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SHUTTLE VEHICLE AND MISSION
SIMULATION REQUIREMENTS REPORT

VOLUME III

10/20/72

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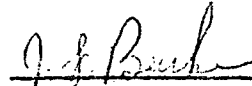
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SHUTTLE VEHICLE AND MISSION
SIMULATION REQUIREMENTS REPORT

VOLUME III

10/20/72



J. F. Burke
Principal Investigator
SMS Definition Study

This document is submitted in compliance with
Line Item No. 2 of the Data Requirements List
as Type I Data, Contract NAS 9-12836

SINGER COMPANY
SIMULATION PRODUCTS DIVISION

SHUTTLE VEHICLE AND MISSION
SIMULATION REQUIREMENTS REPORT

VOLUME III

Prepared by:

J. F. Burke

J. F. Burke
Principal Investigator
SMS Definition Study

Approved by:

C. Olasky
NASA Technical Manager

Contracting Officer

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SINGER COMPANY
SIMULATION PRODUCTS DIVISION

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PREFACE

This document is submitted in compliance with Line Item No. 2 of the Data Requirements List as Type I Data, Contract NAS9-12836. The document is divided into four volumes for ease of handling. The contents of each volume is defined as:

- Volume I: Includes sections entitled Introduction, Mission Envelope and Flight Dynamics which correspond to Sections 1.0, 2.0 and 3.0 of the Table of Contents.
- Volume II: Includes sections entitled Introduction and Shuttle Vehicle Systems which correspond to sections 1.0 and 4.0 to 4.18 of the Table of Contents.
- Volume III: Includes sections entitled Introduction and Shuttle Vehicle Systems which correspond to sections 1.0 and 4.19 to 4.22 of the Table of Contents.
- Volume IV: Includes sections entitled External Interfaces, Crew Procedures, Crew Station, Visual Cues and Aural Cues which correspond to sections 5.0, 6.0, 7.0, 8.0 and 9.0 of the Table of Contents.

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8.11.3 Illuminators/Non-Illuminators

8.11.4 Displacements

8.11.4.1 Translation

8.11.4.2 Rotation

8.11.5 Velocity

8.11.5.1 Translation

8.11.5.2 Rotation

8.11.6 Acceleration

8.11.6.1 Translation

8.11.6.2 Rotation

8.11.7 Assumptions

8.12 Ferry Flight Phase

8.12.1 Scene Content

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- 8.12.1.1 Horizon
- 8.12.1.2 Terrain
- 8.12.1.3 Celestial Bodies
- 8.12.1.4 Other Aircraft
- 8.12.1.5 Own Aircraft
- 8.12.2 Color
- 8.12.3 Illuminators/Non-Illuminators
- 8.12.4 Displacement
 - 8.12.4.1 Translation
 - 8.12.4.2 Rotation
- 8.12.5 Velocity
 - 8.12.5.1 Translation
 - 8.12.5.2 Rotation
- 8.12.6 Acceleration
 - 8.12.6.1 Translation
 - 8.12.6.2 Rotation
- 8.12.7 Assumptions

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9.0 Cue Requirements

9.1 Propulsion Cues

9.1.1 Main Rocket Engines

9.1.2 Solid Rocket Motors

9.1.3 Airbreathing Engines

9.1.4 Abort Solid Rocket Motors

9.2 System Equipment Cues

9.3 Aerodynamic Cues

9.4 Caution and Warning Cues

9.5 Landing Gear Cues

9.6 Malfunction Cues

1.0 Introduction

The objective of the Shuttle Vehicle and Mission Simulation Requirements report is to provide to NASA/MSC documentation of the requirements for faithful simulation of the Shuttle Vehicle, its systems, mission, operations and interfaces. To accomplish this objective the report was divided into eight topics which comprehensively cover the simulation requirements of the Shuttle mission and vehicle. The topics and their main objectives are summarized below.

Mission Envelope - This topic covers the space and atmospheric missions that are envisioned for the Shuttle program. The characteristics of each mission are described by an analysis of the mission phases, trajectory information, timelines and operations for nominal and abort conditions to the extent data was available.

Orbiter Flight Dynamics - This topic covers the flight regimes which the Shuttle vehicle will encounter in the accomplishment of its missions. The requirements were established in the following manner.

The vehicle configurations that must be simulated for horizontal and vertical test flights, operational space missions, atmospheric missions and abort modes were defined.

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The dynamics requirements were established by defining the forces and moments that will act on the vehicle during the entire mission envelope which include, propulsion, gravity, aerodynamic effects, payload effects, docking effects, staging effects, ground reactions and the dumping of material overboard. The translational equations of motion requirements were established by defining the vehicles, satellites and payloads whose state vectors must be calculated and by defining the coordinate systems, relative equations of motion and accuracy of the calculations. A similar analysis was performed for the rotational equations of motion. Mass property and ephemeris requirements were also identified.

Shuttle Vehicle Systems - The Shuttle vehicle systems required for simulation were identified and described. The descriptive data generated in this effort was primarily based on the North American Shuttle proposal. The Shuttle vehicle and its system configuration is currently in a state of flux and therefore the descriptive data

contained in this report undoubtedly will become out of date as the Shuttle program progresses. However, for the purposes of this study, the data is more than adequate to define simulator requirements and a baseline design when it is tempered with the past experience of Apollo and Gemini programs. A cross correlation between the NR definition of systems and LRU's and this report is shown in Table 1-1 for reference purposes.

External Interfaces - The external interfaces of the Shuttle vehicle were identified and a preliminary type interface description established. Due to the fact that for every external interface there also exists an equivalent on-board system, the descriptive data on the workings of the interfaces is contained in the Shuttle Vehicle Systems section of the report and cross references are provided in this section.

Crew Procedures - The actual crew procedures for the Shuttle system will not be available for many years. As a result the study concentrated on identifying tasks by mission phase and crew member and identifying the probable interfaces between work stations. The data used for the

analysis was a RTOP study by MacDonald-Douglas, conversations with George Franklin of NASA/MSC, past experience, and the requirements of the Shuttle vehicle & mission.

Crew Station -

The latest available data at the time of the writing of this report was used to identify the configuration of the Crew Station. The shape of the interior cabin, the location of the work stations and the allocation of the C&D panels by work station were established. Detailed data on the interior composition of the cabin is not currently available.

However, simulation requirements were identified based on past experience and accepted levels of fidelity for mission simulators.

Visual Cues -

The visual scene content was established for each of the mission phases. Attributes of the scene elements, to the extent feasible, were established and will be further defined in the SMSR report. The vehicle window configuration is not defined at this time but the best data available was utilized. The accelerations, velocities and displacements were established to the extent possible. Some

dynamics data was not available such as in the Abort phases of the mission. The missing information will be incorporated if it becomes available when the time frame and ground rules of the study or assumptions will be made.

Aural Cues -

The aural cues requirements associated with the mission and vehicle systems were identified and described. Detailed data on the characteristics of each sound was not available and probably will not be until the vehicle test program is in progress. This factor can be circumvented by specifying flexibility into the simulator aural cue equipment.

This report will be updated at the end of the study based on data received as of January 1, 1972.

Reference to study data sources are included in the margins and the text in order to facilitate update of this report. The numerical references are correlated with the data listing defined by Table 1-2.

TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: AVIONICS	EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks/Assumptions
	Star Sensor	3	4.9	ITT Model used on Aero Bee but does not meet proposed specs. Specs. and data required.
	Rate Sensor Package	3	4.9	Honeywell GG 1027 Model used on F-14 AFCS. Data and Specs. required
	Angle of Attack Transducer	3	4.9	Honeywell HG 280 used on DC 10.
	IMU	3	4.9	Singer model KT70 used on A7D/E.
	IMU Power Supply	3	4.9	Singer model KT70 used on A7D/E.
	TVC Monitor	2 (?)	4.9	No Data Exact function not known.
	Air Data Package	3 (?)	4.9, 4.9	Honeywell Model HG280 used on DC10.
	MPS TVC Drivers	3	4.3, 4.9	No Data Available
	Manual TVC/RCS Control	1	4.9	Honeywell Model BG 286 used on Apollo SC5.
	Aero Control Electronics Unit	?	4.9	Honeywell AFCS used on F-14.
	Horizon Sensor Assembly	3	4.9	Barnes Model 15-163
	OMS/TVC Driver Unit	3(?)	4.9	No Data Available

TABLE 1-1

SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: AVIONICS

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EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks / Assumptions
APS Driver/Monitor	3	4.9.	Honeywell Model BG.287 used on Apollo SCS.
Accelerometer Package	3	4.9.	Honeywell Model G.G.1026 used on F-14 AFCS
Aero Back-up Electronics	1	4.9.	No Data available
Subsystem Sequence Controller	2(?)	4.9	To be used for unmanned flights. No data available
Gyro Accelerometer Package	1	4.9.	No Data Available
Backup Optical Unit	1	4.9.	Apollo COAS
Throttle/Speed Brake Electronics	?		No Data
GN & C Computer	3(?)	4.1.8.3	IBM Model AP101 or Singer/Kearfott SKC2000.
Program I/O Processor	(?)		IBM SP1
FDAI/EDA	(?)		Honeywell JG 264/BG 285 used on Apollo SCS.
FCS Control Panel	(?)		Honeywell F-14

TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: ELECTRICAL POWER

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
BATTERY	2	4.1 ELECTRICAL POWER	NICKEL-CADIUM - 10 AMPHOUR - 28 VOLT
GENERATOR CONTROL UNIT	3	4.1 ELECTRICAL POWER	APU DRIVEN GENERATOR
TRANSFORMER RECTIFIER UNIT	3	4.1 ELECTRICAL POWER	150 AMP
REMOTE CONTROL CIRCUIT BREAKER	?	4.1 ELECTRICAL POWER	MAGNETIC LATCH - HERMETIC SEALED UNITS
REMOTE POWER CONTROLLER	4	4.1 ELECTRICAL POWER	MAGNETIC LATCH - HERMETIC SEALED UNITS
BATTERY CHARGES	1	4.1 ELECTRICAL POWER	CONSTANT CURRENT CHARGER - DUAL REDUNDANT OUTPUT
INVERTERS	4	4.1 ELECTRICAL POWER	30, 1250 VA, 115/200V, 400 HZ
SEQUENCERS	2	4.1 ELECTRICAL POWER	NO DATA AVAILABLE
CONTROL TRANSFORMER RECTIFIER	?	4.1 ELECTRICAL POWER	NO DATA AVAILABLE
FUEL CELL	3	4.1 ELECTRICAL POWER	7/10 KW RESTARTABLE - CRYOGENIC O2 and H2 30 VOLT OUTPUT
ALTERNATOR - GENERATOR	3	4.1 ELECTRICAL POWER	20/30 KVA APU DRIVEN SPRAY OIL COOLED WITH INTEGRATED GEARBOX
FUEL CELL HEAT EXCHANGER	3	4.1 ELECTRICAL POWER	

TABLE 1-1

SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: MECHANICAL POWER

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EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
AUXILLARY POWER UNITS	4	4.2.1 AUXILIARY POWER UNITS	200 HORSEPOWER - USES HYDRAZINE
HYDRAZINE TANK	4	4.2.1 AUXILIARY POWER UNITS	NO DATA AVAILABLE
HELIUM TANK	4	4.2.1 AUXILIARY POWER UNITS	NO DATA AVAILABLE
HEAT EXCHANGER	4	4.2.1 AUXILIARY POWER UNITS	NO DATA AVAILABLE
HYDRALIC PUMPS	8	4.2.2 HYDRALIC POWER SYSTEM	3000 PSI
ALTERNATOR	3	4.2.1 AUXILIARY POWER UNITS	400 HZ, 30, 20/30 KVA

TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: OPERATIONAL INSTRUMENTATION		THE SINGER COMPANY SIMULATION PRODUCTS DIVISION BINGHAMTON, NEW YORK		DATE 10/20/72	PAGE NO. 1-10
EQUIPMENT		NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks	REV.
PILOT VOICE RECORDER	1	4.11.1 RECORDERS			
SWITCH SCAN MULTIPLEXER	12	FIGURE 4.11-1			
CAUTION AND WARNING	2	FIGURE 4.11-1, 4.11.4	AUTONETICS - APOLLO TYPE (NEW ITEM)		
CRASH RECORDER	1	4.11.1 RECORDERS	SUNSTRAND, ECHO SCIENCE, OR DAVOLL FERRY USE ONLY		
SIGNAL CONDITIONING UNIT-DFI	17	4.11.2 SENSORS AND SIGNAL CONDITIONING	SAT/APOLLO AUTONETICS SCE		
TIMING UNIT (MTU)	2	FIGURE 4.11-1	APOLLO CTE, GENERAL TIMC		
LOOP RECORDER	1	FIGURE 4.11-1 4.11.1 RECORDERS	SUNSTRAND, ECHO SCIENCE, OR DAVOLL (5 MINUTE PLAYBACK)		
PCM RECORDER - PAYLOAD	1	FIGURE 4.11-1 4.11.1 RECORDERS	SUNSTRAND, ECHO SCIENCE OR DAVOLL (MAINT. AND PAYLOAD)		
OPER. TRANSDUCERS	2359 DFI 2803 DFI	FIGURE 4.11-1 4.11.2 SENSORS AND SIGNAL CONDITIONING	VARIOUS MAKES		
PCM REMOTE UNIT DFI	1	FIGURE 4.11-1	SCI, TELEDYNE		
PCM MASTER UNIT - DFI	2	FIGURE 4.11-1	DFI ONLY SCI, TELEDYNE		
GROUND CHECKOUT DECODER	?	?	MAY NOT EXIST		

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TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: OPERATIONAL INSTRUMENTATION	EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
	GN&C COMPUTER 64K	2?	4.18.3	IBM MODEL API01 OR SINGER/KEARFOTT SKC 2000
	INPUT-OUTPUT BUFFER	?	4.18.2.9.3/ 4.18.2.9.4	SP-1 COMPUTER STRUCTURES SKYLAB POWER SUPPLY, API/SPI
	MDE UNIT	?	4.19-4.19-7	IBM SPI
	MAGNETIC TAPE READER	?	4.19.2	NO DATA AVAILABLE
	TAPE CONTROL ELECTRONICS	?	4.19.2	NO DATA AVAILABLE
	CRT DISPLAY UNIT	8?	4.19.2.1	IBM-F14 TYPE HEAD WITH ADDITION OF A READ/WRITE REFRESH BUFFER, A SYMBOL GENERATOR, ANALOG AND DIGITAL CONTROL LOGIC, D/A'S AND POWER SUPPLIES
	DFI TIMING UNIT	1		NO DATA AVAILABLE
	WIDEBAND RECORDER	1		NO DATA AVAILABLE
	FREQUENCY MULTIPLEXER	3		NO DATA AVAILABLE
	PCM RECORDER DFI	1		NO DATA AVAILABLE
	PCM RECORDER MAINTENANCE	1		NO DATA AVAILABLE

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SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: OPERATIONAL INSTRUMENTATION

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
PCM MASTER UNIT - OFI	2		NO DATA AVAILABLE
PAYLOAD DATA INTERLEAVER	2		NO DATA AVAILABLE
PCM REMOTE ACQUISITION UNIT	24		NO DATA AVAILABLE
DEDICATED SIGNAL CONDITIONER	6		NO DATA AVAILABLE
COMMAND ACQUISITION UNIT	1		NO DATA AVAILABLE

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TABLE 1-1

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SYSTEM: D&C

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
VERTICAL SPEED	2	Note: The SV&MSR did not address detailed D&C instruments due to the lack of film data	BENDIX E-C, AAK-23/A24G-17A
BARO ALTITUDE	2	NO DATA AVAILABLE	AEROSONICS, AAU-16/A
AS/MACH	2	NO DATA AVAILABLE	BENDIX E-C, ASK-14/A24G-18
DAI (3 AXIS)	2	NO DATA AVAILABLE	MODIFIED APOLLO CM FDAI
SI	2	NO DATA AVAILABLE	BENDIX E-C, ACA AQU-4A
AS/SAT	1	NO DATA AVAILABLE	NO DATA AVAILABLE
ACCELEROMETER	2	NO DATA AVAILABLE	NO DATA AVAILABLE
G POSITION	1	NO DATA AVAILABLE	3 DISPLAYS - LEFT, RIGHT, NOSE
DCS PRESSURE	3	NO DATA AVAILABLE	DOUBLE POINTER
IMS PC	1	NO DATA AVAILABLE	NO DATA AVAILABLE
IMS FUEL	1	NO DATA AVAILABLE	NO DATA AVAILABLE
IMS OX	1	NO DATA AVAILABLE	NO DATA AVAILABLE

TABLE 1-1

SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: D&C

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EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
EVENT TIMER	2	NO DATA AVAILABLE	NO DATA AVAILABLE
HYD. PRESSURE	1	NO DATA AVAILABLE	NO DATA AVAILABLE
MPS PC	1	NO DATA AVAILABLE	NO DATA AVAILABLE
MPS LH2/L02	1	NO DATA AVAILABLE	NO DATA AVAILABLE
EXT. TANK QUANTITY	1	NO DATA AVAILABLE	NO DATA AVAILABLE
ISS DISAGREE	2	NO DATA AVAILABLE	NO DATA AVAILABLE
CMD DISAGREE	2	NO DATA AVAILABLE	NO DATA AVAILABLE
DRIVER FAIL	2	NO DATA AVAILABLE	NO DATA AVAILABLE

TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: COMMUNICATION AND TRACKING		THE SINGER COMPANY SIMULATION PRODUCTS DIVISION BINGHAMTON, NEW YORK		DATE 10/20/72	PAGE NO. 1-15
EQUIPMENT		NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks	REV.
SGLS INTERROGATOR	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
VHF TRANSCEIVER	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
ATC TRANSPONDER	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
SGLS TRANSPONDER	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
SGLS DECODER	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
USB TRANSPONDER	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
SIGNAL PROCESSOR	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
AUDIO CONTROL CENTER	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
TACAN TRANSPONDER	3	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
COMMAND DECODER	2	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
RADAR ALTIMETER	3	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		
WIDEBAND TRANSMITTER S-BAND	1	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE		

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TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: COMMUNICATION AND TRACKING	EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
	S-BAND ANTENNA	4	4.10 COMMUNICATIONS AND TRACKING	HELIX IN CAVITY (RHCP)
	C-BAND ANTENNA	6	4.10 COMMUNICATIONS AND TRACKING	HORN (LP) FOR RADAR ALTIMETER
	L-BAND ANTENNA	1	4.10 COMMUNICATIONS AND TRACKING	ANNULAR SLOT (VP) FOR TACAN AND ATC
	UHF/VHF ANTENNA	3	4.10 COMMUNICATIONS AND TRACKING	HP DUAL CAVITY FOR ILS
	VHF ANTENNA	2	4.10 COMMUNICATIONS AND TRACKING	HELIX IN CAVITY (RHCP)
	VHF ANTENNA	1	4.10 COMMUNICATIONS AND TRACKING	TOP CAP (VP)
	VHF ANTENNA	1	4.10 COMMUNICATIONS AND TRACKING	SPIRAL (VP)
	L-BAND ANTENNA	2	4.10 COMMUNICATIONS AND TRACKING	HELIX IN CAVITY (RHCP) FOR TACAN
	L-BAND ANTENNA SELECTOR	1	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE
	VHF ANTENNA SELECTOR	1	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE
	S-BAND ANTENNA SELECTOR	1	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE
	CCTV CAMERA (B&W)	4	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE

TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: COMMUNICATION AND TRACKING	EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
	TV CAMERA - COLOR	1	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE
	DFI TRANSMITTER	1	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE
	ILS RECEIVER	3	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE
	SECURE TERMINAL	4	4.10 COMMUNICATIONS AND TRACKING	NO DATA AVAILABLE

TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: AIRBREATHING PROPULSION

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
TURBOFAN ENGINE	4	4.6 AIRBREATHING PROPULSION SYSTEM	P&W F401-PW-400 MODIFIED
FUEL TANK	1,2,or3	4.6 AIRBREATHING PROPULSION SYSTEM	22,565 LBS FOR EACH TANK

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TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: SOLID ROCKET MOTORS

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
MOTOR	2	4.7.1 MAIN SRM	SOLID PROPELLANT 156"
MOTOR	12	4.7.1 MAIN SRM	SOLID PROPELLANT 27K LBS @ 2 SECONDS
MOTOR	2	4.7.2 ABORT SOLID ROCKET MOTOR	SOLID PROPELLANT 385,000 LBS AVERAGE @ 21 SECONDS
MOTOR	2	4.7.3 DEORBIT SRM FOR EXTERNAL TANK	SOLID PROPELLANT 18,500 LBS @ 37 SECONDS

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TABLE 1-1
SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: EXTERNAL TANK

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
OXYGEN TANK - LIQUID	1	4.8.1 STRUCTURE	
HYDROGEN TANK - LIQUID	1	4.8.1 STRUCTURE	
BATTERY	2	4.8.4 AVIONICS	
ORDINANCE TIMING SYSTEM (DEORBIT AVIONICS)	1	4.8.4 AVIONICS	
RANGE SAFETY AVIONICS	1	4.8.4 AVIONICS	

TABLE 1-1

SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: MAIN PROPULSION SYSTEM

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
MPS ENGINE INTERFACE UNIT	3	4.3 MAIN PROPULSION SYSTEM	NO DATA AVAILABLE
MPS CONTROLLER	3	4.3 MAIN PROPULSION SYSTEM	NO DATA AVAILABLE
FUEL PREBURNER	3	4.3 MAIN PROPULSION SYSTEM	NO DATA AVAILABLE
OXIDIZER PREBURNER	3	4.3 MAIN PROPULSION SYSTEM	NO DATA AVAILABLE
MAIN ENGINE	3	4.3 MAIN PROPULSION SYSTEM	470K VAC THRUST
ENGINE ACTUATOR	6	4.3.5 ENGINE ACTUATOR	NO DATA AVAILABLE

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TABLE 1-1

SPACE SHUTTLE ON-BOARD EQUIPMENT CROSS REFERENCES

SYSTEM: ORBITAL MANEUVERING SYSTEM (OMS)

EQUIPMENT	NUMBER OF UNITS	SV & MSR Paragraph Number and Title	Remarks
ENGINE	2	4.5 ORBITAL MANEUVERING SYSTEM	5000 LBS VAC
TANK OXIDIZER	2	4.5 ORBITAL MANEUVERING SYSTEM	12,200 LBS MAX. - NITROGEN TETROXIDE
TANK FUEL	2	4.5 ORBITAL MANEUVERING SYSTEM	12,200 LBS MAX. - MONOMETHYLHYDRAZINE
HELIUM TANK	2	4.5 ORBITAL MANEUVERING SYSTEM	3200 PSIA

DOC. SRCE	DOC. DATE	NUMBER	REV	DOCUMENT TITLE	DATE RECD	LOCN	SEQ NO.
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SORTED BY INDEX NUMBER

DATA REFERENCES
SHUTTLE MISSION SIMULATOR STUDY

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GE	15MR72	MSC-03824		SS PHASE B EXTENSION FINAL REPORT-PAYLOAD IMPACT V2A	15JE72	Hb	002
NA	25FF72	FM347234		PAN AMERICAN APPROACH TO SHUTTLE CREW SEL/TRNG/ASSIGN	15JE72	Hb	003
NA	15MA72	MSC-04217	C	SPACE SHUTTLE ON+C DESIGN EQUATION DOCUMENT	15JE72	Hb	004
GP	15MR72	MSC-03824		SS PHASE B EXTENSION FINAL REPORT-MASS PROPERTIES V3	15JE72	Hb	005
GE	15MR72	MSC-03824		SS PHASE B EXTENSION FINAL REPORT-EXECUTIVE SUMMARY V1	15JE72	Hb	006
ME	15MR72	MDC-E0558		TECHNICAL REPORT SYSTEM + ORBITER PART 2 VOL 1	15JE72	Hb	007
ME	15MR72	MDC-E0558		TECHNICAL REPORT SYSTEM + BOOSTER PART 2 VOL 2	15JE72	Hb	008
ME	15MR72	MDC-E0558		FINAL MASS PROPERTIES REPORT PART 4	15JE72	Hb	009
MD	15MR72	MDC-E0558		DEVELOPMENT REQUIREMENTS PART 3	15JE72	Hb	010
ME	15MR72	MDC-E0558		TECHNICAL REPORT-MMC ACTIVITY PART 2 VOL 3	15JE72	Hb	011
NR	15MR72	MSC-03332		SS PHASE B FINAL REPORT-TECHNICAL SUM.ADD.A-BOOSTER	15JE72	Hb	012
LC	15MR72	NAS826362		SPACE SHUTTLE CONCEPTS TECHNICAL REPORT VOL 4	15JE72	Hb	013
ME	15MR72	MDC-E0558		EXECUTIVE SUMMARY PART 1	15JE72	Hb	014
NR	15MR72	MSC-03333		SS PHASE B FINAL REPORT-MASS PROPERTIES STATUS REPORT	15JE72	Hb	015
GR	15MR72	MSC-03824		SS PHASE B FINAL REPORT-TECHNICAL REPORT V2	15JE72	Hb	016
NA	04FA72	EG13728		SPACE SHUTTLE GUIDANCE AND NAVIGATION REVIEW	15JE72	Hb	017
BC	04JA72			STATE OF MOTION SYSTEM REQ. FOR SIM. OF ADV. SPACECR.	15JE72	Hb	018
NA	15MR72	MSC-06720		SOURCE DOCUMENTATION LIST VOL 2 CAT 2	15JE72	Hb	019
NA		RFP		SPACE SHUTTLE PROGRAM REQUEST FOR PROPOSAL PHASE CD	15JE72	Hb	020
NA	14JA72		A	SPACE SHUTTLE AVIONICS CONFIGURATION DEFINITION DATA	15JE72	Hb	021
MM	0C71	MSC-05218		PREL. DES. OF SHUTTLE DOCKING AND CARGO HANDLING SYS.	15JE72	Hb	022
NA	15MR72			DATA PKG FOR SHUTTLE TRAINING AIRCRAFT DEFINITION	15JE72	Hb	023
NP	15MR72	MSC-03332		SS PHASE B FINAL REPORT-EXECUTIVE SUMMARY V1	15JE72	Hb	024
NP	15MR72	MSC-03332		SS PHASE B FINAL REPORT-TECHNICAL SUMMARY V2	15JE72	Hb	025
NA	15NV71	MSC-03698		SS ORBITER ON+C S/W FUNCT.REQ. VERTICAL FLIGHT OPNS.	15JE72	Hb	026
NA	JA70	NHB8040.2		APOLLO CONFIG. MGT. MANUAL	07JL72	Hb	027
NA	01DC71	MSC-04217	B	SHUTTLE GNC DESIGN EQNS VOL.1	15JE72	Hb	028
NA	01DC71	MSC-04217	B	SS ON+C DESIGN EQUATIONS-PREFLIGHT THRU ORBIT INS. V2	15JE72	Hb	029
NA	01DC71	MSC-04217	B	SS ON+C DESIGN EQUATIONS-ORBITAL OPERATIONS V3	15JE72	Hb	030
NA	01DC71	MSC-04217	B	SHUTTLE GNC DESIGN EQUATIONS VOL 4 DEORBITAL ATM OPNS	15JE72	Hb	031
NA	15JE72		B	PROGRAM PLAN C OLASKY	15JE72	Hb	032
NA	15MR72	MSC-06720		SOURCE DOCUMENTATION LIST VOL 1 CAT 1	15JE72	Hb	033
NA		INDEX		SPACE SHUTTLE DATA LIST	15JE72	Hb	034
NR	12NV71	NAS910960		TECHNICAL REPORT PHASE B VOL 1	15JE72	Hb	035
NR	12NV71	NAS910960		TECHNICAL REPORT PHASE B VOL 2	15JE72	Hb	036
NR	25JF71	NAS910960		TECHNICAL SUMMARY ORBITER DEFINITION VOLUME 2 PART1	15JE72	Hb	037
NR	25JF71	NAS910960		TECHNICAL SUMMARY ORBITER DEFINITION VOLUME 2 PART2	15JE72	Hb	038
GF	12NV71	NAS911160		SPACE SHUTTLE LOW COST/RISK AVIONICS STUDY	15JE72	Hb	039
GP	15DC71	NAS911160		SHUTTLE SYSTEMS EVALUATION ORBITER DATA VOLUME 3	15JE72	Hb	040
NP	08MR72	NAS910960		SPACE SHUTTLE PHASE B FINAL AVIONICS REPORT	15JE72	Hb	041
NA	21AF71	NAS826167		ENGINE DESIGN DEFINITION REPORT AVIONICS-PHASE CD	30JE72	Hb	042
ME	01AF72	MDC-E0558		SIMULATION RESULTS REPORT	28JE72	Hb	043
ME	30AF72	MDC-E0573		DISPLAYS + CONTROLS FUNCTIONAL REQUIREMENTS SPEC.	28JE72	Hb	044

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NA	00AF72	MSC INDEX		MSC INFORMATION RETRIEVAL SYSTEM	27JE72	H	045
MC	010C71	MDC-E0484		CREW INTERFACE DEFINITION STUDY PHASE 1	28JE72	H	046
AF	00AF66	FTCTR686		FACILITY DEFINITION STUDY FOR UNIV FLIGHT SIMUL/TRNR	15JE72	H	047
MI	00JE72	E-2687		EVAL OF SYNC/ASync EXECUTIVE SYSTEM FOR SPACE SHUTTLE	06JL72	H	046
NA	01MA71	MSC-02542		TYP. SHUTTLE MISSION PROFILES + AIT. TIMELINES V4	11JL72	H	049
NA	27AG71	T71-14939		REPPES. REENTRY MISSION PROF. FOR DELTA WING ORBITER	11JL72	H	050
NA	31JA72	NASW-2081		ECONOMIC ANALYSIS SHUTTLE SYSTEM VOL 2	11JL72	H	051
LC	15MV71	NAS826362		ALTERNATE CONCEPT + DEFINITION-SKM BOOSTERS PART 3	11JL72	H	052
LC	15MV71	NAS826362		ALTERNATE CONCEPT + DEFINITION-AVIONICS PART 4	11JL72	H	053
NA	20JE72	MSC-07034		FIRST VERTICAL FLIGHT TEST MISSION	14JL72	H	054
NA	15JE72	MSC-07050		OPTIMUM SRM THROUST PROFILE-MINIMUM GLOW	14JL72	H	055
NA	30MA72	MSC-07057		POST BLACK OUT GNC ANALYSIS OF ORBITER SPACE SHUTTLE	14JL72	H	056
MF	15MR72	MDC-E0558		DESIGN DATA BOOK-PROGRAM AND SYSTEM BASELINE PARTS V1	14JL72	H	057
MC	15MR72	MDC-E0558		DESIGN DATA BOOK-DRAWINGS VOL 2	14JL72	H	058
MF	15MR72	MDC-E0558		DESIGN DATA BOOK-ORBITER AERO VOL 3	14JL72	H	059
MF	15MR72	MDC-E0558		DESIGN DATA BOOK-BOOSTER AERO VOL 4	14JL72	H	060
NA	11JI72	470 ICU14		MAIN ENGINE AVIONICS ICU-ROCKETDYNE	20JL72	H	061
NR	14JE72	A1AA71639		ROCKETDYNER SPACE SHUTTLE MAIN ENGINE	20JL72	H	062
NA	MA71	MSC-04400		RECOMMENDED SPACE SHUTTLE COORDINATE SYSTEMS STANDARD	26JL72	H	063
LC	26FE71	MSC02553		ADVANCED SW TECHNIQUES FOR SHUTTLE DATA MAN. SYSTEM	25JL72	H	064
SK	30NV70	SKC-2000		AEROSPACE DIGITAL COMPUTER-SKC 2000	07JL72	H	065
NA	05AF72	MSC067215		SOLID STATE TRANSDUCER DEVELOPMENT/NEW HAND CONTROL	28JL72	H	066
NA	12MA72	MSC-07151		FLYING QUALITY REQUIREMENTS CLOSED LOOP FLY BY WIRE	26JL72	H	067
NA	21DC70	A71-25530		SUPPLY + RESUPPLY OF STATIONS IN SYNCHRONOUS ORBITS	25JL72	H	068
BA	15MR72	A1AA71313		INSTRUMENTATION REQUIRED FOR SHUTTLE MAINT + OPERATION	25JL72	H	069
NA	05AF72	MSC-06766		PERFORMANCE REQUIREMENTS-SHUTTLE FUNCTIONAL SIMULATOR	25JL72	H	070
NA	13JI72	CE2-72M86		HALF JUNCTION STUDY (RELATIVE TO HPTS)	26JL72	H	071
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MF	30JF71	MDC-E0308		B TECHNICAL SUMMARY ORBITER PT11-2A	07JL72	B	073
MF	30JF71	MDC-E0308		B TECHNICAL SUMMARY ORBITER PT11-2B	07JL72	B	074
MC	30JE71	MDC-E0308		B TECH. SUMMARY BOOSTER PART 11-3	07JL72	B	075
MC	30JE71	MDC-E0308		B TECH. SUMMARY BOOSTER PT 11-3 APP	07JL72	B	076
NR	JI70	MSC-00706		SP. STA. C/D CREW TNG PLAN B DEFIN.	07JL72	B	077
NR	25JE71	MSC-03307		SHUTTLE B EXEC. SUMMARY VOL 1	07JL72	B	078
NR	25JE71	MSC-03308		PROGRAM MGT. PLAN FOR PHASE C/D	07JL72	B	079
NR	25JF71	MSC-03327		EXTERNAL H2 TANK STUDY SUMMARY VOL1	07JL72	B	080
NA	17DC70	MSC-03793		SHUTTLE ENG. SIMULATION SURVEY	07JL72	B	081
GP	06JL71	MSC-03809		ALTERNATE CONCEPTS-EXEC. SUM. PART 1	07JL72	B	082
GP	06JL71	MSC-03810		ALT. CONCEPTS. TECH. SUM. SHUT. DEF. P2V1	07JL72	B	083
GP	06JI71	MSC-03811		ALT. CONCEPTS. ENG. DEV. PLAN-ORBITER V2	07JL72	B	084
NA		MSC-04240		PRELIM. MISSION PROFILE-DESC. + LAND	07JL72	B	085
NA	27AF71	MSC-04243		PRE-ENTRY TGT. PLANNING-ORBITER	07JL72	B	086
NA	24AG70	17618H004 0		ENTRY CORRIDORs FOR HI L/D (TRW)	07JL72	B	087
NA	06AF72			FLIGHT PERS. COMP. + SIMULATOR RES-INF	07JL72	B	088
NA	08JF72	C. GLASKY		PROGRAM PLAN-PROCEDURES DEVELOPMENT	28JE72	H	089
SI	28JA72	ER-094		HPTS PROJECTED CONFIGURATION	JE72	H	090
NR	19JF72			AVIONICS WEEK-LAR PHASE C/D CONFIG.	19JE72	B	091
NR				PRELIM NAR CONTROLS DISPLAY LAYOUT		B	092
SI	15JL72	SSPEMM31		SSPE DATA BOOK		B	093
NA	30AF71	MSC-04347		SHUTTLE TOUCHDOWN REQUIREMENTS		B	094

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AF	00MR72	HUMRR0772		TRANSFER OF INET TRAINING + SYNTH FLIGHT TRAINING SYS	28JL72	H	095
NA	30JE70	TMX-2101		FLIGHT TEST RESULTS FOR SPACE SHUTTLES (LIFT BODIES)	28JL72	H	096
NA	11DC70	MSC-02542		TYPICAL SHUTTLE MISSION PROFILES + ATT TIME LINE VOL 3	28JL72	H	097
NA	07AG70	NAS910456		STUDY OF PERSONAL HYGIENE FOR FUTURE MANNED MISSIONS	28JL72	H	098
NA	01CC71	MSC-C-005		GEN SPEC CONTROLS, FUNC DESIGN REUMTS MANNED SPACECRFT	28JL72	H	099
NA	01NV71	MSC-0-007		GEN SPEC DISPLAYS, FUNC DESIGN REUMTS MANNED SPACECRFT	28JL72	H	100
NA	30DC70	MSC-03779		HOUSEKEEPING CONCEPTS-WASTE CONTROL TASKS + SYS VOL 1	28JL72	H	101
NA	17MR71	MSC-04062		ORBITER FLIGHT TECH + LANDING PT SUBORBIT ABORT CNTRL	28JL72	H	102
NA	00FF71	NAS9-4045		MAN ROLE INTEG VEHICULAR INFORMATION MANAGEMENT SYS	28JL72	H	103
NA	25JE71	MSC-03306		ICD FOR SPACE SHUTTLE SYSTEM	28JL72	H	104
NA	27JL71	MSC-04711		ORBITER FLIGHT TECHNIQUES FOR FLYBACK ABORTS	28JL72	H	105
NA	11NV71	MSC-05148		PAYLOAD CG ANALYSIS FOR SHUTTLE, SIDE-BY-SIDE LOADING	28JL72	H	106
NA	10JA72	MSC-05812		PAYLOAD CG ANALYSIS FOR SHUTTLE, END-TO-END LOADING	28JL72	H	107
NA	15DC71	MSC067143		PILOTTED SIMUL STUDY-UNPOWERED CROSSWIND LANDINGS	28JL72	H	108
NA	00JI71	NAS911140		CHECKOUT SYS SUMMARY REPORT/UNIV CONTROL-DISPLAY CONS	28JL72	H	109
NA	00DC71	NAS912420		TIFS SIMUL OF SSV LANDING APPROACH-MONTHLY REPORT	28JL72	H	110
NA	15DC71	NAS912218		DEV OF OPTIMUM SIMUL OF SPACE STATION COMM TECHNIQUE	28JL72	H	111
NA	00DC71	NAS912200		SSV ENTRY SIMULATION	28JL72	H	112
NA	00DC71	NAS910960		STUDY ANALYSIS REPORT OF SSV MANUAL DOCKING SIMULATOR	28JL72	H	113
NA	24SF71	AD444403		AIRCRAFT FLIGHT TEST INSTR ANALYSIS FOR SSV	28JL72	H	114
NA	00FF72	NAS912420		TIFS SIMUL OF SSV LANDING APPROACH-MONTHLY REPORT	28JL72	H	115
NA	15DC71	NAS9-2129		INTEG SPACE PROGRAM + VEHICLE SYS ANALYSIS-STUDY B	28JL72	H	116
NA	00AG71	NAS9-2129		INTEG OPERATIONS/PAYLOAD/FLEET ANALYSIS VOL 2 PAYLOAD	28JL72	H	117
NA	00AG71	NAS9-2129		INTEG OPERATIONS/PAYLOAD/FLEET ANALYSIS VOL 3 MISSION	28JL72	H	118
NA	00AG71	NAS9-2129		INTEG OPERATIONS/PAYLOAD/FLEET ANALYSIS VOL 3 EXEC SM	28JL72	H	119
NA	15JA72	MSC06-723		SIMUL EVAL OF MANUAL CONTROL MODES-UNPOWERED DELTA/WG	28JL72	H	120
NA	02JF71	NAS910960		SPACE SHUTTLE OPERATIONS REVIEW	28JL72	H	121
NA	05JA71	NAS910960		SPACE STATION DOCKING/PAYLOAD XFER TRADE STUDY RESULT	28JL72	H	122
TR	17FF72	724910432		DEF OF ORBITER FLIGHT ENVELOPE + INVESTIGATION FLT-TS	28JL72	H	123
TR	25FF71	717251322		SSV COMMUNICATIONS COVERAGE V-POLAR ORBIT	28JL72	H	124
NA	10JA72	MSC0672-5		PROJECT SPACE SHUTTLE-SSV ENTRY SIMULATION	28JL72	H	125
NR	02AF71	SV71-13		SSV CREW STATION REVIEW NO. 2	28JL72	H	126
NA	25JE71	MSC-03310		SSV OPERATIONS PLAN FOR PHASE C/D VOL. 2 ORBITER	28JL72	H	127
NA	00MA71	MSC-04411		SSV PAYLOAD HANDLING + DOCKING	28JL72	H	128
NA	10AF71	A71-36409		ORBITAL CARGO TRANSFER SYSTEM	28JL72	H	129
NA	00JI71	NAS911948		SPACE STATION BUILDUP SIMULATION-FINAL REPORT	28JL72	H	130
NA	10FF71	SSPE-27		SSV EVALUATION OF FOUR SIDESTICK CONTROLLERS ON SIMUL	28JL72	H	131
NA	16MA72	MSC-04813		SSV PERFORMANCE CAPABILITIES-	01AG72	H	132
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NA		RFP INFO		SSV PROPOSER DOCUMENTATION INFORMATION	01AG72	H	134
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NR	19MA71	NAS910960		FLIGHT STATION + VISION PLOT-ORBITER	01AG72	H	136
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NA	00JF71	N70-40951		SPACE XPORTATION SYS TECH VOL 6 INTEGRATED ELEC/POWER	03AG72	H	140
NA	00JL72	DCPS-1		CREW PROCEDURES TASK DESCRIPTION-POST ABORT	03AG72	H	146
NR	04FE71	SV71-13		SSV CREW STATION REVIEW NO 2	03AG72	H	147
NR	17MA71	VA70-6001		CREW COMPARTMENT-DELTA ORBITER	04AG72	Hb	148
NR	14JF71	VA70-3103		CREW COMPARTMENT-AND IVA TUNNEL STRUCTURE	04AG72	Hb	149
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NA	24MR72	MSC-06747		GNC S/W FUNCTIONAL REQ. FOR FLIGHT OPERATIONS	07AG72	Hb	152
NR	21MR67			CREWMAN OPTICAL ALIGNMENT SIGHT ACROSS APOLLO SPEC	09AG72	Hb	153
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MI	16FE72	23A 11-72		ENTRY + TERMINAL NAV USING MLS OR AILS + VOR/DME	10AG72	Hb	157
MI	040C71	23A 49-71		ENTRY + LANDING ORBITER USING PRS NAVAID	10AG72	Hb	158
NA	31J172	MSC-03690 C		SS ORBITER GNC S/W FUNCT. REQNTS VERTICAL FLIGHT OPN	10AG72	Hb	159
NA	27JE72	MSC-06900		SS BASELINE ACCOMODATIONS FOR PAYLOADS	10AG72	Hb	160
NA	24NV71	LA112971-1		SSV PROGRAM AVIONICS SYSTEM RECOMMENDATIONS	14AG72	Hb	161
NA	11AF72	502-23-33		CENTRAL MULTIPROCESSOR + MAN-MACHINE TECHNIQUES	11AG72	Hb	162
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NR	MA72	PROFUSAL		SS PROGRAM AERA DESIGN DATA BOOK VOL. 1 ORBITER	17AG72	Hb	167
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NA				SPACE SHUTTLE PROGRAM REQUIREMENTS DOCUMENT-LEVEL 1	22SP72	Hb	229
NA	26JA72	MSC-07070		ANALYSIS OF SHUTTLE ORBITER FERRY METHODS	22SP72	Hb	230
NA	00AF72	STD101.1		SPACECRAFT TRAINING + DATA NETWORK-BASELINE DOC.	29SP72	H	231
NR	12NV71	MSC-03329		ALTERNATE AVIONICS SYS STUDY + PHASE B EXTENSION	29SP72	H	232
NR	21JL70	MSC-00718		SPACE STATION CREW OPERATIONS DEF PHASE B	29SP72	Hb	233
XF				REAL TIME 6 DEG FREEDOM AIRCRAFT SIMULATION - SL-1	050C72	Hb	234
NA	FF72	SD72-SA32		SPACE TUG DESIGN STUDY-VOLS 1,2,3-1,3-2,4,5	29SP72	H	235
NA	24JL71	MSC-04075		FUNCTIONAL PERFORMANCE REQ-SHUTTLE AVIONICS SYS	29SP72	H	236
RR				DIGITAL CONTROL SYSTEMS SELF-CHECK	050C72	H	237
GE				SYSTEMS OPERATION SIMULATOR	050C72	Hb	238
CP				ROLE OF MICRO PROGRAMMING IN FOURTH GENERATION COMPU	050C72	Hb	239
IP				AEROSPACE SYSTEMS IMPLICATIONS OF MICROPROGRAMMING	050C72	Hb	240
NA	10AG72	SSPFT2167		LONGITUDINAL + LATERAL-DIRECTIONAL DATA VL 70-000001	050C72	Hb	241
MC	06SF72	982-NC-02		MONTHLY PROGRESS REPORT-SIMUL COMPLEX STUDY	050C72	Hb	242
AF	030C72	ZR1		SSD SHUTTLE MISSION SIMULATOR PLANNING DATA	050C72	Hb	243
GR	OLT	LIS440121		ICB FOR INTERP SIMUL LM GUIDANCE COMPLMS	050C72	Hb	244

SMSS REFERENCE DOCUMENT LISTING

DGC. SRCE	HDC. DATE	NUMBER	REV	DOCUMENT TITLE	DATE RECD	LOCN	SEQ NO.
NA	21JF69	FHP-5-2		BLD NO 5 MISSION SIMULATION + TRAINING FACILITY	050C72	Hb	245
				AIR TRAFFIC CONTROL SYS-DIGITAL SIMULATION FACILITY	050C72	Hb	246
				A REAL TIME RADAR SIMUL USING APL DIGITAL COMP LINKS	050C72	Hb	247
				A COMPARISON OF 3 TYPES OF MANUAL CONTROLS-3RD ORDER	050C72	Hb	248
IN	FE72			INERTIAL SYS FUNCTIONAL + DESIGN REV FOR ORBITER-R	050C72	Hb	249
				REAL TIME SPACE VEHICLE + GSE SOFTWARE SIMULATOR-COD	050C72	Hb	250
				TORQUE SENSITIVITY A-FUNCTION OF KNOB RADIIUS + LOAD	050C72	S	251
MJ	AR72	E-2708		ENERGY MANAGEMENT DURING SHUTTLE TRANSITION	050C72	Hb	252
	AF72			SYSTEM 86 LIBRARY	050C72	Hb	253
NA	JL72	MSC-07036		SIMULATION OF MANNED SPACE FLIGHT FOR CREW TRAINING	060C72	Hb	254
SI	27SF72			PROGRAMMING ELEMENTS-SMS TRAINING-JURKE/VANBUCKEL/GRA	050C72	Hb	255
MI	MR72			PROJECT INTREX	29SP72	Hb	256
IR				AP 101	100C72		257
				VISUAL STUDY MCDONNELL-DOUGLAS	100C72		258
				COMPUTER STUDY MCDONNELL-DOUGLAS	100C72		259
				SHUTTLE DEVELOPMENT SCHEDULE	100C72		260
				LMS CREW TRAINING SCHEDULE	100C72		261
GE	AP72	NAS911946		REMOTE MANIPULATOR DYNAMIC SIMULATION	100C72		262
MA	AF72	CR123570		SHUTTLE PROP SYS ONBOARD CHECKOUT + MONITORING DEV	100C72		263
CC	06MA72	CR61376		COMPUTER SYS SIMULATION + ANALYSIS	100C72		264
IN	16FF72	N7221203		ADV SFTWR TECH FOR DATA MGMT SYS VOL 3-PROG LANGUAGE	100C72		265
IN	16FE72	N7221205		ADV SFTWR TECH FOR DATA MGMT SYS VOL 2-SSV EXEC SYS	100C72		266
IN	16JF71	N7221204		ADV SFTWR TECH FOR DATA MGMT SYS VOL 1-SSV S- STUDY	100C72		267
MS	07MA72	CR123569		FLIGHT PROGRAM LANGUAGE REGMT	100C72		268
SH	- 71			ATC FOR THE SEVENTIES PART 1	100C72		269
SH	- 71			ATC FOR THE SEVENTIES PART 2	100C72		270
SH	- 71			ATC FOR THE SEVENTIES PART 3	100C72		271
AI	06MA71	A71-30381		PROC TECH FOR REAL TIME SYS FORM EXPERIENCE W EXPEKMT	100C72		272
NA	DE70	IN-E-6066		DESIGN E OPER PLAN OF CENTRAL ONLINE DATA PROC-LANGLY	100C72		273
TV	AF71	TSC-FAA71		CONCEPTUAL NETWORK MODEL OF AIR TRANS SYS	100C72		274
MA	JA71	CR118310		VIRTUAL MEMORY SYS DESIGN	100C72		275
RA	JA71	CR118860		EXPERIENCE WITH EXTENDABLE COMPUTER SYS SIMULATOR	100C72		276
MT	MR71	MTR-1995		AIRCRAFT MOCKUP COMPUTER PROGRAM SPECIFICATIONS	100C72		277
AI	05MR69			NOMOGRAM FOR AIRCRAFT RUDDER PEAL DESIGN	100C72		278
AI	05MR69			OPTIMUM KNOB DIAMETER	100C72		279
AI	05MR69			DESTRUCTABLE DIMENSIONS FOR CONCENTRIC CONTROLS	100C72		280
MJ	JFF9	CR106370		MANUAL CONTROL OF UNSTABLE VEHICLES-KINESTHETIC CUES	100C72		281
RA	AL69	RM-6027		ONLINE DEBUGGER FOR 05900 ASSEMBLY LANGUAGE PROGRAMS	100C72		282
MA	JA70	CR110445		METHOD FOR UNIFIED HARWARE-SOFTWARE DESIGN	100C72		283

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4.19 Modular Display Electronics (MDE)

4.19.1 General Function

The Modular Display Electronics (MDE) equipments in the Space Shuttle are a part of the Data Processing and Software Subsystem. The six associated cathode ray tube (CRT) displays and keyboards supplement primary instruments for GN&C computer data entry and readout and are also used for backup guidance and subsystem status.

The MDE concept was developed to satisfy two basic needs:

(1) provide separation of routine display functions from critical GN&C computer control functions, and (2) provide data processing capabilities over and above GN&C computers for both management simplification and avoidance of systematic errors. A standardized CRT/Keyboard interface results from this approach and system growth can be more easily accommodated. A simplified block diagram is shown in Figure 4.19.1-1.

Figure 4.19.1-1 is a more detailed block diagram showing the evolution of the MDE concept.

MDE EVOLUTION

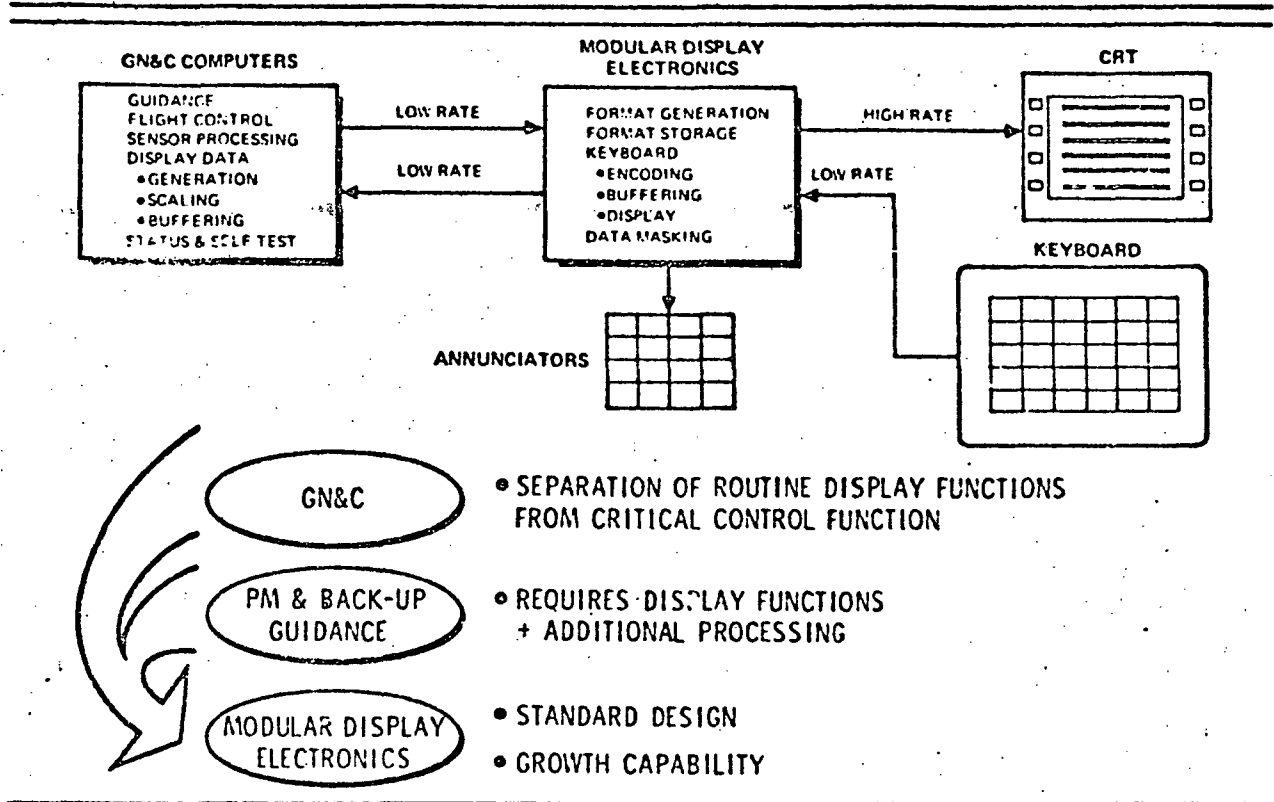


Figure 4.19.1-1

MDE FUNCTIONAL EVOLUTION

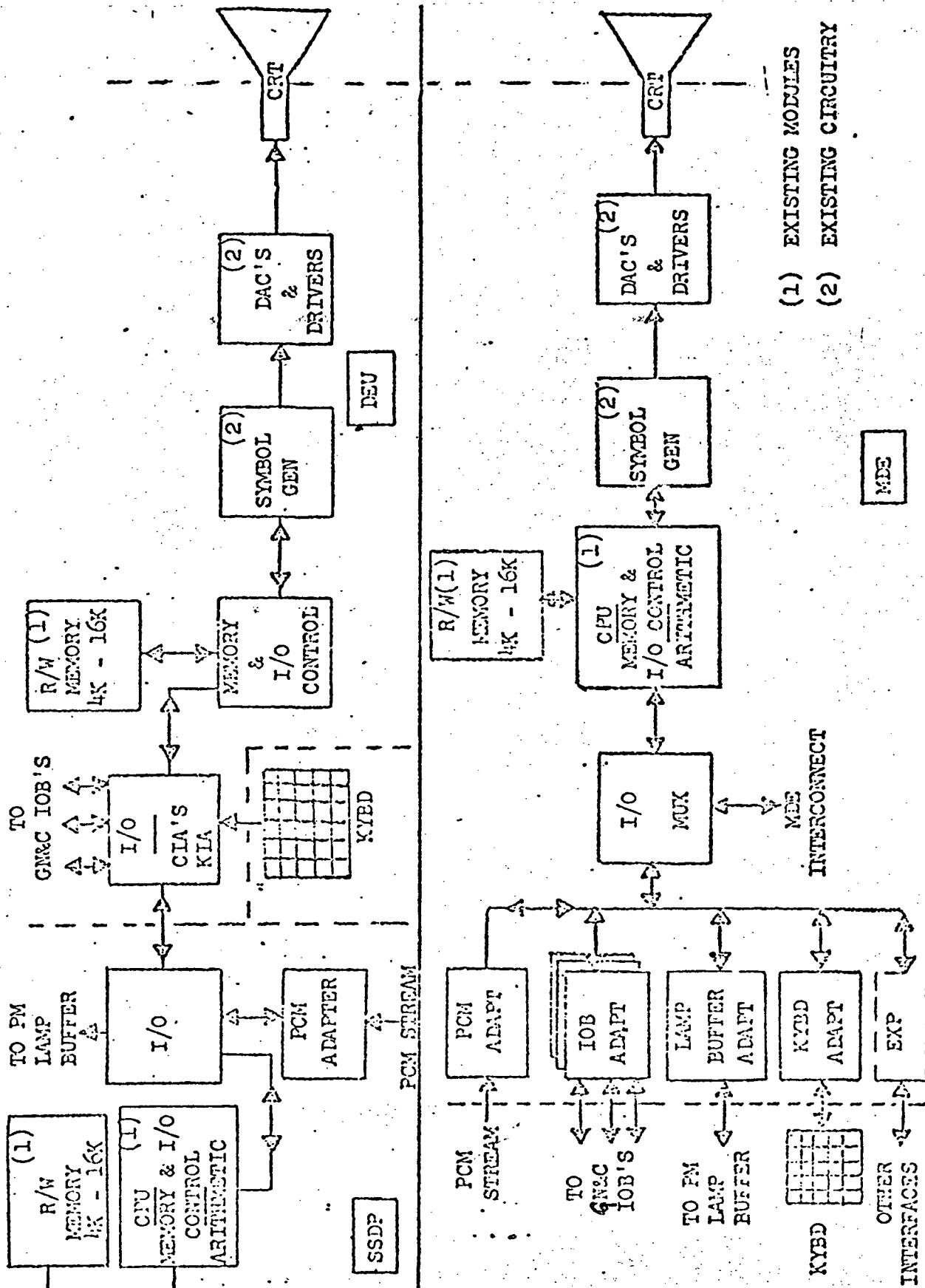


FIGURE 4.19-2

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Four MDE's are used in the baseline system to provide GN&C Display/Keyboard interfaces, performance monitor, and back-up guidance display processing. Three MDE's are interconnected with GN&C computers to provide prime GN&C display and control capability on any combination of the three forward CRT's/Keyboards. Backup guidance displays are normally presented on the center CRT and performance monitoring page formats on the aft CRT. All MDE's are tape cartridge reloadable in non-time critical periods. Refer to Figure 4.19-3.

Significant hardware and software growth capability is available through the addition of two PMS computers (same type as GN&C computer) and using MDE 3 and 4 in the same relationship as MDE 1 and 2 to GN&C computers. Two additional MDE's are used in the payload system for a total of six in the Orbiter vehicle.

MDE PROGRAM LOADING/USAGE

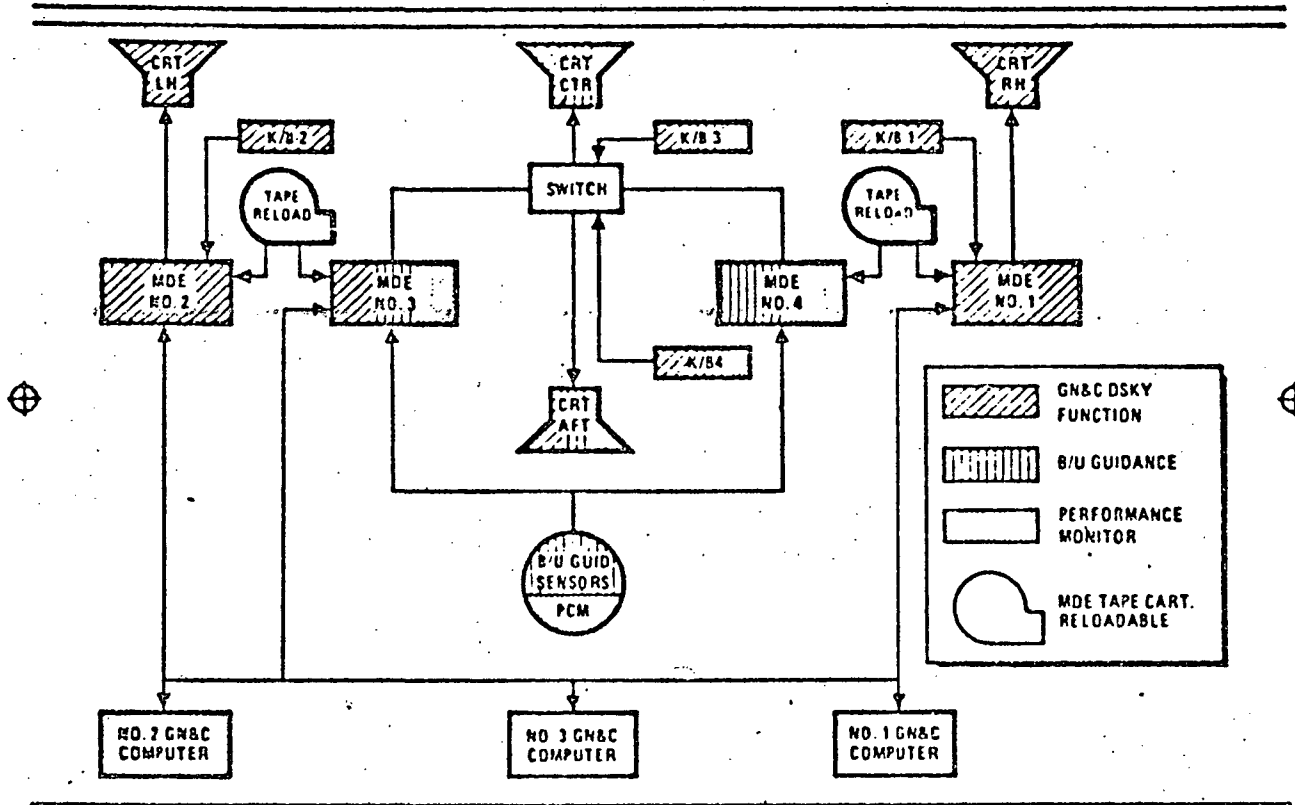


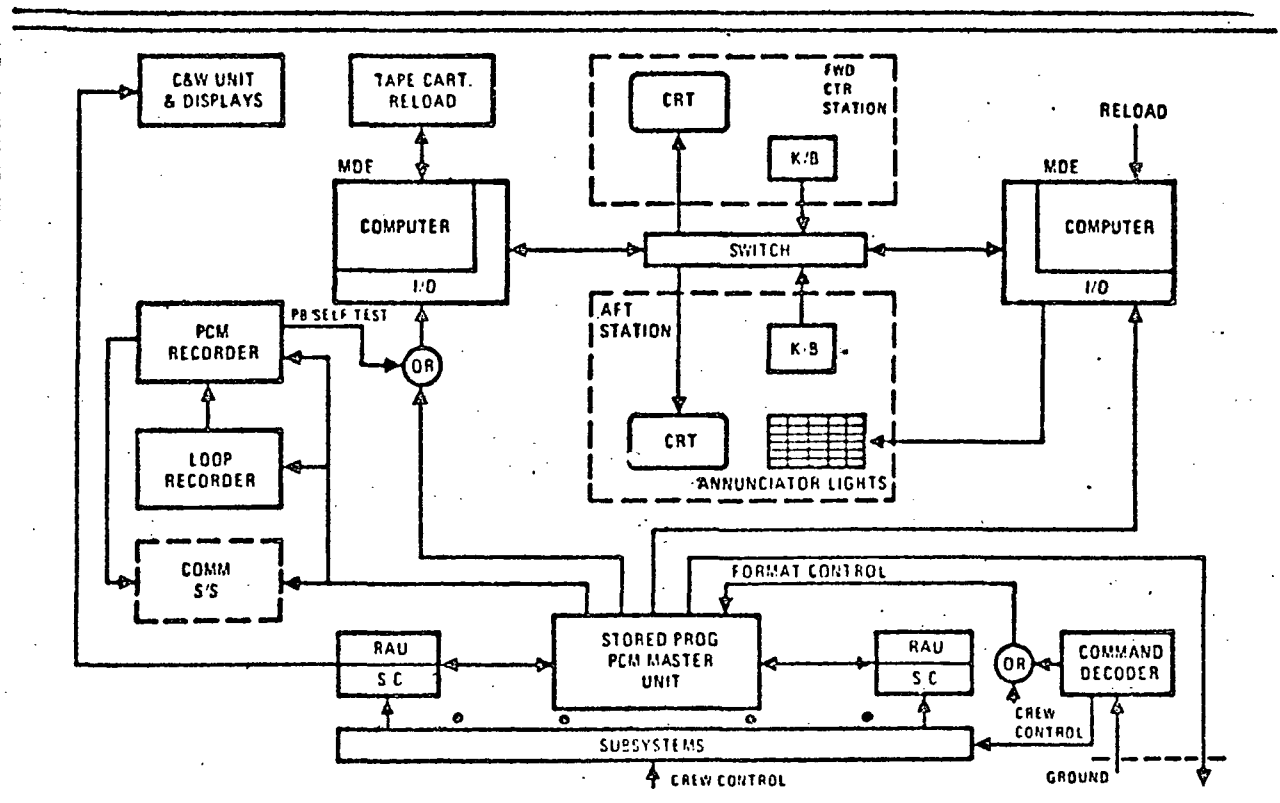
Figure 4.19.1-3

Subsystem Management

Onboard and ground data/control relationships shown (Fig. 4.20.1-4) illustrate how all data users have access to the same data. Up to four unique formats are available in the stored program PCM master unit to accommodate user unique requirements. Tape reload capability for MDE's is available during flight, but is used only in non-time-critical situations. A prerecorded PCM track is available on the PCM recorder for end-to-end ground self test of the MDE/CRT/Annunciator combinations. Continuous self monitoring of the PCM subsystem is accomplished through the use of standard analog and digital words generated within the remote units.

Figure 4.19.1-4.

SUBSYSTEM MANAGEMENT



4.19.2 MDE System Operation and Interfaces

Processing of data for display on the subsystem CRT and for subsystem performance and operation monitoring is accomplished by MDE Subsystem Display Processor set which includes a modular, serial-output, address-programmable PCM data selector/buffer, a small stored-program processor CPU-I/O, and lamp driving logic. The equipment interfaces with the composite PCM stream, with an alphanumeric display/keyboard set which has been loaded with format skeletons for subsystem display, and with a number of fault status and agree/disagree annunciators located on the subsystem panels. There is also an interface with the vehicle Caution & Warning system for use in sleep periods or at times when the subsystem panels are unattended. Functional organization of the equipment is shown in Figure 4.19.1-2.

4.19.2.1 Display Unit (DU)

The unit employs a small (4 x 4 inches usable), high-brightness CRT to present up to 18 line of 24 alphanumeric characters each. Located on the DU bezel are 16 line designator pushbuttons used in conjunction with the keyboard for display selection and data entry. The face of the DU, with a typical GN&C format displayed, is shown in Figure 4.19.2-1. The top line of the format is normally used for page titles and numbers; lines 1 through 16 for data names, data and units; and the bottom line is reserved for keyboard data entry and verification, and for computer error messages.

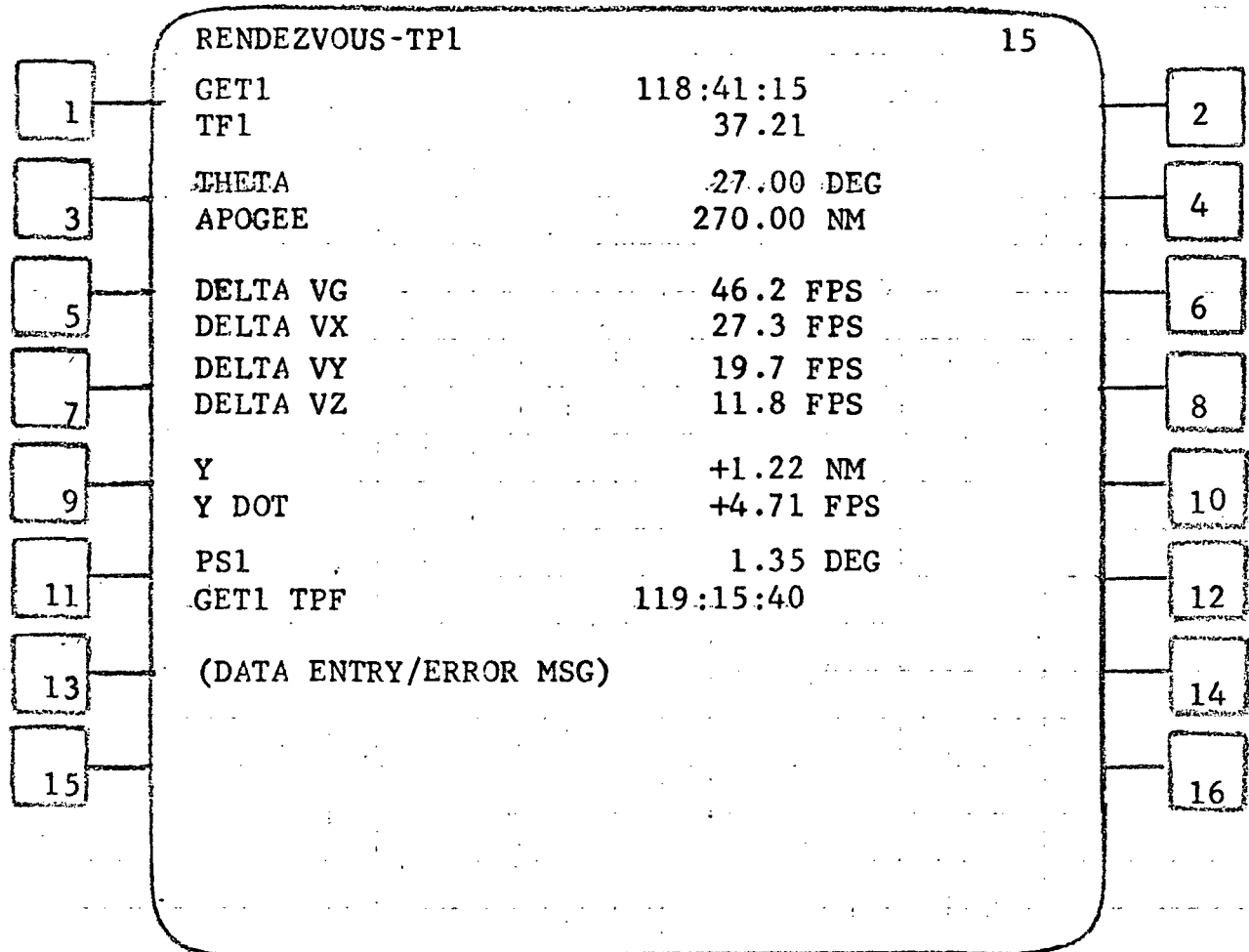


Figure 4.19.2-1 Alphanumeric Display CRT

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4.19.2.2 Keyboard

A 4 x 8 key matrix is used to control the CRT display, select index and data pages, and communicate with the interfacing computer. The standard keys are zero through 9, +, -, Decimal Point, Enter, Resume, Proceed, End, and Clear. The remaining function keys are reformattable for flight and subsystem display applications. See Figure 4.19.2-2.

System Operation

The Display/Keyboard set operates in two basic modes, an index mode and a data mode. Index mode operation is initiated through actuation of an INDEX key on the keyboard; initially the top index page is called from a fixed location in MDE memory and displayed. Each line on this page represents either a subindex page or a data page. A one-selection may then be made by pushing the line selector push-button opposite the desired page title. Alternatively, data pages may be called directly by page number from the keyboard by actuating a PAGE SELECT key, or may be paged through consecutively. When data page selection is made via the index tree, the display shifts to data mode as soon as a specific data page is selected. In the data mode, the MDE assembles a data page from a fixed skeleton called from a selected MDE memory location and variable data requested from the selected interfacing computer. The request to the computer is identified by data page number, which is decoded in the computer to initiate routines which select and convert constants from memory and results of on-going computations, and assemble this data in line order for transmission to the

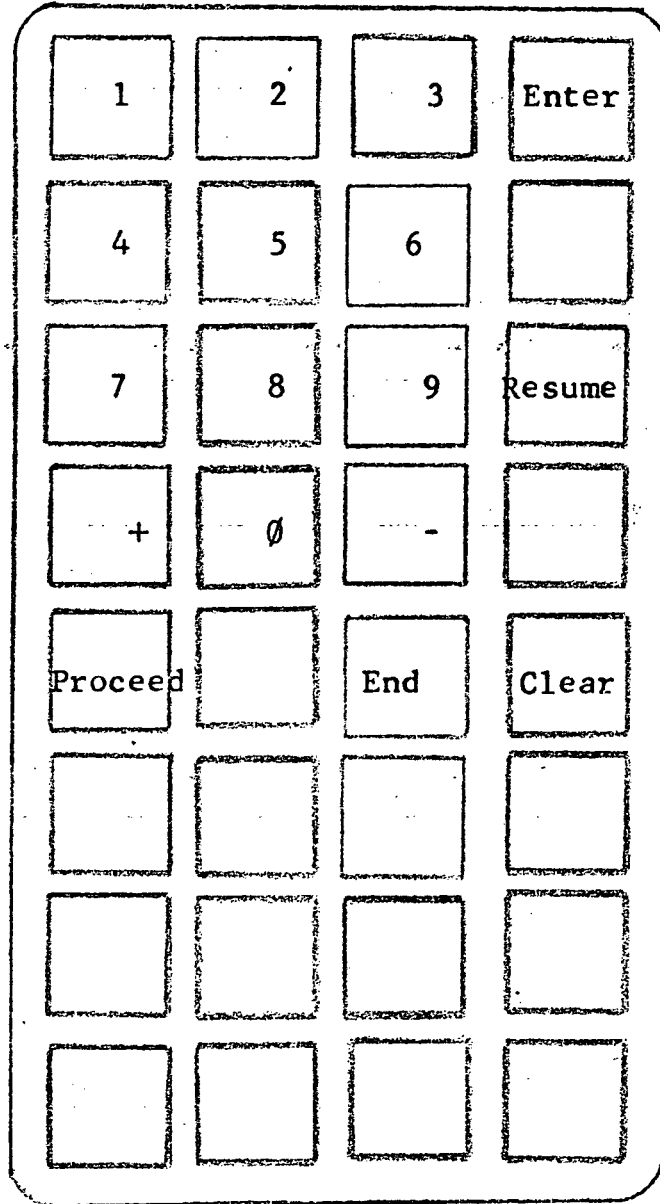


Figure 4.19.2-2

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CRT. This cycle is repeated twice per second for update. The page number is sent with each update block and compared with the called page number in the MDE to assure data/format skeleton compatibility. By a combination of field masking techniques and special instructions, the average alphanumeric data page skeleton occupies less than 120 16-bit words in MDE memory and requires approximately 30 16-bit words of data from the computer for a full page update.

Actuation of the numeric and sign keys on the keyboard when in the data mode is interpreted as a data entry to the computer. The data goes into a buffer line in MDE memory and comes up on the bottom scratchpad line on the display as it is entered; the interfacing computer does not take cognizance of the data until it has been inspected, its disposition identified by a discrete from one of the display line selector buttons, and the ENTER key actuated. The computer then evaluates the entered data for acceptability. If the data is acceptable, the computer clears the scratchpad line and substitutes the entered value for the value in its memory, causing the same number to appear in the selected data line on the next update. If the data is unacceptable (not a program constant, wrong value, no disposition, etc.) the computer sends a discrete to light an OPERATOR ERROR annunciator and an error code to initiate display of an error message on the scratchpad line. If during the execution of programs the computer encounters problems, it can light a PROGRAM ALARM annunciator and send an error code to initiate display of an error message on the scratchpad line.

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The keyboard has priority in that error messages will not be forced displayed while keyboard entry is in process, but will come up if the operator clears the scratchpad line. Error messages are stored in the MDE memory and addressed by conversion of error codes into memory locations.

4.19.2.3 IOB Adapter

The MDE is capable of interfacing with any of three computers, one at a time. The IOB Adapter, therefore, contains the driver and receiver circuits required to send and accept signals from 3 computers. The selection of the one active computer interface is based upon discrete signals received in the MDE from a panel control switch. The computer selection logic samples the selection control discrettes and electrically ties the active computer interface to the remaining MDE logic.

Operation of a function key on the keyboard, such as enter, end, proceed, clear, etc., causes the MDE computer to initiate a command or a data transfer. The computer will first issue a read-I/O address command which causes the MDE to transfer the memory address where the last encoded key action is stored. (Keyboard entries, including line/column select, are stored sequentially in a fixed portion of the MDE core memory.) By performing a subtraction, the computer then initiates read commands to the MDE beginning at the start of keyboard entry storage up to the last entry which initiated the transfer. The computer then issues a write command to reset the keyboard entry table to blanks.

This has the effect of clearing line 17 the scratch pad line. The computer then operates upon the operator request.

The Computer IOB Adapter contains the logic required to communicate with the selected computer. It is capable of responding to read or write commands issued by the computer. It is also capable of generating an interrupt to the computer when commanded to initiate a transfer.

4.19 .2.4 Keyboard Adapter

The Keyboard Adapter receives parallel data from the keyboard which is encoded to define which of the keys on the keyboard or display unit has been depressed. The keyboard initiates data transfers by raising a request line to indicate that a key has been pressed. The Keyboard Adapter acknowledges the keyboard input and then stores the data in the MDE memory.

For computer-destined data, the KA notifies the I/O Multiplexer which interrupts the computer and requests a read of the desired data. An area in the MDE computer memory is reserved for keyboard service data. For this data, the computer does a special formatting operation for processing and display on the data entry (scratchpad) line. If the Enter Key is depressed, indicating that the scratchpad line should be sent to the computer, the computer reads the scratchpad locations in MDE memory and then clears them. This has the effect of transferring the data from the scratchpad line to the selected data line. The scratchpad line can also be cleared from the keyboard.

4.19.2.5 Symbol Generator

The Symbol Generator is comprised of digital and analog circuitry which controls the presentation of display formats. It is used to generate alphanumeric characters. The refresh and generation of the symbols are controlled by a list of instruction words which are stored in the MDE core storage. The digital instruction words are processed by converting them to the x-deflection, y-deflection, and z-axis video signals required to drive the CRT display.

The Symbol Generator provides the following display capabilities:

- . Generate alphanumeric characters from stroke information stored in the MDE memory.
- . Format characters in type mode or random positions.
- . Growth capability for drawing vectors of any length.
- . Position characters at any location on a 512 by 512 matrix.
- . Present a uniform display by controlling the intensity of the characters (and vectors).
- . Operate in a typewriter mode associated with either the X or Y direction.

4.19.2.6 PCM Adapter

This element accepts a Manchester biphase coded data stream at rates up to 100 KB/S, strips sync from the stream to provide frame and word sync and bit clock, and sequentially selects, buffers and transmits RZ-coded logic-level data to the processor. Both the incoming

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PCM address and the outgoing data are buffered for at least one PCM word interval in order that contiguous words in the stream may be selected.

4.19.2.7 Processor CPU - I/O

The processor is a low-cost general-purpose, high-speed, core-memory machine which basically executes four tasks: data selection, display scaling, data limit checking and system self-test. The memory is modular up to 16K, 16-bit words. The processor retains in its reloadable memory the PCM address tables for selection of up to 1,000 measurements; the denormalizing constant tables for scaling of up to 1,000 measurements for display, together with the display address tables for up to 50 12-line tabular alphanumeric CRT display pages; the pre-determined operating limits for limit-checking and logic comparison of up to 600 analog and discrete measurements, together with annunciator address tables for up to 150 fault status annunciators; and the program to accomplish the four tasks defined above. The limit-checking operation may apply up to three selectable sets of limits to monitored measurements, depending on subsystem configuration and/or mission phase.

Further details are to be found in Section 4.19.3 and 4.19.4.

4.19.2.8 Lamp Buffer Adapter

This electronics accepts and decodes outputs words from the CPU to determine which of the fault status annunciators should be activated. A provision is incorporated to hold annunciators activated until acknowledged by the crew. The decoded and processed discretely

are outputted to the annunciators via lamp drivers to provide the required power switching.

4.19.2.9 System Operation

CRT displays are requested by index tree or page number via the keyboard as described in section 4.19.2.1. In either case the page number code is decoded by the processor to access the appropriate denormalizing constant and display address tables for the selected page. The processor then addresses and selects the requested data, converts the data and the PCM frame time into BCD-coded engineering units format, assembles it in display line order and transmits it to the display set as described previously. This operation is repeated an integral number of PCM frames later for update; the number is selectable to achieve a nominal twice-per-second update with either real-time or tape-delayed non-real-time input data.

Measurement selection for limit-checking will be established by a predefined PCM address table. The processor will select from its memory the appropriate limit and status tables for the selected operational phase and subsystem configuration, and will ordinarily make a limit check or a state comparison for all selected measurements. However, if a known off-nominal measurement repeatedly triggers the alarm, the processor can be instructed via the keyboard to disregard the condition of that measurement until it is notified to the contrary. The processor will maintain a table of inhibited measurements for display upon request.

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Limit checking can be done at repetition rates up to about 10 per second. However, the processor will normally be instructed to verify that an off-nominal condition persists for a number of consecutive data samples (2 to 5 for most measurements) before outputting an alarm discrete. When an off-nominal condition is verified, the processor will output discret~~es~~ to the annunciator logic identifying the appropriate individual fault status annunciator, and to the master fault annunciator, and will write the number of the display page containing the offending measurement(s) on the scratchpad line. If the appropriate display page is up, or when it is brought up, the processor will identify the data it has evaluated as off-nominal by requesting a "bug" symbol on the appropriate display line which will flag the measurement(s) as out-of-tolerance high or low. A performance monitor status table will be maintained, to be displayed in page format on request, listing in chronological order the measurements which have been abnormal since the table was last cleared and indicating what that status was (high, low, off, failed, etc.).

In each major cycle of processing for display and performance monitor, the Processor executes a routine which checks the data, the system hardware, and itself. A BITE annunciator is provided which is normally held off by a pulse train from the Processor I/O. However, should the PCM data fail, or a check of calibration words or PMC BITE discret~~es~~ from the data stream indicate "no-go", or the processor self-test routine indicate "no-go", or the processor power fail, the output

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pulse train will cease and the BITE annunciator will illuminate. If the processor itself is still healthy, it will send an error code to the display set to initiate display of an error message identifying the problem.

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4.19.3 MDE Computers

There are presently two different computers being used for the MDE CPU application. For the non GN&C Performance Monitoring application, two IBM Model AP101's will be used. A detailed description of this computer is to be found in section 4.18.3. For the GN&C MDE's and for the Payload System MDE's, small IBM type SP-1 computer is to be used. A detailed description of this computer follows.

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4. 193 MDE Computer Type SP-1

Machine Organization	Type Number System Operation Data Word Length Instruction Word Length Number of Instructions Typical Execution Times Add Multiply Divide Average Instruction Execution Rate Registers	General purpose, stored program, simplex Binary, fixed point, two's complement, fractional Full parallel (16 bits) 16-bit word, including sign; 32-bit doubleword, including sign 16 bits 41 2.7 μ s 5.7 μ s 8.0 μ s 350,000 operations/second 4 (A, Q, and B registers and instruction counter)																		
Main Storage	Type Capacity Modularity Cycle Time Access Time Special Features	Ferrite magnetic core, nonvolatile, random access, destructive readout 4096; 8192; 12,288; or 16,384 17-bit words 4096 17-bit words per pluggable module 1.33 μ s (write or read/restore) 600 ns Power transient protection, separate sense winding, 2-1/2D organization, temperature compensation																		
I/O Parallel Channel	Externally Initiated Program Initiated Data Interface Maximum Data Transfer Rate	Direct memory access; buffered I/O Direct I/O 16 bits plus address and control; single-ended TTL interface 150,000 to 600,000 words/second																		
Logic Circuits	Class Type Package	Monolithic integrated Transistor/transistor logic (TTL) and medium-scale integration (MSI) Flatpaks: 14, 16, and 24 leads																		
Power System	Primary Power Output Regulated DC Features	115/200 V AC, 3-phase, 400 Hz, 72 W average for standard structure, 31 to 52 W for basic assembly (28 V DC primary input power optional) +5, -5, +12 V DC Overvoltage and overcurrent protection, transient protection, power sequencing pluggable modular construction																		
Physical		<table border="1"> <thead> <tr> <th></th> <th>Standard Structure</th> <th>Basic Assembly</th> </tr> </thead> <tbody> <tr> <td>Volume</td> <td>0.35 ft³</td> <td>0.06 ft³</td> </tr> <tr> <td>Weight</td> <td>18.1 lb, for 4K storage 21.7 lb, for 16K storage</td> <td>3.6 lb, for 4K storage</td> </tr> <tr> <td>Construction</td> <td colspan="2">Plug-in modules used throughout</td> </tr> <tr> <td>Cooling</td> <td colspan="2">Indirect air, conductive</td> </tr> <tr> <td>Environment</td> <td colspan="2">Meets or exceeds MIL-E-5400, Class 2X</td> </tr> </tbody> </table>		Standard Structure	Basic Assembly	Volume	0.35 ft ³	0.06 ft ³	Weight	18.1 lb, for 4K storage 21.7 lb, for 16K storage	3.6 lb, for 4K storage	Construction	Plug-in modules used throughout		Cooling	Indirect air, conductive		Environment	Meets or exceeds MIL-E-5400, Class 2X	
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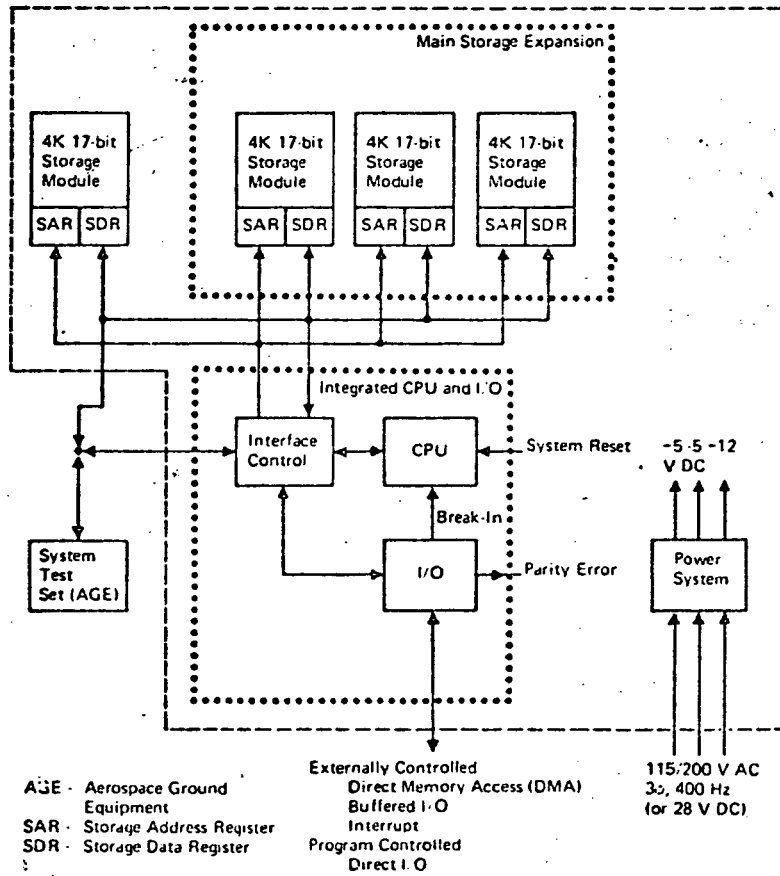


Figure 4.19.3-1
Computer Block Diagram

Central Processing Unit

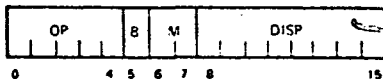
The central processing unit (CPU) contains the logic necessary to fetch, decode, and execute instructions and to perform the necessary arithmetic, logical, and other data-processing operations. All operations are full 16-bit parallel, with a basic cycle time of 333 nanoseconds. Sixteen-bit parallel interfaces are provided for the I/O module, main storage, computer memory loader/verifier, and operator control panel.

Instruction Format

An extensive set of instructions is provided for arithmetic, logical, branching, data moving, and I/O operations. Double-precision add and subtract, together with the multiply and divide operations, provide for supporting extended precision applications.

A 16-bit instruction format is used to combine storage efficiency and powerful addressing capability. Direct, indirect, relative, and immediate addressing modes are provided in the short format (SRS) instruction.

SRS



The B field specifies whether or not the base register is used during address generation. The M field specifies the addressing mode to be used. Direct mode addresses the first 512 locations in main storage. Relative mode provides an address displacement with respect to either the instruction counter or the base register (B).

The 16-bit immediate operand is formed from the B field (bits 0 through 7 of the operand) and the displacement field (bits 8 through 15 of the operand).

Indirect addressing is provided in two formats:

- Indirect
- Indirect and Tally.

Indirect addressing permits full address specification without altering the base register. Also, indirect addresses may be shared by several instructions, thus conserving storage. The Indirect and Tally addressing mode automatically increments the indirect address word following each use, providing the programmer with excellent indexing and data array manipulation potential.

Instruction	Execution Times (μ s)
Arithmetic Add	2.7
Add Double	4.0
Subtract	2.7
Subtract Double	4.0
Add to Storage	3.0
Tally (Skip if zero)	3.0
Tally I/O	3.0
Multiply	5.7
Divide	8.0

Instruction	Execution Times (μ s)	
Logical	Compare High	2.7
	Compare Low	2.7
	Compare Equal	2.7
	AND	2.7
	AND to Storage	3.0
	OR	2.7
	Exclusive OR	2.7
Branch	Exclusive OR to Storage	3.0
	Branch Out	
	Unconditional	1.7
	Branch Unconditional	1.7
	Branch on A Negative	1.7
	Branch on A Zero	1.7
	Branch and Link	4.0
Data Move	Load A	2.7
	Store A	3.0
	Load Base	2.7
	Store Base	3.0
	Modify Base	2.7
	Load Q	2.7
	Store Q	3.0
Register Operations	Reset Interface	1.7
	Base to A	1.7
	A to Base	1.7
	Shift A Right	
	Arithmetic	1.7+*
	Shift A Left Logical	1.7+*
	Shift A, Q Right	
	Arithmetic	1.7+*
	Shift A, Q Left Logical	1.7+*
		BITE Failure
Input/Output	In Service	3.0
	Out Service	2.7
	Direct In	2.7
	Direct Out	2.7

*Shift length (n): add n/6 if shift even; (n+3)/6, if odd.

Input/Output

A fast parallel channel interacts with the high-speed CPU and main storage to provide excellent throughput and to feature performance, operation, and an I/O interface that are upward-compatible with other System/4 Pi machines, such as the IBM-AP-1 computer.

Three I/O modes are provided for the transfer of data and command functions between the SP-1 computer and peripheral equipment:

- **Direct Memory Access (DMA) I/O** – The I/O device provides a 16-bit main storage address; 16 bits of data are written into or read from this storage location. The DMA I/O mode is initiated by the I/O device. A CPU lock-out feature significantly increases the data transfer rate, providing a maximum data transfer rate of 600,000 words per second.

- **Buffered I/O** – The I/O device provides an "address tag," used to access a channel control word (CCW) containing count and address; a single data word or a block of data words is written into or read from main storage. The Buffered I/O mode is initiated by the I/O device. A maximum data transfer rate of 175,000 words per second may be reached when the CPU is locked out.

- **Direct I/O.**— Under control of the CPU instruction stream, a command is sent to an I/O device, and one 16-bit word of data is written into or read from the device. The Direct I/O mode is initiated by the program. The data transfer rate is a function of the operation following the transfer and may be as high as 175,000 words per second.

In addition, an external interrupt is provided, allowing external equipment to cause the CPU to suspend current operations, store the current contents of the instruction counter, and load a new instruction count from the storage locations specified by the I/O device. The I/O device provides the interrupt service routine address, permitting the support of multiple interrupts. The I/O device also implements any priorities required.

Parallel Channel	Externally Initiated	Direct Memory Access: 600,000 words/s (maximum) Buffered I/O: 175,000 words/s (maximum)
	Program Initiated	Direct I/O: 175,000 words/s (maximum)
	Data Interface	16 bits plus address and control; single-ended TTL interface
	Maximum Data Transfer Rate	150,000 to 600,000 words/s
Interrupt	One external interrupt line (multiple interrupts may be handled)	

I/O Interface

The interface between the I/O channel and I/O devices is shown in the accompanying illustration. Each I/O device has unique Service Request and Service Acknowledge lines. Two pairs of these lines are built into the standard CPU and I/O logic pages, supporting two devices. More lines may be added on the custom I/O page if support for additional I/O devices is desired. The interface lines are implemented in standard TTL logic.

Either a single peripheral I/O device or a control unit may be attached to the I/O interface. Each control unit, addressed and controlled by a channel control word (CCW), may interface with as many as 127 peripheral I/O devices.

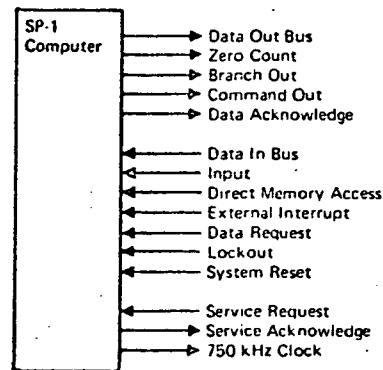


Figure 4.19.3-2

SP-1 Computer Support Software

The SP-1 Support Programming System (SPS) provides the application programmer with a set of aids designed to effectively reduce the time required to get the application programs online and to support program modifications and maintenance. Continuing a field-proven concept, the SP-1 SPS provides the user with an assembler, a linkage editor, and a simulator program:

- **Assembler** — Uses an efficient symbolic language. Allows modular programming and testing. Assembles relocatable programs. Provides syntax error detection and identification. Allows macro-processing and conditional assembly. Produces listed output.
- **Linkage Editor** — Combines and relocates program modules assembled at separate times. Resolves program linkages. Creates input for the simulator. Creates core image object programs for loading SP-1 computer storage.
- **Simulator** — Allows SP-1 program analysis. Facilitates dynamic simulation through a user-written control program. Provides user access to simulated computer object program data (with absolute and symbolic reference). Allows object program correction. Provides program debugging options (dump, snap, trace). Enables simulation of I/O and interrupt initiation and response.

The SP-1 assembler gives the programmer a symbolic source language that produces storage-efficient, high-throughput programs using the effective instruction set defined by the computer architecture. An excellent macroprogram capability significantly reduces the repetitive coding required of the application programmer.

Identical in most respects to the widespread, well known System/360 assembly language, the SP-1 assembler requires minimum retraining of experienced programmers and provides early online release of new trainees, thus significantly reducing training costs. High-quality user and programmer manuals assist programmers in the effective use of the SP-1 assembler language. Programming rules and techniques, such as modular programming (C-sects, D-sects, etc.), syntax, macroprogram generation, symbols and labels, source instructions, comments and continuation lines, and subroutine linkage, are in most cases identical to System/360 operations.

The linkage editor is used to combine object program modules into a core image load module for the SP-1 and to resolve all necessary program linkages. The linkage editor input to the SP-1 simulator program includes not only the core image load module, but symbolic reference data as well.

The simulator dynamically analyzes the SP-1 program modules at the instruction word level and executes any given set of SP-1 instructions prepared by the linkage editor. Facilities such as dumps, traces, and snaps are available under the control of a user-written simulation control program.

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Option Summary

Two major options are available for extending the capability and adaptability of the SP-1 computer:

- Expanded Main Storage – The minimum configuration SP-1 computer has a 4K-word main storage. Storage may be expanded in 4K increments to 16K words by inserting additional pluggable 4K storage pages into the structure. Self-contained timing and storage logic require no changes to the CPU and interface design. This modification can be installed in the field.
- Custom I/O – Space is provided, and the necessary control signals and data buses are included, for the insertion of a custom I/O module, individually designed to meet application requirements not covered by the standard broad-use, high-speed parallel channel.

4.19.4 MDE Software and Systems Applications

4.19.4.1 MDE Computer Software

Software shall be provided to execute in the MDE Computers and shall perform the following functions:

- . Limit check analog parameters
- . Verify correct discrete status
- . Communicate results of the above two functions to CRT and panel annunciators.
- . Display crew selected subsystem status formats on CRT.

The combination of the above software functions along with the assumed hardware configuration will allow the crew to verify and make judgments as to subsystem status.

The software shall consist of a minimal control program, limit checking routines, display support routines and tables. Additionally, predefined format skeletons shall be supplied.

MDE Processor Control Program

The control program for the MDE processor schedules the processor software tasks for execution during a predefined fixed time slice processing cycle occurring every TBD ms, or at a preselected integral PCM frame count. The MDE processor cycle is shown in

Figure 4.19-8. Two control program subprograms, cycle control and data input, are executed prior to dispatching the performance monitor and display processing applications programs. Execution of data output and self-check subprograms complete this cycle. The control program subprograms are discussed in the following paragraphs:

1. Cycle Control - The cycle control function determine major cycle timing. It is presently planned that the occurrence of PCM master frames will be counted and that the processing cycle will be entered after that count reaches a value of two (a measurement sample rate and program iteration rate of 2/second was assumed for sizing purposes). The counter (or clock) is reset immediately before the major cycle is entered.

2. Data Input - Data input processing consists of initiating an I/O sequence to read the required PCM measurements into the processor main storage. Discrete measurements are assumed to be 1 bit each, and analog measurements are assumed to be 8 bits each. For sizing purposes, it was assumed that 300 analog and 300 discrete measurements are obtained for non GN&C performance monitor and display processing.

3. Data Output - The data output subprogram transfers the display update data to the MDE and transfers on/off signals to the subsystem annunciators as determined by the performance monitor software.

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MDE and annunciator output lists are generated by the display processing and performance monitor application programs, respectively. These lists are processed by the control program to effect data output.

4. Self-Check - The self-check subprogram is executed as the last task in each processing cycle. Main storage, internal CPU, and I/O functions are tested. Anomalies detected by self-check are communicated by an external discrete indication and/or an error code to the MDE.

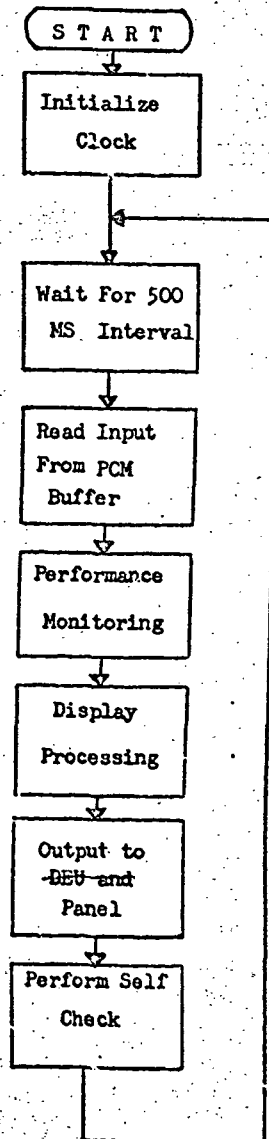


Figure 4.19.4-1 MDE - PROCESSOR OVERALL FLOW

4.19.4.2 GN&C MDE System Application
4.19.4.2.1 GN&C Display Systems Software

The Display subprogram in the GN&C MDE computers provides the capability to selectively support specific crew requested displays. This support includes arithmetic conversion, BCD conversion, formatting and transmission of GN&C data to the crew station displays. For output data, the display support software has the capability to process one parameter per line for twelve lines on each of fifty pages. In addition, the display software also processes input data passed from the crew station to the GN&C MDE computers via an alphanumeric keyboard. The processing of the input data includes interpretation, conversion, limit testing and reasonableness testing. The input processing function is capable of processing 100 parameters. The display system subprogram is capable of generating alphanumeric display messages and a vector symbol generation.

1. Display System Subprogram. The Display System Software performs the function of presenting the Orbiter GN&C system status information to the crew via a combination CRT and keyboard (DSKY) displays. The DSKY consists of numeric and special character keys which the crew will use to communicate with the Display subprogram. The CRT display will accommodate 18 lines of alphanumeric data with 24 characters per data line. The 18 lines of data are dedicated to 1 title line, 16 measurement data lines, and 1 scratch pad line. Fifty CRT page formats, each containing 16 lines of data, are required to accommodate the GN&C display requirements.

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2. Page Formats. The 24 characters for each of the 16 measurement lines is subdivided into a group of 12 characters for measurement identification, 5 characters (including decimal point) for data, 4 characters for units, and 3 blank separator characters. The page skeleton information containing the page title, measurement ID's and units is contained in the MDE computer memory. The MDE memory contains 8K, 16 bit words. The memory required to perform data display calculations is included in the GN&C Display program.

3. Display Selection. The keyboards are each redundant. Data entered on each DSKY is directed toward each of the 3 GN&C computers simultaneously - so that all programs receive the same input data. Either display can be switched to read the outputs of any one of the 3 GN&C computers. The program structure is designed such that a different page of display data can be directed toward each of the CRT displays. Each DSKY can be coded to direct either a common or a unique display to each of the CRT displays.

As data is entered on the DSKY, the MDE will interrogate the DSKY and display the keyed data on the scratch pad line of the CRT display. The program will not react to keyed data requests until the ENTER button is depressed.

4. Input Data Checks. The program will perform input data tests on a selected set of DSKY input data. The tests will attempt to insure that erroneous or unrealistic data is not accepted by the program. In the event of a failure of the input data tests, the program

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will notify the crew of the failure condition and will not act on the entered data. The crew has the option of overriding the test results and forcing the program to accept the data. The input data checks include 50 limit tests and 50 reasonableness tests.

5. Display Types. The program will provide for 50 unique data page displays where each data page contains 12 system measurements, 1 title line and 1 scratch pad line. The 50 display pages are further defined as follows:

(a) 15 Systems Status Display Pages - To provide for 125 GN&C system measurements including 40 analog, 60 discrete and 25 system status measurements.

(b) 35 Parametric Data Displays - To provide a capability for displaying approximately 400 measurements, internal computer calculations, or program constants. The 400 lines of parametric display data are not presently defined.

6. Failure Indications. Any system failures detected by the GN&C Flight program will be presented to the crew via a caution and warning indication in addition to a failure message on the scratch pad line of the CRT display. The scratch pad line will inform the crew of the failure type and present a page number to be entered via the keyboard to obtain a full set of CRT display data for the failed subsystem. Multiple failure indications will be provided for by the program.

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4.19.4.2.2 GN&C Performing Monitoring Software

1. Analog Processing - A Performance Monitor module will be provided to verify that all GN&C system analog parameters are within a predefined set of high/low limits. An out-of-tolerance condition will cause notification to be made to the crew via subsystem annunciators and/or CRT displays. The current estimate is that 40 analog parameters will be processed by the routine. Each parameter will have four sets of high/low limits as an average. One set of these limits will be active during the various flight passes or modes.

The GN&C MDE computer control program will perform all input checks at either a 25/second or 2/second rate. The input data sources are the input buffers.

Upon completion of the input via the executive program, the control program will dispatch the Performance Monitoring tasks. After routine initialization, active interrogation of the current parameter value to the active limits is initiated. If no parameter is found out of tolerance, all parameters will quickly be processed and control passed back to the control program.

If a parameter is found out of tolerance, a test is made to determine if the parameter has been out of tolerance "n" times. The currently assumed value of "n" is two. This test prevents noise from causing superfluous no-go indications. If "n" successive conditions have been encountered, the type of crew notification required is interrogated. If an annunciator activation is specified, an 8-bit

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annunciator address code is placed on the control program output data list for transmission to the annunciator panel at the end of the processing cycle.

Measurements that are out of tolerance can be designated as a disregard for error notification by the crew. This capability is useful for stopping continuous error displays caused by invalid measurement readings. The disregard designation is made by requesting display of the format containing the measurement in error and utilizing the line designator switch on the MDE to identify the measurement. A cancel disregard designation is made in a similar manner.

If a CRT display is specified several actions occur. First, an indicator is set in the format skeleton associated with the out of tolerance parameter. When this format (page) is displayed, the appropriate parameter will have appended the out of tolerance flag which allows the crew to quickly see those out of tolerance conditions associated with the subsystem. For analog measurements, the flag will indicate the direction, high or low, of the out of tolerance condition.

The routine will then request a flag message display which will appear on the scratch pad (line 14) of the display the next time the Display Support routine updates the current display. The message will notify the crew that Performance Monitoring has detected an out of tolerance condition and will specify the page number on which the condition can be viewed. If the scratch pad is currently being used by the crew to enter a command, the display will be delayed until the

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area is free. A related annunciator will notify the crew of the condition. The scratch pad line may then be cleared via the keyboard to free it for the error message.

In addition, a one line message is added to a queue of messages that reflect a summary of all out of tolerance conditions existing at the current time. These one line messages are displayed when the crew requests the Performance Monitor Status page and will reflect the 12 most recent out of tolerance conditions. Earlier malfunctions may be viewed by "paging" through the Performance Monitor Status displays via a special keyboard command. Provision will be made to accommodate up to 64 of the one line malfunction messages (4 x 16).

If both panel and CRT crew notification action is specified for a particular parameter, both of the above described panel and CRT sequences occur.

When a parameter that has previously been out of tolerance comes within tolerance, the converse of the above steps is performed. The annunciator is reset and/or the one line message in the Performance Monitoring Status format is purged and the remaining entries compressed. The crew notification scratch pad line message is removed if applicable.

The above discussion described the comparison of the current parameter value to the active limits. The active limits are established by a separate module identified as the Performance Monitor Phase Initializer. This module is called by the control program upon flight phase changes, or as commanded by the crew. Additionally,

measurement limit changes required for vehicle status change (e.g., engine firing) will be effected by monitoring discrete signals for the change in status. The Performance Monitor Phase initializer will have tables that associate the phase to the appropriate limits to use for each of the parameters for that phase. The tables have been sized to accommodate an average of four sets of high/low limits.

2.. Discrete Processing - The Performance Monitor module will be provided to verify the correct status of certain subsystem input discrettes. Similar to the analog processing module, if a discrete is found to be in an incorrect state, the crew will be notified via panels and/or CRT displays.

The current assumption is that 60 GN&C discrete parameters will be monitored at a 25/second or 2/second rate.

The Executive control program will perform all input operation and pass control to the discrete processing module. After module initialization, groups of 16 discrettes will be tested to determine if any one of the 16 discrettes has changed. If none have changed, other groups are tested until the scan is complete.

If a discrete has changed a table entry is interrogated to determine the type notification specified. Again, this can be via annunciators, CRT, or both. If annunciator notification is specified, an eight bit annunciator address code and an associated on/off bit are queued for output.

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If CRT notification was specified, an "allow/disallow" table is interrogated to determine if the change was allowable. If so, no additional action is taken and the scan of other discrettes continues. Presumably, the discrete for the current phase is not considered a part of the performance monitoring. If the discrete change is not allowed and is currently in the incorrect state, the same sequence as was done in analog processing is performed. The "out of tolerance" indicator is set in the format skeleton on which the discrete appears, a notification is placed on the scratch pad line, and a one line summary message is inserted in the Performance Monitoring Status format buffer. The use of this presentation is the same as described in the analog description. If the discrete change is to the correct state the converse of the above sequence is performed.

The initial discrete status and the control routines access to the proper "allow/disallow" and "should be" tables is established by the Performance Monitor Phase Initializer. This is the same routine mentioned earlier in the analog processing section. A set of allow/disallow and should-be tables are provided for each flight phase.

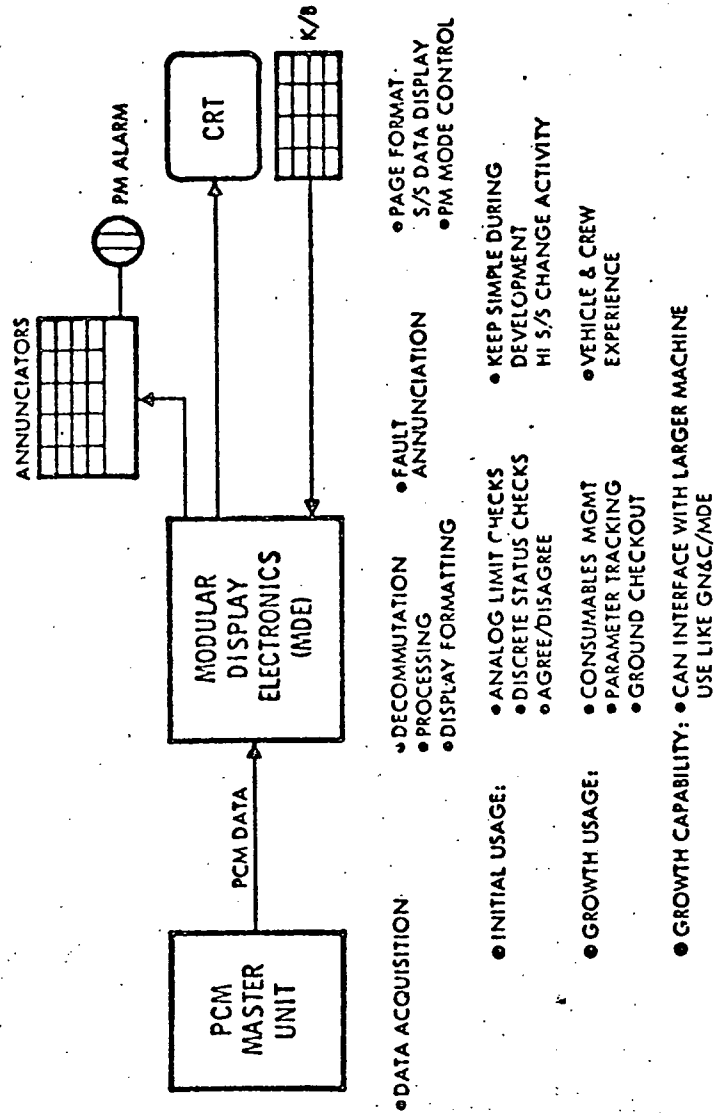
4.19.4.3 Performance Monitor (PM) System

The PM system consists of two MDE processors dedicated to the monitor and display of non-GN&C systems status or to the solution and display of the backup guidance and navigation function. One of the PM MDE processors capabilities is obtained by time sharing the center console GN&C MDE, between the GN&C display functions, the PM function, and the backup G&N functions. The PM MDE's will contain backup G&N programs so that a "get me home" capability is available in the event of a generic software error or other critical system failures. Reload of the MDE memory for a change of functions will be provided by a tape read-only memory under control of the crew.

Performance monitoring includes two primary functions: (1) Continuous limit/status checking of 300 analog and 300 discrete non-GN&C subsystem measurements with fault annunciation and PCM recorder control in the event of a malfunction; (2) Generate page format CRT display of related subsystem measurement sets at the flight crew's discretion.

The limit/status check program is executed at a two/second rate and contains false alarm avoidance provisions. No-go's are displayed on an annunciator light matrix that identifies the problem area and on a CRT "scratch pad" line that identifies the particular page on which the no-go parameter value can be observed. Growth provisions include consumables management, ground checkout usage, and redundant parameter tracking. Emphasis is placed on keeping the processing simple

Figure 4.19.4-2
PERFORMANCE MONITOR



- DATA ACQUISITION
- DECOMMUTATION
- PROCESSING
- DISPLAY FORMATTING
- ANALOG LIMIT CHECKS
- DISCRETE STATUS CHECKS
- AGREE/DISAGREE
- CONSUMABLES MGMT
- PARAMETER TRACKING
- GROUND CHECKOUT
- GROWTH CAPABILITY: • CAN INTERFACE WITH LARGER MACHINE USE LIKE GN&C/MDE
- INITIAL USAGE:
- GROWTH USAGE:
- GROWTH CAPABILITY:
- FAULT ANNUNCIATION
- PAGE FORMAT
- S/S DATA DISPLAY
- PM MODE CONTROL
- KEEP SIMPLE DURING DEVELOPMENT
- HI S/S CHANGE ACTIVITY
- VEHICLE & CREW EXPERIENCE

during the high vehicle subsystem change activity that will be encountered during the development phase.

Performance Monitoring Software

1. Analog Processing - A performance monitor module shall be provided to verify that all non-GN&C subsystem analog parameters are within a predefined set of high/low limits. An out-of-tolerance condition will cause notification to be made to the crew via subsystem annunciators, CRT display, or both annunciator and CRT. The current assumption is that 300 analog parameters will be processed by this routine. Each parameter will have three sets of high/low limits, on the average. One set of those limits will be active at a time.

The control program will input an entire set of the selected PCM measurements at a fixed predetermined rate, as described earlier. The input data source is the OFI Master Controller. Upon completion of the input routine, the control program will dispatch the performance monitor tasks.

After routine initialization, the analog measurements will be converted to engineering units, and in that form will be tested with respect to the active limits. Refer to the general program flow shown in Figure 4.19.4-3. If no parameter is found out of tolerance, all parameters will quickly be processed and control passed back to the control program. If a parameter is found out of tolerance a test is made to determine if it has been out of tolerance "n" consecutive times. This test prevents noise from causing superfluous no-go indications.

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If the error count has not yet reached "n" for that parameter, it's error counter is incremented and processing of other parameters continues. If the error count had reached "n", the type of crew notification required is interrogated. If an annunciator activation is specified, an 8-bit annunciator address code is placed on the control program output data list for transmission to the annunciator panel, at the end of the major processing cycle.

Measurements that are out of tolerance can be designated as "disregard for error notification" by crew. This capability is useful for stopping continuous error displays caused by invalid measurement readings. The disregard designation is made by requesting display of the format containing the erroneous measurement, and utilizing the line designator switch on the MDE assembly to identify the measurement. A "cancel disregard" designation is made in the same manner.

If a CRT display is specified several actions occur. First, an indicator is set to identify the no-go condition as "high" or "low". The routine then sets up a message for line 17 of the current display, which specifies the format number associated with the faulty parameter. The message notifies the crew that an out of tolerance condition has been detected and will specify the page number on which the condition can be viewed. If the scratch pad (line 17) is currently in use, the display will be delayed until the area is free and a discrete notification of the conflict will be issued to the MDE. Next, a one-line message is added to a queue of messages at the current time.

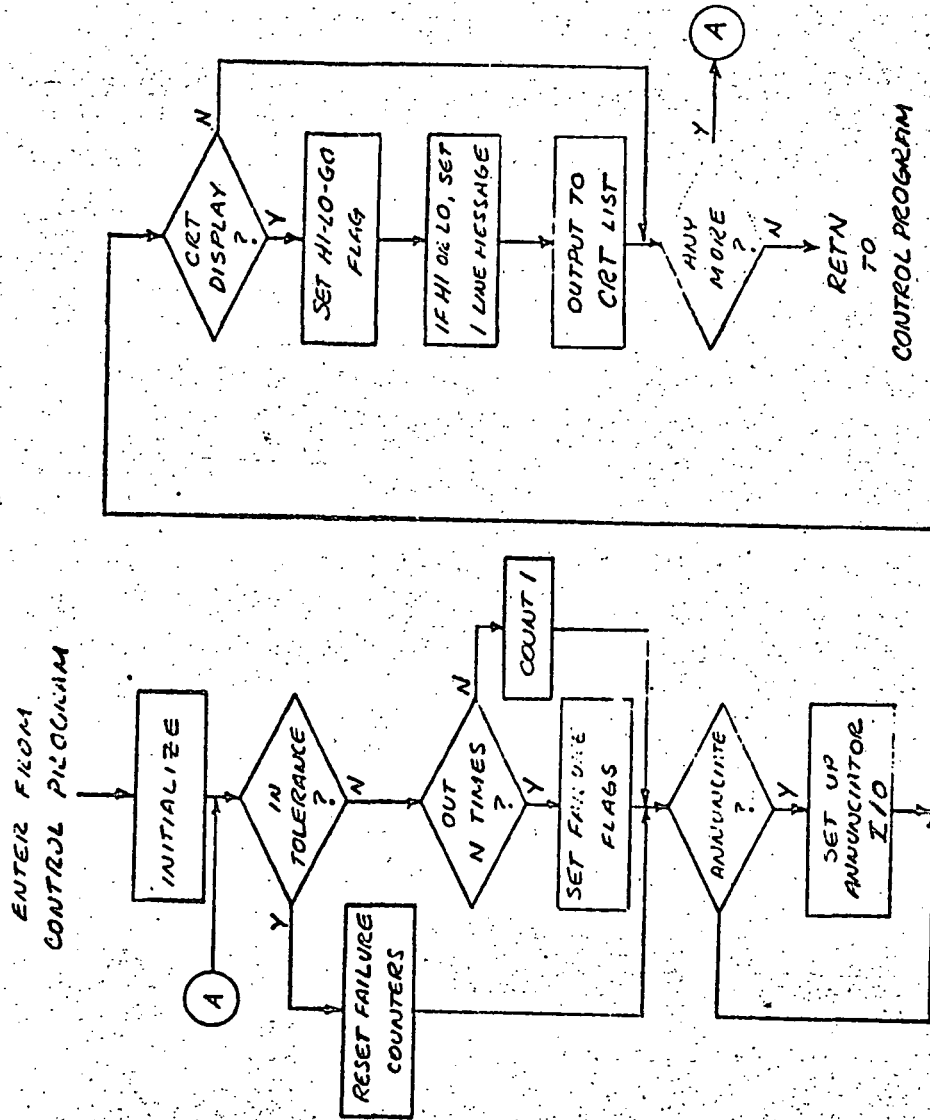


Figure 4. 194-3 Analog-Predictor

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These one-line messages are displayed when the crew requests the Performance Monitor Status page, and will reflect the 16 most recent out of tolerance conditions. Earlier malfunctions may be viewed by "paging" through the four-page Performance Monitor Status displays via a special keyboard command. Provision will be made to accommodate up to 64 of the one-line malfunction messages (4 pages x 16 measurements per page). If both panel and CRT crew notification action is specified for a particular parameter, both of the above described panel and CRT sequences occur.

When a parameter that has previously been out of tolerance comes within tolerance, the converse of the above steps is performed. The annunciator is reset and/or the one line message in the Performance Monitoring Status format is purged and the remaining entries compressed. The crew notification scratch pad line message is removed is appropriate.

The above discussion described the comparison of the current parameter value to the active limits. The active limits are established by a separate module identified as the Performance Monitor Phase Initializer. This module is called by the control program upon flight phase changes or as commanded by the crew. Additionally, measurement limit changes required for vehicle status change (e.g., engine firing) will be effected by monitoring discrete signals for the change in status. The Performance Monitor Phase Initializer will have tables that associate the phase to the appropriate limits to use for each of the parameters for that phase. The tables have been sized to accommodate an average of three sets of high/low limits.

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2. Discrete Processing - A Performance Monitor module shall be provided to verify the correct status of certain subsystem input discrettes. Similar to the analog processing module, if a discrete is found to be in an incorrect state, the crew will be notified via panels, CRT or both panel and CRT.

The current assumption is that 300 discrete parameters will be monitored at twice per second rate. The Discrete Performance Monitor module is briefly described. Refer to Figure 4.19.4-4 for the general program flow.

The control program will perform all input and pass control to the discrete processing module. After module initialization, groups of 16 discrettes will be tested to determine if any one of the 16 discrettes has changed. If none have changed, other groups are tested until the scan is complete.

If a discrete has changed, a table entry is interrogated to determine the type notification specified. Again, this can be via annunciators, CRT, or both. If annunciator notification is specified, an eight bit annunciator address code and an associated on/off bit are queued for output.

If CRT notification was specified, an "allow/disallow" table is interrogated to determine if the change was allowable. If so, no additional action is taken and the scan of other discrettes continues. Presumably, the discrete for the current phase is not considered a part of the performance monitoring. If the discrete change is not allowed

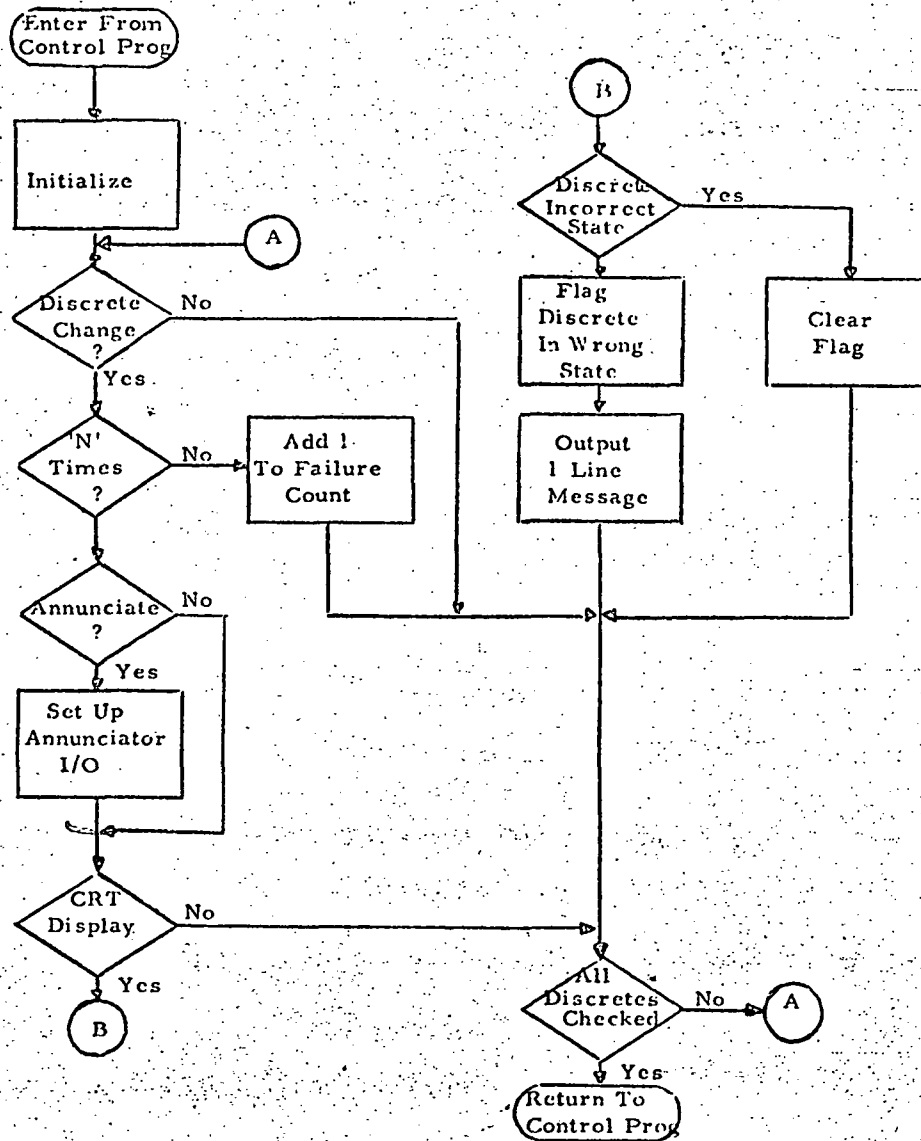


Figure 4. 19.4-4 Discrete Processing Flow.

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and is currently in the incorrect state, the same sequence as was done in analog processing is performed. The "out of tolerance" indicator is set in the format skeleton on which the discrete appears, a notification is placed on the scratch pad line, and a one line summary message is inserted in the Performance Monitoring Status format buffer. The use of this presentation is the same as described in the analog description. If the discrete change is to the correct state, the converse of the above sequence is performed.

The initial discrete status and the control routines access to the proper "allow/disallow" and "should be" tables is established by the Performance Monitor Phase Initializer. This is the same routine mentioned earlier in the analog processing section. A set of allow/disallow and should-be tables are provided for each flight phase.

Display Software - The display software performs the function of organizing and presenting engineering unit subsystem data for CRT display. The following paragraphs describe the display software subprograms, which are stored in the processor, and the display formats, skeletons of which are resident in the MDE memory.

1. For Description - Subsystem status information is presented on the CRT in predefined logical groups. A single group or format is presented at a time. Each format consists of a title line, 1 to 16 measurement lines, and a scratch pad line. Each line may contain up to 24 characters. The measurement lines each contain

three fields; for sizing purposes a 12-character measurement description, a 5-character measurement value, and a 4-character engineering unit label are assumed. The scratch pad line is used for the display of keyboard input data and messages from performance monitoring software. The format skeletons (exclusive of the actual parameter values) are stored in the MDE memory, and contain the alphabetic measurement name, engineering units (for example, "PSIA"), decimal points, display edit information, and Format Control Words (FCW's). The FCW's specify character generation control information, x and y CRT position data, and mode control data.

An "interface dictionary" (table of data), which is resident in the display processor, is associated with each format. It contains data which describes and controls the processing unique to each measurement on a given format. The dictionary contains the measurement number, conversion scale factors and biases, output codes, test limits, and certain flags and pointers.

The maximum MDE storage requirement for a 16-measurement format is:

17 lines of 24 characters + carriage return	215 words
x, y position and control words	4 words
Format Control and edit information	<u>18 words</u>
Total 16-bit words for one format:	237 words

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The display processor storage requirement for the interface dictionary data associated with a 16 (analog) measurement format is:

Measurement designators, 16 x 12 characters	96 words
Scale factors (1 # byte,+ Bias (2 bytes)	24 words
Output codes (9 CRT, 3 annunciator)	2 words
Test Limits, 3 sets at 1 word/set	<u>48 words</u>
Total 16-bit words for one format:	170 words
Total interface dictionary size for	
35 formats:	5950 words

2. MDE Keyboard Processing - The MDE keyboard and line-select pushbuttons are used by the crew to select formats for display, and to specify flight measurements which are to be excluded from performance monitor error notification. Activation of the data entry-format select keys result in its display on line 18 of the CRT. The line-select keys are also stored, but not displayed. Activation of a specific key will result in a signal of the display processor, which responds by reading the input buffer data and routing it to the proper processing program. Figure 4.19.4-5 describes the display processing flow.

3. Display Update Processing - Display update processing consists of determining which format has been selected for display, assembling, and organizing the appropriate parameter values and status flags, and scheduling data for output to the CRT and/or annunciator.

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When the display format has been identified, the interface dictionary is searched to determine which of the parameters are to be displayed. The engineering unit values (previously stored by the performance monitor routines) are queued for output to the CRT by the output program. The status (go or no-go) of each parameter is inspected and if appropriate, a one line message is queued for transmittal and display on one of the four performance mointor status pages.

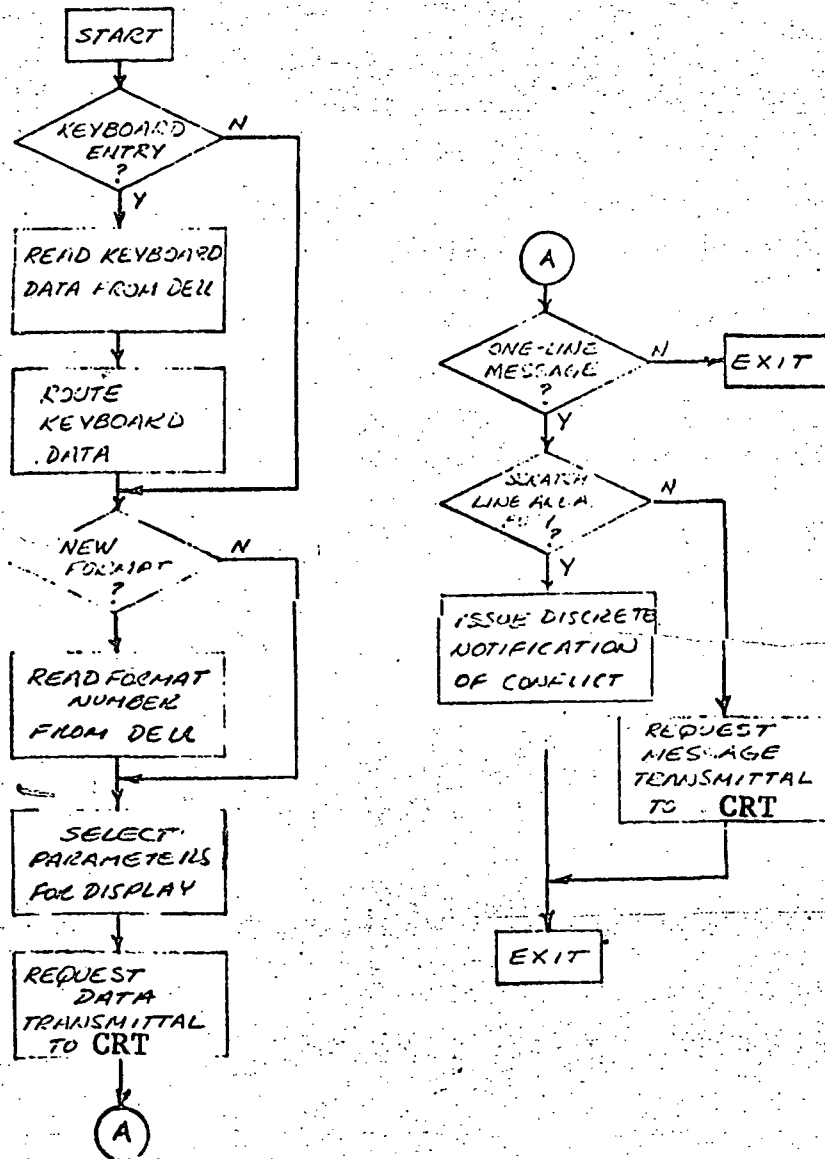


Figure 4.19.4-5

Display Processing Flow

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4.19.4.4 Payload (PL) System

The PL system consists of two MDE processors dedicated to the status, control, checkout, initialization, and display of payload data. The PL computers which contain identical programs will both be active but only one will be in control. The PL system will not be required to process onboard experiment data which will be either recorded onboard or transmitted to the ground for processing. Data transmission and recording will not require the PL computer participation. Memory growth capability for the PL computer system is provided by a dedicated read-only tape memory unit.

4.19.5 Rationale

Not applicable.

4.19.6 Assumptions

"Index" and "Page Select" keys are on keyboard.

4.19.7 Data References

187 AP101/SP1 IBM OBC Candidates for Shuttle

232 MSC-03329 Space Shuttle Alternate Avionics System
Study and Phase B Extension Final Report
12 November 1971
Pages 2.10-1 thru 2.10-48
2.5-16 thru 2.5-24

166 SD72-SH-50-3 Technical Proposal for Space Shuttle
Program Volume III 12 May 1972
Pages 3-95 thru 3-122

41 SD72-SH-0023 Space Shuttle Phase B Avionics Final
Report 8 March 1972
Pages 96 thru 103

4.20 MAIN ENGINE CONTROLLER

REF.
42

When the Space Shuttle vehicle operation requires the engine to start, operate at a given power level, or shut down, the vehicle sends a command to the engine. The controller is the electronic unit that receives these commands, determines the appropriate actions, and issues instructions to the engine controls. If the engine does not respond in a normal manner to these instructions, the controller modifies the instructions appropriately. If the engine parameters exceed predetermined limits and the limit control is enabled by the vehicle the engine is shut down by the controller.

Responsive control of the engine thrust level and mixture ratio is achieved by the controller updating the instructions to the engine controls fifty times a second (every 20 msec). The controller has the capability of interrupting the normal cycle for an update in less than 20 msec when the vehicle transmits a new command to the engine or a component failure warrants the interruption.

Precise engine performance is achieved through closed-loop control, a 16-bit computer word, 12 bit input-output resolution and self calibrating analog to digital conversion.

4.20.1 CONTROLLER DESIGN REQUIREMENTS

REF. 42 The controller is required to perform the following functions to implement the Avionics control, checkout and monitoring requirements.

1. Interface with the vehicle to receive engine commands and transmit data.
2. Interface with and provide signal conditioning, multiplexing and analog-to-digital conversion for 77 sensor signals and 93 analog built-in test signals. Also, provide pulse rate to digital conversion for 16 pulse sensor signals and 6 spark rate built-in-test signals.
3. Interface with and provide output electronics to command 5 proportional actuators (10 hydraulic servovalve torque motor coils and 22 solenoid coils), 13 pneumatic solenoid coils, and 6 spark igniters.
4. Process vehicle commands and engine performance data to provide closed-loop control at a rate of 50 times/second (every 20 msec) for start, shutdown and mainstage control.
5. Provide built-in test hardware and software programs to validate the Avionics and engine system by conducting automatic self tests every 20 msec. performing engine

REF. checkout on vehicle command, and performing engine limit
42 monitoring.

6. Control engine purges upon vehicle command, monitor engines readiness to start and provide an engine-ready signal to the vehicle.

7. Provide engine maintenance data to the vehicle data recording system.

8. Provide redundancy to meet electronic fail-operational/fail-safe design requirements.

9. Provide electrical interfacing with redundant vehicle power buses and provide power switching, conversion, and distribution for the engine.

10. Provide connectors and circuitry for ground support equipment to alter and verify memory.

11. The controller is designed to operate without the use of external cold plates or cooling media.

The controller design requirements listed in Table 4.20-1 are principal requirements imposed by Rocketdyne for the controller design, including those imposed by the engine CEI and ICD requirements.

REF. 42 TABLE 4.20-1 SUMMARY OF SSME CONTROLLER REQUIREMENTS

REQUIREMENT	DESCRIPTION	REQUIREMENT	DESCRIPTION
<u>OPERATING DURATION</u>	0-500 SECONDS, MPL TO MPL 0-460 SECONDS, EPL UNLIMITED, CHECKOUT AREA	<u>ENVIRONMENT</u>	
<u>ELECTRICAL</u>		<u>TRANSPORTATION AND STORAGE</u>	
POWER	DUAL 115/200 VAC, 3 PHASE 400 HZ, 270 W PEAK, 560 W STEADY STATE MAXIMUM AT NOMINAL VOLTAGE	TEMPERATURE	-65 TO +165 F
<u>INTERFACES</u>	VEHICLE - PER 100 RSS-3500-5 GSE - AS REQUIRED TO ALTER MEMORY AND OPERATE CONTROLLER FROM GROUND	HUMIDITY	100 PERCENT
	SENSORS - 29 PRESSURE, 13 TEMPERATURE, 6 FLOW, 8 SPEED, 7 VIBRATION AND 28 POSITION	ACCELERATION	4.0 G
	OUTPUT - 10 SERVO VALVE COILS, 35 SOLENOID-COILS AND 6 SPARK IGNITERS	<u>OPERATION</u>	
<u>DATA PROCESSING</u>		TEMPERATURE	-170 TO +130 G
SAMPLE RATE	20 MS MAJOR CYCLE TIME	HUMIDITY	100 PERCENT
DATA RATE	10,000 BITS/SEC - ENGINE TO VEHICLE	PRESSURE	15 PSIA TO VACUUM
	100,000 BITS/SEC - DEVELOP- MENT TESTING	VIBRATION	70 G PEAK SINE, 900-3000-HZ 31 G RMS RANDOM, COMPOSITE (1 SIGMA LEVEL)
<u>DATA TRANSFER RATE</u>		<u>ACOUSTIC</u>	
MEMORY STORAGE	1,000,000 BITS/SEC	ACCELERATION	174 G
	12,000 WORDS, FULLY REPRO- GRAMMABLE WITH MEMORY LOCKOUT	ADDITIONAL REQUIRE- MENTS	±3.5 G
<u>FAIL SAFE DESIGN</u>	FAIL OPERATIONAL - FIRST FAILURE	<u>WEIGHT</u>	81 LBS
	FAIL SAFE - SECOND FAILURE	<u>SAFETY FACTORS</u>	
<u>SERVICE LIFE</u>			YIELD, 1.1 LIMIT DESIGN LOAD
	100 ENGINE STARTS TO MPL 6 ENGINE STARTS TO EPL CHECKOUT - UNLIMITED		ULTIMATE, 1.4 LIMIT DESIGN LOAD
<u>MAINTAINABILITY</u>		<u>FATIGUE FACTORS</u>	PROOF, 1.2 LIMIT DESIGN LOAD
	NO SCHEDULED SERVICING BETWEEN RECYCLES-ACCESSABLE FOR REPLACEMENT		BURST, 1.5 LIMIT DESIGN LOAD
	BUILT-IN-TEST ISOLATES FAULTS	<u>PARTS</u>	
		<u>CORROSION RESISTANCE</u>	4 (THERMAL CYCLES) 10 (MECHANICAL CYCLES)
		<u>CONNECTORS</u>	PER 85M03928
		<u>EMI/RFI</u>	PER MSFC - DWS-40M39569
		<u>BONDING</u>	PER MIL-STD-461, 462
		<u>IDENTIFICATION</u>	PER MIL-B-5087, CLASS R
		<u>INTERCHANGEABILITY</u>	PER MIL-STD-130
			PHYSICAL AND FUNCTIONAL, COMPLETE,

REF. 4.20.2 CONTROLLER DESIGN DESCRIPTION
42

The controller is a single integral electronics package mounted directly on each of the three main engines. The controller electronics are housed in a pressurized aluminum case assembly specifically designed to provide thermal and vibration protection during ground and flight operation. The total package weight is 81 pounds (36.7 kilograms).

The functional relationship of the controller to the engine is illustrated in Figure 4.20-1. Engine performance data are received from engine sensors. Vehicle commands and requests for data are received from the vehicle/engine interface. Control decisions made by the digital computer on the basis of these inputs are issued to three types of engine controls, i.e., actuators, on-off valves, and igniters. Information on operation of the actuators is fed back to the controller. The controller transmits engine data to the vehicle through the vehicle/engine data bus interface.

The electronics within the controller are divided into five subsystems:

1. Input Electronics - Receives data from all in-flight sensors, converts it to digital form and sends it

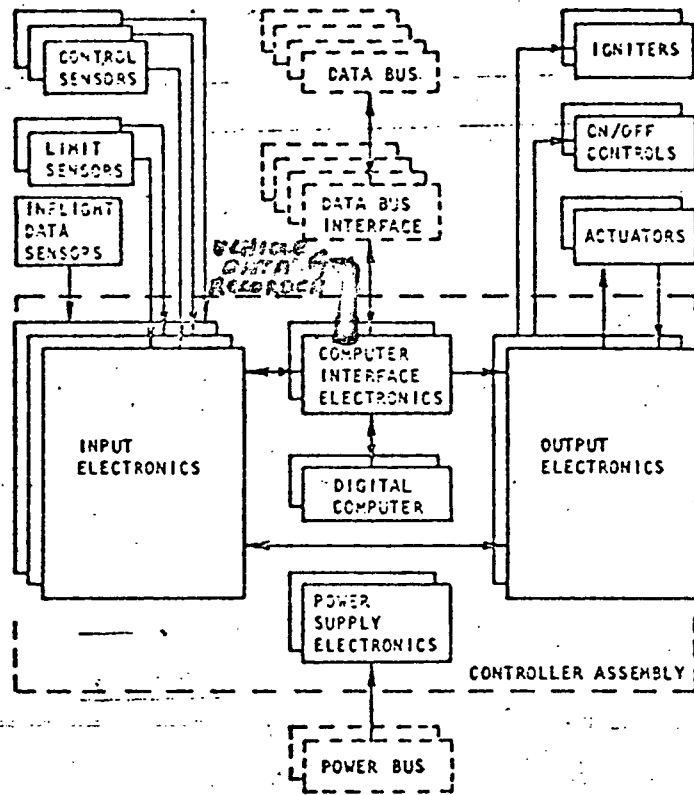


Figure 4.20-1 Engine Controller Functional Relationship

REF. 42 to the computer interface electronics. Since the accuracy of these electronic circuits contributes directly to controller accuracy, they are continuously monitored and recalibrated by the computer.

2. Computer Interface Electronics - Controls the flow of all data within the controller.

3. Computer - Receives sensor data, vehicle commands, and vehicle data requests. It performs computations, issues engine control commands, and stores engine data until requested by vehicle. The computer also conducts tests of all control system components once every 20 msec. The computer includes a 12,288-word memory which stores the control and test programs and the engine performance data.

4. Output Electronics - Converts the computer digital control commands to voltages suitable for powering the engine igniters, on-off controls, and actuators.

5. Power Supply Electronics - Converts the vehicle electrical power to the individual power supply voltages required by the Avionics system.

Detailed functional schematic diagrams of the electronics are contained in Avionics (550K) Drawings Report, Volume 76.

REF.
42

The controller design is straightforward for minimum risk in development and operation. Low risk is achieved through the use of proven technology, built-in flexibility, and conservative design.

The most significant single factor in reducing development risk is the adaptation of the Honeywell HDC-601 airborne computer to the SSME application. The HDC-601 is completely developed, production released.

Much of the substance of the HDC-601 (Table 4.20-2) is directly transferable to the controller application. The remainder is straightforward adaptation with minimal development risk. The HDC-601 has the required speed and accuracy, and is designed specifically for real-time control. The HDC-601 and its commercial counterparts, the DDP-516 and H-316 are presently fulfilling the requirements of numerous real time control applications. The H-316 uses the same logic as the HDC-601 but is packaged for commercial applications. The computer uses a plated-wire memory. The process of reading data from the memory does not disturb the contents of the memory; therefore, no additional time is required to restore the data in the memory as is the case with core types. Plated wire memories are more

**TABLE 4.20-2 APPLICABILITY OF HONEYWELL HDC-601
TO SSME CONTROLLER**

CHARACTERISTICS	HDC-601 COMPUTER	SSME CONTROLLER
LOGIC	FULLY DEVELOPED	SAME AS HDC-601
WORD LENGTH	16 BIT	SAME AS HDC-601
REAL-TIME CONTROL	VIA PRIORITY INTERRUPTS	SAME AS HDC-601
MEMORY ACCESS	DIRECT AND UNDER PROGRAM CONTROL	SAME AS HDC-601
STANDARD SOFTWARE	FULLY DEVELOPED AND FIELD TESTED. COMPATIBLE WITH DDP-516 COMMERCIAL COMPUTER	SAME AS HDC-601
OPERATIONAL SOFTWARE	DEVELOPED SPECIAL FOR EACH APPLICATION	MAY BE VERIFIED ON COMMERCIAL DDP-516 PRIOR TO CONTROLLER AVAILABILITY
MEMORY	5 MIL PLATED WIRE	SAME AS HDC-601 WITH 2 MIL PLATED WIRE FOR LOWER POWER AND GREATER SPEED
INTEGRATED CIRCUITS AND QUALIFICATION	SMALL AND MEDIUM SCALE BIPOLAR TTL TO MIL-STD-883, LEVEL A	SAME AS HDC-601 PLUS NASA X-RAY AND SERIALIZATION
CIRCUIT PACKAGING	EDGE SUPPORTED PRINTED WIRING CARDS WITH PLUG-IN CONNECTORS	USES SAME CIRCUIT LAYOUT, BUT WITH "FOAMPACK" MOUNTING TO MEET SSME ENVIRONMENTAL REQUIREMENTS
CHASSIS WIRING	WIRE-WRAPPED POINT-TO-POINT	SAME AS HDC-601
COMPONENT COOLING	FORCED AIR CONVECTION	DIRECT CONDUCTION TO CHASSIS VIA "FOAM PACK" THERMAL INSERTS

REF. 42 environmentally resistant than core types and operate over wider temperature ranges for any given speed. Vibration resistance is superior since the plated wires are embedded in epoxy planes sandwiched with the electronics boards into a compact rigid package. The controller memory uses 2-mil wire which requires one-fifteenth the power of core memories. The 2-mil memory is operated with low-power electronics, minimizing the number of components and improving the reliability.

The majority of the input-output electronics circuits have been developed and proven on prior Honeywell systems.

Flexibility inherent in the controller design also reduces development risk by accommodating the changes and unforeseen contingencies that arise in a normal development program.

Twenty percent spare connector pins and input/output electronics are included to provide for additional growth in the quantities of sensors, actuators or solenoid valves. The spare electronics will be wired into the controllers for development engines and those needed for the final design can be included in production controllers by adding duplicates of existing wiring board assemblies. Similarly,

REF. 42 added control functions can be accommodated since 30 percent of the computational duty cycle is unused and 41 percent of the memory is uncommitted.

A major contributor to the flexibility of the controller design is the use of digital rather than analog computation. Changes in operational sequences and functions may be accomplished simply by changes in computer software programs, avoiding costly and time-consuming hardware redesign, retrofit, and reverification. The flexibility of software programming also accelerates the schedule by permitting hardware design and build to proceed while software development is conducted in parallel. The use of wire-wrap interconnections greatly simplifies wiring alterations.

4.20.3 CONTROLLER INTERFACES

The main engine controller interfaces are listed in Table 4.20-3.

TABLE 4.20-3 CONTROLLER INTERFACES

REF. 224

<u>Interface</u>	<u>Baseline Number of Interface Circuits Required</u>	<u>Spare Interface Circuits Required</u>	<u>Total Number of Interface Circuits</u>
Vehicle Power Bus	3	0	3
Vehicle/Engine Electrical Interface			
a. Command Channels	3	0	3
b. Recorder Channels	2	0	2
Pressure Sensors			
a. External	28	6	34
b. Internal	2	0	2
Temperature Sensor			
a. Hot Gas (50 ohms)	4	2	6
b. LH2/LOX (5K ohms)	6	1	7
c. LH2/LOX (1.38K ohms)	1	5	6
d. Controller Internal	3	0	3
Leak Detection Sensors (Space Provision Only)			
Flow Sensors	8	2	10
Speed Sensors	8	0	8
Position Sensors			
a. Actuator	10	2	12
b. Servovalve/Bleed Valve	10	2	12
Vibration Sensors			
a. Radial	4	1	5
b. Longitudinal	3	1	4
Spark Igniter			
a. Command	6	0	6
b. Monitor	6	0	6
On/Off Solenoid Coils			
a. Pneumatic	7	2	9
b. Hydraulic	20	5	25
Servo Valve	8	2	10
GSE Interface			

REF. 4.20.3.1 VEHICLE/ENGINE ELECTRICAL INTERFACE
224

The vehicle to each engine controller interface will consist of eight individually twisted shielded pairs of wire. These wires will be divided into three command channels of two shielded pairs each and two recording channels of one shielded pair each. Each command channel will consist of one pair for transmission of commands to the controller and one pair for transmission of data and command echoes to the vehicle. Each recorder channel will consist of one pair for transmission of recorder data to the vehicle. For redundancy, the controller will have three connectors, one connector for each command channel with a recording channel in two of the connectors as defined in the ICD.

Vehicle to Controller Signal Characteristics

Transmission Rate:	10^6 bits per second
Code:	Manchester Bi-Phase (Level) Square Wave
Coupling:	Transformer Isolation
Characteristic Impedance:	150 ohms \pm 10 percent
Input Impedance:	Characteristic impedance
Input Voltage Impedance:	Greater than 5 volts p-p
Signal Rise time:	Less than 250 Nano-seconds
Signal Fall time:	Less than 250 Nano-seconds

REF. Vehicle to Controller Signal Characteristics (cont'd.)
224

Signal Overshoot:	Less than 20 percent
Signal Undershoot	Less than 20 percent
Skew:	Less than 32 microseconds between any two channels

Controller to Vehicle Signal Characteristics

Transmission Rate:	10^6 bits per second
Code:	Manchester Bi-Phase (Level) Square Wave
Coupling:	Transformer Isolation
Characteristic Impedance:	150 ohms \pm 10 percent
Driving Capability:	Minimum of 250 feet
Output Voltage Amplitude:	Greater than 5 volts p-p at receiving end
Signal Rise time:	Less than 250 nano-seconds
Signal Fall time:	Less than 250 nano-seconds
Signal Qvershoot:	Less than 20 percent
Signal Undershoot:	Less than 20 percent
Signal Droop:	Less than 20 percent
Skew:	Less than 32 microseconds between any two channels

REF.
224

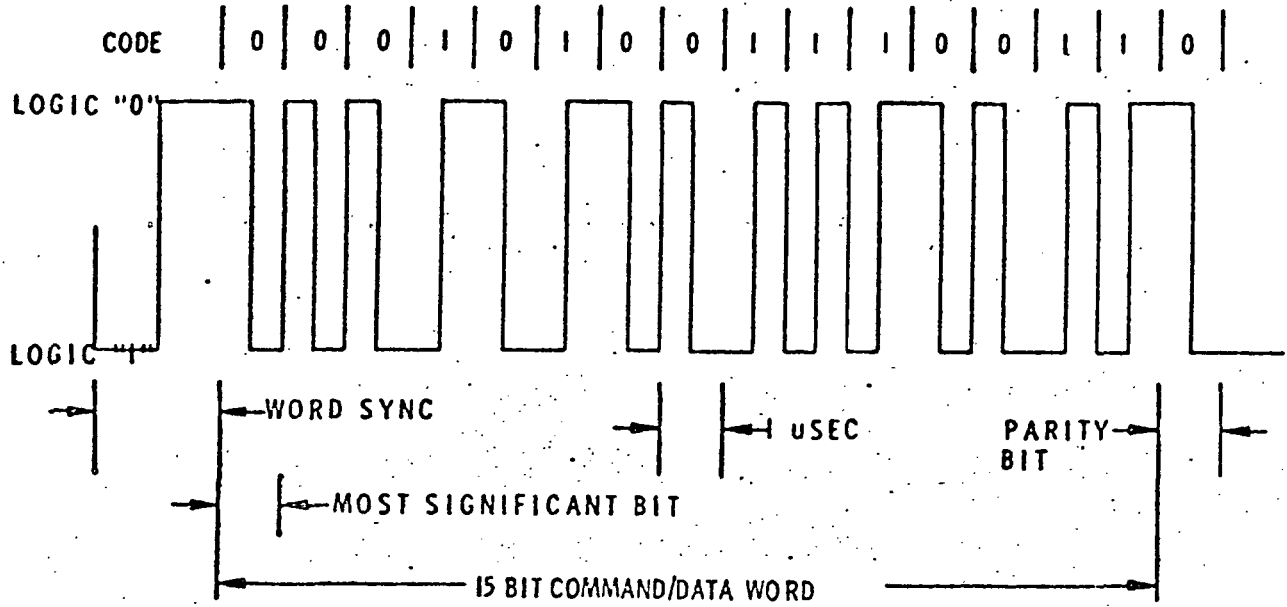
Channel Clock. The clock for each command channel will be derived from the respective command channel information. The clock for each engine status data and command echoes channel to the vehicle will be derived from the controller internal clock. The clock for each recorder channel will be derived from the controller internal clock.

Word Sync. The word sync pulse, for both command and recorder channels, will be designated by two consecutive 360 degree pulses. Each pulse will be one-bit time in duration. The polarity of the first pulse will be equal to the first 180 degrees of a logical "1" state. The polarity of the second pulse will be inverted from the polarity of the first pulse.

Command Word. Command words from the vehicle will consist of 15 bits plus a parity bit per word. The relationship between the word sync pulse, command information, and parity bit is shown in Figure 4.20-2. Valid commands are listed in Table 4.20-4. Command code format is shown in Table 4.20-5.

Commands from the vehicle will consist of two basic types of commands. These are defined as absolute commands (i.e., start, shutdown, automatic checkout, etc.) and variable commands (i.e., thrust and mixture ratio).

REF. 224



NOTE: MANCHESTER BI-PHASE LEVEL
"ONE" IS REPRESENTED BY A 10
"ZERO" IS REPRESENTED BY A 01

Figure 4.20-2 Command/Status, Echo and Recorder Word

TABLE 4.20-4 VEHICLE TO ENGINE COMMANDS

REF.
224

X - COMMAND ACCEPTED TO PERFORM CHECKOUT OF VEHICLE/ENGINE INTERFACE
 X - PHASES WHEN COMMAND IS ACCEPTED
 (X) - PHASES WHEN COMMAND IS NORMALLY REQUIRED BY ENGINE

CHECKOUT
 START PREPARATION
 START
 MAINSTAGE
 SHUTDOWN
 POST-SHUTDOWN

COMMAND	FUNCTION
AUTOMATIC CHECKOUT	INITIATES COMPLETE ENGINE CHECKOUT
PURGE SEQUENCE NO. 1	INITIATES 1) START PREPARATION PHASE 2) GN2 PURGE 3) HPOT INTERMEDIATE SEAL PURGE AND RELEASES FLOW-METER BRAKES
PURGE SEQUENCE NO. 2	INITIATES FUEL SYSTEM PURGE
PURGE SEQUENCE NO. 3	OPENS BLEED VALVES AND APPLIES PUMP LIFTOFF SEALS TERMINATES 1) FUEL SYSTEM PURGE 2) HPOT INTERMEDIATE SEAL PURGE AND APPLIES FLOWMETER BRAKES
PURGE SEQUENCE NO. 4	INITIATES FUEL SYSTEM PURGE DURING PROPELLANT RECIRCULATION
START	INITIATES 1) START PHASE 2) HPOT INTERMEDIATE SEAL PURGE AND RELEASES FLOWMETER BRAKES TERMINATES 1) GN2 PURGE 2) FUEL SYSTEM PURGE CLOSES BLEED VALVES AND RELEASES PUMP LIFTOFF SEALS

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TABLE 4.20-4 VEHICLE TO ENGINE COMMANDS (cont'd.) REF. 224

- COMMAND ACCEPTED TO PERFORM CHECKOUT OF VEHICLE/ENGINE INTERFACE
 X - PHASES WHEN COMMAND IS ACCEPTED
 - PHASES WHEN COMMAND IS NORMALLY REQUIRED BY ENGINE

FUNCTION

COMMAND

SHUTDOWN
 INITIATES ENGINE SHUTDOWN PHASE
 TERMINATES HPOT INTERMEDIATE SEAL PURGE
 AND APPLIES FLOWMETER BRAKES

THRUST LEVEL
 COMMANDS ENGINE THRUST LEVEL

MIXTURE RATIO
 COMMANDS ENGINE MIXTURE RATIO

COMMAND EXECUTE
 EXECUTES COMMAND AFTER VALIDATION

LIMIT CONTROL INHIBIT
 INHIBITS PREBURNER TEMPERATURE LIMIT
 CONTROL AND CONTROLLER INITIATED ENGINE
 SHUTDOWN

LIMIT CONTROL/ENABLE
 ENABLES PREBURNER TEMPERATURE LIMIT
 CONTROL AND CONTROLLER INITIATED ENGINE
 SHUTDOWN

ABORT TURNAROUND PURGE
 SEQUENCE NO. 1
 INITIATES 1) ABORT TURNAROUND MODE
 2) GN2 PURGE
 3) FUEL SYSTEM PURGE
 4) HPOT INTERMEDIATE SEAL
 PURGE AND RELEASES FLOW-
 METER BRAKES

ABORT TURNAROUND PURGE
 SEQUENCE NO. 2
 OPENS BLEED VALVES AND APPLIES
 PUMP LIFTOFF SEALS

CHECKOUT
 START PREPARATION
 START
 MAINSTAGE
 SHUTDOWN
 POST-SHUTDOWN

<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>

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TABLE 4.20-4 VEHICLE TO ENGINE COMMANDS (cont'd.)

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- COMMAND ACCEPTED TO PERFORM CHECKOUT OF VEHICLE/ENGINE INTERFACE

X - PHASES WHEN COMMAND IS ACCEPTED

- PHASES WHEN COMMAND IS NORMALLY REQUIRED BY ENGINE

CHECKOUT
START PREPARATION
START
MAINSTAGE
SHUTDOWN
POST-SHUTDOWN

COMMAND

FUNCTION

TBD

TBD

CONTROLS VALVES DURING ENGINE
COMPONENT CHECKOUT.

RESETS CONTROLLER TO INITIAL CONDITION
OF CHECKOUT PHASE - STANDBY OPERATING
SELFTEST MODE

INITIATES CHECKOUT OF FUEL FLOWMETER

INITIATES CHECKOUT OF OXIDIZER
FLOWMETER

INITIATES SIMULATED START AND SHUTDOWN
SEQUENCE

X FUEL DUMP

X TERMINATE PROPELLANT DUMP

MAIN FUEL VALVE

MAIN OXIDIZER VALVE

FUEL PREBURNER OXIDIZER VALVE

OXIDIZER PREBURNER OXIDIZER VALVE

COOLANT CONTROL VALVE

X CONTROLLER RESET

FUEL FLOWMETER SPIN TEST

OXIDIZER FLOWMETER SPIN TEST

SEQUENCE CHECK

X

X

X

X

X

X

X

X

X

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TABLE 4.20-4 VEHICLE TO ENGINE COMMANDS (cont'd.)

- COMMAND ACCEPTED TO PERFORM CHECKOUT OF VEHICLE/ENGINE INTERFACE
- X - PHASES WHEN COMMAND IS ACCEPTED
- PHASES WHEN COMMAND IS NORMALLY REQUIRED BY ENGINE

	COMMAND	FUNCTION
X	GN2 SYSTEM PURGE CONTROL VALVE	
X	FUEL SYSTEM PURGE CONTROL VALVE	
X	LIFTOFF SEAL AND BLEED VALVE CONTROL VALVE	
X	HPOT INTERMEDIATE SEAL PURGE AND FLOWMETER BRAKES CONTROL VALVE	INITIATES CHECKOUT OF PNEUMATIC VALVES DURING COMPONENT CHECKOUT
X	EMERGENCY SHUTDOWN CONTROL VALVE	
X	SENSOR CHECKOUT	INITIATES CHECKOUT OF SENSORS
X	SPARK IGNITER CHECKOUT	INITIATES CHECKOUT OF SPARK IGNITERS
X	STATUS REQUEST	REQUESTS CURRENT ENGINE STATUS

CHECKOUT
START PREPARATION
START
MAINSTAGE
SHUTDOWN
POST-SHUTDOWN

REF. 225

TABLE 4.20-5 VEHICLE/ENGINE COMMAND CODE FORMAT

BINARY CODE	OCTAL CODE	COMMAND
000 000 010 001 111	217	AUTOMATIC CHECKOUT
000 000 010 000 001	201	PURGE SEQUENCE NO. 1
000 000 010 000 010	202	PURGE SEQUENCE NO. 2
000 000 010 000 011	203	PURGE SEQUENCE NO. 3
000 000 010 000 100	204	PURGE SEQUENCE NO. 4
000 000 010 001 000	210	START
000 000 010 000 101	205	SHUTDOWN
000 000 001 000 000	100	THRUST LEVEL ⁽¹⁾
to	to	
000 000 001 111 011	173	
000 000 000 000 001	001	MIXTURE RATIO ⁽²⁾
to	to	
000 000 000 010 110	026	
000 000 011 000 010	302	COMMAND EXECUTE
000 000 010 000 110	206	LIMIT CONTROL INHIBIT
000 000 010 000 111	207	LIMIT CONTROL ENABLE
000 000 010 001 001	211	ABORT TURNAROUND PURGE SEQUENCE NO. 1
000 000 010 001 010	212	ABORT TURNAROUND PURGE SEQUENCE NO. 2
000 000 010 001 011	213	OXIDIZER DUMP
000 000 010 001 100	214	FUEL DUMP
000 000 010 001 101	215	TERMINATE PROPELLANT DUMP
000 000 010 010 000	220	MAIN FUEL VALVE
000 000 010 010 001	221	MAIN OXIDIZER VALVE
000 000 010 010 010	222	FUEL PREBURNER OXIDIZER VALVE
000 000 010 010 011	223	OXIDIZER PREBURNER OXIDIZER VALVE
000 000 010 010 100	224	COOLANT CONTROL VALVE
000 000 010 001 110	216	CONTROLLER RESET
000 000 010 011 100	234	FUEL FLOWMETER SPIN TEST
000 000 010 011 101	235	OXIDIZER FLOWMETER SPIN TEST
000 000 010 011 110	236	SEQUENCE CHECK
000 000 010 010 101	225	GN ₂ SYSTEM PURGE CONTROL VALVE
000 000 010 010 110	226	FUEL SYSTEM PURGE CONTROL VALVE

TABLE 4.20-5 VEHICLE/ENGINE COMMAND CODE FORMAT
(cont'd.)

BINARY CODE	OCTAL CODE	
000 000 010 010 111	227	LIFTOFF SEAL AND BLEED VALVE CONTROL VALVE
000 000 010 011 000	230	HPOT INTERMEDIATE SEAL PURGE AND FLOWMETER BRAKES CONTROL VALVE
000 000 010 011 001	231	EMERGENCY SHUTDOWN CONTROL VALVE
000 000 010 011 010	232	SENSOR CHECKOUT
000 000 010 011 011	233	SPARK IGNITER CHECKOUT
000 000 011 000 100	304	STATUS REQUEST
000 000 010 111 001	271	COMMAND CHANNEL 1 INHIBIT
000 000 010 111 010	272	COMMAND CHANNEL 2 INHIBIT
000 000 010 111 100	274	COMMAND CHANNEL 3 INHIBIT
000 000 010 110 001	261	COMMAND CHANNEL 1 ENABLE
000 000 010 110 010	262	COMMAND CHANNEL 2 ENABLE
000 000 010 110 100	264	COMMAND CHANNEL 3 ENABLE
000 000 011 111 111	377	MESSAGE REJECT (3)

NOTES:

1. Commands Thrust Level between 50 and 109 percent NPL in one percent increments.
2. Commands Mixture Ratio between 5.5 and 6.5 in 0.05 unit increments.
3. Code transmitted to vehicle from engine if voted command is determined invalid.

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Absolute commands will agree exactly in content for all operable command channels. Voting with 3 good channels, 2 of 3 agreement will constitute a good vote. After first channel failure, 2 out of 2 agreement will constitute a good vote.

The variable command which is executed, assuming that all 3 channels are good, will be the average of all 3 variable commands after it has been determined that all three are within a TBD percentage difference of each other. After the first channel failure, an average of 2 variables will be made to a variable TBD percentage difference. Command values which are outside this limit will be disregarded.

The interval between successive commands from the vehicle to the controller will be a minimum of 2 milliseconds. The number of commands from the vehicle to the controller will not exceed 3 commands for a 20 millisecond period.

Command Echoes to Vehicle. Commands from the vehicle will be echoed twice by the controller. Commands will be echoed immediately, upon receipt of a command, on each individual command channel exactly as received from the vehicle. Concurrent with the individual channel echo and commensurable with the allowable skew between command channels, the controller will initiate voting of commands from

REF. 224 all operable command channels. A validated command will result in the transmission of the voted command to the vehicle to indicate message acceptance by the controller. Conversely, a command which is voted and determined to be invalid by the controller due to disagreement or incorrect phase of engine operation, will result in the transmission of a "message reject" code to the vehicle indicating the command has been rejected. The transmission of either the voted command or message reject code will occur within 400 microseconds of receiving absolute type command words from all operable channels. The transmission of either the voted command or message reject code will occur within 600 microseconds of receiving variable type command words from all operable channels. All command word echoes will be transmitted on all command channels. The design of the controller will be such that, if in the future the command echo requirement is removed, the controller operation would not be degraded.

Execute Command. All commands from the vehicle, except the "status request" command, will be implemented with a "command execute" command. The command execute will be received from the vehicle within 200 microseconds following the transmission of the voted command from the controller.

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REF. 224 The controller will implement the most recent command which has been received and accepted prior to the command execute. Implementation will be concurrent with the transmission to the vehicle which indicates acceptance of the command execute.

Engine Status Data to Vehicle. The parameters listed in Table 4.20-6 Engine Status Transmitted to Vehicle, will be transmitted to the vehicle from the controller via the command channels in response to a "status request" command word. A command execute word is not required to initiate the transmission. The transmission of the parameters will be initiated immediately following the transmission of the voted status request echo. The format of the engine status data will be as shown in Figure 4.20-2 and Table 4.20-7 and will be transmitted on all command channels.

Word 4 of Tables v.20-6 and 4.20-9 is a failure identification of the items listed in Table 4.20-8 Failure Identification. Word 5 is an identifying test number associated with word 4 and shall include information concerning the number of failures experienced. This will not be limited to failures which cause redundancy switching but all detectable failures. Word 6 of Tables 4.20-6 and 4.20-9 is a parameter value associated with information contained in words 4 and 5. The data interval listed in

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TABLE 4.20-6 ENGINE STATUS TRANSMITTED TO VEHICLE

DATA	DATA WORD	SCALED RANGE	PRECISION OF DATA
ENGINE STATUS	1	-	
MIXTURE RATIO	2	0-8	±1%
THRUST	3	0-520K	±6K lbs.
FAILURE IDENTIFICATION	4	-	
TEST NUMBER OF DATA WORD NO. 4	5	-	
PARAMETER VALUE OF DATA WORD NO. 4	6	-	

NOTES:

1. THIS DATA PROVIDED TO VEHICLE VIA COMMAND CHANNELS IN RESPONSE TO A STATUS REQUEST COMMAND.
2. THESE 6 WORDS SHALL BE OBTAINED FROM SAME DATA TABLE AS FIRST 8 WORDS OF TABLE X.
3. THRUST AND MIXTURE RATIO VALUES ARE 15 BIT WORDS.

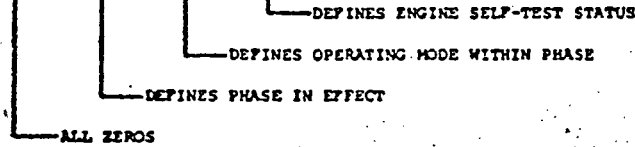
REF.
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TABLE 4.20-7 ENGINE STATUS WORD

WORD FORMAT



WORD EQUALS 15 BITS EXCLUDING PARITY BIT



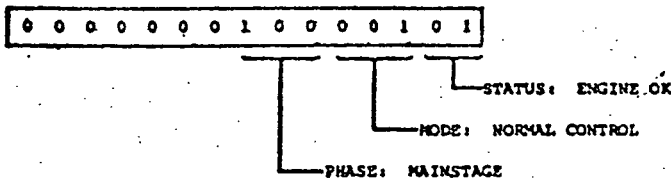
BYTE CODE

PHASE (3 BITS)		SELF TEST		STATUS (LAST 2 BITS)	
BIT CODE	PHASE NAME	BIT CODE	ENGINE STATUS		
000	(NOT USED)	00	(NOT USED)		
001	GROUND CHECKOUT	01	ENGINE OK		
010	START PREPARATION	10	COMPONENT FAILED		
011	START	11	ENGINE LIMIT EXCEEDED		
100	MAINSTAGE				
101	SHUTDOWN				
110	POST SHUTDOWN				
111	(SPARE)				

MODE BY PHASE (3 BITS)

PHASE BIT CODE	GROUND CHECKOUT	START PREPARATION	START	MAINSTAGE	SHUTDOWN	POST- SHUTDOWN
000	← NOT USED →					
001	STANDBY	PURGE SEQUENCE NO. 1	START INITIATION	NORMAL CONTROL	THROTTLING TO MPL	STANDBY
010	AUTOMATIC CHECKOUT	PURGE SEQUENCE NO. 2	CLOSED LOOP THRUST CONTROL	THRUST LIMITING	MPL TO ZERO THRUST	OXIDIZER DUMP
011	CHECKOUT COMPLETE	PURGE SEQUENCE NO. 3	THRUST LIMITING	FAIL SAFE ACTUATOR LOCKUP	PROPELLANT VALVES CLOSED	FUEL DUMP
100	COMPONENT CHECKOUT	PURGE SEQUENCE NO. 4	FAIL SAFE ACTUATOR LOCKUP	(SPARE)	FAIL SAFE PNEUMATIC	ABORT TURNAROUND SEQUENCE NO. 1
101	SEQUENCE CHECK	ENGINE READY	(SPARE)	(SPARE)	(SPARE)	ABORT TURNAROUND SEQUENCE NO. 2
110	(SPARE)	(SPARE)	(SPARE)	(SPARE)	(SPARE)	ENGINE READY
111	(SPARE)	(SPARE)	(SPARE)	(SPARE)	(SPARE)	(SPARE)

EXAMPLE OF WORD CODE AND INTERPRETATION



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TABLE 4.20-8 FAILURE IDENTIFICATION

1. Controller Channel 1
2. Controller Channel 2
3. GN2 Purge Control Valve
4. Fuel System Purge Control Valve
5. Emergency Shutdown Control Valve Channel 1
6. Emergency Shutdown Control Valve Channel 2
7. Invalid Vehicle Command
8. Liftoff Seal and Bleed Valve Control Valve
9. Pressure Actuated Fuel Bleed Valve
10. Pressure Actuated Oxidizer Bleed Valve
11. High Pressure Oxidizer Turbopump Intermediate Seal Purge and Flowmeter Brakes Control Valve Channel 1
12. High Pressure Oxidizer Turbopump Intermediate Seal Purge and Flowmeter Brakes Control Valve Channel 2
13. Oxidizer System Purge Pressure Sensor
14. Fuel System Purge Pressure Sensor
15. Fuel Liftoff Seal and Bleed Valve Control Pressure Sensor
16. Oxidizer Bleed Valve Control Pressure Sensor
17. High Pressure Oxidizer Turbopump Intermediate Seal Purge and Flowmeter Brakes Pressure Sensor Channel 1
18. High Pressure Oxidizer Turbopump Intermediate Seal Purge and Flowmeter Brakes Pressure Sensor Channel 2.
19. Fuel Preburner Igniter Channel 1
20. Fuel Preburner Igniter Channel 2
21. Oxidizer Preburner Igniter Channel 1
22. Oxidizer Preburner Igniter Channel 2

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TABLE 4.20-8 FAILURE IDENTIFICATION (cont'd.)

23. Main Combustion Chamber Igniter Channel 1
24. Main Combustion Chamber Igniter Channel 2
25. Main Fuel Valve Actuator Channel 1
26. Main Fuel Valve Actuator Channel 2
27. Main Oxidizer Valve Actuator Channel 1
28. Main Oxidizer Valve Actuator Channel 2
29. Main Combustion Chamber Coolant Valve Actuator Channel 1
30. Main Combustion Chamber Coolant Valve Actuator Channel 2
31. Fuel Preburner Oxidizer Valve Actuator Channel 1
32. Fuel Preburner Oxidizer Valve Actuator Channel 2
33. Oxidizer Preburner Oxidizer Valve Actuator Channel 1
34. Oxidizer Preburner Oxidizer Valve Actuator Channel 2
35. Spare
36. Spare
37. Spare
38. Spare
39. Spare
40. Spare
41. Spare
42. Spare
43. Low-Pressure Fuel Turbopump Discharge Pressure Sensor No. 1
Channel 1
44. Low-Pressure Fuel Turbopump Discharge Pressure Sensor No. 1
Channel 2

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TABLE 4.20-8 FAILURE IDENTIFICATION (cont'd.)

45. Low-Pressure Fuel Turbopump Discharge Pressure Sensor No. 2 Channel 1
46. Low-Pressure Fuel Turbopump Discharge Temperature Sensor No. 1 Channel 1
47. Low-Pressure Fuel Turbopump Discharge Temperature Sensor No. 1 Channel 2
48. Low-Pressure Fuel Turbopump Discharge Temperature Sensor No. 2 Channel 1
49. Low-Pressure Fuel Turbopump Shaft Speed Sensor
50. High Pressure Oxidizer Turbopump Turbine Seal Purge Pressure Sensor
51. Low-Pressure Fuel Turbopump Radial Vibration Sensor
52. Fuel Flowrate Sensor No. 1 Channel 1
53. Fuel Flowrate Sensor No. 1 Channel 2
54. Fuel Flowrate Sensor No. 2 Channel 1
55. Spare
56. Fuel Preburner Temperature Sensor No. 1
57. Fuel Preburner Temperature Sensor No. ~~2~~
58. Fuel Preburner Chamber Pressure Sensor
59. High-Pressure Fuel Turbopump Discharge Pressure Sensor
60. Spare
61. High-Pressure Fuel Turbopump Shaft Speed Sensor Channel 1
62. High-Pressure Fuel Turbopump Shaft Speed Sensor Channel 2
63. High-Pressure Fuel Turbopump Radial Vibration Sensor
64. Full Preburner Longitudinal Vibration Sensor

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TABLE 4.20-8 FAILURE IDENTIFICATION (cont'd.)

65. Low-Pressure Oxidizer Turbopump Discharge Pressure Sensor Channel 1
66. Low-Pressure Oxidizer Turbopump Discharge Pressure Sensor Channel 2
67. Low-Pressure Oxidizer Turbopump Shaft Speed Sensor
68. Spare
69. Low-Pressure Oxidizer Radial Vibration Sensor
70. High-Pressure Oxidizer Turbopump Discharge Pressure Sensor No. 1 Channel 1
71. High-Pressure Oxidizer Turbopump Discharge Pressure Sensor No. 1 Channel 2
72. High-Pressure Oxidizer Turbopump Discharge Pressure Sensor No. 2 Channel 1
73. High-Pressure Oxidizer Turbopump Discharge Temperature Sensor No. 1 Channel 1
74. High-Pressure Oxidizer Turbopump Discharge Temperature Sensor No. 1 Channel 2
75. High-Pressure Oxidizer Turbopump Discharge Temperature Sensor No. 2 Channel 1
76. High-Pressure Oxidizer Turbopump Shaft Speed Channel 1
77. High-Pressure Oxidizer Turbopump Shaft Speed Channel 2
78. High-Pressure Oxidizer Turbopump Boost Stage Discharge Pressure Sensor
79. High-Pressure Oxidizer Turbopump Radial Vibration Sensor
80. Oxidizer Preburner Temperature Sensor No. 1
81. Oxidizer Preburner Temperature Sensor No. 2
82. Oxidizer Preburner Chamber Pressure Sensor
83. Oxidizer Preburner Longitudinal Vibration Sensor

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TABLE 4.20-8 FAILURE IDENTIFICATION (cont'd.)

84. Oxidizer Flowrate Sensor No. 1 Channel 1
85. Oxidizer Flowrate Sensor No. 1 Channel 2
86. Oxidizer Flowrate Sensor No. 2 Channel 1
87. Spare
88. Oxidizer Tank Pressurant Pressure Sensor Channel 1
89. Oxidizer Tank Pressurant Pressure Sensor Channel 2
90. Main Combustion Chamber Fuel Injection Pressure Sensor
91. Main Combustion Chamber Pressure Sensor No. 1 Channel 1
92. Main Combustion Chamber Pressure Sensor No. 1 Channel 2
93. Main Combustion Chamber Pressure Sensor No. 2 Channel 1
94. Main Combustion Chamber Coolant Temperature Sensor
95. Main Combustion Chamber Coolant Pressure Sensor
96. Main Combustion Chamber Longitudinal Vibration Sensor
97. Hydraulic System Pressure Sensor Channel 1
98. Hydraulic System Pressure Sensor Channel 2
99. Controller Internal Temperature Sensor Channel 1
100. Controller Internal Temperature Sensor Channel 2
101. Controller Internal Pressure Sensor Channel 1
102. Controller Internal Pressure Sensor Channel 2
103. Vehicle/Engine Command Channel 1
104. Vehicle/Engine Command Channel 2
105. Vehicle/Engine Command Channel 3
106. Spare
107. Oxidizer Inlet Pressure Not Ready

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TABLE 4.20-8 FAILURE IDENTIFICATION (cont'd.)

- 108. Oxidizer Inlet Temperature Not Ready
- 109. Fuel Inlet Pressure Not Ready
- 110. Fuel Inlet Temperature Not Ready
- 111. Hydraulic System Pressure Out of Limits
- 112. Vehicle/Engine Recorder Channel 1
- 113. Vehicle/Engine Recorder Channel 2
- 114. Vehicle 400 Hz Power Bus No. 1
- 115. Vehicle 400 Hz Power Bus No. 2
- 116. Spare
- 117. Fuel Preburner Temperature Out of Limits
- 118. Oxidizer Preburner Temperature Out of Limits
- 119. High-Pressure Fuel Turbopump Shaft Speed Out of Limits
- 120. High-Pressure Oxidizer Turbopump Shaft Speed Out of Limits
- 121. Main Combustion Chamber Pressure Out of Limits
- 122. Oxidizer Heat Exchanger Pressure Drop Out of Limits
- 123. High Pressure Oxidizer Turbopump Intermediate Seal Purge and Flowmeter Brakes Pressure Out of Limits
- 124. and greater are Spares

NOTE: Channel Includes Sensor, Harness, Connectors and Controller Input or Output Electronics.

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TABLE 4.20-9 DATA TRANSMITTED TO RECORDER

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DATA (2)	DATA WORD	SCALED RANGE	PRECISION (3) OF DATA	DATA INTERVAL-MS
ENGINE STATUS	1	-		40
MIXTURE RATIO	2	0-8	±1%	40
THRUST	3	0-520K	±6K Lbs.	40
FAILURE IDENTIFICATION	4	-		40
TEST NUMBER OF DATA BYTE NO. 4	5	-		40
PARAMETER VALUE OF DATA BYTE NO. 4	6	-		40
LOW PRESSURE FUEL TURBOPUMP				
DISCHARGE PRESSURE	7-10	0-400 PSI	±2% F.S.	10
DISCHARGE TEMPERATURE	11	-430 to -405F	±2%	40
SHAFT SPEED	12	0-20,000 RPM	±1% F.S. (5)	40
RADIAL VIBRATION	13	0-300g RMS	±0.2 MV/g	40
FUEL FLOWRATE	14-17	0-18,000 GPM	±1% F.S. (4)	10
HIGH PRESSURE FUEL TURBOPUMP				
DISCHARGE PRESSURE	18-21	0-8000 PSI	±2% F.S.	10
SHAFT SPEED	22	0-45,000 RPM	±1% F.S. (5)	40
RADIAL VIBRATION	23	0-300g RMS	±0.2 MV/g	40
FUEL PREBURNER CHAMBER PRESSURE	24-25	0-7000 PSI	±2% F.S.	20
FUEL PREBURNER TEMPERATURE	26	0-2300 F	±2%	40
LOW PRESSURE OXIDIZER TURBOPUMP				
DISCHARGE PRESSURE	27-30	0-600 PSI	±2% F.S.	10
SHAFT SPEED	31	0-5500 RPM	±1% F.S. (5)	40
FACIAL VIBRATION	32	0-300g RMS	±0.2 MV/g	40
HIGH PRESSURE OXIDIZER TURBOPUMP				
DISCHARGE PRESSURE	33-36	0-7000 PSI	±2% F.S.	10
SHAFT SPEED	37	-300 to -250F	±2%	40
DISCHARGE TEMPERATURE	38-39	0-9500 PSI	±2% F.S.	20
BOOST STAGE DISCHARGE PRESSURE	40	0-35,000 RPM	±1% F.S. (5)	40
SHAFT SPEED	41	0-300g RMS	±0.2 MV/g	40
FACIAL VIBRATION	42-45	0-7000 GPM	±1% F.S. (4)	10
OXIDIZER FLOWRATE	46-47	0-7000 PSI	±2% F.S.	20
OXIDIZER PREBURNER CHAMBER PRESS.	48	0-2300F	±2%	40
OXIDIZER PREBURNER TEMPERATURE				
MAIN COMB. CHAMBER FUEL				
INJECTOR PRESSURE	49	0-4500 PSI	±2% F.S.	40
MAIN COMBUSTION CHAMBER PRESSURE	50-53	0-3500 PSI		

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TABLE 4.20-9 DATA TRANSMITTED TO RECORDER (cont'd.)

DATA (2)	DATA WORD	SCALED RANGE	PRECISION (3) OF DATA	DATA INTERVAL-MS
MAIN COMBUSTION CHAMBER				
COOLANT TEMPERATURE	54	-423 to +700F	±2%	40
OXIDIZER TANK PRESSURANT PRESSURE	55-56	0-6500 PSI	±2% F.S.	20
MAIN COMBUSTION CHAMBER				
COOLANT PRESSURE	57	0-6500 PSI	±2% F.S.	40
HYDRAULIC SYSTEM PRESSURE	58	0-4000 PSI	±2% F.S.	40
MAIN FUEL VALVE ACTUATOR POSITION	59	0-100%	±1% F.S.	40
MAIN OXIDIZER VALVE ACTUATOR POS.	60-61	0-100%	±1% F.S.	20
MAIN COMBUSTION CHAMBER COOLANT VALVE ACTUATOR POSITION	62	0-100%	±1% F.S.	40
OXIDIZER PREBURNER OXIDIZER VALVE ACTUATOR POSITION	63-64	0-100%	±1% F.S.	20
FUEL PREBURNER OXIDIZER VALVE ACTUATOR POSITION	65-66	0-100%	±1% F.S.	20
FUEL BLEED VALVE POSITION	67	0-100%	±1% F.S.	40
OXIDIZER BLEED VALVE POSITION	68	0-100%	±1% F.S.	40
OXIDIZER SYSTEM PURGE PRESSURE	69	0-1000 PSI	±2% F.S.	40
FUEL SYSTEM PURGE PRESSURE	70	0-1000 PSI	±2% F.S.	40
OXIDIZER BLEED VALVE CONTROL PRESSURE	71	0-1000 PSI	±2% F.S.	40
FUEL LIFTOFF SEAL AND BLEED VALVE CONTROL PRESSURE	72	0-1000 PSI	±2% F.S.	40
HPOT INTERMEDIATE SEAL PURGE & FLOWMETER BRAKE PRESSURE	73	0-100 PSI	±2% F.S.	40
HPOT				
TURBINE SEAL PURGE PRESSURE	74	0-1000 PSI	±2% F.S.	40
TIME REFERENCE	75	0-1000 PSI	±2% F.S.	40 (1)
FUEL PREBURNER LONGITUDINAL VIBRATION	76	0-1000g RMS	±0.2 MV/g	40
OXIDIZER PREBURNER LONGITUDINAL VIBRATION	77	0-1000g RMS	±0.2 MV/g	40
MAIN COMBUSTION CHAMBER LONGITUDINAL VIBRATION	78	0-1000g RMS	±0.2 MV/g	40
CONTROLLES INTERNAL PRESSURE	79	0-50 PSI	±2% F.S.	40

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TABLE 4.20-9 DATA TRANSMITTED TO RECORDER (cont'd.)

DATA(2)	DATA WORD	SCALED RANGE	PRECISION(3) OF DATA	DATA INTERVAL-MS
CONTROLLER INTERNAL TEMPERATURE	80	-320 to +300F	±2%	40
CONTROLLER BUS NO. 1 VOLTAGE	81	TBD	TBD	40
CONTROLLER BUS NO. 2 VOLTAGE	82	TBD	TBD	40
VEHICLE COMMANDS	83-88	-	-	40

NOTES:

- (1) Updated every 20 milliseconds, maximum value equals 5.10 seconds.
- (2) Data shall be transmitted at a rate of 25 times per second.
- (3) Precision of Thrust and Mixture Ratio is a firm requirement. Precisions stated for other data are desired values. Final precision values are to be determined.
- (4) Useable range of scaled flow data shall extend from 3 percent of full scale to 100 percent of full scale.
- (5) Data word order is not necessarily the order of transmission.
- (6) Word 83 contains first vehicle command received in a 40 millisecond period.

REF. 224 Table 4.20-9 will be alterable by modification of the controller's software program.

Data to Vehicle for Recording. The controller will initiate a transmission of the parameters listed in Table 4.20-9 Data Transmitted to Recorder to the vehicle on the recorder channels every 40 plus or minus 2 milliseconds. The transmission of recorder data will not be interrupted by command words from the vehicle. The data words for recording will consist of 15 bits plus a parity bit per word. The number of logical "ones" in the data word, including the parity bit will sum to an odd number. The relationship of the word sync pulse, data bits, and parity bit will be shown in Figure 4.20-2 and will be transmitted on all recorder channels. A "no data" message will be all zeros.

Operational Capability. The controller will be capable of full operation with the vehicle after the vehicle interface has experienced one failure (Fail Operational). The controller will continue operation in accordance with the most recent valid command after the vehicle interface has experienced a second failure (Fail Safe). The electronics interfacing with the vehicle in the controller must satisfy the requirement of no-single-point-failure (Fail Safe Design). Each failure in the receipt of a command

REF. word from the vehicle will be duly reported in the failure
224 identification provision in the transmission of engine status
data and recorder data to the vehicle. The appropriate
number will be inserted in the failure identification word.
The number of occurrences will be contained in the test
number word. Three consecutive transmission failures on
any command channel will cause that command channel to be
disqualified by the controller and the vehicle will have
the capability to reset the command channel.

Command Validation. The command words from the vehicle
to the controller will be verified by:

- (a) Correct number of bits per word
- (b) Parity check for each word
- (c) Direct vote of all operable inputs
- (d) Command execute word

The number of bits in each command word will include the
parity bit and will equal 16 bits. The parity check of
each word will sum the number of logical "ones" in a word,
including the parity bit, to be an odd number. Command
words from the vehicle which do not pass the number of
bits per word or parity check will be disregarded and
inhibited from entering the voting. Command words, which
are received from the vehicle but not implemented with a

REF. 224 command execute word, will be disregarded upon receipt of a new command word.

Command Channel Control. The controller will be capable, upon command of the vehicle, of disqualifying any single command channel which is found to be in error. Conversely, the controller will be capable, upon command of the vehicle, of removing the inhibit to any single command channel. Command words from the vehicle, to disqualify and restore individual command channels, will be via remaining operational command channels.

Intervals Between Transmissions. Command words consisting of a word sync pulse with the data bits and parity bit equal to logical "zero" will be received from the vehicle whenever any command listed in Table 4.20-4 Vehicle to Engine Commands is not being transmitted. Transmissions to the vehicle during periods of inactive transmission of engine status, command word echo, or recorder data, will consist of data words containing a word sync pulse with the data bits and parity bit equal to logical "zero".

REF. 4.20.3.2 CONTROLLER/ENGINE INTERFACES
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Sensor Input/Output Interfaces. The controller will conform to the requirements of this specification when interfaced with sensors having the following characteristics when installed on the engine. Sensor ranges and levels of redundancy will be as specified in Table 4.20-10 Sensor Ranges and Redundancy Levels.

(a) Pressure Sensors:

Input Impedance: 1250 to 2500 ohms at 75F. Change with temperature, 0.4 percent per 100F.

Output Impedance: 1500 plus or minus 150 ohms at 75F. Change with temperature, 0.4 percent per 100F.

Excitation Voltage: 10.00 plus or minus 0.025 volts dc

Output Voltage Range: 0 to 30 millivolts dc (nominal)

Error Band: plus or minus 0.6 millivolts dc from nominal straight line

Frequency Response: Greater than 600 rad per sec (equivalent first order)

Sensor Repeatability: Readings taken on each sensor under the same pressure conditions will repeat within plus or minus 0.87 percent of the NPL reading at all applicable environmental conditions. This is equivalent to plus or minus 0.75 percent of sensor full scale range. Individual sensor calibration constants, derived from curve fitting equations, will be supplied for the software program defined in RC1010. The form of the equation is:

$$y = a_0 + a_1 X + a_2 X^2 + \dots + a_n X^n$$

REF. 224 TABLE 4.20-10 SENSOR RANGES AND REDUNDANCY LEVELS

PARAMETER	REDUNDANCY	SENSOR RANGE
LOW PRESSURE FUEL TURBOPUMP		
DISCHARGE PRESSURE	3	0 to 400 PSIA
DISCHARGE TEMPERATURE	3	-423 to +700F (R ₀ =5000 ohms)
SHAFT SPEED	2*	0 to 20,000 RPM
FUEL FLOWRATE	4*	0 to 18,000 GPM
RADIAL VIBRATION	1	0 to 300 g RMS
HIGH PRESSURE FUEL TURBOPUMP		
DISCHARGE PRESSURE	1	0 to 8000 PSIA
SHAFT SPEED	2	0 to 45,000 RPM
RADIAL VIBRATION	1	0 to 300 g RMS
FUEL PREBURNER		
CHAMBER PRESSURE	1	0 to 7000 PSIA
TEMPERATURE	2	0 to 2300F (R ₀ =50 ohms)
LONGITUDINAL VIBRATION	1	0 to 1000 g RMS
LOW PRESSURE OXIDIZER TURBOPUMP		
DISCHARGE PRESSURE	2	0 to 600 PSIA
SHAFT SPEED	2*	0 to 5500 RPM
RADIAL VIBRATION	1	0 to 300 g RMS
HIGH PRESSURE OXIDIZER TURBOPUMP		
DISCHARGE TEMPERATURE	3	-423 to +700F (R ₀ =5000 ohms)
DISCHARGE PRESSURE	3	0 to 7000 PSIA
BOOST STAGE DISCHARGE PRESSURE	1	0 to 9500 PSIA
OXIDIZER TANK PRESSURANT PRESSURE	2	0 to 6500 PSIA
SHAFT SPEED	2	0 to 35,000 RPM
OXIDIZER FLOWRATE	4*	0 to 7000 GPM
RADIAL VIBRATION	1	0 to 300 g RMS

*One level of redundancy is used for checkout only.

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REF. 224 TABLE 4.20-10 SENSOR RANGES AND REDUNDANCY LEVELS (cont'd.)

PARAMETER	REDUNDANCY	SENSOR RANGE
OXIDIZER PREBURNER		
CHAMBER PRESSURE	1	0 to 7000 PSIA
TEMPERATURE	2	0 to 2300 F ($P_o = 50$ ohms)
LONGITUDINAL VIBRATION	1	0 to 1000 g RMS
MAIN COMBUSTION CHAMBER		
PRESSURE	3	0 to 3500 PSIA
FUEL INJECTION PRESSURE	1	0 to 4500 PSIA
COOLANT TEMPERATURE	1	-423 to +700 F ($P_o = 1380$ ohms)
COOLANT PRESSURE	1	0 to 6500 PSIA
LONGITUDINAL VIBRATION	1	0 to 1000 g RMS
HYDRAULIC SYSTEM PRESSURE		
	2	0 to 4000 PSIA
PNEUMATIC CONTROL SYSTEM		
OXIDIZER SYSTEM PURGE PRESSURE	1	0 to 1000 PSIA
FUEL SYSTEM PURGE PRESSURE	1	0 to 1000 PSIA
OXIDIZER LIFTOFF SEAL AND BLEED VALVE CONTROL PRESSURE	1	0 to 1000 PSIA
FUEL LIFTOFF SEAL AND BLEED VALVE CONTROL PRESSURE	1	0 to 1000 PSIA
HIGH PRESSURE OXIDIZER TURBOPUMP INTERMEDIATE SEAL PURGE AND FLOWMETER PRAGES PRESSURE	2	0 to 100 PSIA
HIGH PRESSURE OXIDIZER TURBOPUMP TURBINE SEAL PURGE PRESSURE	1	0 to 1000 PSIA
CONTROLLER		
PRESSURE	2	0 to 50 PSIA
TEMPERATURE - OPERATING	2	-320 to +300 F ($P_o = 200$ ohms)
TEMPERATURE - NON-OPERATING	1	-320 to +300 F ($P_o = 200$ ohms)

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TABLE 4.20-10 SENSOR RANGES AND REDUNDANCY LEVELS (cont'd.)

REF. 224

PARAMETER

REDUNDANCY

SENSOR RANGE

FLOW CONTROL VALVES

MAIN FUEL VALVE

ROTATION	-	0 to 90 DEGREES
ACTUATOR STROKE	-	2.500 in NOMINAL
ACTUATOR LVDT SENSITIVITY	2	1.40 VOLTS p-p/in NOMINAL

MAIN OXIDIZER VALVE

ROTATION	-	0 to 90 DEGREES
ACTUATOR STROKE	-	2.389 in NOMINAL
ACTUATOR LVDT SENSITIVITY	2	1.47 VOLTS p-p/in NOMINAL
SERVOVALVE SPOOL LVDT SENSITIVITY	2	15.6 VOLTS p-p/in NOMINAL

OXIDIZER PREBURNER OXIDIZER VALVE

ROTATION	-	0 to 90 DEGREES
ACTUATOR STROKE	-	1.286 in NOMINAL
ACTUATOR LVDT SENSITIVITY	2	2.72 VOLTS p-p/in NOMINAL
SERVOVALVE SPOOL LVDT SENSITIVITY	2	15.6 VOLTS p-p/in NOMINAL

FUEL PREBURNER OXIDIZER VALVE

ROTATION	-	0 to 90 DEGREES
ACTUATOR STROKE	-	1.286 in NOMINAL
ACTUATOR LVDT SENSITIVITY	2	2.72 VOLTS p-p/in NOMINAL
SERVOVALVE SPOOL LVDT SENSITIVITY	2	15.6 VOLTS p-p/in NOMINAL

MAIN COMBUSTION CHAMBER COOLANT VALVE

ROTATION	-	0 to 90 DEGREES
ACTUATOR STROKE	-	1.286 in NOMINAL
ACTUATOR LVDT SENSITIVITY	2	2.72 VOLTS p-p/in NOMINAL
SERVOVALVE SPOOL LVDT SENSITIVITY	2	15.6 VOLTS p-p/in NOMINAL

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REF. 224 TABLE 4.20-10 SENSOR RANGES AND REDUNDANCY LEVELS (cont'd.)

PARAMETER	REDUNDANCY	SENSOR RANGE
FUEL BLEED VALVE		
STROKE	- 1	0 to 0.133 in NOMINAL
LVDT SENSITIVITY		PROPORTIONAL TO SQUARE ROOT OF DISTANCE FROM SENSITIVE FACE
OXIDIZER BLEED VALVE		
STROKE	- 1	0 to 0.133 in NOMINAL
LVDT SENSITIVITY		PROPORTIONAL TO SQUARE ROOT OF DISTANCE FROM SENSITIVE FACE

REF. 224

(b) Temperature Sensors:Sensor Output: $R_T/R_0 = 1 + \alpha [(T - \delta T(T-100)/10^4) - \beta T^3(T-100)/10^8]$

where: T = Temperature in Centigrade

 $\alpha = 0.00391$ to 0.0039275 $\delta = 1.492 \pm 0.07$ $\beta = 0.11 \pm 0.035$ R_T = Sensor resistance at T (ohms) R_0 = Sensor resistance at 0C= 50±1, 200±2, 1380±3, or 5000±10 ohms
as specified in Table 4.20-10Sensor Excitation
Current:

2 milliamperes dc maximum

Sensor Response:

Equivalent first order time constant of 0.5
sec for sensors with R_0 of 50 and 200 ohms;
0.1 sec for sensors with R_0 of 1380 and 5000
ohms at the engine operating flowrate
conditions

Sensor Repeatability:

Readings taken on each sensor under the same
temperature conditions will repeat within
plus or minus 0.25 percent of the measurement
span at all applicable environmental condi-
tions. Individual sensor calibration
constants, derived from curve fitting equa-
tions, will be supplied for the software
program defined in RC1010. The form of the
equation is:

$$y = a_0 + a_1 X + a_2 X^2 + \dots + a_n X^n$$

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(c) Flow Sensors

Sensor Coil Resistance: 1500 ohms maximum

Sensor Coil Inductance: 1.0 henry maximum at 1 K Hz

Sensor Output Voltage:
(Peak to Peak) 0.2 minimum to 10.0 maximum
(Based on resistive load of
10 plus or minus 2 K ohms)
over the frequency range of
5 to 500 Hz.

Flowmeter Frequency
Response: Greater than 200 rad per sec
(equivalent first order)

3 Sigma Precision: plus or minus 0.45 percent of
reading at all applicable
environmental conditions

Pulse characteristics for flow sensor outputs are TBD.

(d) Position Sensors - Servo Valves and Bleed Valves

Sensor Primary Current: 20 milliamperes maximum

Sensor Excitation
Voltage: 20 volts peak-to-peak
(nominal)

Sensor Excitation
Frequency: 2000 plus or minus 100 Hz

Sensor Output Range: minus 0.25 to plus 0.25 volts
peak-to-peak (nominal)
when operating into a 10 K
ohm resistive load

Sensor Error Band: plus or minus 0.5 percent of
point plus or minus
0.5 percent full scale
deviation from nominal
straight line

Sensor Output Phase
Shift: 0 to 5 degrees

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(e) Vibration Sensors

Sensor Source Capacitance:

2000 picofarad minimum

Sensor Output Voltage:

5.0 plus or minus 0.7 millivolt RMS per g RMS operating into a load of 300 picofarads in parallel with 100 megohms.

Sensor Frequency Range:

1 Hz to 6 K Hz (300 g) for radial (turbopumps)
100 Hz to 15 K Hz (1000 g) for longitudinal (combustors)

Sensor Frequency Response:

Greater than 10 K Hz (equivalent first order)

Vibration sensors are for the purpose of obtaining and recording engine maintenance trend data. Controller input circuits for the longitudinal vibration sensors shall be capable of selectively sampling predetermined frequency windows throughout the frequency range of the sensor. Controller input circuits for the radial vibration shall be sensitive to a narrow frequency band centered about the fundamental rotating frequency of the appropriate turbopump. Vibration sensor inputs shall be demodulated and sampled at a frequency rate sufficient to satisfy the data requirements for the vibration parameters listed in Table 4.20-9 Data Transmitted to Recorder.

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(f) Position Sensors - Hydraulic Actuators

Sensor Primary Current:	20 milliamperes maximum
Sensor Excitation Voltage:	20 volts peak-to-peak (nominal)
Sensor Excitation Frequency:	2000 plus or minus 100 Hz.
Sensor Output Range:	0.25 to 4.75 volts peak-to-peak (nominal) when operating into a 10 K ohm resistive load
Sensor Error Band:	plus or minus 0.5 percent of point plus or minus 0.5 percent full scale deviation from nominal straight line
Sensor Output Phase Shift:	0 to 5 degrees

(g) Speed Sensors

Sensor Coil Resistance:	1500 ohms maximum
Sensor Coil Inductance:	0.1 henry maximum at 1 K Hz
Sensor Output Voltage: (Peak-to-Peak)	0.2 minimum to 16.0 maximum (Based on resistive load of 10 plus or minus 2 K ohms)
Sensor Output Frequency Range:	400 Hz to 10 K Hz

Pulse characteristics for speed sensor outputs are TBD.

(h) Leak Detection Sensors

Leak detection sensors may be added at a later date. Since sensor and circuit characteristics are not defined, space equivalent to 80 square inches of circuit board shall be reserved.

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Igniter and Control Devices Interface. The controller will conform to the requirements of this specification when interfaced with igniters and control devices having the following characteristics when installed on the engine.

(a) Servoactuators

Servo Valve Load Resistance:	500 ohms max.
Servo Valve Current Range:	\pm 20 milliamperes dc
Actuator Closed-Loop Frequency Response: (Equiv. second order):	
Main Oxidizer Valve Area:	4 to 10 Hz
Oxidizer Preburner Oxidizer Valve Area:	12 to 20 Hz
Fuel Preburner Oxidizer Valve Area:	12 to 20 Hz
Combustion Coolant Valve Area:	12 to 20 Hz
Actuator Closed-Loop Damping Ratio:	0.5 minimum
Actuator Closed-Loop Threshold:	1% full scale max.
Actuator Closed-Loop Slew Rate:	
Main Oxidizer Valve Area:	150 to 300% per second
Main Fuel Valve Area:	250 to 400% per second
Oxidizer Preburner Oxidizer Valve Area:	150 to 250% per second
Fuel Preburner Oxidizer Valve Area:	150 to 250% per second
Combustion Coolant Valve Area:	150 to 250% per second

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REF. 224 (b) Solenoid Valves (Non-Latching)

Coil Current (Energizing): 1 ampere dc max.

Coil Current (Holding): 0.5 ampere dc max.

Coil Voltage (On): 26 volts dc max.

Valve Response Time:

Pneumatic - Electrically Actuated: 20 milliseconds max.

Pneumatic - Pressure actuated: 50 milliseconds max.

Hydraulic Actuator Solenoids: 14 milliseconds max.

Coil Inductance: 0.05 to 0.3 henries

Valve response time is defined as the time interval from the application of the electrical signal to the completion of the travel of the actuated device.

(c) Spark Igniters

Igniter Power Supply Current (On): 1 ampere dc max.

Igniter Control Current (on): 50 milliamperes dc max.

Igniter Voltage (On): 26 volts dc max.

The servoactuators and solenoid coils will be driven by current sources. The controller will contain networks to suppress electrical transients and protect solenoid coil driver circuits. The spark igniters will be driven by voltage sources. The solenoid valve and igniter control current in the off-state will not exceed 5 milliamperes dc and 1 milli-ampere dc, respectively.

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REF. 4.20.3.3 GROUND EQUIPMENT INTERFACE
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The controller shall contain ground support equipment (GSE) interface connections in accordance with RC1009. The GSE interface will be capable of duplicating the commands and data transmission normally provided through the vehicle/engine electrical interface, and the controller will be capable of operating the engine while installed on the vehicle through this GSE interface. Controller electrical power will be supplied through the vehicle power interface during this mode of operation. The GSE interface will contain provisions for complete reprogramming and verification of the controller memory without removing the controller from the engine. The controller design will preclude acceptance of commands from the vehicle/engine electrical interface when the GSE interface is connected to operating external ground equipment.

REF. 4.20.4 CONTROLLER HARDWARE

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4.20.4.1 INPUT ELECTRONICS DESCRIPTION

The input electronics (Figure 4.20-3) receive analog and pulse rate signals from all inflight sensors, including temperature, pressure, vibration, position, rotational speed and flow rate. Built-in test signals from other portions of the controller are also received. The incoming signals are "conditioned" by amplification, filtering and/or demodulation and then converted to digital form suitable for the computer. Data from nonflight sensors for test stand requirements are not processed through the input electronics.

Because two independent digital computers are necessary for fail-operational/fail-safe performance, two sets of input electronics are provided. One set of input electronics is assigned to each digital computer. These sets are designated as Number 1 and Number 2.

In addition, each of the two sets of electronics contains three redundant data channels, designated A, B, and C, to match the triple redundant inputs from the performance control sensors (see Figure 4.20-4). Inputs from dual redundant limit control sensors, non-redundant maintenance data sensors, and built-in test are distributed among the three data channels in a manner which preserves redundancy

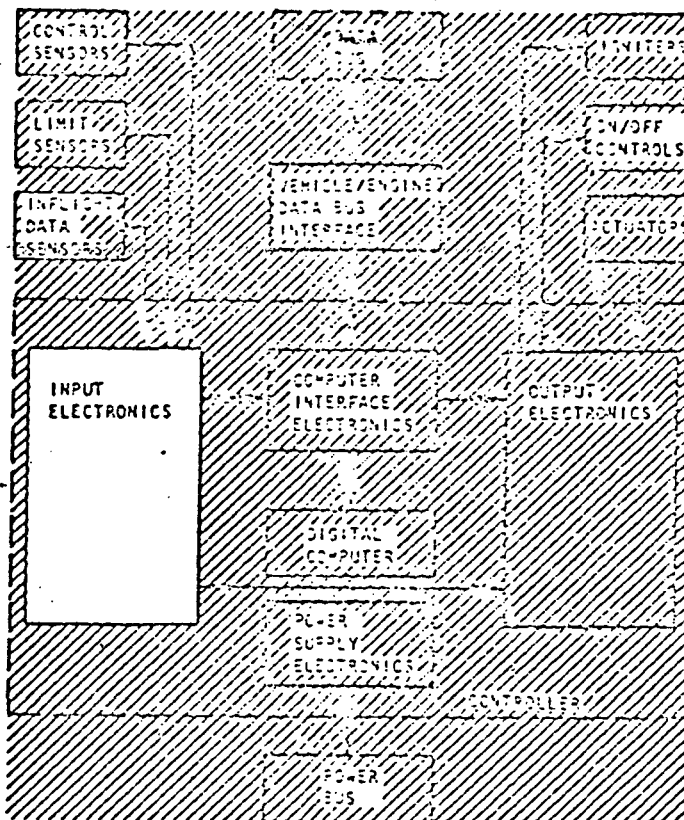


Figure 4.20-3 Input Electronics

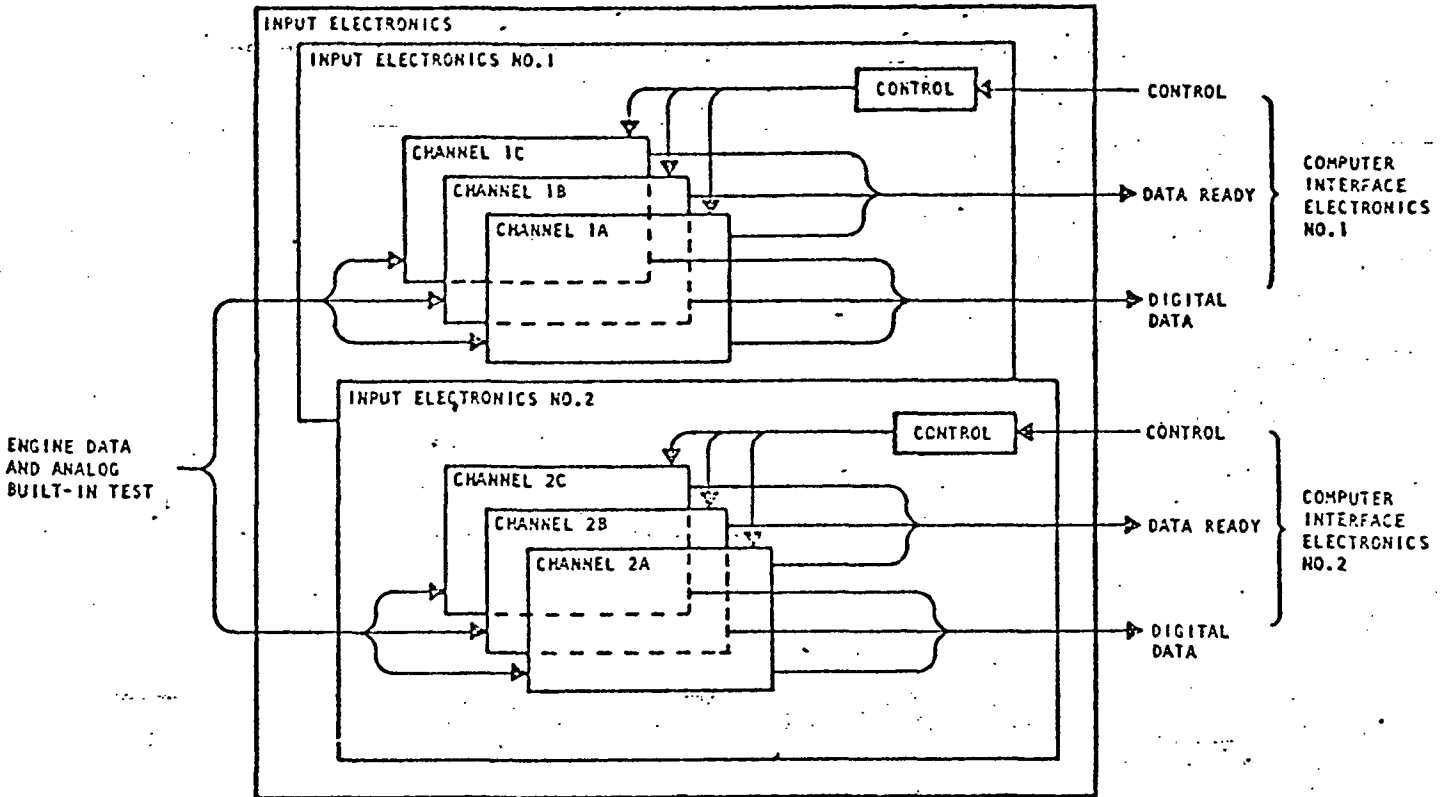


Figure 4.20-4 Input Electronics Organization

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REF. and at the same time achieves equality of signal flow between
42 the channels. The latter is significant because it minimizes data processing time and achieves a fast high response sampling rate. Each of the three data channels in a set of input electronics processes approximately one-third of all the engine inflight sensor outputs.

Input Channel Function

The basic function of each input channel is to convert the analog and pulse rate sensor and built-in test signals to digital form. In order to handle the many pieces of data from multiple sensors with a minimum of hardware, each channel samples or multiplexes the data in a time sequence. Each input is sampled once every 20 msecond operating cycle, conditioned, converted to digital format, and sent to the computer interface electronics.

The signal conditioning and conversion functions for a typical data channel are shown in Figure 4.20-5. To minimize hardware costs, all data channels are identical. The only functional differences are minor variations in the quantities and types of inputs to each channel to accommodate the requirements for sensor redundancy.

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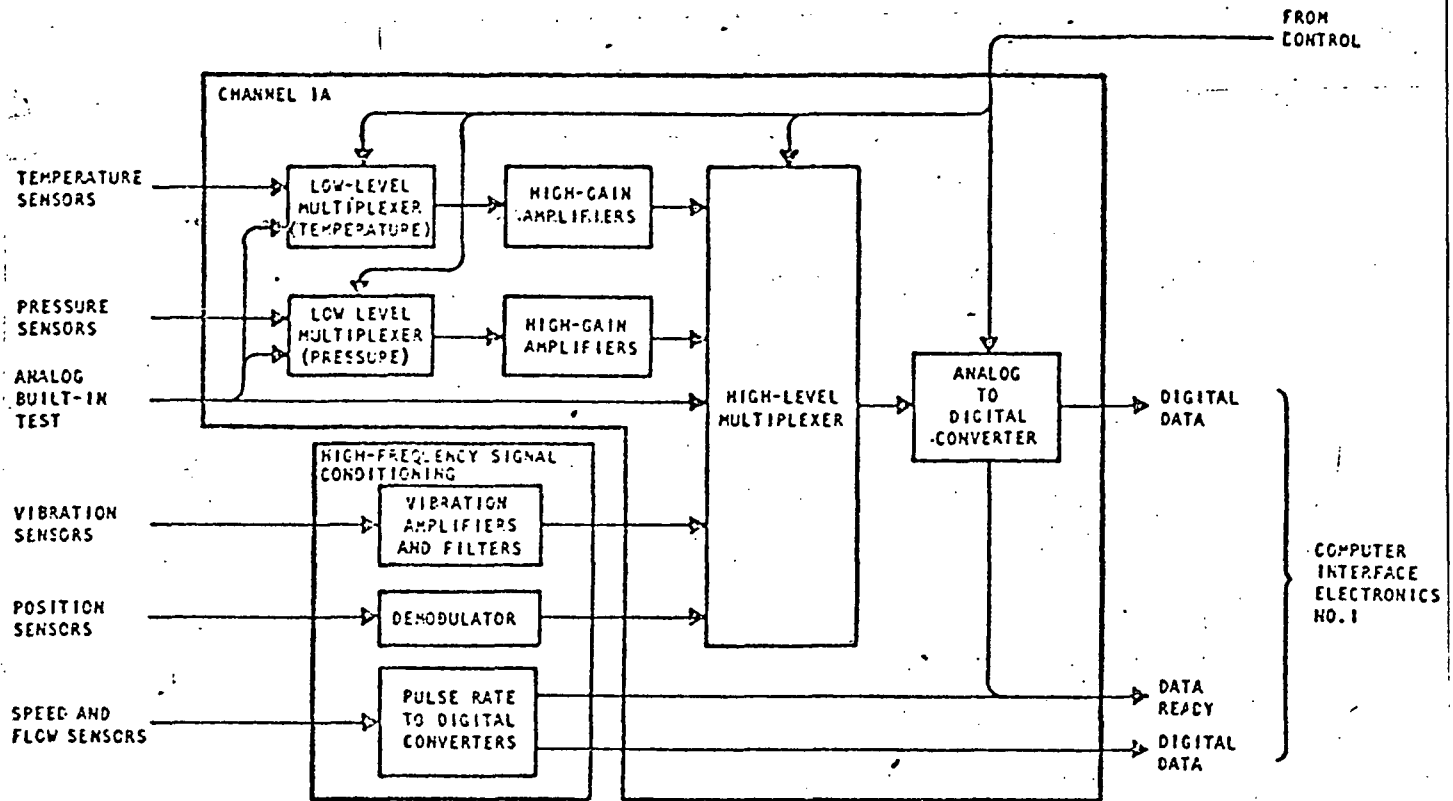


Figure 4.20-5 Input Electronics Channel
(Typical 1 of 6)

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Each input channel has the following additional functions:

1. Distributes redundant dc excitation voltages to the temperature and pressure sensors, and provides reference voltages to the analog-to-digital converters.
2. Generates signals for self-calibration.
3. Provides test signals and switching for sensor calibration and integrity checks.
4. Accepts analog built-in test inputs from power supply and output electronics.

Each input data channel is independently supplied from two sets of redundant power supply regulators. Sensor excitation and converter reference voltages are supplied from the same regulators used to power the respective electronics to take advantage of the resulting cancellation of errors from power supply voltage variations. Failure of a data channel or its regulated power supplies will not propagate into another channel. Figure 4-20-5 presents a complete discussion of power supply decoupling and redundancy.

REF
42Types of Inputs

Two categories of inputs are processed: one is analog and the other is a variable pulse rate where the voltage amplitude and the pulse rate, respectively, are proportional to the measured parameter.

Analog temperature, pressure, vibration, position, and built-in test signals are conditioned through low-level multiplexer gates, amplifiers, and/or modulators to achieve a common scale factor. As shown in Figure 4.20-5, these are then gated through a high-level multiplexer to the analog-to-digital converter. The analog-to-digital converter transforms the high-level multiplexer analog outputs to digital words. Parallel sequencing of the analog-to-digital conversion in all three channels is regulated by the computer interface electronics through a common control in each set of electronics. At fixed intervals, when a conversion is complete, the three data channel digital outputs are transferred sequentially by the computer interface electronics to the computer to update the memory. The transfer is completed in 1 memory cycle (1 microsecond). Data transfer of sensor and built-in test values continues until all inputs have been sampled. The process is repeated every 20 msec for a new sampling cycle.

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A common control unit associated with each set of input electronics regulates the sequencing of the multiplexing and the analog-to-digital conversion in the three associated data channels by decoding control signals from the computer interface electronics.

~~Low-level~~ Low-level multiplexing reduces the number of components by requiring a single high-gain amplifier for up to eight temperature or pressure inputs. It also improves performance by permitting calibration and reference signals to be multiplexed through the high-gain amplifiers to check and correct amplifier gain and offset. Normalizing all the high-level multiplexer inputs to a common scale factor reduces the number of multiplexer components by a factor of 2.

Pulse rate shaft speed and flow rate signals are converted directly to digital format by measuring the pulse period with a high frequency precision clock signal. This yields the reciprocal of the measured parameter. Each pulse rate input is processed through a separate converter. When a conversion is complete, the computer interface electronics transfer the data to the computer in 1 microsecond to update the memory.

REF.
42Analog Signal Processing

Processing of the various analog inputs for a typical channel shown in Figure 4.20-5 is as follows:

1. Temperature sensor dc inputs to each channel are processed through a corresponding number of low-level multiplexer gates to one common programable-gain amplifier. A reference ground is multiplexed into the amplifier just prior to each sensor signal. This improves accuracy by erasing residual signals from prior inputs. Sensor operating range and range midpoint values are multiplexed simultaneously with each sensor input to adjust the amplifier gain and offset for maximum dynamic scaling. The high-gain amplifier output is gated through the high-level multiplexer to the analog-to-digital converter.
2. Pressure sensor dc inputs are processed in a manner similar to those of temperature sensors. The number of inputs to each high-gain amplifier is limited to ensure that gate leakage does not adversely affect the precision of the low-level pressure signals.
3. Vibration sensor ac inputs are individually amplified, filtered, and multiplexed directly through the high-level multiplexer to the analog-to-digital converter. The

REF. 42 amplifier is operated in the current mode to protect the high-impedance, low-level signal from electrical noise pickup in the engine or in the controller. In this mode the signal from the sensor feeds directly to the input of an operational amplifier acting as a charge integrator.

4. Linear position sensor ac inputs are demodulated to an analog voltage, scaled, and multiplexed directly to the analog-to-digital converter. The use of an operational amplifier and full-wave synchronous demodulation provides good accuracy and high-frequency response.

5. Analog built-in test signals from the output electronics and the power supply electronics are gated through the high-level multiplexer to the analog-to-digital converter. Calibration signals to verify the operation and/or accuracy of the input electronics are supplied in accordance with Table 4.20-11. The measured outputs are used by the computers to continuously recalibrate the input electronics by automatic software changes:

Digital output word format is 12 bits from the analog-to-digital converter. Twelve bits provide a resolution of one part in 4095 or 0.025 percent, which is more than adequate to meet engine accuracy requirements. Total

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TABLE 4.20-11 INPUT ELECTRONICS CALIBRATION

FUNCTION	TEST SIGNAL			PARAMETER MEASURED	USAGE	
	TYPE	INPUT	OUTPUT		IN FLIGHT	GROUND CHECKOUT
ANALOG TO DIGITAL CONVERTER	REFERENCE VOLTAGE	HIGH-LEVEL MULTIPLEXER	ANALOG/DIGITAL (A/D) CONVERTER OUTPUT	CONVERTER GAIN	X	X
	REFERENCE GROUND	HIGH-LEVEL MULTIPLEXER	A/D CONVERTER OUTPUT	CONVERTER OFFSET	X	X
HIGH-LEVEL MULTIPLEXER	REFERENCE VOLTAGE	HIGH-LEVEL MULTIPLEXER	ANALOG/DIGITAL (A/D) CONVERTER OUTPUT	MULTIPLEXER OPERATION	X	X
HIGH-GAIN AMPLIFIER	REFERENCE VOLTAGE	LOW-LEVEL MULTIPLEXER	A/D CONVERTER OUTPUT	AMPLIFIER GAIN	X	X
	REFERENCE GROUND	LOW-LEVEL MULTIPLEXER	A/D CONVERTER OUTPUT	AMPLIFIER OFFSET	X	X
LOW-LEVEL MULTIPLEXER	REFERENCE VOLTAGE	LOW-LEVEL MULTIPLEXER	A/D CONVERTER OUTPUT	MULTIPLEXER OPERATION	X	X
ACCELERATION AMPLIFIER	REFERENCE VOLTAGE	AMPLIFIER INPUT	A/D CONVERTER OUTPUT	AMPLIFIER GAIN		X
LINEAR POSITION DEMODULATOR	(1)					X
PULSE RATE CONVERTER	KNOWN FREQUENCY	REDUNDANT SENSOR WINDING	REDUNDANT PULSE RATE CONVERTER	SENSOR AND CONVERTER OPERATION		X

(1) CALIBRATED DURING BUILT-IN TEST BY COMPARISON OF COMMANDED POSITION WITH THAT DERIVED FROM DEMODULATED LINEAR VARIABLE DIFFERENTIAL TRANSDUCER FEEDBACK

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accuracy of the analog-to-digital converter is ± 0.223 percent random and 0.07 percent non-random.

Analog Signal Control

All multiplex switching and analog-to-digital conversions are under the control of the computer interface electronics. A conversion cycle is initiated every 200 microsec. upon receipt of an 11-bit word from the control unit in each set of input electronics. (Figure 4.20-4). Eight bits contain the addresses of the multiplexer gates to be closed for that particular conversion, and 3 bits provide synchronizing information. Control of the multiplexing and conversion process occurs in the following sequence:

1. Receipt of coded control signal by the control. Control addresses and closes designated low- and high-level gates in the three channels (A, B, and C). Control admits timing clock signal to analog-to-digital converters.
2. Timing circuits initiate analog-to-digital conversion after a suitable settling time.
3. Upon completion of conversion (which requires an average of 110 microseconds, excluding settling and decoupling time), each converter sends a data ready signal to the computer interface electronics.

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4. When data ready signals are received from all three channels, the computer interface electronics sequentially acquires the digital data from the converters. If due to a failure, a data ready signal is not received from one or more channels within 190 microsec of initiation of the conversion, the acquisition is performed on the remaining channels.

The process is then repeated for a new set of multiplexed signals. All input signals are sampled once every 20 msec.

Pulse Rate Signal Processing

Each pump speed or flow rate signal is routed directly to its respective pulse-rate-to-digital converter. The pulse period is measured by a clock signal to provide an output proportional to the reciprocal of pulse rate. Pulse-rate-to-digital conversion occurs asynchronously with the analog-to-digital conversion. The frequency of conversion is proportional to the pulse rate. As each conversion is completed, a data ready signal is transmitted to the computer interface electronics. The output is held in the converter for a period dependent upon the incoming pulse rate. The computer interface electronics has the option of acquiring the output data during this period or waiting for the next output if occupied with higher priority operations.

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The pulse-rate-to-digital converter outputs are 16-bit words, providing a resolution of 0.015 percent at full scale (minimum pulse period) and 0.0015 percent at 10-percent scale.

4.20.4.2 COMPUTER INTERFACE ELECTRONICS DESCRIPTION

The computer interface electronics (Figure 4.20-6) control data flow to and from the computers. Each of two electronic sets (Figure 4.20-7) is dedicated to a computer and a set of input electronics performing the functions of:

1. Transferring the commands and data requests from the vehicle/engine data bus interface to the computer, and the data responses from the computer to the vehicle/engine data bus.
2. Controlling the flow of data between the computer and the input and output electronics.
3. Monitoring computer operation by watch-dog timers.
4. Providing a redundant time reference to the digital computer.

The above functions are performed by groups of circuits in each set of electronics, as shown in Figure 4.20-8. These are:

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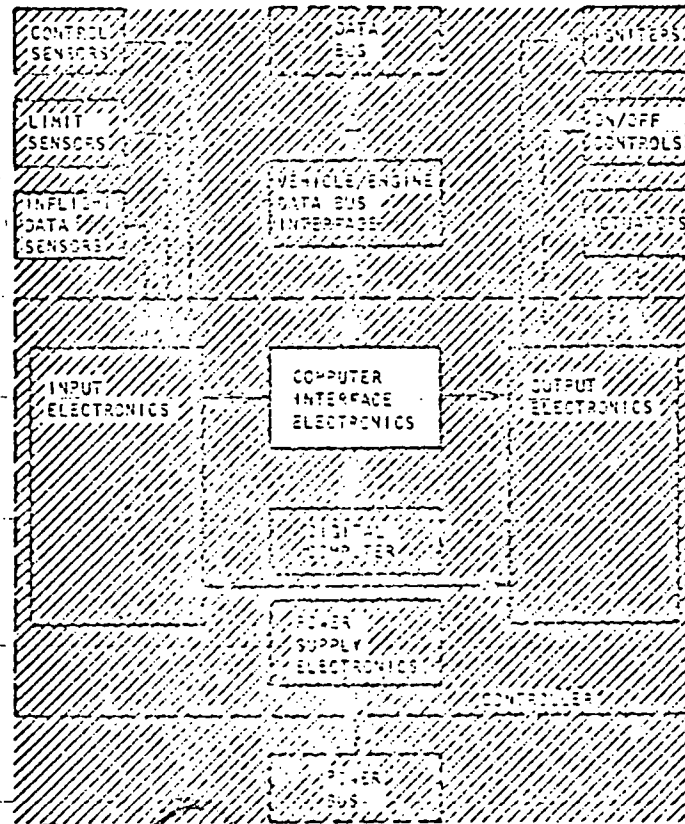


Figure 4.20-6 Computer Interface Electronics

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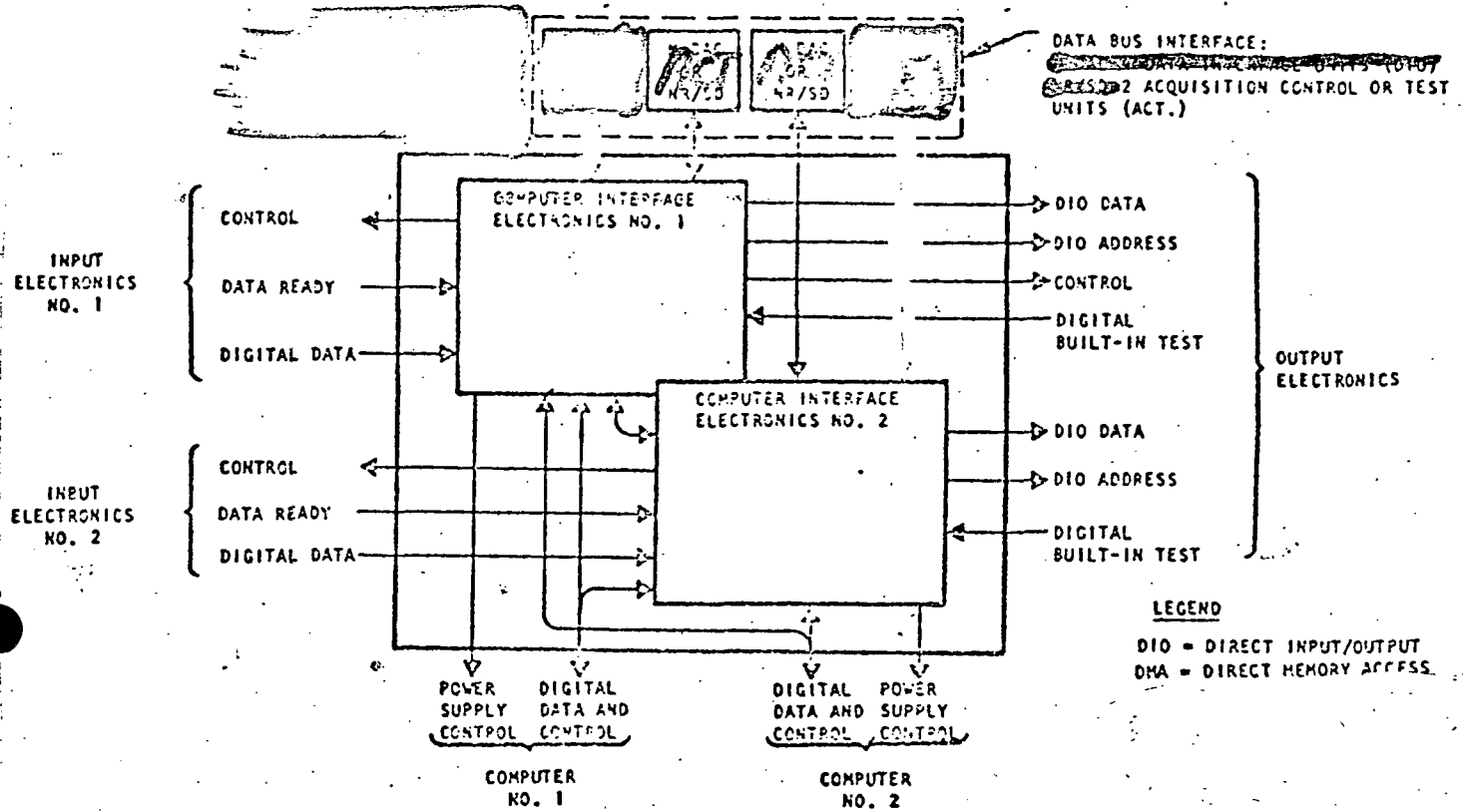


Figure 4.20-7 Computer Interface Electronics Organization

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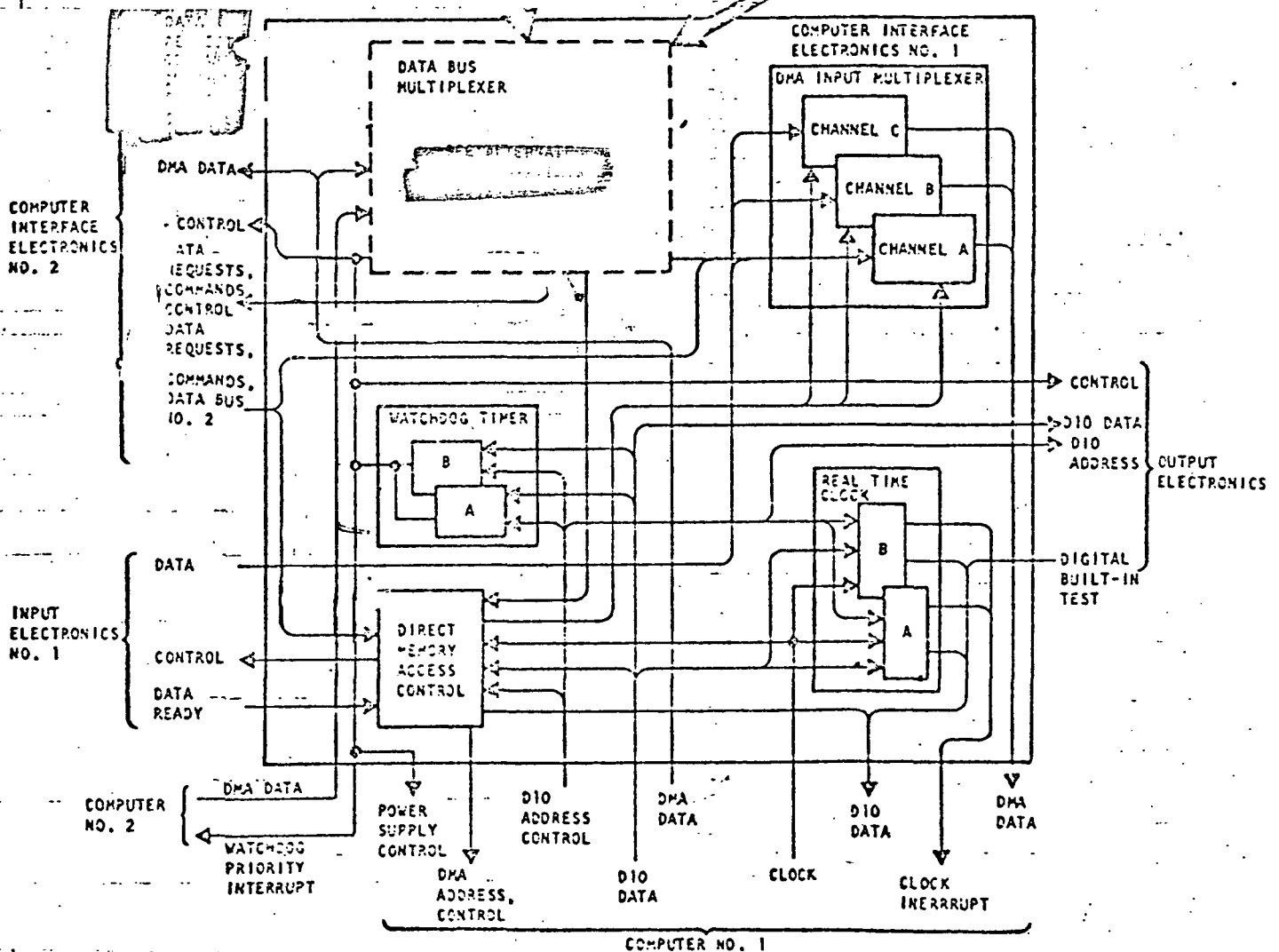
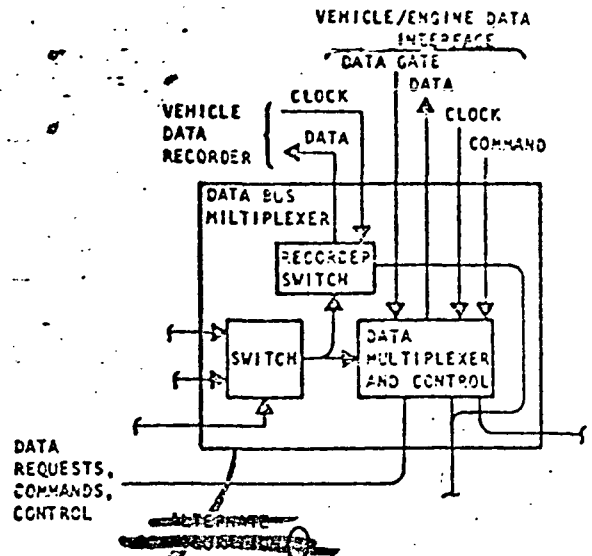


Figure 4.20-8 Computer Interface Electronics No. 1
(Typical 1 of 2)

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1. Data Bus Multiplexer - Provides the communication link between the controller and the vehicle. This communication link is bidirectional, receiving commands and data requests from the vehicle and transmitting the requested data to the vehicle. Commands and data are transmitted via redundant vehicle data buses. These data buses interface with the controller through Acquisition, Control and Test (ACT) units.

2. Direct Memory Access Input Multiplexer - Processes all data entering the computer memory through the direct memory access (DMA) input. This includes data from the associated set of input electronics and from the data bus multiplexer. The DMA multiplexer is triple redundant to match the redundancy of the control sensors and their input electronics. Multiplexer control is provided by the DMA control.

3. Real Time Clock - Provides the computer with redundant time references to initiate the start of each 20 msec control cycle.

4. Direct Memory Access Control - Controls the flow of data in and out of the memory via the DMA data channel. Data is transferred into the memory by halting computer

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42 operations for 1 microsec memory cycle for each data transfer.

Requests for access to the memory are granted on a priority basis. The order of priority is:

- a. Vehicle commands and requests for data.
- b. Analog-to-digital converter data.
- c. Pulse-rate-to-digital converter data.

5. Watchdog Timer - Monitors computer operation to verify that it is progressing through its program per a pre-determined schedule. Two watchdog timers are used with each computer to ensure fail-safe computer monitoring.

Data Bus Multiplexer

The controller interfaces with the vehicle through two Acquisition, Control, and Test (ACT) units and a vehicle recorder bus (Figure 4.20-8). The ACT units transmit commands and data requests to the controller and receive requested data from the controller. Engine maintenance data is sent by the controller directly to the recorder data bus. One ACT unit is normally in control with the other in standby. The data bus multiplexer is capable of communicating with either at any time. As all communication with both sets of computer interface electronics is identical, only one is discussed in detail.

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Each data bus multiplexer has four signal paths with the ACT unit: clock, data input, data output and data gate. The clock serves to clock the data into and out of the controller and operates continuously. The data input supplies the controller with vehicle commands. The data output transmits controller data to the vehicle when enabled by the data gate.

The controller accepts inputs from the two ACT units through separate connectors. The vehicle recorder, used to record engine maintenance data, has data channels dedicated to each engine. The data is transmitted to the recorder bus from the controlling computer.

Direct Memory Access (DMA) Input Multiplexer

Data from the input electronics and the data bus multiplexer is gated into the memory through the DMA input multiplexer. Each of the two multiplexers (No. 1 and No. 2) includes three channels (A, B, and C) that interface with the corresponding channels of the input electronics. The A channels also interface with their respective data bus multiplexers. The functional arrangement of channel 1A is shown in Figure 4.20-9.

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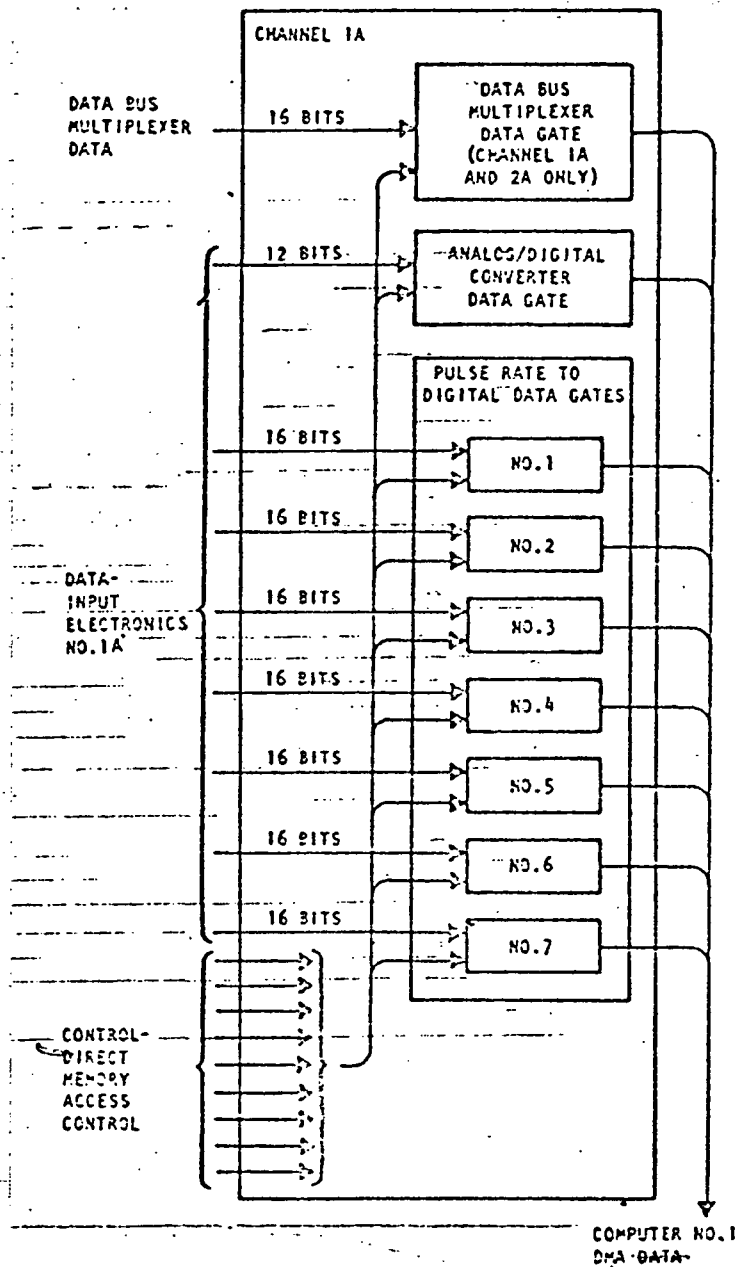


Figure 4.20-9 Direct Memory Access Input Multiplexer Channel (Typical 1 of 6)

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Each of the six multiplexer channels includes one 12-bit gate for analog-to-digital converter data and seven 16-bit gates for pulse-rate-to-digital converter data. As indicated in Figure 4.20-9, channel 1A (and 2A) include an eighth 16-bit gate for data bus multiplexer data. The data is gated under control of the DMA control unit.

Real Time Clock

Each computer interface electronics includes redundant real time clocks. The function of the clock is to interrupt the computer at precise time intervals. As shown in Figure 4.20-10, each real time clock consists of a four-section counter with means for setting time in to and reading time out of the counter. This provides the capability of performing specific tasks in real-time.

In normal operation, the counter is incremented by the incoming clock frequency. When the gate becomes true, the counter is reset and an external priority interrupt is sent to the computer. This interrupts the computer to increment a time location in memory by one. A new cycle is initiated when the preset time location overflows from all ones to all zeros. At the time of the new cycle, the computer also presets the time location and countdown resumes for the next cycle.

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COMPUTER
NO. 1

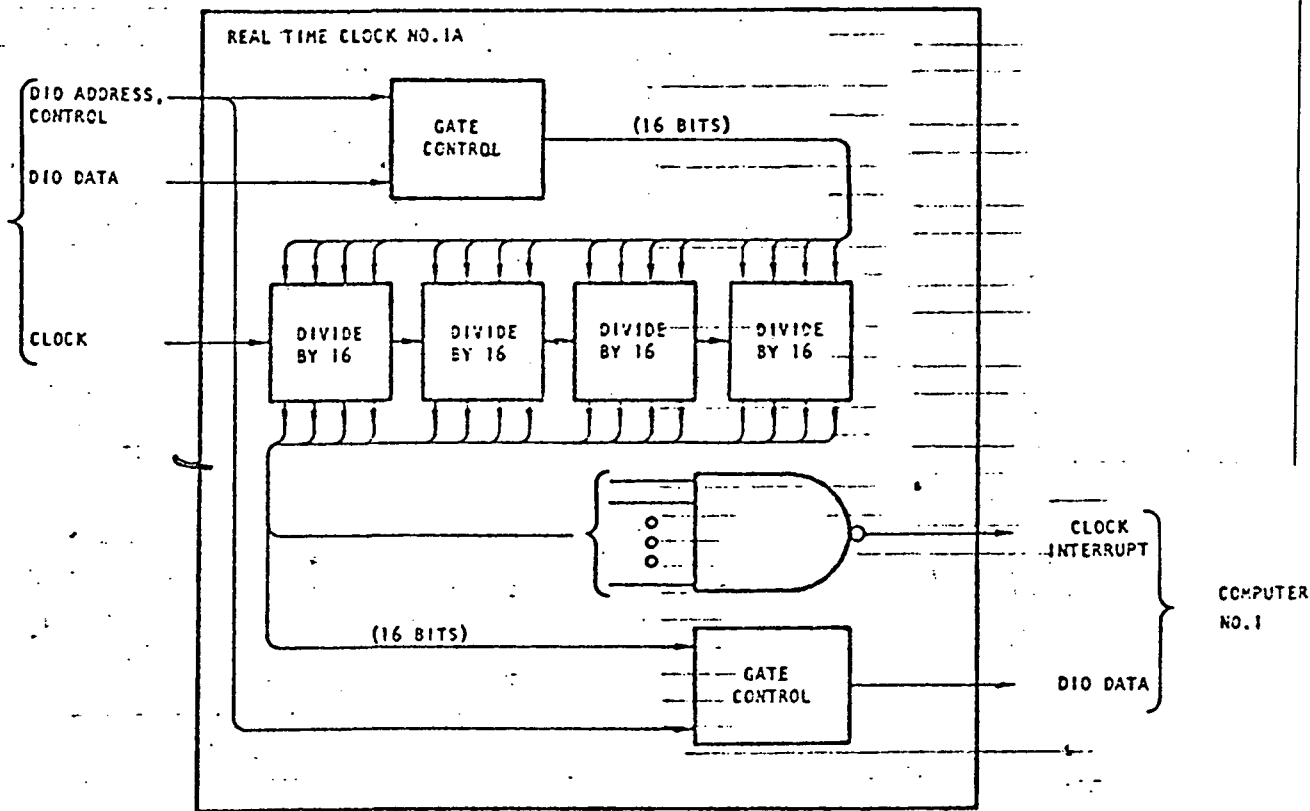


Figure 4.20-10 Real Time Clock (Typical 1 of 4)

REF.
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When operational requirements demand a higher sampling rate, i.e., when limit monitoring indicates a parameter is beyond limits, the computer programs a smaller number into the memory time location and the sampling period is proportionately shorter.

To ensure that a clock failure will be detected, each computer is provided with two real time clocks. The clock outputs are periodically compared during built-in test, and if they differ, appropriate action is taken.

Direct Memory Access Control

The function of the direct memory access control unit is to regulate the data flow in an orderly manner and in accordance with a set order of priorities. To perform this function, the direct memory access control (Figure 4.20-11) is organized into a hierarchy of three channels. Each channel accepts data requests, memory addresses and control signals, and transmits data transfer and memory address control signals. Each channel includes the necessary decoders, counters, and priority and sequence control logic to perform the above functions.

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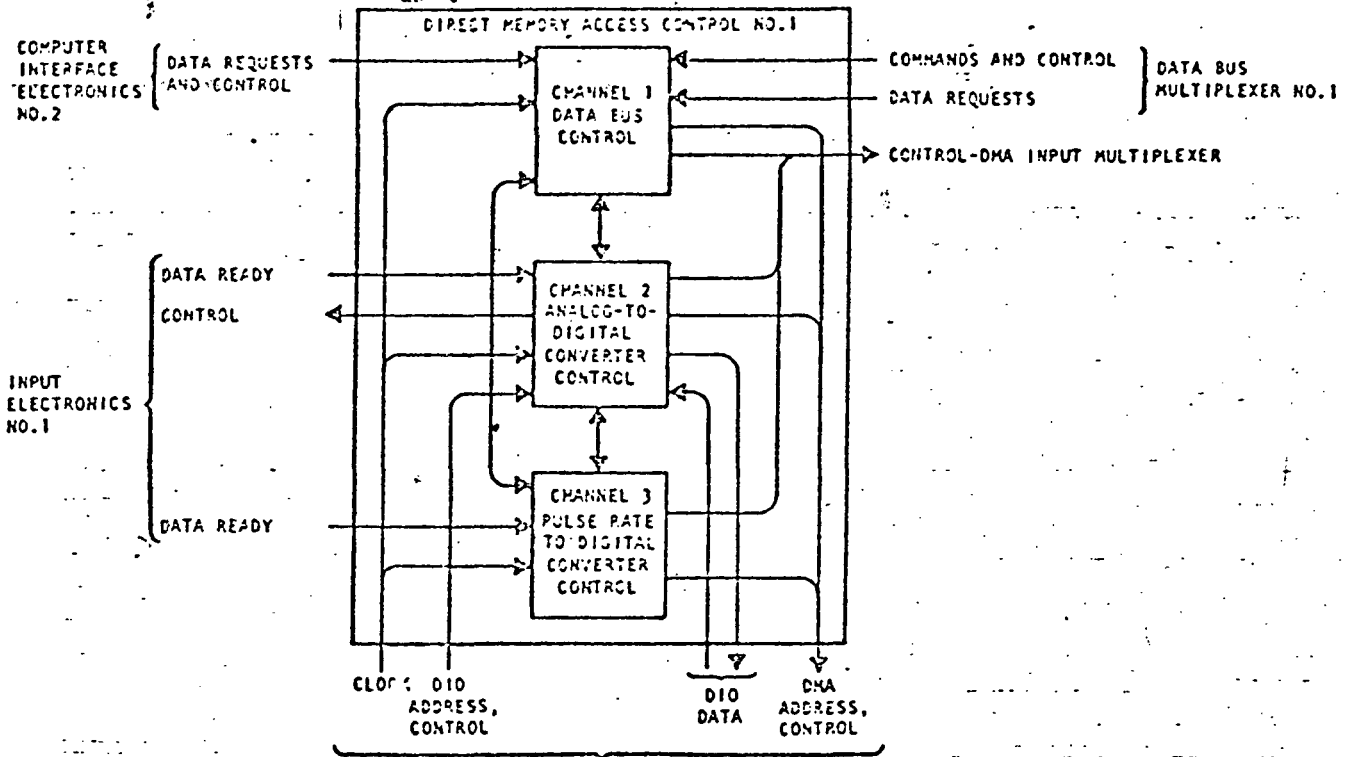


Figure 4.20-11 Direct Memory Access Control
(Typical 1 of 2)

REF.
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Channel 1 Data Bus Control first priority is to vehicle commands and data requests. Upon receipt of a command or data request from the data bus multiplexer, the data bus control will service the request by providing a memory output within 3 microseconds. If either Channel 2 or 3 is transferring data, Channel 1 will interrupt at the completion of the 16-bit transfer in process and will assume control. When the Channel 1 transfer is complete, control will be relinquished to the channel with the next highest priority. The validated command is transferred to both computers, since normally only one ACT unit is operational at a time. Data requests from either data bus multiplexer activate the DMA control to route the requested data onto the DMA data bus by the requesting data bus multiplexer. Channel 2 Analog to Digital Converter Control provides second priority control for data transfer to memory from the analog-to-digital converters. Channel 2 normally receives a data-ready signal from each of the three converters when a conversion is complete. When the three signals have been received or when a predetermined time has elapsed, the ready data is transferred sequentially to dedicated locations in the memory. Memory locations for converters which have not issued a data ready signal are coded in the upper four bits to prevent the processing of incorrect or obsolete data. Channel 2

REF. will not transfer data while Channel 1 is servicing a request
42 and has the same priority relationship with Channel 3 as
Channel 1 with Channel 2.

Channel 3, Pulse Rate to Digital Converter Control, processes pulse rate converter data in a manner similar to Channel 2, except that both Channels 1 and 2 have higher priority.

Watchdog Timer

The watchdog timer (Figure 4.20-12) is a circuit used to verify that the computer is progressing through its program. The timer is designed to be reset by the computer software program within a predetermined time. If the timer is not reset within that period, the output will switch from a logic one to a zero (failed indication). Reset is initiated by instructions within the computer program. Absence of a reset and the resultant shift to zero in the timer output indicates a computer failure. All computer and timer failure modes result in the watchdog timer output going to zero. To avoid the possibility of a failure where the computer repeatedly issues reset instructions from the same subroutine, two watchdog timers are used with each computer. Each subroutine resets only one of the timers.

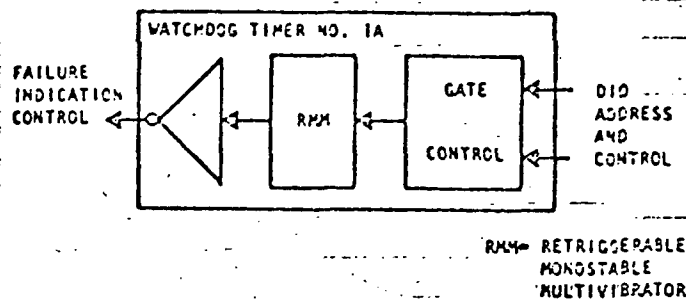
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Figure 4.20-12 Watchdog Timer
(Typical 1 of 4)

If the computer fails to reset either of its watchdog timers, the output goes to zero. A failure indication by the watchdog timer for computer No. 1 will cause the output switch described in paragraph 4.20.4.4 to transfer control to computer No. 2. Simultaneously, the watchdog timer will issue a control signal to the power supply electronics to cause shutdown of computer No. 1 power. The shutdown procedure includes a HALT instruction to the computer to prevent further processing. A failure in No. 2 computer subsequent to a failure in No. 1 will cause the No. 2 watchdog timer to remove computer power, issue a HALT instruction, and remove power from the output electronics to enable a fail-safe shutdown. Each computer monitors the watchdog timer output of the other to determine

REF. operational status which is made available to the vehicle
42 by the controlling computer.

4.20.4.3 DIGITAL COMPUTER DESCRIPTION

Two independent digital computers (Figure 4.20-13 and 4.20-14) receive commands from the vehicle and data from the sensors. Each performs the computations necessary for full-authority closed-loop control of the engine thrust and mixture ratio. Each computer also schedules the sequencing commands for all phases of ground and flight operations.

Normally, computer No. 1 is in control and computer No. 2 is in operational standby. In the event of a failure in computer No. 1 or its power supply, control is transferred to computer No. 2 without impairing engine operation.

In addition to the primary function of engine control each computer performs the following functions:

1. Accepts maintenance data from the sensors, stores the information in the memory and transmits it to the vehicle upon request.
2. Performs continuous self test.
3. Monitors the performance of the engine sensors, igniters, valves, actuators, and the other computer.

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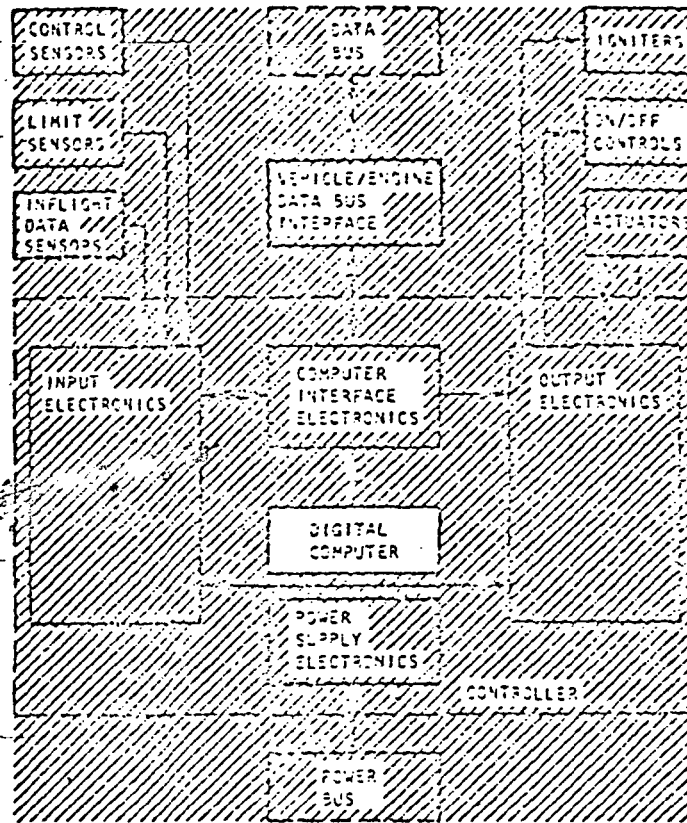


Figure 4.20-13 Digital Computer

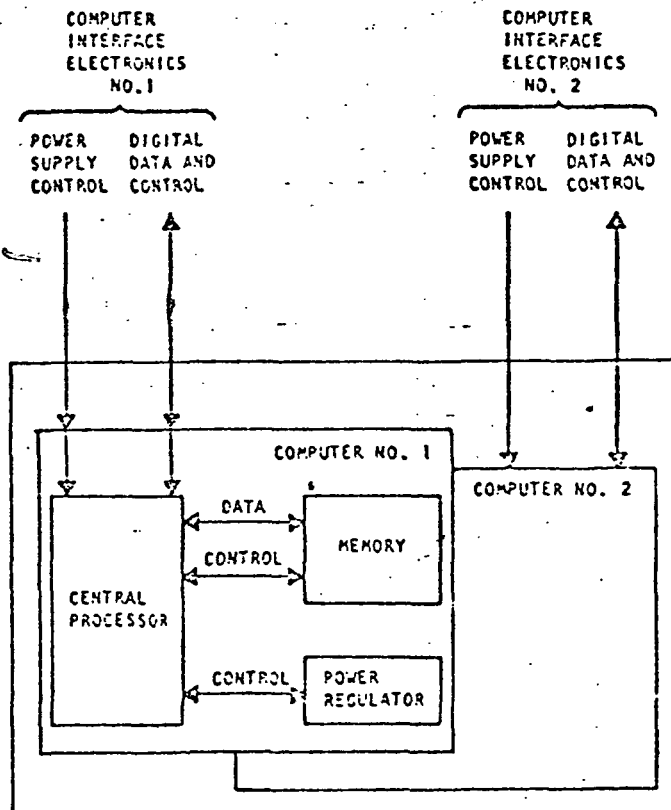


Figure 4.20-14 Digital Computer Organization

REF.
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4. Stores sensor calibration constants and uses them to correct raw sensor data.
5. Measures and compensates for errors introduced into the sensor data by the signal conditioning and analog-to-digital conversion circuitry of the input electronics.

Computer Selection

The Honeywell HDC-601 computer with a plated-wire memory is used for the SSME controller application. The HDC-601 was selected for the following reasons:

1. Off the shelf. The HDC-601 is a fully developed digital computer and has been in production on two U. S. Air Force programs for over six months. Commercial equivalents, the H-316 and DDP-516, have seen extensive application over the last 3-1/2 years. The HDC-601 is repackaged to conform to the controller form factor, but the proven logic, direct memory access, printed wiring board layouts, support software, and diagnostic and maintenance documentation are retained intact.
2. Available support software cuts costs and schedules. The HDC-601 computer is software-compatible with the DDP-516 and the extensive software system developed for the DDP-516 is also available for the HDC-601.

REF.
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3. Plated wire memory. The plated-wire memory used in the HDC-601 is rugged in construction and is fast because of its true nondestructive readout characteristics. The contents of the memory are not altered during a readout operation and do not have to be restored as is the case with cores. The controller computer uses a 2-mil plated wire memory to take advantage of its greater speed and reliability and lower power consumption. The word-organized structure of the plated-wire memory in conjunction with the nondestructive readout makes possible a convenient means of increasing system reliability by implementing memory lockout. Memory lockout allows that part of memory that contains the operational program and program constants to be operated in a read-only mode, thus preventing the inadvertent alteration of these instructions and constants.

4. Efficient data transfer. The HDC-601 achieves efficient data transfer by providing access to the memory through two routes. One is through the customary direct input/output processing channel under control of the computer program. The other is a direct memory access channel which permits independent transfer of data into and out of the memory while normal computing operations continue without interruption. The customary direct input/output cycle

REF. requires from 5 to 15 microsecond per input while the HDC-601
42 direct memory address requires only 1 microsecond. Since
120 sensor and 105 analog and digital built-in-test inputs
(including spares) must be sampled during each 20,000 msec
period, the 4 to 14 microsec per cycle saving through direct
memory access frees an additional 1000 to 3500 microsec or
5 to 17 percent of each sampling period for other operations.
Stated in another way, the 1-microsecond direct memory access
makes more than 98 percent of the sampling period available
for computations. Direct memory access mode of operation
is accomplished on a memory cycle steal basis. That is,
requests for access to the memory are granted at the next
memory cycle on a priority basis.

5. Real time control. The HDC-601 was designed for
real time control and meets the requirements for fast,
efficient, and reliable computations. As previously noted,
the HDC-601 is an aerospace version of the Honeywell H-316
and DDP-516 computers, which were designed for and have
established an excellent record in the field of real time
control. An important function in a real time control
system is the capability to interrupt the normal computations
for priority operations without jeopardizing process control.
The HDC-601 provides priority interrupts for use by the

REF. controller in (1) processing vehicle commands, (2) detecting
42 power failure and initiating action to preserve the engine control status, and (3) detecting errors in the output of the memory.

6. Optimum word length. The HDC-601 uses a 16-bit word, which is optimum for applications that must encompass both control and computation functions. While 12-bit word length is sufficient for most control purposes, in certain types of computations such as multiplication, accuracy is degraded unless the slower double precision mode is used. The 16-bit word length in the HDC-601 provides ample accuracy in the single precision mode for virtually all computations. The double precision operation is still available for the infrequent operations which demand it. The 16-bit instructional word length is also more efficient in memory addressing capability. The memory may be addressed by the fast direct mode in sectors of 512 words. This size is ample to accommodate the majority of addressing requirements with the fast direct mode.

7. Growth capability. The HDC-601 provides growth margin in both memory capacity and computational capability. The memory is organized for optimum cost, size, and weight into planes or increments of 2048 words each. The controller

REF. 42 uses six planes totaling 12,288 words, providing ample growth allowance beyond the current requirements of 7000 words. This capacity for growth permits the user to capitalize on new functions that may subsequently become needed or desirable. If necessary, the controller memory capacity can be expanded to a maximum of 32,768 words. The HDC-601 also has a 30-percent growth margin in computational speed capability since only 14 msec out of each 20 msec sampling period are utilized for computation and built-in test.

Computer Organization

Each of the dual redundant computers in the controller are functionally divided into processor and memory sections as shown in Figure 4.20-15. The processor provides the computer's arithmetic, control, and input/output interfacing capabilities. Interface with the remainder of the system is through the computer interface electronics described in paragraph 4.20.4.2. The memory provides storage for instructions, computational constants, and data from the vehicle and the sensors. Portions of the memory are used as a "scratch pad" to store intermediate computations. The memory system provides a parity bit for each memory word for use in detecting memory system errors.

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COMPUTER INTERFACE ELECTRONICS NO. 1

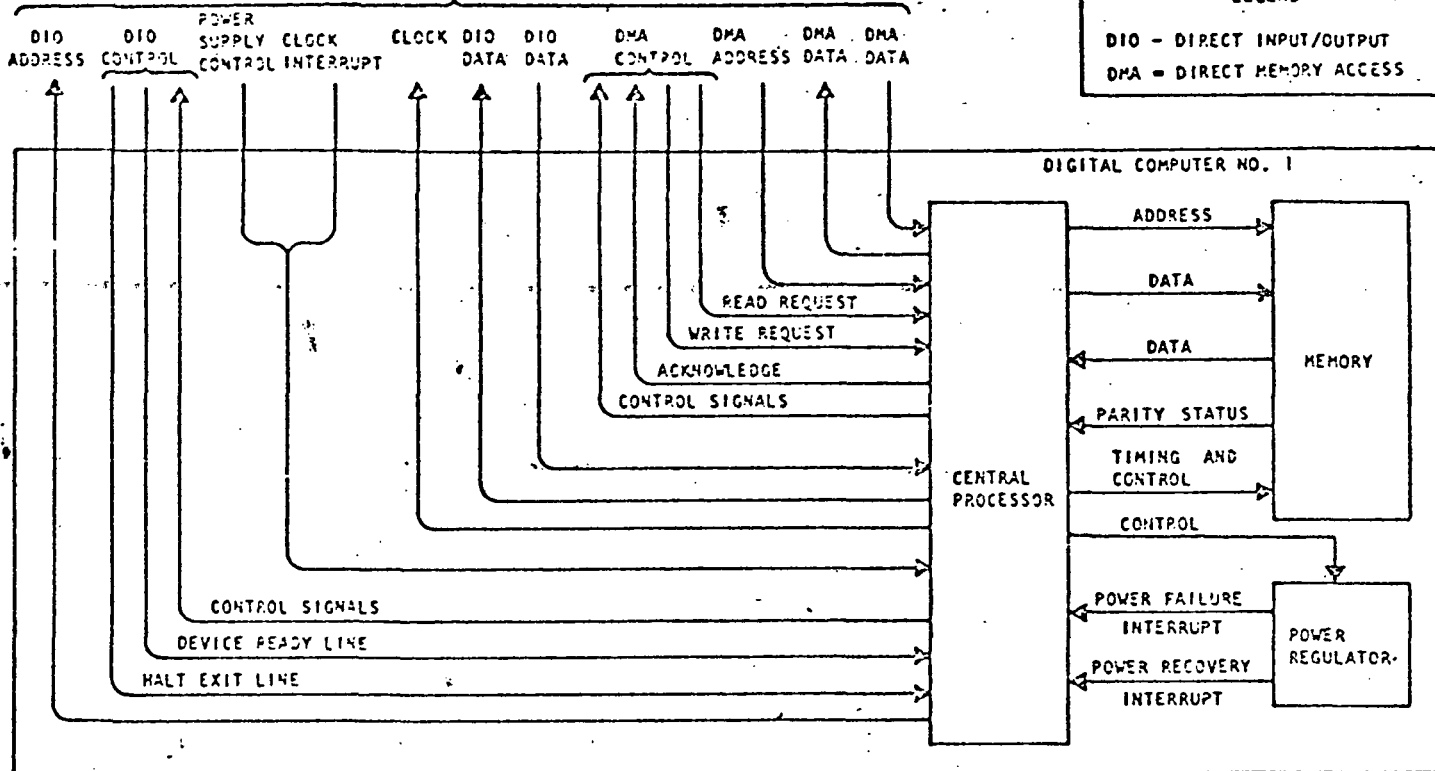


Figure 4.20-15 Digital Computer Interface
(Typical 1 of 2)

REF.
42

The characteristics of the computer are summarized in Table 4.20-12. A more detailed description may be found in the Honeywell HDC-601 Digital Computer General Description P9-003B (Phase B Supporting Analysis Data, Volume 63).

Central Processor

The central processor for the HDC-601 computer employs a parallel-organized data flow structure with conventional organization relative to memory interfacing and instruction execution. Implementation of the logic is accomplished using small and medium scale bi-polar transistor-transistor-logic (TTL) integrated circuits. These circuits have proven reliability backed by substantial field data.

Organization. In its basic functional organization, the central processor can be represented as shown in Figure 4.20-16. Interfaces to the central processor are:

1. Memory interface
2. Direct memory access channel
3. Direct input/output channel
4. Computer clock
5. Interrupt inputs
6. Input discrettes.

All communication with the central processor is via these interfaces.

REF
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PARAMETER	CHARACTERISTICS
ARITHMETIC ADDRESSING	PARALLEL BINARY, TWO'S COMPLEMENT SINGLE ADDRESS WITH INDEXING AND INDIRECT ADDRESSING
INDEX REGISTER	1 HARDWARE
INDIRECT ADDRESSING	MULTILEVEL
LOGIC TYPE	TRANSISTOR, TRANSISTOR LOGIC
CIRCUITRY	SMALL AND MEDIUM SCALE INTEGRATION
DATA INPUT/OUTPUT CHANNELS -PROGRAM -ACCESS	CONTROLLED AND DIRECT MEMORY 16 BIT PARALLEL
SPEED	
ADD AND SUBTRACT	2 MICROSECONDS
MULTIPLY	9 MICROSECONDS
DIVIDE	19 MICROSECONDS
INSTRUCTION COMPLEMENT	87
WORD LENGTH	16 BITS*
INPUT DISCRETES	16 STANDARD
MEMORY CYCLE TIME	
-READ/WRITE	1 MICROSECOND
-ACCESS	350 NANoseconds
MEMORY	12,208 WORDS
INPUTS AND OUTPUTS	BUFFERED
REGISTERS	TWO FULL-WORD ARITHMETIC, ONE HARDWARE INDEX
DOUBLE PRECISION CAPABILITY	YES
INTERRUPTS	18 EXTERNAL PRIORITY, POWER FAILURE/RECOVERY

*THE PARITY BIT (BIT 17) AND ASSOCIATED PARITY GENERATION AND DETECTION IS HANDLED AT THE COMPUTER/MEMORY INTERFACE.

TABLE 4.20-12 HDC-601 COMPUTER CHARACTERISTICS

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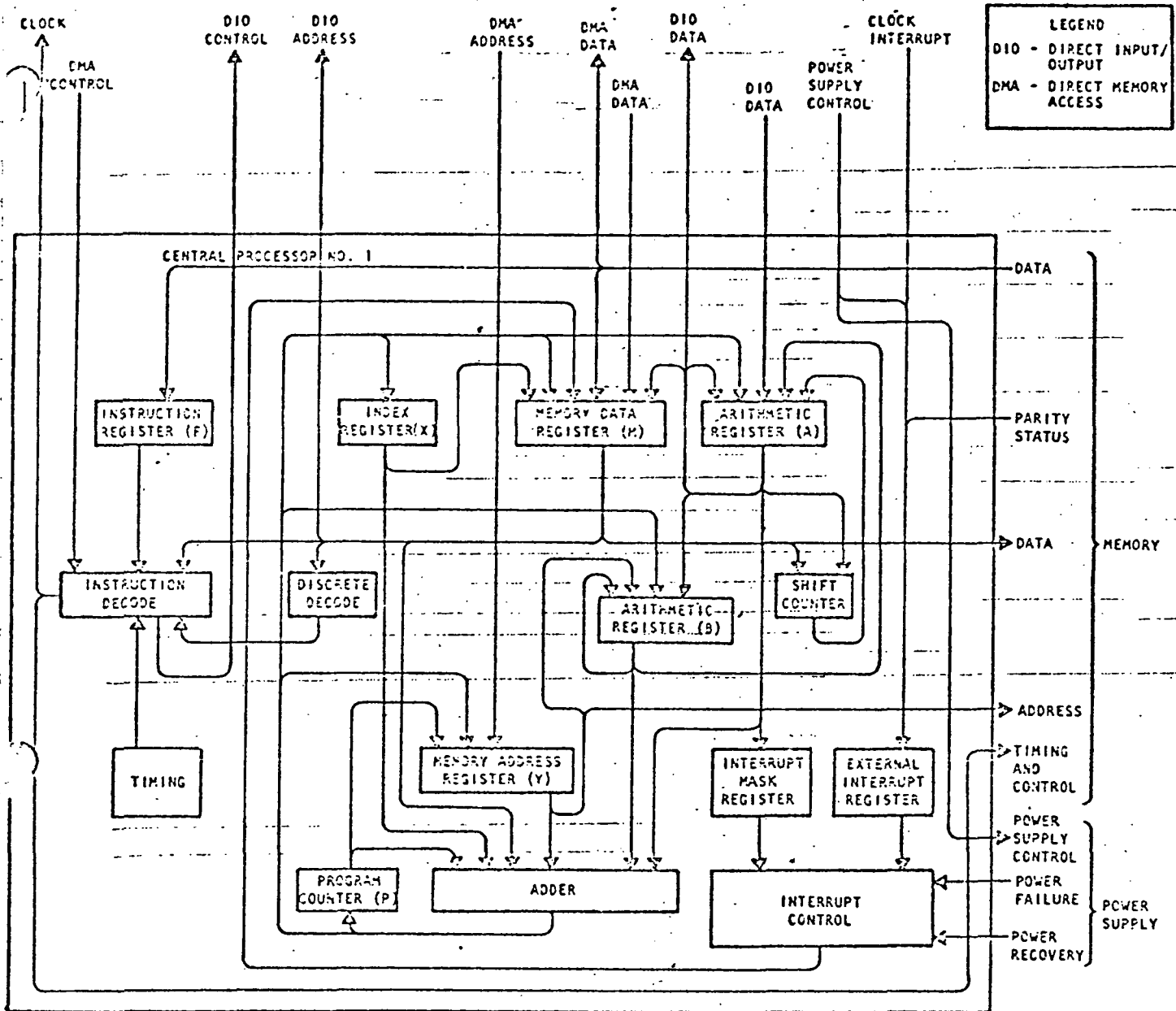


Figure 4.20-16 Central Processor Functional Organization (Typical 1 of 2)

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Data Flow. As shown in Figure 4.20-16, the data flow between the central processor and memory is through the memory data register with memory address information supplied by the memory address register. From the memory data register, data can be routed through the adder to any other register. The adder serves both as a transfer gate and as an arithmetic element during arithmetic operations. Data and information are routed throughout the central processor in accordance with the dictates of the particular instruction being executed. Data is transferred between the central processor and the system via both the direct input/output channel and the direct memory access channel.

Control. Execution of instructions is controlled by timing and instruction decoding logic within the central processor. Each instruction is performed in basic steps called microprograms. These microprogram steps include all the basic operations necessary for operation of the central processor. Timing for central processor operations is obtained from a stable 3-MHz clock, which also supplies timing signals to other points in the system. The interrupt inputs provide control of the central processor by other parts of the system.

REF.
42Memory

A plated wire memory is used with each redundant computer channel. A functional block diagram of the memory organization is shown in Figure 4.20-17. The package consists of four printed wiring boards containing sense/digit and word/timing electronics, and six boards forming a memory stack. Each memory board contains its own word select electronics. The two surfaces of each memory board also contain printed wiring interconnections for the electronics plus parallel conductors (word straps) used for word selection. The 2-mil plated wire memory elements are supported in parallel tunnels lying between and at right angles to the word straps on the board surfaces. All boards are securely fastened and supported by a rigid frame. Interconnections are made by flexible flat cable.

Characteristics of the memory are as follows:

1. Capacity: 12,288 x 17-bit words.
2. Cycle Time: 1 microsec (capability to execute any combination of read and write cycles at the rate of 1 MHz)
3. Access Time: 350 nanosecond
4. Operating Power: 9 watts average

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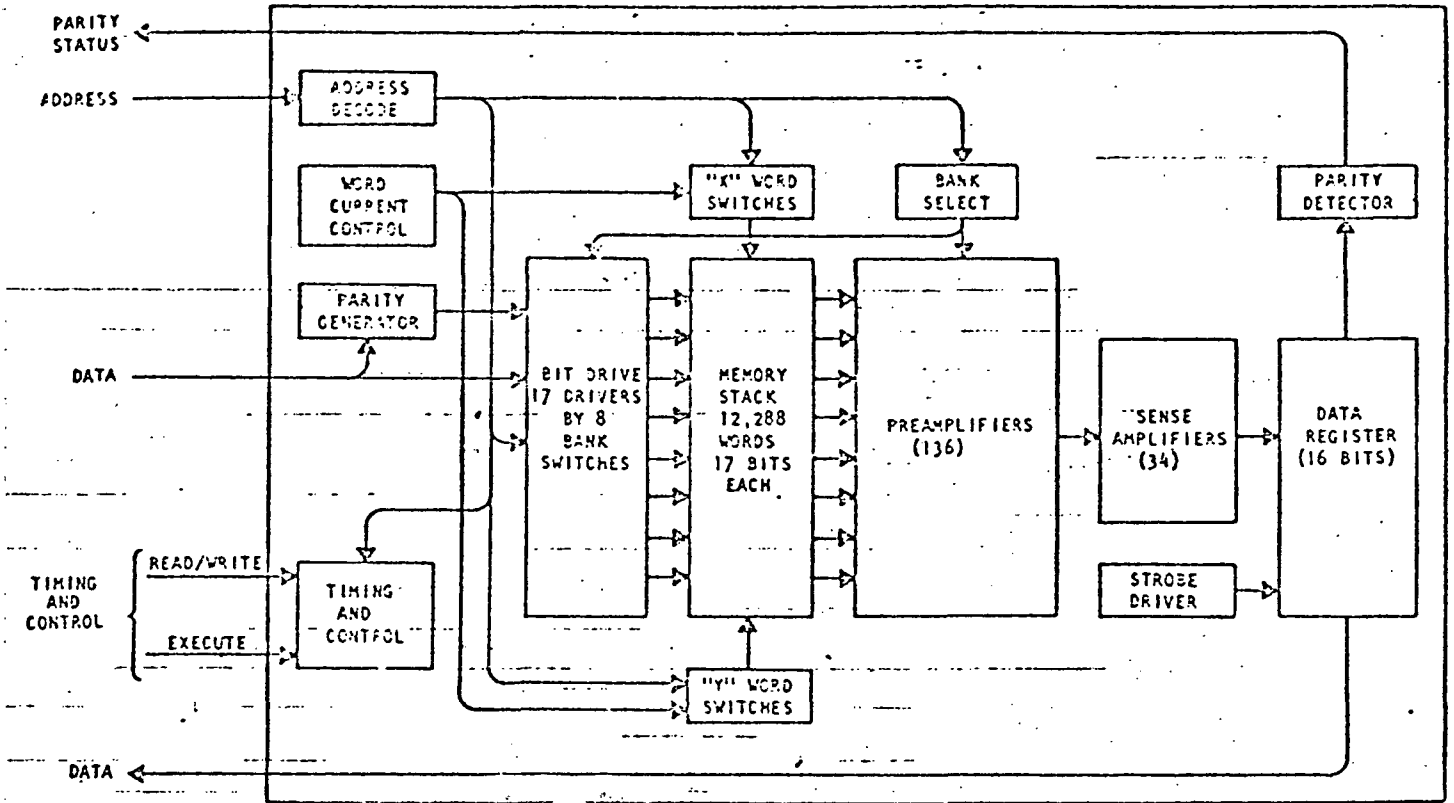


Figure 4.20-17 Plated Wire Memory Block Diagram
(Typical 1 of 2)

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The 2-mil plated wire memory was selected for the controller application over other memory types for the following reasons:

1. Operating speed. The high-speed capability of 2-mil plated wire exceeds that required for the controller application and provides higher reliability of operation.
2. Low power. Nine watts average power is achieved through power switching the fast switching characteristics of the plated-wire memory element and the nondestructive readout characteristic of plated wire.
3. Minimization of electronics. Two-mil wire can be interfaced directly with standard small- and medium-scale integrated circuits eliminating the need for high current drivers.
4. Low volume and weight. Optimization of electronics and use of multilayer printed circuit boards and medium-scale integrated circuits (MSIC's) minimizes volume and weight.
5. High reliability. High reliability is derived from reliability of plated wire and minimization of electronics.
6. Nondestructive readout (NDRO). During a read cycle, the memory contents are not altered (nondestructive readout) precluding the need for a "read restore" cycle.

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7. Lockout capability. By virtue of the "word organized" structure and nondestructive readout operation, blocks of memory can be electrically disabled to prevent inadvertent alterations of critical instructions and constants. Alternatively, the memory can be energized during ground maintenance operations and altered via a special GSE connector. This flexibility is useful for revising the calibration constants stored in the memory, following a sensor replacement.

8. Temperature stability. No temperature compensation is required by the 2-mil plated wire memory over the controller operating temperature range.

9. Rugged vibration-resistant construction. The plated-wire elements, word straps, and associated electronics are securely supported by a sandwich structure of memory planes and electronics boards mounted in a rigid frame.

Details relative to the selection of the memory are presented in the Honeywell Controller Technology Trade Study, 970-1327B (Phase B Supporting Analysis Data, Volume 58).

REF. 4.20.4.4 OUTPUT ELECTRONICS DESCRIPTION
42

The output electronics (Figures 4.20-18 and 4.20-19) accept digital control commands from computer interface electronics No. 1 converting them to analog voltages for control of servovalve actuators, on/off controls, and spark igniters. The output electronics are dual redundant. Each consist of:

1. Output switch and command decoder.
2. On/off controls and igniter drivers to energize engine on-off valves and spark igniters.
3. Servovalve control circuits to energize and position proportional servovalve actuators, and to operate fail-operational and fail-safe solenoids.

Both redundant output electronics channels (A and B) accept digital data from the controlling computer, converting it to on/off and analog commands for the engine controls. Channel A energizes the operational torque motors for the proportional valves, and channel B the standby torque motors. Channels A and B each energize half of the redundant outputs. Nonredundant coils on valves are divided between channels A and B. All output commands are fed back to the digital computer to verify the output electronics operation. In addition, the operation of the actuator servovalves is

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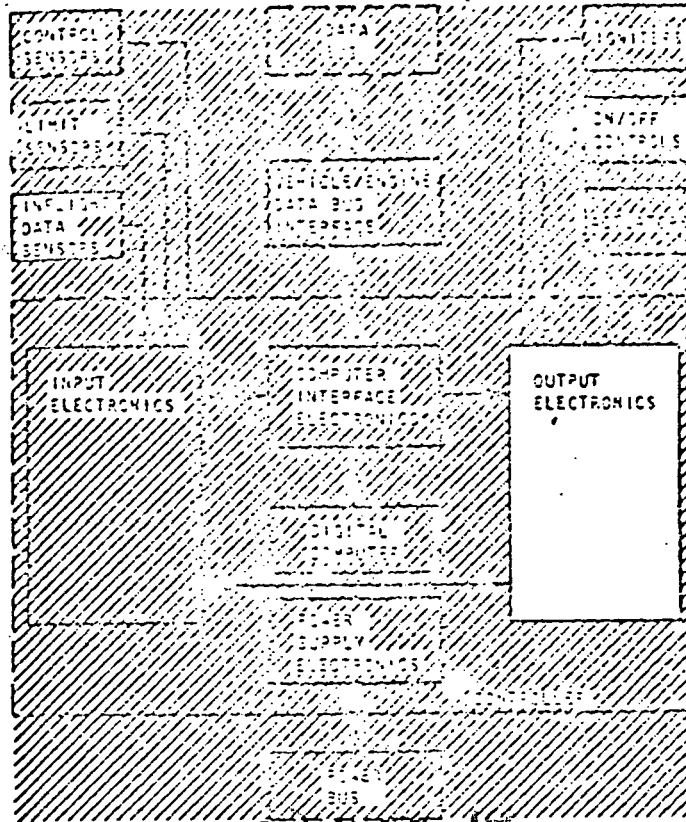


Figure 4.20-18 Output Electronics

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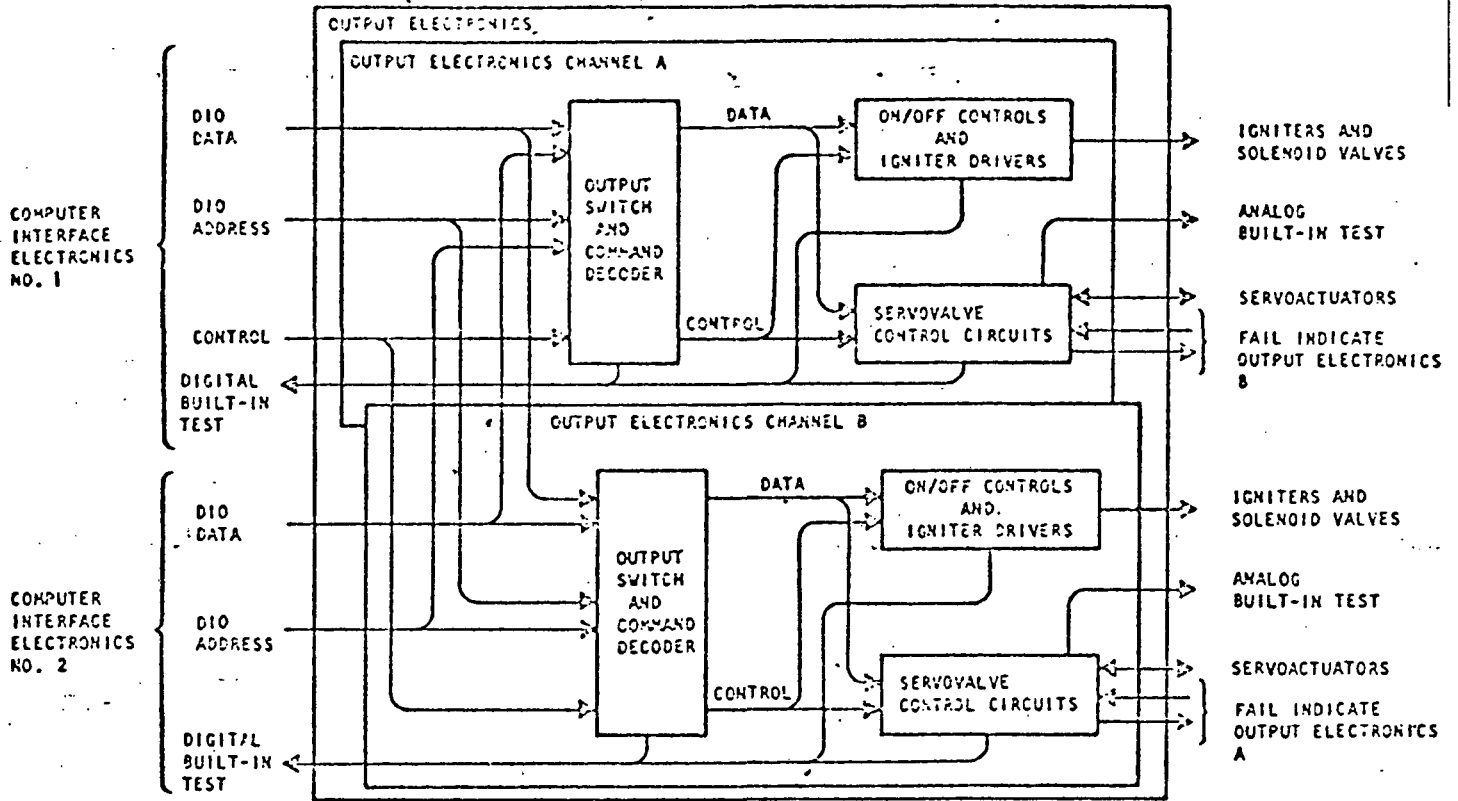


Figure 4.20-19 Output Electronics Organization

REF. compared to an electronic model. If an unacceptable error
42 or failure is detected in one of the dual servovalves, the channel is disabled by removing power. If the second servovalve fails, the associated actuator is hydraulically locked in its last position to maintain engine operation.

Output Switch and Command Decoder

Digital engine commands are presented at the outputs of No. 1 and No. 2 computer interface electronics in 16-bit parallel format. The output switch and command decoder, Figure 4.20-20, is controlled by computer No. 1 watchdog timer. The watchdog timer output logical one enables 18 AND gates to transfer 16 bits of direct output data from computer interface electronics No. 1 into a storage register. The 17th and 18th bits control enable signals from the computer direct input/output address bus to the storage register and the command decoder.

If the watchdog timer output switches to zero signifying a failure in computer No. 1, the first set of AND gates will be disabled and a second set enabled transferring the output of computer No. 2 to the storage register.

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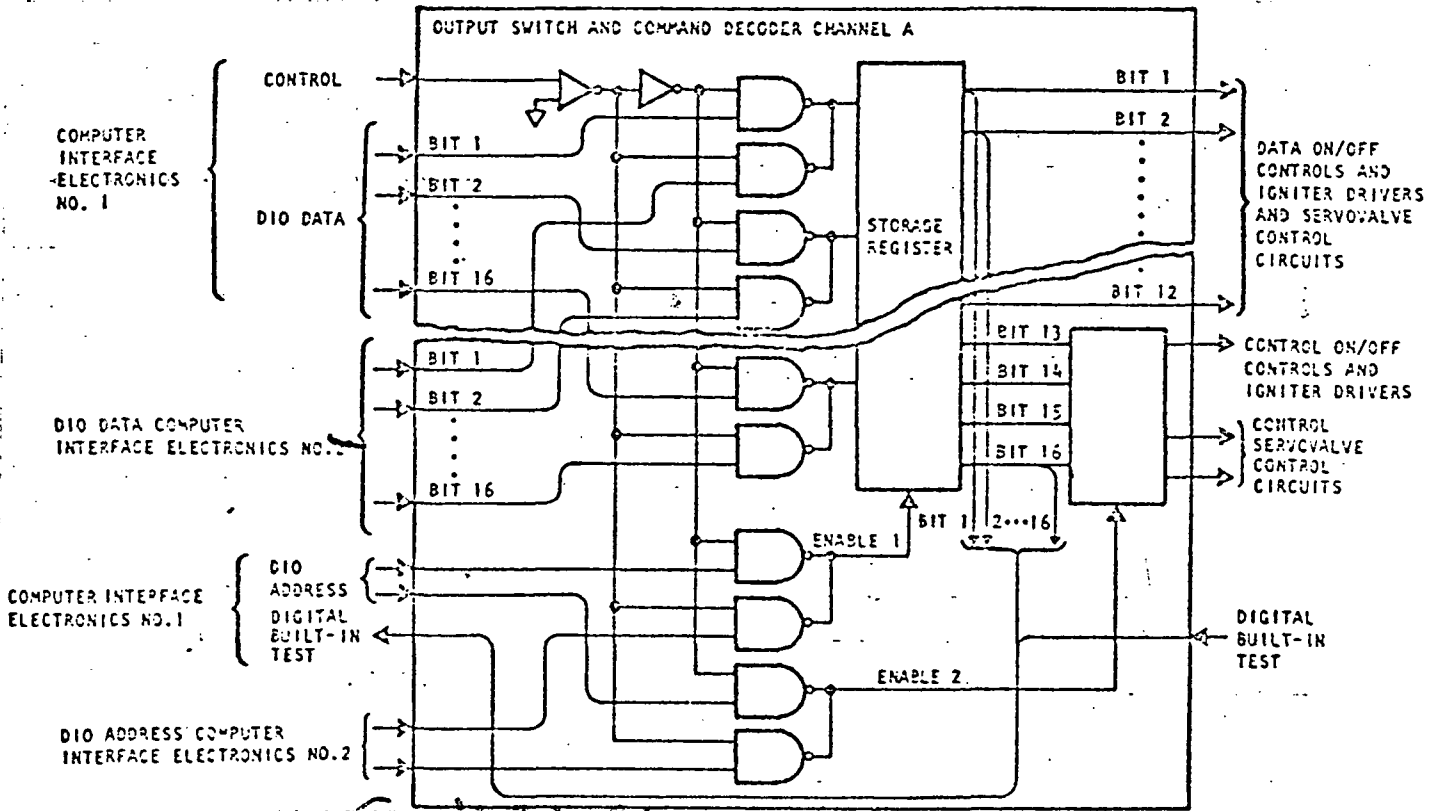


Figure 4.20-20 Output Switch and Command Decoder
(Typical 1 of 2)

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While the digital data is in the storage register, it is fed back to the digital computer built-in-test inputs for verification. Lack of verification will initiate a new command from the computer. Repeated nonverification (3 times) is a failure.

When the data in the storage register is verified, 12 bits are available to the on/off controls and igniter drivers and to the servovalve control circuits. The remaining 4 bits are decoded in the command decoder and used to control the sequencing, routing, and timing of the output signals.

When the controller has verified commands for the igniters and on/off controls in the output switch storage register, all 12 bits are clocked by a second enable signal and routed by the command decoder into the register for the on/off controls and igniter drivers, Figure 4.20-21. The appropriate "on" or "off" inputs are then enabled to the 12 drivers to set the controls for the command. Under software control the register maintains the initially commanded output to each driver until a change is commanded, i.e., to reduce solenoid power to the hold-in level or to energize or de-energize a specific solenoid. The driver outputs are checked periodically by built-in-test.

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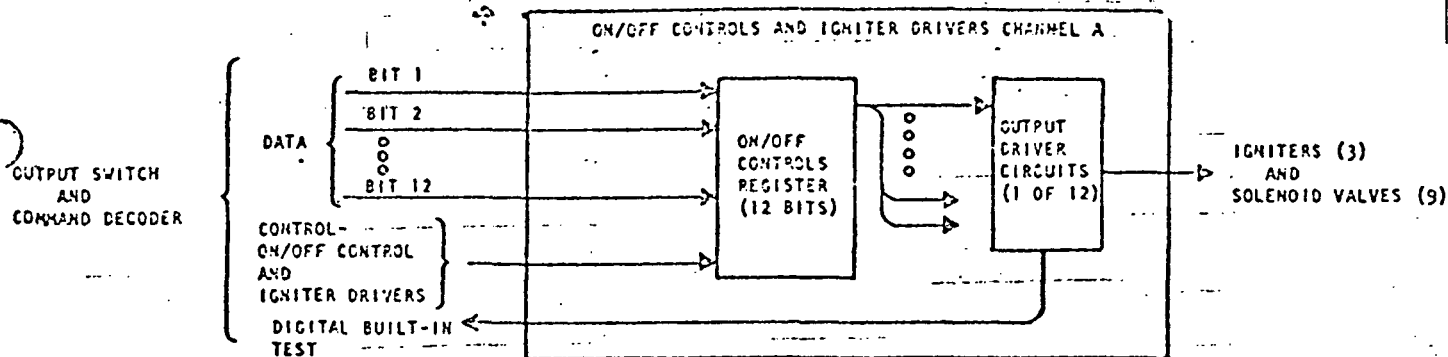


Figure 4.20-21 On-Off Controls and Igniters and Drivers
(Typical 1 of 2)

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42Actuator Servovalve Operation

Each proportional valve actuator is driven by two servovalves. One is normally in control and is energized by output electronics Channel A.

The second is energized by Channel B, but is in standby. Actuator control is transferred to the standby servovalve when either servovalve fail-operational solenoid is energized. When both fail-safe solenoids are de-energized, the actuator is hydraulically locked in its last position.

Servovalve Control Circuits

Verified proportional valve commands in 12-bit digital format are transferred by the command decoder from the output switch storage register to the servovalve command register, Figure 4.20-22. Once every 20 msec the command for each proportional valve is converted to an analog voltage by the digital-to-analog converter and clocked into one of the five sample and hold circuits. Multiplexing these signals one at a time eliminates the need for four additional sets of storage registers and digital-to-analog converters.

The sample and hold analog voltage proportional to the commanded valve position is summed in the driver input circuit with the demodulated actuator position feedback

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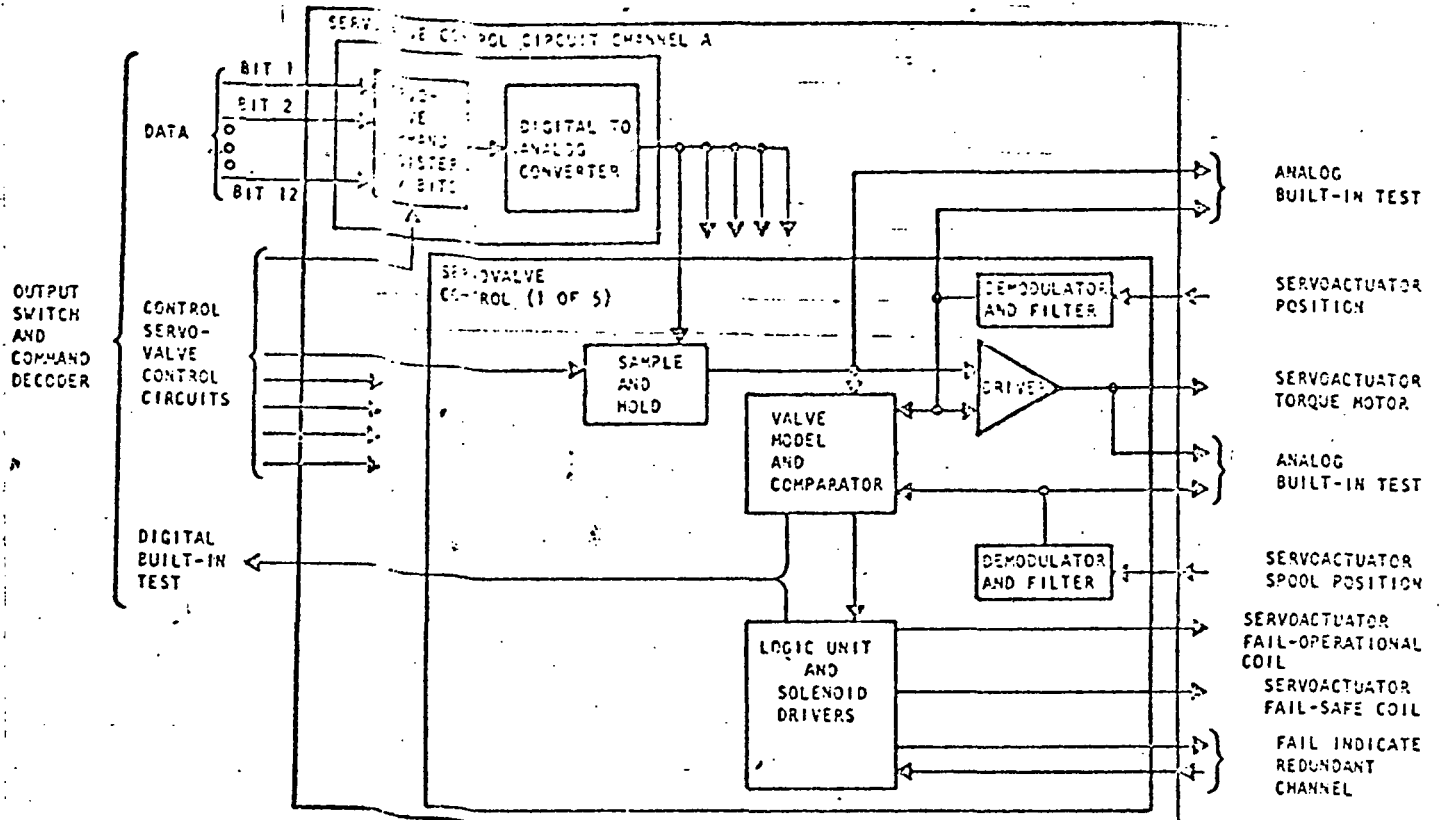


Figure 4.20-22 servovalve Control Circuit
(Typical 1 of 2)

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signal from a linear variable differential transformer (LVDT). The resulting error signal drives the servovalve torque motor until the actuator reaches its commanded position and the error signal is a null.

The analog command from each sample and hold circuit is also summed with the demodulated actuator position feedback signal in a servo valve model and comparator circuit. The resultant error signal is the same as that seen by the servovalve and is applied to an electronic model of the servovalve. The electronic model output is dynamically compared with demodulated LVDT feedback signal representing the servovalve second stage spool position. When either electronic model (Channel A or B) indicates a servovalve is not following its command signal, a fail indicate signal is generated in the logic unit. The logic unit then energizes or de-energizes the servoactuator fail-operational or fail-safe coils per the following logic.

<u>CHANNEL STATUS</u>		<u>SERVOACTUATOR COIL</u>		<u>CHANNEL IN CONTROL</u>
<u>A</u>	<u>B</u>	Fail-operational, volts	Fail-safe volts	
OK	OK	0	28	A
OK	Fail	0	28	A
Fail	OK	28	28	B
		Momentary		
Fail	Fail	Not applicable	0	Hydraulic Lock

REF. 4.20.4.5 POWER SUPPLY ELECTRONICS DESCRIPTION
42

The power supply electronics (Figure 4.20-23) rectify, filter, and regulate 115 volt, 3-phase, 400 Hz for use in the engine controls. Dual redundant power supply electronics energized from redundant vehicle power buses maintain the required fail-operational, fail-safe capability. Redundancy in the regulators matches that of the electronics functional subsystems. Protection is provided against propagation of overload failures. The power supply electronics include provisions for detecting and reacting to out of tolerance voltage, power failure and power recovery.

Power Supply Redundancy

Each of the two redundant power supplies consists of line filter transformer with multiple secondary windings and associated rectifiers, and a family of voltage regulators. As shown in Figure 4.20-24, each load branch is supplied from the redundant vehicle power buses through separate regulators. Uninterrupted power will be maintained to each load in the event of a failure in a power bus, rectifier or regulator. A minimum of two regulator failures to the same load are necessary to shut down a computational channel.

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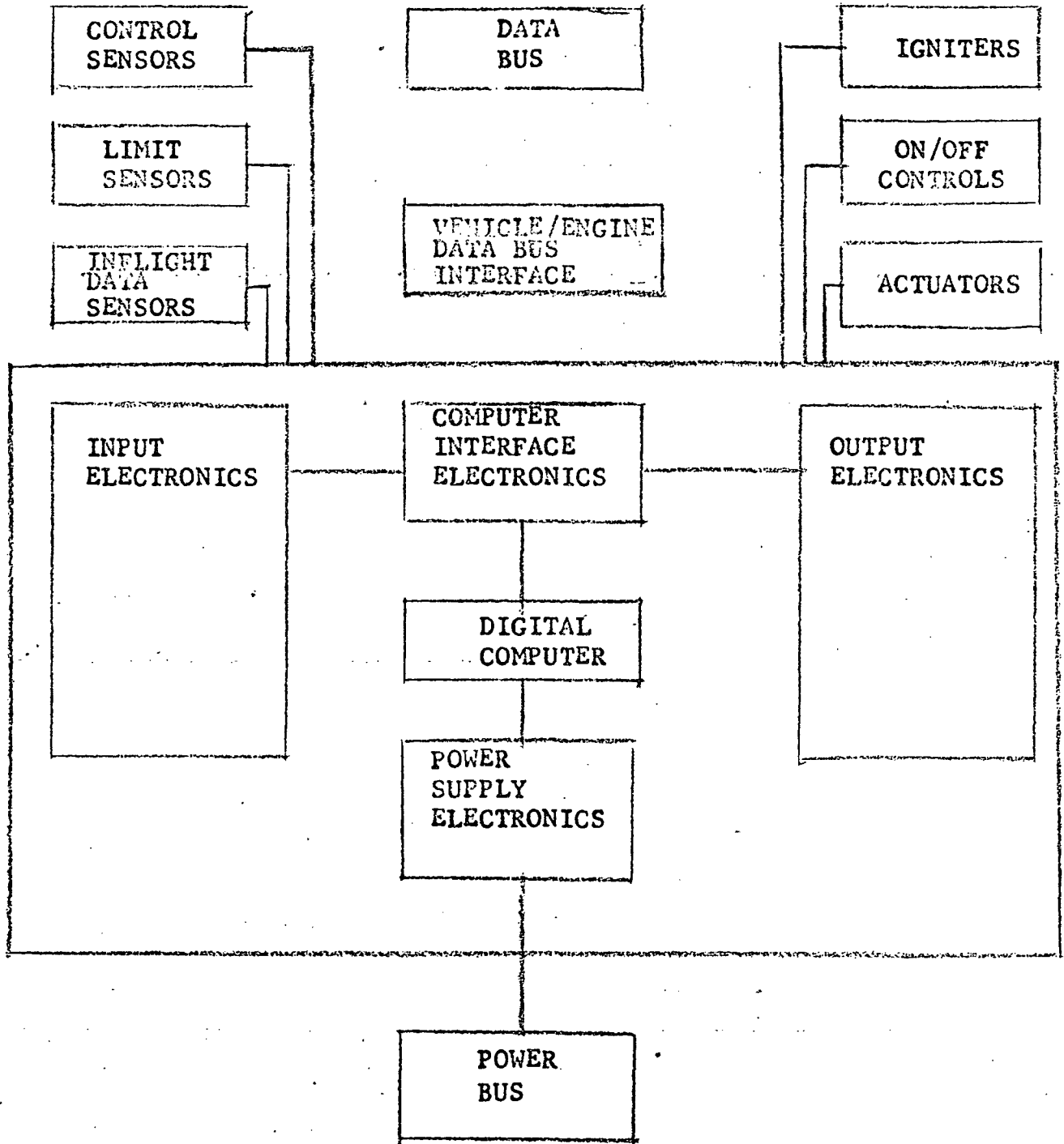


Figure 4.20-23 Power Supply Electronics

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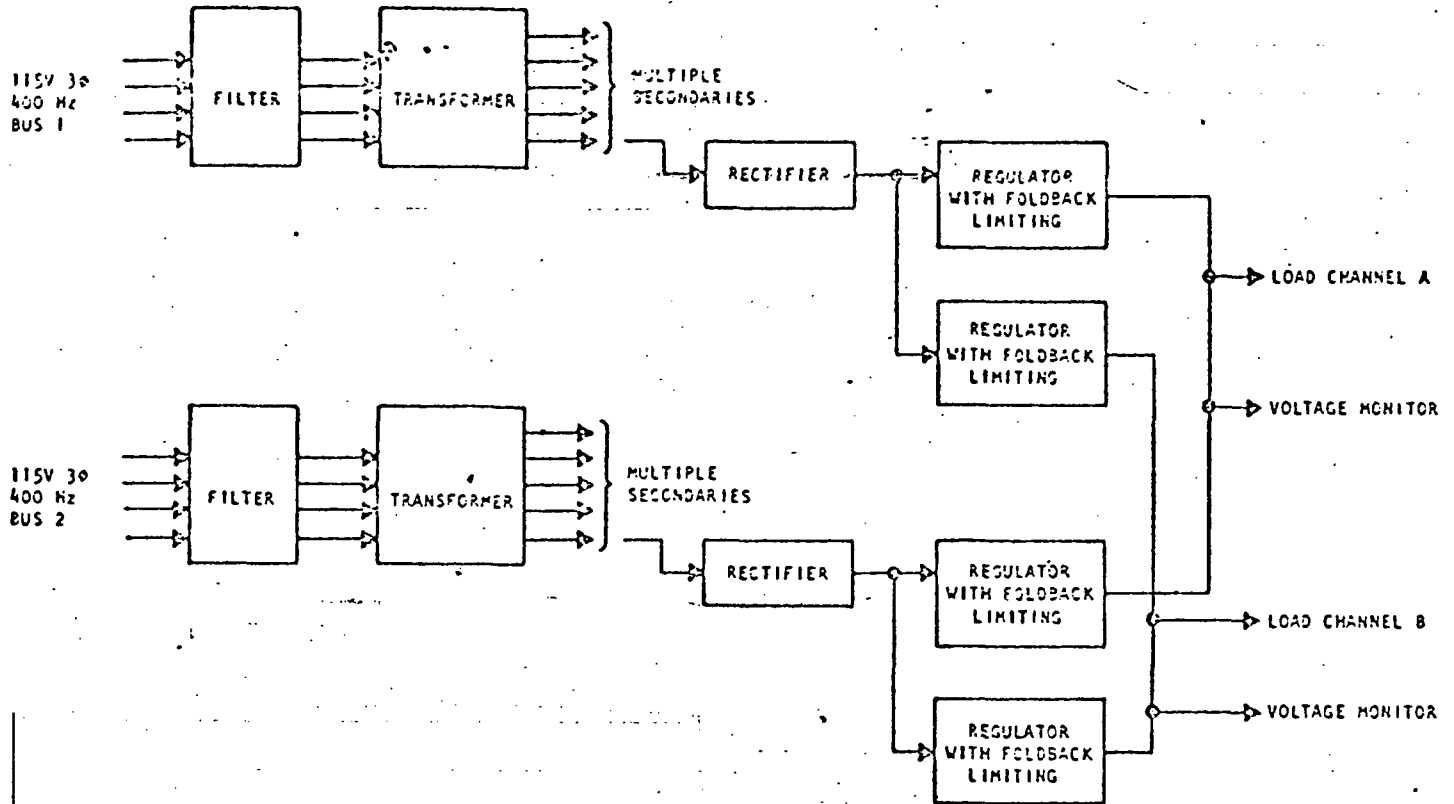


Figure 4.20-24 Typical Power Supply Redundancy

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The redundancy is protected from propagation of overload failure by foldback limiting incorporated in each regulator. If load current exceeds an acceptable level, the foldback limiter will isolate the load until the overload is removed. This feature protects the primary supplies and the remaining functions dependent upon them.

Power supply and regulator redundancy is shown in greater detail in Figure 4.20-25. The two sets of power supply electronics, No. 1 and No. 2, are dedicated to the corresponding computers and computer interface electronics. In addition, each of the three input electronics data channels and the two output electronics data channels are supplied from separate regulators to preserve their redundancy. This also provides a selective turn off capability if an out-of-tolerance condition arises.

Power Supply Electronics Design

Each set of power supply electronics, Figure 4.20-25, incorporates radio frequency interference filtering (not shown), multiple transformer secondaries, and 3-phase, full-wave rectifiers with combination passive and active filtering. Redundant 28-volt regulators in each of the two power supplies independently supply power to both digital computers. The 28 volt regulators also supply power to the random 5 volt

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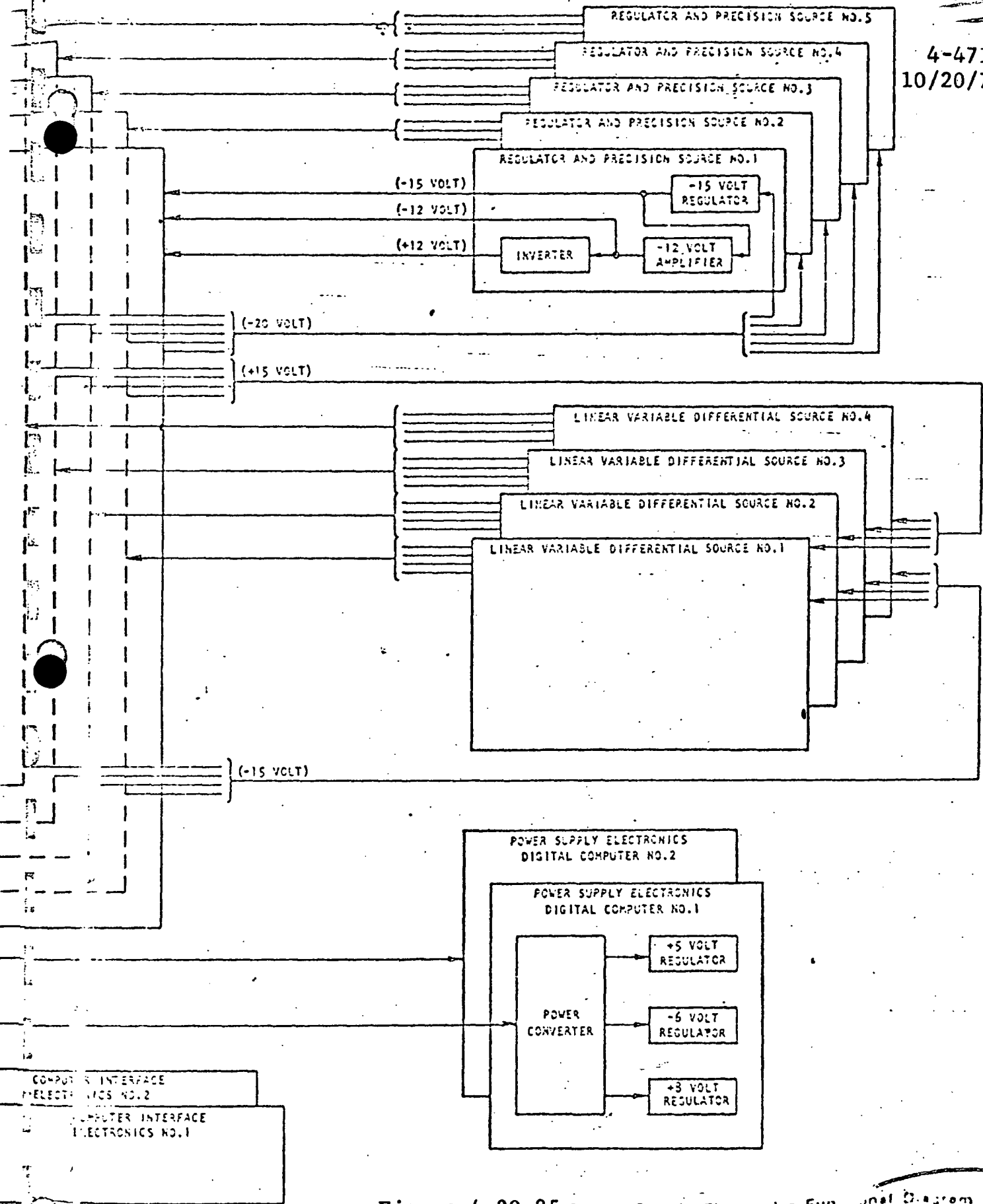
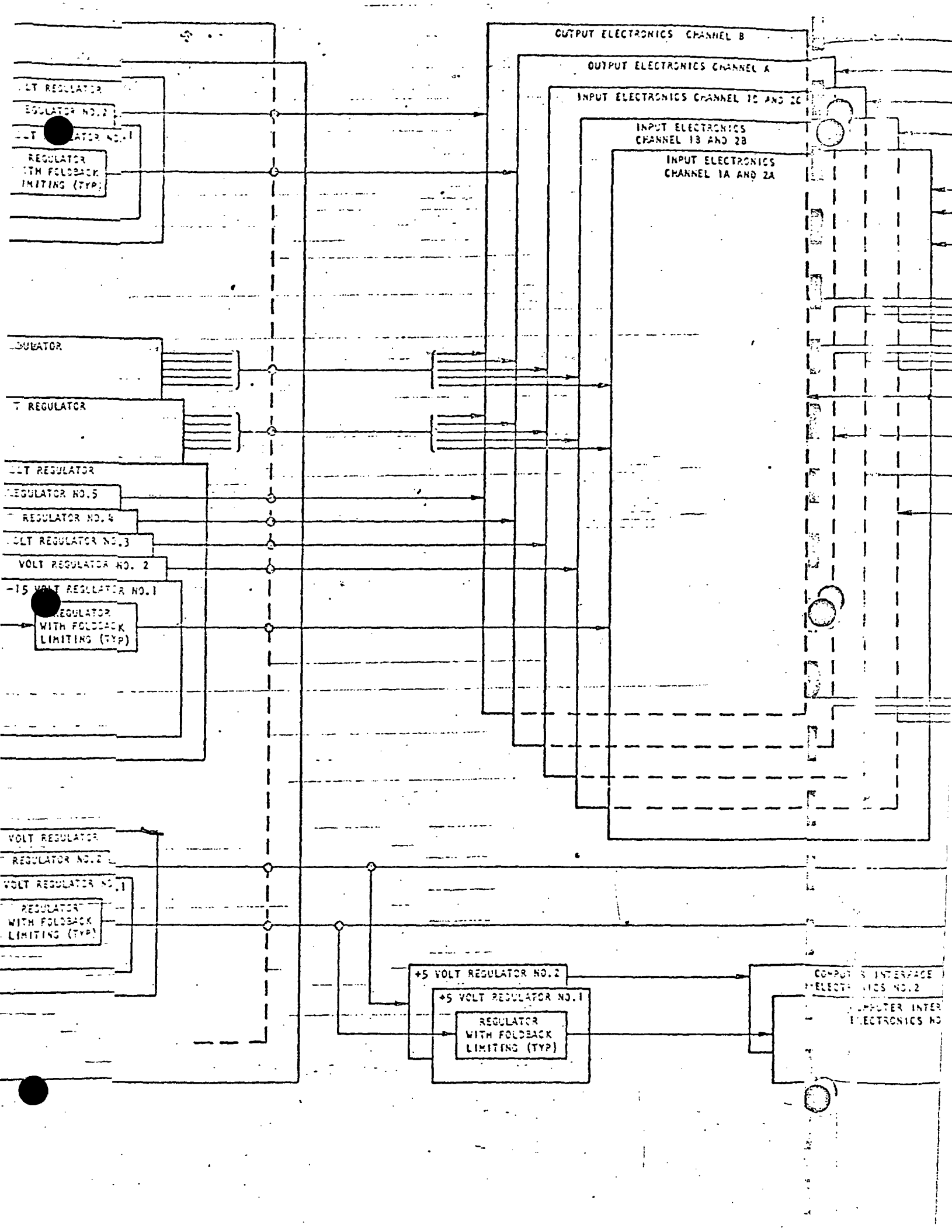


Figure 4.20-25 Power Supply Electronics Functional Diagram

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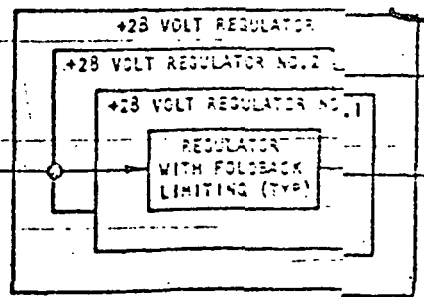
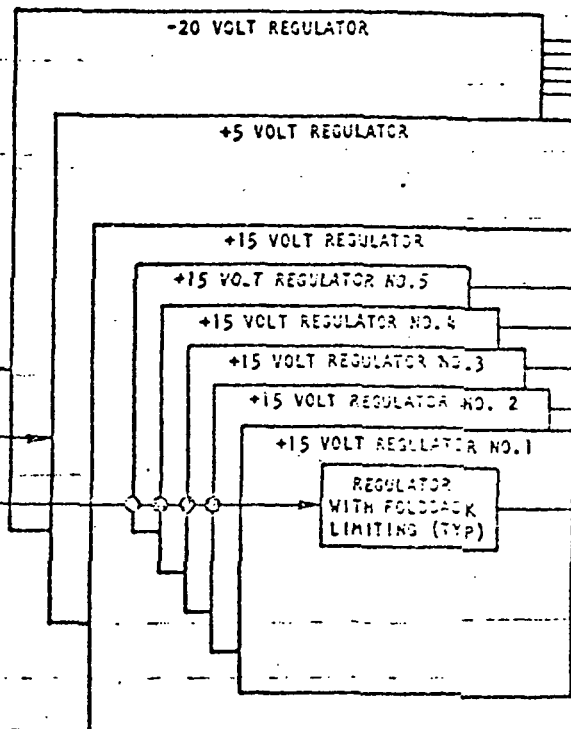
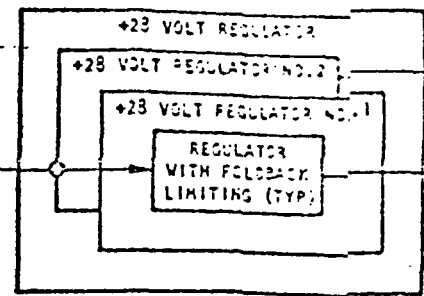
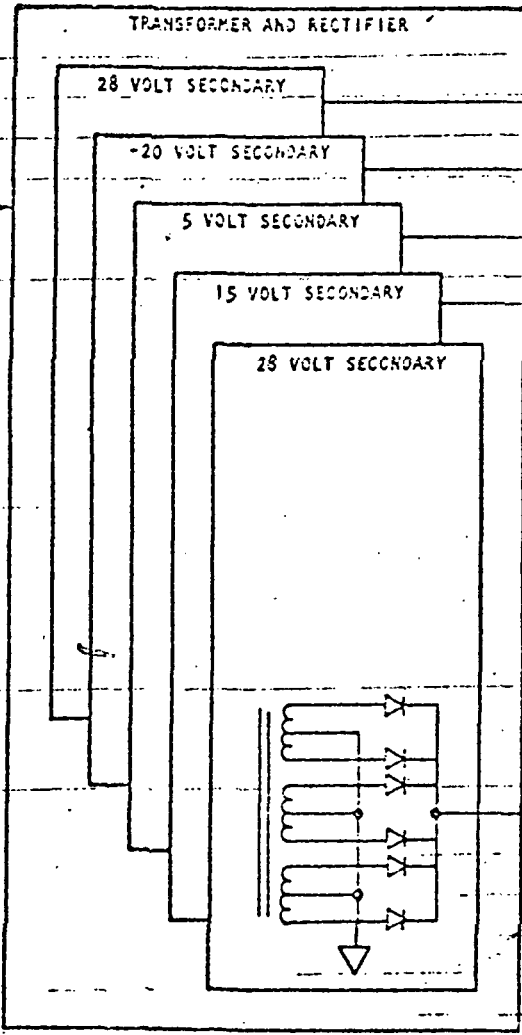


POWER SUPPLY ELECTRONICS NO.2

POWER SUPPLY ELECTRONICS NO.1

115 VOLT
3 PHASE
400 HERTZ
BUS NO.1

115 VOLT
3 PHASE
400 HERTZ
BUS NO.2



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regulators for the input electronics, eliminating an additional regulator in each supply. The digital computer power is obtained from a dc to dc converter to provide isolation and to preserve the existing circuit and logic design of the HDC-601 computer.

Redundant regulators provide +15 volts, +5 volts, and -20 volts for the input and output electronics. Separate +28 volt regulators supply the solenoid valves. The power supply electronics for each input and output electronics channel includes a precision dc reference source for the analog-to-digital and digital-to-analog converters, and the temperature and pressure sensors. Also included is a precision ac reference source for the linear variable differential transformers. The power supplies use both series and switching type regulators. The choice is dictated primarily by efficiency considerations, with the aim of minimizing internal power supply dissipation. The 28 volt regulators with their high and variable current loads and the high-current, 5 volt regulators are of the switching type with noise suppression.

Each power supply branch includes provisions to monitor the voltage levels and to shut down the branch if high out-of-tolerance voltages are experienced. Power shut down

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42 capability is also controlled by the watchdog timers and by the digital computers.

Simultaneous loss of power on both input power buses for more than a few milliseconds will force the controller into an inactive standby condition. If power is restored on one of the buses within 50 msec, normal operation will resume. If not, a safe engine shutdown will be initiated.

The power supply electronics for the digital computer include a power failure and recovery interrupt circuit. Figure 4.20-26. This circuit initiates a computer interrupt to store all critical computation parameters before shutdown, enabling a successful reinitiation of the computer program upon power recovery. The interrupt is initiated by over voltage, under voltage, or loss of power either due to power bus failure or to an intentional shutdown by the watchdog timer.

As shown in Figure 4.20-27, the energy stored in the power supplies will sustain computer operation for a minimum of 125 microsec after power interruption. This is more than adequate time for the computer to perform an orderly and safe shutdown. When power recovery occurs and the supply voltages

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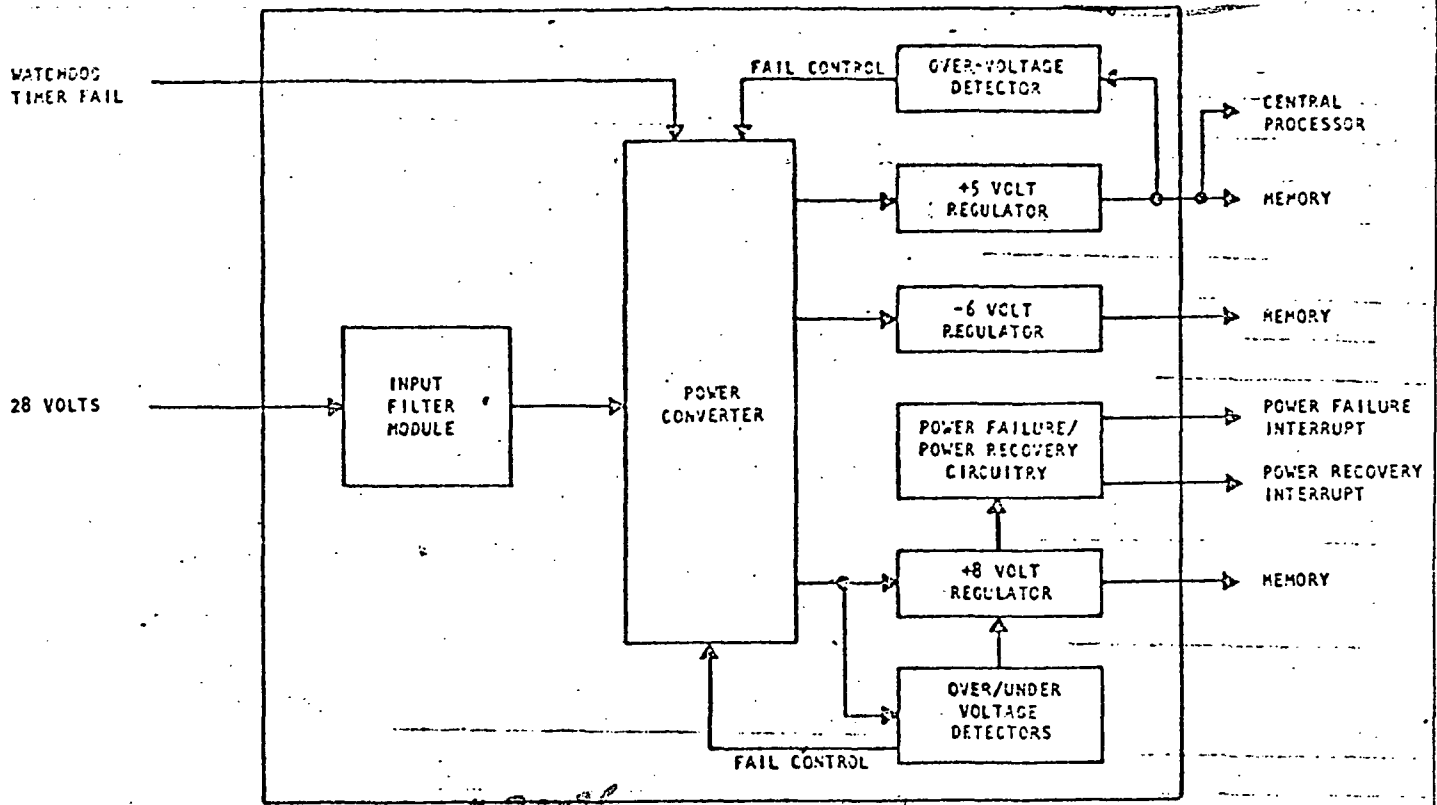


Figure 4.20-26 Processor Power Failure Detection

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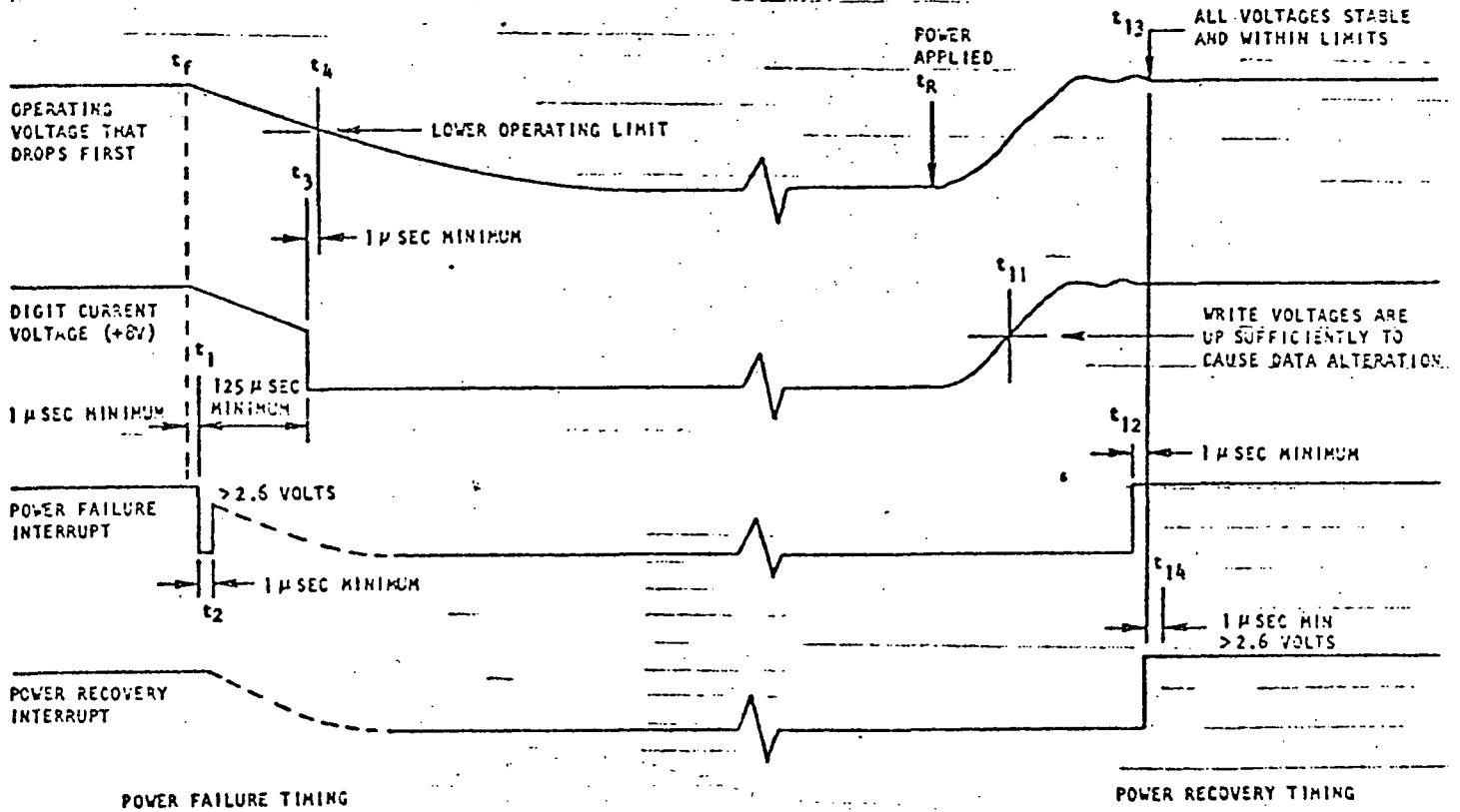


Figure 4.20-27 Power Detection Timing Requirements

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42 stabilize, the power recovery circuit generates an interrupt to resume normal computer operation.

Power Requirements

The total electrical power required by the engine is a maximum of 560 watts during steady state conditions and 870 watts for 3.5 seconds during engine start. Of the 560 watts total required during steady state conditions, 443 watts are dissipated in the controller and 117 watts are dissipated in valves and sensors.

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REF. 42 4.20.5 CONTROLLER SOFTWARE

The selected avionics approach incorporates two general-purpose Honeywell HDC-601 digital computers packaged within each of the three main engine controllers. The computers can be fully reprogrammed to solve any computational problem within the hardware limitations of word length, processing speed, and memory capacity. Each computer has its own program stored within its 2-mil plated-wire computer memory. The programs may easily be changed by using a portable memory loader. The memory loader interfaces with the controller through ground support equipment electrical connectors on the controller. The memory loader obtains the program information from a punched tape, which it encodes into electronic information to be stored in the computer memories. The memory loader also checks the computer program against the punched tape after it is read into the computer memory to ensure that no errors have been introduced into the program.

The capability of easily changing the programs stored in the controller computer memories provides a flexibility to accommodate normal development changes quickly, safely, and at low cost. The approach to developing the flight program for the controller is to create one main program, called the executive program, and several special purpose subprograms.

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The individual subprograms perform special numerical computations on data or make logical decisions (e.g., igniter checkout, start preparation, or start). The executive program has the primary task of supervising the sequence of processing subprograms when needed and for keeping track of the total status of the engine, avionics and commands from the vehicle.

The HDC-601 has a fully developed standard software programming library consisting of:

1. DAP-16 Assembler
2. FORTRAN IV Compiler
3. Standard Input/Output Library
4. Mathematical Library
5. Utility Routines

4.20.5.1 CONTROLLER EXECUTIVE PROGRAM

The executive program establishes the sequence of operations to be performed by the digital computer. Operation of the executive program is cyclic. A complete cycle (one pass through the executive program) is completed every 20 milliseconds. Figure 4.20-28 is a simplified flow chart of the executive program. Under normal operation, whether on the ground for checkout or during flight, the computer progresses through the executive program, performing the indicated operations in an endless loop. The loop is broken and the

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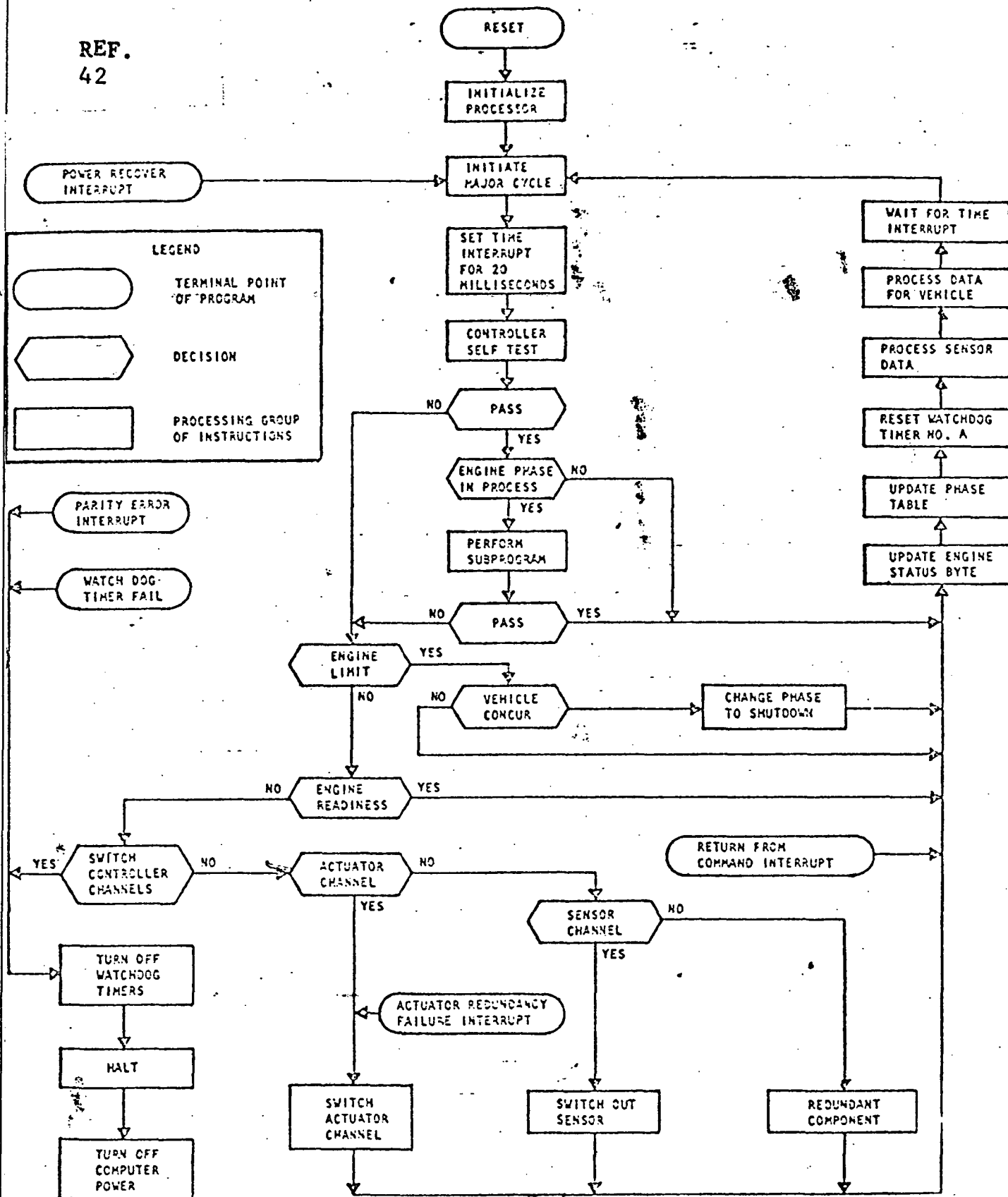


Figure 4.20-28 Major Cycle Executive Program

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sequence of operations is revised by any one of several possible events:

1. Command received from vehicle alters control or checkout phase of operation.
2. Built-in test determines component failure.
3. Engine limit detection monitor determines engine exceeded allowable limits.

The executive program contains the logic to evaluate all of the three events listed, update the engine status byte and phase table stored in computer memory, and change the sub-programs to be processed by the computer.

As indicated in Figure 4.20-28, by the five terminal points, the executive program may be entered from several points with different external conditions. The start of the executive program cycle during ground operation begins with application of power to the controller which resets and initializes the computer. This inhibits controller outputs during the transition to full electrical power and forces the executive program to start from a predetermined memory location. The engine status byte and phase tables are set to the initiation condition. A controller self-test is processed each cycle. Successful completion of the controller self-test is required prior to performing a subprogram of

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42 engine operation. The logical decision "engine phase in process" is processed by the executive program to determine which subprogram, listed in Table 4.20-13, is to be processed. A failure detected during controller self-test or engine phase subprogram processing is evaluated and corrective action taken as indicated. Exceeding an engine limit condition will result in an engine shutdown only if the vehicle will permit a shutdown. The engine status byte and phase tables are updated each cycle to indicate current engine status and engine sequencing phase.

One watchdog timer is reset each time through the executive program cycle. Sensor data which does not require executive program control to be processed into memory are validated, redundancy verified, and parameter values averaged in the block "process sensor data". Maintenance data for vehicle recording is processed in the block process data for vehicle. This completes the major executive cycle in less than 20 msec. The executive program then waits for the computer real time counter to signal a time interrupt to repeat the cycle.

The executive program cycle may be interrupted in any part of the repetitive cycle by interrupts generated by built-in test within the controller or by vehicle command interrupts.

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TABLE 4.20-13 SUBPROGRAM

SUBPROGRAMS

1. AUTOMATIC CHECKOUT
 - A. MEMORY SUM CHECK
 - B. PRESSURE SENSORS CALIBRATION CHECK
 - C. TEMPERATURE SENSOR FUNCTIONAL CHECK
 - D. FLOW/SPEED SENSOR FUNCTIONAL CHECK
 - E. VIBRATION SENSOR FUNCTIONAL CHECK
 - F. SPARK IGNITER FUNCTIONAL CHECK
 - G. ACTUATOR/VALVE FUNCTIONAL CHECK
 - H. PNEUMATIC SHUTDOWN TEST
 - I. EMERGENCY BOOST MODE LIMIT SHUTDOWN
CONTROL FUNCTIONAL CHECK
 - J. EXTENDABLE NOZZLE FUNCTIONAL CHECK
2. START PREPARATION
 - A. GN₂ PURGE
 - B. INTERMEDIATE SEAL PURGE
 - C. HELIUM FUEL SYSTEM PURGE
 - D. PROPELLANT RECIRCULATION
 - E. HELIUM FUEL SYSTEM PURGE: PROPELLANTS
DROPPED
3. FLIGHT
 - A. START
 - B. MAINSTAGE
 - C. SHUTDOWN
4. POST-SHUTDOWN
 - A. PROPELLANT DUMP
 - (1) LIQUID OXYGEN DUMP
 - (2) FUEL DUMP
 - B. ABORT TURNAROUND BOOSTER
 - (1) HELIUM FUEL SYSTEM PURGE
 - (2) PROPELLANT RECIRCULATION

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Memory parity, watchdog timers, actuator redundancy failure, and loss of electrical power initiate interrupts by hardware built-in test within the controller. A loss of power results in a power interrupt which causes computational operation to stop for the duration of the failure. If power is restored, a power recovery interrupt is generated which starts the executive program at the "initiate major cycle" block. This is different from normal power startup because the computer memory still retains all data processed prior to the interrupt, including engine status byte and phase tables. Thus, if the power failure is not too long (less than 50 milliseconds), normal control may be resumed.

Parity error or watchdog timer failure are failures of a controller channel and cause control to switch to the redundant operational channel. They generate interrupts, which turn off both watchdog timers for the failed channel, command the failed computer channel to HALT processing, and turn off power to the failed computer. Power can be restored to the failed channel only by cycling the reset. Normally, this is not done until the flight is ended and the controller is being checked out.

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Vehicle command or data requests are input to the vehicle at any time and interrupt the executive program for processing, as illustrated in Figure 4.20-29. The executive program resumes control upon completion of the processing and implements the command or request for data.

The six engine mission phases are: (1) checkout, (2) start preparation, (3) start, (4) mainstage, (5) shutdown, and (6) post-shutdown. Subprograms common to engine phases are not duplicated for each phase, which conserves memory. The executive program determines entry and exit points for linking programs together. The subprograms are expanded and described in detail in later sections. For the three flight phases (start, mainstage and shutdown), all computations in the subprograms associated with each phase are accomplished each major cycle. The remaining phases each require multiple cycles to complete the required operations. For example, the automatic checkout subprogram may command an actuator to move. It will verify the motion on later major cycles, giving time for the actuator to respond.

Inputting sensor data into memory is not a function of the executive program, but is under control of the direct memory access. This requires no processor time; however, the direct-memory access sequence may be altered by the executive program.

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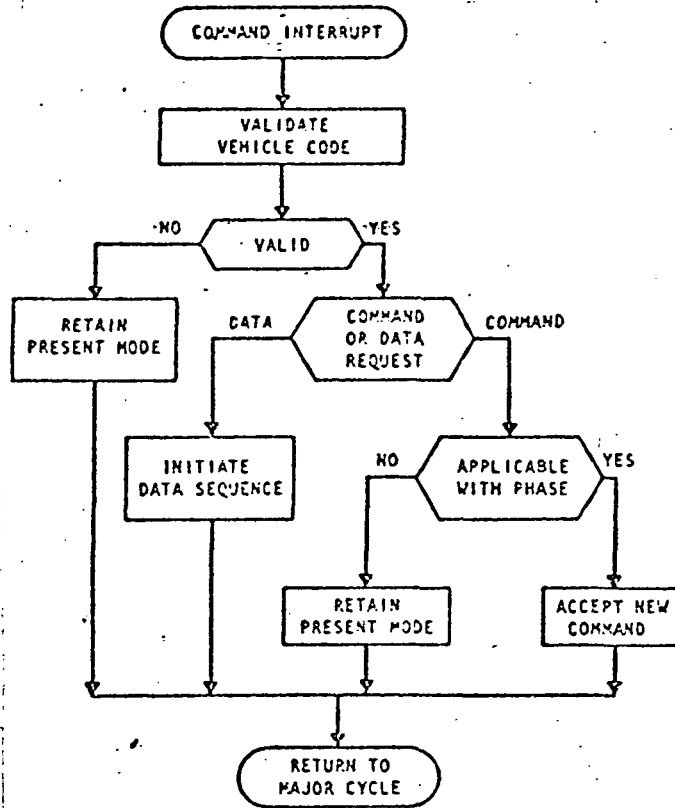


Figure 4.20-29 Vehicle Command Interrupt

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42 4.20.5.2 CONTROLLER SELF-TEST

The controller self-test program (Figure 4.20-30) is executed during each cycle through the executive program. It verifies the status of all controller components except for some of the low-level multiplexer switches, vibration sensor input amplifiers, and position sensor input demodulators. Those components are checked as part of the sensor input tests.

The individual controller subsections are tested in sequential fashion, as shown in Figure 4.20-30. If a component failure which does not impair the operability of the controller is detected, the failure is indicated to the executive and the program returns to the next step normally performed in the test sequence. If a failure occurs which results in an inoperative controller channel, the controller self-test program indicates the failure to the executive and transfers control to the executive for the processing of channel shutdown, indicated in Figure 4.20-28.

4.20.5.3 AUTOMATIC GROUND CHECKOUT

Upon receiving a checkout command via the vehicle data bus, the executive program selects the automatic ground checkout mode. Since the controller self-test has been performed as a part of each pass through the executive program,

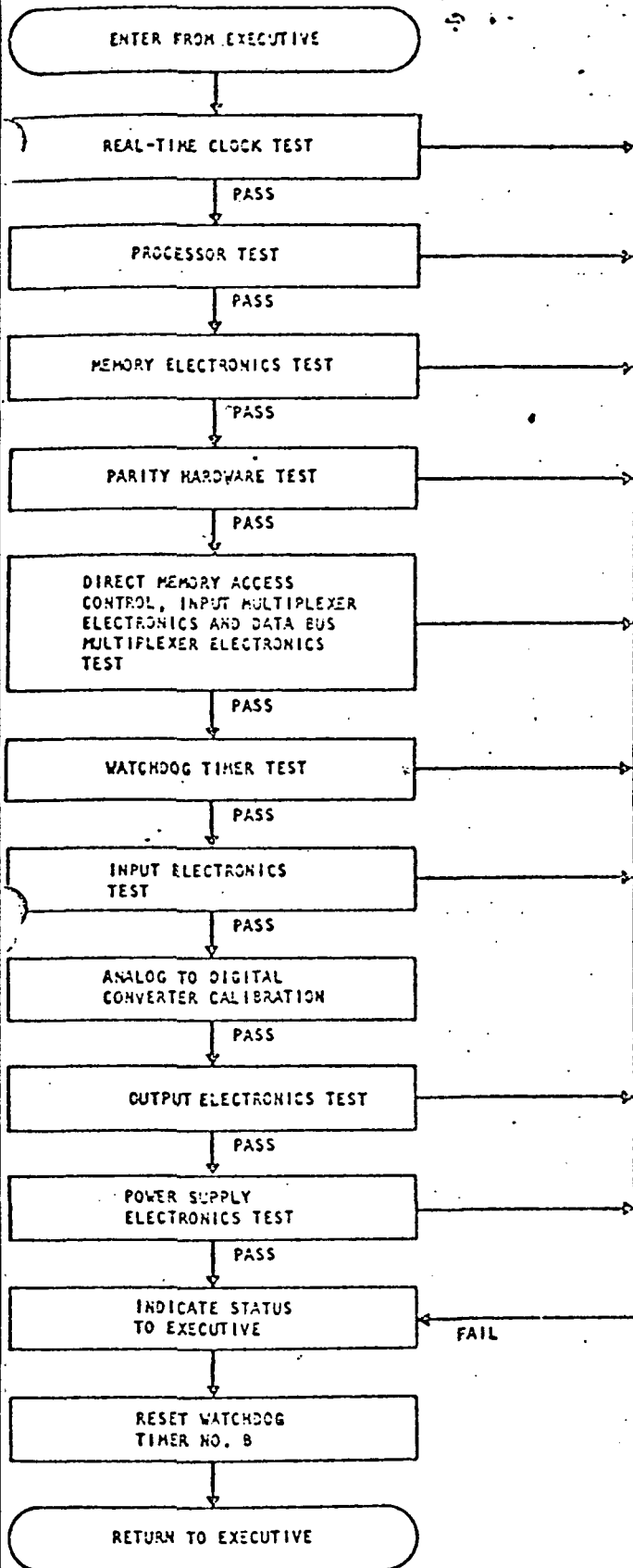


Figure 4.20-30
Controller Self Test

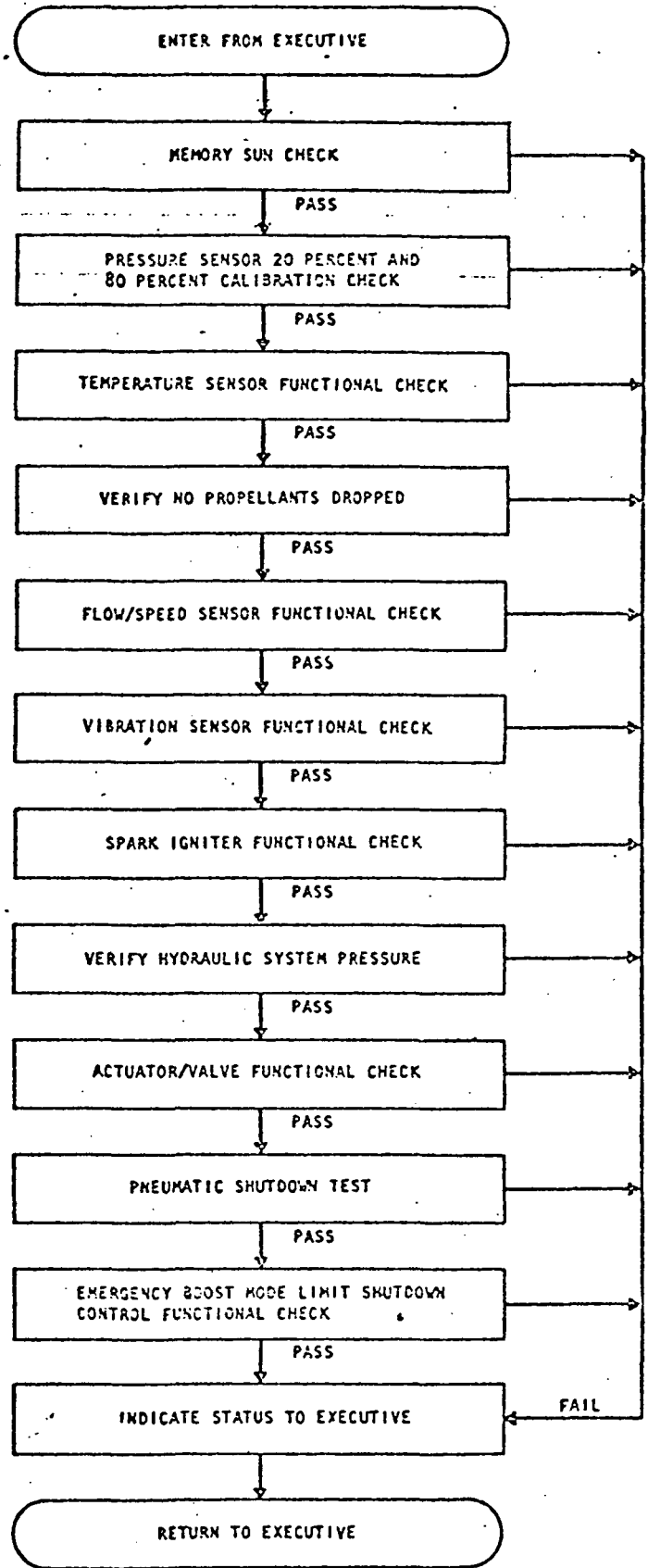


Figure 4.20-31
Automatic Ground Checkout

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the components remaining to be checked include actuators, valves, spark igniters, sensors, and certain sensor interface circuits which cannot be completely checked by the controller self-test. An additional memory sum test of the computer memory is also performed as further assurance that the program is valid and that all memory locations can be addressed.

The automatic checkout begins with the memory sum test, as shown in Figure 4.20-31, and continues with a checkout of pressure and temperature sensors. A check is made to ensure that no propellants have been dropped before any further checkout is performed. Tests of the remaining components noted above are then made. This includes a verification of all redundancy and fail-safe backup provisions.

Any failure detected in the checkout sequence is identified to the executive. If the failure does not prohibit further checkout, the program returns to the checkout sequence and completes the tests. Status upon completion of the checkout is indicated to the executive, which in turn processes it for transmittal to the vehicle when requested.

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Subprograms which provide a checkout of individual components or types of components are contained in the computer memory. The propellant and pneumatic valves and extendible nozzle may be individually checked out. The sensors are checked out as a group. The spark igniters are also checked out as a group. The flow charts for these component tests are presented in Figures 4.20-32, 4.20-33 and 4.20-34.

The propellant valve, extendible nozzle, and spark igniter test programs contain interlocks to verify that propellants have not been admitted to the engine. Since the executive program verifies the engine's operating mode before calling on a subprogram, no additional interlocks are required for the sensor tests.

4.20.5.4 START PREPARATION

The start preparation phase of engine operation may be entered and sequenced by commands from the vehicle following successful completion of an engine checkout. Four purges are required to condition the engine for start. These include:

1. GN_2 purge until engine start and helium purge of high-pressure oxidizer turbopump intermediate seal for approximately 10 minutes prior to dropping propellants.

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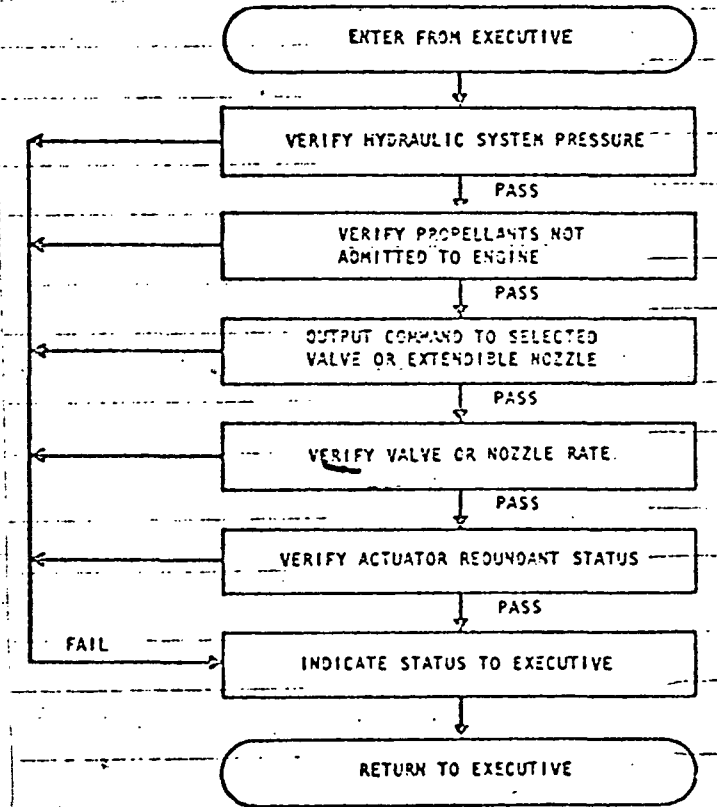


Figure 4.20-32 Propellant Valve/Extendable Nozzle Test

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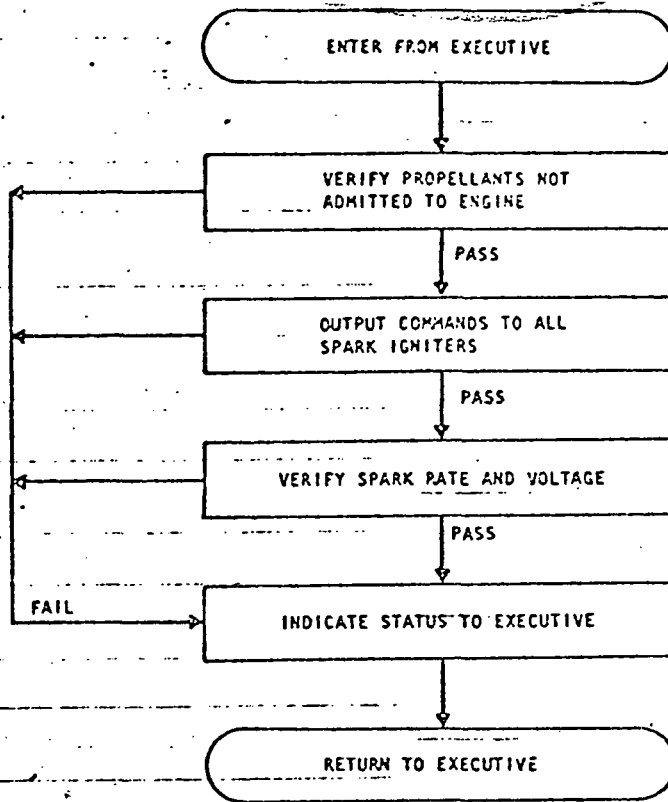


Figure 4.20-33 Igniter Test

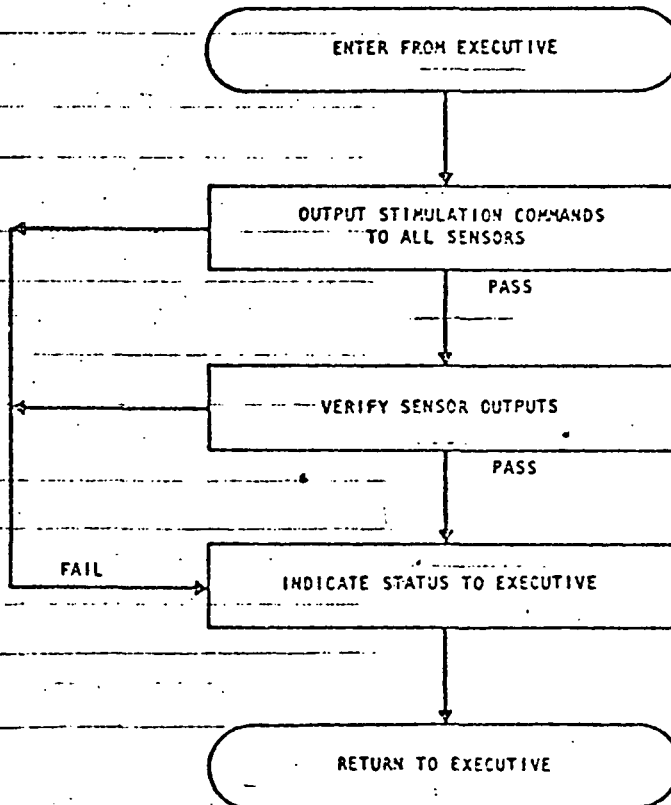


Figure 4.20-34 Sensor Test

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2. Helium purge of the fuel system for approximately 3 minutes prior to dropping propellants.
3. Propellant recirculation when propellants are dropped, and
4. Helium purge of the fuel system repeated for approximately 3 minutes prior to engine start.

The time allocated for each purge is controlled by the vehicle. Interlocks in the executive program phase table verify that the sequence is correct and that conditions are acceptable prior to initiating the first purge.

A flow chart of the start preparation phase is shown in Figure 4.20-35. Each subprogram is designed to be executed for each major cycle.

The first subprograms performed by command from the vehicle are the nitrogen purge and high-pressure oxidizer turbopump intermediate seal purge. Commands to energize the nitrogen and high-pressure oxidizer turbopump intermediate seal solenoids are issued the first time through the subprogram. Correct output command signals and pressure sensor measurements are verified each major cycle of the executive program for the duration of the subprogram. Status is indicated to the executive for evaluation.

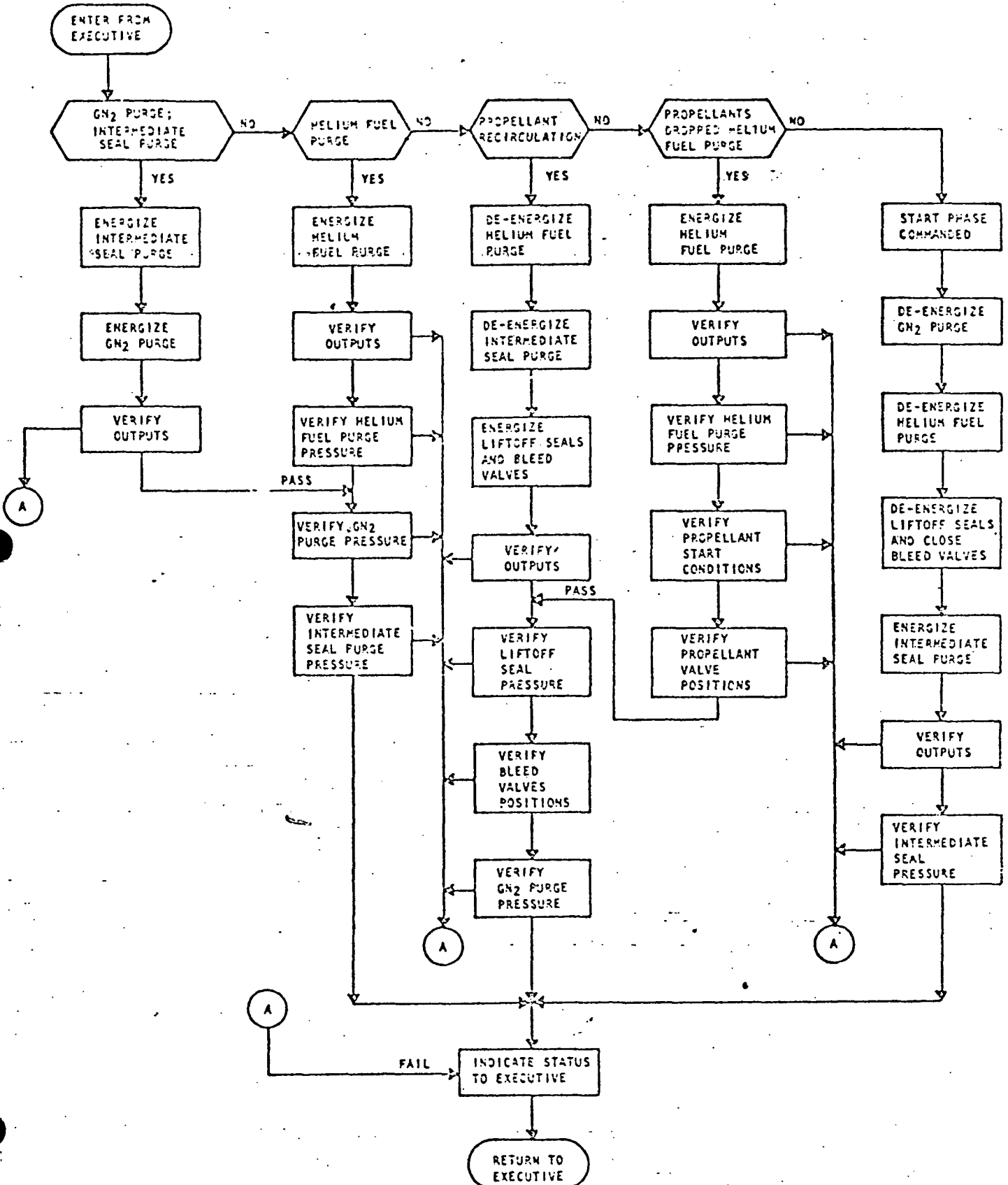


Figure 4.20-35 Start Preparation

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The helium fuel system purge control command from the vehicle sequences the helium fuel system purge subprogram. A command is issued the first time through the subprogram to energize the helium fuel system purge solenoid. Outputs to the solenoids and GN₂ purge pressure, helium fuel system purge pressure, and intermediate seal purge pressure are verified each major cycle for the remainder of the subprogram.

When propellants are admitted to the engine, the vehicle issues a propellant recirculation command. This command terminates the helium fuel system purge and high-pressure oxidizer turbopump intermediate seal purge subprograms and initiates the propellant recirculation subprogram. Commands are issued to de-energize the helium fuel system and intermediate seal purge solenoids. The GN₂ system solenoid remains energized. Additionally, the first time through the subprogram, commands are issued to energize liftoff seals and open bleed valves. Subsequently, GN₂ purge pressure, liftoff seal pressures, fuel and oxidizer bleed valve positions as well as controller output are verified each major cycle for the duration of the subprogram.

The last subprogram of the start preparation is again a helium fuel system purge control commanded by the vehicle and is an addition to the previous subprogram. A command is

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issued the first major cycle to energize the helium fuel system purge solenoid. Outputs to solenoids, GN₂ purge pressure, liftoff seal pressures, helium fuel system purge pressure, and bleed valve positions are verified each major cycle for the duration of the subprogram.

In addition, the propellant pressures and temperatures, and propellant valve positions are measured and verified each major cycle. The engine status byte is updated to "engine ready" 3 minutes after the start of this subprogram if propellant conditions are acceptable for starting the engine. The normal exit from this subprogram is by receiving a start command from the vehicle. Commands are issued to de-energize the GN₂ purge solenoid, the helium fuel system purge solenoid, the liftoff seal solenoids which also close the bleed valves, and energize the intermediate seal purge solenoid. At least one additional major cycle is required to verify that the intermediate seal purge pressure is within limits prior to completing the start preparation phase.

4.20.5.5 FLIGHT PROGRAMS

Repeatable start, mainstage, and shutdown control are implemented with open-loop sequencing of valves, switching to closed-loop thrust control from a thrust level of approximately 10 percent to EPL. Closed-loop mixture ratio control

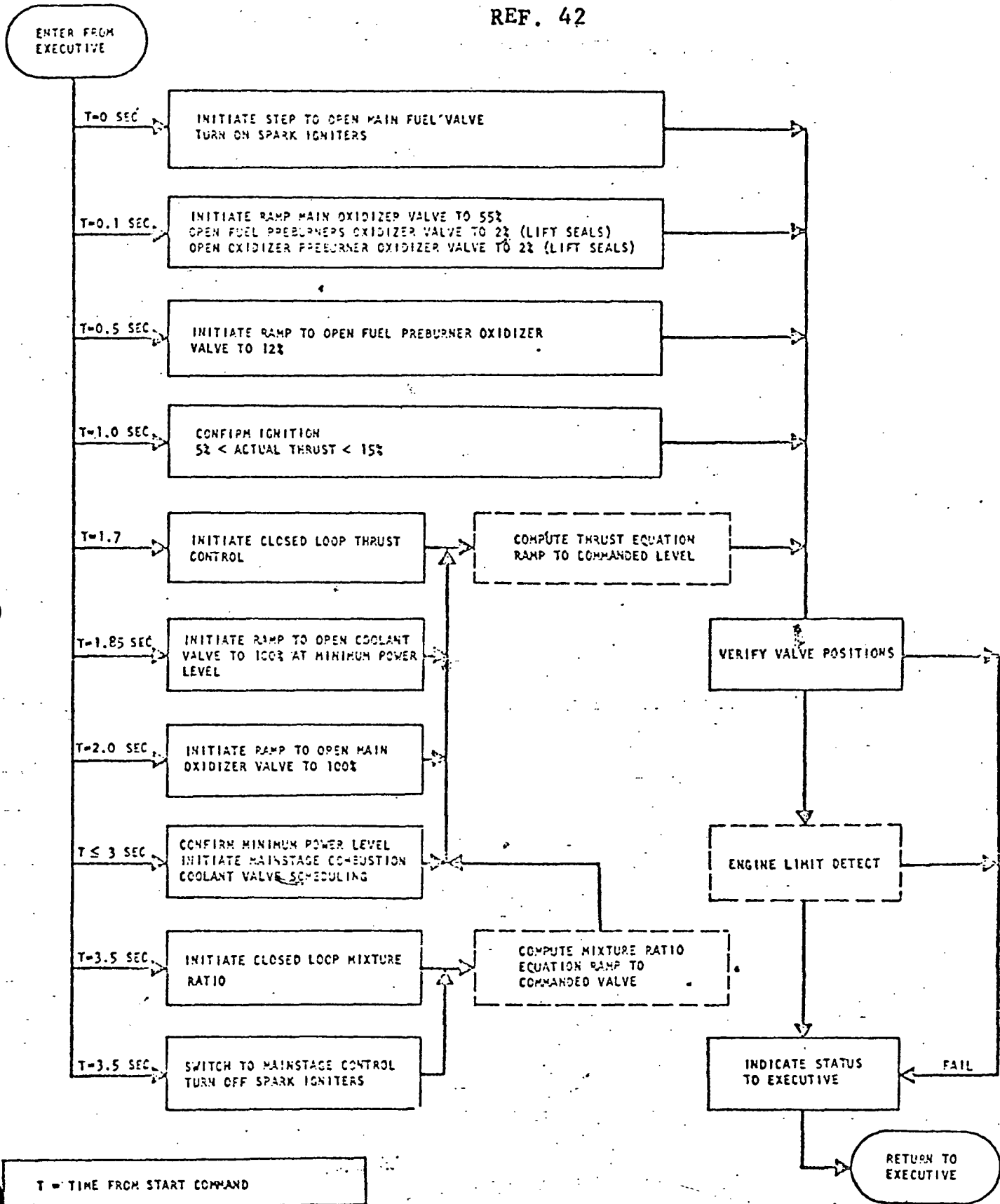
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is implemented 3.5 seconds after start initiation until shut-down. The flexibility of the digital controller allows modification to the sequence of closed-loop logic with simple software program changes.

Start Control

The executive program initiates the start control sub-program upon receipt of the start command from the vehicle. Three interlocks are provided to ensure proper initiation of start. The engine must be in an "engine ready" status and have received thrust level and mixture ratio command values from the vehicle. The start control, shown in Figure 4.20-36, contains a start sequence timer (software program) to control which program branch is followed until time for the next event. The branches correspond to the phases of start control described previously in Section under Engine Start. Actuator commands are computed in the appropriate start control branch, outputted and verified each major cycle. The start sequence timer switches phases as each is completed. Ignition is confirmed at 1 second by verifying that a thrust level of 5 to 15 percent has been achieved. All propellant valves are closed immediately if ignition is not confirmed. The thrust control loop is closed for mainstage control at 1.7 seconds and the thrust is ramped to the commanded level. The loop

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T = TIME FROM START COMMAND

Figure 4.20-36 Start Control

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is closed on mixture ratio control at 3.5 seconds and ramped to the commanded value. Engine limit parameters are monitored each major executive program cycle to ensure safe engine operation throughout the start control. The executive will initiate a shutdown at any time during the start control if an engine limit is exceeded and limit control is enabled by the vehicle or a shutdown command is received from the vehicle.

Mainstage Control

The transition from start to mainstage control is smooth. Closed-loop thrust control is initiated in the start control mode at a 10 percent thrust level. Closed-loop mixture ratio control is initiated at the mixture ratio level present 3.5 seconds after start and ramped to the commanded value. Mainstage control consists of computing and outputting thrust and mixture ratio commands from computed mixture ratio thrust, fuel preburner temperature margin, and oxidizer preburner temperature margin, as illustrated in Figure 4.20-37. Preburner temperature control is only applicable if limit control is enabled by the vehicle. Thrust error is used exclusively to compute the oxidizer preburner oxidizer valve command if limit control is inhibited. The thrust and mixture ratio commands from the vehicle are processed immediately. A shutdown will be initiated during mainstage control by either an

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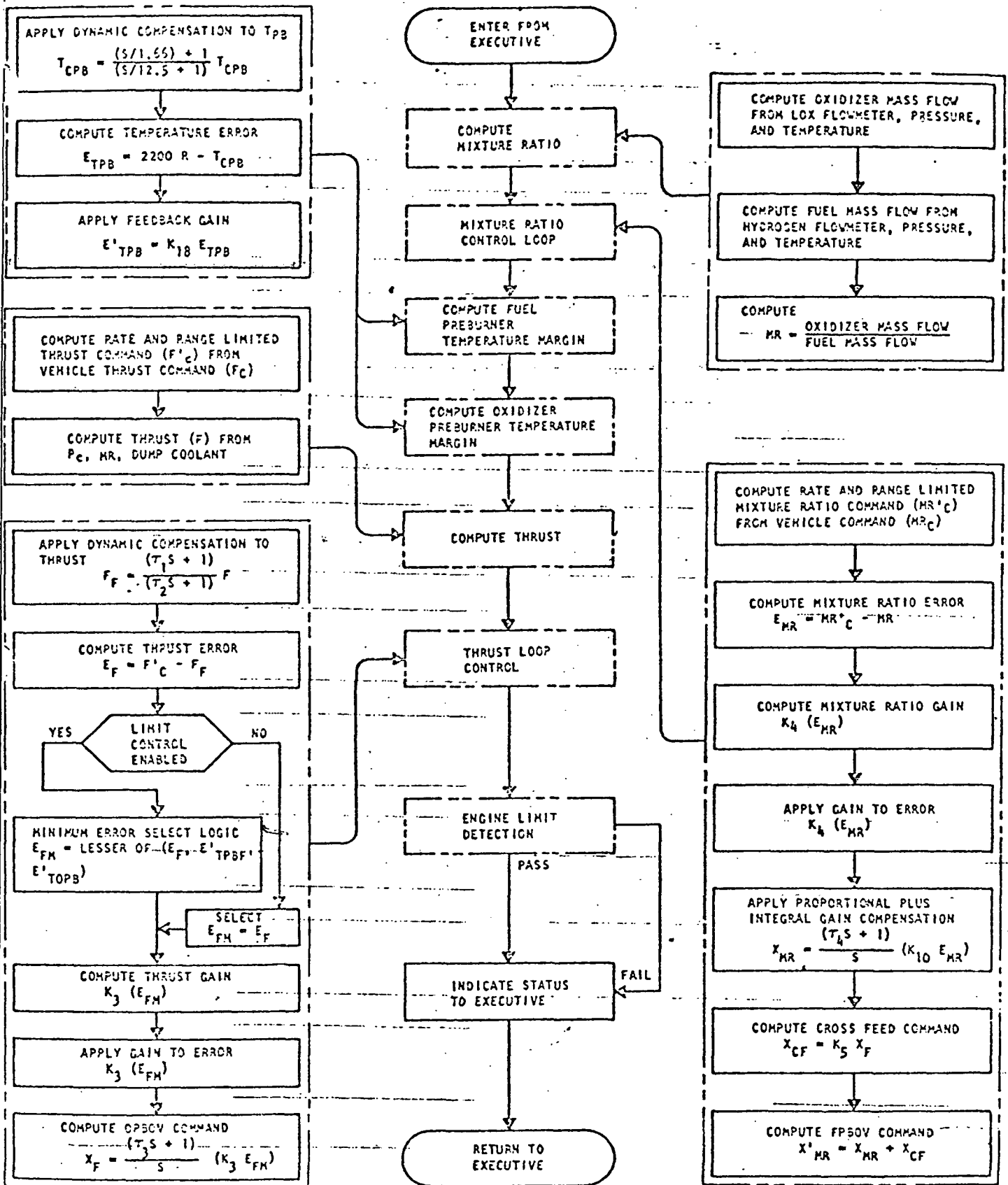


Figure 4.20-37 Mainstage Control

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42 shutdown command from the vehicle.

Shutdown Control

Normal shutdown control is accomplished by closed-loop control thrust decrease followed by a sequencing of propellant valves closed, as shown in Figure 4.20-38. The closed-loop phase uses the same closed-loop thrust and mixture ratio control subprograms as mainstage control. Normal shutdown control is accomplished upon command from the vehicle or by the executive if an engine limit is exceeded and limit control is enabled. The internal thrust reference level determines the entry point of the shutdown phase. Thrust level above MPL initiates a controlled decrease rate of 4800 pounds (21.351 newtons) per 10-msec interval to MPL. Below MPL, a software timer is used to control the sequencing of propellant valves closed. The times indicated in Figure 4.20-38 correspond to when that branch is initiated and followed until the next branch is applicable. Valve positions are monitored each cycle throughout the shutdown subprogram. The executive program automatically initiates retraction of the extendible nozzle 4 seconds after orbiter shutdown.

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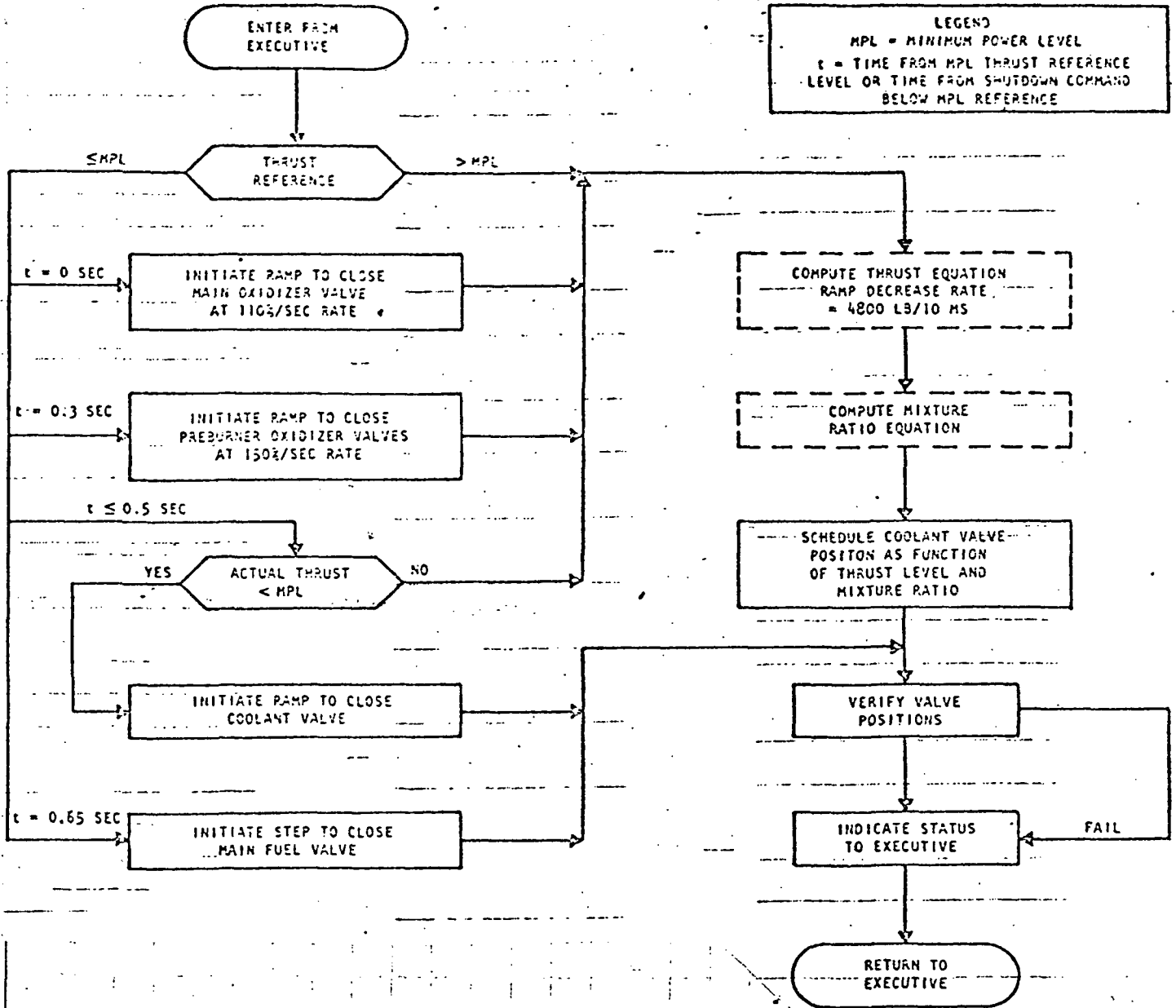


Figure 4.20-38 Shutdown Control

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Post-Shutdown

The post-shutdown phase is entered by the executive with the completion of the nozzle retraction. No subprograms are active during this time; only the controller self-test is performed each major cycle. Power may be safely removed from the engine at this time. Two other options are also available. Propellant dumping through the engine for either the booster or orbiter or an abort turnaround may be commanded for the booster if the preceding shutdown was not due to an engine malfunction.

Propellant Dumping

The executive enters the propellant dump mode of the post-shutdown phase by command from the vehicle. Interlocks are provided by the executive to prohibit opening both fuel and oxidizer valves at the same time. The duration of the mode is controlled by the vehicle. Figure 4.20-39 is a flow chart for the subprogram. Liftoff seals are verified open and bleed valves closed following the propellant dump mode command from the vehicle. Individual valve commands from the vehicle are outputted to the actuators during the appropriate major cycle. An interlock is included to ensure a helium fuel system purge is active for a minimum of 10 seconds following an oxygen dump and prior to a fuel dump.

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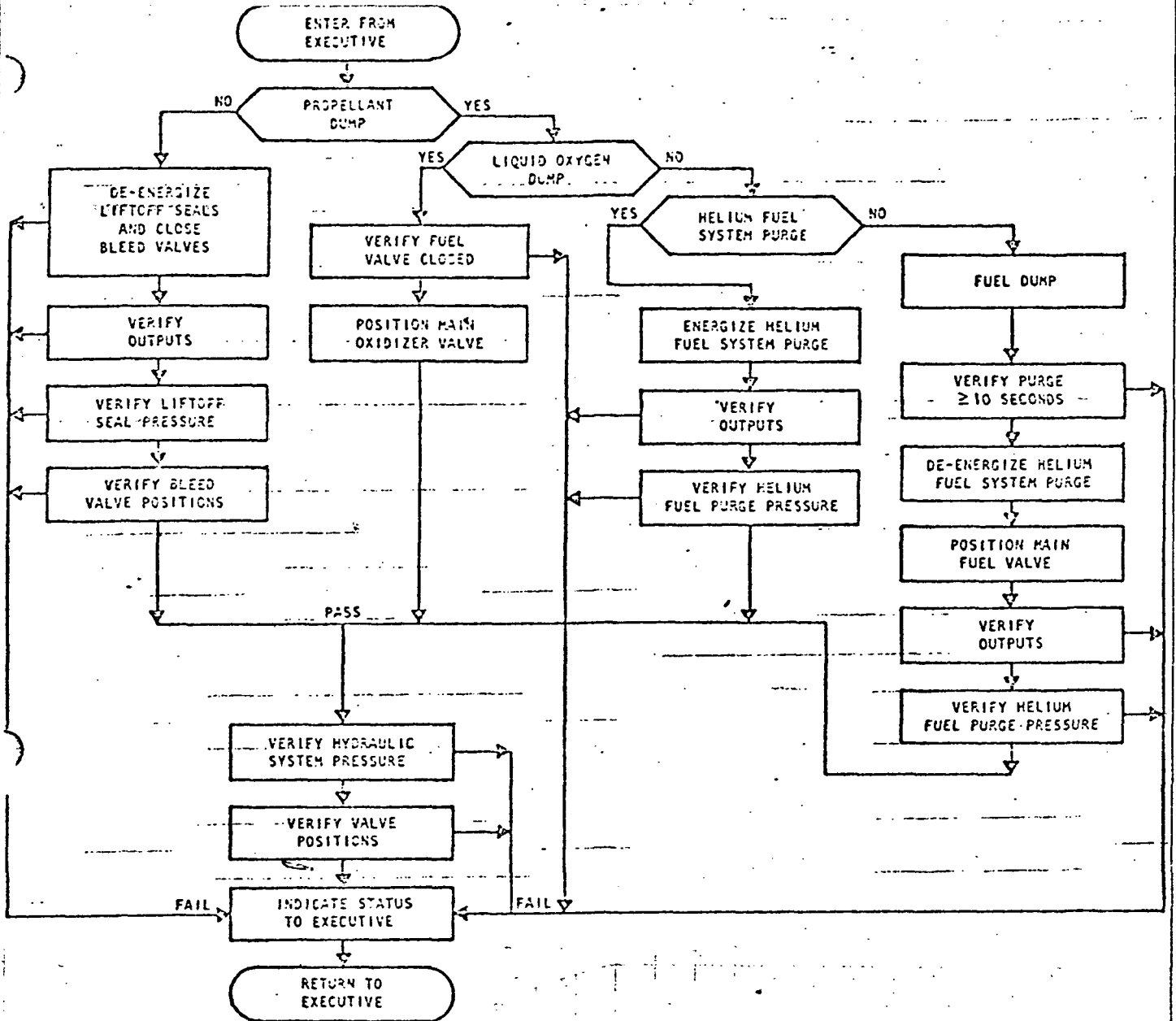


Figure 4.20-39 Post-Shutdown Propellant Dumping

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Following the closing of the main fuel valve, the sequence is complete.

Abort Turnaround

The executive may be commanded to enter an abort turnaround mode of the post-shutdown phase by command from the vehicle. This applies to a booster only if the abort was not due to an engine system malfunction. The sequencing of the mode is controlled by the vehicle, resulting in an engine-ready condition approximately 5 minutes following the shutdown. A flow chart of the subprogram is shown in Figure 4.20-40 and is similar to subprograms of the start preparation phase. Each subprogram is designed to be executed each major cycle.

The first subprogram performed by command from the vehicle is the helium fuel system purge. Commands to energize the helium fuel system intermediate seal, and GN_2 solenoids are issued the first time through the subprogram. Correct output signals and pressure sensor measurements are verified each major cycle for the duration of the subprogram, and any failure detected will be indicated to the executive for evaluation.

The propellant recirculation command from the vehicle sequences to the propellant recirculation subprogram, which

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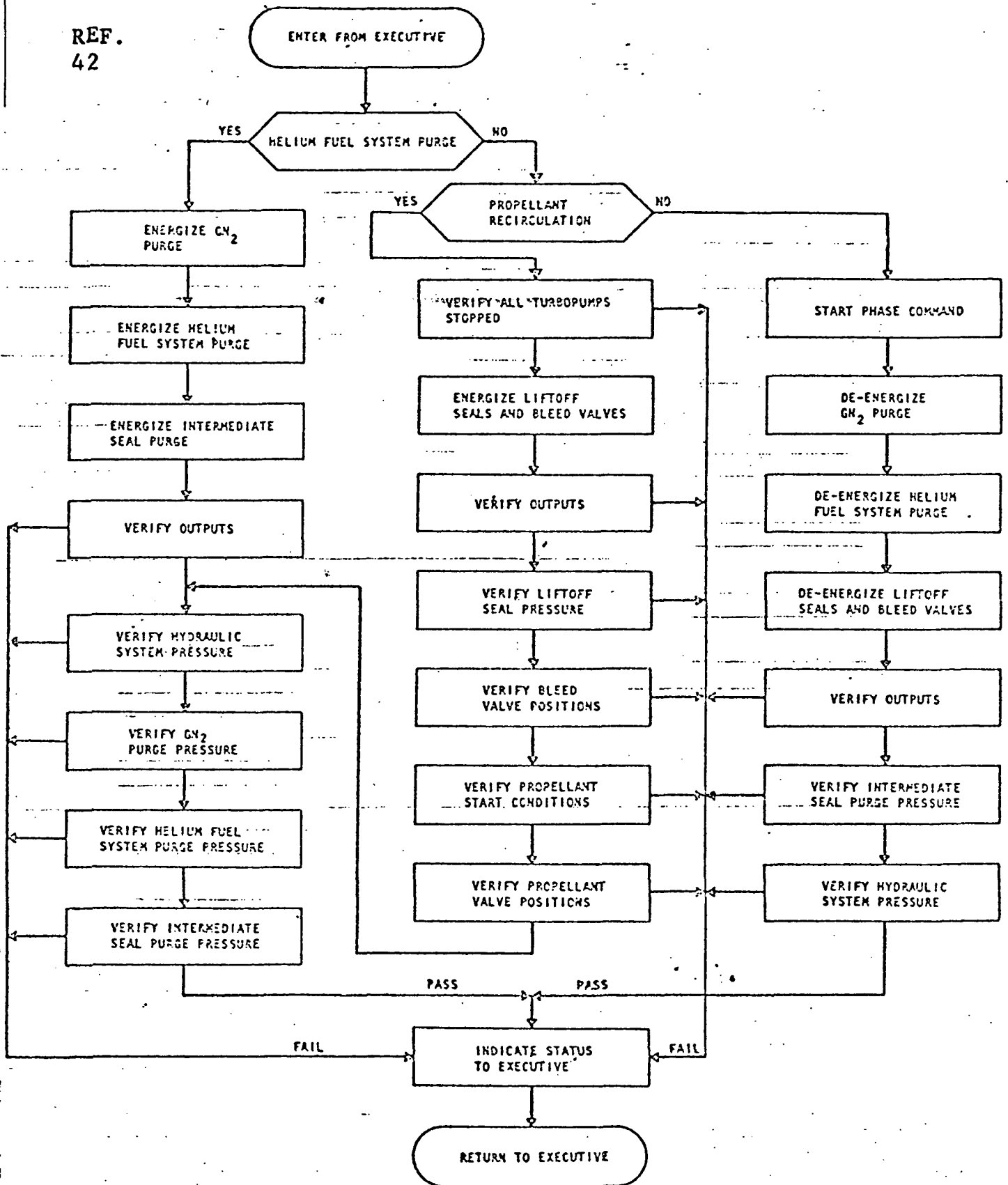


Figure 4.20-40 Post-Shutdown Abort Turnaround

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42 is an addition to the previous one, and a command is issued to energize the liftoff seals and open the bleed valves. Liftoff seal pressure measurements and bleed valve positions are verified each major cycle of the subprogram. In addition, propellant conditions and propellant valve positions are verified each major cycle. Engine status is updated to engine-ready 3 minutes after propellant recirculation commences if propellant conditions are satisfactory for engine start.

The mode is exited when a start command is received from the vehicle. Solenoids for the helium fuel system, GN₂ purge, and propellant recirculation are de-energized. Outputs, intermediate seal pressure, and hydraulic pressure are verified prior to transferring to the start phase.

Power Off

A reset command is required from the vehicle prior to removing engine power. The purpose of the reset is for the executive to differentiate removal of power and a power transient. The phase table and status byte are cleared by the executive with a reset command. Following a power recovery, the executive examines the phase table and determines the correct engine operating phase to return to.

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42 4.20.5.6 SENSOR DATA

Reading of sensor data into memory is sequenced and controlled by direct memory access on a cycle-stealing basis from the processor. Each direct memory access cycle interrupts processing for one memory cycle time (1 microsecond) to directly insert or extract data to/from memory without disturbing computations. Sensor values are computed from raw data and calibration constants stored in memory. Temperature equations are second order and pressure equations first order. After the sensor equations have been calculated, the sensor values are voted and averaged to determine a parameter value which is used in the computational equations and engine limit detection. Figure 4.20-41 is a flow chart illustrating sensor voting and averaging. Each sensor is individually tested and the differences computed. If the differences are within limits, the average value is stored as the parameter value. The subprogram is repeated each major cycle for each parameter except sensors which are for flight maintenance recordings only.

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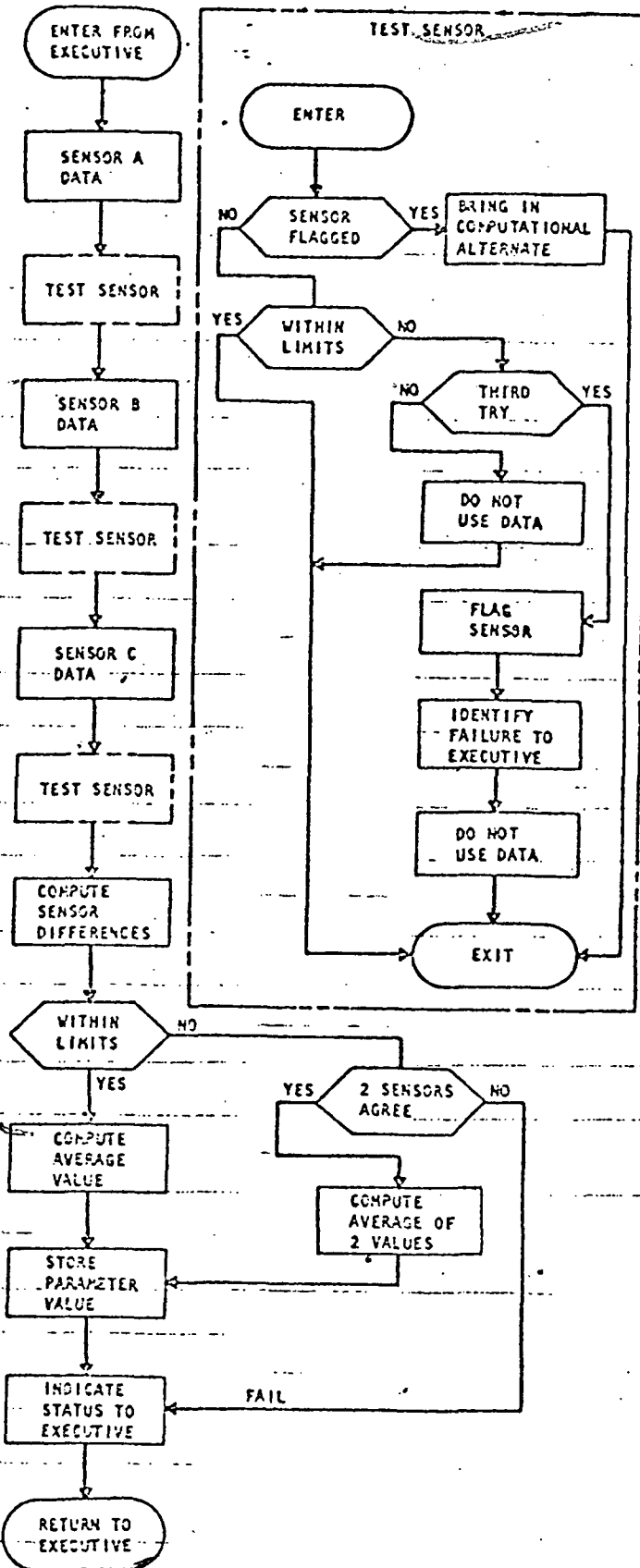


Figure 4.20-41 Sensor Malfunction Detection and Voting

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42 4.20.5.7 ENGINE LIMIT DETECTION

The engine limit flow chart is shown in Figure 4.20-42. Each sensor is tested for range, and if either sensor indicates safe operation, no failure is indicated.

4.20.5.8 COMPUTER SPEED AND MEMORY SIZE CAPABILITY

The controller software requirements are within its computer speed and memory size capabilities, with spare speed and capacity for further software growth.

The required computer speed is dictated by the amount of processing to be performed in the main computational loop, which has an iteration rate of 50 samples per second. The speed requirements for the other executive functions is a slow rate in comparison to the main loop requirements and does not affect the iteration cycle time requirements. The tabulation of the requirement is shown in Table 4.20-14. This requirement is currently being expanded to 16K of memory.

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Since there are 20 msec in each 50 sample per second iteration available for computation, the HDC-601 performs the loop computations 6 msec faster than required, leaving a spare duty cycle capacity of 30 percent for future software growth.

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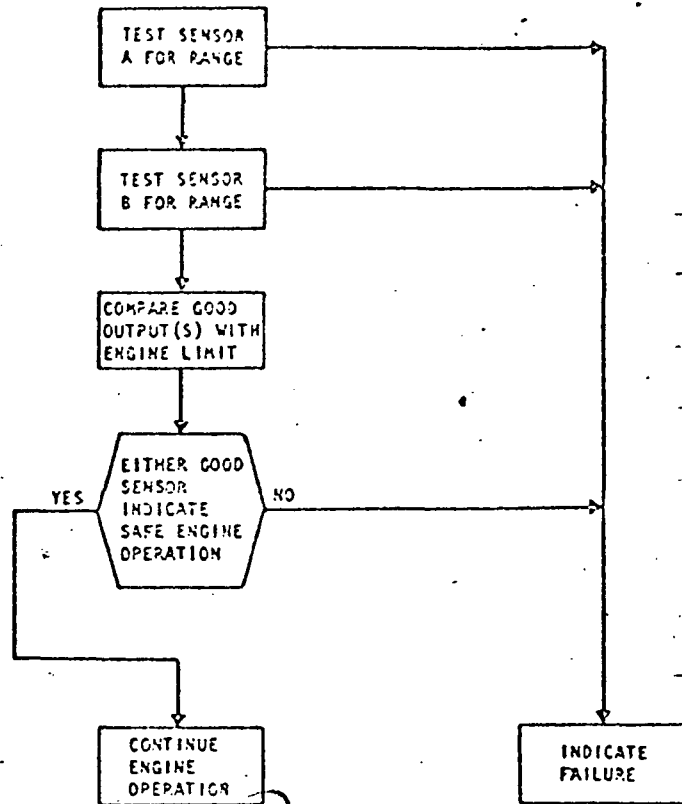


Figure 4.20-42 Engine Limit Detection

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42TABLE 4.20-14 COMPUTER MEMORY AND
SPEED ESTIMATES

FUNCTIONS	MEMORY SIZE (17 BIT WORD)	TIME MS
CONTROLLER BUILT-IN-TEST	1300	1.5
SENSOR BUILT-IN-TEST	1400	7.5
ACTUATOR/VALVE BUILT-IN-TEST	200	0.5
DATA TRANSMISSION	200	0.5
EXECUTIVE PROGRAM	1000	1.0
AUTOMATIC CHECKOUT SUBPROGRAM	500	-
START PREPARATION SUBPROGRAM	300	-
FLIGHT SUBPROGRAM START	300	-
MAINSTAGE	1200	3.0
SHUTDOWN	300	-
POST-SHUTDOWN SUBPROGRAM	300	-
SUBTOTAL	7000	14.0
GROWTH	5000	6.0
TOTAL	12000	20.0

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42Computer Memory Size

Computer memory size is dictated by the capacity required for all programs executed by the controller. The tabulation of this is shown in Table 4.20-14. This tabulation shows that there is a 41 percent spare memory capacity for future software growth.

4.20.5.9 HDC-601 PROGRAMMING FEATURES

The cost and time for development(during Phase CD) of the controller control and checkout program is reduced by the off-the-shelf availability of the complete, thoroughly debugged HDC-601 library. Control of the main program and subprograms is optimized for minimum processor time and software by:

1. Timely processing of vehicle commands using the HDC-601 priority interrupt function.
2. Initiation of main program loop at 20 msec intervals under a lower priority computer clock-driven interrupt.
3. Initiation of lower frequency data transmission sorting loops by lower priority computer clock-driven interrupts.
4. Direct memory access of sensor data independent of central processor operation.

The two standard software systems available for use in programming, debugging and maintenance of the controller processor

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42 and associated memory are (1) DDP-516 standard software and (2) HDC-601 diagnostic programs.

DDP-516 Standard Software

A comprehensive package of DDP-516 programs is available for use with the HDC-601 and controller as part of the Honeywell standard product line software. These programs, designed for a wide range of user skills and applications, include the most widely used programming practices and conventions. The software package includes the following items: DAP-16 Assembly Program, FORTRAN IV Compiler, Utility Routines, Input/Output Routines, and Mathematical Subroutines. For example, the DAP-16 program is used off line in the DDP-516 to convert the controller instructions from the initial assembly language to machine language. Another program simulates all controller programs on a computer with FORTRAN IV capabilities.

HDC-601 Diagnostic Programs

In addition to the DDP-516 programs, an extensive package of diagnostic programs for use with repair depot level is available with the HDC-601. These programs are designed to verify the operation of the processor and memory, and in the case of a faulty operation, to detect and isolate faults to the replaceable subassembly level. The diagnostic package consists of a computer self-test, a processor module

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42 test, and a plated wire module test. The diagnostic tests are performed in conjunction with three pieces of support equipment, the Computer Control Unit (CCU), the ASR-35 Teletype Unit, and a high-speed paper tape reader.

Computer Self-Test

The purpose of this program is to determine whether the processor and memory of the computer are functioning properly and indicate failed subsystems. It is the same as used in flight controller self-tests.

Processor Module Test

The purpose of the processor module test is to check all of the functions of the processor and the Computer Control Unit and to isolate functional failures to the board level.

The processor module test is a semiautomatic procedure composed of a manual portion and an automatic portion. The manual portion is used to check the hard-core of the processor, to check any instructions which require operator intervention, and to initiate the automatic portion. The instructions checked in this manual fashion are those associated with the hard-core (PAS, SKP, and HLT), the switch testing instructions (SR 1, 2, 3 and 4, SSR and SSS), and the interrupt-associated instructions (ENB and INH). Instruction repertoire and

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42 definitions are included in Volume 62, Honeywell Report, "Honeywell HDC-601 Digital Computer Programmers Reference Manual".

In addition to the above instructions, the functions of the PPI/PPH switch and power failure/power recovery circuitry are checked in the manual portion of the processor test.

The automatic portion tests the remaining instructions of the processor. Checkout of the indexing, indirect addressing, and extended addressing function of the processor is included in the automatic portion.

The basic approach of the test program is to use the "successive tests" technique. This technique requires that the individual checks of processor functions be organized in a building-block fashion starting with the hard-core and building toward the more complex functions. Such an approach yields an automatic functional isolation of processor failures. Whenever a functional fault is encountered, the program will output a message to the ASR Teleprinter informing the operator which board has failed.

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Plated Wire Module Test

The purpose of the plated wire module test program is to detect functional faults within a plated wire memory and to isolate these faults to the replaceable subassembly. This program is designed for use with the processor and the plated wire memory. The program tests the functions of the memory, i.e, addressing, writing, and reading. The plated wire modules test is designed to exercise the memory in two parts. The test is contained on two tapes, one of which checks the lower portion of memory, the other checks the remainder.

The test is designed to detect errors through the use of the following checks: (1) addressing test, (2) data complement, and (3) disturb test. The addressing test is designed to ensure all the address electronics are functioning properly and are addressing the proper memory locations. The memory address is decoded by the X and Y decoder to select the proper word strap, and by the bank selection logic to select one of eight banks. The data complement is designed to demonstrate the ability of the memory to accept and retain alternate "ones" along any plated wire. The disturb test exercises the memory by alternately reading and writing. The test also attempts to disturb the data stored in one bit location by writing data of the opposite polarity on either

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42 side of this location along the plated wire.

Through use of the teleprinter a hard copy of the test results is made available to the operator. In the case of a fault in the memory, the printout will indicate the faulty subassembly.

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4.21 Thermal Protection System (TPS)

The orbiter thermal protection and control system consists of two elements. One, the thermal protection system (TPS), is external to the structural shell of the vehicle. It maintains the airframe outer skin within acceptable temperature limits during the vehicle mission. Where internal vehicle special compartments require additional thermal control, the external TPS is augmented by a second element; the internal thermal control system (TCS). The vehicle thermal system also includes the ECLSS, the purge and vent subsystem, and other subsystems. See Figure 4.21-1.

The baseline TPS consists of: (1) ceramic reusable surface insulation (CRSI) (ceramic panels with an external waterproof coating on a strain-isolation foam pad) directly bonded to the airframe in areas exposed to surface temperature between 650°F and 2500°F; (2) elastomeric reusable surface insulation (ERSI) directly bonded to the airframe in areas exposed to temperatures below 650°F, and (3) reinforced carbon-carbon (RCC) material in the wing leading edge and body nose cap in areas exposed to temperatures above 2500°F.

4.21.1 Ceramic RSI

The ceramic insulation material basically consists of mullite and silica.

- Mullite panels - A low-density insulative composite material formed by coating a matrix of mullite fibers rigidized with an aluminum-boria silica refractory glass binder. The panel

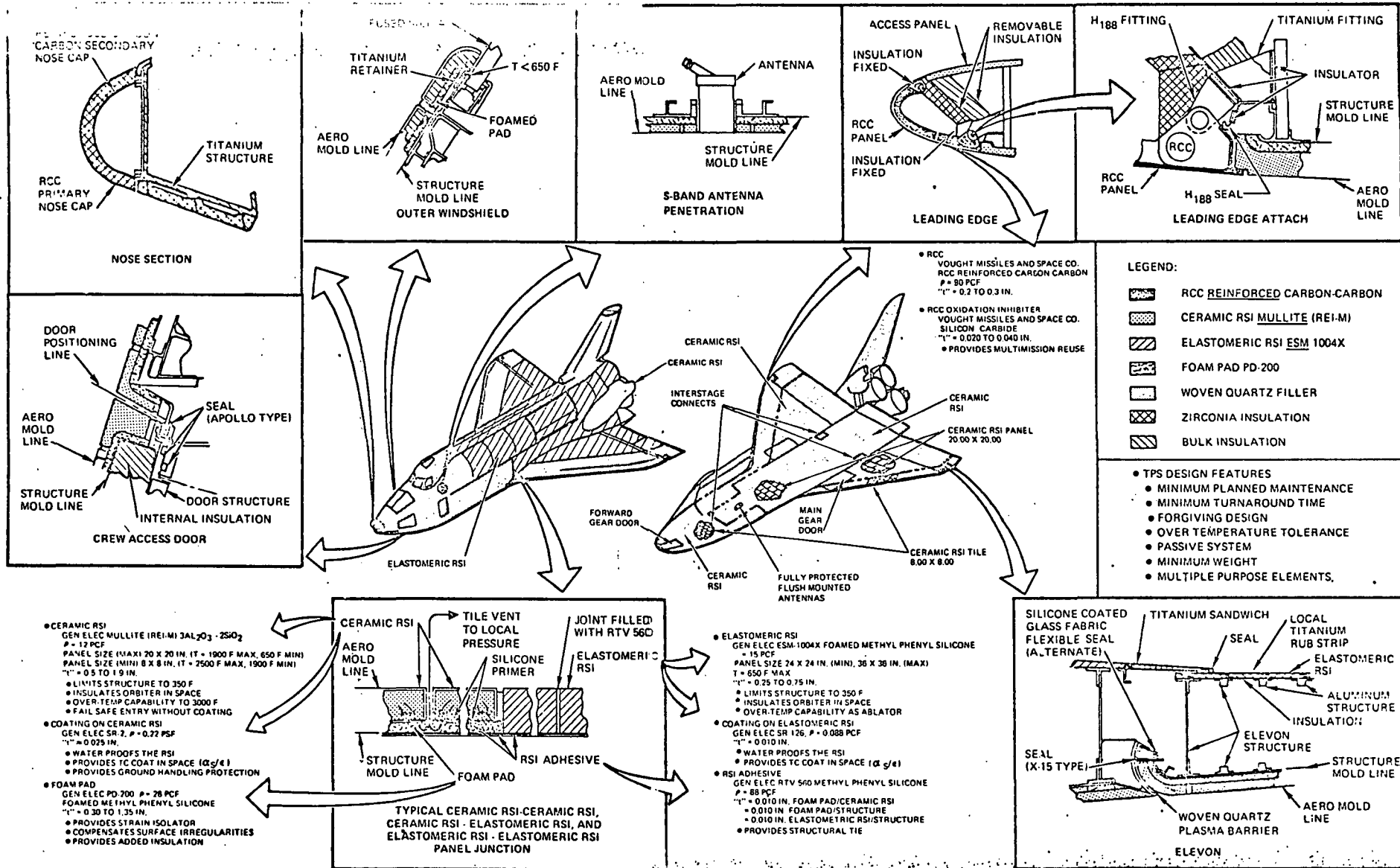


Figure 4.21-1 THERMAL PROTECTION SYSTEM (TPS)

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and pad dimensions are determined by the thermal/structural analyses.

- PD-200 pad - A chemically foamed methylphenyl silicone elastomeric material. This pad provides strain isolation of the CRSI from the aluminum structure and accommodates local surface irregularities. Its outer surface design temperature is 650°F, determined by the allowable bond temperature. The inner surface design temperature is 350°F. This temperature was selected to yield the lowest TPS and aluminum primary structural weight. Analyses indicate that the bottom and chine pad thickness ablative characteristics provide a ceramic panel loss fail safe entry.
- SR-2 coating - A waterproof ceramic coating fired at 2500°F on the top and sides of the panel. This coating is chemically compatible with and similar in expansion coefficient to the mullite insulation. The coating provides the necessary thermal control optical characteristics, rain erosion protection, and abrasion resistance for ground handling and atmospheric flight.
- RTV-560 adhesive - A silicone elastomer room-temperature-cured adhesive system used for both panel and pad bonding.

Panel-to-panel gaps (0.12 to 0.25 inch) are sized to avoid CRSI panel compressive loads at maximum expansion during entry. The gaps are partially filled with a low-density-quartz expandable gasket to thermally protect the substructure at the base of the joint.

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A panel self-venting system is provided which allows venting to the boundary layer pressure through the panel gaps. It consists of a local interruption in the panel to PD-200 bond line (adjacent to the lower outer edge.) A silicone primer, applied to the lower panel surface, provides a water barrier while allowing venting of internal gases.

Two CRSI test prototypes, mounted on simulated air-frame structure and configured to two critical areas of the baseline system, have been successfully tested to withstand 100 orbiter thermal environment cycles. During the test series the prototypes were also subjected to a dynamic/ acoustic energy spectrum of 163 db for the equivalent of 25 missions.

4.21.2 Elastomeric RSI

ERSI (ESM1004X) is used as the primary TPS on the orbiter upper surfaces where lower temperatures (< 650°F) are experienced. Using an elastomer instead of a ceramic results in a TPS weight reduction of 3500 pounds. It is a flexible, open-cell structure material possessing good low-temperature flexural properties, and is attached to the airframe in coated sheets with RTV-560 bond. The ESM1004X is coated with an elastomeric silicone resin (for waterproofing) pigmented with titanium dioxide and carbon black (for thermal control). It is an impact-resistant, easily repairable material which minimizes the susceptibility to handling damage.

The ESM1004X is similar to the material used on Minuteman reentry vehicle. Its thermal stability for 100 missions at 650°F has been demonstrated by tests. No difficulty is anticipated in extending its capacity to 500 missions. Excellent coating stability has been demonstrated

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to peak temperatures of 750°F in a vacuum maintained below 500 microns.

4.21.3 Reinforced Carbon-Carbon (RCC)

Reinforced carbon-carbon (RCC) materials are used for wing leading edge and body nose cap applications. The RCC leading edge elements are approximately 30 inches long, with the radii variations illustrated. Adjacent elements are downstream-lapped for spanwise expansion capability and utilize common attachment points to the prime structure. The joints are designed for individual leading edge element removal for maintainability. Cross-radiation effects are used to reduce maximum temperature and associated thermal stress, wherever possible. High-temperature bulk insulation backs up the RCC material to protect the structure. A silicone carbide oxidation inhibitor covers 100 percent of the RCC surface. The RCC vehicle body nose cap is similar to the leading edge in material details, construction, insulation, and attachment. The RCC material (and oxidation inhibitor) has been tested for 100 thermal cycles.

4.21.4 Special TPS Areas

4.21.4.1 TPS Outer Window

The TPS window employs a pane of fused silica (CGW 7940) to act as a heat shield. The windows, nominally 30 inches wide and 30 inches high, are subjected to a maximum temperature of 1200°F. They are sealed with a wire-mesh core jacketed with a woven ceramic cloth to prevent plasma impingement on internal structure. The outer window is part of a three-pane redundant system where the middle crew cabin window pane (fused silica for thermal protection) is also sealed to contain cabin pressure. The inner crew cabin pane is the primary

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pressure-containing window.

4.21.4.2 Seals

State-of-the-art Apollo CSM seal materials are generally utilized for doors and hatches. The elevon requires the use of high-temperature metals in the seal contact area to ensure adequate abrasion resistance. The upper seal panel is titanium with a metallic mesh seal similar to the seals used on the X-15 aircraft. It consists of an Inconel 602 mesh encased in an Inconel foil sleeve. This concept was proven by test to be reusable for 100 missions at 1200 °F during Phase B development testing. There are no proven fully reusable seal concepts for 1800°F environments in the lower elevon seal area. The current approach is to use a woven quartz plasma shield upstream to protect the metallic mesh seal inside the cavity by reducing the seal temperature. An alternate internal flexible longitudinal total pressure may be used to preclude outer seal leakage.

4.21.5 Rationale

Not Required.

4.21.6 Reference

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4.22 Thermal Control System (TCS)

The TCS basically is passive and integrally designed with the TPS. It consists essentially of insulation (TG 15000) heat sinks and optical coatings, with local active elements as required to maintain vehicle compartments within allowable temperature limits. Where individual components require closer control (heaters, cold plates, etc.), details are given in the applicable system description. FIGURE 4.18-1 shows the salient features of the TCS which is similar to that used on the Apollo CSM. The various subsystem components have been grouped essentially in the cabin area and the aft equipment bay with the required insulation located along the basic structure. This arrangement maximizes energy exchange among the subsystem components and facilitates equipment maintainability. Maximum utilization of existing heat sources and sinks to minimize make-up heater requirements and to achieve a flexible TCS design.

Thermal conditioning is most critical for the vehicle in high inclination orbits where the vehicle is placed in an adverse attitude that is maintained for a long period. This creates cold soak and hot soak conditions that may require special operation on the part of the crew.

The cold soak condition results in temperatures that may go below the "glass-transition" temperature (-170°F) of the foamed pad and room-temperature-vulcanized (RTV) bond, thus causing a ductility loss and sensitivity to thermal and load deformation. There are two aspects of cold soak, both concerned with maintaining ceramic RSI attachment integrity. These occur during (a) on-orbit periods under no loads relating to a "no mission interrupt" for thermal conditioning design approach and (b) entry heating with initial low RSI bondline temperatures

relating to a "no attitude constraint" for thermal conditioning design approach.

Hot soak is a related preentry thermal conditioning aspect. Internal subsystems that are sensitive to the hot-soak orbital condition are currently located in the vehicle fuselage, where temperatures are primarily influenced by the elastomeric RSI thermal control coating properties. As discussed, thermal coatings for the elastomeric RSI which exhibit an $\alpha_s/\epsilon_s = 0.4$ are already developed.

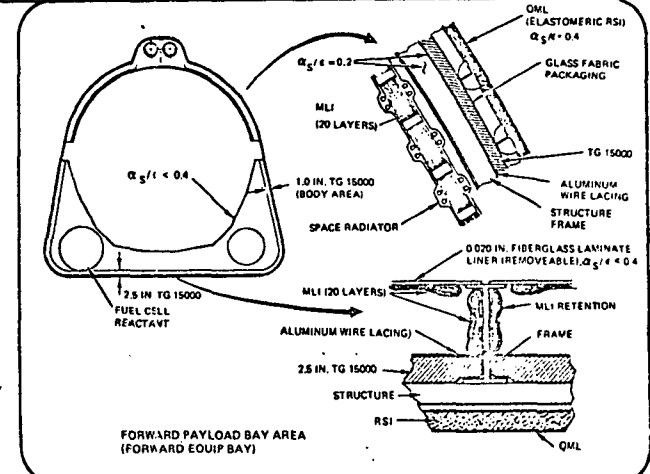
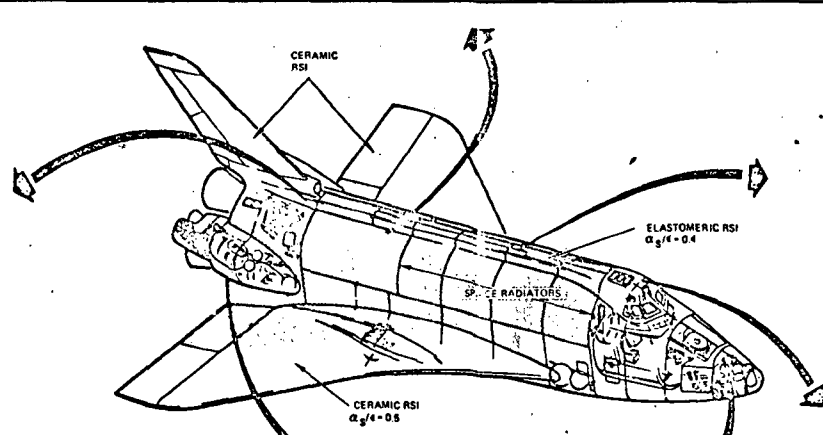
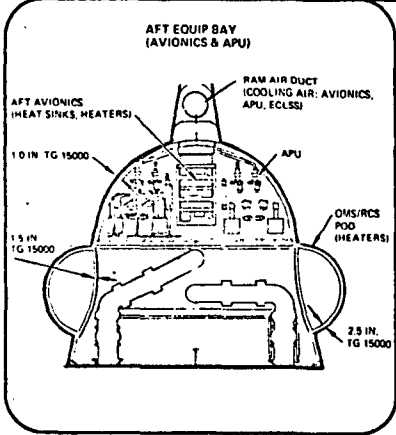
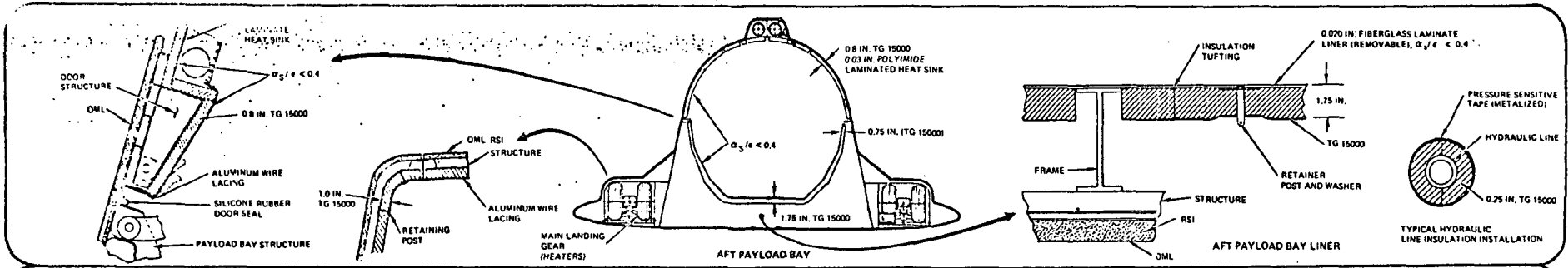
4.22.1 Rationale

Not required.

4.22.2 Reference

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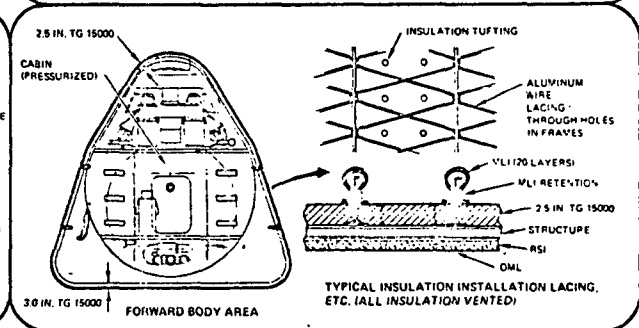
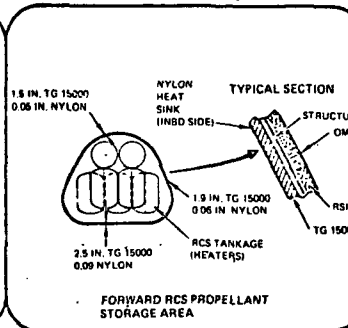
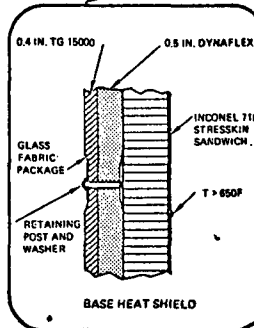
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- MAJOR TCS MATERIALS**
- TG 15000 / BULK INSULATION PACKAGED IN GLASS FABRIC - USED WHERE MAXIMUM TEMPERATURE IS LESS THAN 650 F. PROTECTS SUBSYSTEMS FROM ATMOSPHERIC AND SPACE ENVIRONMENTS
 - DYNAFLEX (PACKAGED BULK INSULATION) - USED WHERE TEMPERATURE EXCEEDS 650 F
 - MULTILAYER INSULATION (MLI) - MINIMIZES HEAT GAINS AND LOSSES FOR SPACE ENVIRONMENT (METALLIZED KAPTON)
 - REUSABLE SURFACE INSULATION (RSI)
 - INSULATION HEAT SINKS IN NYLON AND POLYIMIDE - USED TO TAILOR BULK INSULATION THICKNESS
 - THERMAL CONTROL COATINGS - LOW α_p/ϵ COATINGS EMPLOYED ON EXPOSED VEHICLE SURFACES TO REDUCE MAXIMUM TEMPERATURE. BASELINE: $\alpha_p/\epsilon = 0.5$ ON CERAMIC RSI, $\alpha_p/\epsilon = 0.4$ ON ELASTOMERIC RSI, $\alpha_p/\epsilon < 0.4$ ON PAYLOAD BAY INTERIOR. HIGH ϵ COATINGS USED ON SUBSYSTEM COMPONENTS.

- THERMAL CONTROL SYSTEM ELEMENTS**
- INSULATION
 - HEAT SINKS
 - THERMAL CONTROL COATINGS
 - HEATERS
 - ISOLATORS

- THERMAL CONTROL SYSTEM DESIGN FEATURES**
- PASSIVE SYSTEM - HIGH RELIABILITY
 - MAXIMUM UTILIZATION OF EXISTING HEAT SOURCES AND SINKS
 - MATERIALS AND DESIGN CHOSEN FOR MINIMUM MAINTENANCE
 - PAYLOAD BAY MEETS RFP REQUIREMENTS
 - CABIN INSULATED FOR ENTRY (TWALL - 120 F MAX) AND SPACE (NO CONDENSATION)



4.22-1 THERMAL CONTROL SYSTEM (TCS)