07	72.47	11.744	3.665
30	318.4	44.7	19.4	.1301	-2.7	1.6807	17.74	71.53	9.696	3.139
31	365.7	48.5	20.7	.1495	-1.8	1.9307	19.28	70.87	7.733	2.437
32	413.1	52.2	21.0	.1689	-1.1	2.1807	20.73	70.25	5.639	1.704
33	460.4	54.4	21.6	.1882	-.6	2.4307	21.61	69.84	5.439	.989
34	507.8	55.5	22.0	.2075	-.2	2.6807	22.06	69.26	2.170	.279
35	555.2	55.7	22.1	.2269	-.0	2.9307	22.13	69.14	.763	.000
36	602.5	55.7	22.1	.2462	-.0	3.1807	22.13	69.11	.000	.000
37	648.9	55.7	22.1	.2696	-.0	3.4307	22.13	69.11	.000	.000

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00071 DELM = 3.297 REM = 3672.0
V RUN = 102171-1 CF/2 = .00028 DELM = 3.293 REM = 5924.0
PLATE = 15 UINF = 21.4 DEL2 = .3350 DEL3 = 15.907
X(IN) = 58.00 GM = 7.777 THETA = .5409 DEL4 = 124.417
K(E06) = -.2090 GAM = -1.177 BETA = 7.550 M = 2.052

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-23.1	0.0000	0.00	91.62	1.000	1.000
2	1.2	1.5	.9	.0035	-22.2	.0068	.94	90.83	1.415	1.198
3	1.4	1.7	1.1	.0004	-22.0	.0078	.63	90.60	1.486	1.256
4	1.5	2.0	1.2	.0006	-21.9	.0088	.77	90.42	1.559	1.300
5	1.9	2.5	1.6	.0006	-21.5	.0108	.93	90.07	1.711	1.388
6	2.2	3.1	2.0	.0007	-21.1	.0128	1.14	89.69	1.867	1.483
7	2.6	3.7	2.4	.0010	-20.7	.0148	1.35	89.27	2.023	1.568
8	3.3	4.8	3.2	.0012	-19.8	.0188	1.75	88.45	2.325	1.793
9	4.0	5.5	3.9	.0013	-19.1	.0228	2.11	87.77	2.600	1.963
10	4.9	6.8	5.1	.0018	-18.0	.0278	2.58	86.89	2.902	2.243
11	5.7	7.7	5.9	.0021	-17.2	.0328	2.82	85.85	3.165	2.442
12	6.6	8.5	6.5	.0024	-16.6	.0378	3.12	85.26	3.397	2.589
13	7.5	9.2	6.9	.0027	-16.2	.0428	3.37	84.84	3.604	2.694
14	9.3	9.8	7.6	.0030	-15.5	.0478	3.56	84.22	3.997	2.848
15	10.1	10.5	8.3	.0036	-14.8	.0579	3.98	83.51	4.307	3.025
16	12.7	12.1	8.9	.0045	-14.2	.0729	4.41	82.89	4.639	3.184
17	17.1	13.8	9.9	.0059	-13.2	.0979	5.06	81.94	5.167	3.423
18	21.4	15.3	10.7	.0076	-12.4	.1228	5.59	81.17	5.717	3.614
19	25.8	16.2	11.4	.0091	-11.7	.1478	5.91	80.46	6.096	3.784
20	30.1	16.8	11.8	.0106	-11.2	.1728	6.14	80.04	6.419	3.893
21	38.8	18.4	12.5	.0137	-10.6	.2228	6.73	79.41	7.121	4.050
22	47.6	19.2	12.7	.0167	-10.4	.2729	7.02	79.21	7.625	4.114
23	56.3	20.1	13.1	.0198	-10.0	.3229	7.37	78.79	8.173	4.210
24	73.7	21.8	13.7	.0259	-9.4	.4229	7.97	78.22	9.160	4.339
25	91.2	23.3	14.5	.0321	-8.6	.5228	8.50	77.62	10.024	4.470
26	126.0	26.5	15.5	.0443	-7.6	.7228	9.70	76.46	11.818	4.641
27	160.9	28.6	16.3	.0565	-6.8	.9228	10.47	75.69	12.795	4.731
28	204.5	32.8	17.3	.0718	-5.8	1.1728	11.99	74.70	14.047	4.701
29	248.1	37.2	18.3	.0872	-4.8	1.4228	13.58	73.71	14.722	4.481
30	291.7	40.4	19.1	.1025	-4.0	1.6728	14.78	72.98	13.990	4.210
31	335.3	44.3	19.8	.1178	-3.4	1.9228	16.21	72.30	12.963	3.902
32	378.8	47.9	20.5	.1331	-2.8	2.1728	17.90	71.55	11.825	3.535
33	422.4	51.5	21.2	.1484	-1.9	2.4228	18.82	70.89	9.993	2.662
34	466.0	54.3	21.9	.1637	-1.4	2.6728	19.84	70.34	6.792	1.995
35	509.6	56.6	22.3	.1790	-.8	2.9228	20.70	69.77	5.194	1.134
36	553.2	57.8	22.7	.1943	-.4	3.1728	21.15	69.36	3.425	.457
37	596.8	58.4	23.0	.2096	-.2	3.4228	21.36	69.17	1.879	.098
38	640.4	58.5	23.1	.2249	-.1	3.6728	21.40	69.08	.625	.000
39	684.0	58.5	23.1	.2402	-.1	3.9228	21.39	69.05	.892	.015

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00066 DELM = 4.167 REM = 4354.0
V RUN = 102171-1 CF/2 = .00026 DELM = 3.952 REM = 6992.0
PLATE = 18 UINF = 20.9 DEL2 = .4068 DEL3 = 19.763
X(IN) = 70.00 GM = 7.926 THETA = .6531 DEL4 = 156.641
K(E06) = -.1790 GAM = -1.226 BETA = 8.213 M = 2.019

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-23.9	0.0000	0.00	91.51	1.000	1.080
2	1.1	1.3	.8	.0003	-23.1	.0066	.45	90.77	1.381	1.199
3	1.2	1.6	1.0	.0004	-22.9	.0076	.63	90.57	1.448	1.253
4	1.4	1.8	1.1	.0004	-22.8	.0086	.62	90.42	1.517	1.293
5	1.7	2.3	1.4	.0005	-22.5	.0106	.90	90.16	1.662	1.383
6	2.1	2.8	1.8	.0006	-22.1	.0126	.98	89.77	1.812	1.465
7	2.7	3.9	2.7	.0008	-21.3	.0166	1.39	89.01	2.116	1.672
8	3.4	5.0	3.5	.0010	-20.4	.0206	1.71	88.24	2.406	1.879
9	4.2	6.1	4.3	.0012	-19.6	.0256	2.10	87.47	2.731	2.086
10	5.0	7.1	5.2	.0015	-18.7	.0306	2.44	86.59	3.015	2.422
11	6.7	8.6	6.5	.0020	-17.4	.0406	2.97	85.38	3.484	2.646
12	8.3	9.9	7.6	.0025	-16.2	.0506	3.29	84.37	3.864	2.816
13	9.9	10.8	8.1	.0030	-15.6	.0606	3.71	83.66	4.455	3.106
14	11.6	11.7	9.0	.0035	-14.9	.0706	4.01	83.01	4.635	3.279
15	14.9	13.0	9.9	.0045	-14.0	.0906	4.44	82.21	4.982	3.494
16	19.0	14.3	10.5	.0057	-13.4	.1156	4.92	81.58	5.430	3.665
17	23.1	15.3	11.1	.0069	-12.8	.1406	5.25	81.08	5.850	3.798
18	31.3	16.8	12.0	.0094	-11.8	.1906	5.79	80.16	6.592	4.029
19	39.5	18.3	12.5	.0119	-11.4	.2406	6.29	79.77	7.300	4.122
20	47.7	19.7	13.1	.0144	-10.9	.2906	6.77	79.15	7.980	4.261
21	55.9	20.9	13.4	.0169	-10.5	.3406	7.19	78.85	8.588	4.334
22	72.3	22.0	14.1	.0218	-9.6	.4406	7.56	78.22	9.452	4.496
23	88.7	23.6	14.6	.0268	-9.3	.5406	8.11	77.75	10.476	4.629
24	121.6	26.5	15.8	.0367	-8.1	.7406	9.10	76.61	12.231	4.843
25	154.4	28.5	16.5	.0466	-7.3	.9406	9.91	75.90	13.593	4.959
26	195.4	32.2	17.4	.0590	-6.5	1.1906	11.09	75.09	15.257	5.037
27	236.4	35.1	15.2	.0714	-5.7	1.4406	12.09	74.40	16.092	5.025
28	277.5	38.2	18.8	.0839	-5.1	1.6906	13.16	73.83	16.441	4.939
29	318.5	41.4	19.4	.0961	-4.5	1.9406	14.24	73.20	16.157	4.774
30	359.5	44.3	20.3	.1085	-3.8	2.1906	15.22	72.39	14.852	4.438
31	400.6	47.7	20.8	.1209	-3.1	2.4406	16.41	71.91	13.594	4.207
32	441.6	50.9	21.4	.1333	-2.5	2.6906	17.52	71.37	11.731	3.962
33	482.6	53.6	21.9	.1457	-1.9	2.9406	18.46	70.93	9.262	3.390
34	523.7	56.0	22.5	.1581	-1.4	3.1906	19.27	70.25	6.710	2.803
35	564.7	57.7	23.0	.1705	-.9	3.4406	19.97	69.56	4.347	2.326
36	605.7	59.4	23.3	.1829	-.6	3.6906	20.44	69.59	3.167	1.998
37	646.8	60.1	23.6	.1953	-.2	3.9406	20.69	69.23	1.761	1.459
38	810.9	60.1	23.9	.2449	.0	4.9406	20.67	68.96	1.944	.000

DATE = 102271 (-0.15, 0.004)

T RUN = 102271-1 STNA = .00662 DELH = 4.713 REH = 5007.0
W RUN = 102171-1 CF/2 = .00025 DELM = 4.741 REM = 7926.0
PLATE = 21 UINF = 20.4 DEL2 = .4771 DEL3 = 23.666
X(IN) = 82.00 GM = 5.119 THETA = .7553 DEL4 =192.147
K(E06)= -.1600 GAM = -1.282 BETA = 8.655 M = 1.938

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-25.0	0.0000	0.00	91.44
2	1.3	1.7	1.1	.0004	-23.9	.0046	.58	90.45
3	1.5	2.0	1.2	.0004	-23.8	.0096	.64	90.36
4	1.7	2.2	1.3	.0004	-23.6	.2106	.72	90.22
5	1.9	2.5	1.5	.0005	-23.5	.0116	.81	90.10
6	2.1	3.0	1.7	.0006	-23.2	.0136	.98	89.86
7	2.4	3.5	2.0	.0007	-22.9	.0156	1.15	89.60
8	3.1	4.5	3.3	.0008	-22.0	.0196	1.49	88.74
9	3.7	5.5	3.6	.0010	-21.4	.0236	1.80	88.18
10	4.5	6.0	4.5	.0012	-20.4	.0286	2.14	87.33
11	5.3	7.4	5.0	.0014	-19.9	.0336	2.44	86.88
12	6.1	8.2	5.7	.0016	-19.2	.0386	2.69	86.26
13	7.6	9.5	7.4	.0020	-17.6	.0486	3.11	84.76
14	10.0	10.9	8.4	.0026	-16.5	.0636	3.60	83.81
15	13.1	12.4	9.7	.0035	-15.2	.0836	4.09	82.65
16	17.1	14.0	10.8	.0045	-14.1	.1086	4.60	81.67
17	21.0	15.5	11.3	.0055	-13.7	.1336	5.12	81.26
18	28.9	17.7	12.0	.0076	-12.9	.1836	5.83	80.60
19	36.7	18.8	12.9	.0097	-12.2	.2336	6.18	79.89
20	44.6	19.4	13.2	.0117	-11.7	.2836	6.38	79.50
21	52.4	20.0	13.7	.0138	-11.3	.3336	6.60	79.09
22	66.1	22.6	14.5	.0179	-10.4	.4336	7.45	78.31
23	83.9	23.8	15.3	.0221	-9.7	.5336	7.85	77.63
24	115.3	26.5	16.3	.0304	-8.9	.7336	8.74	76.97
25	146.7	28.4	16.8	.0386	-8.1	.9336	9.35	76.23
26	196.0	31.1	17.9	.0490	-7.2	1.1836	10.26	75.39
27	225.3	34.0	18.4	.0593	-6.6	1.4336	11.21	74.85
28	264.6	36.7	19.0	.0697	-6.0	1.6836	12.07	74.31
29	303.9	38.8	19.7	.0800	-5.2	1.9336	12.77	73.65
30	343.2	41.1	20.5	.0904	-4.5	2.1836	13.54	72.98
31	382.5	44.5	20.9	.1007	-4.1	2.4336	14.65	72.57
32	421.8	47.0	21.4	.1111	-3.6	2.6836	15.48	72.09
33	461.0	49.4	22.0	.1214	-3.0	2.9336	16.28	71.53
34	500.3	52.1	22.5	.1317	-2.5	3.1836	17.14	71.13
35	539.6	54.4	22.9	.1421	-2.1	3.4336	17.93	70.83
36	578.9	57.2	23.4	.1524	-1.6	3.6836	19.88	70.32
37	618.2	59.5	23.9	.1628	-1.1	3.9336	19.59	69.89
38	775.4	57.6	25.0	.2042	.0	4.9336	18.98	68.87

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00395 DELH = .149 REH = 159.0
W RUN = 111571-1 CF/2 = .00249 DELM = .313 REM = 560.0
PLATE = 1 UINF = 29.5 DEL2 = .0114 DEL3 = .295
X(IN) = 2.88 GM = 5.167 THETA = .0368 DEL4 = 1.526
K(E06)= -.4440 GAM = -.402 BETA = .162 M = 1.618

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-12.4	0.0000	0.00	91.86
2	3.2	3.9	2.3	.0109	-10.3	.0044	5.86	87.97
3	3.9	4.4	2.9	.0131	-9.5	.0054	6.69	86.35
4	4.6	5.0	3.5	.0214	-8.8	.0064	7.47	85.14
5	5.4	5.5	4.1	.0247	-8.2	.0074	8.25	83.99
6	6.1	6.0	4.6	.0280	-7.8	.0084	9.01	83.07
7	6.8	6.5	5.1	.0313	-7.3	.0094	9.75	82.12
8	7.5	6.9	5.4	.0346	-6.9	.0104	10.43	81.49
9	9.2	7.4	5.9	.0379	-6.5	.0114	11.08	80.75
10	9.0	7.7	6.2	.0412	-6.2	.0124	11.65	80.06
11	9.7	8.1	6.5	.0445	-5.9	.0134	12.19	79.47
12	10.4	8.4	6.8	.0478	-5.6	.0144	12.68	78.97
13	11.1	8.7	7.0	.0511	-5.4	.0154	13.12	78.49
14	12.6	9.3	7.4	.0578	-4.9	.0174	13.93	77.65
15	14.0	9.7	7.9	.0644	-4.4	.0194	14.63	76.75
16	15.4	10.1	8.2	.0710	-4.1	.0214	15.27	76.07
17	16.9	10.5	8.6	.0776	-3.8	.0234	15.82	75.47
18	18.3	10.8	8.8	.0842	-3.5	.0254	16.26	74.93
19	19.8	11.1	9.1	.0908	-3.3	.0274	15.76	74.51
20	22.6	11.7	9.4	.1040	-2.9	.0314	17.66	73.76
21	25.5	12.1	9.8	.1173	-2.5	.0354	18.25	73.10
22	29.1	12.6	10.1	.1338	-2.2	.0404	18.99	72.47
23	32.7	12.9	10.4	.1503	-1.9	.0454	19.42	71.96
24	36.3	13.2	10.6	.1668	-1.7	.0504	19.81	71.49
25	39.9	13.6	10.8	.1834	-1.5	.0554	20.40	71.12
26	47.1	14.0	11.1	.2164	-1.2	.0654	21.12	70.52
27	54.3	14.5	11.4	.2495	-.9	.0754	21.76	70.04
28	61.5	14.9	11.6	.2825	-.7	.0854	22.35	69.62
29	75.9	15.6	11.9	.3487	-.4	.1054	23.50	69.07
30	90.3	16.2	12.1	.4148	-.2	.1254	24.41	68.69
31	108.3	16.9	12.2	.4974	-.1	.1504	25.50	68.40
32	126.3	17.5	12.3	.5801	-.0	.1754	26.40	68.28
33	144.3	18.1	12.4	.6627	.0	.2004	27.20	68.19
34	162.3	18.5	12.4	.7454	.0	.2254	27.85	68.19
35	198.3	19.2	12.4	.9106	.0	.2754	28.86	68.18
36	209.3	19.3	12.4	.9615	.0	.2908	29.05	68.18
37	230.9	19.5	12.4	1.0606	.0	.3208	29.29	68.19
38	259.7	19.6	12.4	1.1929	.0	.3609	29.46	68.19
39	295.7	19.6	12.4	1.3582	.0	.4108	29.49	68.18
40	331.7	19.6	12.4	1.5235	.0	.4608	29.50	68.19
41	385.7	19.6	12.4	1.7714	.0	.5358	29.50	68.18

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00276 DELH = .497 REH = 609.0
W RUN = 111571-1 CF/2 = .00176 DELM = .543 REM = 1390.0
PLATE = 3 UINF = 26.7 DEL2 = .0442 DEL3 = 1.190
X(IN) = 10.00 GM = 4.964 THETA = .0792 DEL4 = 5.975
K(E06)= -.8430 GAM = -1.389 BETA = .845 M = 1.661

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.9	0.0000	0.00	92.17	1.000	1.000
2	3.0	4.0	2.2	.0046	-12.8	.0095	4.57	88.92	1.134	1.048
3	3.6	4.4	2.6	.0054	-12.4	.0065	5.02	88.30	1.157	1.057
4	4.1	4.8	3.0	.0062	-11.9	.0075	5.47	87.44	1.185	1.069
5	4.7	5.1	3.4	.0070	-11.4	.0085	5.89	86.68	1.180	1.079
6	5.2	5.5	3.9	.0079	-10.9	.0095	6.32	85.94	1.194	1.089
7	5.8	5.9	4.3	.0087	-10.5	.0105	6.75	85.29	1.208	1.098
8	6.3	6.3	4.7	.0095	-10.2	.0115	7.17	84.75	1.223	1.105
9	6.8	6.6	4.9	.0103	-9.9	.0125	7.57	84.34	1.237	1.111
10	7.9	7.3	5.5	.0120	-9.3	.0145	8.34	83.39	1.263	1.124
11	9.0	7.9	6.1	.0136	-8.7	.0165	9.01	82.41	1.286	1.136
12	10.1	8.3	6.6	.0153	-8.3	.0185	9.90	81.71	1.305	1.145
13	11.2	8.7	6.9	.0169	-7.9	.0205	10.01	81.16	1.324	1.153
14	12.3	9.2	7.2	.0186	-7.7	.0225	10.57	80.72	1.343	1.159
15	14.5	9.9	7.8	.0218	-7.1	.0265	11.35	79.92	1.377	1.169
16	16.7	10.4	8.2	.0251	-6.6	.0305	11.87	79.09	1.395	1.177
17	18.9	10.7	8.6	.0284	-6.3	.0345	12.23	78.51	1.411	1.184
18	21.6	11.2	9.0	.0325	-5.9	.0395	12.85	77.89	1.436	1.189
19	24.4	11.6	9.3	.0367	-5.6	.0445	13.31	77.44	1.454	1.193
20	27.1	12.0	9.5	.0408	-5.4	.0495	13.69	77.08	1.470	1.196
21	29.8	12.3	9.9	.0449	-5.1	.0545	14.08	76.66	1.484	1.196
22	35.3	12.8	10.2	.0531	-4.7	.0645	14.63	76.01	1.502	1.194
23	40.8	13.2	10.4	.0613	-4.4	.0745	15.06	75.56	1.511	1.189
24	46.2	13.5	10.8	.0696	-4.1	.0845	15.48	75.08	1.518	1.177
25	51.7	13.9	11.1	.0778	-3.9	.0945	15.93	74.75	1.523	1.166
26	59.9	14.4	11.3	.0901	-3.6	.1095	16.47	74.18	1.518	1.139
27	73.6	15.1	11.8	.1107	-3.1	.1345	17.26	73.33	1.487	1.086
28	87.3	15.8	12.1	.1312	-2.7	.1595	18.04	72.86	1.442	1.029
29	101.0	16.4	12.5	.1518	-2.3	.1845	18.78	72.26	1.383	.956
30	114.8	17.0	12.8	.1724	-2.0	.2095	19.48	71.78	1.309	.885
31	128.3	17.6	13.1	.1929	-1.8	.2345	20.17	71.33	1.231	.809
32	142.0	18.2	13.4	.2135	-1.5	.2595	20.86	70.94	1.150	.732
33	155.7	18.8	13.6	.2341	-1.3	.2845	21.57	70.58	1.075	.654
34	183.8	20.0	14.0	.2752	-.9	.3349	22.89	69.94	.925	.495
35	210.4	21.0	14.3	.3163	-.6	.3845	24.06	69.43	.821	.366
36	237.7	21.9	14.6	.3574	-.3	.4345	25.07	69.01	.735	.206
37	292.4	23.0	14.5	.4397	-.1	.5345	26.30	68.61	.565	.046
38	347.2	23.3	14.9	.5219	-.0	.6345	26.68	68.52	.280	.000
39	401.9	23.3	14.9	.6042	-.0	.7345	26.70	68.52	.023	.000
40	408.3	23.3	14.9	.6139	-.0	.7463	26.69	68.52	.177	.000

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00230 DELH = .924 REH = 1126.0
W RUN = 111571-1 CF/2 = .00144 DELM = .926 REM = 1761.0
PLATE = 6 UINF = 25.3 DEL2 = .0960 DEL3 = 2.497
X(IN) = 22.00 GM = 4.931 THETA = .1467 DEL4 = 12.292
K(E06)= -.4690 GAM = -1.236 BETA = .928 M = 1.668

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.1	0.0000	0.00	92.24	1.000	1.000
2	2.0	3.0	1.5	.0017	-14.8	.0045	2.84	90.27	1.099	1.030
3	2.5	3.3	1.8	.0021	-14.5	.0055	3.10	89.77	1.098	1.037
4	2.9	3.5	2.1	.0025	-14.1	.0065	3.34	89.21	1.103	1.046
5	3.4	3.9	2.5	.0029	-13.7	.0075	3.67	88.62	1.120	1.055
6	3.8	4.3	2.9	.0033	-13.3	.0085	4.01	88.15	1.132	1.062
7	4.3	4.6	3.2	.0037	-12.9	.0095	4.32	87.56	1.143	1.070
8	5.2	5.4	3.9	.0046	-12.3	.0115	5.02	86.59	1.166	1.085
9	6.1	6.1	4.6	.0053	-11.5	.0135	5.72	85.43	1.191	1.102
10	7.0	6.6	5.2	.0061	-11.0	.0155	6.25	84.66	1.210	1.114
11	7.9	7.3	5.6	.0068	-10.6	.0175	6.85	84.10	1.232	1.123
12	9.7	8.1	6.4	.0084	-9.8	.0215	7.67	82.92	1.264	1.140
13	11.5	9.0	7.1	.0100	-9.1	.0255	8.47	81.94	1.296	1.154
14	13.3	9.5	7.6	.0116	-8.5	.0295	8.94	81.11	1.319	1.166
15	15.1	10.1	8.0	.0131	-8.2	.0335	9.58	80.57	1.346	1.173
16	16.9	10.7	8.4	.0147	-7.7	.0375	10.12	79.92	1.371	1.181
17	18.7	11.1	8.7	.0163	-7.5	.0415	10.48	79.56	1.390	1.186
18	21.0	11.4	9.0	.0182	-7.1	.0465	10.73	79.09	1.408	1.192
19	23.2	11.7	9.2	.0202	-6.9	.0515	11.03	78.72	1.427	1.196
20	27.7	12.3	9.7	.0241	-6.4	.0615	11.55	78.04	1.463	1.202
21	32.2	12.7	10.1	.0280	-6.1	.0715	11.96	77.53	1.494	1.206
22	36.7	13.1	10.3	.0320	-5.9	.0815	12.34	77.20	1.525	1.207
23	41.2	13.5	10.6	.0359	-5.6	.0915	12.69	76.82	1.551	1.207
24	45.8	13.8	10.9	.0418	-5.3	.1065	12.97	76.37	1.582	1.205
25	59.2	14.3	11.3	.0516	-4.9	.1315	13.45	75.77	1.628	1.197
26	70.5	14.9	11.6	.0614	-4.6	.1565	14.02	75.35	1.670	1.187
27	81.7	15.3	11.9	.0712	-4.3	.1815	14.46	74.87	1.698	1.171
28	104.3	16.2	12.4	.0908	-3.8	.2315	15.31	74.16	1.730	1.134
29	126.9	17.1	12.9	.1104	-3.4	.2815	16.07	73.53	1.721	1.086
30	149.3	17.9	13.2	.1301	-2.9	.3315	16.91	72.93	1.684	1.027
31	171.8	18.7	13.6	.1497	-2.6	.3815	17.63	72.42	1.601	.963
32	194.3	19.5	13.9	.1693	-2.3	.4315	18.35	71.91	1.492	.888
33	239.4	21.0	14.5	.2085	-1.7	.5315	19.81	71.06	1.230	.728
34	284.4	22.6	15.0	.2478	-1.2	.6315	21.26	70.34	.983	.556
35	329.4	23.9	15.4	.2870	-.8	.7315	22.52	69.74	.792	.381
36	374.5	25.0	15.8	.3262	-.4	.8315	23.52	69.22	.609	.205
37	419.5	25.6	16.0	.3655	-.2	.9315	24.10	68.86	.402	.065
38	464.5	25.8	16.1	.4047	-.1	1.0315	24.30	68.71	.156	.000
39	509.6	25.8	16.1	.4440	-.0	1.1315	24.32	68.69	.000	.000
40	554.6	25.8	16.1	.4832	-.0	1.2315	24.32	68.69	.000	.000
41	555.8	25.8	16.1	.4835	-.0	1.2323	24.32	68.65	.000	.000

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00211 DELM = 1.333 REM = 1553.0
V RUN = 111571-1 CF/2 = .00118 DELM = 1.368 REM = 2321.0
PLATE = 9 UINF = 23.0 DEL2 = .1311 DEL3 = 3.480
X(IN) = 34.00 GM = 4.664 THETA = .1959 DEL* = 16.230
K(E06) = -.3360 GAM = -1.209 BETA = 1.069 M = 1.645

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.9	0.0000	0.00	92.41	1.000	1.000
2	2.0	2.1	1.5	.0015	-14.7	.0053	1.74	90.54	1.066	1.029
3	2.4	2.6	1.7	.0018	-14.4	.0063	2.07	90.18	1.079	1.036
4	2.8	3.0	2.0	.0020	-14.1	.0073	2.41	89.74	1.092	1.041
5	3.2	3.4	2.3	.0023	-13.7	.0083	2.75	89.15	1.111	1.050
6	3.6	3.8	2.6	.0026	-13.4	.0093	3.08	88.68	1.122	1.055
7	4.0	4.2	2.9	.0029	-13.0	.0103	3.41	88.06	1.131	1.057
8	4.3	4.6	3.3	.0032	-12.7	.0113	3.72	87.56	1.147	1.075
9	4.7	5.0	3.6	.0035	-12.3	.0123	4.02	87.09	1.156	1.082
10	5.1	5.4	3.9	.0037	-12.1	.0133	4.35	86.68	1.167	1.089
11	5.5	5.8	4.2	.0040	-11.8	.0143	4.66	86.23	1.178	1.096
12	6.3	6.4	4.7	.0046	-11.2	.0163	5.17	85.43	1.199	1.104
13	7.0	7.1	5.0	.0051	-10.9	.0183	5.74	84.96	1.221	1.116
14	7.8	7.8	5.4	.0057	-10.6	.0203	6.29	84.36	1.242	1.125
15	8.6	8.3	5.8	.0063	-10.1	.0223	6.72	83.81	1.261	1.133
16	10.1	8.9	6.4	.0074	-9.5	.0263	7.17	82.92	1.284	1.147
17	11.7	9.8	6.9	.0085	-9.0	.0303	7.91	82.09	1.315	1.159
18	13.6	10.6	7.5	.0099	-8.4	.0353	8.56	81.24	1.346	1.171
19	15.5	11.1	8.0	.0113	-8.0	.0403	9.01	80.53	1.371	1.181
20	17.5	11.6	8.2	.0127	-7.7	.0453	9.34	80.19	1.392	1.187
21	19.4	12.0	8.5	.0141	-7.4	.0503	9.66	79.74	1.412	1.193
22	23.2	12.6	9.0	.0169	-7.0	.0603	10.20	79.05	1.451	1.202
23	27.1	13.2	9.3	.0195	-6.6	.0703	10.64	78.52	1.485	1.208
24	30.9	13.7	9.6	.0226	-6.3	.0803	11.09	78.07	1.521	1.211
25	40.6	14.7	10.1	.0296	-5.8	.1053	11.93	77.32	1.598	1.215
26	50.2	15.0	10.5	.0366	-5.5	.1303	12.15	76.85	1.647	1.216
27	59.9	15.6	10.8	.0437	-5.1	.1553	12.57	76.34	1.695	1.213
28	69.5	16.0	11.1	.0507	-4.9	.1803	12.95	75.95	1.741	1.208
29	83.6	16.8	11.5	.0647	-4.4	.2203	13.56	75.26	1.816	1.193
30	108.1	17.5	11.9	.0788	-4.0	.2803	14.12	74.73	1.872	1.175
31	127.4	18.1	12.2	.0929	-3.7	.3303	14.65	74.22	1.909	1.149
32	165.9	19.6	12.9	.1210	-3.1	.4303	15.80	73.15	1.953	1.090
33	204.5	20.7	13.3	.1491	-2.6	.5303	16.75	72.60	1.981	1.011
34	243.1	22.0	13.7	.1772	-2.2	.6303	17.78	71.97	1.996	.926
35	281.6	23.2	14.1	.2053	-1.8	.7303	18.74	71.39	1.603	.526
36	320.2	24.3	14.5	.2334	-1.4	.8303	19.66	70.82	1.347	.705
37	358.8	25.4	14.8	.2615	-1.1	.9303	20.55	70.34	1.055	.556
38	435.9	27.3	15.4	.3177	-.5	1.1303	22.07	69.50	.637	.331
39	513.0	28.3	15.3	.3740	-.2	1.3303	22.85	68.95	.261	.116
40	590.1	28.5	15.9	.4302	-.0	1.5303	23.02	68.71	.000	.000
41	667.3	28.5	15.9	.4864	-.0	1.7303	23.01	68.71	.000	.000

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00199 DELM = 1.765 REM = 1937.0
V RUN = 111571-1 CF/2 = .00112 DELM = 1.694 REM = 2971.0
PLATE = 12 UINF = 22.0 DEL2 = .1729 DEL3 = 4.645
X(IN) = 46.00 GM = 4.686 THETA = .2531 DEL* = 21.766
K(E06) = -.2650 GAM = -1.177 BETA = 1.069 M = 1.646

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.5	0.0000	0.00	92.55	1.000	1.000
2	1.4	1.5	1.0	.0008	-15.5	.0039	1.15	91.16	1.042	1.021
3	1.7	1.9	1.2	.0010	-15.2	.0049	1.39	90.80	1.054	1.027
4	2.1	2.2	1.5	.0012	-15.0	.0059	1.69	90.51	1.065	1.031
5	2.5	2.6	1.8	.0014	-14.8	.0069	1.98	90.17	1.076	1.037
6	2.9	3.0	2.0	.0016	-14.4	.0079	2.27	89.63	1.088	1.045
7	3.5	3.8	2.6	.0021	-13.8	.0099	2.95	88.74	1.110	1.059
8	4.3	4.6	3.3	.0025	-13.2	.0119	3.41	87.83	1.137	1.072
9	5.0	5.2	3.8	.0029	-12.8	.0139	3.94	87.03	1.156	1.085
10	5.7	5.9	4.3	.0033	-12.1	.0159	4.45	86.29	1.176	1.095
11	6.4	6.5	4.8	.0037	-11.7	.0179	4.90	85.64	1.194	1.105
12	7.1	7.1	5.2	.0042	-11.2	.0199	5.34	85.02	1.211	1.114
13	7.9	7.6	5.5	.0046	-10.9	.0219	5.71	84.55	1.226	1.121
14	8.6	8.0	5.9	.0050	-10.6	.0239	5.98	84.07	1.239	1.129
15	9.3	8.3	6.1	.0054	-10.3	.0259	6.25	83.66	1.250	1.135
16	10.7	9.1	6.7	.0063	-9.8	.0299	6.83	82.86	1.277	1.147
17	12.5	10.0	7.3	.0073	-9.1	.0349	7.50	81.91	1.308	1.160
18	14.3	10.7	7.6	.0084	-8.8	.0399	8.04	81.46	1.334	1.167
19	16.1	11.2	8.0	.0094	-8.4	.0449	8.46	80.93	1.355	1.175
20	17.9	11.5	8.4	.0105	-8.1	.0499	8.68	80.39	1.373	1.182
21	21.5	12.7	8.9	.0126	-7.6	.0599	9.27	79.64	1.411	1.192
22	25.1	13.0	9.2	.0147	-7.2	.0699	9.52	79.14	1.447	1.199
23	28.7	13.7	9.6	.0168	-6.9	.0799	10.29	78.70	1.483	1.204
24	32.7	14.2	10.0	.0221	-6.4	.1049	10.72	78.01	1.531	1.211
25	46.7	14.5	10.4	.0273	-6.0	.1299	10.94	77.44	1.577	1.214
26	55.6	15.0	10.8	.0326	-5.7	.1549	11.29	76.97	1.620	1.215
27	64.6	15.5	11.0	.0379	-5.4	.1799	11.67	76.55	1.661	1.215
28	82.6	16.3	11.5	.0484	-5.0	.2299	12.25	75.92	1.744	1.211
29	100.6	16.7	11.9	.0589	-4.6	.2799	12.54	75.44	1.821	1.203
30	114.5	17.4	12.1	.0695	-4.4	.3299	13.12	75.07	1.869	1.194
31	154.5	18.8	12.6	.0905	-3.8	.4299	14.18	74.25	1.977	1.165
32	193.4	19.8	13.1	.1116	-3.3	.5299	14.91	73.56	2.010	1.122
33	226.3	20.7	13.5	.1326	-2.9	.6299	15.62	72.96	1.998	1.069
34	262.3	21.8	13.9	.1537	-2.6	.7299	16.39	72.42	1.967	1.007
35	334.1	23.8	14.6	.1958	-1.9	.9299	17.92	71.46	1.721	.861
36	406.3	25.5	15.1	.2380	-1.3	1.1299	19.20	70.64	1.290	.688
37	477.9	27.1	15.6	.2801	-.9	1.3299	20.41	69.95	.841	.497
38	549.7	28.4	16.0	.3222	-.4	1.5299	21.39	69.35	.479	.294
39	621.6	29.0	16.3	.3643	-.2	1.7299	21.86	68.99	.179	.145
40	693.8	29.3	16.4	.4065	-.1	1.9299	22.02	68.81	.000	.059
41	783.3	29.2	16.5	.4591	-.0	2.1799	22.01	68.72	.000	.000

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00190 DELM = 2.102 REM = 2219.0
V RUN = 111571-1 CF/2 = .00108 DELM = 1.994 REM = 3311.0
PLATE = 15 UINF = 21.2 DEL2 = .2127 DEL3 = 5.610
X(IN) = 58.00 GM = 4.687 THETA = .3024 DEL* = 25.295
K(E06) = -.2150 GAM = -1.143 BETA = 1.051 M = 1.631

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.9	0.0000	0.00	92.62	1.000	1.000
2	1.7	1.8	1.2	.0009	-15.8	.0051	1.32	91.07	1.052	1.324
3	2.1	2.2	1.5	.0011	-15.5	.0061	1.58	90.63	1.062	1.031
4	2.4	2.6	1.7	.0012	-15.3	.0071	1.84	90.30	1.072	1.036
5	2.9	3.0	2.0	.0014	-15.0	.0081	2.11	89.86	1.332	1.043
6	3.1	3.3	2.2	.0016	-14.7	.0091	2.37	89.54	1.092	1.048
7	3.4	3.7	2.5	.0018	-14.4	.0101	2.61	89.10	1.103	1.055
8	3.8	4.0	2.9	.0019	-14.1	.0111	2.88	88.65	1.113	1.062
9	4.5	4.7	3.4	.0023	-13.5	.0131	3.37	87.96	1.132	1.074
10	5.1	5.4	3.8	.0026	-13.1	.0151	3.84	87.21	1.159	1.084
11	5.8	6.0	4.4	.0030	-12.5	.0171	4.26	86.39	1.174	1.097
12	6.5	6.6	4.9	.0033	-12.0	.0191	4.68	85.76	1.191	1.106
13	7.2	7.2	5.2	.0037	-11.7	.0211	5.10	85.29	1.210	1.113
14	7.9	7.7	5.6	.0040	-11.3	.0231	5.47	84.75	1.225	1.121
15	8.5	8.2	5.9	.0044	-11.1	.0251	5.80	84.40	1.239	1.127
16	9.9	8.9	6.5	.0051	-10.4	.0291	6.34	83.42	1.263	1.141
17	11.6	10.0	7.1	.0059	-9.9	.0341	7.09	82.68	1.296	1.153
18	13.3	10.7	7.5	.0068	-9.4	.0391	7.62	82.06	1.321	1.162
19	15.0	11.1	8.0	.0077	-8.9	.0441	7.92	81.31	1.339	1.173
20	16.7	11.5	8.3	.0086	-8.6	.0491	8.23	80.90	1.358	1.179
21	20.1	12.4	8.9	.0103	-8.0	.0591	8.81	80.10	1.394	1.190
22	23.5	12.9	9.3	.0121	-7.6	.0691	9.22	79.56	1.422	1.197
23	26.9	13.4	9.6	.0138	-7.3	.0791	9.62	79.11	1.445	1.202
24	32.0	13.8	10.0	.0164	-6.9	.0941	9.86	78.52	1.476	1.210
25	40.5	14.6	10.4	.0209	-6.6	.1191	10.34	78.04	1.527	1.217
26	49.0	15.1	10.8	.0251	-6.1	.1441	10.76	77.39	1.574	1.222
27	57.5	15.4	11.0	.0295	-5.9	.1691	10.99	77.15	1.613	1.227
28	74.5	16.0	11.5	.0382	-5.4	.2191	11.39	76.46	1.686	1.230
29	91.5	16.5	11.8	.0469	-5.1	.2691	11.94	76.01	1.766	1.231
30	125.5	17.9	12.5	.0644	-4.5	.3691	12.75	75.12	1.890	1.222
31	159.5	18.8	12.9	.0818	-4.0	.4691	13.39	74.46	1.967	1.206
32	193.5	19.7	13.3	.0992	-3.6	.5691	14.02	73.92	2.030	1.184
33	244.5	20.9	13.8	.1254	-3.1	.7191	14.92	73.23	2.057	1.133
34	312.5	22.6	14.5	.1603	-2.5	.9191	16.13	72.27	1.982	1.015
35	397.5	24.6	15.1	.2039	-1.8	1.1691	17.55	71.40	1.731	.857
36	482.5	26.5	15.7	.2475	-1.3	1.4191	18.88	70.59	1.336	.656
37	567.5	28.0	16.2	.2911	-.8	1.6691	19.96	69.96	.832	.422
38	652.5	29.3	16.6	.3347	-.4	1.9191	20.84	69.32	.476	.212
39	737.5	29.8	16.8	.3783	-.1	2.1691	21.20	68.99	.195	.067
40	822.5	29.8	16.9	.4219	-.0	2.4191	21.22	68.94	.000	.000
41	907.5	29.8	16.9	.4654	-.0	2.6691	21.21	68.84	.000	.022
42	921.9	29.8	16.9	.4729	-.0	2.7116	21.22	68.94	.000	.029

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00183 DELM = 2.439 REM = 2528.0
V RUN = 111571-1 CF/2 = .00105 DELM = 2.354 REM = 3740.0
PLATE = 18 UINF = 20.6 DEL2 = .2373 DEL3 = 6.631
X(IN) = 70.00 GM = 4.670 THETA = .3511 DEL* = 33.966
K(E06) = -.1940 GAM = -1.111 BETA = 1.060 M = 1.619

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.3	0.0000	0.00	92.75	1.000	1.080
2	1.7	1.8	1.2	.0008	-16.1	.0053	1.26	91.10	1.049	1.025
3	2.1	2.2	1.5	.0009	-15.9	.0063	1.50	90.77	1.059	1.030
4	2.4	2.5	1.7	.0011	-15.7	.0073	1.74	90.51	1.067	1.034
5	2.7	2.9	2.0	.0012	-15.5	.0083	1.98	90.22	1.077	1.039
6	3.0	3.3	2.2	.0013	-15.2	.0093	2.22	89.86	1.086	1.044
7	3.7	3.9	2.7	.0016	-14.6	.0113	2.68	89.14	1.104	1.057
8	4.3	4.6	3.3	.0019	-14.0	.0133	3.15	88.21	1.127	1.070
9	5.0	5.2	3.7	.0022	-13.6	.0153	3.57	87.56	1.142	1.080
10	5.6	5.9	4.3	.0025	-13.0	.0173	4.05	86.62	1.162	1.091
11	6.3	6.5	4.5	.0028	-12.5	.0193	4.44	86.09	1.177	1.102
12	6.9	6.9	5.2	.0031	-12.1	.0213	4.73	85.58	1.190	1.110
13	8.7	8.1	5.9	.0037	-11.4	.0253	5.54	84.55	1.223	1.125
14	9.6	9.6	6.4	.0042	-10.9	.0293	5.88	83.84	1.240	1.136
15	11.2	9.3	7.0	.0053	-10.3	.0343	6.35	82.98	1.262	1.148
16	12.8	10.2	7.6	.0058	-9.7	.0393	6.97	82.24	1.291	1.159
17	14.4	11.0	8.1	.0065	-9.2	.0443	7.53	81.52	1.315	1.169
18	16.1	11.6	8.5	.0072	-8.8	.0493	7.91	80.90	1.334	1.178
19	17.7	11.9	8.7	.0080	-8.6	.0543	8.15	80.63	1.349	1.182
20	19.3	12.1	9.0	.0087	-8.3	.0593	8.29	80.27	1.361	1.187
21	22.6	12.7	9.3	.0102	-8.0	.0693	8.64	79.86	1.387	1.193
22	25.8	13.1	9.5	.0117	-7.8	.0793	8.96	79.53	1.412	1.198
23	29.1	13.5	9.9	.0131	-7.4	.0893	9.23	78.94	1.435	1.204
24	32.2	14.3	10.6	.0169	-6.7	.1143	9.75	78.04	1.495	1.213
25	45.4	14.7	10.9	.0205	-6.5	.1393	10.05	77.77	1.524	1.217
26	51.5	15.1	11.2	.0242	-6.1	.1643	10.29	77.24	1.560	1.220
27	59.8	15.8	11.6	.0316	-5.7	.2143	10.77	76.64	1.636	1.226
28	86.1	16.5	12.0	.0390	-5.3	.2643	11.25	76.10	1.716	1.228
29	110.5	17.2	12.5	.0500	-4.9	.3393	11.74	75.45	1.812	1.225
30	143.1	18.2	12.9	.0648	-4.5	.4393	12.44	74.91	1.929	1.213
31	175.7	19.2	13.3	.0795	-4.0	.5393	13.10	74.31	2.029	1.185
32	240.8	20.5	13.9	.1090	-3.4	.7393	14.03	73.47	2.103	1.140
33	273.4	21.3	14.2	.1238	-3.1	.8393	14.55	73.05	2.110	1.107
34	338.5	22.9	14.7	.1532	-2.6	1.0393	15.56	72.36	2.085	1.029
35	403.7	24.3	15.2	.1827	-2.1	1.2393	16.57	71.64	1.966	.905
36	468.8	25.5	15.6	.2122	-1.7	1.4393	17.35	71.07	1.723	.787
37	550.3	27.1	16.1	.2491	-1.2	1.6893	18.52	70.41	1.362	.627
38	631.7	28.5	16.5	.2860	-.8	1.9393	19.44	69.80	.908	.439
39	794.6	30.0	17.1	.3597	-.2	2.4392	20.51	68.93	.214	.093
40	957.4	30.2	17.3	.4334	.0	2.9393	20.63	68.69	.000	.000
41	1120.3	30.2	17.3	.5072	.0	3.4393	20.63	68.69	.000	.042

DATE = 111471 (-0.15, 0.001, -0.17)

T RUN = 111471-1 STNA = .00178 DELH = 2.956 REM = 2995.0
V RUN = 111571-1 CF/2 = .00102 DELM = 2.687 REM = 4173.9
PLATE = 21 UINF = 28.3 DEL2 = .2772 DEL3 = 7.730
X(IN) = 92.00 GH = 4.699 THETA = .3996 DEL4 = 36.327
K(E06) = -.1560 GAM = -1.091 BETA = 1.937 M = 1.597

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-17.6	0.0000	0.00	92.51
2	1.4	1.5	1.0	.0006	-16.5	.0046	1.00	91.10
3	1.9	1.9	1.3	.0007	-16.3	.0056	1.23	90.83
4	2.1	2.2	1.5	.0008	-16.1	.0066	1.45	90.54
5	2.4	2.5	1.7	.0010	-15.9	.0076	1.68	90.27
6	2.7	2.9	2.0	.0011	-15.6	.0086	1.91	89.86
7	3.3	3.6	2.5	.0014	-15.1	.0106	2.35	89.18
8	4.0	4.2	3.1	.0016	-14.5	.0126	2.79	88.45
9	4.6	4.8	3.5	.0019	-14.1	.0146	3.21	87.83
10	5.2	5.4	4.1	.0021	-13.5	.0166	3.61	87.06
11	5.9	6.0	4.4	.0024	-13.1	.0186	3.97	86.59
12	6.5	6.5	4.8	.0026	-12.7	.0206	4.29	86.06
13	7.1	7.0	5.2	.0029	-12.4	.0226	4.64	85.55
14	8.4	8.2	5.9	.0034	-11.7	.0266	5.43	84.72
15	9.7	9.1	6.6	.0039	-11.1	.0306	6.03	83.97
16	11.3	9.8	6.9	.0045	-10.6	.0356	6.46	83.27
17	12.8	10.3	7.4	.0052	-10.1	.0406	6.82	82.66
18	16.0	11.4	8.3	.0064	-9.3	.0506	7.56	81.43
19	19.2	12.6	9.0	.0077	-8.6	.0606	8.32	80.51
20	22.3	13.1	9.3	.0089	-8.3	.0706	8.69	80.10
21	25.5	13.4	9.5	.0102	-8.0	.0806	8.89	79.74
22	33.4	14.3	10.4	.0134	-7.1	.1056	9.49	78.58
23	41.3	14.6	10.6	.0165	-6.9	.1306	9.71	78.23
24	49.2	15.0	10.9	.0197	-6.6	.1556	9.93	77.89
25	57.1	15.5	11.1	.0229	-6.3	.1806	10.28	77.39
26	73.0	16.4	11.7	.0292	-5.8	.2306	10.90	76.79
27	88.8	17.1	12.0	.0355	-5.5	.2806	11.31	76.37
28	120.4	18.0	12.6	.0482	-5.0	.3806	11.90	75.69
29	152.1	19.7	12.9	.0609	-4.7	.4806	12.42	75.30
30	199.5	19.6	13.5	.0798	-4.1	.6306	13.00	74.46
31	262.8	20.9	14.1	.1052	-3.5	.8306	13.53	73.69
32	326.1	22.4	14.5	.1305	-3.0	1.0306	14.37	73.02
33	389.4	23.5	15.0	.1558	-2.5	1.2306	15.07	72.42
34	452.6	24.8	15.4	.1811	-2.1	1.4306	15.45	71.89
35	531.7	26.0	15.9	.2128	-1.7	1.6806	17.24	71.25
36	610.8	27.6	16.3	.2444	-1.2	1.9306	19.27	70.62
37	689.9	28.8	16.7	.2761	-.9	2.1806	19.96	70.17
38	769.0	29.7	17.0	.3077	-.5	2.4306	19.67	69.68
39	927.2	30.6	17.5	.3710	-.1	2.9306	20.28	69.11
40	1085.4	30.7	17.6	.4343	.0	3.4306	20.32	68.96
41	1243.6	30.7	17.6	.4976	.0	3.9306	20.33	68.96

DATE = 111871 (-0.15, 0.002, -0.17)

T RUN = 111871-1 STNA = .00346 DELH = .168 REM = 187.0
V RUN = 111771-3 CF/2 = .00230 DELM = .319 REM = 542.0
PLATE = 1 UINF = 29.4 DEL2 = .0122 DEL3 = .373
X(IN) = 2.00 GH = 5.662 THETA = .0380 DEL4 = 2.110
K(E06) = -.4520 GAM = -.405 BETA = .189 M = 1.649

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-13.5	0.0000	0.00	91.79
2	3.1	3.9	2.3	.0120	-11.2	.0046	5.59	87.18
3	3.5	4.4	2.9	.0146	-10.6	.0056	6.32	86.03
4	4.5	4.9	3.5	.0172	-10.0	.0066	7.06	84.93
5	5.2	5.4	4.1	.0198	-9.4	.0076	7.80	83.66
6	5.9	5.9	4.7	.0224	-8.8	.0086	8.50	82.56
7	6.6	6.3	5.2	.0250	-8.3	.0096	9.15	81.58
8	7.3	6.8	5.6	.0277	-7.9	.0106	9.82	80.72
9	8.0	7.3	6.1	.0303	-7.4	.0116	10.48	79.86
10	8.7	7.7	6.4	.0329	-7.1	.0126	11.06	79.23
11	9.3	8.0	6.7	.0355	-6.8	.0136	11.54	78.58
12	10.0	8.3	7.1	.0381	-6.4	.0146	12.00	77.83
13	10.7	8.6	7.3	.0407	-6.2	.0156	12.49	77.38
14	11.4	9.0	7.6	.0433	-5.9	.0166	12.95	76.88
15	12.1	9.2	7.8	.0460	-5.7	.0176	13.36	76.46
16	12.8	9.5	8.1	.0486	-5.4	.0186	13.77	75.93
17	14.2	9.8	8.5	.0538	-5.0	.0206	14.33	75.17
18	15.6	10.3	8.8	.0590	-4.7	.0225	14.87	74.52
19	16.9	10.7	9.2	.0643	-4.3	.0246	15.40	73.77
20	18.3	11.0	9.4	.0695	-4.1	.0266	15.91	73.32
21	19.7	11.3	9.7	.0747	-3.8	.0285	16.36	72.84
22	21.1	11.6	9.9	.0799	-3.6	.0306	16.74	72.45
23	23.8	12.0	10.2	.0904	-3.3	.0346	17.34	71.79
24	26.6	12.4	10.5	.1009	-2.9	.0386	17.92	71.12
25	29.3	12.7	10.8	.1114	-2.7	.0426	18.35	70.59
26	32.0	13.1	11.1	.1244	-2.4	.0476	18.89	70.02
27	36.2	13.4	11.3	.1375	-2.1	.0526	19.40	69.54
28	39.7	13.7	11.5	.1505	-1.9	.0576	19.84	69.14
29	43.1	14.0	11.8	.1636	-1.7	.0626	20.23	68.69
30	50.0	14.6	12.1	.1898	-1.4	.0726	21.04	68.03
31	56.9	15.0	12.4	.2159	-1.1	.0826	21.68	67.49
32	63.8	15.4	12.6	.2421	-.9	.0926	22.29	67.06
33	70.7	15.8	12.9	.2682	-.7	.1026	22.90	66.70
34	77.6	16.2	12.9	.2944	-.5	.1126	23.40	66.40
35	91.4	16.9	13.2	.3466	-.3	.1326	24.39	65.97
36	105.1	17.4	13.3	.3989	-.2	.1526	25.22	65.67
37	119.9	18.0	13.4	.4512	-.1	.1726	26.03	65.49
38	132.7	18.5	13.5	.5035	-.0	.1926	26.72	65.39
39	146.5	18.9	13.5	.5558	-.0	.2126	27.35	65.33
40	163.7	19.3	13.5	.6212	.0	.2376	27.92	65.27
41	180.9	19.7	13.5	.6866	.0	.2626	28.45	65.27
42	184.9	19.8	13.5	.7014	.0	.2683	28.55	65.27
43	212.4	20.1	13.5	.8060	.0	.3083	29.06	65.26
44	246.9	20.3	13.5	.9367	.0	.3583	29.36	65.26
45	281.3	20.3	13.5	1.0675	.0	.4083	29.41	65.26
46	322.7	20.4	13.5	1.2243	.0	.4683	29.41	65.26
47	364.0	20.4	13.5	1.3812	.0	.5283	29.41	65.26

DATE = 111971 (-0.15, 0.002, -0.17)

T RUN = 111971-1 STNA = .00232 DELH = .533 REM = 691.0
V RUN = 111771-3 CF/2 = .00150 DELM = .579 REM = 1196.0
PLATE = 3 UINF = 26.5 DEL2 = .0501 DEL3 = 1.529
X(IN) = 10.00 GH = 5.567 THETA = .0968 DEL4 = 5.543
K(E06) = -.9470 GAM = -1.373 BETA = 1.114 M = 1.738

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.3	0.0000	0.00	91.65	1.000	1.000
2	2.6	3.6	1.9	.0033	-14.5	.0051	3.75	88.74	1.247	1.087
3	3.1	3.9	2.7	.0040	-14.1	.0061	4.13	88.09	1.267	1.107
4	3.6	4.3	2.7	.0046	-13.6	.0071	4.52	87.30	1.294	1.130
5	4.1	4.7	3.2	.0052	-13.1	.0081	4.98	86.52	1.322	1.153
6	4.6	5.1	3.6	.0059	-12.6	.0091	5.37	85.76	1.349	1.175
7	5.1	5.5	4.1	.0065	-12.2	.0101	5.75	85.05	1.374	1.195
8	5.6	5.8	4.4	.0071	-11.9	.0111	6.14	84.49	1.400	1.212
9	6.1	6.2	4.8	.0078	-11.5	.0121	6.54	83.84	1.425	1.231
10	6.6	6.6	5.1	.0084	-11.2	.0131	6.93	83.36	1.451	1.249
11	7.1	6.9	5.5	.0091	-10.8	.0141	7.30	82.83	1.474	1.260
12	7.6	7.3	5.7	.0097	-10.6	.0151	7.63	82.44	1.496	1.271
13	8.1	7.6	6.0	.0103	-10.3	.0161	7.95	82.08	1.517	1.284
14	8.6	7.8	6.2	.0110	-10.1	.0171	8.25	81.61	1.537	1.295
15	9.1	8.1	6.5	.0116	-9.8	.0181	8.55	81.17	1.557	1.305
16	9.6	8.4	6.7	.0122	-9.6	.0191	8.83	80.81	1.575	1.318
17	10.1	8.6	6.9	.0129	-9.4	.0201	9.05	80.45	1.592	1.325
18	11.1	9.0	7.3	.0142	-9.0	.0221	9.49	79.89	1.621	1.344
19	12.1	9.3	7.7	.0154	-8.6	.0241	9.93	79.26	1.646	1.361
20	13.1	9.6	7.9	.0167	-8.4	.0261	10.15	78.91	1.669	1.371
21	14.1	9.9	8.1	.0180	-8.2	.0281	10.43	78.52	1.690	1.382
22	15.1	10.2	8.3	.0193	-7.9	.0301	10.70	78.16	1.710	1.392
23	17.6	10.7	8.9	.0225	-7.4	.0351	11.28	77.31	1.754	1.412
24	20.2	11.2	9.2	.0258	-7.0	.0401	11.75	76.70	1.792	1.425
25	22.7	11.7	9.6	.0288	-6.7	.0451	12.26	76.16	1.829	1.439
26	25.2	11.9	9.9	.0320	-6.4	.0501	12.56	75.71	1.847	1.448
27	30.2	12.5	10.3	.0384	-5.9	.0601	13.12	74.94	1.885	1.458
28	35.2	13.1	10.7	.0448	-5.6	.0701	13.73	74.34	1.919	1.462
29	40.2	13.5	11.0	.0512	-5.2	.0801	14.17	73.80	1.938	1.469
30	47.8	14.0	11.5	.0607	-4.8	.0951	14.78	73.14	1.949	1.447
31	60.3	14.9	12.0	.0767	-4.3	.1201	15.67	72.21	1.944	1.411
32	72.9	15.7	12.5	.0926	-3.8	.1451	16.54	71.43	1.914	1.368
33	85.4	16.4	13.0	.1086	-3.3	.1701	17.22	70.71	1.838	1.296
34	97.9	17.1	13.3	.1249	-3.0	.1951	17.96	70.11	1.758	1.227
35	110.5	17.8	13.7	.1405	-2.6	.2201	18.74	69.57	1.673	1.150
36	135.6	19.1	14.3	.1724	-2.0	.2701	20.14	68.57	1.459	.976
37	160.7	20.5	14.8	.2043	-1.5	.3201	21.52	67.73	1.255	.793
38	185.8	21.6	15.2	.2362	-1.0	.3701	22.76	67.00	1.069	.603
39	210.9	22.8	15.6	.2681	-.7	.4201	23.94	66.40	.944	.422
40	261.1	24.4	16.1	.3319	-.2	.5201	25.78	65.61	.731	.136
41	311.3	25.1	16.3	.3957	.0	.6201	26.43	65.30	.363	.000
42	311.8	25.1	16.3	.3964	.0	.6212	26.44	65.30	.357	.000
43	349.5	25.2	16.3	.4443	-.0	.6962	26.51	65.30	.000	.002
44	399.6	25.2	16.3	.5081	-.0	.7962	26.51	65.30	.000	.001

DATE = 111871 (-0.15, 0.002, -0.17)

T RUN = 111871-1 STNA = .00190 DELH = 1.043 REM = 1296.0
V RUN = 111771-3 CF/2 = .00108 DELM = 1.032 REM = 2035.0
PLATE = 6 UINF = 24.2 DEL2 = .1030 DEL3 = 3.140
X(IN) = 22.00 GH = 5.376 THETA = .1618 DEL4 = 16.041
K(E06) = -.4720 GAM = -1.263 BETA = 1.467 M = 1.760

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.9	0.0000	0.00	91.41	1.000	1.000
2	1.9	2.1	1.4	.0016	-15.5	.0049	1.71	89.33	1.133	1.068
3	2.3	2.6	1.7	.0019	-15.2	.0059	2.08	88.83	1.161	1.084
4	2.7	3.0	2.0	.0022	-14.9	.0069	2.45	88.36	1.189	1.100
5	3.1	3.5	2.3	.0025	-14.6	.0079	2.82	87.99	1.238	1.115
6	3.5	3.9	2.6	.0028	-14.3	.0089	3.16	87.36	1.285	1.133
7	3.9	4.4	2.9	.0031	-13.9	.0099	3.55	86.88	1.307	1.148
8	4.3	4.8	3.3	.0034	-13.5	.0109	3.90	86.26	1.324	1.169
9	4.6	5.2	3.6	.0038	-13.3	.0119	4.23	85.82	1.346	1.183
10	5.0	5.6	4.0	.0041	-12.9	.0129	4.58	85.29	1.369	1.200
11	5.4	5.9	4.2	.0044	-12.7	.0139	4.80	84.90	1.390	1.213
12	6.2	6.5	4.8	.0050	-12.0	.0159	5.27	83.93	1.430	1.249
13	7.0	7.1	5.4	.0056	-11.5	.0179	5.77	83.13	1.470	1.271
14	7.8	7.6	5.8	.0062	-11.1	.0199	6.18	82.44	1.505	1.293
15	8.5	8.0	6.1	.0069	-10.8	.0219	6.52	81.97	1.536	1.309
16	9.3	8.5	6.4	.0075	-10.4	.0239	6.89	81.46	1.569	1.326
17	10.1	8.9	6.9	.0081	-10.0	.0259	7.25	80.81	1.602	1.346
18	11.6	9.6	7.3	.0093	-9.6	.0299	7.93	80.16	1.667	1.369
19	13.2	10.3	7.7	.0106	-9.2	.0339	8.43	79.50	1.707	1.389
20	14.8	10.7	8.1	.0119	-8.8	.0379	8.78	78.91	1.742	1.405
21	16.3	11.2	8.3	.0131	-8.5	.0419	9.09	78.49	1.778	1.421
22	17.9	11.5	8.6	.0143	-8.2	.0459	9.38	78.07	1.811	1.434
23	19.8	11.9	9.0	.0159	-7.9	.0509	9.67	77.54	1.847	1.449
24	21.8	12.2	9.1	.0174	-7.7	.0559	9.92	77.27	1.878	1.457
25	25.7	12.7	9.6	.0205	-7.3	.0659	10.32	76.59	1.939	1.476
26	29.5	13.1	9.9	.0236	-6.9	.0759	10.66	76.01	1.987	1.490
27	35.4	13.7	10.3	.0283	-6.5	.0909	11.18	75.39	2.060	1.503
28	45.1	14.6	10.8	.0361	-6.0	.1159	11.95	74.64	2.166	1.514
29	54.8	15.2	11.3	.0438	-5.6	.1409	12.42	73.95	2.247	1.517
30	64.6	15.8	11.6	.0516	-5.3	.1659	12.86	73.47	2.310	1.516
31	74.3	16.4	11.9	.0594	-4.9	.1909	13.34	72.96	2.367	1.508
32	93.8	17.4	12.4	.0749	-4.5	.2409	14.14	72.21	2.427	1.484
33	113.2	18.2	12.9	.0905	-4.0	.2909	14.83	71.43	2.429	1.443
34	142.4	19.7	13.5	.1138	-3.4	.3659	16.04	70.56	2.377	1.370
35	191.3	21.6	14.2	.1449	-2.7	.4659	17.59	69.43	2.163	1.235
36	220.2	23.3	14.8	.1759	-2.1	.5659	19.01	68.52	1.819	1.087
37	259.1	25.1	15.4	.2070	-1.5	.6659	20.42	67.64	1.494	.886
38	299.1	26.7	15.8	.2391	-1.1	.7659	21.74	66.95	1.251	.668
39	337.0	28.1	16.2	.2692	-.8	.8659	22.87	66.28	1.048	.441
40	395.3	29.4	16.7	.3156	-.2	1.0159	23.94	65.58	.682	.156
41	473.2	29.7	16.9	.3780	.0	1.2159	24.28	65.25	.000	.000
42	518.8	29.7	16.9	.4144	.0	1.3332	24.28	65.25	.000	.000

DATE = 111871 (-0.15, 0.002, -0.17)

T RUN = 111871-1 STNA = .00174 DELH = 1.903 REM = 1747.0
V RUN = 111771-3 CF/2 = .00087 DELM = 1.465 REM = 2679.0
PLATE = 9 UINF = 22.5 DEL2 = .1493 DEL3 = 4.362
X(IN) = 34.00 GM = 5.107 THETA = .2250 DEL4 = 22.279
K(E06) = -.3360 GAM = -1.213 BETA = 1.767 M = 1.742

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.5	0.0000	0.00	91.44	1.000	1.000
2	1.7	1.9	1.2	.0012	-15.3	.0092	1.25	89.42	1.123	1.068
3	2.0	2.3	1.5	.0014	-15.0	.0062	1.54	89.07	1.148	1.079
4	2.3	2.6	1.7	.0017	-14.8	.0072	1.80	88.74	1.173	1.090
5	2.7	3.0	2.0	.0019	-14.6	.0082	2.06	88.36	1.198	1.103
6	3.0	3.4	2.3	.0021	-14.3	.0092	2.32	87.96	1.223	1.120
7	3.6	4.2	2.9	.0026	-13.8	.0112	2.85	86.85	1.272	1.153
8	4.3	4.9	3.5	.0030	-13.1	.0132	3.34	85.97	1.320	1.183
9	4.9	5.6	4.1	.0034	-12.5	.0152	3.81	85.02	1.360	1.214
10	5.6	6.2	4.4	.0039	-12.2	.0172	4.22	84.52	1.403	1.231
11	6.2	6.9	4.8	.0043	-11.7	.0192	4.70	83.78	1.452	1.256
12	6.9	7.4	5.2	.0048	-11.3	.0212	5.04	83.13	1.487	1.275
13	7.5	7.8	5.6	.0052	-10.9	.0232	5.25	82.50	1.514	1.299
14	8.2	8.2	5.9	.0057	-10.6	.0252	5.58	82.03	1.545	1.314
15	8.8	8.6	6.2	.0061	-10.3	.0272	5.86	81.61	1.575	1.328
16	9.5	8.9	6.5	.0066	-10.1	.0292	6.09	81.23	1.600	1.341
17	10.8	9.6	6.9	.0075	-9.7	.0332	6.52	80.54	1.649	1.363
18	12.4	10.5	7.3	.0086	-9.2	.0392	7.12	79.63	1.715	1.387
19	14.0	11.2	7.7	.0097	-8.8	.0432	7.62	79.14	1.777	1.407
20	15.7	11.7	8.1	.0108	-8.5	.0482	7.98	78.67	1.818	1.424
21	17.3	12.2	8.3	.0119	-8.2	.0532	8.26	78.28	1.857	1.437
22	20.5	12.8	8.7	.0142	-7.8	.0632	8.73	77.60	1.926	1.455
23	23.8	13.4	9.0	.0164	-7.5	.0732	9.11	77.19	1.987	1.471
24	28.6	14.2	9.5	.0198	-7.0	.0882	9.63	76.31	2.075	1.493
25	36.8	15.1	10.0	.0254	-6.5	.1132	10.25	75.57	2.198	1.512
26	44.9	15.8	10.4	.0310	-6.2	.1382	10.75	75.03	2.297	1.523
27	53.0	16.4	10.7	.0366	-5.9	.1632	11.12	74.55	2.384	1.529
28	69.2	17.1	11.2	.0477	-5.3	.2132	11.65	73.68	2.525	1.534
29	85.5	18.0	11.6	.0589	-4.9	.2632	12.27	73.06	2.666	1.529
30	101.7	18.8	11.9	.0701	-4.6	.3132	12.78	72.52	2.766	1.519
31	126.1	20.0	12.5	.0869	-4.1	.3882	13.58	71.71	2.895	1.489
32	150.5	21.1	12.9	.1037	-3.7	.4632	14.35	71.02	2.963	1.446
33	182.9	22.6	13.4	.1260	-3.2	.5632	15.37	70.23	2.966	1.375
34	215.4	24.0	13.9	.1484	-2.7	.6632	16.34	69.49	2.852	1.286
35	264.1	26.0	14.5	.1820	-2.0	.8132	17.69	68.46	2.644	1.118
36	329.1	28.9	15.2	.2267	-1.3	1.0132	19.63	67.34	1.783	.945
37	394.1	31.2	15.8	.2714	-.7	1.2132	21.21	66.35	1.156	.513
38	459.0	32.6	16.3	.3162	-.2	1.4132	22.17	65.62	.607	.200
39	540.2	33.1	16.5	.3721	-.0	1.6632	22.51	65.26	.000	.000
40	621.4	33.1	16.5	.4280	-.0	1.9132	22.51	65.23	.000	.000

DATE = 111871 (-0.15, 0.002, -0.17)

T RUN = 111871-1 STNA = .00165 DELH = 1.971 REM = 2215.0
V RUN = 111771-3 CF/2 = .00082 DELM = 1.477 REM = 3372.0
PLATE = 12 UINF = 21.9 DEL2 = .1946 DEL3 = 5.767
X(IN) = 46.00 GM = 5.040 THETA = .2963 DEL4 = 29.017
K(E06) = -.2630 GAM = -1.193 BETA = 1.784 M = 1.743

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.9	0.0000	0.00	91.55	1.000	1.000
2	1.4	1.5	1.0	.0008	-15.9	.0048	.98	89.98	1.093	1.053
3	1.7	1.8	1.2	.0010	-15.7	.0055	1.14	89.63	1.115	1.064
4	2.0	2.2	1.5	.0011	-15.5	.0065	1.41	89.24	1.137	1.077
5	2.3	2.6	1.7	.0013	-15.2	.0075	1.63	88.89	1.159	1.089
6	2.6	2.9	1.9	.0015	-15.0	.0085	1.87	88.51	1.181	1.101
7	3.2	3.6	2.4	.0018	-14.5	.0105	2.32	87.77	1.225	1.126
8	3.8	4.3	3.0	.0021	-14.0	.0125	2.78	86.91	1.270	1.154
9	4.5	5.0	3.5	.0026	-13.2	.0155	3.42	85.67	1.342	1.195
10	5.7	6.1	4.4	.0032	-12.6	.0185	3.92	84.79	1.397	1.227
11	6.6	7.0	4.9	.0037	-12.0	.0215	4.52	83.87	1.457	1.255
12	7.5	7.9	5.5	.0042	-11.5	.0245	5.10	83.31	1.507	1.284
13	8.7	8.5	6.0	.0049	-10.9	.0285	5.65	82.15	1.568	1.312
14	10.0	9.5	6.5	.0055	-10.4	.0325	6.10	81.38	1.614	1.337
15	11.2	10.0	6.9	.0062	-10.0	.0365	6.46	80.79	1.655	1.359
16	12.4	10.5	7.2	.0069	-9.7	.0405	6.78	80.28	1.694	1.373
17	13.7	11.0	7.5	.0076	-9.4	.0445	7.06	79.77	1.729	1.390
18	15.2	11.4	8.0	.0084	-9.0	.0495	7.36	79.15	1.764	1.409
19	16.7	11.8	8.2	.0093	-8.7	.0545	7.61	78.70	1.804	1.424
20	18.9	12.6	8.7	.0110	-8.3	.0645	8.07	78.04	1.870	1.445
21	22.9	13.2	9.0	.0126	-8.0	.0745	8.48	77.54	1.931	1.460
22	27.5	13.9	9.3	.0152	-7.6	.0895	8.91	76.97	2.005	1.478
23	35.1	14.4	9.9	.0194	-7.0	.1145	9.22	76.11	2.094	1.502
24	42.8	15.2	10.3	.0237	-6.7	.1395	9.76	75.54	2.191	1.516
25	50.5	15.9	10.6	.0279	-6.4	.1645	10.22	75.06	2.266	1.527
26	65.8	16.7	11.1	.0364	-5.8	.2145	10.74	74.25	2.430	1.542
27	81.2	17.4	11.5	.0449	-5.5	.2645	11.17	73.66	2.562	1.549
28	104.2	18.7	12.1	.0576	-5.0	.3395	12.02	72.91	2.772	1.549
29	127.2	19.6	12.4	.0703	-4.5	.4145	12.61	72.22	2.915	1.541
30	157.9	20.8	12.9	.0872	-4.1	.5145	13.37	71.47	3.054	1.521
31	188.6	21.9	13.3	.1042	-3.7	.6145	14.10	70.87	3.119	1.487
32	250.0	24.1	14.1	.1381	-2.9	.8145	15.48	69.61	3.075	1.387
33	311.4	26.7	14.7	.1720	-2.2	1.0145	17.16	68.61	2.883	1.213
34	372.8	28.7	15.3	.2059	-1.7	1.2145	18.44	67.77	2.349	1.022
35	434.1	30.7	15.7	.2398	-1.2	1.4145	19.76	66.98	1.764	.793
36	510.9	32.7	16.3	.2821	-.8	1.6645	21.05	66.08	1.108	.456
37	587.6	33.9	16.7	.3245	-.2	1.9145	21.76	65.47	.598	.171
38	664.3	34.1	16.9	.3669	-.0	2.1645	21.94	65.17	.187	.033
39	741.1	34.1	16.9	.4092	-.0	2.4145	21.92	65.14	.000	.000
40	817.8	34.1	16.9	.4516	-.0	2.6645	21.92	65.14	.000	.000

DATE = 111871 (-0.15, 0.002, -0.17)

T RUN = 111871-1 STNA = .00158 DELH = 2.368 REM = 2614.0
V RUN = 111771-3 CF/2 = .00079 DELM = 2.365 REM = 3948.0
PLATE = 15 UINF = 21.2 DEL2 = .2374 DEL3 = 7.051
X(IN) = 58.00 GM = 5.019 THETA = .3545 DEL4 = 35.358
K(E06) = -.2180 GAM = -1.206 BETA = 1.797 M = 1.713

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.4	0.0000	0.00	91.27	1.000	1.000
2	1.7	1.8	1.2	.0008	-16.1	.0058	1.12	89.45	1.110	1.062
3	2.0	2.2	1.4	.0009	-15.9	.0068	1.32	89.13	1.130	1.072
4	2.3	2.5	1.7	.0011	-15.8	.0078	1.52	88.86	1.150	1.082
5	2.6	2.8	1.9	.0012	-15.5	.0088	1.72	88.48	1.170	1.094
6	3.2	3.5	2.3	.0015	-15.0	.0108	2.14	87.74	1.210	1.119
7	3.7	4.2	2.8	.0018	-14.5	.0128	2.54	87.00	1.250	1.145
8	4.3	4.8	3.3	.0020	-14.1	.0148	2.93	86.32	1.288	1.168
9	5.2	5.7	4.0	.0025	-13.4	.0178	3.48	85.32	1.342	1.201
10	6.1	6.5	4.7	.0029	-12.7	.0208	3.98	84.25	1.396	1.237
11	6.9	7.2	5.2	.0033	-12.2	.0238	4.37	83.51	1.439	1.262
12	7.8	8.0	5.7	.0037	-11.7	.0268	4.88	82.74	1.489	1.288
13	9.0	8.9	6.2	.0043	-11.2	.0308	5.44	82.00	1.547	1.313
14	10.2	9.6	6.7	.0048	-10.7	.0348	5.82	81.26	1.590	1.338
15	11.6	10.4	7.1	.0055	-10.2	.0398	6.34	80.60	1.646	1.360
16	13.1	11.2	7.5	.0062	-9.8	.0448	6.82	79.99	1.699	1.381
17	15.1	11.9	8.2	.0072	-9.2	.0515	7.27	79.02	1.755	1.412
18	18.9	12.7	8.7	.0090	-8.7	.0648	7.78	78.25	1.830	1.437
19	21.8	13.3	9.1	.0103	-8.2	.0748	8.09	77.60	1.880	1.457
20	26.2	14.0	9.5	.0124	-7.9	.0898	8.52	77.06	1.952	1.474
21	33.5	14.8	10.0	.0159	-7.3	.1148	9.08	76.20	2.053	1.499
22	40.8	15.3	10.3	.0193	-7.0	.1398	9.35	75.75	2.140	1.513
23	55.4	16.4	11.0	.0263	-6.4	.1898	10.00	74.79	2.308	1.536
24	70.0	17.3	11.3	.0332	-6.0	.2398	10.55	74.25	2.459	1.549
25	84.6	18.0	11.7	.0401	-5.7	.2898	10.97	73.72	2.583	1.554
26	106.4	18.8	12.1	.0505	-5.2	.3648	11.58	73.09	2.738	1.556
27	135.6	19.9	12.7	.0643	-4.7	.4648	12.12	72.29	2.903	1.546
28	179.4	21.1	13.2	.0851	-4.1	.6148	12.85	71.41	3.077	1.515
29	237.7	23.2	13.9	.1128	-3.5	.8148	14.18	70.48	3.301	1.454
30	296.1	25.1	14.5	.1405	-2.8	1.0148	15.34	69.46	3.317	1.332
31	361.7	27.3	15.1	.1716	-2.3	1.2398	16.67	68.67	3.083	1.196
32	427.4	29.3	15.6	.2028	-1.7	1.4648	17.89	67.83	2.653	1.002
33	500.3	31.3	16.2	.2374	-1.2	1.7148	19.13	66.98	1.984	.754
34	558.7	32.8	16.5	.2651	-.8	1.9148	20.01	66.47	1.425	.578
35	631.6	34.0	17.0	.2997	-.4	2.1648	20.75	65.81	.914	.306
36	704.5	34.6	17.2	.3343	-.1	2.4148	21.12	65.38	.340	.096
37	777.5	34.8	17.4	.3689	.0	2.6643	21.22	65.20	.032	.000
38	850.4	34.8	17.4	.4035	.0	2.9148	21.22	65.20	.000	.018
39	878.2	34.8	17.4	.4167	.0	3.0101	21.22	65.20	.000	.026

DATE = 111871 (-0.15, 0.002, -0.17)

T RUN = 111871-1 STNA = .00153 DELH = 2.949 REM = 3060.0
V RUN = 111771-3 CF/2 = .00076 DELM = 2.706 REM = 4504.0
PLATE = 18 UINF = 20.6 DEL2 = .2851 DEL3 = 9.427
X(IN) = 70.00 GM = 4.991 THETA = .4197 DEL4 = 42.036
K(E06) = -.1880 GAM = -1.220 BETA = 1.838 M = 1.694

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.6	0.0000	0.00	91.17	1.000	1.000
2	1.5	1.6	1.1	.0006	-16.5	.0054	.94	89.63	1.095	1.053
3	1.9	1.9	1.3	.0007	-16.3	.0064	1.12	89.27	1.117	1.065
4	2.1	2.2	1.5	.0008	-16.1	.0074	1.31	88.99	1.132	1.075
5	2.3	2.6	1.7	.0010	-15.9	.0094	1.45	88.74	1.151	1.083
6	2.9	3.2	2.1	.0012	-15.5	.0104	1.57	88.06	1.188	1.106
7	3.4	3.8	2.6	.0014	-15.0	.0124	2.24	87.33	1.226	1.131
8	4.3	4.9	3.3	.0019	-14.3	.0154	2.78	86.29	1.280	1.167
9	5.1	5.6	4.0	.0021	-13.6	.0184	3.27	85.38	1.331	1.199
10	5.9	6.4	4.6	.0025	-13.0	.0214	3.72	84.40	1.377	1.231
11	6.8	7.1	5.1	.0028	-12.5	.0244	4.12	83.72	1.412	1.255
12	7.9	7.9	5.7	.0033	-11.9	.0284	4.59	82.77	1.470	1.287
13	9.0	8.9	6.2	.0037	-11.3	.0324	5.19	81.97	1.531	1.314
14	10.4	9.9	6.8	.0043	-10.8	.0374	5.71	81.17	1.589	1.341
15	11.8	10.3	7.2	.0049	-10.4	.0424	6.02	80.54	1.627	1.362
16	13.2	11.0	7.5	.0055	-10.0	.0474	6.39	80.07	1.670	1.378
17	15.1	11.8	8.1	.0063	-9.5	.0544	6.98	79.27	1.726	1.405
18	17.3	12.4	8.4	.0072	-9.1	.0624	7.22	78.76	1.775	1.422
19	20.1	13.0	8.8	.0084	-8.8	.0724	7.55	78.25	1.826	1.439
20	24.3	13.7	9.2	.0101	-8.4	.0874	7.98	77.60	1.894	1.460
21	29.9	14.5	9.7	.0124	-7.8	.1074	8.44	76.92	1.978	1.483
22	36.8	15.4	10.1	.0153	-7.4	.1324	8.97	76.26	2.077	1.500
23	43.8	16.0	10.5	.0182	-7.1	.1574	9.31	75.72	2.156	1.515
24	50.7	16.4	10.9	.0211	-6.7	.1824	9.54	75.18	2.224	1.528
25	64.6	17.1	11.2	.0269	-6.3	.2324	9.92	74.64	2.342	1.540
26	85.5	17.8	11.7	.0356	-5.9	.3074	10.38	73.96	2.484	1.550
27	106.3	18.6	12.1	.0443	-5.5	.3824	10.82	73.36	2.625	1.560
28	134.1	19.8	12.5	.0559	-5.0	.4824	11.52	72.73	2.818	1.564
29	162.0	20.5	13.0	.0675	-4.6	.5824	11.91	72.04	2.967	1.551
30	203.7	22.3	13.4	.0849	-4.2	.7324	12.97	71.44	3.223	1.531
31	259.3	23.8	14.0	.1080	-3.6	.9324	13.84	70.57	3.357	1.474
32	328.8	25.7	14.7	.1370	-2.9	1.1824	14.97	69.59	3.324	1.366
33	398.3	27.8	15.2	.1660	-2.4	1.4324	16.19	68.79	3.132	1.237
34	467.9	29.6	15.7	.1950	-1.8	1.6824	17.21	68.01	2.686	1.069
35	537.4	31.3	16.1	.2239	-1.4	1.9324	18.21	67.35	2.049	.898
36	620.8	33.2	16.7	.2587	-.9	2.2324	19.32	66.56	1.261	.612
37	704.2	34.7	17.1	.2935	-.4	2.5324	20.16	65.93	.695	.350
38	787.7	35.3	17.4	.3282	-.2	2.9324	20.55	65.54	.302	.180
39	871.1	35.5	17.6	.3630	-.0	3.1324	20.64	65.32	.040	.034
40	954.5	35.5	17.6	.3978	.0	3.4324	20.63	65.26	.000	.000
41	1010.1	35.5	17.6	.4210	.0	3.6324	20.63	65.26	.000	.000

DATE = 111971 (-0.15, 0.002, -0.17)

T RUN = 111971-1 STNA = .00149 DELM = 3.213 REM = 3386.0
V RUN = 111771-3 CF/2 = .00074 DELM = 3.089 REM = 5066.0
PLATE = 21 UINF = 20.2 DEL2 = .3222 DEL3 = 9.605
X(IN) = 82.00 GM = 4.972 THETA = .4821 DEL4 = 47.753
K(E06) = -.1690 GAM = -1.254 BETA = 1.905 H = 1.683

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-17.6	0.0000	0.00	91.13	1.000	1.000
2	1.7	1.6	1.2	.0006	-16.6	.0062	1.61	89.36	1.103	1.061
3	1.9	2.1	1.4	.0007	-16.4	.0072	1.18	89.04	1.121	1.072
4	2.2	2.4	1.6	.0008	-16.2	.0082	1.35	88.74	1.138	1.082
5	2.5	2.7	1.8	.0009	-16.1	.0092	1.53	88.57	1.156	1.088
6	3.0	3.3	2.3	.0011	-15.8	.0112	1.88	87.86	1.191	1.112
7	3.5	3.9	2.7	.0013	-15.1	.0132	2.22	87.18	1.226	1.135
8	4.1	4.5	3.2	.0016	-14.6	.0152	2.56	86.50	1.260	1.159
9	4.6	5.1	3.6	.0018	-14.2	.0172	2.88	85.94	1.293	1.178
10	5.2	5.7	4.0	.0020	-13.8	.0192	3.19	85.55	1.324	1.192
11	6.0	6.4	4.5	.0023	-13.3	.0222	3.60	84.67	1.368	1.222
12	6.8	7.1	5.1	.0026	-12.7	.0252	3.97	83.72	1.358	1.254
13	7.9	7.8	5.7	.0030	-12.2	.0292	4.41	82.95	1.458	1.280
14	8.9	8.7	6.1	.0034	-11.7	.0332	4.91	82.36	1.508	1.301
15	10.0	9.4	6.6	.0038	-11.2	.0372	5.31	81.58	1.547	1.328
16	11.4	10.1	7.1	.0043	-10.7	.0422	5.70	80.90	1.588	1.351
17	12.7	10.7	7.5	.0048	-10.3	.0472	6.04	80.34	1.626	1.371
18	14.0	11.3	7.9	.0053	-9.9	.0522	6.35	79.77	1.662	1.390
19	16.2	12.1	8.3	.0061	-9.6	.0602	6.84	79.21	1.719	1.409
20	18.9	13.0	8.6	.0071	-9.2	.0702	7.31	78.64	1.778	1.430
21	22.9	13.7	9.4	.0087	-8.4	.0852	7.72	77.60	1.940	1.466
22	27.0	14.2	9.5	.0102	-8.3	.1002	8.02	77.36	1.890	1.477
23	31.7	15.1	10.1	.0127	-7.7	.1252	8.47	76.58	1.972	1.508
24	40.4	15.7	10.6	.0153	-7.2	.1502	8.82	75.97	2.044	1.531
25	48.5	16.2	10.7	.0183	-7.1	.1802	9.13	75.63	2.121	1.543
26	56.6	16.6	11.1	.0214	-6.7	.2102	9.34	75.06	2.199	1.557
27	67.3	17.0	11.3	.0254	-6.5	.2502	9.57	74.82	2.273	1.563
28	80.8	17.5	11.6	.0305	-6.2	.3002	9.87	74.34	2.379	1.573
29	101.0	18.5	12.1	.0381	-5.7	.3752	10.43	73.57	2.537	1.587
30	127.9	19.6	12.5	.0483	-5.3	.4752	11.03	73.00	2.722	1.599
31	154.8	20.4	12.9	.0585	-4.9	.5752	11.49	72.49	2.890	1.601
32	195.2	21.6	13.4	.0737	-4.4	.7252	12.18	71.80	3.077	1.591
33	249.9	23.1	13.9	.0941	-3.9	.9252	12.98	71.05	3.176	1.571
34	316.3	24.8	14.5	.1195	-3.3	1.1752	13.97	70.15	3.330	1.561
35	383.6	26.7	15.0	.1449	-2.8	1.4252	15.04	69.40	3.367	1.421
36	464.3	28.6	15.6	.1754	-2.2	1.7252	16.10	68.61	3.063	1.311
37	545.0	30.5	16.1	.2059	-1.7	2.0252	17.17	67.80	2.628	1.132
38	652.7	33.1	16.7	.2465	-1.1	2.4252	18.62	66.95	1.786	.954
39	760.3	34.8	17.3	.2872	-.5	2.8252	19.61	66.14	.828	.493
40	869.0	35.7	17.7	.3279	-.1	3.2252	20.10	65.60	.233	.195
41	1029.5	35.9	17.8	.3888	.0	3.8252	20.21	65.36	.000	.000
42	1049.0	35.9	17.8	.3962	.0	3.8979	20.20	65.36	.000	.000

DATE = 111871 (-0.15, 0.002, -0.17)

T RUN = 111871-1 STNA = .00147 DELM = 3.560 REM = 3638.0
V RUN = 111771-3 CF/2 = .00073 DELM = 3.388 REM = 5418.0
PLATE = 23 UINF = 19.9 DEL2 = .3518 DEL3 = 10.465
X(IN) = 90.00 GM = 4.905 THETA = .5240 DEL4 = 51.335
K(E06) = -.1650 GAM = -1.345 BETA = 2.057 H = 1.677

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-17.9	0.0000	0.00	91.34
2	1.5	1.6	1.1	.0055	-16.8	.0055	.91	89.74
3	1.8	1.9	1.3	.0066	-16.6	.0066	1.07	89.42
4	2.1	2.2	1.5	.0077	-16.4	.0078	1.23	89.10
5	2.6	2.8	1.9	.0095	-16.0	.0098	1.57	88.54
6	3.1	3.5	2.3	.0011	-15.7	.0118	1.92	88.03
7	3.6	4.0	2.9	.0013	-15.1	.0138	2.23	87.21
8	4.4	4.9	3.5	.0016	-14.4	.0168	2.70	86.29
9	5.2	5.7	4.2	.0018	-13.7	.0195	3.14	85.23
10	5.0	6.4	4.6	.0021	-13.3	.0225	3.54	84.64
11	7.1	7.3	5.1	.0025	-12.8	.0268	4.06	83.90
12	8.1	7.9	5.9	.0029	-12.1	.0309	4.36	82.86
13	9.4	8.5	6.5	.0033	-11.5	.0358	4.70	81.97
14	10.7	9.2	7.0	.0038	-10.9	.0409	5.04	81.20
15	12.6	10.2	7.4	.0045	-10.5	.0478	5.61	80.57
16	14.7	11.3	7.9	.0052	-10.0	.0558	6.21	79.92
17	17.3	12.4	8.6	.0061	-9.4	.0655	6.85	79.24
18	20.0	13.0	9.0	.0071	-8.9	.0758	7.18	78.31
19	23.9	13.6	9.4	.0085	-8.5	.0908	7.45	77.72
20	27.9	14.1	9.8	.0099	-8.1	.1058	7.75	77.18
21	31.8	14.7	10.1	.0113	-7.8	.1208	8.09	76.73
22	39.4	15.6	10.5	.0136	-7.4	.1455	8.61	76.11
23	46.3	16.2	10.7	.0164	-7.2	.1758	8.94	75.57
24	52.5	16.6	11.0	.0187	-6.9	.2008	9.12	75.39
25	62.1	16.9	11.2	.0220	-6.7	.2358	9.33	75.09
26	71.3	17.3	11.4	.0253	-6.5	.2708	9.56	74.85
27	97.6	18.2	12.1	.0346	-5.8	.3708	10.02	73.84
28	123.9	19.3	12.5	.0439	-5.4	.4708	10.65	73.24
29	163.4	20.8	13.0	.0579	-4.9	.6208	11.44	72.55
30	216.0	21.8	13.6	.0766	-4.3	.8208	12.02	71.65
31	295.0	24.2	14.2	.1045	-3.7	1.1208	13.30	70.78
32	373.9	26.1	14.9	.1325	-3.0	1.4208	14.46	69.73
33	479.2	28.5	15.6	.1698	-2.3	1.8208	15.72	68.73
34	610.5	31.4	16.4	.2165	-1.5	2.3208	17.28	67.62
35	742.3	34.1	17.3	.2631	-.9	2.8208	18.80	66.71
36	873.9	35.7	17.6	.3098	-.3	3.3208	19.66	65.94
37	952.9	36.1	17.8	.3377	-.1	3.6205	19.87	65.60
38	1031.8	36.2	17.9	.3657	-.1	3.9205	19.93	65.49
39	1163.4	36.2	17.9	.4124	.0	4.4205	19.93	65.39

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00279 DELM = .183 REM = 215.0
V RUN = 112871-1 CF/2 = .00194 DELM = .336 REM = 649.0
PLATE = 1 UINF = 29.4 DEL2 = .0140 DEL3 = .504
X(IN) = 2.00 GM = 5.472 THETA = .0421 DEL4 = 3.263
K(E06) = -.4450 GAM = -.483 BETA = .253 H = 1.712

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.5	0.0000	0.00	85.06		
2	2.6	3.3	2.0	.0080	-13.4	.0041	4.26	85.05		
3	3.2	3.8	2.6	.0100	-12.9	.0051	4.98	84.25		
4	3.9	4.3	3.2	.0119	-12.2	.0061	5.66	83.24		
5	4.5	4.9	3.9	.0139	-11.5	.0071	6.45	82.27		
6	5.2	5.4	4.6	.0158	-10.8	.0081	7.14	81.27		
7	5.8	5.9	5.2	.0178	-10.2	.0091	7.77	80.37		
8	6.4	6.3	5.7	.0197	-9.8	.0101	8.38	79.66		
9	7.1	6.8	6.1	.0216	-9.3	.0111	8.99	79.03		
10	7.7	7.3	6.6	.0236	-8.9	.0121	9.62	78.34		
11	8.3	7.7	7.0	.0255	-8.4	.0131	10.19	77.72		
12	9.0	8.0	7.3	.0275	-8.1	.0141	10.62	77.27		
13	9.6	8.3	7.6	.0294	-7.9	.0151	11.01	76.85		
14	10.3	8.7	7.9	.0313	-7.6	.0161	11.44	76.40		
15	11.5	9.2	8.4	.0352	-7.0	.0181	12.20	75.63		
16	12.9	9.6	8.9	.0391	-6.6	.0201	12.69	74.94		
17	14.1	10.0	9.2	.0430	-6.2	.0221	13.19	74.43		
18	15.4	10.4	9.6	.0469	-5.8	.0241	13.72	73.80		
19	16.6	10.7	9.9	.0508	-5.5	.0261	14.17	73.35		
20	17.9	11.0	10.1	.0547	-5.3	.0281	14.57	73.11		
21	20.5	11.5	10.7	.0624	-4.8	.0321	15.27	72.27		
22	23.0	12.0	11.0	.0702	-4.4	.0361	15.93	71.73		
23	25.6	12.4	11.4	.0780	-4.0	.0401	16.47	71.16		
24	30.0	13.0	11.9	.0915	-3.5	.0471	17.22	70.44		
25	35.2	13.6	12.4	.1071	-3.1	.0551	18.05	69.78		
26	41.5	14.3	12.9	.1266	-2.5	.0651	18.97	68.97		
27	51.1	15.2	13.5	.1556	-1.9	.0801	20.05	68.03		
28	63.9	16.2	14.2	.1945	-1.3	.1001	21.46	67.10		
29	76.6	17.2	14.6	.2333	-.8	.1201	22.75	66.43		
30	89.4	18.0	14.9	.2722	-.5	.1401	23.86	65.95		
31	105.4	19.0	15.2	.3207	-.2	.1651	25.06	65.58		
32	121.3	19.7	15.3	.3692	-.1	.1901	26.11	65.37		
33	137.3	20.4	15.4	.4178	-.0	.2151	26.93	65.27		
34	153.2	20.9	15.5	.4663	-.0	.2401	27.59	65.21		
35	169.2	21.3	15.5	.5149	-.0	.2651	28.18	65.21		
36	187.8	21.7	15.5	.5715	.0	.2943	28.70	65.20		
37	210.2	22.0	15.5	.6395	.0	.3293	29.09	65.20		
38	242.1	22.2	15.5	.7366	.0	.3793	29.33	65.20		
39	277.2	22.2	15.5	.8434	-.0	.4343	29.39	65.20		
40	325.0	22.2	15.5	.9890	-.0	.5093	29.41	65.20		
41	372.9	22.2	15.5	1.1347	-.0	.5843	29.41	65.20		

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00171 DELM = .619 REM = 549.0
V RUN = 112871-1 CF/2 = .00071 DELM = .655 REM = 1441.0
PLATE = 3 UINF = 26.7 DEL2 = .0611 DEL3 = 1.492
X(IN) = 10.00 GM = 5.549 THETA = .1037 DEL4 = 10.495
K(E06) = -.8440 GAM = -1.362 BETA = 2.935 H = 1.892

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.3	0.0000	0.00	87.95	1.000	1.000
2	1.8	2.2	1.4	.0027	-13.9	.0052	1.62	85.97	1.393	1.187
3	2.2	2.7	1.6	.0032	-13.6	.0062	1.97	85.55	1.477	1.226
4	2.5	3.2	2.0	.0037	-13.2	.0072	2.34	84.99	1.563	1.279
5	3.2	4.2	2.9	.0048	-12.4	.0092	3.06	83.78	1.732	1.393
6	3.9	5.1	3.8	.0058	-11.7	.0112	3.73	82.71	1.959	1.494
7	4.6	6.0	4.2	.0068	-11.0	.0132	4.33	81.70	2.099	1.589
8	5.3	6.7	4.6	.0079	-10.6	.0152	4.89	81.11	2.238	1.645
9	6.0	7.5	5.1	.0089	-10.2	.0172	5.43	80.49	2.372	1.704
10	7.4	8.7	5.8	.0110	-9.5	.0212	6.35	79.47	2.609	1.801
11	8.8	10.1	6.3	.0130	-8.9	.0252	7.35	78.61	2.853	1.882
12	10.2	11.1	6.7	.0151	-8.5	.0292	8.04	78.04	3.032	1.936
13	12.0	11.9	7.1	.0177	-8.1	.0342	8.61	77.42	3.191	1.994
14	14.5	12.8	7.6	.0213	-7.6	.0412	9.31	76.73	3.386	2.056
15	17.3	13.8	8.1	.0255	-7.1	.0492	10.04	75.99	3.582	2.118
16	20.8	14.7	8.5	.0306	-6.7	.0592	10.66	75.39	3.744	2.165
17	24.3	15.4	8.9	.0359	-6.3	.0692	11.22	74.82	3.889	2.202
18	31.3	16.7	9.5	.0462	-5.7	.0892	12.11	73.98	4.076	2.239
19	40.1	18.0	10.0	.0591	-5.2	.1142	13.05	73.14	4.199	2.248
20	48.8	19.2	10.5	.0721	-4.7	.1392	13.93	72.48	4.236	2.226
21	57.6	20.2	10.9	.0850	-4.3	.1642	14.70	71.82	4.171	2.182
22	69.9	21.7	11.6	.1031	-3.7	.1992	15.76	70.92	3.997	2.091
23	87.4	23.7	12.2	.1290	-3.0	.2492	17.24	69.93	3.633	1.923
24	104.9	25.8	12.9	.1549	-2.4	.2992	18.75	69.06	3.231	1.710
25	122.5	27.8	13.4	.1808	-1.9	.3492	20.21	68.24	2.902	1.454
26	140.0	29.8	13.9	.2067	-1.4	.3992	21.63	67.58	2.639	1.192
27	175.1	33.2	14.6	.2584	-.6	.4992	24.15	66.40	2.346	.617
28	210.1	35.8	15.1	.3102	-.2	.5992	26.02	65.73	2.082	.191
29	245.2	36.7	15.2	.3620	.0	.6992	26.65	65.48	.764	.000
30	280.3	36.8	15.3	.4137	.0	.7992	26.74	65.45	.000	.000
31	315.3	36.8	15.3	.4655	.0	.8992	26.71	65.45	.000	.000

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00126 DELM = 1.232 REM = 1630.0
V RUN = 112871-1 CF/2 = .00056 DELM = 1.216 REM = 2613.0
PLATE = 6 UINF = 24.6 DEL2 = .1274 DEL3 = 4.715
X(IN) = 22.00 GM = 6.365 THETA = .2042 DEL4 = 30.013
K(E06) = -.4690 GAM = -1.281 BETA = 3.748 H = 1.957

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-18.4	0.0000	0.00	87.92	1.000	1.000
2	1.1	1.2	.5	.0008	-17.6	.0038	.72	86.94	1.207	1.113
3	1.4	1.6	1.0	.0010	-17.4	.0048	.92	86.68	1.267	1.142
4	1.7	1.9	1.3	.0012	-17.1	.0058	1.15	86.38	1.330	1.177
5	1.9	2.3	1.5	.0014	-16.9	.0068	1.38	86.12	1.394	1.207
6	2.2	2.7	1.7	.0016	-16.6	.0078	1.61	85.79	1.459	1.245
7	2.8	3.5	2.4	.0020	-16.0	.0098	2.09	85.02	1.591	1.333
8	3.4	4.3	3.0	.0024	-15.3	.0118	2.56	84.22	1.722	1.425
9	4.0	5.1	3.6	.0029	-14.8	.0138	3.00	83.51	1.847	1.506
10	4.5	5.7	4.2	.0033	-14.2	.0158	3.41	82.83	2.047	1.584
11	5.4	6.7	4.9	.0039	-13.5	.0188	3.96	82.03	2.176	1.675
12	6.2	7.4	5.5	.0045	-12.9	.0218	4.43	81.26	2.305	1.763
13	7.4	8.3	6.1	.0054	-12.2	.0258	4.95	80.46	2.473	1.854
14	8.8	9.5	6.9	.0064	-11.5	.0308	5.66	79.56	2.685	1.955
15	10.3	10.3	7.3	.0074	-11.1	.0358	6.16	79.09	2.847	2.009
16	12.3	11.1	8.0	.0089	-10.4	.0428	6.59	78.25	3.009	2.101
17	14.6	11.9	8.4	.0105	-9.9	.0508	7.09	77.69	3.192	2.163
18	17.4	12.8	8.9	.0126	-9.5	.0608	7.63	77.12	3.399	2.225
19	21.7	14.0	9.5	.0157	-8.9	.0758	8.29	76.41	3.667	2.300
20	27.5	15.0	10.0	.0199	-8.3	.0958	8.94	75.72	3.955	2.368
21	34.7	16.0	10.5	.0251	-7.9	.1208	9.52	75.21	4.232	2.415
22	41.8	16.8	11.0	.0303	-7.4	.1458	9.98	74.58	4.480	2.464
23	56.2	18.3	11.7	.0407	-6.6	.1958	10.97	73.69	4.853	2.516
24	70.5	19.6	12.2	.0511	-6.2	.2458	11.67	73.09	5.145	2.534
25	92.1	21.6	12.9	.0666	-5.4	.3208	12.87	72.22	5.622	2.526
26	113.6	23.2	13.6	.0822	-4.8	.3958	13.82	71.41	5.375	2.482
27	142.3	25.6	14.4	.1030	-4.2	.4958	15.15	70.44	5.164	2.357
28	185.3	30.0	15.4	.1342	-3.6	.6458	17.93	69.21	4.549	2.078
29	228.4	33.3	16.4	.1653	-2.0	.7958	19.77	68.06	3.419	1.663
30	285.8	38.1	17.4	.2069	-1.0	.9958	22.64	66.82	3.162	1.003
31	343.2	40.9	18.2	.2484	-.2	1.1958	24.29	65.85	2.213	.277
32	400.6	41.4	18.4	.2900	.0	1.3958	24.62	65.58	.098	.000
33	458.0	41.4	18.4	.3315	.0	1.5958	24.62	65.58	.000	.000

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00115 DELM = 1.863 REM = 2258.0
V RUN = 112871-1 CF/2 = .00051 DELM = 1.907 REM = 3588.0
PLATE = 9 UINF = 23.0 DEL2 = .1899 DEL3 = 7.183
X(IN) = 34.00 GM = 6.402 THETA = .3002 DEL4 = 45.865
K(E06) = -.3360 GAM = -1.278 BETA = 4.048 H = 1.943

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.1	0.0000	-19.2	0.0000	0.00	87.95	1.000	1.000
2	1.4	1.7	1.1	.0007	-19.2	.0056	.88	86.74	1.265	1.142
3	1.7	2.0	1.3	.0009	-18.8	.0066	1.08	86.50	1.321	1.172
4	1.9	2.3	1.5	.0010	-17.8	.0076	1.24	86.26	1.376	1.195
5	2.2	2.7	1.7	.0012	-17.6	.0086	1.42	86.03	1.431	1.225
6	2.5	3.0	1.9	.0013	-17.3	.0096	1.61	85.76	1.487	1.256
7	3.0	3.8	2.3	.0016	-16.8	.0116	1.99	85.09	1.600	1.336
8	3.5	4.5	2.9	.0018	-16.3	.0136	2.36	84.55	1.710	1.398
9	4.2	5.4	3.5	.0022	-15.5	.0166	2.87	83.57	1.867	1.512
10	5.0	6.7	4.5	.0027	-14.7	.0196	3.35	82.74	2.046	1.609
11	5.8	7.0	5.2	.0031	-14.1	.0226	3.73	81.97	2.148	1.699
12	6.8	8.0	5.8	.0036	-13.5	.0266	4.26	81.26	2.315	1.782
13	7.8	8.7	6.5	.0042	-12.7	.0306	4.61	80.37	2.437	1.865
14	9.1	9.4	7.0	.0048	-12.2	.0356	5.00	79.77	2.572	1.955
15	10.4	10.2	7.5	.0055	-11.8	.0406	5.40	79.30	2.712	2.009
16	12.2	11.0	7.9	.0065	-11.3	.0476	5.86	78.76	2.876	2.072
17	14.2	11.9	8.5	.0076	-10.7	.0556	6.30	78.09	3.044	2.149
18	16.8	12.7	8.9	.0089	-10.4	.0656	6.76	77.66	3.227	2.197
19	19.4	13.4	9.3	.0103	-9.9	.0756	7.12	77.15	3.382	2.254
20	24.5	14.4	9.9	.0130	-9.3	.0956	7.67	76.47	3.633	2.329
21	30.9	15.2	10.3	.0165	-8.9	.1206	8.06	75.99	3.884	2.382
22	43.7	16.5	11.2	.0233	-8.1	.1706	8.76	75.00	4.327	2.479
23	56.5	17.8	11.9	.0301	-7.5	.2206	9.49	74.32	4.745	2.543
24	75.7	19.1	12.4	.0404	-6.9	.2956	10.35	73.60	5.222	2.597
25	101.3	21.0	13.1	.0541	-6.1	.3956	11.12	72.73	5.789	2.634
26	126.9	22.8	13.9	.0677	-5.5	.4956	12.07	71.99	6.208	2.645
27	152.5	24.8	14.4	.0814	-4.9	.5956	13.17	71.26	6.520	2.620
28	190.9	27.3	15.2	.1019	-4.1	.7456	14.49	70.36	6.507	2.530
29	229.3	30.2	15.9	.1224	-3.3	.8956	16.00	69.48	6.257	2.360
30	283.5	34.0	16.8	.1498	-2.5	1.0956	18.01	68.36	5.360	2.046
31	331.7	37.2	17.5	.1771	-1.7	1.2956	19.75	67.58	3.948	1.635
32	408.5	41.6	18.5	.2181	-.7	1.5956	22.05	66.47	2.644	.852
33	485.4	43.2	19.1	.2592	-.1	1.8956	22.96	65.77	.980	.220
34	587.8	43.4	19.2	.3138	-.0	2.2956	23.01	65.62	.000	.000
35	690.2	43.4	19.2	.3685	-.0	2.6956	23.01	65.62	.000	.000

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00108 DELM = 2.474 REM = 2508.0
V RUN = 112871-1 CF/2 = .00048 DELM = 2.378 REM = 4497.0
PLATE = 12 UINF = 22.1 DEL2 = .2451 DEL3 = 9.430
X(IN) = 46.00 GM = 6.355 THETA = .3925 DEL4 = 59.954
K(E06) = -.2650 GAM = -1.294 BETA = 4.252 H = 1.921

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-19.9	0.0000	0.00	87.99	1.000	1.000
2	1.1	1.2	.5	.0005	-19.0	.0045	.55	87.06	1.189	1.110
3	1.3	1.5	1.0	.0006	-18.9	.0055	.74	86.88	1.233	1.132
4	1.6	1.8	1.2	.0007	-18.7	.0065	.95	86.68	1.280	1.155
5	1.8	2.1	1.4	.0009	-18.5	.0075	1.04	86.50	1.327	1.177
6	2.0	2.4	1.6	.0009	-18.2	.0085	1.20	86.23	1.376	1.209
7	2.5	3.1	2.0	.0011	-17.9	.0105	1.52	85.76	1.475	1.264
8	3.0	3.7	2.5	.0013	-17.4	.0125	1.84	85.17	1.575	1.334
9	3.7	4.7	3.1	.0016	-16.6	.0155	2.32	84.28	1.722	1.447
10	4.4	5.6	4.0	.0019	-15.8	.0185	2.78	83.45	1.869	1.538
11	5.4	6.6	5.0	.0024	-14.9	.0225	3.27	82.36	2.023	1.667
12	6.6	7.7	5.9	.0029	-13.9	.0275	3.82	81.32	2.219	1.790
13	7.8	8.5	6.4	.0034	-13.4	.0325	4.21	80.75	2.359	1.858
14	9.4	9.8	7.3	.0041	-12.6	.0395	4.84	79.83	2.572	1.967
15	11.3	10.8	7.8	.0049	-12.1	.0475	5.35	79.21	2.755	2.041
16	13.7	11.7	8.4	.0060	-11.5	.0575	5.76	78.52	2.920	2.123
17	16.1	12.3	8.9	.0070	-11.0	.0675	6.09	77.99	3.059	2.186
18	19.7	13.1	9.4	.0086	-10.4	.0825	6.47	77.36	3.242	2.259
19	24.5	14.0	10.1	.0107	-9.8	.1025	6.91	76.62	3.462	2.344
20	30.4	14.9	10.5	.0133	-9.4	.1275	7.36	76.17	3.710	2.403
21	37.6	15.7	11.0	.0164	-8.9	.1575	7.77	75.63	3.967	2.464
22	46.0	16.4	11.4	.0200	-8.5	.1925	8.12	75.15	4.229	2.522
23	57.9	17.6	12.0	.0252	-7.9	.2425	8.68	74.47	4.604	2.594
24	75.6	19.1	12.7	.0330	-7.2	.3175	9.45	73.69	5.131	2.666
25	93.7	20.3	13.0	.0408	-6.8	.3925	10.02	73.33	5.567	2.717
26	117.6	21.5	13.7	.0512	-6.2	.4925	10.62	72.55	6.026	2.770
27	165.3	24.7	14.6	.0719	-5.2	.6925	12.23	71.50	6.837	2.807
28	213.0	27.5	15.5	.0927	-4.4	.8925	13.60	70.57	7.136	2.744
29	308.5	33.0	16.9	.1342	-3.0	1.2925	16.33	68.47	6.361	2.382
30	404.0	38.6	18.1	.1758	-1.8	1.6925	19.07	67.64	4.468	1.773
31	499.5	42.9	19.1	.2173	-.8	2.0925	21.23	66.47	2.652	.891
32	618.8	44.6	19.8	.2692	-.0	2.5925	22.07	65.65	.315	.017
33	690.4	44.7	19.9	.3004	-.0	2.8925	22.11	65.62	.000	.000
34	692.9	44.7	19.9	.3015	-.0	2.9025	22.11	65.62	.000	.001

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00104 DELM = 3.027 REM = 3324.0
V RUN = 112871-1 CF/2 = .00046 DELM = 2.930 REM = 5354.0
PLATE = 15 UINF = 21.3 DEL2 = .2999 DEL3 = 11.459
X(IN) = 58.00 GM = 6.202 THETA = .4831 DEL4 = 71.071
K(E06) = -.2200 GAM = -1.326 BETA = 4.385 H = 1.888

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-20.2	0.0000	0.00	87.45	1.000	1.000
2	1.4	1.6	1.0	.0005	-19.1	.0061	.73	86.68	1.236	1.139
3	1.8	2.1	1.4	.0007	-18.8	.0081	1.00	86.29	1.322	1.186
4	2.3	2.7	1.8	.0009	-18.4	.0101	1.29	85.91	1.411	1.231
5	3.0	3.7	2.5	.0011	-17.7	.0131	1.71	85.14	1.548	1.323
6	3.6	4.6	3.2	.0014	-17.0	.0161	2.17	84.34	1.693	1.418
7	4.5	5.7	3.9	.0017	-16.2	.0201	2.65	83.51	1.850	1.517
8	5.4	6.7	5.0	.0021	-15.2	.0241	3.11	82.76	1.999	1.653
9	6.6	7.9	5.4	.0026	-14.4	.0301	3.68	81.44	2.191	1.763
10	8.6	9.2	7.0	.0033	-13.2	.0381	4.28	80.13	2.407	1.917
11	10.6	10.4	7.9	.0041	-12.3	.0481	4.45	79.12	2.602	2.037
12	14.2	11.9	8.9	.0054	-11.2	.0631	5.54	77.99	2.866	2.173
13	19.7	13.2	9.4	.0071	-10.7	.0831	6.15	77.45	3.129	2.239
14	25.5	14.4	10.4	.0097	-9.8	.1131	6.74	76.38	3.436	2.367
15	36.7	16.2	11.2	.0140	-9.0	.1631	7.57	75.51	3.996	2.473
16	52.6	17.6	12.1	.0204	-8.1	.2381	8.22	74.56	4.397	2.587
17	76.2	19.2	12.7	.0299	-7.5	.3381	8.97	73.84	5.016	2.659
18	104.3	20.8	13.6	.0396	-6.8	.4631	9.71	72.98	5.663	2.731
19	138.1	22.5	14.2	.0524	-6.0	.6131	10.48	72.19	6.335	2.776
20	177.6	24.3	14.9	.0674	-5.3	.7881	11.32	71.41	6.961	2.770
21	222.6	26.5	15.4	.0845	-4.6	.9881	12.36	70.90	7.323	2.750
22	290.2	30.2	16.4	.1101	-3.8	1.2881	14.10	69.79	7.599	2.587
23	380.4	35.3	17.5	.1443	-2.7	1.6881	16.45	68.69	7.004	2.232
24	470.5	39.6	18.4	.1785	-1.7	2.0881	19.47	67.53	5.018	1.725
25	560.6	43.1	19.7	.2127	-1.0	2.4881	20.98	66.65	2.944	1.097
26	650.7	45.2	19.9	.2469	-.2	2.8881	21.09	65.95	1.365	.431
27	718.3	45.6	20.1	.2725	-.0	3.1881	21.28	65.65	.407	.083
28	785.9	45.7	20.2	.2982	-.0	3.4881	21.31	65.59	.000	.000
29	976.1	45.7	20.2	.3724	-.0	3.8881	21.31	65.59	.000	.005

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00100 DELH = 3.499 REN = 3795.0
V RUN = 112871-1 CF/2 = .00044 DELM = 3.427 REM = 6149.0
PLATE = 18 UINF = 20.8 DEL2 = .3542 DEL3 = 13.454
X(IN) = 70.00 GM = 6.163 THETA = .5691 DEL4 = 82.919
K(E06) = -.1870 GAM = -1.338 BETA = 4.475 H = 1.860

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-20.6	0.0000	0.00	87.68	1.000	1.000
2	1.5	1.7	1.2	.0005	-19.4	.0071	.79	86.47	1.258	1.147
3	1.7	2.0	1.3	.0006	-19.2	.0081	.90	86.26	1.298	1.172
4	2.2	2.6	1.6	.0007	-18.9	.0101	1.15	85.97	1.381	1.207
5	2.8	3.5	2.2	.0009	-18.4	.0131	1.54	85.39	1.509	1.279
6	3.7	4.6	3.2	.0012	-17.4	.0171	2.09	84.29	1.676	1.412
7	4.5	5.7	4.2	.0015	-16.3	.0211	2.63	83.19	1.831	1.544
8	5.6	6.8	5.1	.0019	-15.4	.0261	3.05	82.18	2.004	1.667
9	6.9	8.0	6.1	.0023	-14.4	.0321	3.56	81.14	2.179	1.792
10	8.6	9.2	7.0	.0029	-13.6	.0401	4.11	80.22	2.376	1.904
11	10.6	10.2	7.9	.0036	-12.7	.0501	4.55	79.30	2.544	2.015
12	12.9	11.3	8.8	.0044	-12.0	.0601	5.34	78.58	2.731	2.101
13	16.2	12.7	9.3	.0055	-11.3	.0751	5.65	77.75	2.971	2.199
14	20.5	13.9	10.3	.0069	-10.2	.0951	6.19	76.65	3.214	2.328
15	25.8	14.8	10.5	.0087	-10.0	.1201	6.61	76.44	3.433	2.360
16	33.4	15.7	11.4	.0113	-9.1	.1551	7.00	75.48	3.697	2.470
17	44.1	16.9	11.8	.0149	-8.8	.2051	7.51	75.12	4.050	2.517
18	65.7	19.1	12.8	.0222	-8.0	.3051	8.45	74.21	4.741	2.605
19	87.2	19.9	13.2	.0295	-7.4	.4051	8.85	73.80	5.217	2.653
20	119.5	21.9	14.3	.0404	-6.6	.5551	9.77	72.73	5.982	2.691
21	151.8	23.3	14.4	.0513	-6.1	.7051	10.36	72.25	6.581	2.697
22	194.8	25.4	15.1	.0659	-5.5	.9051	11.29	71.56	7.337	2.687
23	259.4	28.3	16.0	.0877	-4.6	1.2051	12.60	70.60	8.129	2.649
24	323.9	31.4	16.7	.1096	-3.8	1.5051	13.99	69.79	8.861	2.557
25	410.0	34.9	17.6	.1387	-2.9	1.9051	15.55	68.82	7.491	2.291
26	496.1	39.2	18.9	.1678	-2.1	2.3051	17.44	67.52	6.177	1.888
27	582.2	42.5	19.2	.1970	-1.4	2.7051	18.91	67.16	4.124	1.410
28	668.3	45.0	19.9	.2261	-.7	3.1051	20.05	66.47	2.331	.959
29	754.4	46.5	20.3	.2552	-.2	3.5051	20.71	65.93	1.082	.346
30	840.5	46.7	20.6	.2843	-.0	3.9051	20.79	65.72	.167	.000
31	927.3	46.7	20.6	.3137	-.0	4.3082	20.79	65.72	.162	.000

DATE = 120271 (-0.15, 0.004, -0.17)

T RUN = 120271-1 STNA = .00098 DELH = 4.096 REN = 4329.0
V RUN = 112871-1 CF/2 = .00042 DELM = 4.000 REM = 6986.0
PLATE = 21 UINF = 28.4 DEL2 = .4093 DEL3 = 15.318
X(IN) = 82.00 GM = 6.850 THETA = .6606 DEL4 = 92.693
K(E06) = -.1620 GAM = -1.381 BETA = 4.614 H = 1.820

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-20.5	0.0000	0.00	87.54
2	1.6	1.9	1.2	.0005	-19.2	.0079	.88	86.18
3	1.8	2.1	1.5	.0006	-19.0	.0089	.91	85.97
4	2.2	2.7	1.8	.0007	-18.7	.0109	1.19	85.64
5	2.7	3.2	2.0	.0008	-18.5	.0129	1.39	85.44
6	3.3	4.1	2.7	.0010	-17.7	.0159	1.74	84.61
7	4.1	5.2	3.4	.0013	-17.1	.0199	2.20	83.96
8	4.9	6.1	4.4	.0015	-16.0	.0239	2.61	82.80
9	6.0	7.2	5.3	.0019	-15.1	.0289	3.08	81.85
10	7.2	8.2	5.9	.0022	-14.6	.0349	3.51	81.26
11	8.6	9.4	6.9	.0027	-13.6	.0419	4.03	80.19
12	10.7	10.3	7.8	.0033	-12.7	.0519	4.41	79.21
13	13.8	12.6	8.6	.0043	-11.9	.0669	5.36	78.37
14	17.9	14.1	9.5	.0056	-11.0	.0869	6.00	77.39
15	24.2	15.2	10.7	.0078	-9.8	.1219	6.50	76.20
16	35.5	17.2	11.3	.0110	-9.2	.1719	7.36	75.48
17	50.9	18.5	12.0	.0158	-8.8	.2469	7.91	74.77
18	71.6	20.1	12.5	.0222	-8.0	.3469	8.59	74.20
19	102.5	21.5	13.3	.0318	-7.2	.4969	9.16	73.39
20	143.8	23.4	14.0	.0446	-6.4	.6969	9.98	72.58
21	185.1	25.0	14.8	.0574	-5.7	.8969	10.67	71.80
22	247.0	26.1	15.6	.0766	-4.9	1.1969	11.97	70.93
23	308.9	30.0	16.4	.0958	-4.1	1.4969	12.79	70.12
24	370.8	32.7	16.8	.1150	-3.7	1.7969	13.97	69.61
25	453.3	36.1	17.7	.1405	-2.8	2.1969	15.39	68.74
26	535.8	39.4	18.3	.1661	-2.2	2.5969	16.82	68.10
27	618.4	42.5	19.0	.1917	-1.5	2.9969	18.15	67.35
28	690.6	44.6	19.4	.2141	-1.1	3.3469	19.05	66.83
29	752.5	46.2	19.9	.2333	-.7	3.6469	19.72	66.44
30	804.1	47.2	20.1	.2493	-.4	3.8969	20.12	66.08
31	907.3	47.2	20.5	.2813	-.0	4.3969	20.13	65.72

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00495 DELH = .159 REN = 148.8
V RUN = 121171-3 CF/2 = .00294 DELM = .299 REM = 510.0
PLATE = 1 UINF = 29.4 DEL2 = .0097 DEL3 = .225
X(IN) = 2.00 GM = 4.361 THETA = .0334 DEL4 = .979
K(E06) = -.4450 GAM = -.404 BETA = .121 H = 1.562

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-10.7	0.0000	0.00	91.62
2	3.5	3.7	2.4	.0199	-8.4	.0845	5.99	86.06
3	4.3	4.2	3.0	.0247	-7.8	.0295	6.90	84.64
4	5.1	4.9	3.5	.0295	-7.2	.0065	7.99	83.70
5	5.9	5.5	4.0	.0329	-6.7	.0075	8.95	82.80
6	6.7	6.0	4.5	.0372	-6.2	.0085	9.85	80.99
7	7.4	6.5	4.9	.0415	-5.8	.0095	10.57	79.92
8	8.2	6.9	5.2	.0459	-5.4	.0105	11.24	79.11
9	9.0	7.3	5.6	.0502	-5.1	.0115	11.97	78.19
10	9.8	7.8	5.9	.0546	-4.8	.0125	12.67	77.56
11	10.6	8.1	6.2	.0589	-4.5	.0135	13.23	76.82
12	11.4	8.4	6.4	.0632	-4.2	.0145	13.74	76.25
13	12.1	8.8	6.7	.0676	-4.0	.0155	14.38	75.71
14	12.9	9.1	6.9	.0719	-3.8	.0165	14.90	75.11
15	13.7	9.4	7.1	.0763	-3.6	.0175	15.42	74.63
16	14.5	9.7	7.3	.0806	-3.4	.0185	15.82	74.19
17	15.3	9.9	7.5	.0850	-3.2	.0195	16.20	73.80
18	16.0	10.1	7.6	.0893	-3.1	.0205	16.57	73.47
19	17.6	10.5	7.9	.0980	-2.9	.0225	17.21	72.75
20	19.2	10.9	8.1	.1067	-2.5	.0245	17.76	72.21
21	20.7	11.2	8.3	.1153	-2.4	.0265	18.27	71.79
22	22.3	11.5	8.5	.1240	-2.2	.0285	18.69	71.34
23	24.6	11.7	8.7	.1370	-2.0	.0315	19.15	70.83
24	27.0	12.0	8.9	.1501	-1.8	.0345	19.62	70.31
25	29.3	12.3	9.1	.1631	-1.6	.0375	20.04	69.98
26	32.4	12.5	9.3	.1805	-1.4	.0415	20.36	69.50
27	35.5	12.7	9.4	.1978	-1.3	.0455	20.72	69.17
28	41.2	13.0	9.6	.2239	-1.1	.0515	21.21	68.75
29	46.9	13.4	9.8	.2586	-.9	.0595	21.81	68.24
30	54.3	13.7	10.0	.3020	-.7	.0695	22.40	67.81
31	69.9	14.4	10.2	.3868	-.5	.0895	23.45	67.21
32	89.4	15.0	10.4	.4973	-.3	.1145	24.52	66.73
33	108.9	15.6	10.5	.6059	-.2	.1395	25.46	66.46
34	136.2	16.3	10.6	.7578	-.1	.1745	26.68	66.27
35	167.5	17.0	10.7	.9314	-.0	.2145	27.79	66.17
36	226.0	17.8	10.7	1.2570	-.0	.2895	29.06	66.11
37	304.1	18.6	10.7	1.6911	-.0	.3895	29.41	66.10
38	354.8	18.8	10.7	1.9731	-.0	.4545	29.42	66.10

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00349 DELH = .411 REN = 456.0
V RUN = 121171-3 CF/2 = .00244 DELM = .473 REM = 517.0
PLATE = 3 UINF = 27.0 DEL2 = .0325 DEL3 = .762
X(IN) = 10.00 GM = 4.479 THETA = .0582 DEL4 = 3.413
K(E06) = -.8320 GAM = -1.246 BETA = .435 H = 1.546

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.8	0.0000	0.00	91.58	1.000	1.000
2	4.2	4.2	2.8	.0052	-11.1	.0064	5.72	86.70	.950	.947
3	4.5	4.7	3.2	.0095	-10.6	.0074	6.44	85.67	.945	.935
4	5.5	5.2	3.8	.0108	-10.0	.0084	7.16	84.60	.939	.923
5	6.1	5.7	4.3	.0120	-9.5	.0094	7.72	83.72	.935	.912
6	6.8	6.1	4.8	.0133	-9.1	.0104	8.32	82.95	.930	.903
7	7.4	6.6	5.1	.0146	-8.7	.0114	8.95	82.32	.925	.896
8	8.1	7.0	5.4	.0159	-8.4	.0124	9.53	81.67	.920	.888
9	8.7	7.3	5.9	.0172	-8.0	.0134	10.02	80.90	.917	.879
10	9.4	7.7	6.1	.0184	-7.7	.0144	10.44	80.48	.914	.874
11	10.0	7.9	6.4	.0197	-7.5	.0154	10.85	80.00	.912	.869
12	11.3	8.5	6.9	.0223	-6.9	.0174	11.65	79.05	.907	.856
13	12.6	9.1	7.3	.0249	-6.5	.0194	12.43	78.25	.902	.846
14	13.9	9.6	7.7	.0274	-6.1	.0214	13.14	77.56	.897	.837
15	15.3	10.0	8.0	.0300	-5.8	.0234	13.84	76.99	.895	.830
16	16.6	10.3	8.3	.0325	-5.5	.0254	14.45	76.49	.892	.823
17	19.5	10.8	8.6	.0384	-5.3	.0294	14.72	76.01	.890	.817
18	21.1	11.2	9.0	.0415	-4.8	.0324	15.33	75.14	.888	.803
19	23.7	11.5	9.3	.0466	-4.5	.0364	15.76	74.63	.885	.796
20	26.4	11.8	9.6	.0518	-4.2	.0404	16.10	74.15	.888	.787
21	29.6	12.1	9.9	.0582	-3.9	.0454	16.53	73.55	.888	.774
22	34.2	12.5	10.2	.0671	-3.6	.0524	17.13	73.05	.886	.763
23	39.4	12.9	10.5	.0774	-3.4	.0604	17.62	72.54	.885	.747
24	45.9	13.3	10.8	.0902	-3.1	.0704	18.10	72.03	.883	.728
25	55.7	13.7	11.1	.1094	-2.7	.0854	18.72	71.37	.876	.695
26	68.8	14.2	11.5	.1351	-2.3	.1054	19.34	70.64	.868	.648
27	81.9	14.6	11.9	.1607	-2.0	.1254	19.95	70.10	.838	.602
28	98.2	15.2	12.1	.1927	-1.7	.1504	20.75	69.53	.801	.543
29	121.0	16.0	12.5	.2376	-1.3	.1854	21.80	68.78	.735	.452
30	147.2	16.7	12.9	.2889	-1.0	.2254	22.76	68.17	.638	.361
31	179.8	17.5	13.2	.3529	-.6	.2754	23.89	67.57	.507	.255
32	228.8	18.6	13.5	.4491	-.3	.3504	25.33	66.96	.327	.126
33	294.1	19.5	13.8	.5772	-.1	.4504	26.84	66.54	.166	.023
34	359.4	19.8	13.8	.7054	-.0	.5504	26.96	66.45	.024	.000
35	424.7	19.8	13.8	.8335	-.0	.6504	27.00	66.45	.000	.002

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00309 DELH = .704 REH = 772.0
W RUN = 121171-3 CF/2 = .00212 DELM = .758 REM = 1241.0
PLATE = 6 UINF = 24.5 DEL2 = .0606 DEL3 = 1.416
X(IN) = 22.00 GH = 4.167 THETA = .0977 DEL4 = 5.900
K(E06) = -.4610 GAM = -1.076 BETA = .422 H = 1.532

I	Y+	U+	T+	Y/DEL*	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.6	0.0000	0.00	91.65	1.000	1.000
2	3.6	3.7	2.5	.0046	-12.3	.0066	4.24	87.71	.937	.951
3	4.2	4.1	2.9	.0053	-11.8	.0076	4.70	86.85	.931	.941
4	4.7	4.5	3.2	.0060	-11.3	.0086	5.24	86.06	.923	.931
5	5.3	5.0	3.7	.0066	-10.5	.0096	5.81	85.23	.915	.920
6	5.9	5.4	4.1	.0073	-10.4	.0106	6.28	84.52	.909	.911
7	6.4	5.8	4.5	.0080	-10.0	.0116	6.68	83.94	.903	.902
8	7.0	6.2	4.9	.0087	-9.6	.0126	7.13	83.15	.897	.893
9	7.5	6.6	5.2	.0094	-9.4	.0136	7.59	82.74	.891	.884
10	8.6	7.3	5.7	.0108	-8.8	.0156	8.40	81.76	.880	.876
11	9.7	7.9	6.3	.0122	-8.3	.0176	9.07	80.84	.872	.864
12	10.8	8.4	6.7	.0135	-7.8	.0196	9.64	80.04	.865	.853
13	11.9	8.8	7.1	.0149	-7.5	.0216	10.12	79.44	.860	.845
14	13.0	9.2	7.5	.0163	-7.1	.0236	10.57	78.81	.855	.837
15	14.7	9.5	7.9	.0184	-6.8	.0266	11.27	78.01	.847	.826
16	16.3	10.2	8.3	.0204	-6.3	.0296	11.90	77.44	.840	.819
17	18.0	10.7	8.5	.0225	-6.0	.0326	12.35	77.00	.837	.812
18	20.2	11.1	8.9	.0253	-5.7	.0366	12.82	76.34	.834	.802
19	23.0	11.5	9.3	.0287	-5.3	.0416	13.32	75.68	.831	.792
20	25.7	11.9	9.6	.0322	-5.0	.0466	13.71	75.20	.830	.785
21	29.6	12.2	9.9	.0370	-4.7	.0536	14.13	74.76	.831	.778
22	33.5	12.5	10.1	.0418	-4.4	.0606	14.47	74.22	.832	.767
23	37.9	12.8	10.4	.0474	-4.2	.0686	14.83	73.77	.833	.757
24	46.2	13.3	10.7	.0577	-3.8	.0836	15.40	73.23	.837	.744
25	54.5	13.7	11.0	.0681	-3.6	.0986	15.85	72.75	.840	.730
26	65.5	14.1	11.3	.0819	-3.3	.1186	16.29	72.24	.842	.712
27	84.8	14.7	11.7	.1060	-2.9	.1536	16.99	71.52	.841	.680
28	106.9	15.3	12.1	.1336	-2.4	.1936	17.62	70.83	.829	.638
29	134.5	16.0	12.5	.1682	-2.1	.2436	18.44	70.20	.797	.587
30	175.9	17.0	13.0	.2199	-1.6	.3186	19.64	69.32	.721	.497
31	217.4	18.0	13.4	.2717	-1.2	.3936	20.77	68.63	.611	.406
32	272.6	19.1	13.8	.3407	-.7	.4936	22.05	67.88	.445	.282
33	327.8	20.1	14.1	.4097	-.4	.5936	23.16	67.30	.309	.165
34	383.0	20.8	14.4	.4789	-.1	.6936	23.99	66.85	.197	.082
35	452.1	21.2	14.5	.5650	-.0	.8186	24.46	66.61	.077	.000
36	521.1	21.2	14.6	.6513	.0	.9436	24.51	66.55	.000	.000
37	603.9	21.2	14.6	.7549	.0	1.0936	24.51	66.55	.000	.000

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00289 DELH = 1.004 REH = 1051.0
W RUN = 121171-3 CF/2 = .00203 DELM = .960 REM = 1549.0
PLATE = 9 UINF = 23.1 DEL2 = .0876 DEL3 = 2.051
X(IN) = 34.00 GH = 4.097 THETA = .1251 DEL4 = 9.485
K(E06) = -.3260 GAM = -.985 BETA = .389 H = 1.513

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.2	0.0000	0.00	91.79	1.000	1.000
2	3.5	3.6	2.4	.0032	-13.2	.0068	3.87	88.36	.933	.955
3	4.0	4.0	2.7	.0037	-12.7	.0078	4.24	87.68	.927	.946
4	4.5	4.3	3.1	.0042	-12.3	.0088	4.61	86.94	.921	.936
5	5.0	4.7	3.4	.0047	-11.8	.0098	5.01	86.17	.915	.925
6	5.5	5.1	3.8	.0051	-11.4	.0108	5.47	85.49	.907	.916
7	6.0	5.6	4.2	.0056	-11.0	.0118	5.94	84.81	.899	.907
8	6.5	6.0	4.6	.0061	-10.7	.0128	6.38	84.23	.891	.900
9	7.0	6.4	4.9	.0066	-10.4	.0138	6.79	83.84	.884	.894
10	7.5	6.8	5.1	.0070	-10.1	.0148	7.19	83.36	.877	.887
11	8.6	7.4	5.6	.0080	-9.6	.0168	7.93	82.47	.865	.875
12	9.6	8.1	6.2	.0089	-9.0	.0188	8.59	81.52	.854	.862
13	10.6	8.6	6.6	.0099	-8.6	.0208	9.16	80.90	.846	.853
14	11.6	9.0	6.9	.0108	-8.3	.0228	9.64	80.33	.839	.845
15	13.1	9.4	7.6	.0123	-7.7	.0258	10.06	79.32	.833	.831
16	14.7	9.8	7.9	.0137	-7.3	.0288	10.48	78.73	.828	.823
17	16.2	10.3	8.3	.0151	-6.9	.0318	10.95	78.07	.822	.813
18	18.2	10.8	8.7	.0170	-6.5	.0358	11.53	77.41	.815	.803
19	20.3	11.3	9.0	.0189	-6.2	.0398	12.00	76.83	.810	.795
20	23.3	11.7	9.4	.0218	-5.8	.0458	12.50	76.21	.806	.786
21	26.4	12.1	9.8	.0247	-5.5	.0518	12.88	75.65	.805	.776
22	29.9	12.4	10.0	.0280	-5.2	.0588	13.25	75.23	.804	.769
23	35.0	12.8	10.4	.0327	-4.9	.0688	13.65	74.64	.805	.758
24	42.7	13.2	10.7	.0399	-4.5	.0838	14.11	74.13	.810	.748
25	50.3	13.6	11.0	.0470	-4.3	.0988	14.46	73.68	.815	.737
26	60.5	14.0	11.3	.0566	-3.9	.1188	14.87	73.11	.821	.722
27	78.3	14.5	11.7	.0732	-3.5	.1538	15.43	72.45	.833	.701
28	98.7	15.0	12.1	.0923	-3.1	.1935	16.01	71.82	.843	.676
29	124.2	15.7	12.6	.1161	-2.8	.2438	16.69	71.25	.848	.646
30	162.4	16.4	12.9	.1518	-2.4	.3188	17.45	70.56	.836	.602
31	200.6	17.1	13.3	.1875	-2.0	.3938	18.18	69.84	.803	.542
32	251.5	18.1	13.7	.2351	-1.5	.4938	19.30	69.12	.727	.466
33	302.4	19.0	14.1	.2828	-1.2	.5938	20.27	68.51	.613	.385
34	378.8	20.2	14.5	.3542	-.7	.7439	21.50	67.79	.406	.261
35	455.2	21.1	14.9	.4256	-.3	.8938	22.49	67.18	.220	.134
36	531.6	21.6	15.1	.4970	-.1	1.0438	23.05	66.79	.106	.061
37	608.0	21.7	15.2	.5685	-.0	1.1938	23.13	66.64	.016	.000
38	709.8	21.7	15.2	.6637	-.0	1.3938	23.14	66.64	.000	.000
39	710.7	21.7	15.2	.6645	-.0	1.3955	23.14	66.64	.000	.000

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00276 DELH = 1.251 REH = 1283.0
W RUN = 121171-3 CF/2 = .00196 DELM = 1.240 REM = 1962.0
PLATE = 12 UINF = 22.2 DEL2 = .1115 DEL3 = 2.641
X(IN) = 46.00 GH = 4.065 THETA = .1613 DEL4 = 10.739
K(E06) = -.2540 GAM = -.950 BETA = .377 H = 1.498

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.7	0.0000	0.00	91.89	1.000	1.000
2	3.0	3.4	2.1	.0023	-13.8	.0063	3.41	88.86	.933	.958
3	3.5	3.7	2.4	.0027	-13.4	.0073	3.75	88.30	.927	.950
4	4.0	4.0	2.7	.0030	-13.0	.0083	4.06	87.68	.921	.941
5	4.5	4.3	3.0	.0034	-12.6	.0093	4.34	87.00	.916	.931
6	4.9	4.6	3.5	.0038	-12.2	.0103	4.67	86.29	.910	.921
7	5.4	5.0	3.8	.0042	-11.9	.0113	5.05	85.76	.903	.914
8	5.9	5.4	4.2	.0045	-11.4	.0123	5.44	85.11	.895	.904
9	6.4	5.7	4.5	.0049	-11.1	.0133	5.76	84.61	.889	.897
10	6.9	6.0	4.9	.0053	-10.9	.0143	6.03	84.16	.884	.891
11	7.9	6.6	5.3	.0060	-10.2	.0163	6.65	83.33	.873	.879
12	8.8	7.2	5.9	.0067	-9.8	.0183	7.29	82.47	.863	.867
13	9.8	7.8	6.3	.0075	-9.4	.0203	7.96	81.82	.849	.856
14	10.7	8.3	6.7	.0082	-8.9	.0223	8.33	81.08	.841	.847
15	12.2	8.9	7.2	.0093	-8.4	.0253	8.97	80.27	.829	.835
16	13.6	9.5	7.7	.0104	-7.9	.0283	9.53	79.47	.820	.823
17	15.0	9.9	8.0	.0116	-7.6	.0313	10.00	78.96	.812	.816
18	17.0	10.5	8.5	.0130	-7.1	.0353	10.55	78.16	.804	.806
19	19.4	11.0	9.0	.0149	-6.7	.0403	11.05	77.44	.797	.797
20	21.8	11.4	9.3	.0167	-6.4	.0453	11.48	76.94	.793	.785
21	25.6	11.9	9.8	.0197	-5.9	.0533	11.96	76.19	.790	.773
22	30.4	12.4	10.2	.0234	-5.5	.0633	12.47	75.53	.787	.762
23	37.6	13.0	10.6	.0289	-5.1	.0783	13.08	74.85	.787	.749
24	44.9	13.4	10.9	.0345	-4.7	.0933	13.44	74.34	.792	.738
25	56.9	13.8	11.3	.0437	-4.4	.1183	13.93	73.74	.801	.724
26	73.7	14.4	11.7	.0567	-3.9	.1533	14.50	73.02	.817	.704
27	92.9	14.8	12.1	.0715	-3.6	.1933	14.93	72.45	.826	.686
28	117.0	15.4	12.4	.0899	-3.3	.2433	15.45	71.94	.838	.664
29	153.0	16.1	12.9	.1177	-2.8	.3183	16.21	71.22	.847	.627
30	189.1	16.7	13.3	.1454	-2.4	.3933	16.84	70.56	.846	.586
31	237.2	17.5	13.6	.1824	-2.0	.4933	17.58	69.99	.818	.540
32	297.3	18.4	14.1	.2286	-1.6	.6183	18.52	69.24	.741	.459
33	357.4	19.3	14.4	.2748	-1.2	.7433	19.42	68.66	.629	.385
34	429.5	20.3	14.9	.3303	-.9	.8933	20.39	68.12	.462	.305
35	525.7	21.4	15.3	.4043	-.4	1.0933	21.55	67.34	.251	.157
36	621.8	22.0	15.6	.4782	-.1	1.2933	22.08	66.85	.093	.042
37	718.0	22.1	15.7	.5522	.0	1.4933	22.22	66.70	.012	.000
38	814.2	22.1	15.7	.6261	.0	1.6933	22.22	66.70	.000	.000
39	910.3	22.1	15.7	.7001	.0	1.8933	22.22	66.70	.000	.000

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00266 DELH = 1.531 REH = 1496.0
W RUN = 121171-3 CF/2 = .00191 DELM = 1.488 REM = 2080.0
PLATE = 15 UINF = 21.5 DEL2 = .1344 DEL3 = 3.199
X(IN) = 58.00 GH = 4.073 THETA = .1868 DEL4 = 13.028
K(E06) = -.2100 GAM = -.908 BETA = .357 H = 1.481

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.1	0.0000	0.00	91.82	1.000	1.000
2	3.0	3.1	2.1	.0020	-14.1	.0066	2.96	88.77	.940	.956
3	3.5	3.4	2.4	.0023	-13.8	.0076	3.32	88.24	.933	.948
4	3.8	3.8	2.7	.0026	-13.4	.0086	3.64	87.65	.926	.939
5	4.4	4.1	3.0	.0029	-13.0	.0096	3.96	87.12	.919	.932
6	4.9	4.5	3.4	.0032	-12.7	.0106	4.32	86.56	.912	.923
7	5.3	4.9	3.7	.0035	-12.3	.0116	4.69	85.97	.904	.915
8	5.8	5.2	4.1	.0038	-12.0	.0126	5.03	85.46	.897	.907
9	6.2	5.6	4.4	.0041	-11.7	.0136	5.35	84.99	.891	.900
10	6.7	5.9	4.8	.0044	-11.3	.0146	5.63	84.40	.886	.892
11	7.2	6.1	5.0	.0047	-11.0	.0156	5.96	83.98	.881	.885
12	7.6	6.4	5.3	.0050	-10.8	.0166	6.16	83.67	.876	.879
13	8.5	6.9	5.9	.0057	-10.2	.0196	6.67	82.74	.865	.867
14	9.5	7.5	6.1	.0063	-9.9	.0206	7.23	82.21	.854	.859
15	10.4	8.1	6.6	.0069	-9.4	.0226	7.77	81.43	.844	.847
16	11.3	8.6	7.0	.0075	-9.1	.0246	8.23	80.90	.835	.839
17	12.2	9.0	7.7	.0081	-8.8	.0266	8.67	80.44	.827	.832
18	13.6	9.6	7.8	.0090	-8.3	.0296	9.28	79.71	.816	.822
19	15.4	10.3	8.1	.0102	-7.9	.0336	9.86	79.11	.805	.813
20	17.3	10.8	8.6	.0115	-7.5	.0376	10.39	78.43	.796	.802
21	19.1	11.2	8.9	.0127	-7.2	.0416	10.77	77.95	.791	.795
22	21.9	11.7	9.4	.0145	-6.7	.0476	11.21	77.15	.785	.781
23	24.6	12.0	9.7	.0163	-6.3	.0536	11.56	76.61	.781	.772
24	27.8	12.4	10.1	.0185	-6.0	.0606	11.93	76.10	.778	.764
25	31.5	12.8	10.4	.0209	-5.7	.0686	12.29	75.65	.775	.756
26	38.4	13.4	10.7	.0255	-5.4	.0836	12.89	75.12	.773	.747
27	47.6	13.9	11.2	.0316	-4.9	.1036	13.34	74.40	.776	.731
28	59.1	14.2	11.5	.0392	-4.6	.1286	13.66	73.89	.784	.720
29	72.9	14.5	11.8	.0484	-4.3	.1586	13.99	73.35	.793	.706
30	89.0	15.0	12.2	.0591	-3.9	.1936	14.39	72.76	.803	.687
31	107.4	15.4	12.4	.0713	-3.6	.2336	14.79	72.39	.813	.673
32	130.4	15.9	12.7	.0866	-3.4	.2836	15.20	72.00	.823	.658
33	164.9	16.4	13.1	.1095	-2.9	.3586	15.78	71.31	.832	.624
34	210.8	17.1	13.5	.1400	-2.5	.4586	16.41	70.69	.829	.565
35	268.3	17.9	13.9	.1792	-2.1	.5836	17.20	70.05	.805	.537
36	348.8	19.0	14.5	.2317	-1.6	.7586	18.27	69.21	.733	.453
37	429.2	20.0	15.0	.2851	-1.1	.9336	19.22	68.43	.610	.369
38	521.2	21.0	15.3	.3462	-.7	1.1336	20.22	67.85	.418	.286
39	636.1	22.0	15.7	.4226	-.3	1.3836	21.14	67.22	.193	.131
40	751.1	22.3	16.0	.4989	-.1	1.6336	21.49	66.83	.060	.029
41	866.0	22.4	16.1	.5753	-.0	1.8836	21.51	66.74	.003	.000
42	877.9	22.4	16.1	.5832	-.0	1.9094	21.51	66.74	.000	.000
43	969.8	22.4	16.1	.6442	-.0	2.1094	21.51	66.74	.000	.000

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00258 DELM = 1.746 REM = 1693.0
V RUN = 121171-3 CF/2 = .00187 DELM = 1.671 REM = 2324.0
PLATE = 18 UINF = 20.9 DEL2 = .1559 DEL3 = 1.741
X(IN) = 70.00 GM = 4.044 THETA = .2139 DEL4 = 15.129
K(E06) = -.1818 GAM = -.892 BETA = .351 H = 1.472

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.4	0.0000	0.00	92.10	1.000	1.080
2	1.4	3.7	2.3	.0019	-14.2	.0076	3.44	88.77	.924	.951
3	3.8	4.0	2.6	.0022	-13.9	.0086	3.70	88.24	.918	.943
4	4.3	4.3	2.9	.0025	-13.5	.0098	3.94	87.68	.914	.934
5	4.7	4.5	3.2	.0027	-13.1	.0105	4.20	87.09	.908	.925
6	5.1	4.9	3.7	.0030	-12.6	.0116	4.50	86.35	.902	.914
7	5.6	5.2	4.0	.0033	-12.4	.0126	4.83	85.97	.894	.909
8	6.0	5.6	4.3	.0035	-12.1	.0136	5.17	85.49	.887	.901
9	6.9	6.3	4.9	.0040	-11.5	.0156	5.79	84.55	.877	.887
10	7.8	6.8	5.4	.0046	-11.0	.0176	6.31	83.75	.862	.875
11	8.7	7.4	5.8	.0051	-10.5	.0196	6.87	83.10	.850	.865
12	9.6	8.1	6.3	.0056	-10.1	.0216	7.53	82.44	.835	.855
13	10.9	8.8	6.8	.0064	-9.6	.0246	8.11	81.61	.823	.843
14	12.2	9.2	7.4	.0072	-9.0	.0276	8.56	80.75	.814	.829
15	13.5	9.7	7.8	.0080	-8.6	.0306	8.99	80.07	.806	.819
16	15.3	10.2	8.4	.0090	-8.0	.0346	9.47	79.17	.797	.805
17	17.1	10.7	8.7	.0100	-7.6	.0386	9.85	78.58	.790	.795
18	19.7	11.2	9.1	.0116	-7.2	.0446	10.36	78.01	.782	.787
19	22.4	11.6	9.6	.0132	-6.7	.0506	10.74	77.24	.777	.774
20	25.5	12.0	9.9	.0150	-6.5	.0576	11.12	76.82	.772	.767
21	29.0	12.5	10.2	.0171	-6.1	.0656	11.58	76.25	.766	.758
22	33.4	13.1	10.6	.0197	-5.8	.0756	12.09	75.71	.759	.749
23	40.0	13.5	11.0	.0236	-5.4	.0906	12.46	75.15	.758	.738
24	46.7	13.7	11.2	.0275	-5.2	.1056	12.66	74.82	.761	.732
25	55.5	14.0	11.5	.0326	-4.9	.1256	12.97	74.31	.763	.722
26	71.0	14.5	11.9	.0419	-4.5	.1606	13.42	73.71	.768	.709
27	88.7	14.9	12.2	.0523	-4.2	.2006	13.75	73.23	.778	.697
28	110.7	15.4	12.6	.0654	-3.8	.2506	14.28	72.63	.788	.677
29	143.9	16.0	13.0	.0850	-3.4	.3256	14.79	72.03	.799	.655
30	188.1	16.7	13.4	.1111	-3.0	.4256	15.43	71.37	.806	.623
31	243.3	17.4	13.9	.1437	-2.5	.5506	16.09	70.62	.802	.575
32	309.6	18.4	14.3	.1829	-2.0	.7006	16.98	69.93	.790	.522
33	398.0	19.4	14.8	.2351	-1.5	.9006	17.95	69.18	.694	.444
34	466.3	20.3	15.2	.2674	-1.1	1.1006	18.82	68.58	.556	.360
35	574.7	21.2	15.6	.3396	-.8	1.3006	19.65	67.97	.390	.256
36	663.1	22.0	15.9	.3918	-.4	1.5006	20.33	67.49	.235	.165
37	751.5	22.4	16.2	.4440	-.2	1.7006	20.78	67.19	.117	.079
38	839.8	22.5	16.3	.4963	-.1	1.9006	20.81	66.89	.027	.025
39	928.2	22.6	16.4	.5485	-.0	2.1006	20.91	66.80	.000	.000
40	1016.6	22.6	16.4	.6007	-.0	2.3006	20.93	66.80	.000	.001
41	1019.3	22.6	16.4	.6017	-.0	2.3045	20.93	66.80	.000	.001
42	1106.7	22.6	16.4	.6540	-.0	2.5045	20.93	66.89	.000	.003

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00252 DELM = 2.049 REM = 1928.0
V RUN = 121171-3 CF/2 = .00184 DELM = 1.982 REM = 2558.0
PLATE = 21 UINF = 20.5 DEL2 = .1814 DEL3 = 4.348
X(IN) = 82.08 GM = 4.030 THETA = .2407 DEL4 = 17.519
K(E06) = -.1650 GAM = -.929 BETA = .358 H = 1.455

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.6	0.0000	0.00	91.89	1.000	1.000
2	2.5	2.5	1.7	.0013	-14.9	.0059	2.26	89.27	.947	.960
3	2.9	2.9	2.0	.0015	-14.6	.0069	2.63	88.89	.939	.954
4	3.4	3.3	2.3	.0018	-14.4	.0079	2.99	88.48	.930	.948
5	3.8	3.7	2.6	.0020	-14.0	.0089	3.34	87.95	.921	.939
6	4.2	4.1	2.9	.0022	-13.7	.0099	3.69	87.44	.910	.931
7	4.7	4.5	3.3	.0024	-13.3	.0109	4.03	86.85	.900	.922
8	5.1	4.8	3.7	.0027	-12.9	.0119	4.35	86.29	.895	.914
9	5.5	5.2	4.0	.0029	-12.6	.0129	4.67	85.85	.891	.907
10	6.4	5.8	4.7	.0033	-12.0	.0149	5.25	84.87	.878	.892
11	7.3	6.4	5.1	.0038	-11.5	.0169	5.74	84.19	.867	.881
12	8.1	6.9	5.5	.0042	-11.1	.0189	6.23	83.54	.856	.871
13	9.0	7.5	6.1	.0047	-10.5	.0209	6.71	82.68	.845	.858
14	10.3	8.2	6.5	.0054	-10.1	.0239	7.41	82.06	.829	.849
15	11.6	8.9	7.2	.0060	-9.5	.0269	7.97	81.08	.817	.833
16	13.3	9.6	7.7	.0068	-8.9	.0309	8.61	80.30	.803	.821
17	15.0	10.2	8.2	.0078	-8.4	.0349	9.16	79.53	.792	.809
18	16.7	10.7	8.5	.0087	-8.1	.0389	9.61	79.05	.783	.802
19	18.9	11.2	8.9	.0099	-7.7	.0439	10.06	78.40	.775	.792
20	21.9	11.7	9.5	.0114	-7.2	.0509	10.57	77.62	.766	.780
21	25.3	12.2	10.0	.0132	-6.7	.0589	11.01	76.88	.759	.768
22	29.6	12.7	10.3	.0155	-6.4	.0689	11.44	76.40	.753	.760
23	36.1	13.3	10.9	.0188	-5.8	.0839	11.93	75.54	.747	.745
24	44.7	13.7	11.2	.0233	-5.4	.1039	12.37	75.03	.743	.736
25	55.4	14.1	11.6	.0290	-5.0	.1289	12.73	74.37	.744	.722
26	72.6	14.7	12.0	.0379	-4.6	.1689	13.21	73.74	.747	.706
27	94.1	15.2	12.4	.0492	-4.2	.2189	13.70	73.20	.753	.690
28	126.4	15.8	12.9	.0660	-3.8	.2939	14.19	72.51	.762	.664
29	169.4	16.4	13.3	.0885	-3.4	.3939	14.75	71.88	.771	.637
30	223.2	17.2	13.8	.1166	-2.9	.5189	15.46	71.16	.773	.602
31	287.7	18.0	14.2	.1503	-2.4	.6689	16.19	70.47	.753	.556
32	363.0	18.7	14.6	.1896	-2.0	.8439	16.84	69.87	.706	.502
33	449.0	19.7	15.1	.2346	-1.6	1.0439	17.70	69.18	.644	.426
34	556.5	20.7	15.5	.2907	-1.1	1.2939	18.66	68.49	.526	.333
35	665.6	21.8	16.0	.3562	-.6	1.5939	19.64	67.76	.309	.214
36	814.6	22.5	16.3	.4256	-.3	1.8939	20.24	67.25	.104	.110
37	943.7	22.8	16.6	.4930	-.1	2.1939	20.50	66.92	.023	.030
38	1072.7	22.8	16.6	.5604	-.0	2.4939	20.53	66.83	.000	.000
39	1201.7	22.8	16.6	.6278	-.0	2.7939	20.58	66.83	.000	.000
40	1203.1	22.8	16.6	.6285	-.0	2.7970	20.53	66.83	.000	.000

DATE = 013072 (-0.15, -0.001)

T RUN = 13072-1 STNA = .00248 DELM = 2.191 REM = 2949.0
V RUN = 121171-3 CF/2 = .00191 DELM = 2.102 REM = 2759.0
PLATE = 23 UINF = 20.2 DEL2 = .1959 DEL3 = 4.719
X(IN) = 90.00 GM = 4.019 THETA = .2637 DEL4 = 19.947
K(E06) = -.1650 GAM = -1.019 BETA = .393 H = 1.447

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-16.8	0.0000	0.00	92.06
2	2.4	2.4	1.7	.0012	-15.1	.0057	2.10	89.63
3	2.8	2.8	1.9	.0014	-14.9	.0067	2.45	89.21
4	3.2	3.2	2.2	.0016	-14.6	.0077	2.80	88.83
5	3.7	3.6	2.5	.0018	-14.4	.0087	3.14	88.45
6	4.1	4.0	2.8	.0020	-14.0	.0097	3.48	87.86
7	4.5	4.3	3.1	.0022	-13.6	.0107	3.80	87.36
8	4.9	4.7	3.5	.0024	-13.3	.0117	4.11	86.82
9	5.3	5.0	3.8	.0026	-12.9	.0127	4.42	86.29
10	6.2	5.7	4.5	.0030	-12.3	.0147	5.01	85.35
11	7.0	6.2	5.0	.0034	-11.8	.0167	5.46	84.58
12	7.9	6.7	5.5	.0039	-11.3	.0187	5.92	83.94
13	8.7	7.3	5.9	.0043	-10.8	.0207	6.41	83.12
14	10.0	8.0	6.6	.0049	-10.2	.0237	7.04	82.18
15	11.2	8.7	7.0	.0055	-9.7	.0267	7.61	81.46
16	12.5	9.2	7.5	.0061	-9.2	.0297	8.13	80.72
17	14.2	9.9	8.0	.0070	-8.7	.0337	8.72	79.95
18	15.8	10.5	8.5	.0078	-8.3	.0377	9.24	79.26
19	17.5	10.9	8.9	.0086	-7.8	.0417	9.62	78.61
20	19.6	11.4	9.2	.0097	-7.5	.0467	10.02	78.16
21	22.1	11.8	9.6	.0109	-7.2	.0527	10.36	77.65
22	25.1	12.1	10.0	.0123	-6.7	.0597	10.67	76.97
23	28.0	12.4	10.3	.0138	-6.5	.0667	10.92	76.61
24	31.4	12.7	10.6	.0155	-6.2	.0767	11.21	76.10
25	37.7	13.3	10.9	.0196	-5.9	.0897	11.67	75.68
26	46.2	13.8	11.4	.0237	-5.3	.1147	12.13	74.85
27	62.9	14.4	11.9	.0310	-5.0	.1497	12.63	74.34
28	79.7	14.8	12.1	.0393	-4.6	.1897	13.06	73.80
29	100.7	15.3	12.5	.0496	-4.3	.2397	13.45	73.23
30	132.2	15.8	12.9	.0652	-3.9	.3147	13.90	72.63
31	174.3	16.4	13.4	.0859	-3.4	.4147	14.46	71.94
32	226.8	17.2	13.9	.1118	-2.9	.5397	15.09	71.25
33	289.8	17.9	14.2	.1429	-2.5	.6897	15.81	70.65
34	373.9	18.8	14.7	.1843	-2.1	.8897	16.56	69.93
35	457.9	19.7	15.1	.2257	-1.7	1.0897	17.30	69.33
36	541.9	20.4	15.5	.2671	-1.3	1.2897	17.99	68.76
37	668.0	21.5	15.9	.3293	-.8	1.5897	18.90	68.07
38	794.1	22.2	16.3	.3914	-.4	1.8897	19.64	67.46
39	920.1	22.8	16.6	.4536	-.2	2.1897	20.10	67.07
40	1046.2	23.0	16.7	.5157	-.0	2.4897	20.22	66.86
41	1172.3	23.0	16.8	.5779	-.0	2.7897	20.20	66.83
42	1181.6	23.0	16.8	.5825	-.0	2.8119	20.20	66.83

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00566 DELM = .133 REM = 125.0
V RUN = 121671-3 CF/2 = .00323 DELM = .297 REM = 499.0
PLATE = 1 UINF = 29.5 DEL2 = .0092 DEL3 = .177
X(IN) = 2.00 GM = 4.100 THETA = .0327 DEL4 = .727
K(E06) = -.4410 GAM = -.422 BETA = .104 H = 1.522

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-9.8	0.0000	0.00	91.68
2	4.2	4.2	2.8	.0283	-7.1	.0051	7.27	83.95
3	5.0	4.8	3.3	.0338	-6.5	.0061	8.18	82.20
4	5.8	5.3	3.8	.0393	-6.0	.0071	9.08	80.75
5	6.6	5.8	4.3	.0448	-5.5	.0081	9.94	79.35
6	7.4	6.2	4.7	.0502	-5.1	.0091	10.74	78.13
7	8.2	6.7	5.0	.0557	-4.7	.0101	11.45	77.15
8	9.0	7.1	5.4	.0612	-4.4	.0111	12.15	76.19
9	9.8	7.5	5.7	.0667	-4.1	.0121	12.91	75.33
10	10.6	7.9	6.0	.0722	-3.8	.0131	13.63	74.52
11	11.5	8.3	6.2	.0777	-3.5	.0141	14.23	73.74
12	12.3	8.6	6.4	.0832	-3.3	.0151	14.77	73.14
13	13.1	8.9	6.6	.0887	-3.1	.0161	15.29	72.54
14	13.9	9.2	6.8	.0942	-3.0	.0171	15.77	72.15
15	14.7	9.4	6.9	.0996	-2.8	.0181	16.26	71.70
16	15.5	9.7	7.1	.1051	-2.7	.0191	16.70	71.22
17	17.1	10.1	7.3	.1161	-2.4	.0211	17.41	70.50
18	18.8	10.4	7.6	.1271	-2.2	.0231	17.94	69.78
19	20.4	10.7	7.8	.1381	-2.0	.0251	18.40	69.15
20	22.8	11.1	8.0	.1545	-1.7	.0281	19.03	68.55
21	25.2	11.4	8.2	.1710	-1.5	.0311	19.55	67.94
22	26.5	11.7	8.5	.1930	-1.3	.0351	20.12	67.31
23	31.7	11.9	8.6	.2149	-1.1	.0391	20.59	66.83
24	39.0	12.2	8.8	.2369	-1.0	.0431	20.99	66.44
25	43.1	12.6	9.0	.2918	-.7	.0531	21.76	65.65
26	51.2	13.0	9.2	.3466	-.6	.0631	22.40	65.14
27	59.3	13.3	9.3	.4015	-.4	.0731	22.95	64.77
28	71.5	13.7	9.5	.4839	-.3	.0881	23.68	64.35
29	87.7	14.2	9.6	.5937	-.2	.1081	24.49	63.99
30	103.9	14.7	9.7	.7034	-.1	.1281	25.26	63.80
31	120.1	15.1	9.7	.8132	-.0	.1481	25.96	63.65
32	132.3	15.4	9.7	.8956	-.0	.1631	26.45	63.59
33	152.6	15.8	9.8	1.0328	-.0	.1881	27.21	63.56
34	193.1	16.5	9.8	1.3072	.0	.2381	28.43	63.49
35	231.7	16.9	9.8	1.5817	.0	.2881	29.15	63.49
36	235.6	16.9	9.8	1.5947	.0	.2905	29.17	63.49
37	268.1	17.1	9.8	1.8142	.0	.3305	29.40	63.48
38	304.6	17.1	9.8	2.0612	.0	.3755	29.51	63.48
39	345.1	17.1	9.8	2.3357	.0	.4255	29.51	63.48
40	385.7	17.1	9.8	2.6101	.0	.4755	29.52	63.48
41	446.5	17.1	9.8	3.0218	.0	.5505	29.52	63.48

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00403 DELM = .364 REM = 373.0
V RUN = 121671-3 CF/2 = .00282 DELM = .484 REM = 721.0
PLATE = 3 UINF = 27.1 DEL2 = .0267 DEL3 = .587
X(IN) = 10.00 GM = 4.224 THETA = .0915 DEL4 = 2.477
K(E06) = -.8268 GAM = -1.134 BETA = .321 H = 1.525

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-12.8	0.0000	0.00	91.46	1.000	1.000
2	5.4	4.9	3.5	.0126	-9.3	.0077	7.23	83.81	.859	.869
3	6.1	5.4	4.0	.0145	-8.5	.0087	7.93	82.74	.839	.849
4	6.8	5.8	4.5	.0162	-8.4	.0097	8.55	81.76	.828	.832
5	7.5	6.3	4.9	.0178	-8.0	.0107	9.24	80.87	.813	.816
6	8.2	6.7	5.2	.0195	-7.6	.0117	9.85	80.14	.800	.803
7	8.8	7.1	5.6	.0211	-7.3	.0127	10.43	79.32	.789	.788
8	9.5	7.4	5.9	.0228	-7.0	.0137	10.97	78.70	.778	.776
9	10.2	7.8	6.2	.0245	-6.7	.0147	11.52	78.04	.767	.764
10	11.6	8.5	6.7	.0278	-6.1	.0167	12.55	76.82	.747	.741
11	13.0	9.0	7.2	.0311	-5.7	.0187	13.31	75.92	.733	.725
12	14.4	9.4	7.6	.0344	-5.3	.0207	13.92	74.97	.722	.706
13	15.8	9.8	7.9	.0378	-5.0	.0227	14.54	74.37	.711	.695
14	17.9	10.4	8.2	.0427	-4.6	.0257	15.37	73.62	.696	.680
15	20.0	10.8	8.6	.0477	-4.2	.0287	16.00	72.75	.686	.662
16	22.1	11.2	8.9	.0527	-4.0	.0317	16.48	72.15	.680	.649
17	24.2	11.4	9.1	.0577	-3.7	.0347	16.84	71.64	.676	.639
18	26.3	11.8	9.3	.0627	-3.5	.0377	17.18	71.19	.672	.628
19	29.0	11.9	9.5	.0693	-3.3	.0417	17.57	70.71	.668	.616
20	32.5	12.2	9.8	.0776	-3.1	.0467	17.97	70.17	.664	.602
21	37.4	12.5	10.0	.0893	-2.8	.0537	18.43	69.66	.660	.588
22	43.0	12.8	10.3	.1025	-2.5	.0617	18.91	69.07	.657	.567
23	49.9	13.1	10.5	.1192	-2.3	.0717	19.33	68.51	.653	.546
24	60.4	13.5	10.8	.1441	-2.0	.0867	19.92	67.84	.647	.515
25	70.8	13.8	11.1	.1690	-1.8	.1017	20.44	67.34	.639	.482
26	84.8	14.2	11.4	.2022	-1.5	.1217	20.97	66.71	.624	.436
27	102.2	14.7	11.6	.2438	-1.2	.1467	21.70	66.13	.598	.384
28	119.6	15.1	11.9	.2853	-1.0	.1717	22.34	65.65	.564	.333
29	137.0	15.5	12.1	.3268	-.8	.1967	22.94	65.23	.523	.282
30	161.4	16.1	12.3	.3850	-.6	.2317	23.73	64.77	.456	.218
31	189.3	16.6	12.5	.4514	-.4	.2717	24.53	64.35	.374	.151
32	224.1	17.2	12.6	.5345	-.2	.3217	25.44	63.98	.278	.084
33	258.9	17.8	12.7	.6176	-.1	.3717	26.22	63.77	.201	.042
34	311.2	18.2	12.8	.7422	-.0	.4467	26.84	63.59	.113	.000
35	380.8	18.3	12.8	.9083	-.0	.5467	27.10	63.52	.037	.000
36	450.5	18.4	12.8	1.0745	-.0	.6467	27.12	63.52	.000	.000
37	452.1	18.4	12.8	1.0783	-.0	.6490	27.12	63.52	.000	.000
38	504.3	18.4	12.8	1.2029	-.0	.7240	27.12	63.52	.000	.000

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00359 DELM = .645 REM = 622.0
V RUN = 121671-3 CF/2 = .00264 DELM = .677 REM = 1134.0
PLATE = 6 UINF = 24.5 DEL2 = .0492 DEL3 = 1.053
X(IN) = 22.00 GM = 3.938 THETA = .0817 DEL4 = 4.266
K(E06) = -.4570 GAM = -.945 BETA = .272 H = 1.900

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.9	0.0000	0.00	91.55	1.000	1.000
2	4.1	3.9	2.7	.0060	-11.6	.0067	5.01	86.79	.864	.907
3	4.7	4.2	3.1	.0069	-11.1	.0077	5.48	85.76	.851	.886
4	5.3	4.6	3.5	.0078	-10.5	.0087	6.00	84.70	.837	.865
5	5.9	5.1	3.8	.0087	-10.1	.0097	6.55	83.84	.822	.848
6	6.5	5.5	4.1	.0096	-9.6	.0107	7.12	82.98	.807	.828
7	7.1	5.9	4.6	.0105	-9.3	.0117	7.66	82.24	.792	.816
8	7.7	6.3	5.1	.0114	-8.9	.0127	8.15	81.40	.779	.799
9	8.3	6.7	5.3	.0123	-8.6	.0137	8.60	80.84	.767	.787
10	8.9	7.0	5.7	.0132	-8.3	.0147	9.02	80.16	.756	.774
11	9.6	7.3	5.9	.0141	-8.0	.0157	9.41	79.65	.746	.763
12	10.8	7.6	6.5	.0159	-7.4	.0177	10.13	78.52	.728	.740
13	12.0	8.4	6.9	.0177	-7.0	.0197	10.83	77.68	.709	.723
14	13.2	8.9	7.3	.0195	-6.6	.0217	11.49	76.82	.693	.706
15	14.4	9.3	7.7	.0213	-6.3	.0237	12.05	76.16	.679	.692
16	15.6	9.6	8.0	.0231	-5.9	.0257	12.45	75.48	.668	.678
17	17.5	10.1	8.4	.0258	-5.6	.0287	13.03	74.79	.655	.664
18	19.3	10.5	8.7	.0285	-5.2	.0317	13.52	74.07	.644	.648
19	21.1	10.8	9.0	.0312	-4.9	.0347	13.91	73.47	.636	.635
20	24.2	11.2	9.3	.0357	-4.6	.0397	14.44	72.84	.626	.622
21	27.2	11.5	9.6	.0402	-4.3	.0447	14.99	72.24	.617	.609
22	30.3	11.7	9.9	.0447	-4.0	.0497	15.15	71.73	.613	.597
23	34.5	12.0	10.1	.0510	-3.8	.0567	15.54	71.25	.609	.586
24	39.4	12.4	10.4	.0582	-3.5	.0647	16.06	70.71	.604	.572
25	45.5	12.7	10.6	.0672	-3.3	.0747	16.42	70.23	.596	.558
26	51.6	12.9	10.9	.0762	-3.1	.0847	16.69	69.78	.595	.545
27	58.7	13.2	11.1	.0897	-2.9	.0997	17.10	69.33	.592	.529
28	72.9	13.6	11.4	.1077	-2.6	.1197	17.57	68.79	.588	.508
29	88.2	14.0	11.7	.1302	-2.3	.1447	18.09	68.19	.581	.480
30	103.4	14.3	11.9	.1526	-2.1	.1697	18.51	67.74	.572	.456
31	124.7	14.7	12.2	.1841	-1.8	.2047	19.01	67.16	.554	.419
32	149.1	15.2	12.5	.2201	-1.5	.2447	19.64	66.59	.526	.375
33	179.6	15.8	12.7	.2651	-1.2	.2947	20.36	66.08	.482	.329
34	210.0	16.3	13.0	.3101	-1.0	.3447	21.04	65.53	.427	.273
35	255.7	17.1	13.3	.3775	-.7	.4197	22.01	64.96	.335	.204
36	301.4	17.7	13.5	.4450	-.4	.4947	22.90	64.44	.246	.132
37	362.3	18.4	13.6	.5349	-.2	.5947	23.82	63.99	.149	.061
38	453.7	18.9	12.9	.6699	-.0	.7447	24.45	63.65	.067	.000
39	545.1	19.0	13.9	.8048	.0	.8947	24.53	63.59	.000	.000
40	583.0	19.0	13.9	.9607	.0	.9569	24.53	63.59	.000	.000

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00338 DELM = .569 REM = 942.0
V RUN = 121671-3 CF/2 = .00256 DELM = .576 REM = 1232.0
PLATE = 9 UINF = 22.9 DEL2 = .0710 DEL3 = 1.543
X(IN) = 34.00 GM = 3.867 THETA = .1039 DEL4 = 5.968
K(E06) = -.3250 GAM = -.873 BETA = .238 H = 1.458

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.6	0.0000	0.00	91.46	1.000	1.000
2	3.8	3.7	2.5	.0043	-12.4	.0067	4.46	87.27	.858	.911
3	4.3	4.2	2.9	.0049	-11.9	.0077	4.96	86.35	.843	.892
4	4.9	4.6	3.2	.0055	-11.5	.0087	5.48	85.58	.827	.876
5	5.4	5.0	3.6	.0062	-11.0	.0097	5.92	84.64	.813	.856
6	6.0	5.4	4.0	.0068	-10.6	.0107	6.44	83.90	.797	.840
7	6.6	5.8	4.4	.0074	-10.2	.0117	6.94	83.12	.781	.823
8	7.1	6.2	4.7	.0081	-9.9	.0127	7.46	82.47	.766	.810
9	7.7	6.6	5.0	.0087	-9.6	.0137	7.85	81.91	.752	.798
10	8.2	7.0	5.4	.0093	-9.2	.0147	8.25	81.17	.739	.782
11	8.8	7.3	5.7	.0100	-8.9	.0157	8.72	80.66	.725	.771
12	9.9	8.0	6.2	.0112	-8.4	.0177	9.47	79.69	.702	.750
13	11.1	8.5	6.7	.0125	-7.9	.0197	10.07	78.76	.684	.730
14	12.2	8.9	7.1	.0137	-7.5	.0217	10.58	77.95	.669	.713
15	13.3	9.3	7.4	.0150	-7.2	.0237	11.06	77.30	.655	.699
16	15.0	9.9	7.9	.0169	-6.7	.0267	11.76	76.40	.634	.679
17	16.7	10.3	8.3	.0188	-6.3	.0297	12.23	75.56	.621	.661
18	18.3	10.6	8.7	.0207	-5.9	.0327	12.58	74.86	.612	.646
19	20.0	10.9	9.0	.0226	-5.6	.0357	12.90	74.26	.604	.632
20	22.3	11.2	9.3	.0251	-5.3	.0397	13.27	73.74	.598	.620
21	24.5	11.5	9.5	.0276	-5.0	.0437	13.63	73.22	.586	.604
22	28.4	11.9	9.9	.0321	-4.7	.0507	14.18	72.54	.574	.592
23	32.9	12.2	10.3	.0371	-4.3	.0587	14.52	71.85	.569	.575
24	38.5	12.5	10.6	.0434	-4.0	.0687	14.85	71.25	.565	.560
25	46.9	12.9	10.9	.0529	-3.7	.0837	15.36	70.68	.554	.545
26	55.4	13.3	11.2	.0624	-3.4	.0987	15.77	70.08	.555	.527
27	66.6	13.6	11.4	.0750	-3.1	.1187	16.13	69.63	.555	.512
28	80.6	13.9	11.7	.0908	-2.9	.1437	16.49	69.09	.556	.493
29	100.2	14.2	12.0	.1129	-2.6	.1787	16.93	68.49	.556	.468
30	122.7	14.7	12.3	.1381	-2.3	.2187	17.45	67.95	.552	.442
31	150.7	15.2	12.6	.1697	-2.0	.2687	18.02	67.41	.542	.411
32	206.8	16.0	13.1	.2328	-1.5	.3687	19.04	66.44	.501	.344
33	262.9	16.8	13.5	.2960	-1.1	.4687	19.98	65.63	.435	.273
34	333.0	17.7	13.9	.3749	-.7	.5937	21.04	64.90	.322	.191
35	417.1	18.6	14.3	.4696	-.3	.7437	22.11	64.21	.150	.097
36	501.2	19.1	14.5	.5643	-.1	.8937	22.74	63.78	.076	.030
37	585.3	19.3	14.6	.6590	-.0	1.0437	22.91	63.63	.013	.000
38	669.5	19.3	14.6	.7537	.0	1.1937	22.91	63.57	.000	.000
39	781.6	19.3	14.6	.8800	.0	1.3937	22.91	63.57	.000	.000

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00325 DELM = 1.079 REM = 1022.0
V RUN = 121671-3 CF/2 = .00250 DELM = 1.070 REM = 1441.0
PLATE = 12 UINF = 22.2 DEL2 = .0892 DEL3 = 1.958
X(IN) = 46.00 GM = 3.790 THETA = .1257 DEL4 = 7.422
K(E06) = -.2538 GAM = -.804 BETA = .222 H = 1.454

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.0	0.0000	0.00	91.51	1.000	1.000
2	3.6	3.4	2.4	.0034	-12.8	.0067	3.91	87.50	.869	.913
3	4.1	3.8	2.8	.0039	-12.4	.0077	4.28	86.65	.857	.894
4	4.7	4.1	3.1	.0043	-12.0	.0087	4.62	85.94	.846	.879
5	5.2	4.4	3.4	.0048	-11.5	.0097	4.98	85.05	.834	.859
6	5.8	4.7	3.8	.0053	-11.2	.0107	5.35	84.37	.822	.845
7	6.3	5.1	4.2	.0058	-10.7	.0117	5.76	83.57	.809	.827
8	6.8	5.5	4.6	.0063	-10.4	.0127	6.22	82.86	.793	.812
9	7.4	5.9	4.9	.0068	-10.1	.0137	6.67	82.33	.777	.800
10	7.9	6.2	5.2	.0073	-9.8	.0147	7.07	81.76	.764	.787
11	9.0	6.9	5.7	.0083	-9.3	.0167	7.81	80.81	.739	.767
12	10.1	7.5	6.2	.0093	-8.8	.0187	8.55	79.92	.715	.747
13	11.1	8.1	6.7	.0103	-8.3	.0207	9.24	79.03	.692	.728
14	12.2	8.6	7.0	.0113	-7.9	.0227	9.77	78.31	.675	.712
15	13.8	9.2	7.6	.0128	-7.4	.0257	10.53	77.33	.650	.690
16	15.4	9.6	8.1	.0143	-6.9	.0287	11.21	76.34	.628	.668
17	17.0	10.2	8.4	.0158	-6.5	.0317	11.60	75.72	.616	.654
18	19.2	10.5	8.9	.0178	-6.1	.0357	12.08	74.82	.604	.634
19	21.3	11.0	9.2	.0195	-5.8	.0397	12.50	74.34	.598	.624
20	23.5	11.3	9.4	.0218	-5.6	.0437	12.96	73.89	.580	.613
21	27.2	11.7	9.8	.0252	-5.1	.0507	13.34	73.28	.568	.594
22	31.5	12.1	10.2	.0292	-4.8	.0587	13.74	72.44	.560	.580
23	36.9	12.4	10.6	.0342	-4.4	.0687	14.14	71.71	.553	.561
24	45.0	12.9	11.0	.0417	-4.0	.0837	14.71	70.99	.543	.543
25	53.0	13.2	11.2	.0491	-3.7	.0987	15.00	70.51	.541	.529
26	63.8	13.5	11.5	.0591	-3.5	.1187	15.38	70.09	.539	.517
27	77.2	13.8	11.9	.0715	-3.2	.1437	15.77	69.48	.537	.497
28	96.0	14.2	12.3	.0889	-2.9	.1787	16.17	69.00	.540	.480
29	117.5	14.6	12.3	.1093	-2.6	.2187	16.60	68.43	.541	.457
30	157.8	15.1	12.7	.1462	-2.2	.2937	17.24	67.65	.539	.421
31	211.5	15.9	13.2	.1959	-1.7	.3937	18.00	66.78	.517	.364
32	265.3	16.6	13.6	.2457	-1.4	.4937	18.67	66.08	.478	.320
33	319.0	17.2	13.9	.2955	-1.1	.5937	19.56	65.57	.421	.275
34	399.6	18.0	14.2	.3701	-.7	.7437	20.50	64.94	.311	.197
35	480.2	18.8	14.6	.4447	-.4	.8937	21.39	64.27	.192	.124
36	587.7	19.3	14.9	.5443	-.1	1.0937	22.03	63.89	.070	.037
37	695.1	19.5	15.0	.6438	.0	1.2937	22.21	63.48	.008	.000
38	802.6	19.5	15.0	.7433	.0	1.4937	22.20	63.45	.000	.000
39	807.5	19.5	15.0	.7478	.0	1.5025	22.21	63.45	.000	.000

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00314 DELH = 1.279 REM = 1175.0
W RUN = 121671-3 CF/2 = .00246 DELM = 1.250 REM = 1590.0
PLATE = 15 UINF = 21.5 DEL2 = .1056 DEL3 = 2.322
X(IN) = 58.00 GM = 3.801 THETA = .1428 DEL4 = 5.427
K(E06)= -.2100 GAM = -.785 BETA = .207 H = 1.425

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.4	0.0000	0.00	91.20	1.000	1.000
2	3.9	3.7	2.6	.0031	-13.1	.0075	4.07	87.12	.855	.908
3	4.4	4.0	2.9	.0035	-12.7	.0085	4.42	86.41	.843	.892
4	4.9	4.3	3.2	.0040	-12.2	.0095	4.74	85.52	.832	.871
5	5.4	4.6	3.6	.0044	-11.8	.0105	5.09	84.79	.820	.854
6	5.9	5.0	3.9	.0048	-11.5	.0115	5.45	84.13	.807	.840
7	6.4	5.3	4.3	.0052	-11.1	.0125	5.84	83.42	.794	.823
8	7.0	5.7	4.7	.0056	-10.7	.0135	6.26	82.74	.779	.808
9	7.5	6.1	4.9	.0061	-10.4	.0145	6.72	82.27	.762	.797
10	8.5	6.9	5.4	.0069	-10.0	.0165	7.59	81.40	.732	.777
11	9.5	7.5	6.0	.0077	-9.4	.0185	8.16	80.36	.712	.753
12	10.6	7.9	6.4	.0086	-9.0	.0205	8.59	79.65	.698	.737
13	11.6	8.2	6.9	.0094	-8.5	.0225	8.97	78.76	.685	.717
14	12.6	8.7	7.2	.0103	-8.1	.0245	9.47	78.13	.668	.702
15	14.2	9.4	7.7	.0115	-7.7	.0275	10.38	77.73	.639	.684
16	15.7	9.9	8.1	.0128	-7.2	.0305	10.82	76.46	.621	.664
17	17.3	10.4	8.6	.0140	-6.8	.0335	11.34	75.69	.604	.645
18	18.8	10.8	8.9	.0153	-6.5	.0365	11.77	75.21	.590	.634
19	20.9	11.2	9.2	.0170	-6.2	.0405	12.21	74.52	.576	.618
20	23.0	11.5	9.6	.0187	-5.8	.0445	12.67	73.89	.565	.603
21	25.5	11.8	9.9	.0207	-5.6	.0495	12.95	73.53	.554	.595
22	29.2	12.2	10.1	.0237	-5.2	.0565	13.37	72.84	.543	.578
23	33.3	12.5	10.6	.0270	-4.8	.0645	13.72	72.10	.534	.560
24	38.5	12.8	10.8	.0312	-4.5	.0745	14.02	71.62	.529	.548
25	46.2	13.1	11.2	.0375	-4.2	.0895	14.36	71.02	.525	.533
26	56.5	13.5	11.4	.0459	-3.9	.1095	14.75	70.54	.522	.520
27	74.6	14.0	11.9	.0606	-3.5	.1445	15.29	69.79	.519	.495
28	95.3	14.4	12.2	.0774	-3.1	.1845	15.73	69.09	.522	.475
29	121.1	14.8	12.6	.0984	-2.8	.2345	16.17	68.46	.527	.462
30	159.9	15.3	13.0	.1298	-2.4	.3095	16.70	67.71	.531	.420
31	198.6	15.7	13.3	.1613	-2.1	.3845	17.18	67.29	.528	.396
32	250.3	16.3	13.6	.2033	-1.8	.4845	17.85	66.57	.508	.355
33	327.8	17.1	14.1	.2662	-1.5	.6345	18.71	65.69	.451	.287
34	405.3	17.9	14.5	.3291	-.9	.7845	19.55	65.06	.367	.231
35	509.6	18.7	14.9	.4130	-.5	.9845	20.46	64.33	.228	.150
36	611.9	19.3	15.2	.4970	-.2	1.1845	21.14	63.79	.100	.075
37	715.3	19.6	15.3	.5809	-.0	1.3845	21.47	63.48	.025	.023
38	818.6	19.7	15.4	.6648	.0	1.5845	21.51	63.36	.000	.000
39	921.9	19.6	15.4	.7487	.0	1.7845	21.50	63.36	.000	.000

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00308 DELH = 1.492 REM = 1330.0
W RUN = 121671-3 CF/2 = .00242 DELM = 1.442 REM = 1747.0
PLATE = 18 UINF = 21.0 DEL2 = .1223 DEL3 = 2.676
X(IN) = 70.00 GM = 3.706 THETA = .1686 DEL4 = 9.918
K(E06)= -.1920 GAM = -.767 BETA = .200 H = 1.415

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.6	0.0000	0.00	91.20	1.000	1.000
2	3.1	3.3	2.1	.0022	-13.7	.0062	3.50	87.83	.870	.923
3	3.6	3.6	2.4	.0026	-13.3	.0072	3.82	87.18	.858	.908
4	4.1	3.9	2.7	.0030	-12.9	.0082	4.14	86.50	.846	.892
5	4.6	4.2	3.1	.0033	-12.5	.0092	4.50	85.73	.833	.875
6	5.1	4.6	3.5	.0037	-12.1	.0102	4.87	85.02	.820	.858
7	5.6	4.9	3.8	.0040	-11.8	.0112	5.24	84.40	.806	.844
8	6.1	5.3	4.2	.0044	-11.4	.0122	5.62	83.72	.792	.829
9	6.6	5.7	4.5	.0048	-11.0	.0132	6.00	83.07	.777	.814
10	7.1	6.0	4.7	.0051	-10.8	.0142	6.40	82.74	.763	.806
11	7.6	6.3	5.1	.0055	-10.5	.0152	6.72	82.12	.752	.792
12	8.6	6.8	5.7	.0062	-9.9	.0172	7.26	81.05	.732	.767
13	9.6	7.4	6.1	.0070	-9.4	.0192	7.83	80.28	.710	.750
14	10.6	7.9	6.6	.0077	-8.9	.0212	8.43	79.35	.689	.728
15	12.1	8.7	7.1	.0088	-8.4	.0242	9.24	78.46	.659	.708
16	13.6	9.4	7.6	.0099	-7.9	.0272	9.97	77.54	.633	.687
17	15.1	9.8	8.0	.0110	-7.5	.0302	10.42	76.88	.617	.672
18	17.1	10.3	8.4	.0124	-7.1	.0342	10.95	76.10	.599	.654
19	19.1	10.8	9.0	.0139	-6.5	.0382	11.42	75.06	.583	.629
20	21.1	11.1	9.3	.0153	-6.2	.0422	11.80	74.52	.570	.617
21	23.1	11.4	9.6	.0168	-6.0	.0462	12.11	74.10	.560	.607
22	25.6	11.8	9.9	.0186	-5.6	.0512	12.48	73.50	.548	.593
23	29.1	12.2	10.2	.0212	-5.3	.0582	12.90	72.87	.535	.578
24	33.1	12.5	10.5	.0241	-5.0	.0662	13.21	72.40	.526	.567
25	38.1	12.8	10.8	.0277	-4.7	.0762	13.52	71.83	.516	.554
26	45.6	13.2	11.1	.0332	-4.4	.0912	13.96	71.29	.507	.540
27	59.7	13.5	11.5	.0435	-4.0	.1212	14.36	70.54	.499	.520
28	68.2	13.9	11.8	.0498	-3.7	.1362	14.69	70.09	.494	.509
29	85.2	14.3	12.2	.0641	-3.4	.1762	15.16	69.46	.488	.492
30	113.2	14.8	12.5	.0823	-3.0	.2262	15.65	68.79	.480	.471
31	150.7	15.2	12.9	.1096	-2.7	.3012	16.06	68.19	.479	.449
32	200.8	15.8	13.3	.1461	-2.2	.4012	16.71	67.41	.472	.413
33	275.9	16.5	13.8	.2007	-1.8	.5512	17.44	66.54	.450	.364
34	350.9	17.2	14.2	.2553	-1.4	.7012	18.21	65.84	.406	.314
35	451.0	18.0	14.6	.3281	-.9	.9012	19.12	65.06	.323	.244
36	551.1	18.8	14.9	.4010	-.6	1.1012	19.92	64.48	.219	.179
37	676.3	19.5	15.3	.4920	-.3	1.3512	20.65	63.85	.093	.091
38	801.4	19.8	15.5	.5830	-.1	1.6012	20.99	63.49	.020	.029
39	951.5	19.9	15.6	.6923	.0	1.9012	21.04	63.36	.000	.000
40	978.2	19.8	15.6	.7117	.0	1.9546	21.04	63.36	.000	.000
41	1103.4	19.8	15.6	.8028	.0	2.2046	21.04	63.36	.000	.000

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00702 DELH = 1.698 REM = 1444.0
W RUN = 121671-3 CF/2 = .00240 DELM = 1.606 REM = 1893.0
PLATE = 21 UINF = 20.6 DEL2 = .1358 DEL3 = 3.009
X(IN) = 82.00 GM = 3.698 THETA = .1760 DEL4 = 11.121
K(E06)= -.1660 GAM = -.766 BETA = .199 H = 1.414

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.6	0.0000	0.00	91.30	1.000	1.000
2	3.5	3.2	2.4	.0024	-13.7	.0072	3.36	87.59	.871	.913
3	4.0	3.6	2.7	.0027	-13.3	.0082	3.68	86.85	.859	.896
4	4.5	3.9	3.0	.0030	-12.9	.0092	3.99	86.23	.847	.881
5	5.0	4.1	3.3	.0033	-12.5	.0102	4.28	85.52	.836	.864
6	5.5	4.5	3.7	.0037	-12.1	.0112	4.62	84.78	.823	.846
7	6.0	4.8	4.0	.0040	-11.8	.0122	5.01	84.19	.809	.833
8	6.5	5.2	4.3	.0047	-11.5	.0132	5.38	83.60	.795	.819
9	6.9	5.5	4.7	.0046	-11.1	.0142	5.77	83.04	.782	.806
10	7.4	5.8	4.9	.0050	-10.9	.0152	6.06	82.62	.769	.796
11	8.4	6.4	5.4	.0056	-10.4	.0172	6.65	81.67	.747	.773
12	9.4	7.0	6.0	.0063	-9.8	.0192	7.27	80.72	.724	.751
13	10.4	7.7	6.3	.0069	-9.5	.0212	7.95	80.12	.697	.737
14	11.3	8.2	6.8	.0076	-9.0	.0232	8.51	79.26	.678	.716
15	12.3	8.7	7.2	.0082	-8.6	.0252	8.97	78.61	.659	.701
16	13.3	9.1	7.5	.0088	-8.3	.0272	9.38	78.04	.644	.687
17	14.8	9.5	7.9	.0098	-7.9	.0302	9.88	77.30	.625	.669
18	16.2	10.0	8.3	.0108	-7.5	.0332	10.39	76.61	.609	.653
19	18.7	10.6	9.0	.0124	-6.9	.0382	11.00	75.39	.585	.623
20	21.1	11.1	9.3	.0140	-6.5	.0432	11.54	74.79	.566	.609
21	24.5	11.8	9.8	.0163	-6.0	.0502	12.26	74.01	.540	.590
22	28.4	12.1	10.3	.0189	-5.5	.0582	12.57	73.14	.529	.568
23	33.3	12.5	10.6	.0221	-5.2	.0682	12.90	72.55	.519	.553
24	38.2	12.8	11.0	.0254	-4.8	.0782	13.27	71.86	.507	.534
25	45.6	13.2	11.3	.0302	-4.6	.0932	13.64	71.38	.497	.522
26	57.8	13.5	11.7	.0383	-4.1	.1182	13.98	70.66	.491	.502
27	70.0	13.8	11.9	.0464	-3.9	.1432	14.31	70.18	.486	.486
28	87.1	14.2	12.3	.0578	-3.5	.1782	14.69	69.58	.481	.466
29	106.7	14.5	12.5	.0707	-3.3	.2182	15.04	69.10	.477	.450
30	131.1	14.9	12.9	.0869	-3.0	.2682	15.41	68.68	.473	.435
31	167.8	15.3	13.1	.1112	-2.7	.3432	15.87	68.07	.466	.413
32	216.7	15.9	13.5	.1436	-2.3	.4432	16.43	67.41	.454	.383
33	295.0	16.5	13.9	.1922	-1.9	.5932	17.07	66.66	.438	.345
34	387.7	17.4	14.4	.2570	-1.4	.7932	17.98	65.81	.400	.293
35	485.5	18.1	14.9	.3218	-1.0	.9932	18.72	65.12	.330	.233
36	583.3	18.7	15.1	.3866	-.7	1.1932	19.41	64.55	.241	.174
37	729.9	19.5	15.5	.4837	-.3	1.4932	20.23	63.88	.113	.090
38	925.5	19.9	15.8	.6133	-.0	1.8932	20.62	63.37	.011	.000
39	1169.9	19.9	15.9	.7753	-.0	2.3932	20.63	63.34	.000	.000

DATE = 122171 (-0.15, -0.002)

T RUN = 122171-1 STNA = .00298 DELH = 1.824 REM = 1594.0
W RUN = 121671-3 CF/2 = .00238 DELM = 1.736 REM = 2002.0
PLATE = 23 UINF = 20.2 DEL2 = .1488 DEL3 = 3.285
X(IN) = 90.00 GM = 3.686 THETA = .1917 DEL4 = 12.105
K(E06)= -.1660 GAM = -.935 BETA = .212 H = 1.398

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-16.0	0.0000	0.00	91.17
2	3.0	2.9	2.0	.0019	-14.1	.0062	2.93	87.98
3	3.4	3.3	2.3	.0022	-13.9	.0072	3.36	87.44
4	3.9	3.7	2.6	.0025	-13.5	.0082	3.79	86.89
5	4.4	4.1	2.9	.0028	-13.1	.0092	4.19	86.26
6	4.9	4.5	3.2	.0031	-12.7	.0102	4.58	85.58
7	5.3	5.3	4.0	.0037	-12.0	.0122	5.33	84.22
8	6.8	5.9	4.5	.0043	-11.4	.0142	5.98	83.24
9	7.7	6.5	5.1	.0047	-10.8	.0162	6.57	82.24
10	8.7	7.2	5.6	.0054	-10.3	.0182	7.28	81.34
11	9.7	7.7	6.1	.0060	-9.8	.0202	7.90	80.45
12	10.6	8.1	6.6	.0066	-9.4	.0222	8.20	79.71
13	11.6	8.3	7.0	.0072	-9.0	.0242	8.43	79.03
14	13.0	9.2	7.4	.0081	-8.6	.0272	9.30	78.28
15	14.4	9.7	7.9	.0090	-8.1	.0302	9.85	77.42
16	16.3	10.2	9.4	.0102	-7.5	.0342	10.31	76.46
17	18.7	10.8	8.9	.0117	-7.0	.0392	10.96	75.60
18	21.1	11.3	9.3	.0132	-6.6	.0442	11.39	74.91
19	24.5	11.5	9.9	.0152	-6.1	.0512	11.64	73.95
20	28.3	12.0	10.2	.0176	-5.7	.0592	12.15	73.35
21	33.0	12.4	10.6	.0206	-5.4	.0692	12.55	72.76
22	40.2	12.9	11.0	.0250	-4.9	.0842	13.03	71.92
23	49.8	13.3	11.5	.0310	-4.5	.1142	13.47	71.14
24	66.5	13.8	11.9	.0413	-4.1	.1392	13.97	70.51
25	90.3	14.3	12.3	.0562	-3.6	.1892	14.45	69.67
26	126.2	14.8	12.9	.0784	-3.1	.2642	14.99	68.77
27	173.9	15.4	13.2	.1081	-2.7	.3642	15.54	68.07
28	233.6	16.0	13.7	.1452	-2.3	.4892	16.15	67.35
29	305.2	16.7	14.1	.1897	-1.9	.6392	16.85	66.54
30	376.8	17.2	14.4	.2342	-1.6	.7892	17.41	66.03
31	472.3	17.9	14.8	.2935	-1.2	.9892	18.11	65.36
32	567.8	18.6	15.1	.3529	-.9	1.1892	18.78	64.79
33	711.1	19.4	15.5	.4419	-.5	1.4892	19.60	64.12
34	902.0	19.9	15.8	.5605	-.1	1.8892	20.16	63.52
35	1093.0	20.0	16.0	.6792	-.0	2.2892	20.21	63.34
36	1284.0	20.0	16.0	.7979	-.0	2.6892	20.21	63.34

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00712 DELM = .118 REM = 106.0
V RUN = 122271-2 CF/2 = .00397 DELM = .283 REM = 453.0
PLATE = 1 UINF = 29.4 DEL2 = .0069 DEL3 = .128
X(IN) = 2.00 GM = 3.688 THETA = .0259 DEL4 = .471
K(E06)= -.4460 GAM = -.444 BETA = .074 M = 1.455

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T
1	.0	0.0	.0	0.0000	-8.6	0.0000	0.00	91.75
2	4.8	4.2	3.0	.0402	-5.6	.0093	9.07	81.82
3	5.7	4.9	3.5	.0478	-5.0	.0063	9.31	79.97
4	6.6	5.5	4.0	.0555	-4.6	.0073	10.45	79.54
5	7.5	6.0	4.4	.0631	-4.2	.0083	11.49	77.35
6	8.4	6.6	4.9	.0707	-3.8	.0093	12.55	76.13
7	9.3	7.1	5.1	.0783	-3.5	.0103	13.45	75.20
8	10.2	7.5	5.3	.0959	-3.3	.0113	14.22	74.33
9	11.1	7.9	5.6	.0935	-3.0	.0123	14.97	73.38
10	12.0	8.2	5.8	.1011	-2.8	.0133	15.68	72.72
11	12.9	8.5	6.0	.1087	-2.6	.0143	16.19	72.12
12	13.9	8.7	6.2	.1163	-2.4	.0153	16.64	71.58
13	14.8	9.0	6.4	.1239	-2.3	.0163	17.05	71.01
14	15.7	9.2	6.5	.1315	-2.1	.0173	17.44	70.53
15	17.5	9.5	6.5	.1467	-1.8	.0193	18.14	69.60
16	19.3	9.9	7.0	.1620	-1.6	.0213	18.82	68.97
17	21.1	10.2	7.1	.1772	-1.5	.0233	19.41	68.42
18	22.9	10.5	7.3	.1924	-1.3	.0253	19.89	67.94
19	24.7	10.7	7.4	.2076	-1.2	.0273	20.31	67.58
20	26.6	10.9	7.5	.2228	-1.1	.0293	20.67	67.22
21	29.3	11.1	7.6	.2456	-1.0	.0323	21.09	66.80
22	32.0	11.2	7.7	.2684	-.9	.0353	21.37	66.47
23	35.6	11.4	7.9	.2989	-.7	.0393	21.66	66.01
24	40.2	11.6	8.0	.3369	-.6	.0443	22.05	65.68
25	44.7	11.8	8.1	.3749	-.5	.0493	22.37	65.38
26	51.0	12.0	8.2	.4282	-.4	.0563	22.76	65.05
27	58.3	12.2	8.3	.4890	-.3	.0643	23.16	64.68
28	67.4	12.4	8.3	.5651	-.3	.0743	23.60	64.57
29	81.0	12.7	8.4	.6792	-.2	.0893	24.20	64.20
30	99.1	13.2	8.5	.8314	-.1	.1093	25.02	63.95
31	117.3	13.5	8.6	.9835	-.1	.1293	25.69	63.80
32	149.0	14.1	8.6	1.2497	-.0	.1643	26.80	63.65
33	194.4	14.8	8.6	1.6301	.0	.2143	28.12	63.58
34	239.7	15.2	8.6	2.0104	.0	.2643	28.94	63.55
35	353.1	15.5	8.6	2.9613	-.0	.3897	29.42	63.61
36	387.6	15.5	8.6	3.2502	-.0	.4273	29.41	63.61
37	455.6	15.5	8.6	3.8207	-.0	.5023	29.40	63.61

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00509 DELM = .289 REM = 261.0
V RUN = 122271-2 CF/2 = .00380 DELM = .396 REM = 555.0
PLATE = 3 UINF = 26.8 DEL2 = .0186 DEL3 = .371
X(IN) = 10.00 GM = 4.002 THETA = .0399 DEL4 = 1.485
K(E06)= -.0000 GAM = -1.042 BETA = .179 M = 1.449

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-11.6	0.0000	0.00	91.79	1.000	1.000
2	4.8	4.4	3.0	.0156	-9.1	.0059	7.48	85.49	.731	.826
3	5.6	4.9	3.5	.0182	-8.5	.0069	8.32	83.98	.695	.783
4	6.4	5.4	3.9	.0209	-7.9	.0079	9.13	82.69	.669	.744
5	7.2	5.8	4.4	.0235	-7.4	.0089	9.90	81.43	.641	.711
6	8.0	6.3	4.9	.0261	-7.0	.0099	10.64	80.45	.614	.683
7	8.9	6.7	5.2	.0288	-6.6	.0109	11.34	79.53	.589	.657
8	9.7	7.1	5.5	.0314	-6.3	.0119	11.98	78.75	.567	.634
9	10.5	7.4	5.8	.0340	-6.0	.0129	12.58	77.89	.546	.609
10	11.3	7.7	6.1	.0366	-5.8	.0139	13.10	77.17	.527	.589
11	12.1	8.0	6.4	.0393	-5.4	.0149	13.62	76.49	.508	.569
12	12.9	8.3	6.7	.0419	-5.1	.0159	14.15	75.86	.490	.550
13	13.7	8.6	6.9	.0445	-4.9	.0169	14.65	75.32	.473	.534
14	14.5	8.9	7.2	.0472	-4.6	.0179	15.10	74.75	.458	.517
15	15.3	9.1	7.4	.0498	-4.4	.0189	15.50	74.19	.444	.501
16	16.1	9.4	7.6	.0524	-4.2	.0199	15.86	73.69	.432	.489
17	17.7	9.7	7.8	.0577	-3.9	.0219	16.46	72.93	.412	.467
18	19.4	10.0	8.2	.0629	-3.6	.0239	16.97	72.27	.396	.448
19	21.0	10.3	8.5	.0682	-3.3	.0259	17.46	71.61	.380	.422
20	22.6	10.6	8.7	.0734	-3.1	.0279	17.94	71.10	.365	.407
21	25.0	10.9	9.0	.0813	-2.8	.0309	18.48	70.36	.349	.384
22	27.5	11.1	9.2	.0892	-2.6	.0339	18.83	69.96	.340	.371
23	29.9	11.3	9.4	.0971	-2.4	.0369	19.20	69.48	.331	.356
24	33.1	11.5	9.6	.1076	-2.2	.0409	19.55	68.96	.323	.334
25	36.4	11.7	9.7	.1181	-2.1	.0449	19.82	68.63	.314	.329
26	40.4	11.9	9.9	.1313	-1.9	.0499	20.19	68.15	.311	.310
27	46.9	12.2	10.2	.1523	-1.6	.0579	20.61	67.61	.305	.289
28	55.0	12.4	10.4	.1766	-1.4	.0679	21.01	67.07	.302	.266
29	63.0	12.6	10.5	.2048	-1.2	.0779	21.36	66.71	.300	.249
30	75.2	12.9	10.6	.2442	-1.0	.0929	21.82	66.19	.296	.221
31	87.3	13.1	10.9	.2837	-.9	.1079	22.22	65.89	.292	.203
32	103.5	13.4	11.1	.3363	-.7	.1279	22.68	65.44	.285	.171
33	123.7	13.7	11.2	.4020	-.6	.1529	23.15	65.05	.277	.140
34	144.1	14.2	11.5	.4334	-.2	.2029	24.03	64.53	.231	.089
35	204.6	14.7	11.6	.6648	-.2	.2529	24.88	64.20	.175	.051
36	245.0	15.1	11.7	.7962	-.1	.3029	25.61	63.95	.119	.018
37	285.5	15.4	11.8	.9276	-.1	.3529	26.19	63.83	.074	.000
38	366.3	15.8	11.8	1.1904	-.0	.4529	26.76	63.74	.024	.000
39	447.2	15.8	11.9	1.4532	-.0	.5529	26.81	63.74	.005	.000
40	505.4	15.8	11.9	1.6421	-.0	.6248	26.82	63.74	.000	.000
41	566.0	15.8	11.9	1.8393	-.0	.6995	26.82	63.74	.000	.000

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00470 DELM = .456 REM = 374.0
V RUN = 122271-2 CF/2 = .00383 DELM = .547 REM = 665.0
PLATE = 6 UINF = 24.4 DEL2 = .0293 DEL3 = .545
X(IN) = 22.00 GM = 3.539 THETA = .0522 DEL4 = 2.244
K(E06)= -.4698 GAM = -.744 BETA = .115 M = 1.418

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-12.8	0.0000	0.00	91.82	1.000	1.000
2	4.6	4.0	2.9	.0104	-10.3	.0061	6.24	86.35	.744	.835
3	5.4	4.6	3.4	.0121	-9.8	.0073	7.07	85.17	.715	.799
4	6.1	5.1	3.8	.0137	-9.2	.0083	7.94	83.84	.675	.759
5	6.8	5.7	4.1	.0154	-8.7	.0093	8.88	82.96	.639	.727
6	7.6	6.2	4.6	.0171	-8.2	.0103	9.61	81.73	.606	.694
7	8.3	6.7	5.0	.0187	-7.8	.0113	10.34	80.87	.576	.665
8	9.1	7.1	5.4	.0204	-7.4	.0123	10.96	80.04	.551	.643
9	9.8	7.4	5.6	.0221	-7.0	.0133	11.49	79.20	.529	.617
10	10.5	7.7	6.1	.0237	-6.7	.0143	11.94	78.52	.511	.596
11	11.3	7.9	6.4	.0254	-6.5	.0153	12.32	77.98	.496	.579
12	12.8	8.4	6.9	.0287	-5.9	.0173	13.09	76.79	.466	.543
13	14.2	9.0	7.3	.0321	-5.5	.0193	13.90	75.83	.437	.517
14	15.7	9.3	7.7	.0354	-5.1	.0213	14.42	74.93	.413	.489
15	17.2	9.7	8.1	.0387	-4.7	.0233	14.96	74.25	.392	.464
16	18.7	10.0	8.4	.0421	-4.4	.0253	15.44	73.58	.374	.441
17	20.2	10.2	8.7	.0454	-4.1	.0273	15.77	72.97	.361	.421
18	21.6	10.4	8.9	.0487	-3.9	.0293	16.12	72.39	.348	.406
19	23.8	10.7	9.2	.0537	-3.6	.0323	16.63	71.85	.329	.389
20	26.1	11.0	9.5	.0587	-3.3	.0353	17.04	71.13	.314	.366
21	29.0	11.3	9.8	.0654	-3.0	.0393	17.44	70.53	.300	.347
22	32.0	11.4	10.0	.0721	-2.8	.0433	17.73	70.11	.291	.333
23	36.4	11.7	10.3	.0821	-2.5	.0493	18.08	69.39	.280	.309
24	40.9	11.9	10.4	.0920	-2.4	.0553	18.39	69.06	.271	.299
25	48.2	12.1	10.7	.1087	-2.1	.0653	18.80	68.47	.259	.277
26	55.6	12.3	10.9	.1254	-1.9	.0753	19.09	68.04	.253	.263
27	66.7	12.5	11.1	.1504	-1.7	.0903	19.42	67.52	.247	.243
28	81.5	12.8	11.4	.1837	-1.4	.1103	19.80	66.95	.240	.218
29	100.0	13.0	11.6	.2253	-1.2	.1353	20.21	66.47	.232	.195
30	125.9	13.4	11.9	.2837	-.9	.1703	20.72	65.96	.221	.169
31	162.8	13.8	12.1	.3670	-.7	.2203	21.43	65.41	.201	.134
32	199.8	14.2	12.3	.4503	-.5	.2703	22.02	64.99	.177	.102
33	255.2	14.7	12.5	.5753	-.3	.3453	22.75	64.56	.134	.065
34	329.2	15.2	12.7	.7419	-.1	.4453	23.61	64.17	.075	.025
35	403.1	15.6	12.8	.9085	-.0	.5453	24.17	63.96	.031	.000
36	477.0	15.7	12.8	1.0751	.0	.6453	24.38	63.87	.000	.000
37	551.0	15.7	12.8	1.2418	.0	.7453	24.41	63.87	.000	.000
38	624.9	15.7	12.8	1.4084	.0	.8453	24.40	63.87	.000	.000

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00452 DELM = .595 REM = 459.0
V RUN = 122271-2 CF/2 = .00381 DELM = .849 REM = 714.0
PLATE = 9 UINF = 23.0 DEL2 = .0382 DEL3 = .746
X(IN) = 34.00 GM = 3.733 THETA = .0564 DEL4 = 2.795
K(E06)= -.3350 GAM = -.619 BETA = .091 M = 1.396

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.3	0.0000	0.00	91.96	1.000	1.000
2	4.5	4.1	2.9	.0096	-10.8	.0065	6.05	86.76	.731	.837
3	5.2	4.6	3.3	.0099	-10.3	.0075	6.72	85.58	.701	.800
4	5.9	5.0	3.7	.0112	-9.4	.0085	7.31	84.49	.676	.765
5	6.6	5.4	4.0	.0125	-9.3	.0095	7.93	83.49	.648	.733
6	7.3	5.9	4.5	.0138	-8.8	.0105	8.55	82.53	.621	.703
7	8.0	6.3	4.8	.0151	-8.5	.0115	9.16	81.79	.594	.680
8	8.7	6.7	5.2	.0164	-8.1	.0125	9.75	81.02	.569	.656
9	9.4	7.1	5.5	.0177	-7.8	.0135	10.32	80.38	.547	.633
10	10.1	7.4	5.9	.0190	-7.4	.0145	10.91	79.59	.521	.610
11	11.5	8.1	6.5	.0216	-6.8	.0165	11.75	78.31	.479	.570
12	12.9	8.6	7.0	.0243	-6.3	.0185	12.56	77.29	.443	.537
13	14.3	9.1	7.4	.0269	-5.9	.0205	13.23	76.40	.414	.509
14	15.7	9.5	7.9	.0295	-5.5	.0225	13.77	75.53	.391	.481
15	17.0	9.7	8.1	.0321	-5.2	.0245	14.20	74.88	.372	.460
16	18.4	10.0	8.4	.0347	-4.9	.0265	14.57	74.16	.357	.438
17	19.8	10.3	8.8	.0373	-4.6	.0285	14.94	73.47	.341	.415
18	21.9	10.6	9.1	.0412	-4.2	.0315	15.42	72.79	.321	.397
19	24.0	10.9	9.4	.0452	-3.9	.0345	15.83	72.15	.304	.374
20	26.1	11.1	9.6	.0491	-3.7	.0375	16.16	71.73	.291	.360
21	28.2	11.3	9.9	.0530	-3.4	.0405	16.47	71.16	.278	.341
22	30.9	11.5	10.1	.0582	-3.2	.0445	16.91	70.65	.265	.324
23	34.4	11.8	10.4	.0647	-2.9	.0495	17.13	70.11	.252	.307
24	37.9	11.9	10.5	.0713	-2.8	.0545	17.36	69.75	.246	.295
25	42.7	12.1	10.8	.0804	-2.5	.0615	17.66	69.15	.235	.276
26	48.3	12.3	11.0	.0909	-2.3	.0695	17.97	68.79	.226	.263
27	55.2	12.5	11.2	.1039	-2.1	.0795	18.24	68.34	.218	.247
28	65.7	12.7	11.4	.1235	-1.9	.0945	18.52	67.92	.212	.232
29	79.6	12.9	11.6	.1496	-1.7	.1145	18.80	67.44	.209	.213
30	93.4	13.1	11.9	.1758	-1.5	.1345	19.09	67.01	.205	.198
31	117.8	13.4	12.1	.2215	-1.2	.1695	19.50	66.47	.200	.175
32	152.5	13.7	12.3	.2868	-1.0	.2195	20.00	65.93	.196	.148
33	187.2	14.0	12.5	.3521	-.8	.2695	20.43	65.57	.179	.128
34	239.3	14.4	12.6	.4500	-.6	.3445	21.01	65.05	.156	.093
35	308.7	14.9	13.0	.5806	-.3	.4445	21.74	64.60	.113	.057
36	378.2	15.2	13.1	.7113	-.2	.5445	22.31	64.27	.069	.027
37	482.4	15.7	13.3	.9072	-.1	.6945	22.87	64.02	.020	.000
38	621.3	15.8	13.3	1.1684	-0.0	.8945	23.00	63.90	.000	.000
39	760.2	15.8	13.3	1.4296	-0.0	1.0945	23.00	63.90	.000	.000

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00461 DELM = .692 REM = 521.0
V RUN = 122271-2 CF/2 = .00379 DELM = .761 REM = 757.0
PLATE = 12 UINF = 22.0 DEL2 = .0453 DEL3 = .684
X(IN) = 46.00 GM = 3.649 THETA = .0659 DEL4 = 3.225
K(E06) = -.2630 GAM = -.525 BETA = .076 M = 1.379

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.6	0.0000	0.00	91.93	1.000	1.000
2	4.3	3.9	2.7	.0070	-11.2	.0065	5.48	86.94	.742	.839
3	4.9	4.3	3.1	.0061	-10.7	.0075	6.00	85.91	.718	.805
4	5.6	4.7	3.5	.0092	-10.2	.0085	6.60	84.93	.690	.774
5	6.3	5.1	3.8	.0103	-9.7	.0095	7.17	83.98	.665	.743
6	6.9	5.5	4.3	.0114	-9.3	.0105	7.63	83.09	.642	.714
7	7.6	5.8	4.7	.0125	-8.9	.0115	8.13	82.32	.618	.689
8	8.3	6.2	5.1	.0136	-8.5	.0125	8.61	81.49	.596	.662
9	8.9	6.5	5.4	.0147	-8.2	.0135	9.08	80.84	.574	.641
10	9.6	6.9	5.7	.0157	-7.9	.0145	9.54	80.10	.552	.617
11	10.2	7.2	6.0	.0170	-7.6	.0155	10.00	79.53	.531	.598
12	10.9	7.5	6.3	.0181	-7.3	.0165	10.41	78.93	.511	.579
13	11.6	7.8	6.6	.0192	-7.0	.0175	10.78	78.43	.494	.562
14	12.2	8.0	6.9	.0203	-6.8	.0185	11.15	77.99	.477	.548
15	13.6	8.6	7.2	.0225	-6.4	.0205	11.95	77.03	.439	.517
16	14.9	9.0	7.6	.0247	-6.0	.0225	12.57	76.19	.411	.489
17	16.2	9.4	8.0	.0269	-5.6	.0245	13.06	75.44	.388	.465
18	17.5	9.8	8.4	.0291	-5.2	.0265	13.58	74.70	.364	.441
19	18.9	10.1	8.6	.0313	-5.0	.0285	13.98	74.19	.346	.424
20	20.2	10.3	8.8	.0335	-4.8	.0305	14.27	73.71	.333	.408
21	21.5	10.5	9.1	.0357	-4.5	.0325	14.58	73.20	.319	.391
22	23.5	10.8	9.4	.0390	-4.2	.0355	15.03	72.51	.299	.369
23	25.5	11.1	9.7	.0423	-3.9	.0385	15.40	71.97	.282	.351
24	28.1	11.4	10.0	.0467	-3.6	.0425	15.80	71.34	.265	.330
25	30.8	11.6	10.2	.0511	-3.4	.0465	16.12	70.95	.251	.317
26	33.4	11.7	10.4	.0555	-3.2	.0505	16.31	70.44	.243	.308
27	36.1	12.0	10.7	.0632	-2.9	.0575	16.68	69.84	.228	.291
28	43.4	12.2	11.0	.0721	-2.6	.0655	17.02	69.24	.215	.280
29	50.0	12.5	11.3	.0831	-2.3	.0755	17.33	68.73	.204	.243
30	56.6	12.7	11.4	.0941	-2.2	.0855	17.59	68.40	.195	.232
31	66.6	12.9	11.6	.1106	-2.0	.1005	17.87	68.04	.187	.220
32	79.8	13.0	11.8	.1327	-1.8	.1205	18.13	67.56	.182	.202
33	96.4	13.2	12.1	.1602	-1.5	.1455	18.48	67.08	.173	.184
34	129.5	13.6	12.3	.2154	-1.2	.1955	18.88	66.47	.168	.180
35	179.2	14.0	12.6	.2980	-1.0	.2705	19.35	65.99	.158	.134
36	228.9	14.3	12.9	.3807	-.7	.3455	19.88	65.42	.145	.109
37	323.4	14.9	13.2	.5460	-.4	.4955	20.75	64.75	.104	.069
38	460.9	15.5	13.5	.7665	-.1	.6955	21.61	64.18	.041	.022
39	593.5	15.8	13.6	.9869	-.0	.8955	21.98	63.93	.005	.000
40	726.0	15.8	13.6	1.2074	-.0	1.0955	22.01	63.90	.000	.000
41	746.7	15.8	13.6	1.2419	-0.0	1.1268	22.02	63.90	.000	.000

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00432 DELM = .805 REM = 570.0
V RUN = 122271-2 CF/2 = .00377 DELM = .832 REM = 768.0
PLATE = 15 UINF = 21.4 DEL2 = .0511 DEL3 = .995
X(IN) = 58.00 GM = 3.608 THETA = .0688 DEL4 = 3.589
K(E06) = -.2180 GAM = -.446 BETA = .069 M = 1.376

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.8	0.0000	0.00	91.93	1.000	1.000
2	4.1	3.7	2.7	.0063	-11.5	.0064	4.94	87.21	.761	.845
3	4.8	4.3	3.0	.0073	-11.0	.0074	5.78	86.23	.720	.813
4	5.4	4.7	3.4	.0082	-10.6	.0084	6.36	85.29	.690	.782
5	6.1	5.2	3.8	.0092	-10.1	.0094	7.02	84.31	.660	.749
6	6.7	5.6	4.2	.0102	-9.7	.0104	7.53	83.51	.635	.723
7	7.3	5.9	4.5	.0112	-9.3	.0114	8.00	82.74	.613	.698
8	8.0	6.3	4.9	.0122	-8.9	.0124	8.46	82.00	.590	.673
9	8.6	6.6	5.3	.0131	-8.6	.0134	8.92	81.28	.568	.649
10	9.3	7.0	5.5	.0141	-8.3	.0144	9.41	80.72	.545	.631
11	9.9	7.3	5.8	.0151	-8.0	.0154	9.88	80.18	.522	.613
12	10.6	7.7	6.1	.0161	-7.8	.0164	10.34	79.69	.500	.595
13	11.8	8.2	6.6	.0180	-7.3	.0184	11.09	78.81	.463	.561
14	13.1	8.6	7.1	.0200	-6.8	.0204	11.61	77.59	.439	.527
15	14.4	9.0	7.4	.0220	-6.4	.0224	12.17	76.88	.412	.504
16	15.7	9.4	7.8	.0239	-6.0	.0244	12.62	76.07	.390	.477
17	17.6	9.9	8.3	.0269	-5.5	.0274	13.32	75.12	.357	.445
18	19.6	10.3	8.8	.0298	-5.0	.0304	13.96	74.10	.327	.411
19	21.5	10.7	9.2	.0327	-4.7	.0334	14.39	73.35	.307	.386
20	24.1	11.0	9.5	.0366	-4.4	.0374	14.85	72.72	.286	.365
21	26.0	11.2	9.8	.0396	-4.0	.0404	15.14	72.09	.272	.344
22	29.2	11.5	10.2	.0445	-3.6	.0454	15.50	71.28	.257	.316
23	32.4	11.8	10.5	.0494	-3.4	.0504	15.90	70.74	.239	.299
24	35.6	12.0	10.8	.0543	-3.1	.0554	16.23	70.11	.225	.277
25	38.5	12.2	11.0	.0592	-2.9	.0604	16.40	69.75	.218	.265
26	45.3	12.4	11.3	.0690	-2.6	.0704	16.74	69.15	.205	.245
27	51.7	12.7	11.4	.0788	-2.4	.0804	17.07	68.92	.193	.234
28	61.3	12.9	11.7	.0934	-2.2	.0954	17.35	68.28	.182	.215
29	71.0	13.0	11.9	.1081	-2.0	.1104	17.60	67.95	.176	.203
30	87.1	13.3	12.1	.1326	-1.8	.1354	17.88	67.47	.169	.186
31	103.1	13.4	12.3	.1571	-1.6	.1604	18.12	67.08	.164	.172
32	135.3	13.7	12.5	.2061	-1.3	.2104	18.42	66.53	.162	.150
33	183.5	14.1	12.8	.2795	-1.0	.2854	19.03	66.02	.146	.127
34	247.8	14.5	13.1	.3774	-.7	.3854	19.54	65.39	.134	.095
35	312.1	14.8	13.3	.4753	-.5	.4854	20.01	65.00	.115	.072
36	376.4	15.2	13.5	.5732	-.4	.5854	20.48	64.69	.088	.052
37	472.8	15.5	13.7	.7201	-.2	.7354	20.95	64.38	.049	.022
38	569.2	15.8	13.8	.8670	-.1	.8854	21.29	64.06	.017	.000
39	730.0	15.9	13.8	1.1118	-.0	1.1354	21.41	63.91	.000	.000
40	777.8	15.9	13.8	1.1847	-.0	1.2098	21.41	63.91	.000	.000

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00426 DELM = .857 REM = 522.0
V RUN = 122271-2 CF/2 = .00376 DELM = .917 REM = 789.0
PLATE = 18 UINF = 20.8 DEL2 = .0572 DEL3 = 1.098
X(IN) = 70.00 GM = 3.542 THETA = .0726 DEL4 = 3.582
K(E06) = -.1870 GAM = -.422 BETA = .057 M = 1.350

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.0	0.0000	0.00	91.96	1.000	1.000
2	4.1	3.8	2.6	.0059	-11.8	.0066	5.00	87.50	.748	.851
3	4.7	4.2	3.0	.0068	-11.4	.0076	5.53	86.62	.722	.822
4	5.4	4.6	3.4	.0077	-10.9	.0086	6.08	85.70	.694	.791
5	6.0	5.0	3.7	.0085	-10.4	.0096	6.55	84.72	.669	.759
6	6.6	5.4	4.0	.0094	-10.0	.0106	7.02	83.99	.647	.731
7	7.2	5.7	4.4	.0103	-9.6	.0116	7.46	83.18	.625	.707
8	7.9	6.0	4.8	.0112	-9.2	.0126	7.92	82.41	.602	.681
9	8.5	6.4	5.0	.0121	-9.0	.0136	8.35	81.85	.580	.663
10	9.1	6.7	5.3	.0130	-8.7	.0146	8.73	81.28	.561	.644
11	9.7	7.0	5.7	.0139	-8.4	.0156	9.12	80.66	.542	.623
12	10.4	7.3	5.9	.0148	-8.1	.0166	9.52	80.15	.521	.606
13	11.0	7.6	6.3	.0157	-7.7	.0176	9.94	79.41	.501	.581
14	11.6	7.9	6.5	.0165	-7.6	.0186	10.31	79.05	.482	.569
15	12.2	8.1	6.7	.0174	-7.3	.0196	10.66	78.52	.464	.551
16	12.9	8.4	6.9	.0183	-7.1	.0206	11.00	78.10	.448	.537
17	13.5	8.6	7.1	.0192	-6.9	.0216	11.29	77.71	.434	.524
18	14.7	9.0	7.6	.0210	-6.4	.0236	11.78	76.70	.410	.490
19	16.0	9.4	8.0	.0228	-6.0	.0256	12.32	75.95	.382	.466
20	17.2	9.8	8.3	.0245	-5.7	.0276	12.88	75.38	.359	.446
21	18.5	10.2	8.6	.0263	-5.4	.0296	13.31	74.79	.334	.426
22	19.7	10.4	8.8	.0281	-5.2	.0316	13.60	74.34	.319	.411
23	21.6	10.7	9.1	.0308	-4.9	.0346	14.01	73.71	.299	.390
24	24.1	11.1	9.6	.0343	-4.4	.0386	14.51	72.81	.275	.360
25	26.6	11.4	9.9	.0379	-4.1	.0426	14.99	72.06	.252	.335
26	29.7	11.7	10.3	.0423	-3.7	.0476	15.33	71.28	.236	.308
27	32.9	11.9	10.7	.0468	-3.3	.0526	15.63	70.50	.223	.282
28	37.2	12.3	10.9	.0530	-3.1	.0596	16.08	70.20	.202	.272
29	42.2	12.6	11.2	.0601	-2.8	.0676	16.44	69.54	.186	.249
30	48.4	12.7	11.4	.0690	-2.6	.0776	16.68	69.06	.176	.232
31	57.8	12.9	11.7	.0823	-2.3	.0926	16.91	68.55	.168	.215
32	70.3	13.1	11.9	.1001	-2.1	.1126	17.19	68.07	.159	.199
33	82.7	13.3	12.2	.1179	-1.9	.1326	17.43	67.62	.152	.183
34	104.6	13.6	12.4	.1490	-1.6	.1676	17.78	67.11	.142	.164
35	126.4	13.8	12.6	.1801	-1.4	.2026	18.02	66.78	.137	.151
36	157.6	14.0	12.8	.2245	-1.2	.2526	18.29	66.35	.133	.134
37	220.0	14.3	13.1	.3134	-.9	.3526	18.76	65.75	.122	.108
38	313.6	14.8	13.4	.4467	-.6	.5026	19.38	65.15	.099	.079
39	438.4	15.3	13.7	.6245	-.3	.7026	20.09	64.54	.057	.043
40	563.2	15.7	13.9	.8022	-.1	.9026	20.57	64.16	.022	.018
41	688.0	15.9	14.0	.9800	-.0	1.1026	20.79	63.97	.002	.000
42	812.8	15.9	14.0	1.1577	-.0	1.3026	20.81	63.91	.000	.000
43	845.5	15.9	14.0	1.2044	-.0	1.3591	20.81	63.91	.000	.000
44	939.1	15.9	14.0	1.3377	-.0	1.5091	20.81	63.91	.000	.000

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00420 DELM = .969 REM = 645.0
V RUN = 122271-2 CF/2 = .00375 DELM = .987 REM = 812.0
PLATE = 21 UINF = 20.4 DEL2 = .0606 DEL3 = 1.177
X(IN) = 82.00 GM = 3.516 THETA = .0763 DEL4 = 4.138
K(E06) = -.1640 GAM = -.373 BETA = .052 M = 1.357

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.2	0.0000	0.00	91.82	1.000	1.000
2	4.4	3.9	2.6	.0060	-11.8	.0072	5.01	87.15	.743	.842
3	5.0	4.3	3.2	.0068	-11.3	.0082	5.91	86.11	.717	.807
4	5.6	4.6	3.5	.0077	-10.8	.0092	5.92	85.11	.696	.773
5	6.2	5.0	3.8	.0085	-10.4	.0102	6.35	84.37	.677	.748
6	6.8	5.3	4.2	.0093	-10.0	.0112	6.83	83.48	.650	.717
7	7.4	5.7	4.6	.0101	-9.6	.0122	7.27	82.86	.628	.696
8	8.1	6.0	4.9	.0110	-9.3	.0132	7.72	82.18	.605	.673
9	8.7	6.4	5.3	.0118	-8.9	.0142	8.18	81.49	.582	.649
10	9.3	6.7	5.5	.0126	-8.7	.0152	8.62	81.05	.559	.634
11	9.9	7.0	5.9	.0134	-8.3	.0162	9.00	80.27	.540	.607
12	10.5	7.3	6.1	.0143	-8.1	.0172	9.35	79.59	.522	.594
13	11.1	7.6	6.3	.0151	-7.9	.0182	9.74	79.47	.502	.580
14	12.3	8.3	6.5	.0168	-7.4	.0202	10.61	78.52	.458	.547
15	13.6	8.7	7.2	.0184	-7.0	.0222	11.20	77.68	.428	.517
16	14.8	9.2	7.6	.0201	-6.6	.0242	11.77	76.94	.399	.492
17	16.0	9.6	8.0	.0217	-6.2	.0262	12.33	76.19	.371	.466
18	17.2	10.0	8.3	.0234	-6.0	.0282	12.77	75.62	.348	.446
19	18.5	10.2	8.6	.0250	-5.7	.0302	13.08	75.03	.332	.425
20	19.7	10.4	8.9	.0267	-5.3	.0322	13.32	74.37	.320	.402
21	20.9	10.6	9.2	.0283	-5.0	.0342	13.58	73.83	.307	.383
22	22.7	10.9	9.5	.0308	-4.7	.0372	13.98	73.17	.288	.360
23	24.6	11.2	9.8	.0333	-4.5	.0402	14.33	72.66	.270	.342
24	27.0	11.5	10.1	.0366	-4.1	.0442	14.73	71.97	.250	.317
25	30.1	11.8	10.5	.0408	-3.7	.0492	15.12	71.13	.230	.286
26	33.1	12.0	10.7	.0449	-3.5	.0542	15.42	70.85	.217	.274
27	37.4	12.3	11.0	.0507	-3.2	.0612	15.73	70.17	.202	.250
28	42.3	12.5	11.3	.0573	-2.9	.0692	16.04	69.69	.187	.232
29	48.4	12.8	11.6	.0656	-2.7	.0792	16.35	69.12	.173	.212
30	57.6	13.0	11.9	.0780	-2.4	.0942	16.68	68.55	.159	.193
31	72.9	13.3	12.2	.0987	-2.0	.1192	16.99	67.86	.148	.170
32	88.2	13.4	12.3	.1194	-1.9	.1442	17.24	67.59	.140	.163
33	118.7	13.7	12.7	.1608	-1.6	.1942	17.60	66.96	.128	.141
34	164.6	14.1	13.0	.2229	-1.2	.2692	18.02	66.36	.118	.120
35	225.8	14.4	13.3	.3057	-1.0	.3692	18.45	65.81	.107	.099
36	302.2	14.7	13.5	.4092	-.7	.4942	18.90	65.27	.093	.072
37	393.9	15.1	13.7	.5334	-.5	.6442	19.38	64.88	.073	.052
38	501.0	15.3	14.0	.6783	-.3	.8192	19.90	64.45	.041	.025
39	608.0	15.8	14.1	.8232	-.1	.9942	20.21	64.18	.015	.008
40	730.3	15.9	14.2	.9888	-.1	1.1942	20.38	64.00	.001	.000
41	852.6	15.9	14.2	1.1543	-.0	1.3942	20.40	63.94	.000	.010

DATE = 122371 (-0.15, -0.004)

T RUN = 122371-1 STNA = .00417 DELH = 1.806 REH = 653.0
V RUN = 122271-2 CF/2 = .00375 DELH = 1.029 REH = 513.0
PLATE = 23 UINF = 19.9 DEL2 = .0627 DEL3 = 1.212
X(IN) = 90.00 GH = 3.959 THETA = .0781 DEL4 = 4.316
K(E06)= -.1600 GAM = -.385 BETA = .050 H = 1.338

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-14.3	0.0000	0.00	92.10
2	4.4	4.1	2.8	.0059	-11.8	.0073	5.88	87.15
3	5.0	4.4	3.1	.0067	-11.3	.0083	5.49	86.17
4	5.6	4.8	3.4	.0075	-10.9	.0093	6.05	85.32
5	6.2	5.3	3.9	.0083	-10.4	.0103	6.58	84.49
6	6.8	5.8	4.3	.0091	-10.0	.0113	7.02	83.72
7	7.3	6.0	4.6	.0099	-9.7	.0123	7.49	83.09
8	7.9	6.4	4.9	.0107	-9.4	.0133	7.98	82.41
9	8.5	6.8	5.3	.0115	-9.0	.0143	8.44	81.70
10	9.1	7.1	5.5	.0123	-8.8	.0153	8.86	81.25
11	9.7	7.4	5.8	.0131	-8.5	.0163	9.23	80.66
12	10.9	7.9	6.4	.0147	-7.9	.0183	9.92	79.62
13	12.1	8.4	6.7	.0163	-7.6	.0203	10.50	78.84
14	13.3	8.8	7.2	.0179	-7.1	.0223	11.01	77.92
15	14.5	9.2	7.6	.0195	-6.7	.0243	11.52	77.09
16	15.7	9.5	8.0	.0211	-6.3	.0263	11.88	76.34
17	16.9	9.7	8.3	.0227	-6.0	.0283	12.19	75.80
18	18.1	10.1	8.6	.0244	-5.7	.0303	12.66	75.18
19	19.3	10.4	8.9	.0260	-5.4	.0323	12.99	74.52
20	21.1	10.8	9.3	.0294	-5.0	.0393	13.45	73.83
21	22.8	11.1	9.6	.0308	-4.7	.0283	13.88	73.26
22	25.2	11.4	10.0	.0340	-4.3	.0423	14.24	72.51
23	27.6	11.6	10.3	.0372	-4.0	.0463	14.56	71.88
24	30.6	11.8	10.6	.0412	-3.7	.0513	14.82	71.34
25	33.6	12.1	10.8	.0452	-3.4	.0563	15.11	70.77
26	36.6	12.3	11.0	.0493	-3.2	.0613	15.17	70.38
27	41.3	12.5	11.3	.0557	-3.0	.0693	15.62	69.87
28	47.7	12.7	11.6	.0617	-2.8	.0793	15.94	69.21
29	53.3	13.0	11.9	.0718	-2.6	.0893	16.21	68.73
30	62.2	13.1	12.1	.0838	-2.2	.1043	16.45	68.24
31	77.1	13.3	12.3	.1039	-2.0	.1293	16.68	67.96
32	98.0	13.5	12.6	.1320	-1.7	.1643	16.92	67.35
33	127.8	13.8	12.8	.1722	-1.4	.2143	17.31	66.94
34	172.5	14.1	13.1	.2325	-1.2	.2893	17.66	66.30
35	232.1	14.4	13.4	.3128	-.9	.3892	18.04	65.79
36	321.5	14.8	13.7	.4333	-.6	.5793	18.56	65.24
37	425.6	15.2	13.9	.5739	-.4	.7143	19.06	64.76
38	530.2	15.6	14.1	.7145	-.2	.8893	19.47	64.39
39	649.4	15.8	14.2	.8752	-.1	1.0893	19.75	64.15
40	768.6	15.9	14.3	1.0359	-.0	1.2893	19.90	64.00
41	887.9	15.9	14.3	1.1966	.0	1.4893	19.91	63.97
42	960.7	15.9	14.3	1.2948	.0	1.6115	19.91	63.97

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00499 DELH = .155 REH = 150.0
V RUN = 10372-1 CF/2 = .00293 DELH = .298 REH = 518.0
PLATE = 1 UINF = 29.2 DEL2 = .0058 DEL3 = .271
X(IN) = 2.00 GH = 4.295 THETA = .0336 DEL4 = .949
K(E06)= -.4330 GAM = -.408 BETA = .119 H = 1.550

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T
1	.0	0.0	.0	0.0000	-10.6	0.0000	0.00	91.93
2	3.7	4.0	2.6	.0210	-8.0	.0048	6.44	85.17
3	4.5	4.5	3.1	.0255	-7.5	.0058	7.40	83.57
4	5.3	5.1	3.7	.0299	-6.9	.0068	8.38	82.03
5	6.1	5.7	4.2	.0343	-6.4	.0079	9.26	80.69
6	6.9	6.2	4.6	.0387	-5.9	.0089	10.05	79.53
7	7.6	6.6	5.0	.0431	-5.6	.0099	10.91	78.46
8	8.4	7.1	5.4	.0475	-5.2	.0109	11.55	77.44
9	9.2	7.5	5.7	.0519	-4.9	.0119	12.25	76.70
10	10.0	7.9	6.0	.0563	-4.6	.0128	12.89	75.89
11	10.8	8.2	6.2	.0607	-4.3	.0138	13.42	75.14
12	11.6	8.5	6.5	.0651	-4.1	.0148	13.89	74.46
13	12.3	8.8	6.7	.0695	-3.9	.0159	14.36	73.86
14	13.1	9.1	6.9	.0739	-3.6	.0168	14.81	73.26
15	14.7	9.5	7.3	.0828	-3.2	.0188	15.53	72.24
16	16.2	9.9	7.6	.0916	-3.0	.0208	16.17	71.52
17	17.8	10.3	7.8	.1004	-2.7	.0228	16.84	70.93
18	19.4	10.7	8.1	.1092	-2.5	.0248	17.46	70.29
19	20.9	11.0	8.3	.1180	-2.3	.0268	17.99	69.66
20	22.5	11.3	8.4	.1268	-2.1	.0288	18.36	69.27
21	24.8	11.6	8.7	.1401	-1.9	.0318	18.86	68.64
22	27.2	11.9	8.8	.1533	-1.7	.0348	19.37	68.19
23	30.3	12.2	9.0	.1709	-1.5	.0388	19.83	67.61
24	34.2	12.5	9.3	.1930	-1.3	.0438	20.20	66.99
25	38.1	12.7	9.4	.2150	-1.1	.0488	20.74	66.62
26	42.0	13.0	9.6	.2370	-1.0	.0538	21.18	66.23
27	47.5	13.3	9.7	.2679	-.9	.0608	21.68	65.82
28	53.7	13.6	9.9	.3031	-.7	.0688	22.15	65.44
29	61.5	13.9	10.0	.3472	-.6	.0788	22.68	65.02
30	73.2	14.4	10.2	.4133	-.4	.0938	23.42	64.56
31	88.8	14.9	10.3	.5015	-.3	.1138	24.26	64.23
32	109.3	15.5	10.4	.6117	-.1	.1388	25.25	63.89
33	127.9	16.1	10.5	.7219	-.1	.1638	26.20	63.71
34	147.4	16.6	10.5	.8321	-.0	.1888	26.96	63.62
35	186.4	17.3	10.6	1.0525	.0	.2388	28.19	63.49
36	225.4	17.8	10.6	1.2729	.0	.2888	28.95	63.49
37	244.6	17.9	10.6	1.3814	.0	.3134	29.19	63.49
38	279.8	18.0	10.6	1.5797	.0	.3584	29.30	63.49
39	336.3	18.0	10.6	1.9103	.0	.4334	29.33	63.49
40	396.9	18.0	10.6	2.2409	.0	.5084	29.33	63.48

DATE = 011072 (-0.15, -0.031, -0.17)

T RUN = 11072-1 STNA = .03348 DELH = .405 REH = 459.0
V RUN = 10372-1 CF/2 = .00238 DELH = .468 REH = 639.0
PLATE = 3 UINF = 26.8 DEL2 = .0326 DEL3 = .760
X(IN) = 10.00 GH = 4.422 THETA = .0565 DEL4 = 1.360
K(E06)= -.8210 GAM = -1.243 BETA = .449 H = 1.554

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.7	0.0000	0.00	91.82	1.000	1.000
2	4.0	4.3	2.7	.0079	-11.1	.0061	5.77	86.65	.951	.954
3	4.6	4.7	3.2	.0092	-10.6	.0071	6.36	85.46	.941	.943
4	5.2	5.2	3.6	.0104	-10.1	.0081	6.98	84.43	.944	.933
5	5.9	5.5	4.1	.0117	-9.6	.0091	7.35	83.39	.943	.923
6	6.5	5.9	4.5	.0130	-9.1	.0101	7.88	82.47	.940	.914
7	7.2	6.3	4.9	.0143	-8.8	.0111	8.49	81.70	.936	.907
8	7.8	6.7	5.3	.0156	-8.3	.0121	9.04	80.84	.932	.898
9	8.5	7.1	5.6	.0168	-8.1	.0131	9.55	80.27	.929	.893
10	9.1	7.4	6.0	.0181	-7.7	.0141	9.99	79.50	.926	.885
11	9.7	7.7	6.2	.0194	-7.4	.0151	10.39	78.96	.924	.879
12	10.4	8.0	6.5	.0207	-7.2	.0161	10.78	78.46	.922	.874
13	11.7	8.6	6.9	.0233	-6.8	.0181	11.54	77.59	.918	.865
14	13.0	9.2	7.3	.0259	-6.3	.0201	12.25	76.67	.915	.855
15	14.2	9.6	7.7	.0284	-6.0	.0221	12.85	76.01	.912	.848
16	15.5	9.9	8.0	.0310	-5.6	.0241	13.27	75.29	.912	.839
17	16.8	10.3	8.3	.0335	-5.4	.0261	13.79	74.79	.909	.834
18	18.1	10.6	8.5	.0361	-5.2	.0281	14.22	74.34	.908	.828
19	20.0	10.9	8.8	.0399	-4.9	.0311	14.62	73.71	.908	.820
20	22.0	11.2	9.0	.0438	-4.7	.0341	15.05	73.26	.909	.814
21	23.9	11.5	9.3	.0476	-4.4	.0371	15.45	72.69	.907	.805
22	26.5	11.8	9.5	.0528	-4.2	.0411	15.84	72.30	.907	.799
23	29.1	12.0	9.7	.0579	-4.0	.0451	16.15	71.82	.906	.790
24	32.9	12.4	10.0	.0656	-3.6	.0511	16.64	71.16	.909	.775
25	38.1	12.8	10.3	.0758	-3.4	.0591	17.15	70.49	.908	.760
26	44.5	13.1	10.6	.0887	-3.1	.0691	17.62	70.05	.907	.742
27	54.2	13.6	10.9	.1079	-2.8	.0841	18.30	69.33	.902	.709
28	63.8	14.0	11.2	.1271	-2.4	.0991	18.83	68.67	.892	.671
29	79.9	14.6	11.6	.1592	-2.1	.1241	19.64	67.88	.868	.612
30	96.0	15.2	12.0	.1913	-1.7	.1491	20.37	67.19	.829	.544
31	118.5	15.9	12.3	.2361	-1.3	.1841	21.37	66.38	.762	.458
32	144.3	16.7	12.7	.2874	-1.0	.2241	22.41	65.62	.667	.355
33	176.4	17.5	13.0	.3516	-.6	.2741	23.55	64.92	.535	.240
34	208.6	18.3	13.3	.4157	-.4	.3241	24.57	64.44	.408	.148
35	240.8	19.0	13.5	.4798	-.2	.3741	25.50	64.04	.309	.084
36	289.1	19.7	13.6	.5760	-.1	.4491	26.40	63.77	.191	.000
37	353.4	20.0	13.7	.7042	-.0	.5491	26.79	63.65	.058	.000
38	417.8	20.0	13.7	.8325	-.0	.6491	26.81	63.65	.000	.000
39	436.0	20.0	13.7	.8688	-.0	.6774	26.81	63.65	.000	.000

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00302 DELH = .719 REH = 786.0
V RUN = 10372-1 CF/2 = .00204 DELH = .744 REH = 1269.0
PLATE = 6 UINF = 24.4 DEL2 = .0613 DEL3 = 1.447
X(IN) = 22.00 GH = 4.218 THETA = .0991 DEL4 = 6.091
K(E06)= -.4550 GAM = -1.043 BETA = .429 H = 1.553

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.6	0.0000	0.00	91.72	1.000	1.000
2	3.5	3.7	2.4	.0044	-12.4	.0065	4.13	87.59	.952	.962
3	4.1	4.1	2.5	.0049	-11.9	.0075	4.59	86.65	.948	.954
4	4.6	4.5	3.2	.0057	-11.4	.0085	5.07	85.64	.942	.944
5	5.1	4.9	3.6	.0064	-10.9	.0095	5.58	84.75	.937	.936
6	5.7	5.3	4.0	.0071	-10.6	.0105	5.99	84.04	.933	.929
7	6.2	5.7	4.4	.0077	-10.1	.0115	6.42	83.24	.929	.922
8	6.8	6.1	4.7	.0084	-9.8	.0125	6.85	82.65	.924	.916
9	7.3	6.5	5.0	.0091	-9.5	.0135	7.32	82.09	.919	.911
10	7.9	6.8	5.4	.0098	-9.2	.0145	7.71	81.40	.915	.904
11	8.4	7.1	5.6	.0104	-8.9	.0155	8.03	80.96	.912	.900
12	8.9	7.4	5.9	.0111	-8.7	.0165	8.32	80.51	.910	.896
13	10.0	7.9	6.4	.0125	-8.2	.0185	8.94	79.44	.904	.886
14	11.1	8.4	6.7	.0138	-7.8	.0205	9.49	78.82	.900	.880
15	12.2	8.8	7.2	.0151	-7.4	.0225	9.97	77.95	.896	.871
16	13.3	9.3	7.5	.0165	-7.1	.0245	10.49	77.39	.893	.865
17	14.9	9.9	7.9	.0185	-6.7	.0275	11.16	76.61	.885	.857
18	16.5	10.3	8.2	.0205	-6.3	.0305	11.66	75.92	.885	.850
19	18.2	10.7	8.5	.0226	-6.0	.0335	12.35	75.39	.883	.844
20	20.3	11.1	8.9	.0252	-5.7	.0375	12.80	74.67	.881	.836
21	22.5	11.5	9.2	.0279	-5.4	.0415	13.28	74.10	.881	.829
22	25.8	11.9	9.5	.0320	-5.1	.0475	13.43	73.53	.882	.821
23	29.0	12.2	9.8	.0360	-4.8	.0535	13.80	73.02	.884	.814
24	32.8	12.6	10.0	.0407	-4.6	.0605	14.20	72.54	.886	.807
25	37.2	12.9	10.2	.0461	-4.3	.0685	14.57	72.09	.889	.799
26	42.6	13.2	10.4	.0528	-4.1	.0785	14.94	71.70	.892	.792
27	50.7	13.6	10.6	.0629	-3.8	.0935	15.38	71.07	.898	.776
28	64.2	14.0	11.2	.0798	-3.4	.1185	15.89	70.26	.905	.751
29	77.8	14.6	11.5	.0966	-3.0	.1435	16.51	69.66	.908	.728
30	91.4	15.1	11.7	.1134	-2.8	.1685	17.05	69.21	.905	.706
31	110.4	15.6	12.1	.1370	-2.4	.2035	17.63	68.49	.892	.664
32	132.1	16.1	12.4	.1639	-2.1	.2435	18.25	67.92	.866	.622
33	159.2	16.8	12.8	.1976	-1.8	.2935	19.03	67.25	.819	.582
34	199.9	17.8	13.2	.2481	-1.4	.3685	20.14	66.41	.721	.488
35	240.6	18.7	13.6	.2986	-1.0	.4435	21.17	65.74	.601	.376
36	294.9	19.9	14.0	.3659	-.6	.5435	22.47	64.96	.449	.247
37	362.7	21.0	14.4	.4500	-.2	.6685	23.75	64.23	.308	.101
38	444.1	21.5	14.6	.5510	-.0	.8185	24.37	63.81	.157	.000
39	539.0	21.6	14.6	.6688	-.0	.9935	24.43	63.81	.025	.004
40	574.9	21.6	14.6	.7134	-.0	1.0597	24.43	63.81	.000	.004
41	629.2	21.6	14.6	.7807	-.0	1.1597	24.43	63.81	.000	.004

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00279 DELM = 1.044 REM = 1107.0
V RUN = 10372-1 CF/2 = .00191 DELM = 1.011 REM = 1625.0
PLATE = 9 UINF = 23.0 DEL2 = .0917 DEL3 = 2.164
X(IN) = 34.00 GH = 4.167 THETA = .1346 DEL4 = 9.010
K(E06) = -.3250 GAM = -1.007 BETA = .429 H = 1.524

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.3	0.0000	0.00	91.79	1.000	1.000
2	2.9	2.9	2.0	.0027	-13.5	.0059	3.04	88.62	.961	.971
3	3.4	3.4	2.3	.0031	-13.1	.0069	3.54	87.89	.955	.964
4	3.9	3.9	2.7	.0036	-12.7	.0079	4.02	87.18	.943	.957
5	4.4	4.4	3.0	.0040	-12.3	.0089	4.49	86.38	.941	.950
6	4.9	4.7	3.4	.0045	-11.9	.0099	4.89	85.61	.936	.942
7	5.4	5.1	3.7	.0049	-11.5	.0109	5.26	84.93	.932	.936
8	5.9	5.5	4.1	.0054	-11.2	.0119	5.69	84.34	.926	.930
9	6.4	5.9	4.4	.0058	-10.8	.0129	6.12	83.66	.921	.924
10	6.9	6.4	4.8	.0063	-10.5	.0139	6.57	83.04	.915	.918
11	7.8	7.1	5.3	.0072	-9.9	.0159	7.31	82.03	.906	.908
12	8.8	7.6	5.8	.0081	-9.4	.0179	7.88	81.14	.899	.900
13	9.8	8.3	6.2	.0090	-9.1	.0199	8.57	80.45	.891	.893
14	10.8	8.8	6.7	.0099	-8.6	.0219	9.10	79.50	.885	.884
15	11.8	9.1	7.1	.0108	-8.2	.0239	9.43	78.88	.883	.876
16	12.8	9.5	7.4	.0117	-7.9	.0259	9.79	78.31	.879	.872
17	13.8	9.8	7.6	.0126	-7.7	.0279	10.14	77.89	.876	.868
18	15.3	10.3	8.0	.0139	-7.2	.0309	10.58	77.09	.873	.859
19	16.7	10.6	8.3	.0153	-6.9	.0339	10.95	76.49	.871	.853
20	18.7	11.1	8.7	.0171	-6.6	.0379	11.41	75.83	.869	.846
21	20.7	11.4	9.0	.0189	-6.3	.0419	11.80	75.33	.866	.841
22	23.2	11.8	9.2	.0211	-6.0	.0469	12.17	74.88	.865	.835
23	26.6	12.2	9.7	.0243	-5.6	.0539	12.59	74.10	.866	.825
24	30.6	12.6	9.9	.0279	-5.3	.0619	13.02	73.59	.868	.818
25	35.6	13.0	10.3	.0324	-5.0	.0719	13.37	72.96	.872	.809
26	43.0	13.4	10.6	.0391	-4.7	.0869	13.78	72.36	.879	.798
27	50.4	13.8	10.9	.0459	-4.4	.1019	14.25	71.85	.885	.788
28	60.3	14.2	11.2	.0549	-4.1	.1219	14.61	71.29	.894	.775
29	72.7	14.5	11.5	.0661	-3.7	.1469	14.93	70.69	.905	.758
30	90.0	15.0	11.8	.0819	-3.4	.1819	15.42	70.11	.915	.738
31	107.3	15.4	12.1	.0977	-3.1	.2169	15.91	69.57	.921	.715
32	132.0	16.0	12.5	.1202	-2.8	.2669	16.53	68.97	.921	.685
33	169.1	16.8	12.9	.1539	-2.4	.3419	17.36	68.16	.901	.631
34	218.6	17.9	13.4	.1990	-1.9	.4419	18.43	67.26	.838	.562
35	268.1	18.8	13.9	.2440	-1.4	.5419	19.39	66.41	.734	.460
36	329.9	20.0	14.3	.3003	-1.0	.6669	20.63	65.67	.569	.357
37	391.8	21.0	14.7	.3565	-.6	.7919	21.61	64.93	.382	.244
38	466.0	21.8	15.0	.4241	-.3	.9419	22.51	64.35	.203	.130
39	565.0	22.3	15.2	.5141	-.1	1.1419	23.01	63.90	.050	.022
40	663.9	22.3	15.3	.6041	-.0	1.3419	23.02	63.84	.000	.000
41	678.1	22.3	15.3	.6170	-.0	1.3705	23.04	63.84	.000	.000

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00264 DELM = 1.303 REM = 1359.0
V RUN = 10372-1 CF/2 = .00182 DELM = 1.280 REM = 1971.0
PLATE = 12 UINF = 22.0 DEL2 = .1174 DEL3 = 2.837
X(IN) = 46.00 GH = 4.193 THETA = .1703 DEL4 = 11.893
K(E06) = -.2560 GAM = -.966 BETA = .430 H = 1.522

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.7	0.0000	0.00	91.89	1.000	1.000
2	2.6	3.1	1.8	.0019	-14.0	.0057	2.95	88.71	.958	.970
3	3.1	3.3	2.2	.0023	-13.7	.0067	3.44	88.18	.956	.965
4	3.6	3.6	2.5	.0026	-13.3	.0077	3.67	87.62	.951	.959
5	4.0	3.9	2.8	.0029	-13.0	.0087	3.73	86.97	.949	.953
6	4.5	4.2	3.2	.0033	-12.5	.0097	4.02	86.28	.945	.946
7	5.0	4.5	3.5	.0036	-12.2	.0107	4.34	85.58	.940	.940
8	5.4	4.8	3.9	.0040	-11.9	.0117	4.66	84.93	.936	.934
9	5.9	5.2	4.2	.0043	-11.5	.0127	4.98	84.40	.932	.928
10	6.3	5.5	4.5	.0047	-11.2	.0137	5.30	83.84	.928	.923
11	6.9	5.8	4.8	.0050	-11.0	.0147	5.61	83.[illegible]	.924	.918
12	7.3	6.1	5.1	.0053	-10.6	.0157	5.92	82.80	.919	.913
13	8.2	6.8	5.6	.0060	-10.1	.0177	6.55	81.91	.911	.904
14	9.1	7.4	6.0	.0067	-9.7	.0197	7.12	81.17	.903	.897
15	10.0	7.9	6.5	.0074	-9.3	.0217	7.64	80.36	.897	.889
16	11.0	8.5	6.8	.0081	-9.0	.0237	8.14	79.83	.890	.884
17	11.9	9.0	7.1	.0088	-8.6	.0257	8.62	79.14	.884	.877
18	12.8	9.4	7.5	.0095	-8.3	.0277	9.05	78.61	.879	.872
19	13.7	9.7	7.7	.0102	-8.1	.0297	9.33	78.19	877	.867
20	15.1	10.1	8.2	.0112	-7.6	.0327	9.69	77.36	.874	.859
21	16.5	10.4	8.4	.0122	-7.4	.0357	9.99	76.94	.872	.855
22	17.9	10.7	8.6	.0132	-7.1	.0387	10.31	76.55	.870	.850
23	19.7	11.1	8.9	.0146	-6.8	.0427	10.71	75.95	.867	.844
24	22.0	11.6	9.4	.0163	-6.4	.0477	11.14	75.21	.864	.835
25	25.3	12.1	9.5	.0187	-6.2	.0547	11.61	75.00	.863	.834
26	29.0	12.4	9.9	.0215	-5.9	.0627	11.95	74.34	.864	.826
27	33.6	12.8	10.2	.0249	-5.5	.0727	12.37	73.62	.866	.816
28	40.5	13.3	10.6	.0301	-5.1	.0877	12.82	72.96	.872	.806
29	47.5	13.6	10.9	.0352	-4.9	.1027	13.10	72.52	.879	.798
30	54.4	13.8	11.1	.0404	-4.7	.1177	13.34	72.19	.886	.792
31	65.9	14.2	11.4	.0490	-4.3	.1427	13.72	71.53	.898	.777
32	82.1	14.8	11.8	.0610	-4.0	.1777	14.27	70.87	.913	.759
33	100.6	15.3	12.1	.0747	-3.7	.2177	14.72	70.39	.928	.743
34	123.7	15.7	12.5	.0919	-3.3	.2677	15.16	69.67	.940	.713
35	158.3	16.4	12.9	.1176	-2.9	.3427	15.80	68.97	.948	.677
36	204.5	17.2	13.3	.1520	-2.5	.4427	16.68	68.19	.951	.628
37	273.9	18.6	13.9	.2035	-1.9	.5927	17.91	67.11	.955	.536
38	366.2	20.1	14.6	.2722	-1.2	.7927	19.35	65.93	.954	.395
39	458.6	21.4	15.1	.3409	-.7	.9927	20.63	65.05	.940	.252
40	551.0	22.4	15.5	.4095	-.3	1.1927	21.56	64.36	.184	.117
41	643.4	22.8	15.7	.4782	-.1	1.3927	21.96	63.93	.052	.020
42	735.8	22.8	15.7	.5469	-.0	1.5927	22.01	63.84	.000	.000
43	786.3	22.8	15.7	.5845	-.0	1.7021	22.01	63.84	.000	.002

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00253 DELM = 1.551 REM = 1586.0
V RUN = 10372-1 CF/2 = .00176 DELM = 1.524 REM = 2256.0
PLATE = 15 UINF = 21.4 DEL2 = .1411 DEL3 = 3.437
X(IN) = 58.00 GH = 4.178 THETA = .2007 DEL4 = 14.357
K(E06) = -.2120 GAM = -.951 BETA = .421 H = 1.503

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.2	0.0000	0.00	91.79	1.000	1.000
2	2.8	3.2	1.9	.0017	-14.5	.0062	2.92	88.95	.956	.973
3	3.2	3.4	2.2	.0020	-14.2	.0072	3.15	88.36	.953	.967
4	3.6	3.7	2.5	.0023	-13.8	.0082	3.39	87.80	.950	.961
5	4.1	4.0	2.9	.0026	-13.4	.0092	3.73	87.06	.946	.954
6	4.5	4.4	3.2	.0029	-13.0	.0102	4.08	86.32	.941	.947
7	5.0	4.8	3.5	.0031	-12.7	.0112	4.40	85.82	.936	.942
8	5.4	5.1	3.8	.0034	-12.3	.0122	4.72	85.14	.932	.935
9	5.8	5.5	4.1	.0037	-12.1	.0132	5.08	84.73	.926	.931
10	6.3	5.9	4.5	.0040	-11.7	.0142	5.41	84.10	.921	.925
11	6.7	6.2	4.7	.0043	-11.5	.0152	5.78	83.69	.917	.921
12	7.6	6.6	5.2	.0048	-10.9	.0172	6.06	82.80	.913	.912
13	8.5	7.1	5.7	.0054	-10.5	.0192	6.52	81.97	.907	.904
14	9.4	7.7	6.1	.0060	-10.0	.0212	7.07	81.20	.899	.896
15	10.7	8.4	6.7	.0068	-9.5	.0242	7.77	80.28	.889	.886
16	12.0	9.2	7.2	.0077	-9.0	.0272	8.51	79.41	.879	.877
17	13.4	9.7	7.6	.0085	-8.6	.0302	8.91	78.73	.875	.870
18	14.7	10.1	8.0	.0094	-8.1	.0332	9.29	77.98	.871	.862
19	16.9	10.8	8.5	.0108	-7.7	.0382	9.91	77.12	.864	.852
20	19.1	11.2	8.8	.0122	-7.3	.0432	10.33	76.58	.861	.846
21	22.2	11.7	9.4	.0142	-6.8	.0502	10.75	75.66	.860	.836
22	25.7	12.4	9.7	.0165	-6.4	.0582	11.39	74.97	.855	.827
23	30.2	12.6	10.2	.0193	-6.0	.0682	11.65	74.19	.855	.817
24	36.8	13.3	10.6	.0236	-5.6	.0832	12.28	73.56	.859	.809
25	47.8	14.0	11.0	.0306	-5.1	.1082	12.87	72.79	.867	.796
26	58.9	14.3	11.3	.0377	-4.8	.1332	13.16	72.22	.879	.785
27	74.3	14.7	11.8	.0477	-4.4	.1682	13.58	71.47	.894	.769
28	92.0	15.2	12.1	.0590	-4.1	.2082	13.99	70.93	.909	.753
29	114.1	15.7	12.4	.0732	-3.7	.2582	14.46	70.36	.926	.734
30	147.3	16.3	12.9	.0944	-3.3	.3332	15.06	69.64	.947	.703
31	213.6	17.4	13.5	.1370	-2.6	.4832	16.02	68.43	.962	.632
32	302.0	18.8	14.2	.1937	-1.9	.6832	17.35	67.26	.903	.539
33	390.3	20.1	14.8	.2504	-1.4	.8832	18.53	66.29	.762	.432
34	478.7	21.3	15.2	.3071	-.9	1.0832	19.61	65.51	.564	.319
35	567.1	22.3	15.7	.3638	-.5	1.2832	20.52	64.78	.344	.187
36	655.5	22.9	15.9	.4205	-.2	1.4832	21.14	64.30	.165	.085
37	743.9	23.2	16.1	.4772	-.0	1.6832	21.37	63.97	.052	.027
38	832.3	23.2	16.2	.5340	-.0	1.8832	21.48	63.91	.002	.000
39	840.1	23.2	16.2	.5390	-.0	1.9008	21.48	63.91	.028	.001

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00245 DELM = 1.935 REM = 1534.0
V RUN = 10372-1 CF/2 = .00171 DELM = 1.784 REM = 2540.0
PLATE = 18 UINF = 20.9 DEL2 = .1674 DEL3 = 4.108
X(IN) = 70.70 GH = 4.183 THETA = .2319 DEL4 = 17.186
K(E06) = -.1800 GAM = -.918 BETA = .415 H = 1.498

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.4	0.0000	0.00	91.82	1.000	1.000
2	2.6	3.3	1.8	.0015	-14.9	.0062	2.99	89.13	.955	.974
3	3.0	3.6	2.1	.0017	-14.5	.0072	3.19	88.54	.951	.969
4	3.5	3.9	2.4	.0020	-14.2	.0082	3.45	88.03	.947	.963
5	3.9	4.2	2.7	.0022	-13.8	.0092	3.72	87.36	.943	.957
6	4.3	4.5	3.0	.0024	-13.4	.0102	3.99	86.74	.939	.951
7	4.7	4.8	3.3	.0027	-13.1	.0112	4.23	86.17	.935	.945
8	5.2	5.0	3.7	.0029	-12.7	.0122	4.47	85.49	.932	.938
9	5.6	5.3	4.0	.0031	-12.4	.0132	4.72	85.05	.929	.934
10	6.0	5.6	4.3	.0034	-12.1	.0142	4.98	84.49	.926	.929
11	6.9	6.2	4.9	.0039	-11.5	.0162	5.47	83.54	.918	.919
12	7.7	6.7	5.3	.0043	-11.2	.0182	5.96	82.89	.911	.913
13	8.6	7.4	5.7	.0048	-10.7	.0202	6.54	82.12	.902	.905
14	9.4	8.0	6.1	.0053	-10.3	.0222	7.07	81.43	.894	.899
15	10.3	8.4	6.4	.0058	-10.1	.0242	7.49	81.02	.889	.895
16	11.6	9.0	7.0	.0065	-9.4	.0272	7.94	79.92	.883	.883
17	12.8	9.4	7.4	.0072	-9.0	.0302	8.35	79.23	.878	.876
18	14.1	9.9	7.9	.0079	-8.6	.0332	8.82	78.49	.871	.869
19	15.4	10.3	8.0	.0086	-8.4	.0362	9.14	78.28	.869	.867
20	17.1	10.6	8.5	.0095	-8.0	.0402	9.44	77.48	.865	.859
21	18.8	11.1	8.8	.0105	-7.7	.0442	9.84	76.97	.862	.853
22	20.9	11.6	9.2	.0117	-7.3	.0492	10.26	76.28	.858	.846
23	23.0	11.9	9.6	.0129	-6.9	.0542	10.55	75.63	.856	.839
24	25.6	12.2	9.7	.0143	-6.7	.0602	10.82	75.36	.856	.836
25	29.0	12.5	10.0	.0162	-6.4	.0682	11.12	74.82	.856	.829
26	33.2	13.0	10.3	.0186	-6.1	.0782	11.55	74.31	.856	.823
27	39.6	13.5	10.7	.0221	-5.8	.0932	11.95	73.74	.857	.815
28	50.3	13.8	11.1	.0280	-5.3	.1182	12.27	73.03	.863	.804
29	63.0	14.4	11.5	.0352	-5.0	.1482	12.61	72.40	.869	.793
30	77.9	14.9	11.9	.0435	-4.6	.1832	13.22	71.71	.880	.779
31	94.9	15.3	12.1	.0529	-4.3	.2232	13.55	71.26	.893	.769
32	116.2	15.7	12.5	.0648	-3.9	.2732	13.92	70.69	.908	.752
33	158.7	16.6	13.0	.0885	-3.5	.3732	14.70	69.86	.927	.721
34	211.9	17.4	13.5	.1182	-2.9	.4982	15.43	68.95	.937	.672
35	297.0	18.5	14.1	.1658	-2.3	.6982	16.44	67.86	.904	.594
36	382.1	19.8	14.7	.2133	-1.7	.8982	17.56	66.90	.825	.501
37	509.7	21.3	15.4	.2842	-1.0	1.1982	18.93	65.78	.686	.357
38	637.3	22.6	15.9	.3554	-.5	1.4982	20.03	64.93	.286	.213
39	807.4	23.5	16.4	.4502	-.1	1.8982	20.84	64.12	.040	.030
40	977.6	23.6	16.4	.5451	.0	2.2982	20.91	63.97	.000	.000

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00238 DELM = 2.102 REM = 2063.0
V RUN = 10372-1 CF/2 = .00167 DELM = 1.977 REM = 2766.0
PLATE = 21 UINF = 20.4 DEL2 = .1929 DEL3 = 4.745
X(IN) = 82.00 GM = 4.181 THETA = .2565 DEL4 = 19.841
K(E06) = -.1560 GAM = -.987 BETA = .401 M = 1.486

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.7	0.0000	0.00	91.75	1.000	1.000
2	2.7	2.8	1.9	.0014	-14.9	.0066	2.37	88.80	.961	.971
3	3.1	3.2	2.2	.0016	-14.7	.0076	2.72	88.33	.956	.966
4	3.5	3.6	2.4	.0018	-14.3	.0086	3.06	87.77	.950	.961
5	3.9	4.0	2.8	.0020	-13.9	.0096	3.39	87.15	.946	.955
6	4.4	4.3	3.1	.0022	-13.7	.0106	3.71	86.68	.941	.950
7	4.8	4.7	3.4	.0024	-13.3	.0116	4.02	86.14	.936	.945
8	5.6	5.4	4.1	.0028	-12.7	.0136	4.61	85.02	.927	.934
9	6.4	6.0	4.6	.0032	-12.1	.0156	5.14	84.16	.919	.925
10	7.2	6.6	5.0	.0036	-11.7	.0176	5.65	83.49	.910	.918
11	8.0	7.4	5.5	.0041	-11.2	.0196	6.29	82.62	.900	.910
12	9.3	8.1	6.1	.0047	-10.6	.0226	6.90	81.70	.890	.901
13	10.5	8.5	6.6	.0053	-10.1	.0256	7.28	80.78	.885	.892
14	11.7	9.1	7.0	.0059	-9.7	.0286	7.77	80.13	.878	.886
15	13.0	9.6	7.6	.0065	-9.2	.0316	8.25	79.23	.872	.876
16	14.2	10.1	7.8	.0071	-8.9	.0346	8.67	78.79	.866	.872
17	15.8	10.6	8.4	.0080	-8.3	.0386	9.11	77.89	.861	.863
18	17.5	11.0	8.7	.0088	-8.1	.0426	9.45	77.42	.857	.858
19	19.1	11.4	9.0	.0096	-7.7	.0466	9.74	76.82	.854	.851
20	22.0	12.0	9.5	.0110	-7.3	.0536	10.24	76.10	.849	.843
21	25.3	12.5	9.9	.0127	-6.9	.0616	10.71	75.51	.844	.836
22	29.4	13.0	10.2	.0147	-6.6	.0716	11.14	74.94	.841	.829
23	35.5	13.4	10.6	.0178	-6.1	.0866	11.47	74.13	.841	.819
24	45.8	13.8	11.0	.0230	-5.7	.1116	11.78	73.56	.844	.810
25	58.1	14.4	11.5	.0291	-5.2	.1416	12.29	72.73	.848	.798
26	72.5	14.9	11.8	.0363	-4.9	.1766	12.74	72.19	.850	.789
27	88.9	15.4	12.2	.0445	-4.5	.2166	13.13	71.53	.856	.774
28	109.4	15.8	12.5	.0548	-4.2	.2666	13.50	71.11	.862	.762
29	140.2	16.2	12.9	.0702	-3.8	.3416	13.90	70.49	.872	.743
30	181.2	16.9	13.3	.0907	-3.5	.4416	14.48	69.82	.885	.721
31	242.7	17.8	13.9	.1215	-2.9	.5916	15.24	68.89	.885	.679
32	324.8	19.0	14.4	.1626	-2.3	.7916	16.22	67.89	.863	.612
33	427.4	20.3	15.0	.2140	-1.7	1.0416	17.32	66.96	.773	.521
34	529.9	21.3	15.5	.2653	-1.2	1.2916	18.20	66.11	.635	.411
35	653.0	22.6	16.0	.3269	-.7	1.5916	19.33	65.27	.406	.272
36	776.1	23.5	16.4	.3885	-.3	1.8916	20.07	64.63	.181	.153
37	899.2	23.8	16.6	.4502	-.1	2.1916	20.39	64.21	.042	.055
38	1022.3	23.9	16.7	.5118	.0	2.4916	20.42	64.06	.000	.000
39	1145.4	23.9	16.7	.5734	.0	2.7916	20.42	64.06	.000	.000

DATE = 011072 (-0.15, -0.001, -0.17)

T RUN = 11072-1 STNA = .00234 DELM = 2.264 REM = 2215.0
V RUN = 10372-1 CF/2 = .00164 DELM = 2.120 REM = 2928.0
PLATE = 23 UINF = 20.0 DEL2 = .2106 DEL3 = 5.191
X(IN) = 90.00 GM = 4.167 THETA = .2781 DEL4 = 21.629
K(E06) = -.1480 GAM = -.893 BETA = .409 M = 1.485

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T
1	.0	0.0	.0	0.0000	-16.9	0.0000	0.00	91.86
2	2.9	3.4	2.0	.0014	-15.0	.0074	2.81	88.80
3	3.3	3.6	2.3	.0015	-14.7	.0084	3.02	88.33
4	3.7	3.9	2.5	.0017	-14.4	.0094	3.26	87.74
5	4.1	4.2	3.0	.0019	-13.9	.0104	3.52	87.00
6	4.5	4.5	3.3	.0021	-13.6	.0114	3.76	86.47
7	4.9	4.8	3.6	.0023	-13.3	.0124	4.01	86.30
8	5.7	5.5	4.1	.0027	-12.7	.0144	4.53	85.05
9	6.5	6.1	4.6	.0030	-12.2	.0164	5.10	84.25
10	7.3	6.7	5.2	.0034	-11.7	.0184	5.57	83.36
11	8.1	7.2	5.6	.0038	-11.3	.0204	6.00	82.65
12	8.9	7.8	5.9	.0042	-10.9	.0224	6.47	82.09
13	9.7	8.2	6.4	.0045	-10.5	.0244	6.85	81.37
14	10.9	8.7	6.9	.0051	-9.9	.0274	7.22	80.48
15	12.1	9.3	7.4	.0057	-9.5	.0304	7.76	79.74
16	13.3	9.9	7.7	.0062	-9.2	.0334	8.20	79.20
17	14.9	10.4	8.2	.0070	-8.7	.0374	8.84	78.43
18	16.5	10.8	8.4	.0077	-8.4	.0414	8.99	77.98
19	18.1	11.2	8.8	.0085	-8.0	.0454	9.29	77.38
20	20.1	11.6	9.1	.0094	-7.7	.0504	9.61	76.85
21	23.3	12.1	9.5	.0109	-7.4	.0584	10.03	76.22
22	27.2	12.6	10.0	.0126	-6.9	.0684	10.48	75.45
23	33.2	13.2	10.4	.0156	-6.4	.0834	11.01	74.67
24	43.2	13.5	10.9	.0203	-6.0	.1084	11.22	73.92
25	55.1	14.2	11.4	.0259	-5.4	.1384	11.76	73.03
26	69.1	14.8	11.8	.0325	-5.0	.1734	12.29	72.40
27	85.0	15.2	12.1	.0400	-4.8	.2134	12.61	72.01
28	105.0	15.6	12.5	.0494	-4.4	.2634	12.96	71.35
29	134.9	16.2	12.8	.0635	-4.0	.3384	13.42	70.75
30	174.7	16.9	13.2	.0823	-3.6	.4384	14.05	70.06
31	234.5	17.7	13.8	.1104	-3.1	.5884	14.71	69.16
32	294.3	18.6	14.2	.1386	-2.6	.7384	15.44	68.46
33	354.0	19.3	14.6	.1667	-2.3	.8884	16.04	67.89
34	433.8	20.2	15.0	.2043	-1.8	1.0884	16.82	67.11
35	513.5	21.1	15.4	.2418	-1.5	1.2884	17.55	66.54
36	633.0	22.3	15.9	.2981	-1.0	1.5884	18.51	65.69
37	752.6	23.3	16.4	.3544	-.5	1.8884	19.47	64.94
38	912.0	24.0	16.7	.4295	-.1	2.2884	19.98	64.33
39	1071.4	24.1	16.8	.5046	-.0	2.6884	20.04	64.12
40	1230.8	24.1	16.9	.5797	.0	3.0884	20.04	64.09

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00548 DELM = .160 REM = 147.0
V RUN = 122971-1 CF/2 = .00320 DELM = .296 REM = 509.0
PLATE = 1 UINF = 29.5 DEL2 = .0096 DEL3 = .201
X(IN) = 2.00 GM = 4.032 THETA = .0326 DEL4 = .809
K(E06) = -.4400 GAM = -.418 BETA = .105 M = 1.526

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-10.1	0.0000	0.00	91.79		
2	4.9	4.5	3.2	.0290	-6.8	.0060	7.76	82.74		
3	5.7	5.2	3.8	.0338	-6.2	.0070	8.93	81.05		
4	6.5	5.9	4.3	.0387	-5.8	.0080	10.04	79.71		
5	7.3	6.5	4.7	.0435	-5.4	.0090	11.12	78.64		
6	8.1	7.0	5.1	.0484	-5.0	.0100	11.97	77.53		
7	8.9	7.4	5.4	.0533	-4.6	.0110	12.71	76.58		
8	9.8	7.9	5.7	.0581	-4.4	.0120	13.51	75.77		
9	10.6	8.3	5.9	.0630	-4.1	.0130	14.20	75.11		
10	11.4	8.6	6.2	.0678	-3.8	.0140	14.69	74.31		
11	12.2	8.8	6.4	.0727	-3.6	.0150	15.12	73.71		
12	13.0	9.1	6.6	.0775	-3.4	.0160	15.58	73.14		
13	13.8	9.4	6.8	.0824	-3.2	.0170	16.02	72.60		
14	14.6	9.6	7.0	.0872	-3.0	.0180	16.41	72.09		
15	15.5	9.8	7.1	.0921	-2.9	.0190	16.76	71.67		
16	17.1	10.2	7.5	.1018	-2.6	.0210	17.41	70.77		
17	18.7	10.5	7.7	.1115	-2.3	.0230	17.97	70.14		
18	20.3	10.8	7.9	.1212	-2.1	.0250	18.46	69.54		
19	22.8	11.1	8.2	.1357	-1.9	.0280	19.07	68.79		
20	25.2	11.4	8.4	.1503	-1.7	.0310	19.61	68.21		
21	28.5	11.8	8.6	.1697	-1.4	.0350	20.21	67.58		
22	31.7	12.0	8.8	.1891	-1.3	.0390	20.59	67.07		
23	35.8	12.3	8.9	.2133	-1.1	.0440	21.01	66.65		
24	39.9	12.5	9.1	.2376	-1.0	.0490	21.44	66.25		
25	45.6	12.8	9.2	.2716	-.8	.0560	21.95	65.77		
26	52.1	13.1	9.4	.3104	-.7	.0640	22.44	65.41		
27	60.2	13.4	9.5	.3589	-.5	.0740	22.96	65.02		
28	72.4	13.8	9.7	.4316	-.4	.0890	23.68	64.62		
29	84.7	14.3	9.8	.5257	-.3	.1090	24.52	64.23		
30	105.0	14.8	9.9	.6257	-.2	.1290	25.29	63.98		
31	133.4	15.5	10.0	.7955	-.1	.1640	26.50	63.74		
32	174.1	16.3	10.0	1.0380	-.0	.2140	27.92	63.58		
33	214.8	16.9	10.0	1.2806	-.0	.2640	28.89	63.52		
34	275.8	17.2	10.1	1.6444	.0	.3390	29.45	63.44		
35	289.1	17.2	10.1	1.7236	.0	.3553	29.48	63.44		
36	329.8	17.2	10.1	1.9662	.0	.4053	29.50	63.44		
37	411.1	17.2	10.1	2.4513	.0	.5053	29.50	63.44		

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00384 DELM = .376 REM = 357.0
V RUN = 122971-1 CF/2 = .00275 DELM = .447 REM = 739.0
PLATE = 3 UINF = 26.9 DEL2 = .0276 DEL3 = .624
X(IN) = 10.00 GM = 4.329 THETA = .0526 DEL4 = 2.703
K(E06) = -.8260 GAM = -1.162 BETA = .338 M = 1.524

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.2	0.0000	0.00	91.79	1.000	1.000
2	4.6	4.5	3.2	.0183	-10.5	.0066	6.46	85.79	.950	.907
3	5.2	4.9	3.5	.0119	-9.8	.0076	7.07	84.37	.869	.879
4	5.9	5.4	4.1	.0134	-9.2	.0086	7.76	83.18	.857	.859
5	6.6	5.8	4.5	.0150	-8.8	.0096	8.42	82.20	.844	.843
6	7.3	6.2	4.9	.0166	-8.3	.0106	9.02	81.31	.834	.828
7	8.0	6.6	5.3	.0181	-8.0	.0116	9.63	80.49	.827	.813
8	8.7	7.1	5.7	.0197	-7.6	.0126	10.27	79.77	.811	.801
9	9.4	7.5	6.1	.0212	-7.2	.0136	10.82	79.05	.801	.789
10	10.1	7.7	6.3	.0228	-7.0	.0146	11.21	78.46	.794	.778
11	10.8	8.0	6.6	.0244	-6.7	.0156	11.62	77.89	.787	.769
12	11.4	8.4	6.9	.0259	-6.4	.0166	12.13	77.24	.778	.757
13	12.1	8.7	7.0	.0275	-6.2	.0176	12.61	76.94	.770	.752
14	12.8	9.0	7.2	.0290	-6.1	.0186	12.99	76.46	.763	.743
15	13.5	9.2	7.5	.0306	-5.8	.0196	13.34	75.95	.757	.733
16	14.9	9.7	7.6	.0337	-5.5	.0216	13.99	75.20	.747	.720
17	16.3	10.1	8.2	.0368	-5.1	.0236	14.56	74.49	.739	.706
18	17.6	10.3	8.4	.0399	-4.9	.0256	14.98	73.92	.737	.695
19	19.0	10.6	8.7	.0431	-4.6	.0276	15.37	73.35	.727	.684
20	21.1	11.0	9.0	.0477	-4.2	.0306	15.94	72.51	.719	.674
21	23.1	11.3	9.2	.0524	-4.1	.0336	16.35	72.24	.714	.661
22	25.9	11.6	9.5	.0587	-3.8	.0376	16.78	71.61	.710	.647
23	28.6	11.9	9.8	.0649	-3.5	.0416	17.20	71.10	.706	.635
24	31.4	12.1	10.0	.0711	-3.3	.0456	17.59	70.71	.702	.625
25	34.2	12.4	10.1	.0774	-3.2	.0496	17.91	70.32	.700	.614
26	37.6	12.6	10.3	.0852	-3.0	.0546	18.26	69.90	.698	.601
27	44.5	12.9	10.7	.1008	-2.6	.0646	18.69	69.21	.695	.576
28	54.8	13.4	11.0	.1242	-2.3	.0796	19.37	68.45	.688	.541
29	68.6	13.8	11.4	.1554	-2.0	.0996	20.04	67.76	.677	.500
30	85.8	14.3	11.7	.1943	-1.6	.1246	20.74	67.01	.658	.443
31	103.0	14.8	12.0	.2333	-1.3	.1496	21.42	66.35	.625	.386
32	137.4	15.7	12.5	.3113	-.9	.1996	22.67	65.44	.590	.286
33	171.9	16.4	12.8	.3893	-.5	.2496	23.79	64.77	.434	.197
34	206.2	17.1	13.0	.4673	-.4	.2996	24.90	64.35	.326	.130
35	275.0	18.1	13.2	.6232	-.1	.3996	26.28	63.80	.159	.030
36	343.9	18.5	13.4	.7792	-.0	.4996	26.86	63.65	.056	.000
37	412.7	18.6	13.3	.9352	-.0	.5998	26.91	63.65	.000	.002
38	447.6	18.6	13.3	1.0144	-.0	.6504	26.91	63.65	.000	.002

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00338 DELH = .697 REH = 674.0
V RUN = 122971-1 CF/2 = .00244 DELM = .693 REM = 1073.0
PLATE = 6 UINF = 24.4 DEL2 = .0930 DEL3 = 1.185
X(IN) = 22.00 GM = 4.060 THETA = .0844 DEL4 = 4.811
K(E06) = -.4600 GAM = -.982 BETA = .309 H = 1.903

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.2	0.0000	0.00	91.69	1.000	1.000
2	4.2	4.0	2.8	.0056	-11.7	.0071	4.92	86.74	.886	.918
3	4.8	4.5	3.2	.0067	-11.2	.0081	5.61	85.76	.870	.902
4	5.3	5.1	3.6	.0075	-10.7	.0091	6.26	84.67	.855	.883
5	5.9	5.5	4.0	.0083	-10.2	.0101	6.80	83.67	.842	.870
6	6.5	5.9	4.5	.0091	-9.8	.0111	7.35	82.95	.830	.854
7	7.1	6.4	4.8	.0099	-9.4	.0121	7.90	82.29	.817	.843
8	7.7	6.8	5.2	.0108	-9.1	.0131	8.37	81.55	.806	.830
9	8.3	7.1	5.5	.0116	-8.7	.0141	8.78	80.90	.797	.819
10	8.9	7.4	5.7	.0124	-8.5	.0151	9.21	80.45	.788	.812
11	9.5	7.8	6.1	.0132	-8.2	.0161	9.63	79.83	.778	.801
12	10.1	8.1	6.3	.0141	-8.0	.0171	9.97	79.38	.771	.793
13	11.2	8.5	6.7	.0157	-7.5	.0191	10.51	78.46	.760	.777
14	12.4	8.9	7.1	.0174	-7.1	.0211	11.05	77.71	.749	.764
15	13.6	9.3	7.5	.0190	-6.7	.0231	11.56	77.00	.738	.752
16	14.8	9.7	7.9	.0206	-6.4	.0251	12.02	76.28	.730	.739
17	16.5	10.2	8.3	.0231	-6.0	.0281	12.65	75.47	.717	.724
18	18.9	10.8	8.7	.0264	-5.5	.0321	13.31	74.67	.705	.709
19	21.2	11.1	9.1	.0297	-5.2	.0361	13.74	73.92	.698	.695
20	23.6	11.5	9.4	.0330	-4.9	.0401	14.21	73.32	.690	.684
21	25.3	11.7	9.5	.0354	-4.7	.0431	14.49	73.02	.686	.678
22	25.3	12.0	9.8	.0396	-4.4	.0481	14.92	72.45	.682	.666
23	31.2	12.2	10.0	.0437	-4.2	.0531	15.08	72.03	.679	.657
24	37.1	12.6	10.4	.0519	-3.9	.0631	15.66	71.40	.675	.642
25	48.9	13.2	10.9	.0683	-3.4	.0831	16.33	70.58	.669	.614
26	60.6	13.6	11.2	.0848	-3.4	.1031	16.88	69.72	.665	.592
27	72.4	14.0	11.5	.1013	-2.7	.1231	17.30	69.18	.661	.570
28	84.2	14.3	11.7	.1177	-2.5	.1431	17.67	68.76	.656	.558
29	113.6	15.0	12.2	.1588	-2.1	.1931	18.57	67.83	.634	.495
30	143.0	15.6	12.6	.2000	-1.6	.2431	19.31	67.04	.600	.437
31	172.4	16.2	12.9	.2411	-1.4	.2931	20.05	66.50	.554	.386
32	201.8	16.8	13.1	.2822	-1.1	.3431	20.74	65.96	.496	.329
33	231.2	17.3	13.4	.3233	-.9	.3931	21.46	65.50	.431	.277
34	290.0	18.3	13.7	.4056	-.5	.4931	22.65	64.78	.297	.170
35	349.9	19.1	14.0	.4879	-.2	.5931	23.60	64.29	.184	.089
36	407.7	19.6	14.2	.5701	-.1	.6931	24.21	63.93	.103	.023
37	466.5	19.7	14.2	.6524	-.0	.7931	24.39	63.81	.037	.000
38	525.3	19.7	14.2	.7346	.0	.8931	24.41	63.78	.000	.000
39	563.3	19.7	14.2	.7878	.0	.9577	24.41	63.78	.000	.000

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00315 DELH = .869 REH = 901.0
V RUN = 122971-1 CF/2 = .00231 DELM = .894 REM = 1330.0
PLATE = 9 UINF = 23.0 DEL2 = .0781 DEL3 = 1.688
X(IN) = 34.00 GM = 4.006 THETA = .1109 DEL4 = 6.767
K(E06) = -.3280 GAM = -.912 BETA = .288 H = 1.479

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.9	0.0000	0.00	91.82	1.000	1.000
2	3.9	3.9	2.6	.0042	-12.5	.0072	4.35	87.33	.899	.925
3	4.4	4.3	3.0	.0047	-12.1	.0082	4.86	86.53	.877	.912
4	5.0	4.7	3.4	.0053	-11.5	.0092	5.32	85.43	.866	.893
5	5.5	5.1	3.8	.0059	-11.1	.0102	5.78	84.67	.855	.880
6	6.0	5.5	4.1	.0065	-10.7	.0112	6.20	84.01	.844	.869
7	6.6	5.9	4.5	.0070	-10.4	.0122	6.66	83.33	.837	.858
8	7.1	6.3	4.9	.0076	-9.9	.0132	7.14	82.53	.821	.844
9	7.7	6.7	5.1	.0082	-9.7	.0142	7.61	82.12	.809	.837
10	8.2	7.0	5.4	.0088	-9.4	.0152	7.98	81.55	.800	.827
11	8.7	7.3	5.7	.0094	-9.1	.0162	8.31	81.02	.792	.818
12	9.3	7.6	6.0	.0099	-8.8	.0172	8.68	80.48	.783	.809
13	10.4	8.2	6.4	.0111	-8.4	.0192	9.33	79.71	.767	.796
14	11.4	8.7	6.9	.0122	-8.0	.0212	9.92	78.91	.753	.783
15	12.5	9.2	7.3	.0134	-7.6	.0232	10.55	78.13	.738	.769
16	13.6	9.7	7.6	.0145	-7.2	.0252	11.02	77.42	.727	.757
17	14.7	9.9	7.9	.0157	-6.9	.0272	11.26	76.91	.722	.748
18	15.7	10.1	8.2	.0169	-6.7	.0292	11.49	76.37	.717	.738
19	17.4	10.5	8.5	.0186	-6.3	.0322	11.96	75.74	.707	.727
20	19.0	10.9	8.8	.0203	-6.0	.0352	12.34	75.18	.700	.717
21	20.6	11.2	9.0	.0220	-5.8	.0382	12.68	74.79	.693	.713
22	22.9	11.5	9.4	.0244	-5.5	.0422	13.08	74.16	.686	.699
23	25.5	11.9	9.7	.0272	-5.1	.0472	13.47	73.50	.679	.686
24	29.8	12.4	10.1	.0320	-4.7	.0572	14.03	72.79	.672	.671
25	36.2	12.8	10.5	.0388	-4.4	.0672	14.47	72.06	.664	.656
26	41.6	13.0	10.7	.0445	-4.1	.0772	14.80	71.61	.665	.645
27	49.7	13.3	11.0	.0532	-3.8	.0922	15.12	70.98	.666	.630
28	63.2	13.7	11.4	.0676	-3.4	.1172	15.60	70.29	.667	.610
29	76.7	14.2	11.7	.0820	-3.2	.1422	16.08	69.78	.666	.592
30	103.6	14.8	12.2	.1109	-2.7	.1922	16.81	68.85	.667	.553
31	130.6	15.4	12.5	.1397	-2.4	.2422	17.44	68.25	.655	.522
32	157.6	15.9	12.8	.1686	-2.0	.2922	18.00	67.65	.640	.485
33	211.5	16.7	13.3	.2263	-1.5	.3922	18.97	66.71	.599	.411
34	265.4	17.6	13.7	.2840	-1.1	.4922	19.97	65.93	.505	.334
35	319.3	18.3	14.1	.3417	-.8	.5922	20.82	65.29	.397	.256
36	373.3	19.1	14.3	.3993	-.5	.6922	21.69	64.78	.285	.183
37	481.1	20.1	14.7	.5147	-.1	.8922	22.77	64.05	.103	.055
38	589.0	20.3	14.9	.6301	-.0	1.0922	23.00	63.78	.000	.000
39	696.8	20.3	14.9	.7455	.0	1.2922	23.00	63.78	.000	.000

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00300 DELH = 1.136 REH = 1108.0
V RUN = 122971-1 CF/2 = .00221 DELM = 1.120 REM = 1575.0
PLATE = 12 UINF = 22.1 DEL2 = .0961 DEL3 = 2.143
X(IN) = 46.00 GM = 3.956 THETA = .1366 DEL4 = 9.637
K(E06) = -.2570 GAM = -.852 BETA = .280 H = 1.475

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.3	0.0000	0.00	91.86	1.000	1.000
2	4.2	3.9	2.9	.0037	-12.6	.0053	4.21	86.94	.869	.915
3	4.7	4.3	3.1	.0041	-12.2	.0093	4.57	86.14	.860	.905
4	5.2	4.7	3.6	.0046	-11.7	.0103	4.96	85.23	.869	.989
5	5.7	5.0	3.9	.0050	-11.3	.0113	5.37	84.64	.859	.979
6	6.2	5.4	4.3	.0055	-11.0	.0123	5.77	83.98	.849	.868
7	6.7	5.8	4.6	.0059	-10.6	.0133	6.14	83.33	.839	.857
8	7.2	6.1	4.9	.0064	-10.3	.0143	6.47	82.80	.830	.848
9	7.7	6.4	5.2	.0068	-10.0	.0153	6.79	82.24	.822	.839
10	8.2	6.7	5.6	.0073	-9.7	.0163	7.14	81.67	.813	.829
11	8.7	7.0	5.7	.0077	-9.5	.0173	7.45	81.34	.804	.824
12	9.8	7.7	6.2	.0086	-9.0	.0193	8.16	80.39	.787	.808
13	10.8	8.2	6.6	.0095	-8.6	.0213	8.73	79.69	.772	.795
14	11.8	8.6	7.1	.0104	-8.2	.0233	9.13	78.85	.762	.781
15	13.3	9.2	7.6	.0117	-7.7	.0263	9.83	77.92	.745	.765
16	14.8	9.9	8.0	.0131	-7.2	.0293	10.51	77.12	.728	.752
17	16.9	10.5	8.5	.0148	-6.8	.0333	11.15	76.28	.713	.737
18	18.9	11.0	8.8	.0166	-6.4	.0373	11.69	75.63	.701	.726
19	20.9	11.4	9.2	.0184	-6.1	.0413	11.86	74.97	.698	.714
20	23.4	11.8	9.5	.0206	-5.8	.0463	12.34	74.46	.689	.705
21	26.5	12.0	9.8	.0233	-5.5	.0523	12.84	73.86	.679	.694
22	29.5	12.3	10.1	.0260	-5.1	.0583	13.17	73.26	.674	.683
23	33.1	12.5	10.3	.0291	-4.9	.0653	13.38	72.90	.672	.676
24	37.1	12.8	10.5	.0327	-4.7	.0733	13.65	72.51	.669	.668
25	42.2	13.1	10.8	.0372	-4.5	.0833	13.98	72.01	.666	.658
26	49.8	13.5	11.1	.0438	-4.1	.0983	14.39	71.44	.663	.645
27	59.9	13.8	11.4	.0528	-3.8	.1183	14.71	70.87	.665	.630
28	72.6	14.1	11.6	.0639	-3.6	.1433	15.04	70.48	.668	.620
29	90.3	14.5	12.0	.0795	-3.3	.1783	15.50	69.84	.670	.599
30	110.6	15.0	12.3	.0974	-3.0	.2183	15.97	69.24	.670	.576
31	135.9	15.4	12.7	.1197	-2.6	.2683	16.47	68.64	.669	.549
32	173.9	16.1	13.0	.1532	-2.3	.3433	17.14	68.01	.659	.513
33	224.6	16.9	13.5	.1978	-1.8	.4433	17.97	67.14	.631	.451
34	288.0	17.8	13.9	.2535	-1.4	.5683	18.94	66.35	.565	.380
35	351.3	18.5	14.3	.3093	-1.0	.6933	19.78	65.69	.462	.305
36	427.3	19.4	14.6	.3762	-.7	.8433	20.74	65.02	.322	.214
37	503.3	20.2	14.9	.4432	-.4	.9933	21.52	64.45	.195	.122
38	604.7	20.7	15.2	.5324	-.1	1.1933	22.03	63.99	.074	.035
39	706.0	20.7	15.3	.6216	-.0	1.3933	22.12	63.84	.010	.000
40	736.0	20.7	15.3	.6480	-.0	1.4525	22.12	63.84	.000	.000
41	812.0	20.7	15.3	.7150	-.0	1.6025	22.12	63.84	.000	.000

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00289 DELH = 1.352 REH = 1294.0
V RUN = 122971-1 CF/2 = .00215 DELM = 1.330 REM = 1776.0
PLATE = 15 UINF = 21.4 DEL2 = .1161 DEL3 = 2.676
X(IN) = 58.00 GM = 3.916 THETA = .1554 DEL4 = 10.124
K(E06) = -.2110 GAM = -.932 BETA = .266 H = 1.450

I	Y+	U+	T+	Y/DEL3	-IO	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.6	0.0000	0.00	91.79	1.000	1.000
2	3.1	3.2	2.1	.0023	-13.7	.0063	3.24	88.36	.909	.942
3	3.6	3.6	2.4	.0027	-13.4	.0073	3.63	87.74	.899	.931
4	4.0	3.9	2.7	.0031	-13.0	.0083	3.97	87.03	.890	.919
5	4.5	4.2	3.0	.0035	-12.6	.0093	4.27	86.35	.881	.908
6	5.0	4.6	3.5	.0038	-12.2	.0103	4.72	85.61	.870	.895
7	5.5	5.0	3.9	.0042	-11.8	.0113	5.13	84.99	.859	.885
8	6.0	5.4	4.2	.0046	-11.4	.0123	5.47	84.28	.849	.873
9	6.5	5.7	4.6	.0049	-11.1	.0133	5.80	83.63	.840	.861
10	6.9	6.1	4.8	.0053	-10.9	.0143	6.18	83.24	.829	.855
11	7.9	6.8	5.3	.0060	-10.3	.0163	6.96	82.24	.810	.835
12	8.9	7.3	5.9	.0068	-9.8	.0183	7.47	81.29	.794	.821
13	9.8	7.9	6.1	.0075	-9.3	.0203	8.01	80.48	.780	.808
14	10.8	8.3	6.7	.0083	-8.9	.0223	8.47	79.77	.769	.795
15	11.8	8.7	7.1	.0090	-8.6	.0243	8.97	79.14	.757	.785
16	12.8	9.2	7.4	.0097	-8.2	.0263	9.35	78.55	.744	.774
17	13.7	9.6	7.7	.0105	-8.0	.0283	9.79	78.07	.737	.766
18	15.2	9.9	8.1	.0116	-7.5	.0313	10.12	77.24	.725	.751
19	16.6	10.4	8.5	.0127	-7.1	.0343	10.55	76.61	.714	.740
20	18.1	10.8	8.8	.0138	-6.8	.0373	11.04	76.04	.702	.730
21	20.0	11.3	9.2	.0153	-6.4	.0417	11.49	75.36	.691	.717
22	22.0	11.6	9.5	.0168	-6.2	.0463	11.93	74.55	.683	.708
23	24.4	12.0	9.7	.0186	-6.0	.0513	12.19	74.49	.675	.702
24	28.2	12.3	10.2	.0216	-5.5	.0593	12.56	73.59	.669	.684
25	33.1	12.7	10.5	.0253	-5.1	.0693	12.90	72.99	.665	.672
26	40.4	13.2	10.9	.0308	-4.7	.0843	13.49	72.31	.657	.658
27	52.5	13.7	11.3	.0400	-4.3	.1043	13.96	71.50	.654	.640
28	64.6	14.1	11.7	.0493	-4.0	.1233	14.35	70.90	.654	.625
29	81.5	14.5	12.0	.0622	-3.6	.1683	14.79	70.24	.656	.606
30	100.9	14.9	12.3	.0770	-3.3	.2083	15.20	69.73	.660	.590
31	125.1	15.4	12.6	.0955	-3.0	.2583	15.64	69.21	.661	.570
32	161.4	16.0	13.0	.1232	-2.6	.3333	16.26	68.52	.656	.537
33	209.8	16.6	13.4	.1601	-2.2	.4333	16.92	67.80	.642	.495
34	282.4	17.5	13.9	.2156	-1.7	.5833	17.80	66.84	.592	.421
35	379.3	18.7	14.5	.2895	-1.2	.7833	19.04	65.67	.488	.319
36	476.1	19.7	14.9	.3634	-.7	.9833	20.09	65.06	.334	.218
37	597.1	20.6	15.4	.4558	-.3	1.2333	20.98	64.33	.163	.099
38	694.0	21.0	15.6	.5297	-.1	1.4233	21.34	63.94	.044	.023
39	790.8	21.0	15.6	.6036	-.0	1.6133	21.42	63.82	.000	.000
40	876.1	21.0	15.6	.6687	-.0	1.8095	21.42	63.82	.000	.007

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00281 DELH = 1.603 REH = 1689.0
V RUN = 122971-1 CF/2 = .00206 DELM = 1.520 REM = 1995.0
PLATE = 18 UINF = 20.9 DEL2 = .1368 DEL3 = 3.117
X(IN) = 70.00 GH = 3.883 THETA = .1835 DEL4 = 12.105
K(E06)= -.1790 GAM = -.797 BETA = .262 M = 1.449

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-15.4	0.0000	0.00	91.79	1.000	1.000
2	2.9	3.0	2.0	.0020	-13.9	.0063	2.96	88.42	.916	.943
3	3.4	3.4	2.3	.0023	-13.6	.0073	3.29	87.92	.907	.935
4	3.9	3.7	2.6	.0026	-13.3	.0083	3.59	87.33	.898	.925
5	4.3	4.0	2.9	.0029	-12.9	.0093	3.91	86.65	.890	.914
6	4.8	4.3	3.3	.0032	-12.5	.0103	4.24	86.03	.881	.903
7	5.2	4.7	3.7	.0035	-12.1	.0113	4.56	85.29	.871	.891
8	5.7	5.0	4.0	.0039	-11.8	.0123	4.98	84.81	.863	.883
9	6.7	5.7	4.6	.0045	-11.2	.0143	5.54	83.66	.844	.863
10	7.6	6.3	5.2	.0051	-10.6	.0163	6.20	82.62	.825	.846
11	8.5	6.9	5.6	.0057	-10.2	.0183	6.80	82.00	.809	.835
12	9.4	7.4	6.1	.0064	-9.7	.0203	7.28	81.05	.795	.819
13	10.4	7.9	6.5	.0070	-9.3	.0223	7.71	80.28	.783	.806
14	11.8	8.5	7.1	.0079	-8.7	.0253	8.36	79.29	.766	.789
15	13.2	9.2	7.5	.0089	-8.3	.0283	8.99	78.61	.749	.778
16	14.6	9.7	7.8	.0098	-8.0	.0313	9.52	77.98	.735	.768
17	16.4	10.4	9.3	.0110	-7.5	.0353	10.14	77.12	.719	.753
18	15.7	10.9	9.9	.0126	-6.9	.0403	10.62	76.13	.707	.736
19	21.1	11.3	9.3	.0142	-6.5	.0453	11.04	75.51	.697	.725
20	23.4	11.9	9.6	.0157	-6.2	.0503	11.50	74.82	.685	.713
21	28.0	12.4	10.0	.0189	-5.8	.0603	12.14	74.16	.671	.702
22	35.0	12.9	10.5	.0236	-5.3	.0753	12.60	73.35	.667	.686
23	42.0	13.3	10.9	.0282	-4.9	.0903	13.06	72.61	.656	.670
24	46.6	13.6	11.1	.0314	-4.7	.1003	13.25	72.22	.657	.661
25	58.2	13.9	11.5	.0392	-4.3	.1253	13.63	71.65	.650	.648
26	69.9	14.4	11.9	.0470	-4.0	.1503	14.04	71.05	.648	.634
27	93.2	14.9	12.2	.0626	-3.6	.2003	14.57	70.39	.646	.615
28	116.4	15.2	12.5	.0783	-3.3	.2503	14.99	69.82	.649	.593
29	139.7	15.6	12.8	.0939	-3.0	.3003	15.25	69.34	.649	.571
30	186.2	16.3	13.2	.1251	-2.6	.4003	15.97	68.61	.637	.537
31	232.7	16.9	13.6	.1564	-2.2	.5003	16.52	67.89	.619	.487
32	325.7	18.0	14.1	.2189	-1.7	.7003	17.62	66.96	.567	.419
33	418.7	19.0	14.6	.2814	-1.2	.9003	18.57	66.05	.467	.331
34	558.2	20.3	15.2	.3752	-.6	1.2003	19.94	65.06	.267	.191
35	697.8	21.1	15.6	.4690	-.2	1.5003	20.67	64.36	.094	.067
36	837.3	21.4	15.8	.5628	-.0	1.8003	20.90	64.03	.005	.000
37	883.8	21.4	15.8	.5940	-0.0	1.9003	20.90	64.00	.000	.000
38	1023.3	21.4	15.8	.6878	.0	2.2003	20.90	63.97	.000	.000

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00274 DELH = 1.739 REH = 1631.0
V RUN = 122971-1 CF/2 = .00203 DELM = 1.739 REM = 2200.0
PLATE = 21 UINF = 20.4 DEL2 = .1532 DEL3 = 3.521
X(IN) = 92.00 GH = 3.562 THETA = .2066 DEL4 = 13.598
K(E06)= -.1550 GAM = -.771 BETA = .256 M = 1.442

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-16.0	0.0000	0.00	91.75	1.000	1.000
2	3.0	3.1	2.0	.0019	-14.1	.0067	2.89	88.39	.916	.943
3	3.4	3.3	2.3	.0021	-13.9	.0077	3.14	87.83	.909	.934
4	3.9	3.5	2.6	.0024	-13.6	.0087	3.31	87.27	.904	.924
5	4.3	3.8	2.9	.0027	-13.3	.0097	3.65	86.71	.896	.915
6	4.8	4.1	3.3	.0030	-12.9	.0107	3.85	85.97	.888	.902
7	5.2	4.4	3.7	.0032	-12.6	.0117	4.15	85.44	.879	.893
8	5.7	4.8	4.0	.0035	-12.3	.0127	4.50	84.84	.870	.883
9	6.6	5.5	4.6	.0041	-11.6	.0147	5.19	83.78	.851	.865
10	7.5	6.1	5.1	.0046	-10.9	.0167	5.74	82.95	.835	.850
11	8.4	6.6	5.6	.0052	-10.4	.0187	6.24	82.09	.821	.836
12	9.3	7.2	6.1	.0057	-10.0	.0207	6.90	81.29	.808	.822
13	10.2	7.9	6.4	.0063	-9.6	.0227	7.42	80.63	.787	.811
14	11.6	8.5	7.0	.0071	-9.0	.0257	8.27	79.65	.762	.794
15	12.9	9.3	7.5	.0079	-8.5	.0287	8.76	78.85	.747	.780
16	14.2	9.8	8.0	.0088	-8.0	.0317	9.28	77.95	.734	.764
17	15.5	10.3	8.2	.0096	-7.8	.0347	9.66	77.54	.722	.757
18	17.3	10.7	8.9	.0107	-7.2	.0387	10.05	76.61	.714	.740
19	19.1	11.0	9.0	.0118	-7.0	.0427	10.34	76.19	.707	.733
20	21.4	11.5	9.5	.0132	-6.6	.0477	10.92	75.42	.694	.719
21	25.9	12.2	9.9	.0160	-6.1	.0577	11.54	74.54	.674	.703
22	30.3	12.6	10.3	.0187	-5.7	.0677	11.90	73.95	.669	.691
23	37.1	13.1	10.7	.0229	-5.3	.0827	12.35	73.26	.660	.679
24	46.0	13.5	11.2	.0284	-4.9	.1027	12.73	72.49	.656	.667
25	55.0	13.8	11.4	.0340	-4.6	.1227	13.02	72.01	.654	.652
26	64.0	14.1	11.8	.0395	-4.2	.1427	13.31	71.44	.657	.617
27	86.4	14.9	12.2	.0533	-3.8	.1927	13.97	70.75	.644	.614
28	131.2	15.6	12.7	.0810	-3.3	.2927	14.72	69.82	.637	.581
29	176.1	16.1	13.1	.1087	-2.9	.3927	15.23	69.10	.642	.558
30	268.7	17.3	13.9	.1641	-2.2	.5927	16.36	67.83	.637	.476
31	355.4	18.2	14.4	.2194	-1.6	.7927	17.21	66.93	.598	.404
32	445.1	19.1	14.8	.2748	-1.2	.9927	18.08	66.20	.501	.332
33	579.6	20.3	15.3	.3574	-.7	1.2927	19.16	65.33	.337	.220
34	714.1	21.2	15.7	.4408	-.3	1.5927	19.98	64.63	.154	.112
35	849.7	21.6	16.0	.5239	-.0	1.8927	20.37	64.19	.033	.031
36	881.2	21.7	16.0	.5569	.0	2.1927	20.47	64.06	.000	.000
37	1117.7	21.7	16.0	.6900	.0	2.4927	20.47	64.06	.000	.000

DATE = 011772 (-0.15, -0.002, -0.17)

T RUN = 11772-1 STNA = .00270 DELH = 1.921 REH = 1783.0
V RUN = 122971-1 CF/2 = .00201 DELM = 1.949 REM = 2294.0
PLATE = 23 UINF = 20.1 DEL2 = .1762 DEL3 = 3.954
X(IN) = 90.00 GH = 3.906 THETA = .2190 DEL4 = 15.248
K(E06)= -.1490 GAM = -.788 BETA = .260 M = 1.435

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T
1	.0	0.0	.0	0.0000	-16.2	0.0000	0.00	91.86
2	1.5	1.5	1.2	.0010	-14.7	.0041	1.65	89.27
3	2.2	2.2	1.5	.0013	-14.5	.0051	2.05	89.04
4	2.7	2.6	1.8	.0015	-14.2	.0061	2.44	88.71
5	3.1	3.0	2.1	.0018	-14.1	.0071	2.82	88.30
6	3.5	3.4	2.4	.0020	-13.8	.0081	3.19	87.74
7	4.0	3.8	2.8	.0023	-13.4	.0091	3.55	87.15
8	4.4	4.2	3.1	.0025	-13.1	.0101	3.91	86.59
9	5.3	5.0	3.8	.0030	-12.4	.0121	4.62	85.58
10	6.2	5.8	4.4	.0036	-11.8	.0141	5.14	84.48
11	7.1	6.1	5.0	.0040	-11.2	.0161	5.62	83.36
12	7.9	6.8	5.4	.0045	-10.8	.0181	6.28	82.65
13	8.8	7.4	5.9	.0050	-10.3	.0201	6.86	81.76
14	9.7	7.9	6.3	.0055	-9.9	.0221	7.30	81.11
15	11.0	8.4	6.8	.0063	-9.3	.0251	7.75	80.16
16	12.3	8.9	7.4	.0070	-8.8	.0281	8.24	79.20
17	13.6	9.5	7.8	.0078	-8.4	.0311	8.78	78.61
18	15.0	10.1	8.4	.0085	-8.1	.0341	9.24	77.95
19	17.2	10.7	8.8	.0098	-7.6	.0391	9.86	77.12
20	19.4	11.2	9.1	.0110	-7.1	.0441	10.31	76.34
21	21.6	11.6	9.4	.0123	-6.8	.0491	10.70	75.87
22	26.0	12.2	10.0	.0148	-6.2	.0591	11.27	74.82
23	30.3	12.6	10.3	.0173	-5.8	.0691	11.69	74.19
24	39.1	13.3	10.9	.0223	-5.2	.0891	12.26	73.20
25	50.1	13.8	11.3	.0285	-4.9	.1141	12.77	72.52
26	61.1	14.2	11.6	.0347	-4.6	.1391	13.17	72.10
27	83.1	14.6	12.1	.0472	-4.1	.1891	13.50	71.17
28	127.0	15.6	12.7	.0722	-3.5	.2891	14.42	70.18
29	171.0	16.2	13.1	.0971	-3.1	.3891	15.00	69.43
30	258.9	17.3	13.8	.1471	-2.4	.5891	15.97	68.28
31	346.8	18.2	14.3	.1970	-1.9	.7891	16.75	67.38
32	434.7	19.0	14.7	.2469	-1.4	.9891	17.52	66.66
33	566.5	20.1	15.2	.3219	-.9	1.2891	18.59	65.79
34	698.3	21.0	15.7	.3967	-.5	1.5891	19.43	65.03
35	830.2	21.6	16.0	.4715	-.2	1.8891	19.96	64.48
36	962.0	21.8	16.2	.5464	-.0	2.1891	20.13	64.24
37	1137.8	21.7	16.2	.6463	.0	2.5891	20.10	64.18
38	1149.1	21.7	16.2	.6527	.0	2.6149	20.10	64.18

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00690 DELH = .154 REH = 127.0
V RUN = 122771-3 CF/2 = .00389 DELM = .295 REM = 471.0
PLATE = 1 UINF = 29.3 DEL2 = .0052 DEL3 = .149
X(IN) = 2.00 GH = 3.441 THETA = .0305 DEL4 = .509
K(E06)= -.4450 GAM = -.435 BETA = .589 M = 1.482

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T
1	.0	0.0	.0	0.0000	-8.8	0.0000	0.00	90.61
2	3.4	3.2	2.2	.0248	-6.6	.0034	5.93	83.63
3	4.3	3.9	2.9	.0313	-6.1	.0048	7.27	81.91
4	5.2	4.5	3.7	.0379	-5.5	.0054	8.53	80.13
5	6.1	5.2	3.9	.0445	-5.0	.0068	9.65	78.40
6	7.0	5.7	4.2	.0510	-4.6	.0078	10.76	77.09
7	7.9	6.3	4.6	.0576	-4.2	.0088	11.75	75.92
8	8.8	6.7	4.9	.0641	-3.9	.0098	12.67	74.79
9	9.7	7.2	5.2	.0707	-3.6	.0108	13.48	73.89
10	10.6	7.6	5.5	.0772	-3.3	.0118	14.21	73.02
11	11.5	7.9	5.7	.0838	-3.1	.0128	14.89	72.33
12	12.4	8.3	5.9	.0904	-2.9	.0138	15.49	71.58
13	13.3	8.5	6.1	.0969	-2.7	.0148	16.01	70.95
14	14.2	8.8	6.3	.1035	-2.5	.0158	16.47	70.35
15	15.1	9.0	6.5	.1100	-2.3	.0168	16.91	69.78
16	16.0	9.2	6.6	.1166	-2.2	.0178	17.32	69.30
17	16.9	9.4	6.7	.1232	-2.1	.0188	17.70	68.94
18	17.8	9.6	6.9	.1297	-2.0	.0198	18.06	68.61
19	19.6	10.0	7.1	.1428	-1.7	.0218	18.69	67.92
20	21.4	10.3	7.2	.1559	-1.6	.0238	19.24	67.34
21	24.0	10.6	7.4	.1756	-1.4	.0268	19.83	66.66
22	26.7	10.8	7.6	.1953	-1.2	.0298	20.32	66.14
23	30.7	11.1	7.8	.2215	-1.0	.0338	20.92	65.59
24	33.9	11.4	7.9	.2478	-.9	.0378	21.34	65.17
25	40.2	11.7	8.1	.2937	-.7	.0448	21.99	64.60
26	46.5	11.9	8.2	.3396	-.6	.0518	22.34	64.23
27	53.7	12.1	8.3	.3920	-.5	.0598	22.76	63.97
28	62.7	12.4	8.4	.4576	-.4	.0698	23.20	63.57
29	80.6	12.6	8.5	.5888	-.2	.0898	24.03	63.11
30	103.1	13.3	8.6	.7528	-.2	.1148	24.94	62.91
31	125.5	13.7	8.7	.9167	-.1	.1398	25.74	62.62
32	170.4	14.6	8.8	1.2446	-.0	.1898	27.31	62.41
33	215.3	15.1	8.9	1.5726	-.0	.2398	28.41	62.34
34	260.2	15.5	8.8	1.9005	.0	.2898	29.05	62.28
35	350.0	15.6	8.9	2.5563	.0	.3898	29.31	62.26
36	363.1	15.6	8.8	2.6521	.0	.4044	29.31	62.26
37	417.0	15.6	8.8	3.0456	.0	.4644	29.31	62.26

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00472 DELM = .308 REM = 282.0
V RUN = 122771-3 CF/2 = .00369 DELM = .398 REM = 568.0
PLATE = 3 UINF = 26.8 DEL2 = .0280 DEL3 = .426
X(IN) = 10.00 GM = 4.301 THETA = .0403 DEL4 = 1.831
K(E06) = -.9360 GAM = -1.004 BETA = .191 H = 1.473

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-12.5	0.0000	0.00	90.54	1.000	1.000
2	5.7	5.0	3.6	.0163	-9.0	.0072	6.32	82.77	.725	.790
3	6.5	5.4	4.1	.0186	-8.4	.0082	6.98	81.43	.704	.752
4	7.3	5.8	4.5	.0209	-8.0	.0092	7.70	80.45	.680	.725
5	8.1	6.2	5.0	.0232	-7.5	.0102	10.41	79.41	.657	.696
6	8.9	6.6	5.4	.0255	-7.1	.0112	11.09	78.49	.635	.671
7	9.7	7.0	5.8	.0277	-6.7	.0122	11.76	77.65	.613	.647
8	10.5	7.4	6.1	.0300	-6.4	.0132	12.37	76.91	.593	.626
9	11.3	7.8	6.5	.0323	-6.1	.0142	12.96	76.16	.573	.605
10	12.1	8.1	6.8	.0346	-5.8	.0152	13.52	75.50	.555	.586
11	12.9	8.4	7.0	.0369	-5.5	.0162	14.04	74.85	.539	.567
12	13.7	8.7	7.3	.0392	-5.2	.0172	14.51	74.31	.524	.552
13	14.5	8.9	7.5	.0415	-5.0	.0182	14.93	73.83	.511	.538
14	15.3	9.2	7.7	.0438	-4.8	.0192	15.31	73.35	.499	.524
15	16.9	9.6	8.1	.0483	-4.4	.0212	16.02	72.45	.477	.498
16	18.5	10.0	8.5	.0529	-4.0	.0232	16.63	71.61	.459	.473
17	20.1	10.2	8.7	.0575	-3.8	.0252	17.10	71.07	.445	.457
18	21.7	10.5	9.0	.0620	-3.6	.0272	17.53	70.56	.432	.441
19	24.1	10.8	9.3	.0689	-3.2	.0302	18.04	69.78	.419	.417
20	26.5	11.0	9.6	.0758	-3.0	.0232	18.44	69.21	.409	.399
21	29.7	11.4	9.9	.0849	-2.7	.0372	18.98	68.64	.395	.780
22	32.9	11.6	10.1	.0940	-2.5	.0412	19.40	68.12	.386	.362
23	36.9	11.8	10.3	.1055	-2.2	.0462	19.72	67.58	.381	.343
24	40.9	12.0	10.5	.1169	-2.0	.0512	20.04	67.16	.375	.327
25	46.5	12.2	10.7	.1329	-1.8	.0582	20.42	66.69	.370	.307
26	52.9	12.4	10.9	.1512	-1.7	.0662	20.77	66.32	.366	.291
27	60.9	12.7	11.1	.1740	-1.5	.0762	21.20	65.86	.361	.268
28	68.9	12.9	11.2	.1969	-1.3	.0862	21.58	65.50	.359	.249
29	80.9	13.1	11.4	.2312	-1.1	.1012	21.99	65.06	.356	.223
30	100.9	13.5	11.7	.2843	-.9	.1262	22.45	64.51	.347	.184
31	120.9	13.8	11.9	.3455	-.7	.1512	23.03	64.11	.333	.153
32	149.0	14.2	12.1	.4255	-.5	.1862	23.71	63.72	.303	.117
33	181.0	14.6	12.2	.5169	-.3	.2262	24.42	63.32	.257	.077
34	221.0	15.1	12.4	.6312	-.2	.2762	25.23	63.02	.192	.043
35	261.0	15.5	12.4	.7455	-.1	.3262	25.89	62.84	.131	.021
36	321.0	15.9	12.5	.9170	-.0	.4012	26.56	62.68	.066	.000
37	381.0	16.0	12.5	1.0884	-.0	.4762	26.79	62.62	.027	.000
38	406.6	16.0	12.5	1.1616	-.0	.5062	26.82	62.62	.016	.000
39	458.6	16.1	12.5	1.3102	-.0	.5732	26.83	62.62	.000	.000
40	518.6	16.1	12.5	1.4817	-.0	.6482	26.83	62.62	.000	.000

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00423 DELM = .486 REM = 423.0
V RUN = 122771-3 CF/2 = .00340 DELM = .563 REM = 720.0
PLATE = 6 UINF = 24.3 DEL2 = .0331 DEL3 = .694
X(IN) = 22.00 GM = 4.020 THETA = .0564 DEL4 = 2.759
K(E06) = -.4650 GAM = -.763 BETA = .146 H = 1.439

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-13.4	0.0000	0.00	90.75	1.000	1.000
2	4.7	4.6	3.0	.0095	-10.9	.0067	6.70	85.52	.751	.858
3	5.4	4.9	3.4	.0109	-10.3	.0077	7.05	84.31	.738	.825
4	6.1	5.1	3.9	.0123	-9.8	.0087	7.49	83.19	.723	.794
5	6.7	5.6	4.2	.0137	-9.3	.0097	8.17	82.15	.698	.766
6	7.4	6.0	4.7	.0151	-8.8	.0107	8.78	81.08	.676	.736
7	8.1	6.5	5.0	.0165	-8.4	.0117	9.38	80.27	.654	.714
8	8.8	6.9	5.4	.0179	-8.0	.0127	9.98	79.59	.632	.696
9	9.5	7.3	5.7	.0193	-7.7	.0137	10.54	78.85	.611	.675
10	10.2	7.6	6.1	.0207	-7.4	.0147	11.05	78.16	.593	.656
11	10.9	7.9	6.3	.0221	-7.1	.0157	11.48	77.59	.577	.640
12	11.6	8.1	6.6	.0235	-6.8	.0167	11.94	77.00	.564	.624
13	13.0	8.6	7.1	.0264	-6.3	.0187	12.54	75.95	.539	.595
14	14.4	9.1	7.6	.0292	-5.9	.0207	13.23	75.06	.515	.570
15	15.8	9.5	7.9	.0320	-5.5	.0227	13.88	74.40	.492	.551
16	17.2	9.9	8.3	.0349	-5.1	.0247	14.39	73.59	.474	.526
17	19.3	10.2	8.7	.0390	-4.7	.0277	14.90	72.69	.457	.502
18	21.4	10.7	9.1	.0432	-4.4	.0307	15.56	71.97	.434	.482
19	23.4	11.0	9.4	.0474	-4.0	.0337	15.95	71.31	.419	.462
20	25.5	11.2	9.7	.0516	-3.7	.0367	16.33	70.69	.408	.443
21	29.3	11.5	9.9	.0573	-3.5	.0407	16.66	70.14	.397	.427
22	31.1	11.7	10.2	.0629	-3.2	.0447	16.98	69.63	.385	.411
23	34.6	11.9	10.4	.0699	-3.1	.0497	17.30	69.24	.378	.399
24	39.4	12.1	10.7	.0797	-2.7	.0567	17.66	68.61	.368	.378
25	45.0	12.4	10.9	.0910	-2.5	.0647	18.01	68.19	.358	.363
26	52.0	12.7	11.1	.1050	-2.3	.0747	18.40	67.65	.348	.342
27	62.4	12.9	11.4	.1261	-2.0	.0897	18.81	67.13	.337	.320
28	76.3	13.2	11.7	.1542	-1.7	.1097	19.22	66.53	.324	.292
29	93.7	13.5	11.9	.1893	-1.5	.1347	19.70	65.99	.318	.264
30	115.1	13.9	12.2	.2345	-1.2	.1697	20.25	65.45	.299	.230
31	152.9	14.4	12.5	.3047	-.9	.2197	20.99	64.79	.272	.181
32	187.7	14.8	12.8	.3790	-.7	.2697	21.59	64.27	.241	.138
33	239.8	15.4	13.0	.4843	-.4	.3447	22.44	63.78	.197	.090
34	309.4	16.1	13.2	.6248	-.2	.4447	23.39	63.30	.114	.035
35	379.0	16.5	13.4	.7653	-.1	.5447	23.99	63.02	.059	.000
36	448.6	16.7	13.4	.9057	.0	.6447	24.27	62.90	.027	.000
37	552.9	16.7	13.4	1.1165	-.0	.7947	24.33	62.90	.004	.000
38	622.5	16.7	13.4	1.2569	-.0	.8947	24.33	62.90	.000	.000
39	645.6	16.7	13.4	1.3095	-.0	.9322	24.33	62.90	.000	.000

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00394 DELM = .638 REM = 553.0
V RUN = 122771-3 CF/2 = .00322 DELM = .700 REM = 942.0
PLATE = 9 UINF = 23.0 DEL2 = .0459 DEL3 = .959
X(IN) = 34.00 GM = 4.024 THETA = .0699 DEL4 = 3.858
K(E06) = -.3310 GAM = -.679 BETA = .125 H = 1.411

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.0	0.0000	0.00	91.10	1.000	1.000
2	5.2	4.7	3.3	.0083	-10.9	.0061	6.25	84.78	.756	.829
3	5.8	5.1	3.7	.0093	-10.3	.0091	6.80	83.69	.734	.799
4	6.4	5.5	4.1	.0103	-9.9	.0101	7.34	82.89	.713	.778
5	7.1	5.9	4.6	.0113	-9.5	.0111	7.99	82.06	.692	.755
6	7.7	6.3	4.9	.0123	-9.1	.0121	8.46	81.31	.669	.735
7	8.4	6.7	5.3	.0134	-8.7	.0131	9.02	80.60	.648	.715
8	9.0	7.1	5.6	.0144	-8.4	.0141	9.49	79.99	.630	.696
9	9.6	7.4	5.9	.0154	-8.1	.0151	9.98	79.35	.614	.681
10	10.3	7.6	6.2	.0164	-7.9	.0161	10.14	78.82	.605	.667
11	10.9	7.8	6.5	.0174	-7.6	.0171	10.43	78.28	.593	.652
12	12.2	8.6	6.9	.0195	-7.1	.0191	11.50	77.32	.552	.626
13	13.5	9.1	7.5	.0215	-6.5	.0211	12.13	76.19	.528	.595
14	14.8	9.4	7.8	.0235	-6.2	.0231	12.58	75.62	.511	.579
15	16.1	9.9	8.1	.0256	-5.9	.0251	13.27	74.94	.484	.560
16	18.0	10.3	8.6	.0286	-5.4	.0281	13.98	74.04	.465	.535
17	19.9	10.6	9.0	.0316	-5.0	.0311	14.23	73.23	.449	.513
18	21.8	10.9	9.3	.0347	-4.7	.0341	14.61	72.57	.435	.494
19	24.4	11.2	9.7	.0388	-4.3	.0361	15.05	71.79	.419	.472
20	26.9	11.5	9.9	.0428	-4.1	.0421	15.41	71.43	.407	.462
21	30.1	11.8	10.2	.0479	-3.8	.0471	15.79	70.80	.394	.443
22	33.3	12.0	10.5	.0530	-3.6	.0521	16.11	70.29	.383	.428
23	37.8	12.3	10.7	.0601	-3.3	.0591	16.45	69.84	.372	.414
24	44.2	12.6	11.0	.0703	-3.0	.0691	16.82	69.18	.361	.393
25	50.6	12.8	11.2	.0804	-2.8	.0791	17.18	68.82	.350	.381
26	60.2	13.1	11.5	.0957	-2.5	.0941	17.55	68.19	.341	.359
27	76.2	13.5	11.9	.1211	-2.2	.1191	18.02	67.59	.329	.335
28	92.2	13.8	12.1	.1465	-1.9	.1441	18.43	67.02	.318	.309
29	114.7	14.1	12.4	.1821	-1.7	.1791	18.96	66.50	.305	.283
30	140.3	14.4	12.6	.2227	-1.4	.2191	19.29	65.99	.291	.254
31	172.3	14.6	12.9	.2735	-1.1	.2691	19.81	65.45	.270	.220
32	220.3	15.4	13.2	.3497	-.8	.3441	20.56	64.84	.233	.175
33	284.3	15.9	13.5	.4514	-.5	.4441	21.33	64.21	.175	.119
34	348.4	16.4	13.8	.5530	-.3	.5441	22.03	63.78	.115	.076
35	444.4	17.0	14.0	.7054	-.1	.6941	22.76	63.36	.043	.027
36	572.5	17.2	14.1	.9087	.0	.8941	23.01	63.18	.003	.000
37	700.5	17.2	14.0	1.1119	-.0	1.0941	23.01	63.24	.000	.000

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00375 DELM = .811 REM = 583.0
V RUN = 122771-3 CF/2 = .00310 DELM = .831 REM = 966.0
PLATE = 12 UINF = 22.0 DEL2 = .0593 DEL3 = 1.251
X(IN) = 46.00 GM = 3.876 THETA = .0841 DEL4 = 4.798
K(E06) = -.2570 GAM = -.586 BETA = .119 H = 1.424

I	Y+	U+	T+	Y/DEL3	-ID	Y	U	T	TAU+	Q+
1	.0	0.0	.0	0.0000	-14.5	0.0000	0.00	91.30	1.000	1.000
2	4.5	4.0	3.0	.0059	-11.8	.0078	4.99	86.12	.798	.859
3	5.1	4.3	3.3	.0067	-11.2	.0088	5.46	85.11	.779	.832
4	5.7	4.7	3.6	.0075	-10.8	.0098	5.97	84.28	.758	.809
5	6.3	5.2	4.1	.0083	-10.3	.0108	6.49	83.30	.737	.782
6	6.9	5.5	4.5	.0090	-10.0	.0118	6.96	82.65	.718	.764
7	7.5	5.9	4.8	.0098	-9.6	.0128	7.41	81.94	.700	.745
8	8.1	6.2	5.2	.0106	-9.3	.0138	7.83	81.26	.682	.726
9	8.7	6.6	5.5	.0114	-9.0	.0148	8.25	80.69	.666	.711
10	9.3	6.9	5.8	.0122	-8.7	.0158	8.69	80.16	.648	.696
11	9.9	7.3	6.1	.0129	-8.4	.0168	9.12	79.59	.630	.681
12	11.1	7.9	6.6	.0145	-7.9	.0188	9.91	78.55	.599	.652
13	12.3	8.3	7.0	.0161	-7.5	.0208	10.48	77.80	.576	.632
14	13.5	8.9	7.5	.0176	-7.0	.0228	11.23	76.85	.545	.605
15	15.4	9.4	8.0	.0199	-6.4	.0258	11.87	75.74	.520	.575
16	17.2	10.0	8.5	.0223	-6.0	.0288	12.55	74.94	.492	.552
17	19.0	10.3	8.9	.0246	-5.6	.0318	13.00	74.13	.475	.530
18	20.8	10.7	9.2	.0270	-5.3	.0348	13.41	73.53	.459	.513
19	23.2	11.1	9.5	.0301	-4.9	.0388	13.97	72.84	.438	.494
20	25.6	11.5	9.9	.0332	-4.5	.0428	14.41	72.09	.422	.472
21	28.6	11.8	10.2	.0371	-4.3	.0478	14.79	71.59	.408	.456
22	31.6	12.0	10.4	.0410	-4.1	.0528	15.04	71.22	.399	.447
23	35.8	12.2	10.7	.0464	-3.7	.0598	15.31	70.56	.390	.428
24	40.0	12.4	10.9	.0519	-3.5	.0668	15.62	70.14	.380	.415
25	44.8	12.7	11.2	.0581	-3.3	.0746	15.96	69.69	.368	.401
26	53.9	13.0	11.5	.0698	-3.0	.0896	16.40	69.09	.356	.381
27	65.8	13.3	11.8	.0853	-2.6	.1096	16.72	68.43	.346	.359
28	80.8	13.6	12.1	.1048	-2.4	.1346	17.07	67.95	.337	.341
29	101.8	14.0	12.4	.1321	-2.1	.1696	17.54	67.39	.324	.316
30	131.9	14.4	12.7	.1710	-1.8	.2196	18.09	66.75	.308	.284
31	176.9	14.9	13.1	.2294	-1.4	.2946	18.72	65.99	.285	.239
32	237.0	15.5	13.5	.3072	-1.0	.3946	19.47	65.27	.246	.190
33	297.1	16.1	13.7	.3851	-.7	.4946	20.19	64.72	.207	.144
34	387.2	16.8	14.1	.5019	-.4	.6446	21.07	64.06	.122	.080
35	477.3	17.3	14.3	.6187	-.2	.7946	21.69	63.63	.053	.033
36	597.4	17.5	14.5	.7744	-.0	.9946	21.98	63.36	.005	.000
37	717.5	17.5	14.5	.9301	-.0	1.1946	21.98	63.32	.012	.000
38	837.6	17.5	14.5	1.0858	-.0	1.3946	21.98	63.33	.012	.000

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00340 DELM = 1.325 REM = 1096.0
V RUN = 122771-3 CF/2 = .00262 DELM = 1.259 REM = 1112.0
PLATE = 23 UINF = 20.2 DEL2 = .1041 DEL3 = 2.202
X(IN) = 90.00 GH = 3.738 THETA = .1246 DEL4 = 9.230
K(E06) = -.1440 GAM = -.500 BETA = .099 M = 1.378

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T
1	.0	0.0	.0	0.0000	-15.5	0.0000	0.00	92.06
2	3.1	2.9	2.1	.0027	-13.6	.0059	3.24	84.71
3	3.6	3.4	2.4	.0031	-13.2	.0069	3.74	83.09
4	4.1	3.8	2.7	.0036	-12.9	.0079	4.22	87.41
5	4.7	4.3	3.1	.0040	-12.4	.0089	4.68	86.62
6	5.2	4.7	3.4	.0044	-12.1	.0099	5.13	85.96
7	5.7	5.0	3.8	.0049	-11.7	.0109	5.54	85.26
8	6.2	5.4	4.2	.0053	-11.3	.0119	5.94	84.59
9	6.8	5.8	4.5	.0058	-11.0	.0129	6.33	84.04
10	7.3	6.1	4.8	.0062	-10.7	.0139	6.74	83.44
11	7.8	6.5	5.1	.0067	-10.4	.0149	7.18	83.06
12	8.3	6.9	5.3	.0071	-10.2	.0159	7.57	82.56
13	9.4	7.5	6.0	.0080	-9.5	.0179	8.21	81.43
14	10.4	7.9	6.4	.0089	-9.1	.0199	8.72	80.63
15	11.5	8.5	6.9	.0098	-8.6	.0219	9.32	79.77
16	12.5	9.0	7.1	.0106	-8.4	.0239	9.87	79.15
17	13.6	9.3	7.6	.0115	-7.9	.0259	10.26	79.43
18	15.1	9.8	8.2	.0128	-7.4	.0289	10.77	77.53
19	16.7	10.2	9.4	.0142	-7.1	.0319	11.27	77.03
20	18.8	10.7	9.1	.0159	-6.4	.0359	11.82	75.83
21	21.4	11.2	9.8	.0182	-6.1	.0409	12.30	75.21
22	24.1	11.8	9.9	.0204	-5.6	.0459	12.85	74.40
23	27.7	11.9	10.3	.0235	-5.2	.0529	13.08	73.71
24	31.9	12.3	10.7	.0270	-4.8	.0609	13.53	73.05
25	37.2	12.7	11.1	.0314	-4.4	.0709	13.92	72.27
26	46.0	13.0	11.4	.0381	-4.1	.0859	14.35	71.73
27	58.1	13.5	11.9	.0492	-3.6	.1109	14.91	70.87
28	73.9	13.9	12.2	.0624	-3.3	.1409	15.27	70.27
29	92.2	14.2	12.5	.0779	-3.0	.1759	15.66	69.69
30	113.2	14.5	12.8	.0956	-2.7	.2159	15.99	69.24
31	139.4	14.8	13.1	.1179	-2.4	.2659	16.30	68.73
32	191.8	15.3	13.5	.1621	-2.0	.3659	16.69	68.01
33	257.3	15.9	13.9	.2174	-1.6	.4909	17.50	67.20
34	336.0	16.5	14.7	.2838	-1.2	.6409	18.13	66.57
35	414.6	17.0	14.6	.3502	-.9	.7909	18.71	65.93
36	519.4	17.6	15.0	.4389	-.5	.9909	19.36	65.36
37	624.3	18.1	15.2	.5273	-.3	1.1909	19.87	64.87
38	781.5	18.3	15.5	.6601	-.0	1.4909	20.22	64.48
39	938.9	18.4	15.5	.7930	-.0	1.7909	20.22	64.42
40	1096.0	18.4	15.6	.9258	-.0	2.0909	20.22	64.42

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00339 DELM = 1.223 REM = 1020.0
V RUN = 122771-3 CF/2 = .00286 DELM = 1.206 REM = 1256.0
PLATE = 21 UINF = 20.4 DEL2 = .0956 DEL3 = 2.029
X(IN) = 82.00 GH = 3.766 THETA = .1176 DEL4 = 7.641
K(E06) = -.1510 GAM = -.498 BETA = .095 M = 1.338

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	D+
1	.0	0.0	.0	0.0000	-15.4	0.0000	0.00	91.96	1.000	1.000
2	4.0	3.8	2.6	.0036	-12.9	.0075	4.22	87.33	.817	.876
3	4.6	4.0	3.0	.0041	-12.4	.0085	4.50	86.53	.805	.854
4	5.1	4.3	3.3	.0046	-12.0	.0095	4.84	85.82	.790	.834
5	5.6	4.7	3.8	.0051	-11.5	.0105	5.25	84.96	.773	.811
6	6.2	5.1	4.2	.0055	-11.2	.0115	5.69	84.31	.754	.793
7	6.7	5.5	4.5	.0060	-10.8	.0125	6.11	83.69	.735	.776
8	7.2	5.8	4.8	.0065	-10.5	.0135	6.50	83.15	.719	.761
9	8.3	6.4	5.4	.0076	-10.0	.0155	7.15	82.12	.691	.732
10	9.4	7.1	5.9	.0084	-9.4	.0175	7.97	81.14	.656	.705
11	10.4	7.9	6.4	.0094	-9.0	.0195	8.85	80.39	.618	.682
12	11.5	8.4	6.9	.0103	-8.5	.0215	9.42	79.41	.593	.657
13	12.6	8.8	7.3	.0113	-8.0	.0235	9.97	78.61	.575	.635
14	13.6	9.2	7.7	.0123	-7.7	.0255	10.33	77.98	.555	.618
15	15.2	9.8	8.1	.0137	-7.3	.0285	10.92	77.24	.530	.597
16	16.8	10.1	8.5	.0151	-6.8	.0315	11.35	76.43	.512	.574
17	18.4	10.5	8.9	.0166	-6.4	.0345	11.75	75.71	.495	.554
18	20.6	10.9	9.3	.0185	-6.1	.0385	12.21	75.06	.476	.536
19	24.3	11.5	9.9	.0219	-5.4	.0455	12.91	73.92	.447	.504
20	28.6	12.0	10.4	.0257	-5.0	.0535	13.39	73.11	.427	.481
21	33.9	12.4	10.9	.0305	-4.5	.0635	13.90	72.30	.406	.457
22	41.9	12.9	11.3	.0377	-4.1	.0785	14.44	71.44	.385	.431
23	49.9	13.2	11.6	.0449	-3.8	.0935	14.77	70.90	.373	.414
24	63.3	13.6	12.0	.0569	-3.4	.1185	15.19	70.24	.359	.393
25	82.0	14.0	12.4	.0737	-3.0	.1535	15.70	69.51	.342	.367
26	103.3	14.4	12.7	.0929	-2.7	.1935	16.09	69.00	.329	.347
27	130.0	14.7	13.0	.1170	-2.4	.2435	16.41	68.46	.319	.324
28	170.1	15.1	13.3	.1530	-2.0	.3185	16.92	67.80	.300	.292
29	223.4	15.6	13.7	.2010	-1.7	.4185	17.46	67.11	.278	.254
30	290.2	16.1	14.1	.2610	-1.3	.5435	18.13	66.44	.248	.212
31	370.3	16.7	14.5	.3331	-.9	.6935	18.71	65.72	.203	.158
32	477.0	17.4	14.8	.4291	-.5	.8935	19.45	65.09	.134	.105
33	583.8	17.9	15.1	.5252	-.3	1.0935	20.00	64.60	.069	.060
34	690.6	18.1	15.3	.6213	-.1	1.2935	20.31	64.24	.026	.022
35	858.7	18.2	15.4	.7654	.0	1.5935	20.46	64.09	.000	.000
36	1010.9	18.2	15.4	.9094	.0	1.8935	20.39	64.09	.013	.000

DATE = 012472 (-0.15, -0.004, -0.17)

T RUN = 12472-1 STNA = .00349 DELM = 1.356 REM = 910.0
V RUN = 122771-3 CF/2 = .00293 DELM = 1.289 REM = 1164.0
PLATE = 19 UINF = 20.9 DEL2 = .0836 DEL3 = 1.760
X(IN) = 73.00 GH = 3.752 THETA = .1071 DEL4 = 6.610
K(E06) = -.1760 GAM = -.527 BETA = .104 M = 1.390

I	Y+	U+	T+	Y/DEL3	-TD	Y	U	T	TAU+	D+
1	.0	0.0	.0	0.0000	-15.1	0.0000	0.00	91.72	1.000	1.000
2	3.9	3.7	2.6	.0039	-12.6	.0070	4.26	87.53	.815	.885
3	4.5	4.1	2.9	.0045	-12.4	.0080	4.78	86.76	.796	.864
4	5.0	4.5	3.2	.0050	-12.0	.0090	5.24	85.91	.777	.840
5	5.6	4.8	3.6	.0056	-11.6	.0100	5.56	85.17	.763	.820
6	6.1	5.2	3.9	.0062	-11.2	.0110	6.05	84.46	.742	.800
7	6.7	5.7	4.5	.0067	-10.8	.0120	6.57	83.51	.720	.774
8	7.2	6.0	4.7	.0073	-10.4	.0130	7.00	83.09	.702	.762
9	7.8	6.4	5.0	.0078	-10.1	.0140	7.40	82.44	.685	.744
10	8.3	6.7	5.3	.0084	-9.8	.0150	7.78	81.94	.669	.731
11	8.9	7.0	5.6	.0089	-9.5	.0160	8.12	81.43	.654	.716
12	10.0	7.5	6.2	.0100	-9.0	.0180	8.76	80.33	.627	.686
13	11.1	8.1	6.6	.0111	-8.5	.0200	9.36	79.56	.602	.665
14	12.2	8.5	7.2	.0122	-7.9	.0220	9.92	78.52	.579	.636
15	13.3	9.0	7.4	.0134	-7.7	.0240	10.47	78.04	.558	.623
16	14.4	9.4	7.8	.0145	-7.3	.0261	10.98	77.30	.540	.602
17	15.5	9.7	8.1	.0156	-7.0	.0280	11.25	76.76	.527	.587
18	16.6	10.0	8.4	.0167	-6.7	.0300	11.61	76.22	.509	.572
19	18.3	10.4	9.0	.0183	-6.3	.0330	12.12	75.51	.487	.552
20	20.0	10.8	9.2	.0200	-5.9	.0360	12.55	74.92	.468	.533
21	22.2	11.2	9.5	.0222	-5.6	.0400	13.03	74.22	.450	.516
22	24.4	11.4	9.9	.0244	-5.2	.0440	13.26	73.56	.441	.497
23	27.2	11.7	10.2	.0272	-4.9	.0490	13.64	72.93	.425	.479
24	29.9	12.1	10.4	.0300	-4.7	.0540	14.06	72.48	.405	.466
25	33.8	12.3	10.8	.0339	-4.3	.0610	14.32	71.95	.399	.447
26	39.4	12.6	11.1	.0394	-4.0	.0710	14.65	71.26	.386	.430
27	47.7	13.0	11.5	.0477	-3.7	.0860	15.09	70.63	.370	.410
28	56.0	13.3	11.9	.0560	-3.3	.1010	15.41	70.05	.358	.391
29	69.8	13.6	12.1	.0699	-3.0	.1260	15.76	69.45	.346	.370
30	83.7	13.9	12.7	.0837	-2.8	.1510	16.12	69.00	.335	.354
31	103.1	14.2	12.6	.1031	-2.5	.1860	16.50	68.46	.324	.332
32	125.2	14.5	12.9	.1253	-2.2	.2260	16.85	68.04	.312	.313
33	152.9	14.8	13.1	.1530	-2.0	.2760	17.14	67.53	.302	.289
34	205.3	15.4	13.6	.2044	-1.6	.3760	17.84	66.81	.276	.250
35	277.6	15.9	14.0	.2776	-1.1	.5010	18.50	65.99	.239	.198
36	360.7	16.6	14.3	.3607	-.8	.6510	19.26	65.42	.184	.154
37	443.7	17.1	14.6	.4438	-.5	.8010	19.90	64.98	.127	.108
38	554.5	17.7	14.9	.5547	-.2	1.0010	20.54	64.70	.057	.051
39	665.3	17.9	15.1	.6655	-.1	1.2010	20.84	64.00	.010	.016
40	776.1	18.0	15.1	.7763	.0	1.4010	20.91	63.88	.000	.000
41	779.3	18.0	15.1	.7795	.0	1.4068	20.91	63.88	.000	.000
42	862.4	18.0	15.1	.8626	.0	1.5568	20.91	63.88	.000	.000

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APPENDIX A

ANALYSIS OF TEMPERATURE DISTRIBUTION IN BOUNDARY LAYER TEMPERATURE PROBE

When any temperature sensing instrument is immersed in a fluid, the indicated temperature will differ from the true undisturbed fluid temperature. If one assumes that the temperature sensing instrument does not appreciably alter the temperature field at the location of the sensor, then the most common causes of error are radiation, velocity, and conduction losses. This analysis is aimed at estimating the conduction losses.

A thermocouple probe was used in this study and will be idealized as two butt welded cylinders in cross flow, as shown in Figure A-1. Each end of the probe is assumed to be maintained at temperature T_o, and the local gas temperature is named T_∞. Since the thermal properties of the two thermoelectric materials are different, the analysis will be divided into two regions. The applicable differential equation and boundary conditions for the two regions are as follows:

Region 1	Region 2	
$\frac{d^2\theta_1}{dx^2} - m_1^2\theta_1 = 0$	$\frac{d^2\theta_2}{dx^2} - m_2^2\theta_2 = 0$	
$\theta_1(-L/2) = \theta_o$	$\theta_2(L/2) = \theta_o$	(A-1)
$\theta_1(0) = \theta_2(0)$	$k_1 \frac{d\theta_1}{dx}\Big)_{x=0} = k_2 \frac{d\theta_2}{dx}\Big)_{x=0}$	

where $\theta = T - T_\infty$ and the fin parameters are given by

$$m_{1,2} = 2\sqrt{Nu_D\, k_f/k_{1,2}/D} \qquad \text{(A-2)}$$

The solution to (A-1) is

$$\frac{\theta_1(x)}{\theta_o} = A_3\cosh(m_1x) + \beta A_4\sinh(m_1x)$$

$$\frac{\theta_2(x)}{\theta_o} = A_3\cosh(m_2x) + A_4\sinh(m_2x) \qquad \text{(A-3)}$$

where

$$A_3 = \frac{\beta\sinh(p_1) + \sinh(p_2)}{\beta\cosh(p_2)\sinh(p_1) + \cosh(p_1)\sinh(p_2)} \qquad \text{(A-4)}$$

$$A_4 = \frac{\cosh(p_1) - \cosh(p_2)}{\beta\cosh(p_2)\sinh(p_1) + \cosh(p_1)\sinh(p_2)}$$

$$p_{1,2} = m_{1,2}L/2 \ , \quad \beta = \sqrt{k_2/k_1}$$

In order to compute the temperature distribution in the probe, the Nusselt number based on the wire diameter must be known. From Kreith [A-1], the Nusselt number for a cylinder in cross flow in air can be correlated by

$$Nu_D = C(Re_D)^n \qquad \text{(A-5)}$$

The thermal conductivity of the two thermoelectric elements must also be known. Two of the more common thermocouple pairs are Chromel/constantan and iron/constantan. From Benedict [A-2], the following thermal conductivity data was obtained:

iron	:	0.0096	Btu/ft-sec-^oF
constantan:		0.0038	"
Chromel	:	0.0031	"

Using the above data, the non-dimensional temperature distribution was computed for $D = 0.003$ inches, $L = 0.5$ inches, and an assumed velocity of 2 ft/sec. This velocity represents a lower bound on the velocity encountered in any of the experiments; hence, it represents the most severe test of the probe design. The computed results for the two different thermocouple types are shown in Figure (A-2). Since the thermal conductivities of the Chromel/constantan pair are more nearly equal than the iron/constantan pair, the Chromel/constantan probe has a more symmetrical temperature distribution. Also, the Chromel/constantan probe has a much smaller difference between the probe center temperature and the local gas temperature. Consequently, the Chromel/constantan probe was judged superior to the iron/constantan probe.

In order to estimate the actual temperature error, one must know both T_o and T_∞ . Since we do not know either of these two temperatures, let us assume that $T_o - T_\infty = 10°F$. From the data in Figure (A-2), the resulting thermocouple error would be $\Delta T = (10)\ (0.005) = 0.05°F$. This error is within the accuracy of the digital voltmeter used to measure the thermocouple output voltage. Hence, the Chromel/constantan probe should have negligible conduction errors at all conditions.

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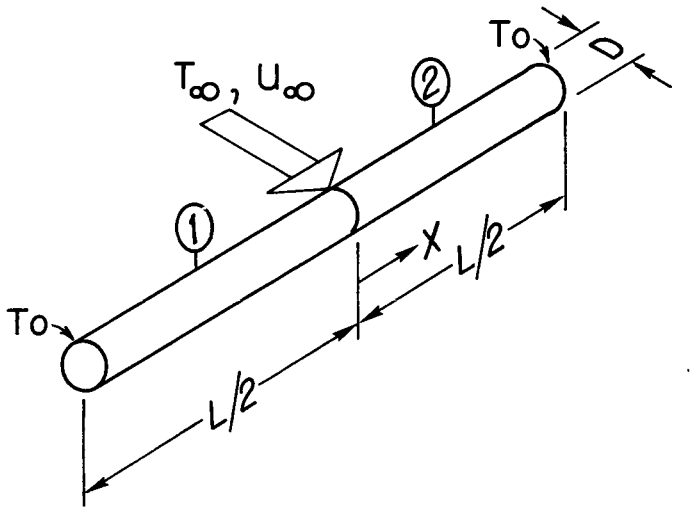

Figure A-1 Schematic of temperature probe

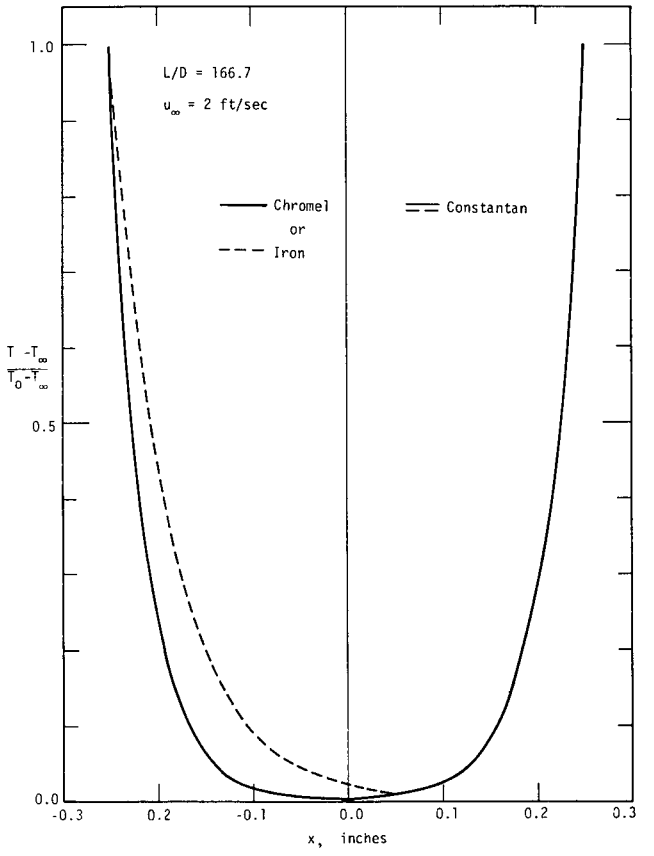

Figure A-2 Comparison of temperature distribution in Chromel/constantan probe with iron/constantan probe