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MCR-70-457 (Vol I)

FINAL REPORT

SPIN VECTOR CONTROL FOR A SPINNING SPACE STATION

VOLUME I: USER'S MANUAL

By:

- T. Hendricks
- W. Guderian
- G. Johnson
- G. Haynes

November 1970

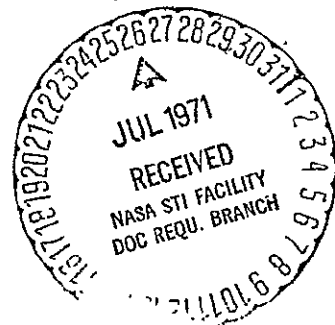
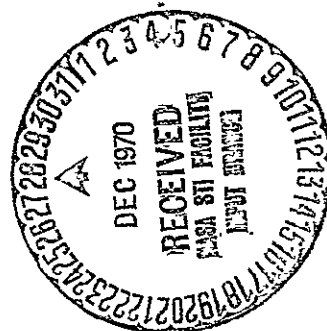
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 George C. Marshall Space Flight Center
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FOREWORD

This document represents Volume II of the final report on NASA Huntsville Contract entitled "Spin Vector Control for a Spinning Space Station". The report is prepared in two volumes:

Volume I - User's Manual

Volume II - Analytical Manual

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FINAL REPORT

SPIN VECTOR CONTROL OF A ROTATING SPACE STATION

VOLUME I: USER'S MANUAL

By: T. Hendricks, Walter Guderian, George Haynes, Gary Johnson

SUMMARY

This document presents the formulation, computational logic, input/output options, subroutine description and other pertinent information that should aid the user of the SPIN VECTOR CONTROL COMPUTER PROGRAM (MD246).

I. INTRODUCTION

This document is concerned with the design use and implementation of a digital computer program to facilitate the study of the dynamic behaviour and control of dual spin space vehicles. This volume is a companion to Volume II (analytical manual) of the final report under NASA-Huntsville Contract NAS8-25247.

The Spin Vector Control Program (MD246) is a Fortran Program that was written and checked out using the CDC 6400/6500 digital computer. To minimize possible system incompatibilities care has been exercised to assume that only the basic features of the system are used. Thus the program should be

operable on most digital machines with a FORTRAN 4 compiler.

The program is capable of solving the rotational dynamics of dual spin earth orbiting spacecraft. Several control options as well as spacecraft configurations are possible. Among the available control actuators are CMGs, reaction wheels, reaction jets and torque motors. This program is intended for but not restricted to attitude control studies of a rotating space station. The generalized spacecraft configuration along with geometrical definitions is shown in Figure 1. Figure 2 is a specific spacecraft configuration.

The remaining contents of this document discusses in varying degree of detail how to use the program. The first chapter Input Deck Construction describes those cards which are necessary when exercising the various program options. Chapter 2 Data Deck User's Guide presents a complete sequence and format description of all the data input cards. For a description and definition of the input variables refer to Appendix A.

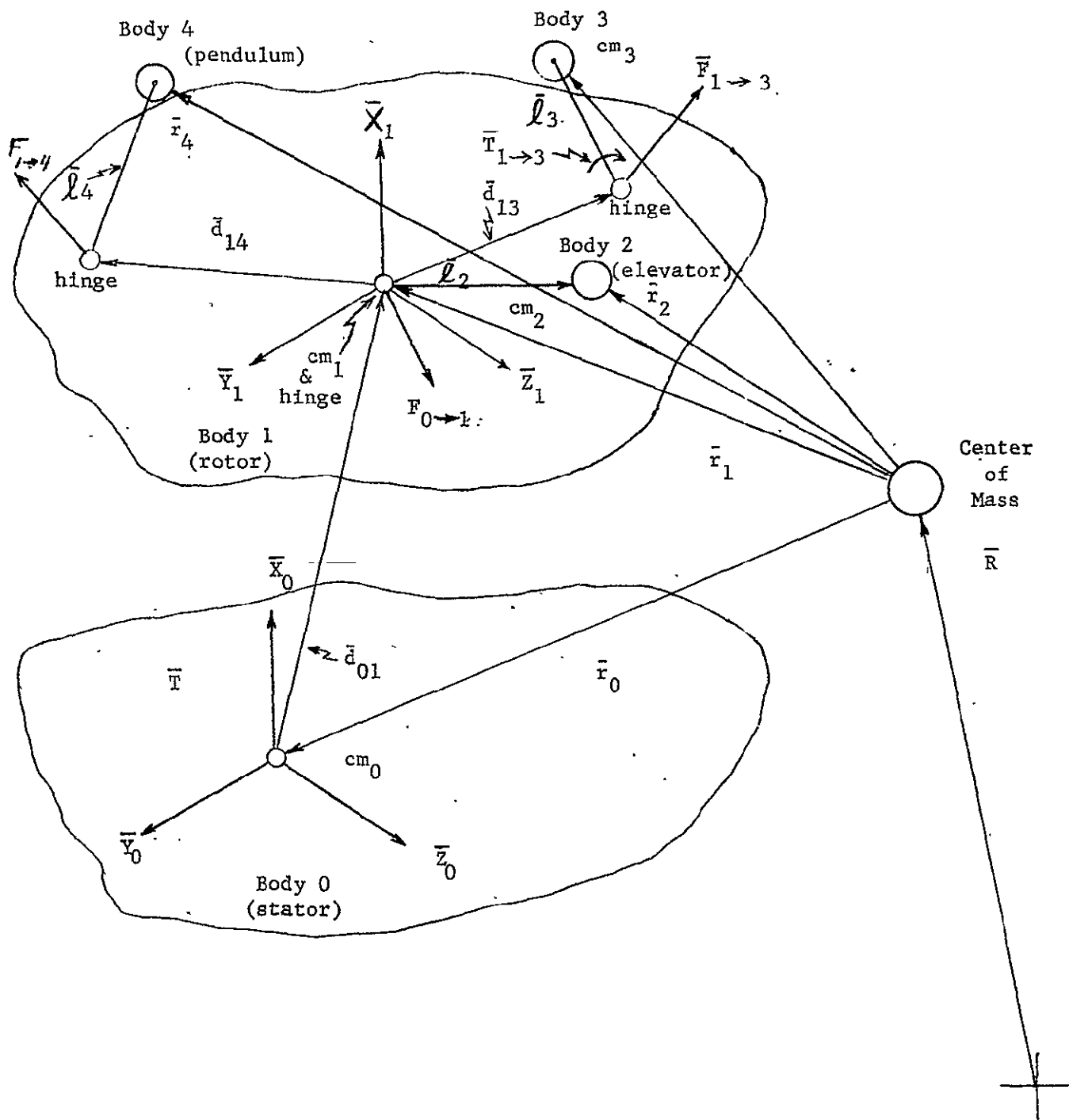


Figure 1 General Body Configuration

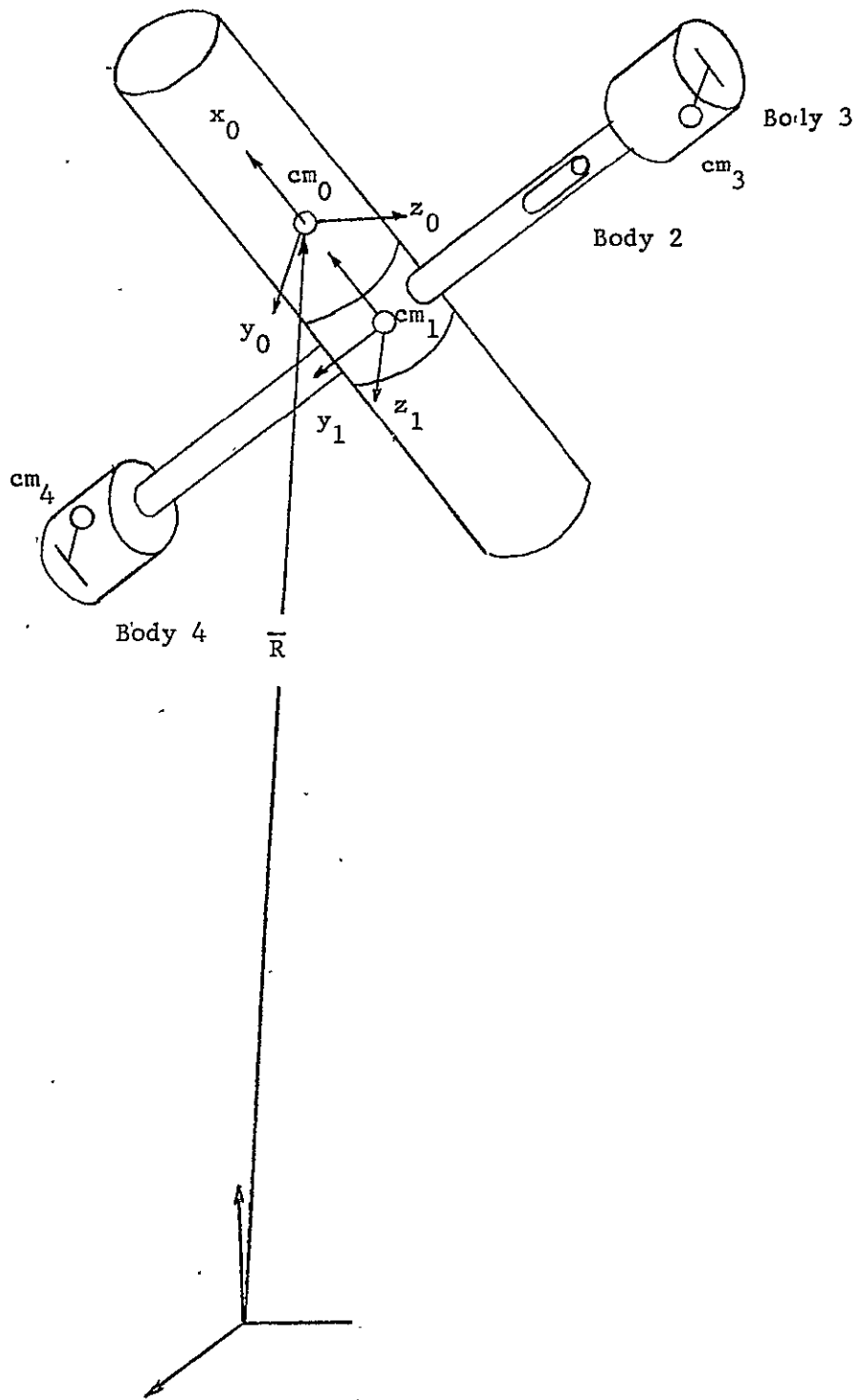


Figure 2 Spacecraft Body Configuration

INPUT DECK CONSTRUCTION

The basic data deck for operating the program with essentially no designated options is as follows.

| Card # | Variable |
|---------|--|
| 1 | NDECK = ___ |
| 2 | IPNDLM = 0 First card of run data |
| 3 | IPRINT = ___ |
| 4 | TSTART, TSTOP, DELTAT |
| 5 | Alt. |
| 6-14 | TIBOI(1,1) - TIBOI(3,3) |
| 15 | WO(1), WO(2), WO(3) |
| 16 | BOMASS |
| 17-25 | BODYOI(1,1) - BODYOI(3,3) |
| 26 | NUMCMG = 0 |
| 225 | IPROPF = 0 ___ |
| 242 | BIMASS |
| 243-251 | BODYII(1,1) - BODYII(3,3) |
| 252 | THETA1 |
| 253 | OMEGA1 |
| 254 | DO1(1), DO1(2), DO1(3) |
| 255 | IB2F = 0 |
| 282 | SP |
| 283 | NGAIN = 0 |
| 294 | IGRAVF = 0 |
| 295 | IDOCK = 0 |

Note that the above is also a list of the cards that must always be present.

Some examples of data deck arrangements for various options will be given. All data decks consist of the basic data deck with changes indicated.

1. Pendulum

Card #2 IPNDLM = 1

Before card #282 add cards #268 through #281, the pendulum parameter and initial value data.

2. Two single DOF CMGs

Card #26 NUMCMG = 2

After card #26 add -

Card #27 IDOF(1) = 1

#28 - HW(1)

#29 - #37 AOCJ(1,1,1) - AOCJ(1,3,3)

#38 - #42 AII(1,1,1) - AII(1,3,3)

#47 - THATA(1)

#48 - THATAD(1)

#60 - IDOF(2) = 1

#61 - HW(2)

#62 - #70 AOCJ(2,1,1) - AOCJ(2,3,3)

#71 - #79 AII(2,1,1) - AII(2,3,3)

#80 - THATA(2)

#81 - THATAD(2)

Card #283 NGAIN = 5

After card #283 add cards #284 - #288

(Cards #287 is control gain for CMG #1 and
card #288 is control gain for CMG #2 in the
present subroutines)

3. Propulsion on Body 0 (no attitude control)

Card #225 IPROPF = 1

After card #225 add -

Card #226 IATTIF = 0

Card #230 AOJ(1) = (non-zero) CGAINO(1)

Card #231 AOJ(2) = (non-zero) CGAINO(2)

Card #232 AOJ(3) = (non-zero) CGAINO(3)

After card #259, if present, otherwise after card

#255 add -

Card #260 ALJ(1) = (non-zero) CGAIN1(1) = 0

Card #261 ALJ(2) = (non-zero) CGAIN(2) = 0

4. Movable Mass

Card #255 IB2F = 1

After card #255 add cards #256 - #259 per-
taining to movable mass

5. Attitude Control with Propulsion on Body 1

Card #225 IPROPF = 1

After card #225 add -

Card #226 IATT1F = 1

Card #227 CA(1), CA(2), CA(3)

Card #230 AOJ(1) = (non-zero) CGAIN(1) = 0

Card #231 AOJ(2) = (non-zero) CGAIN(2) = 0

Card #232 AOJ(3) = (non-zero) CGAIN(3) = 0

After card #259 if present, otherwise after card

#255 add -

Card #260 ALJ(1) = (non-zero) CGAIN1(1)

Card #261 ALJ(2) = (non-zero) CGAIN1(2)

6. Gravity Gradient

Card #294 IGRAVF = 1

7. Docking

Card #295 IDOCK = 1

After card #295 add cards #296 - #307 docking
quantities.

DATA DECK USER'S GUIDE

CARD: 5

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: ALT

FORMAT: \pm . $E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 4

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLES: TSTART TSTOP DELTAT

FORMAT: \pm . \pm . . \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 .15 16 17 18 19 20 21 22 23 24 25 -28 29 30 31 32 33 34 35 36 37 38

CARD: 3

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IPRINT

FORMAT:

COLUMN: 2 3

CARD: 2

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IPNDLM

FORMAT:

COLUMN: 3

CARD: 1

INSTRUCTION: THIS CARD GOES IN FRONT OF DATA DECK 1 ONLY.

VARIABLE: NDECK

FORMAT:

COLUMN: 2 3

CARD: 14
VARIABLE: TIBOI (3,3)

CARD: 13
VARIABLE: TIBOI (3,2)

CARD: 12
VARIABLE: TIBOI (3,1)

CARD: 11
VARIABLE: TIBOI (2,3)

CARD: 10
VARIABLE: TIBOI (2,2)

CARD: 9
VARIABLE: TIBOI (2,1)

CARD: 8
VARIABLE: TIBOI (1,3)

CARD: 7
VARIABLE: TIBOI (1,2)

CARD: 6
INSTRUCTION: THE NEXT 9 CARDS MUST ALWAYS BE PRESENT.
VARIABLE: TIBOI (1,1)
FORMAT: $\frac{+}{\quad}$.
COLUMN: 2 3 4 5 6 7 8 9 10 11 12.

CARD: 16
INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.
VARIABLE: BOMASS
FORMAT: $\underline{+}$. $\underline{E+}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 15
INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.
VARIABLES: WO(1) WO(2) WO(3)
FORMAT: $\underline{+}$. $\underline{+}$. $\underline{+}$.
2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 25
VARIABLE: BODYOI (3,3)

CARD: 24
VARIABLE: BODYOI (3,2)

CARD: 23
VARIABLE: BODYOI (3,1)

CARD: 22
VARIABLE: BODYOI (2,3)

CARD: 21
VARIABLE: BODYOI (2,2)

CARD: 20
VARIABLE: BODYOI (2,1)

CARD: 19
VARIABLE: BODYOI (1,3)

CARD: 18
VARIABLE: BODYOI (1,2)

CARD: 17
INSTRUCTION: THE NEXT 9 CARDS MUST ALWAYS BE PRESENT.
VARIABLE: BODYOI (1,1)
FORMAT: $\pm . E\pm$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 28

INSTRUCTION: IF NUMCMG = 0, IGNORE THIS CARD.

VARIABLE: HW (1)

FORMAT: \pm . E \pm

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 27

INSTRUCTION: IF NUMCMG = 0, IGNORE THIS CARD.

VARIABLE: IDOF (1)

FORMAT:

COLUMN: 3

CARD: 26

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: NUMCMG

FORMAT:

COLUMN: 3

CARD: 37
VARIABLE: AOCJ (1,3,3)

CARD: 36
VARIABLE: AOCJ (1,3,2)

CARD: 35
VARIABLE: AOCJ (1,3,1)

CARD: 34
VARIABLE: AOCJ (1,2,3)

CARD: 33
VARIABLE: AOCJ (1,2,2)

CARD: 32
VARIABLE: AOCJ (1,2,1)

CARD: 31
VARIABLE: AOCJ (1,1,3)

CARD: 30
VARIABLE: AOCJ (1,1,2)

CARD: 29
INSTRUCTION: IF NUMCMG = 0, IGNORE THE NEXT 9 CARDS.
VARIABLE: AOCJ (1,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 46
VARIABLE: AII (1,3,3)

CARD: 45
VARIABLE: AII (1,3,2)

CARD: 44
VARIABLE: AII (1,3,1)

CARD: 43
VARIABLE: AII (1,2,3)

CARD: 42
VARIABLE: AII (1,2,2)

CARD: 41
VARIABLE: AII (1,2,1)

CARD: 40
VARIABLE: AII (1,1,3)

CARD: 39
VARIABLE: AII (1,1,2)

CARD: 38
INSTRUCTION: IF NUMCMG OR IDOF (1) = 0, IGNORE THE NEXT 9 CARDS.
VARIABLE: AII (1,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 48
VARIABLE: THATAD (1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 47
INSTRUCTION: IF NUMCMG OR IDOF (1) = 0, IGNORE THE NEXT 2 CARDS.
VARIABLE: THATA (1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 57
VARIABLE: AIO (1,3,3)

CARD: 56
VARIABLE: AIO (1,3,2)

CARD: 55
VARIABLE: AIO (1,3,1)

CARD: 54
VARIABLE: AIO (1,2,3)

CARD: 53
VARIABLE: AIO (1,2,2)

CARD: 52
VARIABLE: AIO (1,2,1)

CARD: 51
VARIABLE: AIO (1,1,3)

CARD: 50
VARIABLE: AIO (1,1,2)

CARD: 49
INSTRUCTION: IF NUMCMG = 0, OR IDOF (1) = 0, OR IDOF (1) = 1,
IGNORE THE NEXT 9 CARDS.
VARIABLE: AIO (1,1,1)
FORMAT: + .
COLUMN: 2,3,4,5,6,7,8,9,10,11,12,

CARD: 61

INSTRUCTION: IF NUMCMG < 2, IGNORE THIS CARD.

VARIABLE: HW (2)

FORMAT: $\frac{+}{.}$ E $\frac{+}{.}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 60

INSTRUCTION: IF NUMCMG < 2, IGNORE THIS CARD.

VARIABLE: IDOF (2)

FORMAT:

COLUMN: 3

CARD: 59

VARIABLE: FEED (-1)

FORMAT: $\frac{+}{.}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 58

INSTRUCTION: IF NUMCMG = 0, OR IDOF (1) = 0, OR IDOF (1) = 1,
IGNORE THE NEXT 2 CARDS.

VARIABLE: FEE (1)

FORMAT: $\frac{+}{.}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 70
VARIABLE: AOCJ (2,3,3)

CARD: 69
VARIABLE: AOCJ (2,3,2)

CARD: 68
VARIABLE: AOCJ (2,3,1)

CARD: 67
VARIABLE: AOCJ (2,2,3)

CARD: 66
VARIABLE: AOCJ (2,2,2)

CARD: 65
VARIABLE: AOCJ (2,2,1)

CARD: 64
VARIABLE: AOCJ (2,1,3)

CARD: 63
VARIABLE: AOCJ (2,1,2)

CARD: 62
INSTRUCTION: IF NUMCMG < 2, IGNORE THE NEXT 9 CARDS.
VARIABLE: AOCJ (2,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 79
VARIABLE: AII (2,3,3)

CARD: 78
VARIABLE: AII (2,3,2)

CARD: 77
VARIABLE: AII (2,3,1)

CARD: 76
VARIABLE: AII (2,2,3)

CARD: 75
VARIABLE: AII (2,2,2)

CARD: 74
VARIABLE: AII (2,2,1)

CARD: 73
VARIABLE: AII (2,1,3)

CARD: 72
VARIABLE: AII (2,1,2)

CARD: 71
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0,
 IGNORE THE NEXT 9 CARDS.
VARIABLE: AII (2,1,1)
FORMAT: + .
COLUMN: 1 2 4 5 6 7 8 9 10 11 12

CARD: 81
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, IGNORE THIS CARD.
VARIABLE: THATAD (2)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 80
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, IGNORE THIS CARD.
VARIABLE: THATA (2)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 90
VARIABLE: AIO (2,3,3)

CARD: 89
VARIABLE: AIO (2,3,2)

CARD: 88
VARIABLE: AIO (2,3,1)

CARD: 87
VARIABLE: AIO (2,2,3)

CARD: 86
VARIABLE: AIO (2,2,2)

CARD: 85
VARIABLE: AIO (2,2,1)

CARD: 84
VARIABLE: AIO (2,1,3)

CARD: 83
VARIABLE: AIO (2,1,2)

CARD: 82
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, OR IDOF (2) = 1,
IGNORE THE NEXT 9 CARDS.
VARIABLE: AIO (2,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 8 7 8 9 10 11 12

CARD: 94
INSTRUCTION: IF NUMCMG < 3, IGNORE THIS CARD.
VARIABLE: HW (3)
FORMAT: $\frac{+}{.}$ E+
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 93
INSTRUCTION: IF NUMCMG < 3, IGNORE THIS CARD.
VARIABLE: IDOF (3)
FORMAT:
COLUMN: 3

CARD: 92
VARIABLE: FEED (2)

CARD: 91
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, OR IDOF (2) = 1,
IGNORE THE NEXT 2 CARDS.
VARIABLE: FEE (2)
FORMAT: $\frac{+}{.}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 103
VARIABLE: AOCJ (3,3,3)

CARD: 102
VARIABLE: AOCJ (3,3,2)

CARD: 101
VARIABLE: AOCJ (3,3,1)

CARD: 100
VARIABLE: AOCJ (3,2,3)

CARD: 99
VARIABLE: AOCJ (3,2,2)

CARD: 98
VARIABLE: AOCJ (3,2,1)

CARD: 97
VARIABLE: AOCJ (3,1,3)

CARD: 96
VARIABLE: AOCJ (3,1,2)

CARD: 95
INSTRUCTION: IF NUMCMG < 3, IGNORE THE NEXT 9 CARDS.
VARIABLE: AOCJ (3,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 112
VARIABLE: AII (3,3,3)

CARD: 111
VARIABLE: AII (3,3,2)

CARD: 110
VARIABLE: AII (3,3,1)

CARD: 109
VARIABLE: AII (3,2,3)

CARD: 108
VARIABLE: AII (3,2,2)

CARD: 107
VARIABLE: AII (3,2,1)

CARD: 106
VARIABLE: AII (3,1,3)

CARD: 105
VARIABLE: AII (3,1,2)

CARD: 104
INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0,
 IGNORE THE NEXT 9 CARDS.
VARIABLE: AII (3,1,1)
FORMAT: + .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 114

INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0, IGNORE THIS CARD.

VARIABLE: THATAD (3)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 113

INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0, IGNORE THIS CARD.

VARIABLE: THATA (3)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 123
VARIABLE: AIO (3,3,3)

CARD: 122
VARIABLE: AIO (3,3,2)

CARD: 121
VARIABLE: AIO (3,3,1)

CARD: 120
VARIABLE: AIO (3,2,3)

CARD: 119
VARIABLE: AIO (3,2,2)

CARD: 118
VARIABLE: AIO (3,2,1)

CARD: 117
VARIABLE: AIO (3,1,3)

CARD: 116
VARIABLE: AIO (3,1,2)

CARD: 115
INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0, OR IDOF (3) = 1,
IGNORE THE NEXT 9 CARDS.
VARIABLE: AIO (3,1,1)
FORMAT: ± .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 127
INSTRUCTION: IF NUMCMG < 4, IGNORE THIS CARD.
VARIABLE: HW (4)
FORMAT: $\pm . E\pm$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 126
INSTRUCTION: IF NUMCMG < 4, IGNORE THIS CARD.
VARIABLE: IDOF (4)
FORMAT:
COLUMN: 3

CARD: 125
VARIABLE: FEED (3)

CARD: 124
INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0, OR IDOF (3) = 1,
IGNORE THE NEXT 2 CARDS.
VARIABLE: FEE (3)
FORMAT: $\pm .$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 136
VARIABLE: AOCJ (4,3,3)

CARD: 135
VARIABLE: AOCJ (4,3,2)

CARD: 134
VARIABLE: AOCJ (4,3,1)

CARD: 133
VARIABLE: AOCJ (4,2,3)

CARD: 132
VARIABLE: AOCJ (4,2,2)

CARD: 131
VARIABLE: AOCJ (4,2,1)

CARD: 130
VARIABLE: AOCJ (4,1,3)

CARD: 129
VARIABLE: AOCJ (4,1,2)

CARD: 128
INSTRUCTION: IF NUMCMG < 4, IGNORE THE NEXT 9 CARDS.
VARIABLE: AOCJ (4,1,1)
FORMAT: $\frac{+}{.}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 145
VARIABLE: AII (4,3,3)

CARD: 144
VARIABLE: AII (4,3,2)

CARD: 143
VARIABLE: AII (4,3,1)

CARD: 142
VARIABLE: AII (4,2,3)

CARD: 141
VARIABLE: AII (4,2,2)

CARD: 140
VARIABLE: AII (4,2,1)

CARD: 139
VARIABLE: AII (4,1,3)

CARD: 138
VARIABLE: AII (4,1,2)

CARD: 137
INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0,
 IGNORE THE NEXT 9 CARDS.
VARIABLE: AII (4,1,1)
FORMAT: + .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 147

INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, IGNORE THIS CARD.

VARIABLE: THATA (4)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 146

INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, IGNORE THIS CARD.

VARIABLE: THATA (4)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 156
VARIABLE: AIO (4,3,3)

CARD: 155
VARIABLE: AIO (4,3,2)

CARD: 154
VARIABLE: AIO (4,3,1)

CARD: 153
VARIABLE: AIO (4,2,3)

CARD: 152
VARIABLE: AIO (4,2,2)

CARD: 151
VARIABLE: AIO (4,2,1)

CARD: 150
VARIABLE: AIO (4,1,3)

CARD: 149
VARIABLE: AIO (4,1,2)

CARD: 148
INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, OR IDOF (4) = 1,
IGNORE THE NEXT 9 CARDS.

VARIABLE: AIO (4,1,1)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 160
INSTRUCTION: IF NUMCMG < 5, IGNORE THIS CARD.
VARIABLE: HW (5)
FORMAT: $\frac{+}{.}$ E+
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 159
INSTRUCTION: IF NUMCMG < 5, IGNORE THIS CARD.
VARIABLE: IDOF (5)
FORMAT:
COLUMN: 3

CARD: 158
VARIABLE: FEED (4)

CARD: 157
INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, OR IDOF (4) = 1,
IGNORE THE NEXT 2 CARDS.
VARIABLE: FEE (4)
FORMAT: $\frac{+}{.}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 169
VARIABLE: AOCJ (5,3,3)

CARD: 168
VARIABLE: AOCJ (5,3,2)

CARD: 167
VARIABLE: AOCJ (5,3,1)

CARD: 166
VARIABLE: AOCJ (5,2,3)

CARD: 165
VARIABLE: AOCJ (5,2,2)

CARD: 164
VARIABLE: AOCJ (5,2,1)

CARD: 163
VARIABLE: AOCJ (5,1,3)

CARD: 162
VARIABLE: AOCJ (5,1,2)

CARD: 161
INSTRUCTION: IF NUMCMG < 5, IGNORE THE NEXT 9 CARDS.
VARIABLE: AOCJ (5,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 178
VARIABLE: AII (5,3,3)

CARD: 177
VARIABLE: AII (5,3,2)

CARD: 176
VARIABLE: AII (5,3,1)

CARD: 175
VARIABLE: AII (5,2,3)

CARD: 174
VARIABLE: AII (5,2,2)

CARD: 173
VARIABLE: AII (5,2,1)

CARD: 172
VARIABLE: AII (5,1,3)

CARD: 171
VARIABLE: AII (5,1,2)

CARD: 170
INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0,
 IGNORE THE NEXT 9 CARDS.
VARIABLE: AII (5,1,1)
FORMAT: + .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 180

INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, IGNORE THIS CARD.

VARIABLE: THATAD (5)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 179

INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, IGNORE THIS CARD.

VARIABLE: THATA (5)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 189
VARIABLE: AIO (5,3,3)

CARD: 188
VARIABLE: AIO (5,3,2)

CARD: 187
VARIABLE: AIO (5,3,1)

CARD: 186
VARIABLE: AIO (5,2,3)

CARD: 185
VARIABLE: AIO (5,2,2)

CARD: 184
VARIABLE: AIO (5,2,1)

CARD: 183
VARIABLE: AIO (5,1,3)

CARD: 182
VARIABLE: AIO (5,1,2)

CARD: 181
INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, OR IDOF (5) = 1,
IGNORE THE NEXT 9 CARDS.
VARIABLE: AIO (5,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 193
INSTRUCTION: IF NUMCMG < 6, IGNORE THIS CARD.
VARIABLE: HW (6)
FORMAT: \pm . E \pm
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 192
INSTRUCTION: IF NUMCMG < 6, IGNORE THIS CARD.
VARIABLE: IDOF (6)
FORMAT:
COLUMN: 3

CARD: 191
VARIABLE: FEED (5)

CARD: 190
INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, OR IDOF (5) = 1
IGNORE THE NEXT 2 CARDS.
VARIABLE: FEE (5)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 202
VARIABLE: AOCJ (6,3,3)

CARD: 201
VARIABLE: AOCJ (6,3,2)

CARD: 200
VARIABLE: AOCJ (6,3,1)

CARD: 199
VARIABLE: AOCJ (6,2,3)

CARD: 198
VARIABLE: AOCJ (6,2,2)

CARD: 197
VARIABLE: AOCJ (6,2,1)

CARD: 196
VARIABLE: AOCJ (6,1,3)

CARD: 195
VARIABLE: AOCJ (6,1,2)

CARD: 194
INSTRUCTION: IF NUMCMG < 6, IGNORE THE NEXT 9 CARDS.
VARIABLE: AOCJ (6,1,1)
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 211
VARIABLE: AII (6,3,3)

CARD: 210
VARIABLE: AII (6,3,2)

CARD: 209
VARIABLE: AII (6,3,1)

CARD: 208
VARIABLE: AII (6,2,3)

CARD: 207
VARIABLE: AII (6,2,2)

CARD: 206
VARIABLE: AII (6,2,1)

CARD: 205
VARIABLE: AII (6,1,3)

CARD: 204
VARIABLE: AII (6,1,2)

CARD: 203
INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0,
IGNORE THE NEXT 9 CARDS.

VARIABLE: AII (6,1,1)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 213

INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, IGNORE THIS CARD.

VARIABLE: THATAD (6)

FORMAT: + .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 212

INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, IGNORE THIS CARD.

VARIABLE: THATA (6)

FORMAT: + .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 222
VARIABLE: AIO (6,3,3)

CARD: 221
VARIABLE: AIO (6,3,2)

CARD: 220
VARIABLE: AIO (6,3,1)

CARD: 219
VARIABLE: AIO (6,2,3)

CARD: 218
VARIABLE: AIO (6,2,2)

CARD: 217
VARIABLE: AIO (6,2,1)

CARD: 216
VARIABLE: AIO (6,1,3)

CARD: 215
VARIABLE: AIO (6,1,2)

CARD: 214
INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, OR IDOF (6) = 1,
IGNORE THE NEXT 9 CARDS.

VARIABLE: AIO (6,1,1)

FORMAT: \pm .

COLUMN: $\frac{1}{2}$ 3 4 5 6 7 8 9 10 11 12

DUE TO MODIFICATIONS, THE NEXT DATA CARD HAS THE NUMBER 230.

CARD: 227

INSTRUCTION: IF IPROP_F OR LATTIF = 0, IGNORE THIS CARD.

VARIABLES: CA(1) CA(2) CA(3)

FORMAT: \pm . \pm . \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 226

INSTRUCTION: IF IPROP_F = 0, IGNORE THIS CARD.

VARIABLE: LATTIF

FORMAT:

COLUMN: 3

CARD: 225

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IPROP_F

FORMAT:

COLUMN: 3

CARD: 224

VARIABLE: FEED (6)

CARD: 223

INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, OR IDOF (6) = 1, IGNORE THE NEXT 2 CARDS.

VARIABLE: FEE (6)

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

DUE TO MODIFICATIONS, THE NEXT DATA CARD
HAS THE NUMBER 242.

CARD: 232
VARIABLES: AOJ (3) CGAINO (3)

CARD: 231
VARIABLES: AOJ (2) CGAINO (2)

CARD: 230
INSTRUCTION: IF IPROP = 0, IGNORE THE NEXT 3 CARDS.
VARIABLES: AOJ(1) CGAINO(1)
FORMAT: + . E+ + . E+
COLUMN: 2 3 4 5 6 7 8 9 10 11 12 1 15 17 18 19 20 21 22 23 24 25

CARD: 251
VARIABLE: BODYII (3,3)

CARD: 250
VARIABLE: BODYII (3,2)

CARD: 249
VARIABLE: BODYII (3,1)

CARD: 248
VARIABLE: BODYII (2,3)

CARD: 247
VARIABLE: BODYII (2,2)

CARD: 246
VARIABLE: BODYII (2,1)

CARD: 245
VARIABLE: BODYII (1,3)

CARD: 244
VARIABLE: BODYII (1,2)

CARD: 243
INSTRUCTION: THE NEXT 9 CARDS MUST ALWAYS BE PRESENT.
VARIABLE: BODYII (1,1)
FORMAT:- + . E+
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 255

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IB2F

FORMAT:

COLUMN: 3

CARD: 254

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLES: DO1(1) DO1(2) DO1(3)

FORMAT: \pm . \pm . \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 253

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: OMEGA1

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 252

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: THETA1

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 259
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.
 VARIABLES: S SDOT
 FORMAT: \pm . \pm .
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25

CARD: 258
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.
 VARIABLES: S2(1) S2(2) S2(3)
 FORMAT: \pm . \pm . \pm .
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 257
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.
 VARIABLES: D12(1) D12(2) D12(3)
 FORMAT: \pm . \pm . \pm .
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 256
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.
 VARIABLE: B2MASS
 FORMAT: \pm . E \pm
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

DUE TO MODIFICATIONS, THE NEXT DATA CARD
HAS THE NUMBER 268.

CARD: 261
VARIABLES: ALJ(2) CGAIN1(2)

CARD: 260
INSTRUCTION: IF IPROP = 0, IGNORE THE NEXT 2 CARDS.
VARIABLES: ALJ(1) CGAIN1(1)
FORMAT: $\pm . . E\pm$ $\pm . E\pm$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25

CARD: 271
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
 VARIABLES: D13(1) D13(2) D13(3)
 FORMAT: \pm . \pm . \pm .
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 270
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
 VARIABLE: B3MASS
 FORMAT: \pm . E \pm
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 269
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
 VARIABLE: CP2
 FORMAT: \pm . E \pm
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 268
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
 VARIABLE: CP1
 FORMAT: \pm . E \pm
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 279

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: PEND4L

FORMAT: \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 278

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLES: S4(1) S4(2) S4(3)

FORMAT: \pm . \pm . \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 277

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLES: D14(1) D14(2) D14(3)

FORMAT: \pm . \pm . \pm .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 276

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: B4MASS

FORMAT: \pm . E \pm

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 275
INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
VARIABLE: OMEGA3
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 274
INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
VARIABLE: THETA3
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 273
INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
VARIABLE: PEND3L
FORMAT: \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 272
INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
VARIABLES: S3(1) S3(2) S3(3)
FORMAT: \pm . \pm . \pm .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 283
INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.
VARIABLE: NGAIN
FORMAT:
COLUMN: 2 3

CARD: 282
INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.
VARIABLE: SP
FORMAT: $\frac{+}{\quad}$.
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 281
INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD
VARIABLE: OMEGA4
FORMAT: $\frac{+}{\quad}$.
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 280
INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.
VARIABLE: THETA4
FORMAT: $\frac{+}{\quad}$.
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 288

INSTRUCTION: IF NGAIN < 5, IGNORE THIS CARD.

VARIABLE: GAIN (5)

FORMAT: $\pm . E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 287

INSTRUCTION: IF NGAIN < 4, IGNORE THIS CARD.

VARIABLE: GAIN (4)

FORMAT: $\pm . E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 286

INSTRUCTION: IF NGAIN < 3, IGNORE THIS CARD.

VARIABLE: GAIN (3)

FORMAT: $\pm . E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 285

INSTRUCTION: IF NGAIN < 2, IGNORE THIS CARD.

VARIABLE: GAIN (2)

FORMAT: $\pm . E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 284

INSTRUCTION: IF NGAIN = 0, IGNORE THIS CARD.

VARIABLE: GAIN (1)

FORMAT: $\pm . E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 293
INSTRUCTION: IF NGAIN < 10, IGNORE THIS CARD.
VARIABLE: GAIN (10)
FORMAT: $\underline{+}$. $\underline{E+}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 292
INSTRUCTION: IF NGAIN < 9, IGNORE THIS CARD.
VARIABLE: GAIN (9)
FORMAT: $\underline{+}$. $\underline{E+}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 291
INSTRUCTION: IF NGAIN < 8, IGNORE THIS CARD.
VARIABLE: GAIN (8)
FORMAT: $\underline{+}$. $\underline{E+}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 290
INSTRUCTION: IF NGAIN < 7, IGNORE THIS CARD.
VARIABLE: GAIN (7)
FORMAT: $\underline{+}$. $\underline{E+}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 289
INSTRUCTION: IF NGAIN < 6, IGNORE THIS CARD.
VARIABLE: GAIN (6)
FORMAT: $\underline{+}$. $\underline{E+}$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 297

INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.

VARIABLE: BDMASS

FORMAT: $\frac{+}{.}$ E $\frac{+}{.}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 296

INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.

VARIABLE: DTIME

FORMAT: $\frac{+}{.}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 295

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IDOCK

FORMAT:

COLUMN: 3

CARD: 294

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IGRAVF

FORMAT:

COLUMN: 3:

CARD: 306
VARIABLE: BODYDI (3,3)

CARD: 305
VARIABLE: BODYDI (3,2)

CARD: 304
VARIABLE: BODYDI (3,1)

CARD: 303
VARIABLE: BODYDI (2,3)

CARD: 302
VARIABLE: BODYDI (2,2)

CARD: 301
VARIABLE: BODYDI (2,1)

CARD: 300
VARIABLE: BODYDI (1,3)

CARD: 299
VARIABLE: BODYDI (1,2)

CARD: 298
INSTRUCTION: IF IDOCK = 0, IGNORE THE NEXT 9 CARDS.
VARIABLE: BODYDI (1,1)
FORMAT: \pm . $E\pm$
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 308

INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.

VARIABLES: DD01(1) DD01(2) DD01(3)

FORMAT: + . + . + .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 307

INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.

VARIABLES: DTI(1) DTI(2) DTI(3)

FORMAT: + . + . + .
COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

APPENDIX A, DEFINITIONS AND REFERENCES FOR INPUT VARIABLES

This appendix is in two parts. The first part contains a list of all input variables in alphabetical order. The second part contains the input variables in categories and the input variables in each category are alphabetized.

[AII(J,M,N)]:

$$[AII(J,M,N)] = [II_J] = \begin{bmatrix} AII(J,1,1) & AII(J,1,2) & AII(J,1,3) \\ AII(J,2,1) & AII(J,2,2) & AII(J,2,3) \\ AII(J,3,1) & AII(J,3,2) & AII(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the inner gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are also constrained to be located at the center of mass on the stator, body 0. If the Jth CMG has one or two degrees of freedom, it will have an inner gimbal. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft²)

FORMAT: # 5006 = (1X, F11.5)

AIO(J,M,N):

$$[AIO(J,M,N)] = [IO_J] = \begin{bmatrix} AIO(J,1,1) & AIO(J,1,2) & AIO(J,1,3) \\ AIO(J,2,1) & AIO(J,2,2) & AIO(J,2,3) \\ AIO(J,3,1) & AIO(J,3,2) & AIO(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the outer gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are constrained to be located at the center of mass on the stator, body 0. The

Jth CMG will have an outer gimbal only if it has two degrees of freedom. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft²)

FORMAT: # 5006 = (1X, F11.5)

ALT:

ALT is altitude of the center of mass of the space station configuration measured from the surface of the earth. All orbits are constrained to be circular with no oblateness effects. Therefore, altitude is the only pertinent orbit parameter.

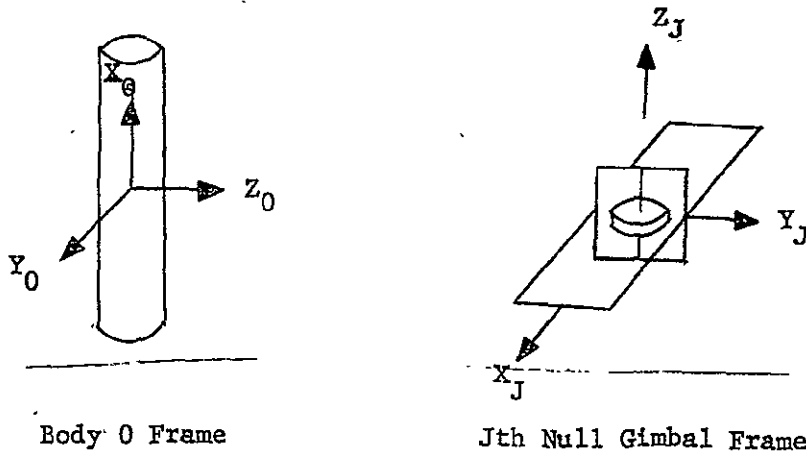
UNITS: (miles)

FORMAT: # 5004 = (1X, E11.4)

AOCJ(J,M,N):

$$[AOCJ(J,M,N)] = [O,C_J] = \begin{bmatrix} AOCJ(J,1,1) & AOCJ(J,1,2) & AOCJ(J,1,3) \\ AOCJ(J,2,1) & AOCJ(J,2,2) & AOCJ(J,2,3) \\ AOCJ(J,3,1) & AOCJ(J,3,2) & AOCJ(J,3,3) \end{bmatrix}$$

This array is the coordinate transformation matrix from the CMG null gimbal coordinate frame to the coordinate frame of body 0, the stator. (Refer to the coordinate transformation appendix.) For example, consider the two coordinate systems shown below:



For the above situation:

$$[AOCJ(J,M,N)] = \begin{bmatrix} 0. & 0. & 1. \\ 1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$

UNITS: (None)

FORMAT: # 5006 = (1X, F11.5)

AOJ(M):

AOJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 0.

AOJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 0.

AOJ(3) is the distance between the jets of the pure couple producing the torque around the Z axis of body 0.

Note: The variables CGAIN0(1), CGAIN0(2), and CGAIN0(3) are also read on the same data cards as AOJ(1), AOJ(2), and AOJ(3). Punch the values of AOJ(1), AOJ(2), and AOJ(3) in columns 2 through 12 of the data cards. Non-zero values should be read in for AOJ(M). Control on an axis can be disabled by reading zero for the CGAIN0.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

ALJ(M):

ALJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 1.

ALJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 1.

Note: The variables CGAIN1(1) and CGAIN1(2) are also read on the same data cards as ALJ(1) and ALJ(2). Punch the values of ALJ(1) and ALJ(2) in columns 2 through 12 of the data cards. Non-zero values should

be read in for ALJ(M). Control on an axis can be disabled by reading zero for the CGAIN1.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

BDMASS:

BDMASS is the sum of the mass of body 0, the stator, and the mass of the docking vehicle. The docking vehicle is constrained to dock on body 0, the stator. $BDMASS = m_D$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

BODYDI(M,N):

$$[BODYDI(M,N)] = [I_D] = \begin{bmatrix} BODYDI(1,1) & BODYDI(1,2) & BODYDI(1,3) \\ BODYDI(2,1) & BODYDI(2,2) & BODYDI(2,3) \\ BODYDI(3,1) & BODYDI(3,2) & BODYDI(3,3) \end{bmatrix}$$

This array is the inertia matrix of the docked body which consists of the docking vehicle connected to the stator.

UNITS: (slug-ft²)

FORMAT: # 5004 = (1X, E11.4)

BODYOI(M,N):

$$[BODYOI(M,N)] = [I_0] = \begin{bmatrix} BODYOI(1,1) & BODYOI(1,2) & BODYOI(1,3) \\ BODYOI(2,1) & BODYOI(2,2) & BODYOI(2,3) \\ BODYOI(3,1) & BODYOI(3,2) & BODYOI(3,3) \end{bmatrix}$$

This array is the inertia matrix of body 0, the stator.

UNITS: (slug-ft²).

FORMAT: # 5004 = (1X, E11.4)

BODY1I(M,N):

$$[\text{BODY1I}(M,N)] = [I_1] = \begin{bmatrix} \text{BODY1I}(1,1) & \text{BODY1I}(1,2) & \text{BODY1I}(1,3) \\ \text{BODY1I}(2,1) & \text{BODY1I}(2,2) & \text{BODY1I}(2,3) \\ \text{BODY1I}(3,1) & \text{BODY1I}(3,2) & \text{BODY1I}(3,3) \end{bmatrix}$$

This array is the inertia matrix for body 1, the rotor.

UNITS: (slug-ft²)

FORMAT: # 5004 = (1X, E11.4)

BOMASS:

BOMASS is the mass of body 0, the stator. BOMASS = m₀

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B1MASS:

B1MASS is the mass of body 1, the rotor. B1MASS = m₁

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B2MASS:

B2MASS is the mass of body 2, the elevator. B2MASS = m₂

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B3MASS:

B3MASS is the mass of body 3, a pendulum. $B3MASS = m_3$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B4MASS:

B4MASS is the mass of body 4, a pendulum. $B4MASS = m_4$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

CA(M):

CA(1), CA(2), and CA(3) are the three direction cosines of the desired attitude reference direction in the inertial frame.

UNITS: (None)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

CGAINO(M):

CGAINO(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 0.

CGAINO(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 0.

CGAINO(3) equals the control gain of all four reaction jets in the pure force couples producing torque around the Z axis of body 0.

Note: The variables AOJ(1), AOJ(2), and AOJ(3) are also read in on the same data cards as CGAINO(1), CGAINO(2), and CGAINO(3). Punch the values of CGAINO(1), CGAINO(2), and CGAINO(3) in columns 15 through 25 of the data cards.

UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

CGAIN1(M):

CGAIN1(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 1.

CGAIN1(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 1.

Note: The variables ALJ(1) and ALJ(2) are also read in on the same data cards as CGAIN1(1) and CGAIN1(2). Punch the values of CGAIN1(1) and CGAIN1(2) in columns 15 through 25 of the data cards.

UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

CP1 and CP2:

CP1 and CP2 are parameters used in determining the stiffness and the resonant frequency of the pendulums. For example, the control laws which are governed by the parameters are:

$$T13 = - CP1 * OMEGA3 - CP2 * THETA3$$

$$T14 = - CP1 * OMEGA4 - CP2 * (THETA4 - \pi)$$

Note: These variables are read on separate data cards.

UNITS: (none)

FORMAT: # 5004 = (1X, E11.4)

DD01(M):

DD01(1), DD01(2), and DD01(3) are the X, Y, and Z components of the vector from the center of mass of the docked body to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. The docked body shall be defined as the configuration of the docking vehicle attached to body 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DELTAT:

DELTAT = Δt

DELTAT is the time increment used in the integration algorithm which solves the rotational equations of motion. When "TIME" is updated we have:

TIME = TIME + DELTAT

Note: Punch the value of DELTAT in columns 28 through 38

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

D01(M):

D01(1), D01(2), and D01(3) are the X, Y, and Z components of the vector from the center of mass of body 0 to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. D01(1) should in most cases be zero.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTI(M):

DTI(1), DTI(2) and DTI(3) are the X, Y, and Z components of the docking torque impulse.

UNITS: lb-ft-sec

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTIME:

DTIME is the time when docking occurs. (i.e. "Docking Time")
The restrictions placed on DTIME are as follows:

- a) $T_{\text{start}} < \text{DTIME} < T_{\text{stop}}$
- b) DTIME must be an integer multiple of Δt .

UNITS: (seconds)

FORMAT: # 5006 = (1X, F11.5)

D12(M):

D12(1), D12(2) and D12(3) are the X, Y and Z components of a fixed vector locating the starting position of the movable mass, the elevator. The vector equation that describes the motion of the movable mass is $\vec{l}_2 = \vec{d}_{12} + \vec{s}_2 s$. Where \vec{s}_2 is a unit vector which defines the direction in which the movable mass travels and s is a scalar prespecified function of time. For most cases $s(t_0 = 0) = 0$ so that \vec{d}_{12} specifies the initial starting position of the movable mass. The elevator is known alternately as the movable mass or body 2. D12 is expressed in body 1 coordinates. For example, if the elevator were constrained to travel along the X axis, then \vec{d}_{12} could have the following values: D12(1) = 1., D12(2) = 0., D12(3) = 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

D13(M):

D13(1), D13(2), and D13(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 3. $\vec{D13}$ is expressed in body 1 coordinates.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

D14(M):

D14(1), D14(2), and D14(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 4.

D14 is expressed in body 1 coordinates.

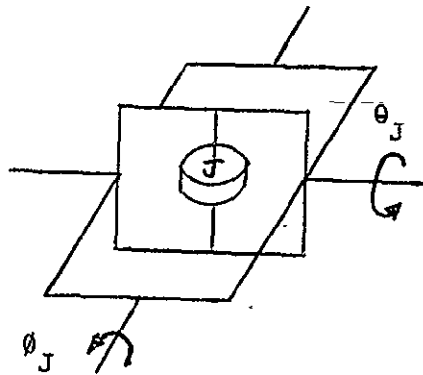
UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

FEE(J):

$$FEE(J) = \theta_J$$

FEE(J) is the outer gimbal angle of a two degree of freedom control moment gyro as shown pictorially below:



The subscript J refers to the number assigned to the CMG.
(Refer to the write up on CMGs for further discussion.)

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

FEED(J):

$$\text{FEED}(J) = \dot{\theta}_J$$

FEED(J) is the outer gimbal rate of a two degree of freedom control moment gyro. The subscript J refers to the number assigned to the CMG. (Refer to the write up on CMGs for further discussion.)

UNITS: (radians/second)

FORMAT: # 5006 = (1X, F11.5)

GAIN(M):

GAIN(M) is an array of numbers the dimension of which is determined by another input variable NGAIN. These numbers, once read in, are stored in common and can be used for a variety of purposes. In many CMG control laws it is necessary to have control gains. GAIN(M) can be used for this purpose among others.

UNITS: (None)

FORMAT: # 5004 = (1X, E11.4)

HW(J):

HW(J) is the angular momentum of the wheel associated with the Jth momentum device. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft²/second)

FORMAT: # 5004 = (1X, E11.4)

IATTIF:

IATTIF is the attitude flag.

IATTIF = 1 implies an attempt to change attitude will be made.

IATCIF = 0 implies an attempt to change attitude will not be made.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IB2F:

IB2F is the body 2 flag. (i.e. the elevator flag)

IB2F = 1 implies body 2 will be present.

IB2F = 0 implies body 2 will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IDOCK:

IDOCK is the docking flag.

IDOCK = 1 implies docking will occur.

IDOCK = 0 implies docking will not occur.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IDOF(J):

IDOF(J) = 0 implies the Jth controller aboard body 0 is a reaction wheel.

IDOF(J) = 1 implies the Jth controller aboard body 0 is a one degree of freedom control moment gyro.

IDOF(J) = 2 implies the Jth controller aboard body 0 is a two degree of freedom control moment gyro.

SPECIAL INSTRUCTIONS: Punch a 0, 1, or a 2 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IGRAVF:

IGRAVF is the gravity gradient flag.

IGRAVF = 1 implies gravity gradient torques will be present.

IGRAVF = 0 implies gravity gradient torques will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPNDLM:

IPNDLM is the pendulum flag.

IPNDLM = 1 implies body 3 and body 4, the pendulums, will be present.

IPNDLM = 0 implies body 3 and body 4, the pendulums, will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPRINT:

IPRINT is an integer variable used to determine how often output data is printed. Data is printed in time increments of IPRINT * DELTAT. For example, if IPRINT = 50 and DELTAT = .2, then data will be printed when time = 10, 20, 30, 40, 50,

SPECIAL INSTRUCTIONS: If IPRINT has a value less than 10, punch the integer in column 3 of the data card. If IPRINT has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPROP:

IPROP is the propulsion flag.

IPROP = 1 implies propulsion forces will be considered.

IPROP = 0 implies propulsion forces will not be considered.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

NDECK:

NDECK is an integer variable equal to the number of data decks present at run time.

SPECIAL INSTRUCTIONS: This variable goes in front of the first data deck only. If NDECK has a value less than 10, punch the integer in column 3 of the data card. If NDECK has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

NGAIN:

NGAIN is an integer variable and refers to the number of arbitrary gains which are input. If NGAIN = 3 then values for GAIN(1), GAIN(2) and GAIN(3) will be input. The maximum value of NGAIN is 10.

SPECIAL INSTRUCTIONS: If NGAIN has a value less than 10, punch the integer in column 3 of the data card. Otherwise, use columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

NUMCMG:

NUMCMG is the number of controllers aboard body 0. A maximum of 6 controllers may be used.

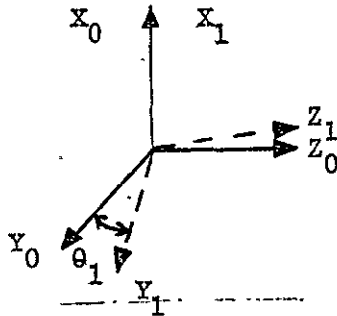
SPECIAL INSTRUCTIONS: Punch the integer in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

OMEGA1:

OMEGA1 is the initial relative angular velocity measure about the spin axis between bodies 0 and 1. Another definition of OMEGA1 can be visualized by referring to the sketch shown below showing the orthogonal coordinate systems located on bodies 0 and 1.



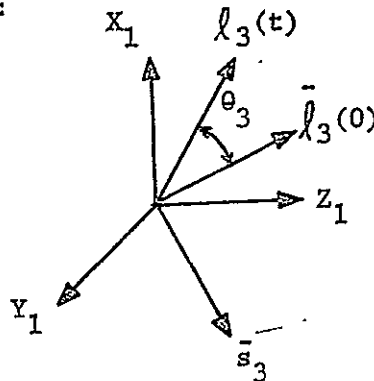
Implicit in this sketch is the hinge line between the stator and rotor is aligned parallel to both the \bar{X}_0 and \bar{X}_1 axes. Therefore, the orientation of the stator and the rotor differ only in a rotation $\theta_1 = \text{THETA1}$ and $\text{OMEGA1} = \dot{\theta}_1$.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

OMEGA3:

OMEGA3 is the angular velocity of body 3 about the hinge line \bar{s}_3 . OMEGA3 is also the time derivative of THETA3 when the datum for the angle THETA3 will be the \bar{Y}_1, \bar{Z}_1 plane as illustrated below:



In other words, \bar{s}_3 determines the positive direction of rotation by the right hand rule and the positive $Y_1 - Z_1$ plane determines to starting position.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

OMEGA4:

OMEGA4 is the angular velocity of body 4 about the hinge line \bar{s}_4 . OMEGA4 is also the time derivative of THETA4 where the datum for the angle THETA4 is the same as THETA3. (See OMEGA3)

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

PEND3L:

PEND3L is the scalar distance from the hinge line, \bar{s}_3 , to the center of mass of body 3. (i.e. the length of pendulum 3)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

PEND4L:

PEND4L is the scalar distance from the hinge line, \bar{s}_4 , to the center of mass of body 4. (i.e. the length of pendulum 4)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

S:

S is a scalar parameter used in defining the position of body 2. S defines the magnitude of displacement of body 2 from the zero position.

Note: Punch the value of S in columns 2 through 12.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME = T_{start}

SDOT:

SDOT defines the magnitude of the velocity vector of body 2.

Note: Punch the value of SDOT in columns 15 through 25.

UNITS: (feet per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME = T_{start}

SP:

SP is the desired spin magnitude of body 1 relative to body 0.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

S2(M):

S2(1), S2(2), and S2(3) are the X, Y, and Z components of a unit vector defining the direction of travel of body 2. \bar{s}_2 is expressed in body 1 coordinates.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

S3(M):

S3(1), S3(2), and S3(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 3. \bar{s}_3 is expressed in body 1 coordinates. S3(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

S4(M):

S4(1), S4(2), and S4(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 4. \bar{s}_4 is expressed in body 1 coordinates. S4(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

THATA(J):

THATA(J) is the gimballed angle of the Jth controller aboard body 0 assuming this controller is either a one or two degree of freedom control moment gyro. If it is a two degree of freedom CMG, then this variable refers to the inner gimballed angle. J may have a maximum value of 6.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

THATAD(J):

THATAD(J) is the gimballed rate associated with THATA(J).

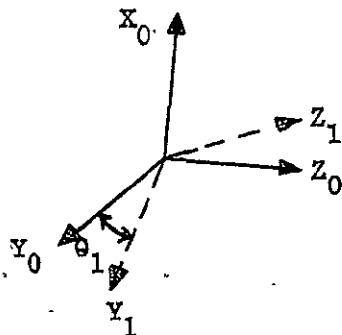
UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

THETA1:

THETA1 is the relative angular displacement measured about the spin axis, between bodies 0 and 1.



UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

THETA3:

THETA3 is the angle between pendulum 3 and the Y, Z, plane. The axis about which THETA3 rotates is the hinge line s_3 . For an explanation of the THETA3 datum refer to the discussion of OMEGA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

THETA4:

THETA4 is the angle between pendulum 4 and the Y, Z, plane. The axis about which THETA4 rotates is the hinge line s_4 . The datum for THETA4 is the same as for THETA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

TIBOI(M,N):

$$[TIBOI(M,N)] = \begin{bmatrix} TIBOI(1,1) & TIBOI(1,2) & TIBOI(1,3) \\ TIBOI(2,1) & TIBOI(2,2) & TIBOI(2,3) \\ TIBOI(3,1) & TIBOI(3,2) & TIBOI(3,3) \end{bmatrix}$$

This array is the initial transformation matrix of the body 0 coordinate system to the inertial coordinate system. If initially body 0 is aligned with the inertial system, TIBOI(M,N) would be the identity matrix. Refer to the coordinate transformation appendix for further details.

UNITS: (none)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUES AT TIME = T_{start}

TSTART:

TSTART is the time at which you wish the program to start calculating the equations of motion. Except for restarting, TSTART is usually set to zero.

SPECIAL INSTRUCTIONS: Punch the value of TSTART in columns 2 through 12.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

TSTOP:

TSTOP is the time at which you wish the program to stop calculating.

SPECIAL INSTRUCTIONS: Punch the value of TSTOP in columns 15 through 25.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

WO(M):

WO(1), WO(2), and WO(3) are the X, Y, and Z components of the angular velocity vector of body 0.

UNITS: (radians per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUES AT TIME = T_{start}

GENERAL INPUT VARIABLES

ALT:

ALT is altitude of the center of mass of the space station configuration measured from the surface of the earth. All orbits are constrained to be circular with no oblateness effects. Therefore, altitude is the only pertinent orbit parameter.

UNITS: (miles)

FORMAT: # 5004 = (1X, E11.4)

BDMASS:

BDMASS is the sum of the mass of body 0, the stator, and the mass of the docking vehicle. The docking vehicle is constrained to dock on body 0, the stator. $BDMASS = m_D$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

BODYDI(M,N):

$$[BODYDI(M,N)] = [I_D] = \begin{bmatrix} BODYDI(1,1) & BODYDI(1,2) & BODYDI(1,3) \\ BODYDI(2,1) & BODYDI(2,2) & BODYDI(2,3) \\ BODYDI(3,1) & BODYDI(3,2) & BODYDI(3,3) \end{bmatrix}$$

This array is the inertia matrix of the docked body which consists of the docking vehicle connected to the stator.

UNITS: (slug-ft²)

FORMAT: # 5004 = (1X, E11.4)

CA(M):

CA(1), CA(2), and CA(3) are the three direction cosines of the desired attitude reference direction in the inertial frame.

UNITS: (None)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

CP1 and CP2:

CP1 and CP2 are parameters used in determining the stiffness and the resonant frequency of the pendulums. For example, the control laws which are governed by the parameters are:

$$T13 = - CP1 * OMEGA3 - CP2 * THETA3$$

$$T14 = - CP1 * OMEGA4 - CP2 * (THETA4 - \pi)$$

Note: These variables are read on separate data cards.

UNITS: (none)

FORMAT: # 5004 = (1X, E11.4)

DD01(M):

DD01(1), DD01(2), and DD01(3) are the X, Y, and Z components of the vector from the center of mass of the docked body to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. The docked body shall be defined as the configuration of the docking vehicle attached to body 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DELTAT:

$$\text{DELTAT} = \Delta t$$

DELTAT is the time increment used in the integration algorithm which solves the rotational equations of motion. When "TIME" is updated we have:

$$\text{TIME} = \text{TIME} + \text{DELTAT}$$

Note: Punch the value of DELTAT in columns 28 through 38.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTI(M):

DTI(1), DTI(2) and DTI(3) are the X, Y, and Z components of the docking torque impulse.

UNITS: lb-ft-sec

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTIME:

DTIME is the time when docking occurs. (i.e. "Docking Time"). The restrictions placed on DTIME are as follows:

a) $T_{\text{start}} < \text{DTIME} < T_{\text{stop}}$

b) DTIME must be an integer multiple of Δt .

UNITS: (seconds)

FORMAT: # 5006 = (1X, F11.5)

GAIN(M):

GAIN(M) is an array of numbers the dimension of which is determined by another input variable NGAIN. These numbers, once read in, are stored in common and can be used for a variety of purposes. In many CMG control laws it is necessary to have control gains. GAIN(M) can be used for this purpose among others.

UNITS: (None)

FORMAT: # 5004 = (1X, E11.4)

IATTIF:

IATTIF is the attitude flag.

IATTIF = 1 implies an attempt to change attitude will be made.

IATTIF = 0 implies an attempt to change attitude will not be made.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IB2F:

IB2F is the body 2 flag. (i.e. the elevator flag)

IB2F = 1 implies body 2 will be present.

IB2F = 0 implies body 2 will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IDOCK:

IDOCK is the docking flag.

IDOCK = 1 implies docking will occur.

IDOCK = 0 implies docking will not occur.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IGRAVF:

IGRAVF is the gravity gradient flag.

IGRAVF = 1 implies gravity gradient torques will be present.

IGRAVF = 0 implies gravity gradient torques will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPNDLM:

IPNDLM is the pendulum flag.

IPNDLM = 1 implies body 3 and body 4, the pendulums, will be present.

IPNDLM = 0 implies body 3 and body 4, the pendulums, will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPRINT:

IPRINT is an integer variable used to determine how often output data is printed. Data is printed in time increments of IPRINT * DELTAT. For example, if IPRINT = 50 and DELTAT = .2, then data will be printed when time = 10, 20, 30, 40, 50,

SPECIAL INSTRUCTIONS: If IPRINT has a value less than 10, punch the integer in column 3 of the data card. If IPRINT has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (IX, I2)

IPROP:

IPROP is the propulsion flag.

IPROP = 1 implies propulsion forces will be considered.

IPROP = 0 implies propulsion forces will not be considered.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (IX, I2)

NDECK:

NDECK is an integer variable equal to the number of data decks present at run time.

SPECIAL INSTRUCTIONS: This variable goes in front of the first data deck only. If NDECK has a value less than 10, punch the integer in column 3 of the data card. If NDECK has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (IX, I2)

NGAIN:

NGAIN is an integer variable and refers to the number of arbitrary gains which are input. If NGAIN = 3 then values for GAIN(1), GAIN(2) and GAIN(3) will be input. The maximum value of NGAIN is 10.

SPECIAL INSTRUCTIONS: If NGAIN has a value less than 10, punch the integer in column 3 of the data card. Otherwise, use columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

TSTART:

TSTART is the time at which you wish the program to start calculating the equations of motion. Except for restarting, TSTART is usually set to zero.

SPECIAL INSTRUCTIONS: Punch the value of TSTART in columns 2 through 12.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

TSTOP:

TSTOP is the time at which you wish the program to stop calculating.

SPECIAL INSTRUCTIONS: Punch the value of TSTOP in columns 15 through 25.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

BODY 0 INPUT VARIABLES

AIJ(J,M,N):

$$[AIJ(J,M,N)] = [II_J] = \begin{bmatrix} AIJ(J,1,1) & AIJ(J,1,2) & AIJ(J,1,3) \\ AIJ(J,2,1) & AIJ(J,2,2) & AIJ(J,2,3) \\ AIJ(J,3,1) & AIJ(J,3,2) & AIJ(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the inner gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are also constrained to be located at the center of mass on the stator, body 0. If the Jth CMG has one or two degrees of freedom, it will have an inner gimbal. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft²).

FORMAT: # 5006 = (1X, F11.5)

AIO(J,M,N):

$$[AIO(J,M,N)] = [IO_J] = \begin{bmatrix} AIO(J,1,1) & AIO(J,1,2) & AIO(J,1,3) \\ AIO(J,2,1) & AIO(J,2,2) & AIO(J,2,3) \\ AIO(J,3,1) & AIO(J,3,2) & AIO(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the outer gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are constrained to be located at the center of mass on the stator, body 0. The Jth CMG will have an outer gimbal only if it has two degrees of freedom. (Refer to the write up on CMGs for further discussion.)

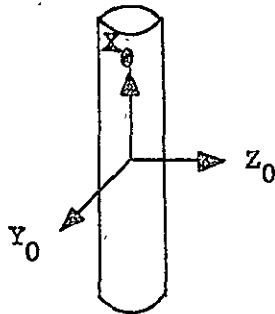
UNITS: (slug-ft²)

FORMAT: # 5006 = (1X, F11.5)

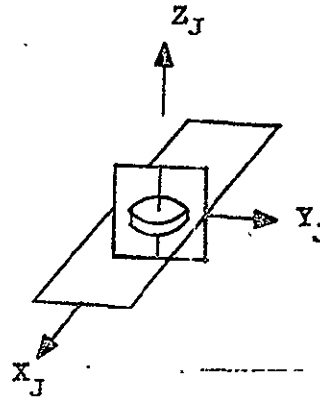
AOCJ(J,M,N):

$$[AOCJ(J,M,N)] = [O, C_J] = \begin{bmatrix} AOCJ(J,1,1) & AOCJ(J,1,2) & AOCJ(J,1,3) \\ AOCJ(J,2,1) & AOCJ(J,2,2) & AOCJ(J,2,3) \\ AOCJ(J,3,1) & AOCJ(J,3,2) & AOCJ(J,3,3) \end{bmatrix}$$

This array is the coordinate transformation matrix from the CMG null gimbal coordinate frame to the coordinate frame of body 0, the stator. (Refer to the coordinate transformation appendix.) For example, consider the two coordinate systems shown below:



Body 0 Frame



Jth Null Gimbal Frame

For the above situation:

$$[AOCJ(J,M,N)] = \begin{bmatrix} 0. & 0. & 1. \\ 1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$

UNITS: (None)

FORMAT: # 5006 = (1X, F11.5)

AOJ(M):

AOJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 0.

AOJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 0.

AOJ(3) is the distance between the jets of the pure couple producing the torque around the Z axis of body 0.

Note: The variables CGAINO(1), CGAINO(2), and CGAINO(3) are also read on the same data cards as AOJ(1), AOJ(2), and AOJ(3). Punch the values of AOJ(1), AOJ(2), and AOJ(3) in columns 2 through 12 of the data cards.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

BODYOI(M,N):

$$[\text{BODYOI}(M,N)] = [I_0] = \begin{bmatrix} \text{BODYOI}(1,1) & \text{BODYOI}(1,2) & \text{BODYOI}(1,3) \\ \text{BODYOI}(2,1) & \text{BODYOI}(2,2) & \text{BODYOI}(2,3) \\ \text{BODYOI}(3,1) & \text{BODYOI}(3,2) & \text{BODYOI}(3,3) \end{bmatrix}$$

This array is the inertia matrix of body 0, the stator.

UNITS: (slug-ft²)

FORMAT: # 5004 = (1X, E11.4)

BOMASS:

BOMASS is the mass of body 0, the stator. BOMASS = m₀

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

CGAINO(M):

CGAINO(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 0.

CGAINO(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 0.

CGAINO(3) equals the control gain of all four reaction jets in the pure force couples producing torque around the Z axis of body 0.

Note: The variables AOJ(1), AOJ(2), and AOJ(3) are also read in on the same data cards as CGAINO(1), CGAINO(2), and CGAINO(3). Punch the values of CGAINO(1), CGAINO(2), and CGAINO(3) in columns 15 through 25 of the data cards.

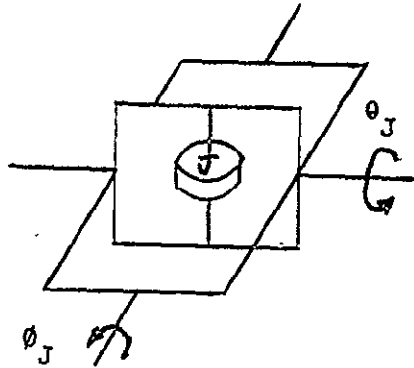
UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

FEE(J):

$$FEE(J) = \theta_J$$

FEE(J) is the outer gimbal angle of a two degree of freedom control moment gyro as shown pictorially below:



The subscript J refers to the number assigned to the CMG. (Refer to the write up on CMGs for further discussion.)

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

FEED(J):

$$\text{FEED}(J) = \dot{\theta}_J$$

FEED(J) is the outer gimbal rate of a two degree of freedom control moment gyro. The subscript J refers to the number assigned to the CMG. (Refer to the write up on CMGs for further discussion.)

UNITS: (radians/second)

FORMAT: # 5006 = (IX, F11.5)

HW(J):

HW(J) is the angular momentum of the wheel associated with the Jth momentum device. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft²/second)

FORMAT: # 5004 = (IX, E11.4)

IDOF(J):

IDOF(J) = 0 implies the Jth controller aboard body 0 is a reaction wheel.

IDOF(J) = 1 implies the Jth controller aboard body 0 is a one degree of freedom control moment gyro.

IDOF(J) = 2 implies the Jth controller aboard body 0 is a two degree of freedom control moment gyro.

SPECIAL INSTRUCTIONS: Punch a 0, 1, or a 2 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (IX, I2)

NUMCMG:

NUMCMG is the number of controllers aboard body 0. A maximum of 6 controllers may be used.

SPECIAL INSTRUCTIONS: Punch the integer in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

THATA(J):

THATA(J) is the gimbale angle of the Jth controller aboard body 0 assuming this controller is either a one or two degree of freedom control moment gyro. If it is a two degree of freedom CMG, then this variable refers to the inner gimbale angle. J may have a maximum value of 6.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

THATAD(J):

THATAD(J) is the gimbale rate associated with THATA(J).

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

TIBOI(M,N):

$$[TIBOI(M,N)] = \begin{bmatrix} TIBOI(1,1) & TIBOI(1,2) & TIBOI(1,3) \\ TIBOI(2,1) & TIBOI(2,2) & TIBOI(2,3) \\ TIBOI(3,1) & TIBOI(3,2) & TIBOI(3,3) \end{bmatrix}$$

This array is the initial transformation matrix of the body 0 coordinate system to the inertial coordinate system. If initially body 0 is aligned with the inertial system, TIBOI(M,N) would be the identity matrix. Refer to the coordinate transformation appendix for further details.

UNITS: (none)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUES AT TIME = T_{start}

WO(M):

WO(1), WO(2), and WO(3) are the X, Y, and Z components of the angular velocity vector of body 0.

UNITS: (radians per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUES AT TIME = T_{start}

BODY 1 INPUT VARIABLES

ALJ(M):

ALJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 1.

ALJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 1.

Note: The variables CGAIN1(1) and CGAIN1(2) are also read on the same data cards as ALJ(1) and ALJ(2).
Punch the values of ALJ(1) and ALJ(2) in columns 2 through 12 of the data cards.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

BODY1I(M,N):

$$[\text{BODY1I}(M,N)] = [I_1] = \begin{bmatrix} \text{BODY1I}(1,1) & \text{BODY1I}(1,2) & \text{BODY1I}(1,3) \\ \text{BODY1I}(2,1) & \text{BODY1I}(2,2) & \text{BODY1I}(2,3) \\ \text{BODY1I}(3,1) & \text{BODY1I}(3,2) & \text{BODY1I}(3,3) \end{bmatrix}$$

This array is the inertia matrix for body 1, the rotor.

UNITS: (slug-ft²)

FORMAT: # 5004 = (1X, E11.4)

BLMASS:

BLMASS is the mass of body 1, the rotor. BLMASS = m_1

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

CGAIN1(M):

CGAIN1(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 1.

CGAIN1(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 1.

Note: The variables AIJ(1) and AIJ(2) are also read in on the same data cards as CGAIN1(1) and CGAIN1(2). Punch the values of CGAIN1(1) and CGAIN1(2) in columns 15 through 25 of the data cards.

UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

D01(M):

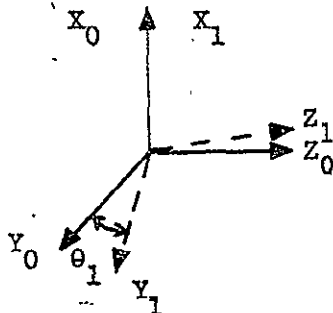
D01(1), D01(2), and D01(3) are the X, Y, and Z components of the vector from the center of mass of body 0 to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. D01(1) should in most cases be zero.

UNITS: (feet) e

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

OMEGA1:

OMEGA1 is the initial relative angular velocity measure about the spin axis between bodies 0 and 1. Another definition of OMEGA1 can be visualized by referring to the sketch shown below showing the orthogonal coordinate systems located on bodies 0 and 1.



Implicit in this sketch is the hinge line between the stator and rotor is aligned parallel to both the \bar{X}_0 and \bar{X}_1 axes. Therefore, the orientation of the stator and the rotor differ only in a rotation $\theta_1 = \text{THETA1}$ and $\text{OMEGA1} = \dot{\theta}_1$.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

SP:

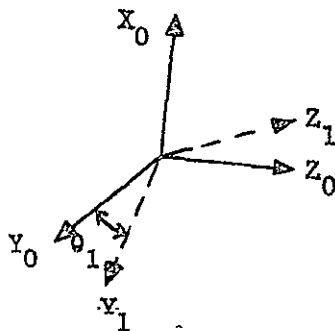
SP is the desired spin magnitude of body 1 relative to body 0.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

THETA1:

THETA1 is the relative angular displacement measured about the spin axis, between bodies 0 and 1.



UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

BODY 2 INPUT VARIABLES

B2MASS:

B2MASS is the mass of body 2, the elevator. $B2MASS = m_2$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

D12(M):

D12(1), D12(2) and D12(3) are the X, Y and Z components of a fixed vector locating the starting position of the movable mass, the elevator. The vector equation that describes the motion of the movable mass is $\vec{l}_2 = \vec{d}_{12} + \vec{s}_2 s$. Where \vec{s}_2 is a unit vector which defines the direction in which the movable mass travels and s is a scalar prespecified function of time. For most cases $s(t = 0) = 0$ so that \vec{d}_{12} specifies the initial starting position of the movable mass. The elevator is known alternately as the movable mass or body 2. D12 is expressed in body 1 coordinates. For example, if the elevator were constrained to travel along the X axis, then \vec{d}_{12} could have the following values: D12(1) = 1., D12(2) = 0., D12(3) = 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

S:

S is a scalar parameter used in defining the position of body 2. S defines the magnitude of displacement of body 2 from the zero position.

Note: Punch the value of S in columns 2 through 12.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME = T_{start}

SDOT:

SDOT defines the magnitude of the velocity vector of body 2.

Note: Punch the value of SDOT in columns 15 through 25.

UNITS: (feet per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME = T_{start}

S2(M):

S2(1), S2(2), and S2(3) are the X, Y, and Z components of a unit vector defining the direction of travel of body 2. \bar{s}_2 is expressed in body 1 coordinates.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

BODY 3 INPUT VARIABLES

B3MASS:

B3MASS is the mass of body 3, a pendulum. $B3MASS = m_3$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

D13(M):

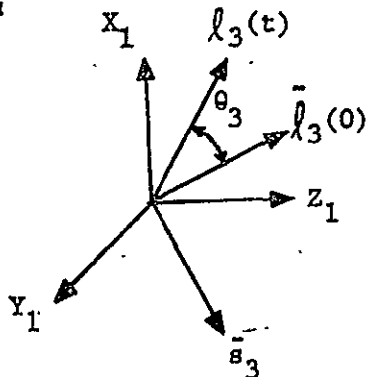
D13(1), D13(2), and D13(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 3. $\overline{D13}$ is expressed in body 1 coordinates.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

OMEGA3:

OMEGA3 is the angular velocity of body 3 about the hinge line \overline{s}_3 . OMEGA3 is also the time derivative of THETA3 when the datum for the angle THETA3 will be the $\overline{Y}_1, \overline{Z}_1$ plane as illustrated below:



In other words, \overline{s}_3 determines the positive direction of rotation by the right hand rule and the positive $Y_1 - Z_1$ plane determines to starting position.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

PEND3L:

PEND3L is the scalar distance from the hinge line, \vec{s}_2 , to the center of mass of body 3. (i.e. the length of pendulum 3)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

S3(M):

S3(1), S3(2), and S3(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 3. \vec{s}_3 is expressed in body 1 coordinates. S3(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

THETA3:

THETA3 is the angle between pendulum 3 and the Y, Z, plane. The axis about which THETA3 rotates is the hinge line \vec{s}_2 . For an explanation of the THETA3 datum refer to the discussion of OMEGA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

BODY 4 INPUT VARIABLES

B4MASS:

B4MASS is the mass of body 4, a pendulum. $B4MASS = m_4$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

D14(M):

D14(1), D14(2), and D14(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 4.

D14 is expressed in body 1 coordinates.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

OMEGA4:

OMEGA4 is the angular velocity of body 4 about the hinge line \bar{s}_4 . OMEGA4 is also the time derivative of THETA4 where the datum for the angle THETA4 is the same as THETA3. (See OMEGA3)

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

PEND4L:

PEND4L is the scalar distance from the hinge line, \bar{s}_4 , to the center of mass of body 4. (i.e. the length of pendulum 4)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

S4(M):

S4(1), S4(2), and S4(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 4. \bar{s}_4 is expressed in body 1 coordinates. S4(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

THETA4:

THETA4 is the angle between pendulum 4 and the Y, Z, plane. The axis about which THETA4 rotates is the hinge line \bar{s}_4 . The datum for THETA4 is the same as for THETA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME = T_{start}

APPENDIX B, COORDINATE TRANSFORMATIONS

The following pages contain a pictorial guide to aid the user in computing the initial transformation matrix from one right hand orthogonal coordinate system to another. The transformation matrix from coordinate system B to coordinate A shall be denoted $[A,B]$.

Mathematically:

$$\begin{bmatrix} X_A \\ Y_A \\ Z_A \end{bmatrix} = [A,B] \begin{bmatrix} X_B \\ Y_B \\ Z_B \end{bmatrix}$$

$$\text{i.e. } X_A = AB(1,1) * X_B + AB(1,2) * Y_B + AB(1,3) * Z_B$$

$$Y_A = AB(2,1) * X_B + AB(2,2) * Y_B + AB(2,3) * Z_B$$

$$Z_A = AB(3,1) * X_B + AB(3,2) * Y_B + AB(3,3) * Z_B$$

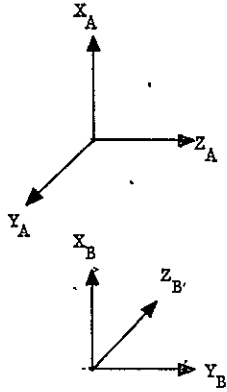
For simplicity, the coordinate systems in the following illustrations are orthogonal to each other in one way or another, i.e. There are not small offsetting rotations. Hence, the components of A,B may assume only certain values. The components may be $\pm 1.$, $0.$, $\pm \sin\phi$, $\pm \cos\phi$, $\pm \sin\theta$, $\pm \cos\theta$, $\pm \sin\psi$, or $\pm \cos\psi$ where ϕ , θ , and ψ are angles of rotation about the X, Y, Z axes respectively.

FLOW CHART & BLOCK DIAGRAM

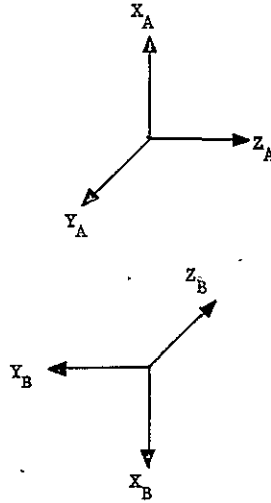
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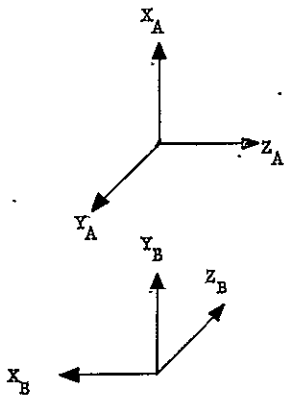
Procedure _____ Drawn By _____



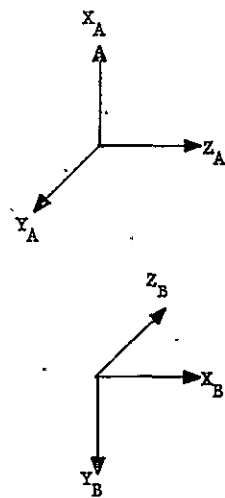
$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & 0. & -1. \\ 0. & 1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & 0. & -1. \\ 0. & -1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ 0. & 0. & -1. \\ -1. & 0. & 0. \end{bmatrix}$$

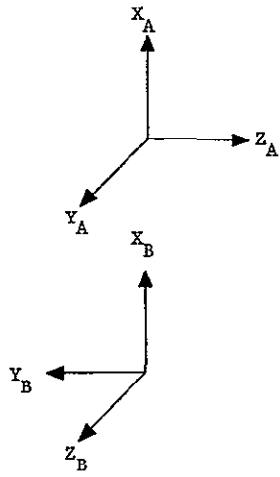


$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ 0. & 0. & -1. \\ 1. & 0. & 0. \end{bmatrix}$$

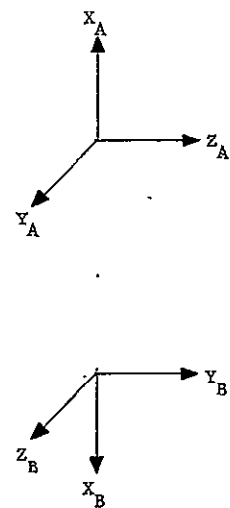
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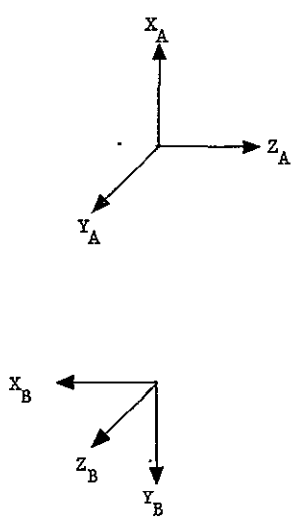


$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & 0. & 1. \\ 0. & -1. & 0. \end{bmatrix}$$

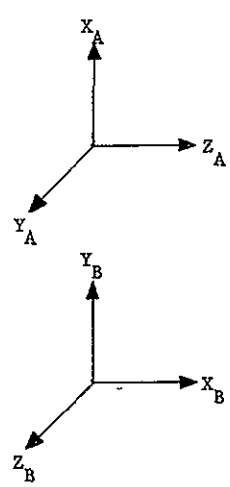


$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & 0. & 1. \\ 0. & 1. & 0. \end{bmatrix}$$

fold



$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ 0. & 0. & 1. \\ -1. & 0. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ 0. & 0. & 1. \\ 1. & 0. & 0. \end{bmatrix}$$

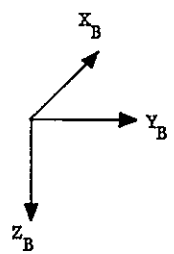
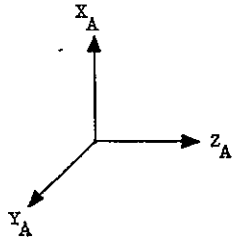
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FLOW CHART & BLOCK DIAGRAM

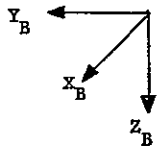
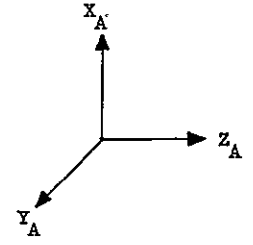
FORM DEN 1102-01 (1-6-1)

Application _____ Date _____ Page _____ of _____

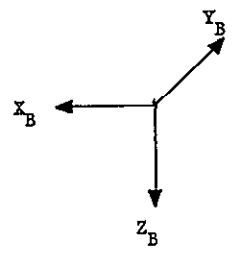
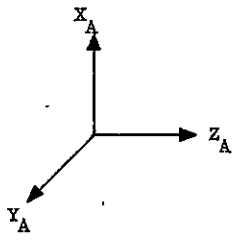
Procedure _____ Drawn By _____



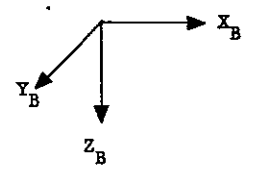
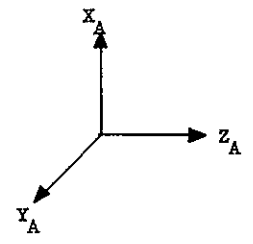
$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ -1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ 1. & 0. & 0. \\ 0. & -1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ 0. & -1. & 0. \\ -1. & 0. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ 0. & 1. & 0. \\ 1. & 0. & 0. \end{bmatrix}$$

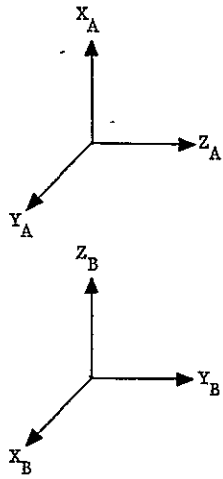
old

Fold to related line

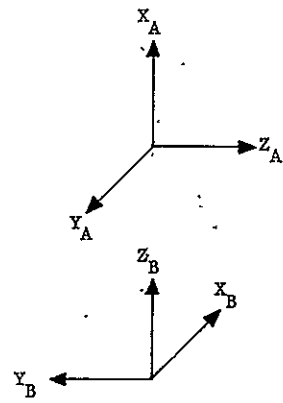
FLOW CHART & BLOCK DIAGRAM

Application _____ Date _____ Page _____ of _____

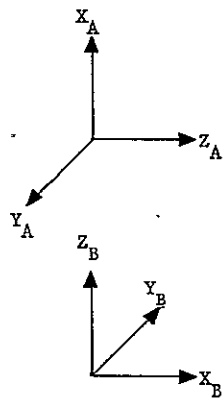
Procedure _____ Drawn By _____



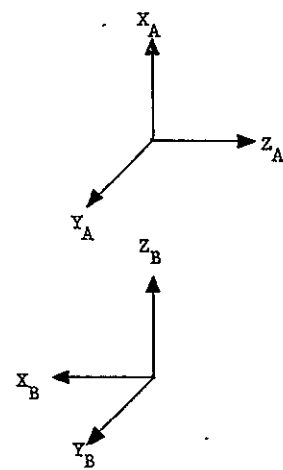
$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ 1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ -1. & 0. & 0. \\ 0. & -1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ 0. & -1. & 0. \\ 1. & 0. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ 0. & 1. & 0. \\ -1. & 0. & 0. \end{bmatrix}$$

Field

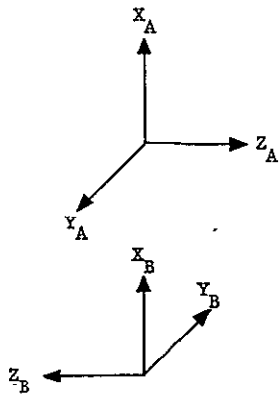
Field to center line

FLOW CHART & BLOCK DIAGRAM

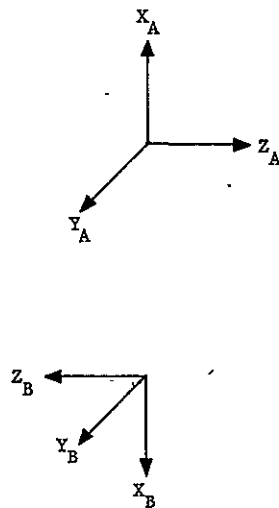
FORM DEN 1103-D1 (2-62)

Application _____ Date _____ Page _____ of _____

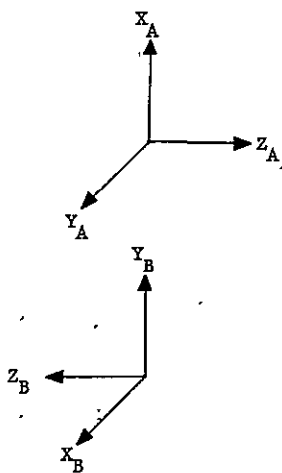
Procedure _____ Drawn By _____



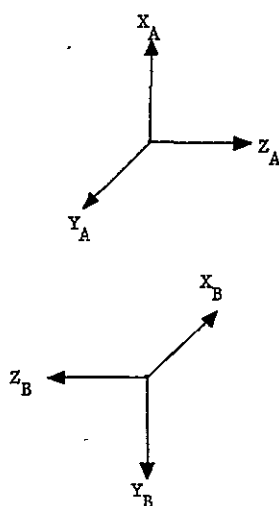
$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & -1. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & 1. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ 1. & 0. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ -1. & 0. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$

old

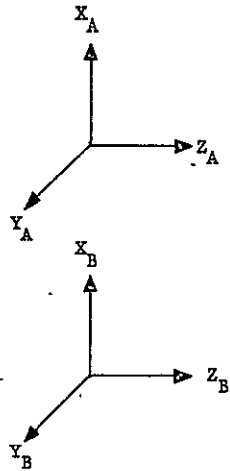
FORM DEN 1103-D1 (2-62)

FLOW CHART & BLOCK DIAGRAM

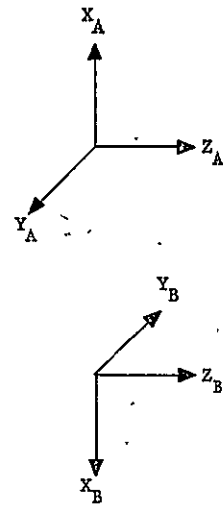
FORM DEN 1103-D1 (4-64)

Application _____ Date _____ Page _____ of _____

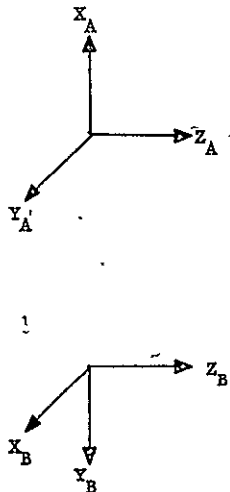
Procedure _____ Drawn By _____



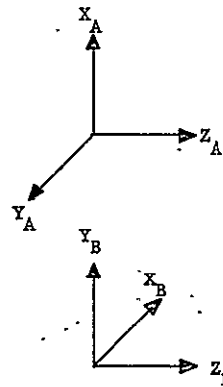
$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & 1. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & -1. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ 1. & 0. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ -1. & 0. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$

CHARGE. 03 MD246 2070000603744524 8947 56665

P.HENDRICKS2284

MAP.
RUN24(P,,,,,37777,,1)
LGO.
EXIT.
DMP.
DMP(0,150000)

PROGRAM MD246 (INPUT, OUTPUT, TAPES=INPUT, TAPES=OUTPUT, FILMPL)

C
C
C
C

```

*****
COMMON  A(3)          °          AE(5)          °          AED(5)          °  COMMC
*        AFOUR(2)     °          AII(6,3,3)    °          °          °  COMMC
*        AIO(6,3,3)   °          AJ1(3)        °          ALT          °  COMMC
*        AOCJ(6,3,3)  °          AOJ(3)       °          ACNE(7)      °  COMMC
*        ATCPT2(3,3)  °          ATHREE(5)  °          ATWO(4)      °  COMMC
*        A1(3,3)      °          A1J(2)       °          °          °  COMMC
COMMON  BDMASS        °          BFOUR(2)     °          BMOM         °  COMMC
*        BODYDI(3,3)  °          BODYOI(3,3)  °          BODY1I(3,3)  °  COMMC
*        BOMASS       °          BONE(7)       °          BTHREE(5)    °  COMMC
*        BTWO(4)      °          B1MASS        °          B2MASS        °  COMMC
*        B3MASS       °          B4MASS        °          °          °  COMMC
COMMON  CA(3)        °          CB(3)         °          CGAIN0(3)    °  COMMC
*        CGAIN1(2)    °          °          °          °          °  COMMC
*        COSFEJ       °          COSTTJ       °          COSTT0       °  COMMC
*        COSTT1       °          COSTT3       °          COSTT4       °  COMMC
*        CO2T         °          CP1          °          CPR          °  COMMC
*        CST          °          C1           °          °          °  COMMC
COMMON  DB(3)        °          DD01(3)     °          °          °  COMMC
*        DELTAT       °          D01(3)       °          D01DOT(3)    °  COMMC
*        DTI(3)       °          °          °          °          °  COMMC
*        DTIME        °          D12(3)       °          D13(3)       °  COMMC
*        D13DOT(3)    °          D13YCS       °          D13YSN       °  COMMC
*        D13ZCS       °          D13ZSN       °          D14(3)       °  COMMC
*        D14DOT(3)    °          D14YCS       °          D14YSN       °  COMMC
*        D14ZCS       °          D14ZSN       °          °          °  COMMC
COMMON  EEE(3,3)     °          EEJ(3,3)    °          EL2(3)       °  COMMC
*        EL2DOT(3)    °          EL2YCS       °          EL2YSN       °  COMMC
*        EL2ZCS       °          EL2ZSN       °          ELB(3)       °  COMMC
*        EL3DOT(3)    °          EL3YCS       °          ELBYSN       °  COMMC
*        EL3ZCS       °          EL3ZSN       °          EL4(3)       °  COMMC
*        EL4DOT(3)    °          EL4YCS       °          EL4YSN       °  COMMC
*        EL4ZCS       °          EL4ZSN       °          EM(6,6)     °  COMMC
COMMON  FAT(8)       °          °          °          °          °  COMMC
*        FEE(6)       °          FEED(6)      °          FFF(3)       °  COMMC
*        FFJ(3)       °          FLAG1       °          FLAG2       °  COMMC
*        FLAG3       °          FLAG4       °          FN          °  COMMC
*        FO(3)        °          FO1(3)      °          F02(3)      °  COMMC
*        FO3(3)       °          F1(3)       °          F11(3)      °  COMMC
*        FPT(5)       °          °          °          °          °  COMMC
*        F12(3)       °          F13(3)      °          °          °  COMMC
COMMON  GAIN(10)     °          G3           °          °          °  COMMC
*        G3DOT       °          G4          °          G4DOT       °  COMMC
COMMON  H(3)         °          HCMG(3)     °          HDOT(3)     °  COMMC
*        HI(3)        °          HO(3)       °          HW(6)       °  COMMC
*        H1(3)        °          HIPDOT(3)   °          HIPRIM(3)   °  COMMC

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| | | | | | | | |
|--------|-------------|---|-------------|---|-------------|---|-------|
| * | H3PRIM(3) | , | H4PRIM(3) | , | ICFB | , | COMMC |
| COMMON | IB2F | , | ICFA | , | IDOCK | , | COMMC |
| * | ICFC | , | ICFD | , | | , | COMMC |
| * | IDOF(6) | , | | , | IPNTCK | , | COMMC |
| * | IGRAVF | , | IPNDLM | , | | , | COMMC |
| * | IPRINT | , | IPROPF | , | | , | COMMC |
| COMMON | NCASE | , | NCHECK | , | NDECK | , | COMMC |
| * | NGAIN | , | NUMCMG | , | | , | COMMC |
| COMMON | OMEGA1 | , | OMEGA3 | , | OMEGA4 | , | COMMC |
| COMMON | PEND3L | , | PEND4L | , | | , | COMMC |
| COMMON | Q(4,4) | , | | , | | , | COMMC |
| * | R | , | R0(3) | , | R1(3) | , | COMMC |
| * | R1DOT(3) | , | R1YCS | , | R1YSN | , | COMMC |
| * | R1ZCS | , | R1ZSN | , | R2(3) | , | COMMC |
| * | R2DOT(3) | , | R2YCS | , | R2YSN | , | COMMC |
| * | R2ZCS | , | R2ZSN | , | R3(3) | , | COMMC |
| * | R3DOT(3) | , | R3YCS | , | R3YSN | , | COMMC |
| * | R3ZCS | , | R3ZSN | , | R4(3) | , | COMMC |
| * | R4DOT(3) | , | R4YCS | , | R4YSN | , | COMMC |
| * | R4ZCS | , | R4ZSN | , | | , | COMMC |
| COMMON | S | , | SDOT | , | SINFEJ | , | COMMC |
| * | SINTTJ | , | SINTT0 | , | SINTT1 | , | COMMC |
| * | SINTT2 | , | SINTT3 | , | SINTT4 | , | COMMC |
| * | SP | , | SUM1 | , | SUM2 | , | COMMC |
| * | SUM3 | , | S2(3) | , | S3(3) | , | COMMC |
| * | S4(3) | , | | , | | , | COMMC |
| COMMON | T(3,3) | , | TC(3,3) | , | TEMP1(3) | , | COMMC |
| * | TEMP2(3) | , | | , | | , | COMMC |
| * | TEMP3(3) | , | TEMP4(3) | , | TEMP5(3,3) | , | COMMC |
| * | TEMP6(3,3) | , | TEMP7(3,3) | , | TEMP8(3,3) | , | COMMC |
| * | TEMP9(3,3) | , | TEMP10(3,3) | , | TEMP11(3,3) | , | COMMC |
| * | TEMP12(3,3) | , | TEMP13(3,3) | , | TEMP14(3,3) | , | COMMC |
| * | TEMP15(3,3) | , | TERM1(3) | , | TERM2(3) | , | COMMC |
| * | TFRICT | , | THATA(6) | , | THATAD(6) | , | COMMC |
| * | THETA1 | , | THETA3 | , | THETA4 | , | COMMC |
| * | THETO | , | TIB0(3,3) | , | TIB0I(3,3) | , | COMMC |
| * | TIME | , | TJ | , | TJ1(10) | , | COMMC |
| * | TJ2(10) | , | TJ3(10) | , | TJ4(10) | , | COMMC |
| * | TMOTOR | , | | , | | , | COMMC |
| * | TOEF(3) | , | TOTMAS | , | T01 | , | COMMC |
| * | TQOG(3) | , | TQOP(3) | , | TQ1G(3) | , | COMMC |
| * | TQ1P(3) | , | TSTART | , | TSTOP | , | COMMC |
| * | TT1DOT | , | TT3DOT | , | TT4DOT | , | COMMC |
| * | T1EF(3) | , | T13 | , | T14 | , | COMMC |
| COMMON | V(3) | , | | , | | , | COMMC |
| COMMON | W0(3) | , | WS | , | W1(3) | , | COMMC |
| * | W3(3) | , | W4(3) | , | | , | COMMC |
| COMMON | X(6,7) | , | XC | , | XCDOT | , | COMMC |
| * | XMU | , | | , | | , | COMMC |

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THIS IS THE ENTRY POINT TO THE RUN CONTROL MODULE.
THE FUNCTION OF THIS MODULE IS TO MAKE THE DECISION TO STOP ALL
CALCULATIONS AND EXIT THE PROGRAM OR CONTINUE TO THE INPUT MODULE
AND READ IN THE DATA FOR THE NEXT CASE.

```

NCHECK = 0

C
C
C
C
C
C
C
C
C
C
C

RCON
RCON
RCON
RCON
RCON
RCON
RCON

```

C READ IN THE NUMBER OF DATA DECKS PRESENT AT RUN TIME. RCON
READ (5,5000) NDECK RCON
C PRINT NDECK ON A NEW SHEET OF PAPER. RCON
WRITE(6,6000) NDECK RCON
C THE PROGRAM RETURNS TO THE FOLLOWING STATEMENT NUMBER AFTER EACH RCON
C DATA DECK HAS BEEN COMPLETELY PROCESSED. RCON
10 NCHECK = NCHECK + 1 RCON
IF (NDECK .GE. NCHECK) GO TO 20 RCON
STOP RCON
20 CONTINUE RCON
RCON
C ***** RCON
C * RCON
C * RCON
C ***** RCON
C THIS IS THE ENTRY POINT TO THE INPUT MODULE. INPUT
C THE FUNCTION OF THIS MODULE IS TO READ IN ALL DATA PERTAINING TO INPUT
C THE NEXT CASE. AFTER EACH VARIABLE HAS BEEN READ IN, IT WILL BE INPUT
C PRINTED OUT TO INSURE PROPER CONVERSION AND TO RETAIN A RECORD OF INPUT
C THE INPUT DATA. INPUT
C INPUT
C DO 25 M=1,10 INPUT
GAIN(M) = 0. INPUT
25 CONTINUE INPUT
WRITE(6,6500) NCHECK INPUT
READ THE PENDULUM FLAG. INPUT
READ (5,5000) IPNDLM INPUT
WRITE(6,6082) IPNDLM INPUT
C READ THE PRINT FLAG. (I.E. PRINT EVERY IPRINT TIME POINT.) INPUT
READ (5,5000) IPRINT INPUT
WRITE(6,6544) IPRINT INPUT
C READ THE STARTING TIME, STOPING TIME, AND DELTAT. INPUT
READ (5,5002) TSTART,TSTOP,DELTAT INPUT
WRITE(6,6002) TSTART,TSTOP,DELTAT INPUT
C READ THE ORBIT ALTITUDE. INPUT
READ (5,5004) ALT INPUT
WRITE(6,6004) ALT INPUT
C READ THE TRANSFORMATION FROM THE BODY 0 FRAME TO THE I FRAME. INPUT
DO 30 M=1,3 INPUT
DO 30 N=1,3 INPUT
READ (5,5006) TIBOI(M,N) INPUT
30 CONTINUE INPUT
DO 35 M=1,3 INPUT
WRITE(6,6006) M,TIBOI(M,1),M,TIBOI(M,2),M,TIBOI(M,3) INPUT
35 CONTINUE INPUT
C READ BODY 0 ANGULAR RATES. INPUT
READ (5,5002) WO(1),WO(2),WO(3) INPUT
WRITE(6,6008) WO(1),WO(2),WO(3) INPUT
C READ THE MASS OF BODY 0. INPUT
READ (5,5004) BOMASS INPUT
J = 0 INPUT
WRITE(6,6010) J,BOMASS INPUT
C READ THE INERTIA MATRIX FOR BODY 0. INPUT
DO 40 M=1,3 INPUT
DO 40 N=1,3 INPUT
READ (5,5004) BODYOI(M,N) INPUT
40 CONTINUE INPUT
DO 45 M=1,3 INPUT
WRITE(6,6012) M,BODYOI(M,1),M,BODYOI(M,2),M,BODYOI(M,3) INPUT
45 CONTINUE INPUT

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| | | |
|-----|--|-------|
| C | READ THE NUMBER OF CONTROL MOMENT GYROs ABOARD BODY 0. | INPUT |
| | READ (5,5000) NUMCMG | INPUT |
| | WRITE(6,6014) NUMCMG | INPUT |
| | IF (NUMCMG .EQ. 0) GO TO 120 | INPUT |
| | DO 110 J=1,NUMCMG | INPUT |
| C | READ THE DEGREE OF FREEDOM OF THE JTH CMG. | INPUT |
| | READ (5,5000) IDOF(J) | INPUT |
| | IF (IDOF(J) .NE. 0) GO TO 50 | INPUT |
| | WRITE(6,6016) J | INPUT |
| | GO TO 70 | INPUT |
| 50 | IF (IDOF(J) .NE. 1) GO TO 60 | INPUT |
| | WRITE(6,6018) J | INPUT |
| | GO TO 70 | INPUT |
| 60 | WRITE(6,6020) J | INPUT |
| 70 | CONTINUE | INPUT |
| C | READ THE ANGULAR MOMENTUM OF THE JTH CMG. | INPUT |
| | READ (5,5004) HW(J) | INPUT |
| | WRITE(6,6022) J,HW(J) | INPUT |
| C | READ THE TRANSFORMATION FROM THE JTH NULL GIMBAL FRAME TO BODY 0 | INPUT |
| C | FRAME. | INPUT |
| | DO 80 M=1,3 | INPUT |
| | DO 80 N=1,3 | INPUT |
| | READ (5,5006) AOCJ(J,M,N) | INPUT |
| 80 | CONTINUE | INPUT |
| | DO 85 M=1,3 | INPUT |
| | WRITE(6,6024) J,M,AOCJ(J,M,1),J,M,AOCJ(J,M,2),J,M,AOCJ(J,M,3) | INPUT |
| 85 | CONTINUE | INPUT |
| | IF (IDOF(J) .EQ. 0) GO TO 110 | INPUT |
| C | READ THE INERTIA MATRIX FOR THE JTH INNER GIMBAL. | INPUT |
| | DO 90 M=1,3 | INPUT |
| | DO 90 N=1,3 | INPUT |
| | READ (5,5006) AII(J,M,N) | INPUT |
| 90 | CONTINUE | INPUT |
| | DO 95 M=1,3 | INPUT |
| | WRITE(6,6026) J,M,AII(J,M,1),J,M,AII(J,M,2),J,M,AII(J,M,3) | INPUT |
| 95 | CONTINUE | INPUT |
| C | READ THE INNER GIMBAL ANGLE AND RATE OF THE JTH CMG. | INPUT |
| | READ (5,5006) THATA(J) | INPUT |
| | READ (5,5006) THATAD(J) | INPUT |
| | WRITE(6,6028) J,THATA(J),J,THATAD(J) | INPUT |
| | FEE(J) = 0. | INPUT |
| | FEED(J) = 0. | INPUT |
| | IF (IDOF(J) .EQ. 1) GO TO 110 | INPUT |
| C | READ THE INERTIA MATRIX FOR THE JTH OUTER GIMBAL. | INPUT |
| | DO 100 M=1,3 | INPUT |
| | DO 100 N=1,3 | INPUT |
| | READ (5,5006) AIO(J,M,N) | INPUT |
| 100 | CONTINUE | INPUT |
| | DO 105 M=1,3 | INPUT |
| | WRITE(6,6030) J,M,AIO(J,M,1),J,M,AIO(J,M,2),J,M,AIO(J,M,3) | INPUT |
| 105 | CONTINUE | INPUT |
| C | READ THE OUTER GIMBAL ANGLE AND RATE OF THE JTH CMG. | INPUT |
| | READ (5,5006) FEE(J) | INPUT |
| | READ (5,5006) FEED(J) | INPUT |
| | WRITE(6,6032) J,FEE(J),J,FEED(J) | INPUT |
| 110 | CONTINUE | INPUT |
| 120 | CONTINUE | INPUT |
| C | READ THE PROPULSION FLAG. | INPUT |
| | READ (5,5000) IPROPF | INPUT |
| | WRITE(6,6072) IPROPF | INPUT |
| | IF (IPROPF .EQ. 0) GO TO 140 | INPUT |
| | READ (5,5000) IATTIF | INPUT |

| | | |
|-----|--|-------|
| | WRITE(6,6562) IATTIF | INPUT |
| | IF (IATTIF .EQ. 0) GO TO 125 | INPUT |
| | READ (5,5002) CA(1),CA(2),CA(3) | INPUT |
| | WRITE(6,6564) CA(1),CA(2),CA(3) | INPUT |
| 125 | CONTINUE | INPUT |
| | DO 130 J=1,3 | INPUT |
| | READ (5,5008) AOJ(J), CGAINO(J) | INPUT |
| | WRITE(6,6074) J,AOJ(J),J,CGAINO(J) | INPUT |
| 130 | CONTINUE | INPUT |
| 140 | CONTINUE | INPUT |
| C | READ IN VARIABLES RELATED TO BODY 1. | INPUT |
| C | READ THE MASS OF BODY 1. | INPUT |
| | READ (5,5004) B1MASS | INPUT |
| | J = 1 | INPUT |
| | WRITE(6,6010) J,B1MASS | INPUT |
| C | READ THE INERTIA MATRIX FOR BODY 1. | INPUT |
| | DO 150 M=1,3 | INPUT |
| | DO 150 N=1,3 | INPUT |
| | READ (5,5004) BODY1I(M,N) | INPUT |
| 150 | CONTINUE | INPUT |
| | DO 153 M=1,3 | INPUT |
| | WRITE(6,6040) M,BODY1I(M,1),M,BODY1I(M,2),M,BODY1I(M,3) | INPUT |
| 153 | CONTINUE | INPUT |
| C | READ THE PRIMARY GIMBAL ANGLE AND RATE OF BODY 1 W.R.T. BODY 0. | INPUT |
| | READ (5,5006) THETA1 | INPUT |
| | READ (5,5006) OMEGA1 | INPUT |
| | WRITE(6,6042) THETA1,OMEGA1 | INPUT |
| C | READ THE VECTOR FROM THE CM OF BODY 0 TO THE HINGE POINT BETWEEN | INPUT |
| C | BODY 0 AND BODY 1. (BODY 0 COORDINATES) | INPUT |
| | READ (5,5002) D01(1),D01(2),D01(3) | INPUT |
| | WRITE(6,6044) D01(1),D01(2),D01(3) | INPUT |
| C | READ THE BODY 2 FLAG. (I.E. THE ELEVATOR FLAG.) | INPUT |
| | READ (5,5000) IB2F | INPUT |
| | WRITE(6,6546) IB2F | INPUT |
| C | IF (IB2F .EQ. 0) GO TO 155 | INPUT |
| | READ THE MASS OF THE ELEVATOR. | INPUT |
| | READ (5,5004) B2MASS | INPUT |
| | J = 2 | INPUT |
| | WRITE(6,6010) J,B2MASS | INPUT |
| | READ (5,5002) D12(1),D12(2),D12(3) | INPUT |
| | WRITE(6,6535) D12(1),D12(2),D12(3) | INPUT |
| | READ (5,5002) S2(1), S2(2), S2(3) | INPUT |
| | J = 2 | INPUT |
| | WRITE(6,6052) J,S2(1),J,S2(2),J,S2(3) | INPUT |
| C | READ THE POSITION AND VELOCITY OF THE ELEVATOR. | INPUT |
| | READ (5,5002) S,SDOT | INPUT |
| | WRITE(6,6548) S,SDOT | INPUT |
| | GO TO 157 | INPUT |
| 155 | B2MASS = 0. | INPUT |
| | D12(1) = 0. | INPUT |
| | D12(2) = 0. | INPUT |
| | D12(3) = 0. | INPUT |
| | S2(1) = 0. | INPUT |
| | S2(2) = 0. | INPUT |
| | S2(3) = 0. | INPUT |
| | SDOT = 0. | INPUT |
| | S = 0. | INPUT |
| 157 | CONTINUE | INPUT |
| | IF (IPROPF .EQ. 0) GO TO 170 | INPUT |
| | DO 160 J=1,2 | INPUT |
| | READ (5,5008) AJJ(J), CGAIN1(J) | INPUT |
| | WRITE(6,6076) J,AJJ(J),J,CGAIN1(J) | INPUT |

D14(2) = 0.
D14(3) = 0.
S4(1) = 0.
S4(2) = 0.
S4(3) = 0.
PEND4L = 0.
THETA4 = 0.
OMEGA4 = 0.

174 CONTINUE
READ (5,5006) SP
WRITE(6,6080) SP
READ (5,5000) NGAIN
WRITE(6,6570) NGAIN
IF (NGAIN .EQ. 0) GO TO 176
DO 175 J=1,NGAIN
READ (5,5004) GAIN(J)
WRITE(6,6572) J,GAIN(J)

175 CONTINUE

176 CONTINUE

C READ THE GRAVITY GRADIENT FLAG.

READ (5,5000) IGHAVF

WRITE(6,6078) IGRAVF

C READ THE DOCKING FLAG. IDOCK = 1 IMPLIES A DOCKING WILL OCCUR.

READ (5,5000) IDOCK

WRITE(6,6068) IDOCK

IF (IDOCK .EQ. 0) GO TO 180

C READ THE TIME OF DOCKING.

READ (5,5006) DTIME

WRITE(6,6070) DTIME

DTMIN = DTIME * DELTAT/10.

DTMAX = DTIME + DELTAT/10.

DCHMIN = DTIME - 1.1*DELTAT

UCHMAX = DTIME + 0.9*DELTAT

READ (5,5004) BDMASS

WRITE(6,6574) BDMASS

DO 177 M=1,3

DO 177 N=1,3

READ (5,5004) BODYDI(M,N)

177 CONTINUE

DO 178 M=1,3

WRITE(6,6576) M,BODYDI(M,1),M,BODYDI(M,2),M,BODYDI(M,3)

178 CONTINUE

READ (5,5002) DTI(1),DTI(2),DTI(3)

WRITE(6,6578) DTI(1),DTI(2),DTI(3)

READ (5,5002) DDO1(1),DDO1(2),DDO1(3)

WRITE(6,6586) DDO1(1),DDO1(2),DDO1(3)

180 CONTINUE

*
*
*

THIS IS THE ENTRY POINT TO THE INITIALIZATION BLOCK.
ALL INITIAL CALCULATIONS ARE PERFORMED ONE TIME ONLY FOR EACH CASE

CALCULATE THE TOTAL MASS OF THE CONFIGURATION.
TOTMAS = BOMASS + B1MASS + B2MASS + B3MASS + B4MASS
ICFA = 0
ICFB = 0
ICFC = 0

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```
AONE(7) = G4                                INTEG
BONE(1) = DELTAT                            INTEG
BONE(2) = HDOT(1)                           INTEG
BONE(3) = HDOT(2)                           INTEG
BONE(4) = HDOT(3)                           INTEG
BONE(5) = H1PDOT(1)                         INTEG
BONE(6) = G3DOT                             INTEG
BONE(7) = G4DOT                             INTEG
CALL FOMS(AONE,BONE,7,FLAG1,TJ1)           INTEG
H(1) = AONE(2)                              INTEG
H(2) = AONE(3)                              INTEG
H(3) = AONE(4)                              INTEG
IF (IDOCK .EQ. 0) GO TO 193                 INTEG
IF ((TIME .LT. DCHMIN) .OR. (TIME .GT. DCHMAX)) GO TO 193 INTEG
H(1) = H(1) + DTI(1)                       INTEG
H(2) = H(2) + DTI(2)                       INTEG
H(3) = H(3) + DTI(3)                       INTEG
193 CONTINUE                               INTEG
H1PRIM(1) = AONE(5)                        INTEG
G3 = AONE(6)                                INTEG
G4 = AONE(7)                                INTEG
*****
*
*
*
*****
```

THIS SEGMENT SIMPLY CALCULATES THE GIMBAL ANGLE RATES OF BODIES ONE, THREE, AND FOUR. THAT IS TO SAY THE SUBSTITUTION NEEDED BY INTEGRATION BLOCK TWO IS DONE AT THIS POINT.

```
TT1DOT = OMEGA1
TT3DOT = OMEGA3
TT4DOT = OMEGA4
```

THIS IS THE ENTRY POINT TO INTEGRATION BLOCK TWO. THE PURPOSE OF THE BLOCK IS TO CALL AN INTEGRATION SUBROUTINE TO INTEGRATE THE GIMBAL ANGLE RATES OF BODIES ONE, THREE, AND FOUR TO PRODUCE THE CORRESPONDING GIMBAL ANGLE POSITIONS. AS BEFORE, THE ARRAYS USED BY THE INTEGRATION SUBROUTINE MUST BE CALCULATED EACH TIME BEFORE CALLING THE INTEGRATION SUBROUTINE.

```
ATWO(1) = TIME                              INTEG
BTWO(1) = DELTAT                            INTEG
BTWO(2) = TT1DOT                           INTEG
BTWO(3) = TT3DOT                           INTEG
BTWO(4) = TT4DOT                           INTEG
CALL FOMS(ATWO,BTWO,4,FLAG2,TJ2)           INTEG
THETA1 = ATWO(2)                            INTEG
THETA3 = ATWO(3)                            INTEG
THETA4 = ATWO(4)                            INTEG
*****
*
*
*
*****
```

C
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C

*

THIS IS THE ENTRY POINT TO THE QUATERNION BLOCK.

```

Q(1,1) = 0.
Q(1,2) = -0.5*W0(1)
Q(1,3) = -0.5*W0(2)
Q(1,4) = -0.5*W0(3)
Q(2,1) = -Q(1,2)
Q(2,2) = 0.
Q(2,3) = -Q(1,4)
Q(2,4) = Q(1,3)
Q(3,1) = -Q(1,3)
Q(3,2) = Q(1,4)
Q(3,3) = 0.
Q(3,4) = -Q(1,2)
Q(4,1) = -Q(1,4)
Q(4,2) = -Q(1,3)
Q(4,3) = Q(1,2)
Q(4,4) = 0.

```

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```

AED(2) = Q(1,1)*AE(2) + Q(1,2)*AE(3) + Q(1,3)*AE(4) + Q(1,4)*AE(5)
AED(3) = Q(2,1)*AE(2) + Q(2,2)*AE(3) + Q(2,3)*AE(4) + Q(2,4)*AE(5)
AED(4) = Q(3,1)*AE(2) + Q(3,2)*AE(3) + Q(3,3)*AE(4) + Q(3,4)*AE(5)
AED(5) = Q(4,1)*AE(2) + Q(4,2)*AE(3) + Q(4,3)*AE(4) + Q(4,4)*AE(5)

```

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SET UP MATRICES USED BY THE INTEGRATION SUBROUTINE

```

ATHREE(1) = TIME
BTHREE(1) = DELTAT
BTHREE(2) = AED(2)
BTHREE(3) = AED(3)
BTHREE(4) = AED(4)
BTHREE(5) = AED(5)
CALL FOMS(ATHREE,BTHREE,5,FLAG3,TJ3)
AE(2) = ATHREE(2)
AE(3) = ATHREE(3)
AE(4) = ATHREE(4)
AE(5) = ATHREE(5)

```

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CALCULATE THE NORMALIZING FACTOR.

```

FN = SQRT( AE(2)**2 + AE(3)**2 + AE(4)**2 + AE(5)**2 )
AE(2) = AE(2)/FN
AE(3) = AE(3)/FN
AE(4) = AE(4)/FN
AE(5) = AE(5)/FN
T(1,1) = AE(2)**2 + AE(3)**2 - AE(4)**2 - AE(5)**2
T(1,2) = 2.*(AE(3)*AE(4) - AE(2)*AE(5))
T(1,3) = 2.*(AE(3)*AE(5) + AE(2)*AE(4))
T(2,1) = 2.*(AE(3)*AE(4) + AE(2)*AE(5))
T(2,2) = AE(2)**2 - AE(3)**2 + AE(4)**2 - AE(5)**2
T(2,3) = 2.*(AE(4)*AE(5) - AE(2)*AE(3))
T(3,1) = 2.*(AE(3)*AE(5) - AE(2)*AE(4))
T(3,2) = 2.*(AE(4)*AE(5) + AE(2)*AE(3))
T(3,3) = AE(2)**2 - AE(3)**2 - AE(4)**2 + AE(5)**2
CALL MULT(DUM,DUM,DUM,TIBO,TIBOI,T,2)
CALL MULT(HI,TIBO,H,DUM,DUM,DUM,1)

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*

THIS IS THE ENTRY POINT TO CONTM

CONTM
CONTM


```

WRITE(6,6590) TBP
212 CONTINUE
IF (NUMCMG .EQ. 0) GO TO 214
DO 213 J=1,NUMCMG
WRITE(6,6028) J,THATA(J),J,THATAD(J)
IF (IDOF(J) .NE. 2) GO TO 213
WRITE(6,6032) J,FEE(J),J,FEED(J)
213 CONTINUE
214 CONTINUE
IPNTCK = 0
215 IPNTCK = IPNTCK + 1

```

```

OUTPL
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```

```

C
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```

*****
*
*
*****
IF (IDOCK .NE. 1) GO TO 220
IF ((TIME.LT.DCHMIN).OR.(TIME.GT.DCHMAX)) GO TO 220
DO 218 M=1,3
DO 218 N=1,3
BODYOI(M,N) = BODYDI(M,N)
218 CONTINUE
BOMASS = BDMASS
DO1(1) = DD01(1)
DO1(2) = DD01(2)
DO1(3) = DD01(3)
TOTMAS = BOMASS + B1MASS + B2MASS + B3MASS + B4MASS
GO TO 190
220 IF (TIME.GT.TSTOP) GO TO 10
GO TO 190

```

```

C
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```

THIS SECTION CONTAINS ALL OF THE INPUT AND OUTPUT FORMATS.

```

5000 FORMAT(1X,I2)
5002 FORMAT(1X,3(F11.5,2X))
5004 FORMAT(1X,E11.4)
5006 FORMAT(1X,F11.5)
5008 FORMAT(1X,E11.4,2X,E11.4)
6000 FORMAT(1H1,1X,16H THERE ARE (IS) ,I2,22H DATA DECK(S) PRESENT.)
6002 FORMAT(1H1,1X,14HTSTART = ,E13.6,23X,14HTSTOP = ,E13.6,
* 23X,14HDELTA = ,E13.6)
6004 FORMAT(1X,14HALTITUDE = ,E13.6)
6006 FORMAT(1X,6HTIBOI(,I1,7H,1) = ,F11.5,25X,6HTIBOI(,I1,7H,2) = ,
* F11.5,25X,6HTIBOI(,I1,7H,3) = ,F11.5)
6008 FORMAT(1X,14HWO(1) = ,E13.6,23X,14HWO(2) = ,E13.6,23X,
* 14HWO(3) = ,E13.6)
6010 FORMAT(1X,1HB,I1,12HMASS = ,E13.6)
6012 FORMAT(1X,7HBODYOI(,I1,6H,1) = ,E13.6,23X,7HBODYOI(,I1,6H,2) = ,
* E13.6,23X,7HBODYOI(,I1,6H,3) = ,E13.6)
6014 FORMAT(1X,14HNUMCMG = ,I2)
6016 FORMAT(1X,11HCMG NUMBER ,I1,21H IS A REACTION WHEEL.)
6018 FORMAT(1X,11HCMG NUMBER ,I1,26H HAS ONE DEGREE OF FREEDOM)
6020 FORMAT(1X,11HCMG NUMBER ,I1,27H HAS TWO DEGREES OF FREEDOM)
6022 FORMAT(1X,35HTHE ANGULAR MOMENTUM OF CMG NUMBER ,I1,3H = ,E13.6)
6024 FORMAT(1X,5SHAOCJ(,I1,1H,;I1,6H,1) = ,F11.5,25X,5SHAOCJ(,I1,1H,;I1,
* 6H,2) = ,F11.5,25X,5SHAOCJ(,I1,1H,;I1,6H,3) = ,F11.5)

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6026 FORMAT(1X,4HAI1(,I1,1H,1) = ,E13.6,23X,4HAI1(,I1,1H,1, I/O
* 7H,2) = ,E13.6,23X,4HAI1(,I1,1H,1,7H,3) = ,E13.6) I/O
6028 FORMAT(1X,6HTHATA(,I1,7H) = ,E13.6,23X,7HTHATA(,I1,6H) = , I/O
* E13.6) I/O
6030 FORMAT(1X,4HAI0(,I1,1H,1) = ,E13.6,23X,4HAI0(,I1,1H,1, I/O
* 7H,2) = ,E13.6,23X,4HAI0(,I1,1H,1,7H,3) = ,E13.6) I/O
6032 FORMAT(1X,4HFEE(,I1,9H) = ,E13.6,23X,5HFEE(,I1,8H) = , I/O
* E13.6) I/O
6040 FORMAT(1X,7HBODY1I(,I1,6H,1) = ,E13.6,23X,7HBODY1I(,I1,6H,2) = , I/O
* E13.6,23X,7HBODY1I(,I1,6H,3) = ,E13.6) I/O
6042 FORMAT(1X,14HTHETA1 = ,E13.6,23X,14HOMEGA1 = ,E13.6) I/O
6044 FORMAT(1X,14HD01(1) = ,E13.6,23X,14HD01(2) = ,E13.6, I/O
* 23X,14HD01(3) = ,E13.6) I/O
6048 FORMAT(1X,14HD13(1) = ,E13.6,23X,14HD13(2) = ,E13.6, I/O
* 23X,14HD13(3) = ,E13.6) I/O
6050 FORMAT(1X,14HD14(1) = ,E13.6,23X,14HD14(2) = ,E13.6, I/O
* 23X,14HD14(3) = ,E13.6) I/O
6052 FORMAT(1X,1HS,I1,12H(1) = ,E13.6,23X,1HS,I1,12H(2) = ,I/O
*E13.6,23X,1HS,I1,12H(3) = ,E13.6) I/O
6058 FORMAT(1X,14HPEND3L = ,E13.6) I/O
6060 FORMAT(1X,14HTHETA3 = ,E13.6) I/O
6062 FORMAT(1X,14HOMEGA3 = ,E13.6) I/O
6064 FORMAT(1X,14HPEND4L = ,E13.6) I/O
6066 FORMAT(1X,14HTHETA4 = ,E13.6,23X,14HOMEGA4 = ,E13.6) I/O
6068 FORMAT(1X,14HIDOCK = ,I2) I/O
6070 FORMAT(1X,14HDTIME = ,E13.6) I/O
6072 FORMAT(1X,14HIPROPF = ,I2) I/O
6074 FORMAT(1X,4HA0J(,I2,8H) = ,E13.6,23X,7HCGAIN0(,I2,5H) = , I/O
* E13.6) I/O
6076 FORMAT(1X,4HA1J(,I1,9H) = ,E13.6,23X,7HCGAIN1(,I1,6H) = , I/O
* E13.6) I/O
6078 FORMAT(1X,14HIGRAVF = ,I2) I/O
6080 FORMAT(1X,14HSP = ,E13.6) I/O
6082 FORMAT(1H1,1X,9HIPNDLM = ,I2,/) I/O
6500 FORMAT(1H1,1X,46H THE FOLLOWING INPUT CORRESPONDS TO DATA DECK ,I2I/O
*) I/O
6502 FORMAT(1H1,1X,127H*****I/O
*****I/O
*****I/O
*****,/) I/O
6504 FORMAT(1X,14HTIME = ,F11.5,/) I/O
6506 FORMAT(1X,1HW,I1,12H(1) = ,E13.6,23X,1HW,I1,12H(2) = ,I/O
*E13.6,23X,1HW,I1,12H(3) = ,E13.6) I/O
6510 FORMAT(1X,14HH(1) = ,E13.6,23X,14HH(2) = ,E13.6, I/O
* 23X,14HH(3) = ,E13.6) I/O
6512 FORMAT(1X,14HMI(1) = ,E13.6,23X,14HMI(2) = ,E13.6, I/O
* 23X,14HMI(3) = ,E13.6) I/O
6514 FORMAT(1X,14HHDOT(1) = ,E13.6,23X,14HHDOT(2) = ,E13.6, I/O
* 23X,14HHDOT(3) = ,E13.6) I/O
6516 FORMAT(1X,1HH,I1,12HPRIM(1) = ,E13.6,23X,1HH,I1,12HPRIM(2) = ,I/O
*E13.6,23X,1HH,I1,12HPRIM(3) = ,E13.6) I/O
6522 FORMAT(1X,2HEL,I1,11H(1) = ,E13.6,23X,2HEL,I1,11H(2) = ,I/O
*E13.6,23X,2HEL,I1,11H(3) = ,E13.6) I/O
6524 FORMAT(1X,2HEL,I1,11HDOT(1) = ,E13.6,23X,2HEL,I1,11HDOT(2) = ,I/O
*E13.6,23X,2HEL,I1,11HDOT(3) = ,E13.6) I/O
6526 FORMAT(1X,1HR,I1,12H(1) = ,E13.6,23X,1HR,I1,12H(2) = ,I/O
*E13.6,23X,1HR,I1,12H(3) = ,E13.6) I/O
6528 FORMAT(1X,1HR,I1,12HDOT(1) = ,E13.6,23X,1HR,I1,12HDOT(2) = ,I/O
*E13.6,23X,1HR,I1,12HDOT(3) = ,E13.6) I/O
6535 FORMAT(1X,14HD12(1) = ,E13.6,23X,14HD12(2) = ,E13.6, I/O
* 23X,14HD12(3) = ,E13.6) I/O
6536 FORMAT(1X,14HTHETO = ,F11.5,25X,14HTOTMAS = ,E13.6,/) I/O
6538 FORMAT(1X,5HTIB0(,I1,8H,1) = ,F11.5,25X,5HTIB0(,I1,8H,2) = , I/O

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*F11.5,25X,5HTIB0(,I1,8H,3) = ,F11.5)
6544 FORMAT(1X,14HIPRINT = ,I2)
6546 FURMAT(1X,14HIB2F = ,I2)
6548 FURMAT(1X,14HS = ,E13.6,23X,14HSDOT = ,E13.6)
6550 FORMAT(1X,19HGENERAL INFORMATION,/)
6552 FURMAT(1X,5HBODY ,I1,12M INFORMATION,/)
6554 FORMAT(/)
6556 FORMAT(1X,14HS = ,E13.6,23X,14HSDOT = ,E13.6)
6558 FURMAT(1X,5HTHETA,I1,8H = ,E13.6,23X,5HOMEGA,I1,8H = ,
* E13.6)
6560 FORMAT(1X,1HG,I1,12H = ,E13.6,23X,1HG,I1,12HDOT = ,
* E13.6)
6562 FORMAT(1X,14HIATTIF = ,I1)
6564 FORMAT(1X,14HCA(1) = ,E13.6,23X,14HCA(2) = ,E13.6,
* 23X,14HCA(3) = ,E13.6)
6566 FORMAT(1X,14HAA01 = ,E13.6,23X,14HAGAIN1 = ,E13.6)
6568 FORMAT(1X,14HAA02 = ,E13.6,23X,14HAGAIN2 = ,E13.6)
6570 FORMAT(1X,14HNGAIN = ,I2)
6572 FURMAT(1X,5HGAIN(,I1,8H) = ,E13.6)
6574 FORMAT(1X,14HBDMASS = ,E13.6)
6576 FORMAT(1X,7HBODYDI(,I1,6H,1) = ,E13.6,23X,7HBODYDI(,I1,6H,2) = ,
* E13.6,23X,7HBODYDI(,I1,6H,3) = ,E13.6)
6578 FORMAT(1X,14HDTI(1) = ,E13.6,23X,14HDTI(2) = ,E13.6,
* 23X,14HDTI(3) = ,E13.6)
6580 FORMAT(1X,20HDOCKING HAS OCCURRED)
6582 FORMAT(1X,14HCP1 = ,E13.6)
6584 FURMAT(1X,14HCP2 = ,E13.6)
6586 FURMAT(1X,14HDD01(1) = ,E13.6,23X,14HDD01(2) = ,E13.6,
* 23X,14HDD01(3) = ,E13.6)
6588 FORMAT(1X,54HTHE TOTAL PROPULSION IMPULSE ON THE TRANSVERSE AXIS =I/O
* ,E13.6)
6590 FORMAT(1X,48HTHE TOTAL PROPULSION IMPULSE ON THE SPIN AXIS = ,
* E13.6)

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END

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SUBROUTINE ATT

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*****
COMMON      A (3)          ,          AE (5)          ,          AED (5)          ,          COMMC
*           AF0UR (2)      ,          AII (6,3,3)     ,          ,          COMMC
*           AIO (6,3,3)    ,          AJ1 (3)        ,          ALT          ,          COMMC
*           AOCJ (6,3,3)   ,          AOJ (3)        ,          AONE (7)       ,          COMMC
*           ATCPT2 (3,3)   ,          ATHREE (5)     ,          ATWO (4)       ,          COMMC
*           A1 (3,3)       ,          AIJ (2)        ,          ,          COMMC
COMMON      BDMASS        ,          BFOUR (2)        ,          BMOM          ,          COMMC
*           BODYDI (3,3)   ,          BODYOI (3,3)    ,          BODY1I (3,3)   ,          COMMC
*           BOMASS        ,          BONE (7)         ,          BTHREE (5)     ,          COMMC
*           BTWO (4)       ,          B1MASS          ,          B2MASS         ,          COMMC
*           B3MASS        ,          B4MASS          ,          ,          COMMC
COMMON      CA (3)        ,          CB (3)          ,          CGAINO (3)     ,          COMMC
*           CGAIN1 (2)     ,          ,          ,          COMMC
*           COSFEJ        ,          COSTTJ         ,          COSTTO        ,          COMMC
*           COSTT1        ,          COSTT3         ,          COSTT4        ,          COMMC
*           CO2T          ,          CP1            ,          CP2           ,          COMMC
*           CST           ,          C1              ,          ,          COMMC
COMMON      DB (3)        ,          DD01 (3)        ,          ,          COMMC
*           DELTAT        ,          D01 (3)         ,          D01DOT (3)     ,          COMMC
*           DTI (3)       ,          ,          ,          COMMC
*           DTIME        ,          D12 (3)         ,          D13 (3)        ,          COMMC
*           D13DOT (3)    ,          D13YCS         ,          D13YSN        ,          COMMC
*           D13ZCS       ,          D13ZSN         ,          D14 (3)        ,          COMMC
*           D14DOT (3)    ,          D14YCS         ,          D14YSN        ,          COMMC
*           D14ZCS       ,          D14ZSN         ,          ,          COMMC
COMMON      EEE (3,3)    ,          EEJ (3,3)       ,          EL2 (3)        ,          COMMC
*           EL2DOT (3)    ,          EL2YCS         ,          EL2YSN        ,          COMMC
*           EL2ZCS       ,          EL2ZSN         ,          EL3 (3)        ,          COMMC
*           EL3DOT (3)    ,          EL3YCS         ,          EL3YSN        ,          COMMC
*           EL3ZCS       ,          EL3ZSN         ,          EL4 (3)        ,          COMMC
*           EL4DOT (3)    ,          EL4YCS         ,          EL4YSN        ,          COMMC
*           EL4ZCS       ,          EL4ZSN         ,          EM (6,6)      ,          COMMC
COMMON      FAT (8)      ,          ,          ,          COMMC
*           FEE (6)       ,          FEED (6)       ,          FFF (3)        ,          COMMC
*           FFJ (3)       ,          FLAG1          ,          FLAG2         ,          COMMC
*           FLAG3        ,          FLAG4          ,          FNI           ,          COMMC
*           FO (3)        ,          FO1 (3)        ,          FO2 (3)       ,          COMMC
*           FO3 (3)       ,          F1 (3)         ,          F11 (3)       ,          COMMC
*           FPT (5)       ,          ,          ,          COMMC
*           F12 (3)       ,          F13 (3)        ,          ,          COMMC
COMMON      GAIN (10)    ,          G3              ,          ,          COMMC
*           G3DOT        ,          G4              ,          G4DOT         ,          COMMC
COMMON      H (3)        ,          HCMG (3)       ,          HDOT (3)      ,          COMMC
*           HI (3)        ,          HO (3)         ,          HW (6)         ,          COMMC
*           H1 (3)        ,          HIPDOT (3)     ,          HIPRIM (3)    ,          COMMC
*           HIPRIM (3)    ,          H4PRIM (3)     ,          ,          COMMC
COMMON      IBZF         ,          ICFA           ,          ICFB          ,          COMMC
*           ICFC         ,          ICFD           ,          IDOCK         ,          COMMC
*           IDOF (6)     ,          ,          ,          COMMC
*           IGRAVF       ,          IPNDLM         ,          IPNTCK        ,          COMMC
*           IPRINT      ,          IPROPF         ,          ,          COMMC
COMMON      NCASE       ,          NCHECK         ,          NDECK         ,          COMMC
*           NGAIN        ,          NUMCMG         ,          ,          COMMC
COMMON      OMEGA1      ,          OMEGA3         ,          OMEGA4        ,          COMMC
COMMON      PEND3L      ,          PEND4L         ,          ,          COMMC
COMMON      Q (4,4)     ,          ,          ,          COMMC

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C
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SUBROUTINE CMG

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*
*
*****
COMMON      A(3)          9          AE(5)          9          AED(5)          9  COMMC
*           AF0UR(2)      9          AII(6,3,3)     9          COMMC
*           AIO(6,3,3)    9          AJ1(3)         9          ALIT           9  COMMC
*           AOCJ(6,3,3)  9          AOJ(3)         9          AONE(7)        9  COMMC
*           ATCPT2(3,3)  9          ATHREE(5)     9          ATWO(4)        9  COMMC
*           A1(3,3)      9          A1J(2)         9          COMMC
* COMMON     BDMASS       9          BFOUR(2)      9          BMOM           9  COMMC
*           BODYDI(3,3)  9          BODYOI(3,3)   9          BODY1I(3,3)   9  COMMC
*           BOMASS       9          BONE(7)        9          BTHREE(5)      9  COMMC
*           BTWO(4)      9          B1MASS         9          B2MASS         9  COMMC
*           B3MASS       9          B4MASS         9          COMMC
* COMMON     CA(3)        9          CB(3)          9          CGAINO(3)      9  COMMC
*           CGAIN1(2)    9          COMMC
*           COSFEJ       9          COSTTJ        9          COSTTO         9  COMMC
*           COSTT1       9          COSTT3        9          COSTT4         9  COMMC
*           CO2T         9          CP1           9          CPR            9  COMMC
*           CST          9          C1            9          COMMC
* COMMON     DB(3)        9          DDO1(3)       9          COMMC
*           DELTAT       9          DO1(3)        9          DD1DOT(3)      9  COMMC
*           DTI(3)       9          COMMC
*           DTIME        9          D12(3)        9          D13(3)         9  COMMC
*           D13DOT(3)    9          D13YCS        9          D13YSN         9  COMMC
*           D13ZCS       9          D13ZSN        9          D14(3)         9  COMMC
*           D14DOT(3)    9          D14YCS        9          D14YSN         9  COMMC
*           D14ZCS       9          D14ZSN        9          COMMC
* COMMON     EEE(3,3)    9          EEJ(3,3)     9          EL2(3)         9  COMMC
*           EL2DOT(3)    9          EL2YCS        9          EL2YSN         9  COMMC
*           EL2ZCS       9          EL2ZSN        9          EL3(3)         9  COMMC
*           EL3DOT(3)    9          EL3YCS        9          EL3YSN         9  COMMC
*           EL3ZCS       9          EL3ZSN        9          EL4(3)         9  COMMC
*           EL4DOT(3)    9          EL4YCS        9          EL4YSN         9  COMMC
*           EL4ZCS       9          EL4ZSN        9          EM1(6,6)       9  COMMC
* COMMON     FAT(8)      9          COMMC
*           FEE(6)       9          FEED(6)       9          FFF(3)         9  COMMC
*           FFJ(3)       9          FLAG1         9          FLAG2         9  COMMC
*           FLAG3       9          FLAG4         9          FNI           9  COMMC
*           FO(3)        9          FO1(3)        9          FO2(3)         9  COMMC
*           FO3(3)       9          F1(3)         9          F11(3)         9  COMMC
*           FPT(5)       9          COMMC
*           F12(3)       9          F13(3)        9          COMMC
* COMMON     GAIN(10)    9          G3            9          COMMC
*           G3DOT       9          G4            9          G4DOT         9  COMMC
* COMMON     H(3)        9          HCMG(3)       9          HDOT(3)        9  COMMC
*           HI(3)        9          HO(3)         9          HW(6)         9  COMMC
*           H1(3)        9          H1PDOT(3)     9          H1PRIM(3)      9  COMMC
*           H3PRIM(3)    9          H4PRIM(3)     9          COMMC
* COMMON     IB2F        9          ICFA          9          ICFB           9  COMMC
*           ICFC         9          ICFD          9          IDOCK         9  COMMC
*           IDOF(6)      9          COMMC
*           IGRAVF       9          IPNDLM        9          IPNTCK        9  COMMC
*           IPRINT       9          IPROPF        9          COMMC
* COMMON     NCASE       9          NCHECK        9          NDECK         9  COMMC
*           NGAIN        9          NUMCMG        9          COMMC
* COMMON     OMEGA1      9          OMEGA3        9          OMEGA4         9  COMMC
* COMMON     PEND3L     9          PEND4L        9          COMMC
* COMMON     Q(4,4)     9          COMMC

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COMMON      R          *          RO(3)          *          R1(3)          *          COMMC
*          RIDOT(3)      *          R1YCS          *          R1YSN          *          COMMC
*          R1ZCS          *          R1ZSN          *          R2(3)          *          COMMC
*          R2DOT(3)      *          R2YCS          *          R2YSN          *          COMMC
*          R2ZCS          *          R2ZSN          *          R3(3)          *          COMMC
*          R3DOT(3)      *          R3YCS          *          R3YSN          *          COMMC
*          R3ZCS          *          R3ZSN          *          R4(3)          *          COMMC
*          R4DOT(3)      *          R4YCS          *          R4YSN          *          COMMC
*          R4ZCS          *          R4ZSN          *          COMMC
COMMON      S          *          SDOT          *          SINFEJ          *          COMMC
*          SINTTJ          *          SINTT0          *          SINTT1          *          COMMC
*          SINTT2          *          SINTT3          *          SINTT4          *          COMMC
*          SP              *          SUM1            *          SUM2            *          COMMC
*          SUM3            *          S2(3)           *          S3(3)           *          COMMC
*          S4(3)           *          COMMC
COMMON      T(3,3)      *          TC(3,3)        *          TEMP1(3)        *          COMMC
*          TEMP2(3)        *          COMMC
*          TEMP3(3)        *          TEMP4(3)        *          TEMP5(3,3)      *          COMMC
*          TEMP6(3,3)      *          TEMP7(3,3)      *          TEMP8(3,3)      *          COMMC
*          TEMP9(3,3)      *          TEMP10(3,3)     *          TEMP11(3,3)     *          COMMC
*          TEMP12(3,3)     *          TEMP13(3,3)     *          TEMP14(3,3)     *          COMMC
*          TEMP15(3,3)     *          TERM1(3)        *          TERM2(3)        *          COMMC
*          TFRICT          *          THATA(6)         *          THATAD(6)       *          COMMC
*          THETA1          *          THETA3          *          THETA4          *          COMMC
*          THETA          *          TIB0(3,3)        *          TIB01(3,3)      *          COMMC
*          TIME           *          TJ              *          TJ1(10)          *          COMMC
*          TJ2(10)         *          TJ3(10)          *          TJ4(10)          *          COMMC
*          TOTOR          *          COMMC
*          TOEF(3)         *          TOTMAS          *          TOL              *          COMMC
*          TQOG(3)         *          TQOP(3)          *          TQ1G(3)          *          COMMC
*          TQ1P(3)         *          TSTART          *          TSTOP           *          COMMC
*          TT1DOT         *          TT3DOT          *          TT4DOT           *          COMMC
*          T1EF(3)         *          T13              *          T14              *          COMMC
COMMON      V(3)        *          COMMC
COMMON      W0(3)        *          WS              *          W1(3)            *          COMMC
*          W3(3)          *          W4(3)            *          COMMC
COMMON      X(6,7)       *          XC              *          XCDOT            *          COMMC
*          XMU            *          COMMC

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C
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FFF(1) = 0.          CMG
FFF(2) = 0.          CMG
FFF(3) = 0.          CMG
DO 5 M=1,3           CMG
DO 5 N=1,3           CMG
EEE(M,N) = 0.        CMG
5 CONTINUE           CMG
J = 0                CMG
10 J = J + 1         CMG
IF(J .GT. NUMCMG) RETURN CMG
IF(IDOF(J) .NE. 0) GO TO 20 CMG
FFJ(1) = AOCJ(J,1,3)*HW(J) CMG
FFJ(2) = AOCJ(J,2,3)*HW(J) CMG
FFJ(3) = AOCJ(J,3,3)*HW(J) CMG
DO 15 M=1,3         CMG
DO 15 N=1,3         CMG
EEJ(M,N) = 0.        CMG

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15 CONTINUE
GO TO 65
20 IF (IDOF(J) .NE. 1) GO TO 35
SINTTJ = SIN(THATA(J))
COSTTJ = COS(THATA(J))
SINFEJ = SIN(FEE(J))
COSFEJ = COS(FEE(J))
TEMP12(1) = COSTTJ*AII(J,1,2)*THATAD(J)
*
*   +SINTTJ*AII(J,3,2)*THATAD(J) + HW(J)*SINTTJ
TEMP12(2) = SINFEJ*SINTTJ*AII(J,1,2)*THATAD(J)
*
*   +COSFEJ*AII(J,2,2)*THATAD(J)
*
*   -SINFEJ*COSTTJ*AII(J,3,2)*THATAD(J)
TEMP12(3) = -SINTTJ*COSFEJ*AII(J,1,2)*THATAD(J)
*
*   +SINFEJ*AII(J,2,2)*THATAD(J)
*
*   +COSFEJ*COSTTJ*AII(J,3,2)*THATAD(J) + HW(J)*COSTTJ
DO 22 M=1,3
FFJ(M) = AOCJ(J,M,1)*TEMP12(1) + AOCJ(J,M,2)*TEMP12(2)
*
*   +AOCJ(J,M,3)*TEMP12(3)
22 CONTINUE
TEMP13(1,1) = COSTTJ*AOCJ(J,1,1) + SINFEJ*SINTTJ*AOCJ(J,1,2)
*
*   -SINTTJ*COSFEJ*AOCJ(J,1,3)
TEMP13(1,2) = COSTTJ*AOCJ(J,2,1) + SINFEJ*SINTTJ*AOCJ(J,2,2)
*
*   -SINTTJ*COSFEJ*AOCJ(J,2,3)
TEMP13(1,3) = COSTTJ*AOCJ(J,3,1) + SINFEJ*SINTTJ*AOCJ(J,3,2)
*
*   -SINTTJ*COSFEJ*AOCJ(J,3,3)
TEMP13(2,1) = COSFEJ*AOCJ(J,1,2) + SINFEJ*AOCJ(J,1,3)
TEMP13(2,2) = COSFEJ*AOCJ(J,2,2) + SINFEJ*AOCJ(J,2,3)
TEMP13(2,3) = COSFEJ*AOCJ(J,3,2) + SINFEJ*AOCJ(J,3,3)
TEMP13(3,1) = SINTTJ*AOCJ(J,1,1) - SINFEJ*COSTTJ*AOCJ(J,1,2)
*
*   +COSFEJ*COSTTJ*AOCJ(J,1,3)
TEMP13(3,2) = SINTTJ*AOCJ(J,2,1) - SINFEJ*COSTTJ*AOCJ(J,2,2)
*
*   +COSFEJ*COSTTJ*AOCJ(J,2,3)
TEMP13(3,3) = SINTTJ*AOCJ(J,3,1) - SINFEJ*COSTTJ*AOCJ(J,3,2)
*
*   +COSFEJ*COSTTJ*AOCJ(J,3,3)
DO 25 M=1,3
DO 25 N=1,3
TEMP14(M,N) = AII(J,M,1)*TEMP13(1,N) + AII(J,M,2)*TEMP13(2,N)
*
*   +AII(J,M,3)*TEMP13(3,N)
25 CONTINUE
TEMP15(1,1) = COSTTJ*TEMP14(1,1) + SINTTJ*TEMP14(3,1)
TEMP15(1,2) = COSTTJ*TEMP14(1,2) + SINTTJ*TEMP14(3,2)
TEMP15(1,3) = COSTTJ*TEMP14(1,3) + SINTTJ*TEMP14(3,3)
TEMP15(2,1) = SINFEJ*SINTTJ*TEMP14(1,1) + COSFEJ*TEMP14(2,1)
*
*   -SINFEJ*COSTTJ*TEMP14(3,1)
TEMP15(2,2) = SINFEJ*SINTTJ*TEMP14(1,2) + COSFEJ*TEMP14(2,2)
*
*   -SINFEJ*COSTTJ*TEMP14(3,2)
TEMP15(2,3) = SINFEJ*SINTTJ*TEMP14(1,3) + COSFEJ*TEMP14(2,3)
*
*   -SINFEJ*COSTTJ*TEMP14(3,3)
TEMP15(3,1) = -SINTTJ*COSFEJ*TEMP14(1,1) + SINFEJ*TEMP14(2,1)
*
*   +COSFEJ*COSTTJ*TEMP14(3,1)
TEMP15(3,2) = -SINTTJ*COSFEJ*TEMP14(1,2) + SINFEJ*TEMP14(2,2)
*
*   +COSFEJ*COSTTJ*TEMP14(3,2)
TEMP15(3,3) = -SINTTJ*COSFEJ*TEMP14(1,3) + SINFEJ*TEMP14(2,3)
*
*   +COSFEJ*COSTTJ*TEMP14(3,3)
DO 30 M=1,3
DO 30 N=1,3
EEJ(M,N) = AOCJ(J,M,1)*TEMP15(1,N) + AOCJ(J,M,2)*TEMP15(2,N)
*
*   +AOCJ(J,M,3)*TEMP15(3,N)
30 CONTINUE
GO TO 60
35 CONTINUE
SINTTJ = SIN(THATA(J))

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COSTTJ = COS(THATA(J))
SINFEJ = SIN(FEE(J))
COSFEJ = COS(FEE(J))
TEMP1(1) = AIO(J,1,1)*FEED(J)
TEMP1(2) = COSFEJ*AIO(J,2,1)*FEED(J) - SINFEJ*AIO(J,3,1)*FEED(J)
TEMP1(3) = SINFEJ*AIO(J,2,1)*FEED(J) + COSFEJ*AIO(J,3,1)*FEED(J)
TEMP2(1) = COSTTJ*(AII(J,1,1)*COSTTJ*FEED(J) + AII(J,1,2)*THATAD(J) +
* AII(J,1,3)*SINTTJ*FEED(J)) + SINTTJ*(AII(J,3,1)*COSTTJ*FEED(J) +
* AII(J,3,2)*THATAD(J) + AII(J,3,3)*SINTTJ*FEED(J))
TEMP2(2) = SINFEJ*SINTTJ*(AII(J,1,1)*COSTTJ*FEED(J) +
* AII(J,1,2)*THATAD(J) + AII(J,1,3)*SINTTJ*FEED(J)) +
* COSFEJ*(AII(J,2,1)*COSTTJ*FEED(J) + AII(J,2,2)*THATAD(J) +
* AII(J,2,3)*SINTTJ*FEED(J)) -
* SINFEJ*COSTTJ*(AII(J,3,1)*COSTTJ*FEED(J) + AII(J,3,2)*THATAD(J) +
* AII(J,3,3)*SINTTJ*FEED(J))
TEMP2(3) = -SINTTJ*COSFEJ*(AII(J,1,1)*COSTTJ*FEED(J) +
* AII(J,1,2)*THATAD(J) + AII(J,1,3)*SINTTJ*FEED(J)) +
* SINFEJ*(AII(J,2,1)*COSTTJ*FEED(J) + AII(J,2,2)*THATAD(J) +
* AII(J,2,3)*SINTTJ*FEED(J)) +
* COSFEJ*COSTTJ*(AII(J,3,1)*COSTTJ*FEED(J) + AII(J,3,2)*THATAD(J) +
* AII(J,3,3)*SINTTJ*FEED(J))
TEMP3(1) = HW(J)*SINTTJ
TEMP3(2) = HW(J)*COSTTJ*SINFEJ
TEMP3(3) = HW(J)*COSTTJ*COSFEJ
TEMP4(1) = TEMP1(1) + TEMP2(1) + TEMP3(1)
TEMP4(2) = TEMP1(2) + TEMP2(2) + TEMP3(2)
TEMP4(3) = TEMP1(3) + TEMP2(3) + TEMP3(3)
FFJ(1) = AOCJ(J,1,1)*TEMP4(1)
* AOCJ(J,1,2)*TEMP4(2) + AOCJ(J,1,3)*TEMP4(3)
FFJ(2) = AOCJ(J,2,1)*TEMP4(1)
* AOCJ(J,2,2)*TEMP4(2) + AOCJ(J,2,3)*TEMP4(3)
FFJ(3) = AOCJ(J,3,1)*TEMP4(1)
* AOCJ(J,3,2)*TEMP4(2) + AOCJ(J,3,3)*TEMP4(3)
TEMP5(1,1) = AOCJ(J,1,1)
TEMP5(1,2) = AOCJ(J,2,1)
TEMP5(1,3) = AOCJ(J,3,1)
TEMP5(2,1) = COSFEJ*AOCJ(J,1,2) + SINFEJ*AOCJ(J,1,3)
TEMP5(2,2) = COSFEJ*AOCJ(J,2,2) + SINFEJ*AOCJ(J,2,3)
TEMP5(2,3) = COSFEJ*AOCJ(J,3,2) + SINFEJ*AOCJ(J,3,3)
TEMP5(3,1) = -SINFEJ*AOCJ(J,1,2) + COSFEJ*AOCJ(J,1,3)
TEMP5(3,2) = -SINFEJ*AOCJ(J,2,2) + COSFEJ*AOCJ(J,2,3)
TEMP5(3,3) = -SINFEJ*AOCJ(J,3,2) + COSFEJ*AOCJ(J,3,3)
DO 40 M=1,3
DO 40 N=1,3
TEMP6(M,N) = AIO(J,M,1)*TEMP5(1,N) + AIO(J,M,2)*TEMP5(2,N)
* AIO(J,M,3)*TEMP5(3,N)
40 CONTINUE
TEMP7(1,1) = TEMP6(1,1)
TEMP7(1,2) = TEMP6(1,2)
TEMP7(1,3) = TEMP6(1,3)
TEMP7(2,1) = COSFEJ*TEMP6(2,1) - SINFEJ*TEMP6(3,1)
TEMP7(2,2) = COSFEJ*TEMP6(2,2) - SINFEJ*TEMP6(3,2)
TEMP7(2,3) = COSFEJ*TEMP6(2,3) - SINFEJ*TEMP6(3,3)
TEMP7(3,1) = SINFEJ*TEMP6(2,1) + COSFEJ*TEMP6(3,1)
TEMP7(3,2) = SINFEJ*TEMP6(2,2) + COSFEJ*TEMP6(3,2)
TEMP7(3,3) = SINFEJ*TEMP6(2,3) + COSFEJ*TEMP6(3,3)
TEMP8(1,1) = COSTTJ*AOCJ(J,1,1) + SINFEJ*SINTTJ*AOCJ(J,1,2)
* SINTTJ*COSFEJ*AOCJ(J,1,3)
TEMP8(1,2) = COSTTJ*AOCJ(J,2,1) + SINFEJ*SINTTJ*AOCJ(J,2,2)
* SINTTJ*COSFEJ*AOCJ(J,2,3)
TEMP8(1,3) = COSTTJ*AOCJ(J,3,1) + SINFEJ*SINTTJ*AOCJ(J,3,2)
* SINTTJ*COSFEJ*AOCJ(J,3,3)

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TEMP8(2,1) = COSFEJ*AOCJ(J,1,2) + SINFEJ*AOCJ(J,1,3)
TEMP8(2,2) = COSFEJ*AOCJ(J,2,2) + SINFEJ*AOCJ(J,2,3)
TEMP8(2,3) = COSFEJ*AOCJ(J,3,2) + SINFEJ*AOCJ(J,3,3)
TEMP8(3,1) = SINTTJ*AOCJ(J,1,1) + SINFEJ*COSTTJ*AOCJ(J,1,2)
*
+COSFEJ*COSTTJ*AOCJ(J,1,3)
TEMP8(3,2) = SINTTJ*AOCJ(J,2,1) + SINFEJ*COSTTJ*AOCJ(J,2,2)
*
+COSFEJ*COSTTJ*AOCJ(J,2,3)
TEMP8(3,3) = SINTTJ*AOCJ(J,3,1) + SINFEJ*COSTTJ*AOCJ(J,3,2)
*
+COSFEJ*COSTTJ*AOCJ(J,3,3)
DO 45 M=1,3
DO 45 N=1,3
TEMP9(M,N) = AII(J,M,1)*TEMP8(1,N) + AII(J,M,2)*TEMP8(2,N)
*
+ AII(J,M,3)*TEMP8(3,N)
45 CONTINUE
TEMP10(1,1) = COSTTJ*TEMP9(1,1) + SINTTJ*TEMP9(3,1)
TEMP10(1,2) = COSTTJ*TEMP9(1,2) + SINTTJ*TEMP9(3,2)
TEMP10(1,3) = COSTTJ*TEMP9(1,3) + SINTTJ*TEMP9(3,3)
TEMP10(2,1) = SINFEJ*SINTTJ*TEMP9(1,1) + COSFEJ*TEMP9(2,1)
*
- SINFEJ*COSTTJ*TEMP9(3,1)
TEMP10(2,2) = SINFEJ*SINTTJ*TEMP9(1,2) + COSFEJ*TEMP9(2,2)
*
- SINFEJ*COSTTJ*TEMP9(3,2)
TEMP10(2,3) = SINFEJ*SINTTJ*TEMP9(1,3) + COSFEJ*TEMP9(2,3)
*
- SINFEJ*COSTTJ*TEMP9(3,3)
TEMP10(3,1) = -SINTTJ*COSFEJ*TEMP9(1,1) + SINFEJ*TEMP9(2,1)
*
+ COSFEJ*COSTTJ*TEMP9(3,1)
TEMP10(3,2) = -SINTTJ*COSFEJ*TEMP9(1,2) + SINFEJ*TEMP9(2,2)
*
+ COSFEJ*COSTTJ*TEMP9(3,2)
TEMP10(3,3) = -SINTTJ*COSFEJ*TEMP9(1,3) + SINFEJ*TEMP9(2,3)
*
+ COSFEJ*COSTTJ*TEMP9(3,3)
DO 50 M=1,3
DO 50 N=1,3
TEMP11(M,N) = TEMP7(M,N) + TEMP10(M,N)
50 CONTINUE
DO 55 M=1,3
DO 55 N=1,3
EEJ(M,N) = AOCJ(J,M,1)*TEMP11(1,N) + AOCJ(J,M,2)*TEMP11(2,N)
*
+ AOCJ(J,M,3)*TEMP11(3,N)
55 CONTINUE
60 THATA(J) = THATA(J) + THATAD(J)*DELTAT
FEE(J) = FEE(J) + FEED(J)*DELTAT
65 CONTINUE
DO 70 M=1,3
FFF(M) = FFF(M) + FFJ(M)
70 CONTINUE
DO 75 M=1,3
DO 75 N=1,3
EEE(M,N) = EEE(M,N) + EEJ(M,N)
75 CONTINUE
GO TO 10
*****
*
*
*
END

```

C
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SUBROUTINE EMCALC

C
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*****
COMMON  A(3)          9          AE(5)          9          AED(5)          9  COMM
*        AFOUR(2)     9          AII(6,3,3)    9          COMM
*        AIO(6,3,3)   9          AJ1(3)        9          ALT          9  COMM
*        AOCJ(6,3,3)  9          AOJ(3)        9          ADNE(7)       9  COMM
*        ATCPT2(3,3)  9          ATHREE(5)     9          ATWO(4)       9  COMM
*        A1(3,3)      9          AIJ(2)        9          COMM
COMMON  BDMASS        9          BFOUR(2)     9          BMOM          9  COMM
*        BODYDI(3,3)  9          BODYUI(3,3)  9          BODY1I(3,3)  9  COMM
*        BOMASS       9          BONE(7)        9          BTHREE(5)     9  COMM
*        BTWO(4)      9          B1MASS        9          B2MASS        9  COMM
*        B3MASS       9          B4MASS        9          COMM
COMMON  CA(3)        9          CB(3)         9          CGAINO(3)     9  COMM
*        CGAIN1(2)    9          COMM
*        COSFEJ       9          COSTTJ       9          COSTTQ       9  COMM
*        COSTT1       9          COSTI3       9          COSTT4       9  COMM
*        CO2T         9          CP1          9          CP2          9  COMM
*        CST          9          C1           9          COMM
COMMON  DB(3)        9          DDO1(3)     9          COMM
*        DELTAT       9          DO1(3)      9          DO1DOT(3)    9  COMM
*        DT1(3)       9          COMM
*        DTIME        9          D12(3)      9          D13(3)       9  COMM
*        D13DOT(3)    9          D13YCS      9          D13YSN      9  COMM
*        D13ZCS      9          D13ZSN      9          D14(3)       9  COMM
*        D14DOT(3)    9          D14YCS      9          D14YSN      9  COMM
*        D14ZCS      9          D14ZSN      9          COMM
COMMON  EEE(3,3)     9          EEJ(3,3)    9          EL2(3)       9  COMM
*        EL2DOT(3)    9          EL2YCS      9          EL2YSN      9  COMM
*        EL2ZCS      9          EL2ZSN      9          EL3(3)       9  COMM
*        EL3DOT(3)    9          EL3YCS      9          EL3YSN      9  COMM
*        EL3ZCS      9          EL3ZSN      9          EL4(3)       9  COMM
*        EL4DOT(3)    9          EL4YCS      9          EL4YSN      9  COMM
*        EL4ZCS      9          EL4ZSN      9          EM(6,6)     9  COMM
COMMON  FAT(8)       9          COMM
*        FEE(6)       9          FEED(6)     9          FFF(3)       9  COMM
*        FFJ(3)       9          FLAG1       9          FLAG2       9  COMM
*        FLAG3       9          FLAG4       9          FN          9  COMM
*        FO(3)        9          FO1(3)      9          FO2(3)      9  COMM
*        FO3(3)      9          F1(3)       9          F11(3)      9  COMM
*        FPT(5)       9          COMM
*        F12(3)      9          F13(3)     9          COMM
COMMON  GAIN(10)     9          G3          9          COMM
*        G3DOT       9          G4          9          G4DOT       9  COMM
COMMON  H(3)         9          HCMG(3)     9          HDOT(3)     9  COMM
*        HI(3)        9          HO(3)       9          HW(6)       9  COMM
*        H1(3)        9          HIPDOT(3)   9          H1PRIM(3)   9  COMM
*        H3PRIM(3)   9          H4PRIM(3)   9          COMM
COMMON  IBZF         9          ICFA        9          ICFB        9  COMM
*        ICFC         9          ICFD        9          IDOCK       9  COMM
*        IDOF(6)     9          COMM
*        IGRAVF       9          IPNDLM      9          IPNTCK      9  COMM
*        IPRINT      9          IPROPF      9          COMM
COMMON  NCASE        9          NCHECK      9          NDECK       9  COMM
*        NGAIN       9          NUMCMG     9          COMM
COMMON  OMEGA1       9          OMEGA3      9          OMEGA4      9  COMM
COMMON  PEND3L       9          PEND4L     9          COMM
COMMON  Q(4,4)      9          COMM

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COMMON      R      ,      RO(3)      ,      R1(3)      ,      COMM
*           R1DOT(3) ,      R1YCS      ,      R1YSN      ,      COMM
*           R1ZCS      ,      R1ZSN      ,      R2(3)      ,      COMM
*           R2DOT(3)  ,      R2YCS      ,      R2YSN      ,      COMM
*           R2ZCS      ,      R2ZSN      ,      R3(3)      ,      COMM
*           R3DOT(3)  ,      R3YCS      ,      R3YSN      ,      COMM
*           R3ZCS      ,      R3ZSN      ,      R4(3)      ,      COMM
*           R4DOT(3)  ,      R4YCS      ,      R4YSN      ,      COMM
*           R4ZCS      ,      R4ZSN      ,      SINFEJ      ,      COMM
COMMON      S      ,      SDOT      ,      SINTT1      ,      COMM
*           SINTTJ      ,      SINTTO      ,      SINTT2      ,      COMM
*           SINTT2      ,      SINTT3      ,      SINTT4      ,      COMM
*           SP      ,      SUM1      ,      SUM2      ,      COMM
*           SUM3      ,      S2(3)      ,      S3(3)      ,      COMM
*           S4(3)      ,      TC(3,3)      ,      TEMP1(3)      ,      COMM
COMMON      T(3,3)      ,      TEMP2(3)      ,      TEMP3(3)      ,      COMM
*           TEMP3(3)      ,      TEMP4(3)      ,      TEMP5(3,3)      ,      COMM
*           TEMP6(3,3)      ,      TEMP7(3,3)      ,      TEMP6(3,3)      ,      COMM
*           TEMP9(3,3)      ,      TEMP10(3,3)      ,      TEMP11(3,3)      ,      COMM
*           TEMP12(3,3)      ,      TEMP13(3,3)      ,      TEMP14(3,3)      ,      COMM
*           TEMP15(3,3)      ,      TERM1(3)      ,      TERM2(3)      ,      COMM
*           TFRICT      ,      THATA(6)      ,      THATAD(6)      ,      COMM
*           THETA1      ,      THETA3      ,      THETA4      ,      COMM
*           THETO      ,      TIBO(3,3)      ,      TIBO1(3,3)      ,      COMM
*           TIME      ,      TJ      ,      TJ1(10)      ,      COMM
*           TJ2(10)      ,      TJ3(10)      ,      TJ4(10)      ,      COMM
*           TMOTOR      ,      TOTMAS      ,      TO1      ,      COMM
*           TOEF(3)      ,      TQOP(3)      ,      TQ1G(3)      ,      COMM
*           TQOG(3)      ,      TSTART      ,      TSTOP      ,      COMM
*           TQ1P(3)      ,      TT3DOT      ,      TT4DOT      ,      COMM
*           TT1DOT      ,      T13      ,      T14      ,      COMM
*           T1EF(3)      ,      V(3)      ,      COMM
COMMON      V(3)      ,      COMM
COMMON      W0(3)      ,      WS      ,      W1(3)      ,      COMM
*           W3(3)      ,      W4(3)      ,      COMM
COMMON      X(6,7)      ,      XC      ,      XCDOT      ,      COMM
*           XMU      ,      COMM

```

C
C
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*****
*
*
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*****

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THE FOLLOWING CALCULATIONS WILL BE USED REPEATEDLY TO CALCULATE M

```

SINTT1 = SIN(THETA1)
COSTT1 = COS(THETA1)
CO2T = COSTT1**2
CST = COSTT1*SINTT1
SI2T = SINTT1**2
R1YCS = R1(2)*COSTT1
R2YCS = R2(2)*COSTT1
R3YCS = R3(2)*COSTT1
R4YCS = R4(2)*COSTT1
R1ZCS = R1(3)*COSTT1
R2ZCS = R2(3)*COSTT1
R3ZCS = R3(3)*COSTT1
R4ZCS = R4(3)*COSTT1
R1YSN = R1(2)*SINTT1
R2YSN = R2(2)*SINTT1

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R3YSN = R3(2)*SINTT1
R4YSN = R4(2)*SINTT1
R1ZSN = R1(3)*SINTT1
R2ZSN = R2(3)*SINTT1
R3ZSN = R3(3)*SINTT1
R4ZSN = R4(3)*SINTT1
EL2YCS = EL2(2)*COSTT1
EL3YCS = EL3(2)*COSTT1
EL4YCS = EL4(2)*COSTT1
EL2ZCS = EL2(3)*COSTT1
EL3ZCS = EL3(3)*COSTT1
EL4ZCS = EL4(3)*COSTT1
EL2YSN = EL2(2)*SINTT1
EL3YSN = EL3(2)*SINTT1
EL4YSN = EL4(2)*SINTT1
EL2ZSN = EL2(3)*SINTT1
EL3ZSN = EL3(3)*SINTT1
EL4ZSN = EL4(3)*SINTT1
D13YCS = D13(2)*COSTT1
D14YCS = D14(2)*COSTT1
D13ZCS = D13(3)*COSTT1
D14ZCS = D14(3)*COSTT1
D13YSN = D13(2)*SINTT1
D14YSN = D14(2)*SINTT1
D13ZSN = D13(3)*SINTT1
D14ZSN = D14(3)*SINTT1
BMOM=BOMASS/TOTMAS
EM(1,1)=BODY0I(1,1)+BODY1I(1,1)+B1MASS*D01(2)*(R1YCS-R1ZSN)+
* B1MASS*D01(3)*(R1YSN+R1ZCS)+B2MASS*(R2YCS-R2ZSN)*(D01(2)+EL2YCS-
* EL2ZSN)+B2MASS*(R2YSN+R2ZCS)*(D01(3)+EL2YSN+EL2ZCS)+B3MASS*(R3YCS-
* -R3ZSN)*(D01(2)+D13YCS-D13ZSN+EL3YCS-EL3ZSN)+B3MASS*(R3YSN+R3ZCS)
* *(D01(3)+D13YSN+D13ZCS+EL3YSN+EL3ZCS)+B4MASS*(R4YCS-R4ZSN)*
* (D01(2)+D14YCS-D14ZSN+EL4YCS-EL4ZSN)+B4MASS*(R4YSN+R4ZCS)*
* (D01(3)+D14YSN+D14ZCS+EL4YSN+EL4ZCS)
C
EM(1,2)=BODY0I(1,2)+BODY1I(1,2)*COSTT1-BODY1I(1,3)*SINTT1
* -B1MASS*R1(1)*D01(2)-
* B2MASS*R2(1)*(D01(2)+EL2YCS-EL2ZSN)-
* B3MASS*R3(1)*(D01(2)+D13YCS-D13ZSN+EL3YCS-EL3ZSN)-
* B4MASS*R4(1)*(D01(2)+D14YCS-D14ZSN+EL4YCS-EL4ZSN)
C
EM(1,3)=BODY0I(1,3)+BODY1I(1,2)*SINTT1+BODY1I(1,3)*COSTT1
* -B1MASS*R1(1)*D01(3)-
* B2MASS*R2(1)*(D01(3)+EL2YSN+EL2ZCS)-
* B3MASS*R3(1)*(D01(3)+D13YSN+D13ZCS+EL3YSN+EL3ZCS)-
* B4MASS*R4(1)*(D01(3)+D14YSN+D14ZCS+EL4YSN+EL4ZCS)
C
EM(1,4)=BODY1I(1,1)-B1MASS*D01(3)*(BMOM*D01(3)-R1YSN-R1ZCS)+
* B1MASS*D01(2)*(R1YCS-R1ZSN-BMOM*D01(2))-
* B2MASS*(D01(3)+EL2YSN+EL2ZCS)*(BMOM*D01(3)-R2YSN-R2ZCS)+
* B2MASS*(D01(2)+EL2YCS-EL2ZSN)*(R2YCS-R2ZSN-BMOM*D01(2))-
* B3MASS*(D01(3)+(D13(2)+EL3(2))*SINTT1+(D13(3)+EL3(3))*COSTT1)*
* (BMOM*D01(3)-R3YSN-R3ZCS)+
* B3MASS*(D01(2)+(D13(2)+EL3(2))*COSTT1-(D13(3)+EL3(3))*SINTT1)*
* (R3YCS-R3ZSN-BMOM*D01(2))-
* B4MASS*(D01(3)+(D14(2)+EL4(2))*SINTT1+(D14(3)+EL4(3))*COSTT1)*
* (BMOM*D01(3)-R4YSN-R4ZCS)+
* B4MASS*(D01(2)+(D14(2)+EL4(2))*COSTT1-(D14(3)+EL4(3))*SINTT1)*
* (R4YCS-R4ZSN-BMOM*D01(2))
C
EM(1,5)=-B3MASS*R3(3)*(S3(3)*EL3(1)+S3(1)*EL3(3))+
* B3MASS*R3(2)*(-S3(2)*EL3(1)+S3(1)*EL3(2))

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C      EM(1,6)=-B4MASS*R4(3)*(S4(3)*EL4(1)-S4(1)*EL4(3))+
* B4MASS*R4(2)*(-S4(2)*EL4(1)+S4(1)*EL4(2))

C      EM(2,1)=BODYOI(2,1)+BODYII(2,1)*COSTT1-BODYII(3,1)*SINTT1-
* B1MASS*DO1(1)*(R1YCS-R1ZSN)-
* B2MASS*(R2YCS-R2ZSN)*(DO1(1)+EL2(1))-
* B3MASS*(R3YCS-R3ZSN)*(DO1(1)+D13(1)+EL3(1))-
* B4MASS*(R4YCS-R4ZSN)*(DO1(1)+D14(1)+EL4(1))

C      EM(2,2)=BODYOI(2,2)+BODYII(2,2)*COSTT1-BODYII(2,3)*CST
* -BODYII(3,2)*CST + BODYII(3,3)*SI2T +
* B1MASS*R1(1)*DO1(1)+B1MASS*DO1(3)*(R1YSN+R1ZCS)+
* B2MASS*R2(1)*(DO1(1)+EL2(1))+
* B2MASS*(R2YSN+R2ZCS)*(DO1(3)+EL2YSN+EL2ZCS)+
* B3MASS*R3(1)*(DO1(1)+D13(1)+EL3(1))+
* B3MASS*(R3YSN+R3ZCS)*(DO1(3)+D13YSN+D13ZCS+EL3YSN+EL3ZCS)+
* B4MASS*R4(2)*(DO1(1)+D14(1)+EL4(1))+
* B4MASS*(R4YSN+R4ZCS)*(DO1(3)+D14YSN+D14ZCS+EL4YSN+EL4ZCS)

C      EM(2,3)=BODYOI(2,3)+BODYII(2,2)*CST +BODYII(2,3)*COSTT1
* -BODYII(3,2)*SI2T - BODYII(3,3)*CST -
* B1MASS*DO1(3)*(R1YCS-R1ZSN)-
* B2MASS*(R2YCS-R2ZSN)*(DO1(3)+EL2YSN+EL2ZCS)-
* B3MASS*(R3YCS-R3ZSN)*(DO1(3)+D13YSN+D13ZCS+EL3YSN+EL3ZCS)-
* B4MASS*(R4YCS-R4ZSN)*(DO1(3)+D14YSN+D14ZCS+EL4YSN+EL4ZCS)

C      EM(2,4)=BODYII(1,2)*COSTT1-BODYII(1,3)*SINTT1-B1MASS*DO1(1)*R1YCS+
* B1MASS*DO1(1)*R1ZSN+BMOM*B1MASS*DO1(1)*DO1(2)-
* B2MASS*(DO1(1)+EL2(1))*(R2YCS-R2ZSN-BMOM*DO1(2))-
* B3MASS*(DO1(1)+D13(1)+EL3(1))*(R3YCS-R3ZSN-BMOM*DO1(2))-
* B4MASS*(DO1(1)+D14(1)+EL4(1))*(R4YCS-R4ZSN-BMOM*DO1(2))

C      EM(2,5)=(B3MASS*R3(3)*(-S3(3)*EL3(2)+S3(2)*EL3(3))-
* B3MASS*R3(1)*(-S3(2)*EL3(1)+S3(1)*EL3(2))*COSTT1-
* (-B3MASS*R3(2)*(-S3(3)*EL3(2)+S3(2)*EL3(3))+
* B3MASS*R3(1)*(S3(3)*EL3(1)-S3(1)*EL3(3)))*SINTT1

C      EM(2,6)=(B4MASS*R4(3)*(-S4(3)*EL4(2)+S4(2)*EL4(3))-
* B4MASS*R4(1)*(-S4(2)*EL4(1)+S4(1)*EL4(2))*COSTT1-
* (-B4MASS*R4(2)*(-S4(3)*EL4(2)+S4(2)*EL4(3))+
* B4MASS*R4(1)*(S4(3)*EL4(1)-S4(1)*EL4(3)))*SINTT1

C      EM(3,1)=BODYOI(3,1)+BODYII(2,1)*SINTT1+BODYII(3,1)*COSTT1-
* B1MASS*DO1(1)*(R1YSN+R1ZCS)-
* B2MASS*(DO1(1)+EL2(1))*(R2YSN+R2ZCS)-
* B3MASS*(DO1(1)+D13(1)+EL3(1))*(R3YSN+R3ZCS)-
* B4MASS*(DO1(1)+D14(1)+EL4(1))*(R4YSN+R4ZCS)

C      EM(3,2)=BODYOI(3,2)+BODYII(2,2)*CST -BODYII(2,3)*SI2T
* +BODYII(3,2)*COSTT1-BODYII(3,3)*CST-
* B1MASS*DO1(2)*(R1YSN+R1ZCS)-
* B2MASS*(R2YSN+R2ZCS)*(DO1(2)+EL2YCS-EL2ZSN)-
* B3MASS*(R3YSN+R3ZCS)*(DO1(2)+D13YCS-D13ZSN+EL3YCS-EL3ZSN)-
* B4MASS*(R4YSN+R4ZCS)*(DO1(2)+D14YCS-D14ZSN+EL4YCS-EL4ZSN)

C      EM(3,3)=BODYOI(3,3)+BODYII(2,2)*SI2T +BODYII(2,3)*CST
* +BODYII(3,2)*CST + BODYII(3,3)*COSTT1 +
* B1MASS*R1(1)*DO1(1)+B1MASS*(R1YCS-R1ZSN)*DO1(2)+
* B2MASS*R2(1)*(DO1(1)+EL2(1))+
* B2MASS*(R2YCS-R2ZSN)*(DO1(2)+EL2YCS-EL2ZSN)+
* B3MASS*R3(1)*(DO1(1)+D13(1)+EL3(1))+

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* B3MASS*(R3YCS=R3ZSN)*(D01(2)+D13YCS=D13ZSN+EL3YCS=EL3ZSN)*
 * B4MASS*R4(1)*(D01(1)+D14(1)+EL4(1))*
 * B4MASS*(R4YCS=R4ZSN)*(D01(2)+D14YCS=D14ZSN+EL4YCS=EL4ZSN)

EM(3,4)=BODY1I(1,2)*SINTT1+BODY1I(1,3)*COSTT1*
 * B1MASS*D01(1)*(BMOM*D01(3)-R1YSN=R1ZCS)*
 * B2MASS*(D01(1)+EL2(1))*(BMOM*D01(3)-R2YSN=R2ZCS)*
 * B3MASS*(D01(1)+D13(1)+EL3(1))*(BMOM*D01(3)-R3YSN=R3ZCS)*
 * B4MASS*(D01(1)+D14(1)+EL4(1))*(BMOM*D01(3)-R4YSN=R4ZCS)

EM(3,5)=(B3MASS*R3(3)*(-S3(3)*EL3(2)+S3(2)*EL3(3)) +
 * B3MASS*R3(1)*(-S3(2)*EL3(1)+S3(1)*EL3(2)))*SINTT1*
 * (-B3MASS*R3(2)*(-S3(3)*EL3(2)+S3(2)*EL3(3)) +
 * B3MASS*R3(1)*(S3(3)*EL3(1)-S3(1)*EL3(3)))*COSTT1

EM(3,6)=(B4MASS*R4(3)*(-S4(3)*EL4(2)+S4(2)*EL4(3)) +
 * B4MASS*R4(1)*(-S4(2)*EL4(1)+S4(1)*EL4(2)))*SINTT1*
 * (-B4MASS*R4(2)*(-S4(3)*EL4(2)+S4(2)*EL4(3)) +
 * B4MASS*R4(1)*(S4(3)*EL4(1)-S4(1)*EL4(3)))*COSTT1

NOW SET UP THE LOWER HALF OF THE M MATRIX.

DEFINE SOME REOCCURRING TERMS

SR3 = B3MASS*(D13(2) + EL3(2))
 SR4 = B3MASS*(D13(3) + EL3(3))
 SR5 = B4MASS*(D14(2) + EL4(2))
 SR6 = B4MASS*(D14(3) + EL4(3))
 SR1=BODY1I(1,2)+B2MASS*EL2(2)*R2(1)-SR3*R3(1)-SR5*R4(1)
 SR2=BODY1I(1,3)+B2MASS*EL2(3)*R2(1)-SR4*R3(1)-SR6*R4(1)

EM(4,1)=BODY1I(1,1)+B2MASS*(EL2(3)*R2(3)+EL2(2)*R2(2)) +
 * SR4*R3(3)+SR3*R3(2)+SR6*R4(3)+SR5*R4(2)

EM(4,2)=SR1*COSTT1-SR2*SINTT1

EM(4,3)=SR1*SINTT1+SR2*COSTT1

REDEFINE SR1 AND SR2

SR1=BMOM*(D01(2)*COSTT1+D01(3)*SINTT1)
 SR2=BMOM*(-D01(2)*SINTT1+D01(3)*COSTT1)

EM(4,4) = BODY1I(1,1)
 * B2MASS*(EL2(3)*(R2(3)-SR2) + EL2(2)*(R2(2)-SR1)) +
 * SR4*(R3(3)-SR2)+SR3*(R3(2)-SR1)+SR6*(R4(3)-SR2)+SR5*(R4(2)-SR1)

EM(4,5) = B3MASS*((R3(3)-SR2)*EL3(3)+(R3(2)-SR1)*EL3(2))*S3(1) +
 * (R3(2)-SR1)*EL3(1)*S3(2)-(R3(3)-SR2)*EL3(1)*S3(3)

EM(4,6) = B4MASS*((R4(3)-SR2)*EL4(3)+(R4(2)-SR1)*EL4(2))*S4(1) +
 * (R4(2)-SR1)*EL4(1)*S4(2)-(R4(3)-SR2)*EL4(1)*S4(3)

EM(5,1) = -B3MASS*EL3(1)*(R3(2)*S3(2)+R3(3)*S3(3))

EM(5,2) = B3MASS*((EL3(3)*R3(3)+EL3(1)*R3(1))*COSTT1 +
 * EL3(3)*R3YSN)*S3(2)+(-EL3(2)*R3ZCS+(EL3(2)*R3(2)+EL3(1)*R3(1))*
 * SINTT1)*S3(3)

EM(5,3) = B3MASS*((EL3(3)*R3(3)+EL3(1)*R3(1))*SINTT1 +
 * EL3(3)*R3YCS)*S3(2)+(-EL3(2)*R3ZSN+(EL3(2)*R3(2)+EL3(1)*R3(1))*
 * COSTT1)*S3(3)

EM(5,4) = B3MASS*EL3(1)*(-R3(2)+SR1)*S3(2)+(-R3(3)+SR2)*S3(3)

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C: EM(5,5)=B3MASS*(1.-B3MASS/TOTMAS)*((EL3(3)**2+EL3(1)**2)*S3(2)-
* EL3(3)*EL3(2)*S3(3))*S3(2)+((EL3(2)**2+EL3(1)**2)*S3(3)-
* EL3(2)*EL3(3)*S3(2))*S3(3)
C: EM(5,6)=(B3MASS*B4MASS/TOTMAS)*((-EL3(3)*EL4(3)+EL3(1)*EL4(1))*
* S4(2)+EL3(3)*EL4(2)*S4(3))*S3(2)+((-EL3(2)*EL4(2)+EL3(1)*EL4(1))*
* S4(3)+EL3(2)*EL4(3)*S4(2))*S3(3)
C: EM(6,1)=B4MASS*EL4(1)*(R4(2)*S4(2)+R4(3)*S4(3))
C: EM(6,2)=B4MASS*((EL4(3)*R4(3)+EL4(1)*R4(1))*COSTT1+EL4(3)*R4YSN)*
* S4(2)+(-EL4(2)*R4ZCS-(EL4(2)*R4(2)+EL4(1)*R4(1))*SINTT1)*S4(3)
C: EM(6,3)=B4MASS*((EL4(3)*R4(3)+EL4(1)*R4(1))*SINTT1-EL4(3)*R4YCS)*
* S4(2)+(-EL4(2)*R4ZSN+(EL4(2)*R4(2)+EL4(1)*R4(1))*COSTT1)*S4(3)
C: EM(6,4)=B4MASS*EL4(1)*((-R4(2)+SR1)*S4(2)+(-R4(3)+SR2)*S4(3))
C: EM(6,5)=(B3MASS*B4MASS/TOTMAS)*((-EL4(3)*EL3(3)+EL4(1)*EL3(1))*
* S3(2)+EL4(3)*EL3(2)*S3(3))*S4(2)+((-EL4(2)*EL3(2)+EL4(1)*EL3(1))*
* S3(3)+EL4(2)*EL3(3)*S3(2))*S4(3)
C: EM(6,6)=B4MASS*(1.-B4MASS/TOTMAS)*((EL4(3)**2+EL4(1)**2)*S4(2)-
* EL4(3)*EL4(2)*S4(3))*S4(2)+((EL4(2)**2+EL4(1)**2)*S4(3)-
* EL4(2)*EL4(3)*S4(2))*S4(3)
DO 10 M=1,3
DO 10 N=1,3
EM(M,N)=EM(M,N) + EEE(M,N)
10 CONTINUE
RETURN
C: *****
C: *
C: *
C: *
END

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SUBROUTINE FOMS(A,B,N,E,TJ)
DIMENSION A(1),B(1),TJ(1)

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A(1) CONTAINS THE CURRENT TIME. I.E. A(1) = TIME.
A(2) THROUGH A(N) CONTAIN THE INTEGRALS WHERE N EQUALS THE
NUMBER OF INTEGRALS PLUS 1.
TJ IS A SCRATCH ARRAY. TJ(1) CONTAINS THE INITIAL DELT AND TJ(2)
THROUGH TJ(N) CONTAIN THE BACK VALUES OF THE DERIVATIVES.
B(1) CONTAINS THE CURRENT DELT AND B(2) THROUGH B(N) CONTAIN THE
CURRENT DERIVATIVES.
IF E = 0., REINITIALIZE THE DERIVATIVES.
IF E = 1., CONTINUE THE INTEGRATION.

IF(N .LE. 1) RETURN
IF(E .NE. 0.) GO TO 20
E = 1.
DO 10 I=1,N
TJ(I) = B(I)
10 CONTINUE
20 H02 = B(1)*0.5
DO 30 I=2,N
A(I) = A(I) + H02*(3.*B(I)-TJ(I))
TJ(I) = B(I)
30 CONTINUE
A(1) = A(1) + B(1)
RETURN

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END

C
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SUBROUTINE GGRAD

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*
*
*
*****
COMMON      A(3)          ,      AE(5)          ,      AED(5)          ,      COMMC
*            AFOUR(2)     ,      AII(6,3,3)    ,      COMMC
*            AIO(6,3,3)   ,      AJ1(3)      ,      ALT            ,      COMMC
*            AOCJ(6,3,3)  ,      AOJ(3)     ,      ADNE(7)       ,      COMMC
*            ATCPT2(3,3)  ,      ATHREE(5)  ,      ATWO(4)        ,      COMMC
*            A1(3,3)      ,      A1J(2)     ,      COMMC
COMMON      BDMASS       ,      BFOUR(2)    ,      BMOM           ,      COMMC
*            BODYDI(3,3)  ,      BODYOI(3,3) ,      BODY1I(3,3)   ,      COMMC
*            BOMASS       ,      BONE(7)    ,      BTHREE(5)     ,      COMMC
*            BTWO(4)      ,      B1MASS     ,      B2MASS         ,      COMMC
*            B3MASS       ,      B4MASS     ,      COMMC
COMMON      CA(3)        ,      CB(3)        ,      CGAIN0(3)     ,      COMMC
*            CGAIN1(2)    ,      COMMC
*            COSFEJ       ,      COSTTJ      ,      COSTT0        ,      COMMC
*            COSTT1      ,      COSTT3      ,      COSTT4        ,      COMMC
*            CO2T         ,      CP1         ,      CP2           ,      COMMC
*            CST          ,      C1          ,      COMMC
COMMON      DB(3)        ,      DD01(3)     ,      COMMC
*            DELTAT      ,      D01(3)      ,      D01DOT(3)     ,      COMMC
*            DTI(3)      ,      COMMC
*            DTIME       ,      D12(3)     ,      D13(3)         ,      COMMC
*            D13DOT(3)   ,      D13YCS      ,      D13YSN        ,      COMMC
*            D13ZCS      ,      D13ZSN      ,      D14(3)         ,      COMMC
*            D14DOT(3)   ,      D14YCS      ,      D14YSN        ,      COMMC
*            D14ZCS      ,      D14ZSN      ,      COMMC
COMMON      EEE(3,3)     ,      EEJ(3,3)    ,      EL2(3)         ,      COMMC
*            EL2DOT(3)   ,      EL2YCS      ,      EL2YSN        ,      COMMC
*            EL2ZCS      ,      EL2ZSN      ,      EL3(3)         ,      COMMC
*            EL3DOT(3)   ,      EL3YCS      ,      EL3YSN        ,      COMMC
*            EL3ZCS      ,      EL3ZSN      ,      EL4(3)         ,      COMMC
*            EL4DOT(3)   ,      EL4YCS      ,      EL4YSN        ,      COMMC
*            EL4ZCS      ,      EL4ZSN      ,      EM(6,6)       ,      COMMC
COMMON      FAT(8)       ,      FEED(6)     ,      FFF(3)         ,      COMMC
*            FEE(6)      ,      FLAG1       ,      FLAG2         ,      COMMC
*            FFJ(3)      ,      FLAG4       ,      FNI           ,      COMMC
*            FLAG3       ,      FO1(3)      ,      F02(3)        ,      COMMC
*            FO(3)       ,      F1(3)       ,      F11(3)        ,      COMMC
*            F03(3)     ,      COMMC
*            FPT(5)      ,      COMMC
*            F12(3)     ,      F13(3)     ,      COMMC
COMMON      GAIN(10)     ,      G3           ,      COMMC
*            G3DOT      ,      G4           ,      G4DOT         ,      COMMC
COMMON      H(3)        ,      HCMG(3)     ,      HDOT(3)       ,      COMMC
*            HI(3)      ,      HO(3)       ,      HW(6)         ,      COMMC
*            H1(3)      ,      H1PDOT(3)   ,      HIPRIM(3)     ,      COMMC
*            H3PRIM(3)  ,      H4PRIM(3)   ,      COMMC
COMMON      IB2F        ,      ICFA        ,      ICFB          ,      COMMC
*            ICFC       ,      ICFD        ,      IDOCK         ,      COMMC
*            IDOF(6)    ,      COMMC
*            IGRAVF     ,      IPNDLM      ,      IPNTCK        ,      COMMC
*            IPRINT     ,      IPROPF      ,      COMMC
COMMON      NCASE       ,      NCHECK      ,      NDECK         ,      COMMC
*            NGAIN      ,      NUMCMG     ,      COMMC
COMMON      OMEGA1      ,      OMEGA3     ,      OMEGA4        ,      COMMC
COMMON      PEND3L     ,      PEND4L     ,      COMMC
COMMON      Q(4,4)     ,      COMMC

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|--------|-------------|---|-------------|---|-------------|---|-------|
| COMMON | R | 9 | RO(3) | 9 | R1(3) | 9 | COMMC |
| * | R1DOT(3) | 9 | R1YCS | 9 | R1YSN | 9 | COMMC |
| * | R1ZCS | 9 | R1ZSN | 9 | R2(3) | 9 | COMMC |
| * | R2DOT(3) | 9 | R2YCS | 9 | R2YSN | 9 | COMMC |
| * | R2ZCS | 9 | R2ZSN | 9 | R3(3) | 9 | COMMC |
| * | R3DOT(3) | 9 | R3YCS | 9 | R3YSN | 9 | COMMC |
| * | R3ZCS | 9 | R3ZSN | 9 | R4(3) | 9 | COMMC |
| * | R4DOT(3) | 9 | R4YCS | 9 | R4YSN | 9 | COMMC |
| * | R4ZCS | 9 | R4ZSN | 9 | | | COMMC |
| COMMON | S | 9 | SDOT | 9 | SINFEJ | 9 | COMMC |
| * | SINTTJ | 9 | SINTTO | 9 | SINTT1 | 9 | COMMC |
| * | SINTT2 | 9 | SINTT3 | 9 | SINTT4 | 9 | COMMC |
| * | SP | 9 | SUM1 | 9 | SUM2 | 9 | COMMC |
| * | SUM3 | 9 | S2(3) | 9 | S3(3) | 9 | COMMC |
| * | S4(3) | 9 | | 9 | | 9 | COMMC |
| COMMON | T(3,3) | 9 | TC(3,3) | 9 | TEMP1(3) | 9 | COMMC |
| * | TEMP2(3) | 9 | | 9 | | 9 | COMMC |
| * | TEMP3(3) | 9 | TEMP4(3) | 9 | TEMP5(3,3) | 9 | COMMC |
| * | TEMP6(3,3) | 9 | TEMP7(3,3) | 9 | TEMP8(3,3) | 9 | COMMC |
| * | TEMP9(3,3) | 9 | TEMP10(3,3) | 9 | TEMP11(3,3) | 9 | COMMC |
| * | TEMP12(3,3) | 9 | TEMP13(3,3) | 9 | TEMP14(3,3) | 9 | COMMC |
| * | TEMP15(3,3) | 9 | TERM1(3) | 9 | TERM2(3) | 9 | COMMC |
| * | TFRICT | 9 | THATA(6) | 9 | THATAD(6) | 9 | COMMC |
| * | THETA1 | 9 | THETA3 | 9 | THETA4 | 9 | COMMC |
| * | THETO | 9 | TIBO(3,3) | 9 | TIBO1(3,3) | 9 | COMMC |
| * | TIME | 9 | TJ | 9 | TJ1(10) | 9 | COMMC |
| * | TJ2(10) | 9 | TJ3(10) | 9 | TJ4(10) | 9 | COMMC |
| * | TMOTOR | 9 | | 9 | | 9 | COMMC |
| * | TOEF(3) | 9 | TOTMAS | 9 | TO1 | 9 | COMMC |
| * | TQOG(3) | 9 | TQOP(3) | 9 | TQ1G(3) | 9 | COMMC |
| * | TQ1P(3) | 9 | TSTART | 9 | TSTOP | 9 | COMMC |
| * | TT1DOT | 9 | TT3DOT | 9 | TT4DOT | 9 | COMMC |
| * | TIEF(3) | 9 | T13 | 9 | T14 | 9 | COMMC |
| COMMON | V(3) | 9 | | 9 | | 9 | COMMC |
| COMMON | W0(3) | 9 | WS | 9 | W1(3) | 9 | COMMC |
| * | W3(3) | 9 | W4(3) | 9 | | 9 | COMMC |
| COMMON | X(6,7) | 9 | XC | 9 | XCDOT | 9 | COMMC |
| * | XMU | 9 | | 9 | | 9 | COMMC |

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SINTTO = SIN(THETO)
COSTTO = COS(THETO)
DB(1) = -SINTTO*TIBO(1,1) + COSTTO*TIBO(2,1)
DB(2) = -SINTTO*TIBO(1,2) + COSTTO*TIBO(2,2)
DB(3) = -SINTTO*TIBO(1,3) + COSTTO*TIBO(2,3)
REMP = 0.
DO 10 M=1,3
REMP = REMP + DB(M)*RO(M)
10 CONTINUE
DO 20 L=1,3
FO1(L) = C1*BOMASS*(3.*REMP+DB(L) - RO(L))
A(L) = 0.
DO 20 M=1,3
A(L) = A(L) + BODYO1(L,M)*DB(M)
20 CONTINUE
TQOG(1) = 3.*C1*(DB(2)*A(3) - DB(3)*A(2))
TQOG(2) = 3.*C1*(DB(3)*A(1) - DB(1)*A(3))

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TQOG(3) = 3.*C1*(DB(1)*A(2) - DB(2)*A(1))
DB(1) = -SINTTO*TIBO(1,1) + COSTTO*TIBO(2,1)
DB(2) = COSTT1*(-SINTTO*TIBO(1,2) + COSTTO*TIBO(2,2)) +
* SINTT1*(-SINTTO*TIBO(1,3) + COSTTO*TIBO(2,3))
DB(3) = -SINTT1*(-SINTTO*TIBO(1,2) + COSTTO*TIBO(2,2)) +
* COSTT1*(-SINTTO*TIBO(1,3) + COSTTO*TIBO(2,3))
REMP = 0.
DO 30 M=1,3
REMP = REMP + DB(M)*R1(M)
30 CONTINUE
DO 40 L=1,3
F11(L) = C1*B1MASS*(3.*REMP*DB(L) - R1(L))
A(L) = 0.
DO 40 M=1,3
A(L) = A(L) + BODY11(L,M)*DB(M)
40 CONTINUE
TQ1G(1) = 3.*C1*(DB(2)*A(3) - DB(3)*A(2))
TQ1G(2) = 3.*C1*(DB(3)*A(1) - DB(1)*A(3))
TQ1G(3) = 3.*C1*(DB(1)*A(2) - DB(2)*A(1))
RETURN
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SUBROUTINE HCON

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COMMON      A (3)      ,      AE (5)      ,      AED (5)      ,      COMMC
*            AF0UR (2)  ,      AII (6,3,3) ,      ,      COMMC
*            AIO (6,3,3) ,      AJI (3)    ,      ALT        ,      COMMC
*            AOCJ (6,3,3) ,      AOJ (3)   ,      AONE (7)   ,      COMMC
*            ATCPT2 (3,3) ,      ATHREE (5) ,      ATWO (4)  ,      COMMC
*            A1 (3,3)   ,      AIJ (2)   ,      ,      COMMC
COMMON      BDMASS    ,      BFOUR (2)  ,      BMOM       ,      COMMC
*            BODYDI (3,3) ,      BODYOI (3,3) ,      BODY1I (3,3) ,      COMMC
*            BOMASS    ,      BONE (7)  ,      BTHREE (5) ,      COMMC
*            BTWO (4)  ,      B1MASS   ,      B2MASS    ,      COMMC
*            B3MASS   ,      B4MASS   ,      ,      COMMC
COMMON      CA (3)    ,      CB (3)    ,      CGAINO (3) ,      COMMC
*            CGAIN1 (2) ,      ,      ,      COMMC
*            COSFEJ    ,      COSTTJ    ,      COSTTO     ,      COMMC
*            COSTT1    ,      COSTT3    ,      COSTT4     ,      COMMC
*            CO2T      ,      CP1       ,      CP2       ,      COMMC
*            CST       ,      C1        ,      ,      COMMC
COMMON      DB (3)    ,      DD01 (3)  ,      ,      COMMC
*            DELTAT    ,      D01 (3)   ,      D01DOT (3) ,      COMMC
*            DTI (3)   ,      ,      ,      COMMC
*            DTIME     ,      D12 (3)   ,      D13 (3)    ,      COMMC
*            D13DOT (3) ,      D13YCS    ,      D13YSN    ,      COMMC
*            D13ZCS    ,      D13ZSN    ,      D14 (3)    ,      COMMC
*            D14DOT (3) ,      D14YCS    ,      D14YSN    ,      COMMC
*            D14ZCS    ,      D14ZSN    ,      ,      COMMC
COMMON      EEE (3,3) ,      EEJ (3,3) ,      EL2 (3)    ,      COMMC
*            EL2DOT (3) ,      EL2YCS    ,      EL2YSN    ,      COMMC
*            EL2ZCS    ,      EL2ZSN    ,      EL3 (3)    ,      COMMC
*            EL3DOT (3) ,      EL3YCS    ,      EL3YSN    ,      COMMC
*            EL3ZCS    ,      EL3ZSN    ,      EL4 (3)    ,      COMMC
*            EL4DOT (3) ,      EL4YCS    ,      EL4YSN    ,      COMMC
*            EL4ZCS    ,      EL4ZSN    ,      EM (6,6)  ,      COMMC
COMMON      FAT (8)   ,      ,      ,      COMMC
*            FEE (6)   ,      FEED (6)  ,      FFF (3)    ,      COMMC
*            FFJ (3)   ,      FLAG1     ,      FLAG2     ,      COMMC
*            FLAG3    ,      FLAG4     ,      FNI       ,      COMMC
*            FO (3)    ,      FO1 (3)   ,      FO2 (3)   ,      COMMC
*            FO3 (3)   ,      F1 (3)    ,      F11 (3)   ,      COMMC
*            FPT (5)   ,      ,      ,      COMMC
*            F12 (3)   ,      F13 (3)   ,      ,      COMMC
COMMON      GAIN (10) ,      G3        ,      ,      COMMC
*            G3DOT    ,      G4        ,      G4DOT     ,      COMMC
COMMON      H (3)     ,      HCMG (3)  ,      HDOT (3)  ,      COMMC
*            HI (3)    ,      HO (3)    ,      HW (6)    ,      COMMC
*            H1 (3)    ,      H1PDOT (3) ,      H1PRIM (3) ,      COMMC
*            H3PRIM (3) ,      H4PRIM (3) ,      ,      COMMC
COMMON      IB2F      ,      ICFA     ,      ICFB      ,      COMMC
*            ICFC      ,      ICFD     ,      IDOCK     ,      COMMC
*            IDOF (6)  ,      ,      ,      COMMC
*            IGRAVF    ,      IPNDLM   ,      IPNTCK    ,      COMMC
*            IPRINT    ,      IPROPF   ,      ,      COMMC
COMMON      NCASE     ,      NCHECK   ,      NDECK     ,      COMMC
*            NGAIN     ,      NUMCMG   ,      ,      COMMC

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COMMON      OMEGA1      *      OMEGA3      *      OMEGA4      *      COMM
COMMON      PEND3L      *      PEND4L      *      *      COMM
COMMON      Q(4,4)      *      *      *      *      COMM
COMMON      R          *      R0(3)       *      R1(3)       *      COMM
*          R1DOT(3)    *      R1YCS      *      R1YSN      *      COMM
*          R1ZCS      *      R1ZSN      *      R2(3)       *      COMM
*          R2DOT(3)    *      R2YCS      *      R2YSN      *      COMM
*          R2ZCS      *      R2ZSN      *      R3(3)       *      COMM
*          R3DOT(3)    *      R3YCS      *      R3YSN      *      COMM
*          R3ZCS      *      R3ZSN      *      R4(3)       *      COMM
*          R4DOT(3)    *      R4YCS      *      R4YSN      *      COMM
*          R4ZCS      *      R4ZSN      *      *      *      COMM
COMMON      S          *      SDOT        *      SINFEJ      *      COMM
*          SINTTJ      *      SINTT0     *      SINTT1     *      COMM
*          SINTT2      *      SINTT3     *      SINTT4     *      COMM
*          SP          *      SUM1       *      SUM2       *      COMM
*          SUM3        *      S2(3)      *      S3(3)      *      COMM
*          S4(3)       *      *      *      *      *      COMM
COMMON      T(3,3)     *      TC(3,3)    *      TEMP1(3)   *      COMM
*          TEMP2(3)    *      *      *      *      *      COMM
*          TEMP3(3)    *      TEMP4(3)   *      TEMP5(3,3) *      COMM
*          TEMP6(3,3)  *      TEMP7(3,3) *      TEMP8(3,3)  *      COMM
*          TEMP9(3,3)  *      TEMP10(3,3)*      TEMP11(3,3) *      COMM
*          TEMP12(3,3) *      TEMP13(3,3)*      TEMP14(3,3) *      COMM
*          TEMP15(3,3) *      TERM1(3)   *      TERM2(3)   *      COMM
*          TFRICT      *      THATA(6)  *      THATAD(6)  *      COMM
*          THETA1      *      THETA3     *      THETA4     *      COMM
*          THETO       *      TIBO(3,3) *      TIBO1(3,3) *      COMM
*          TIME        *      TJ         *      TJ1(10)    *      COMM
*          TJ2(10)     *      TJ3(10)   *      TJ4(10)    *      COMM
*          TMOTOR      *      *      *      *      *      COMM
*          TOEF(3)     *      TOTMAS     *      TO1        *      COMM
*          TQOG(3)     *      TQOP(3)   *      TQ1G(3)    *      COMM
*          TQ1P(3)     *      TSTART     *      TSTOP      *      COMM
*          TT1DOT      *      TT3DOT     *      TT4DOT     *      COMM
*          TIEF(3)     *      T13       *      T14        *      COMM
COMMON      V(3)       *      *      *      *      *      COMM
COMMON      W0(3)      *      WS         *      W1(3)       *      COMM
*          W3(3)       *      W4(3)      *      *      *      COMM
COMMON      X(6,7)     *      XC         *      XCDOT      *      COMM
*          XMU         *      *      *      *      *      COMM

```

```

*****
*
*
*****
THATAD(1) = +GAIN(4)*TIBO(3,2) +GAIN(5)*W0(1)
THATAD(2) = +THATAD(1)
CALL CMG
RETURN
*****

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```

*
*
*
END

```

C
C
C
C
C
C

C
C
C
C
C

SUBROUTINE MULT(C,A,B,F,D,E,MTYPE)

C
C
C
C
C

*
*
*

DIMENSION A(3,3) , B(3) , C(3) , D(3,3) , E(3,3) , F(3,3) , MULT

C

IF (MTYPE .NE. 1) GO TO 100
 C(1) = A(1,1)*B(1) + A(1,2)*B(2) + A(1,3)*B(3) MULT
 C(2) = A(2,1)*B(1) + A(2,2)*B(2) + A(2,3)*B(3) MULT
 C(3) = A(3,1)*B(1) + A(3,2)*B(2) + A(3,3)*B(3) MULT
 RETURN MULT

100 CONTINUE

F(1,1) = D(1,1)*E(1,1) + D(1,2)*E(2,1) + D(1,3)*E(3,1) MULT
 F(1,2) = D(1,1)*E(1,2) + D(1,2)*E(2,2) + D(1,3)*E(3,2) MULT
 F(1,3) = D(1,1)*E(1,3) + D(1,2)*E(2,3) + D(1,3)*E(3,3) MULT
 F(2,1) = D(2,1)*E(1,1) + D(2,2)*E(2,1) + D(2,3)*E(3,1) MULT
 F(2,2) = D(2,1)*E(1,2) + D(2,2)*E(2,2) + D(2,3)*E(3,2) MULT
 F(2,3) = D(2,1)*E(1,3) + D(2,2)*E(2,3) + D(2,3)*E(3,3) MULT
 F(3,1) = D(3,1)*E(1,1) + D(3,2)*E(2,1) + D(3,3)*E(3,1) MULT
 F(3,2) = D(3,1)*E(1,2) + D(3,2)*E(2,2) + D(3,3)*E(3,2) MULT
 F(3,3) = D(3,1)*E(1,3) + D(3,2)*E(2,3) + D(3,3)*E(3,3) MULT
 RETURN MULT

C
C
C
C

*
*
*
END

SUBROUTINE PCON

C
C
C
C

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*****
COMMON      A(3)          ,          AE(5)          ,          AED(5)          ,          COMMC
*           AFOUR(2)       ,          AII(6,3,3)       ,          COMMC
*           AIO(6,3,3)     ,          AJ1(3)        ,          ALIT           ,          COMMC
*           AOCJ(6,3,3)    ,          AOJ(3)        ,          AONE(7)        ,          COMMC
*           ATCPT2(3,3)    ,          ATHREE(5)     ,          ATWO(4)       ,          COMMC
*           A1(3,3)        ,          AIJ(2)        ,          COMMC
COMMON      BDMASS        ,          BFOUR(2)       ,          BMDM           ,          COMMC
*           BODYDI(3,3)    ,          BODYOI(3,3)     ,          BODY1I(3,3)   ,          COMMC
*           BOMASS        ,          BONE(7)        ,          BTHREE(5)     ,          COMMC
*           BTWO(4)        ,          B1MASS         ,          B2MASS         ,          COMMC
*           B3MASS        ,          B4MASS         ,          COMMC
COMMON      CA(3)         ,          CB(3)          ,          CGAINO(3)     ,          COMMC
*           CGAIN1(2)     ,          COSTTJ         ,          COSTTO         ,          COMMC
*           COSFEJ        ,          COSTT3         ,          COSTT4         ,          COMMC
*           COSTT1        ,          CP1           ,          CP2           ,          COMMC
*           C02T         ,          C1            ,          COMMC
COMMON      DB(3)         ,          DD01(3)        ,          COMMC
*           DELTAT        ,          D01(3)         ,          D01DOT(3)      ,          COMMC
*           DTI(3)        ,          COMMC
*           DTIME         ,          D12(3)         ,          D13(3)         ,          COMMC
*           D13DOT(3)     ,          D13YCS         ,          D13YSN         ,          COMMC
*           D13ZCS        ,          D13ZSN         ,          D14(3)         ,          COMMC
*           D14DOT(3)     ,          D14YCS         ,          D14YSN         ,          COMMC
*           D14ZCS        ,          D14ZSN         ,          COMMC
COMMON      EEE(3,3)     ,          EEJ(3,3)       ,          EL2(3)         ,          COMMC
*           EL2DOT(3)     ,          EL2YCS         ,          EL2YSN         ,          COMMC
*           EL2ZCS        ,          EL2ZSN         ,          EL3(3)         ,          COMMC
*           EL3DOT(3)     ,          EL3YCS         ,          EL3YSN         ,          COMMC
*           EL3ZCS        ,          EL3ZSN         ,          EL4(3)         ,          COMMC
*           EL4DOT(3)     ,          EL4YCS         ,          EL4YSN         ,          COMMC
*           EL4ZCS        ,          EL4ZSN         ,          EM(6,6)        ,          COMMC
COMMON      FAT(8)        ,          FEED(6)        ,          FFF(3)         ,          COMMC
*           FEE(6)        ,          FLAG1         ,          FLAG2         ,          COMMC
*           FFJ(3)        ,          FLAG4         ,          FNI           ,          COMMC
*           FLAG3        ,          F01(3)        ,          F02(3)        ,          COMMC
*           F0(3)         ,          F1(3)         ,          F11(3)        ,          COMMC
*           F03(3)        ,          COMMC
*           FPT(5)        ,          F13(3)        ,          COMMC
*           F12(3)        ,          G3            ,          COMMC
COMMON      GAIN(10)     ,          G4            ,          G4DOT         ,          COMMC
*           G3DOT        ,          HCMG(3)        ,          HDOT(3)       ,          COMMC
COMMON      H(3)         ,          HO(3)         ,          HW(6)         ,          COMMC
*           HI(3)         ,          H1PDOT(3)     ,          H1PRIM(3)     ,          COMMC
*           H1(3)         ,          H4PRIM(3)     ,          COMMC
COMMON      H3PRIM(3)    ,          IGFA          ,          ICFB          ,          COMMC
*           IB2F         ,          ICFD          ,          IDOCK         ,          COMMC
*           ICFC         ,          IPNDLM         ,          IPNTCK        ,          COMMC
*           IDOF(6)      ,          IPROPF        ,          COMMC
COMMON      IGRAVF       ,          NCHECK        ,          NDECK         ,          COMMC
*           IPRINT       ,          NUMCMG        ,          COMMC
COMMON      NCASE        ,          OMEGA3        ,          OMEGA4        ,          COMMC
*           NGAIN        ,          PEND3L        ,          COMMC
COMMON      OMEGA1       ,          PEND4L        ,          COMMC
*           PEND3L       ,          Q(4,4)        ,          COMMC
COMMON

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COMMON      R          .          RO(3)          .          R1(3)          .  COMMC
*          R1DOT(3)      .          R1YCS          .          R1YSN          .  COMMC
*          R1ZCS          .          R1ZSN          .          R2(3)          .  COMMC
*          R2DOT(3)      .          R2YCS          .          R2YSN          .  COMMC
*          R2ZCS          .          R2ZSN          .          R3(3)          .  COMMC
*          R3DOT(3)      .          R3YCS          .          R3YSN          .  COMMC
*          R3ZCS          .          R3ZSN          .          R4(3)          .  COMMC
*          R4DOT(3)      .          R4YCS          .          R4YSN          .  COMMC
*          R4ZCS          .          R4ZSN          .          SINFEJ          .  COMMC
COMMON      S          .          SDOT          .          SINTT1          .  COMMC
*          SINTTJ          .          SINTTO          .          SINTT2          .  COMMC
*          SINTT2          .          SINTT3          .          SINTT4          .  COMMC
*          SP          .          SUM1          .          SUM2          .  COMMC
*          SUM3          .          S2(3)          .          S3(3)          .  COMMC
*          S4(3)          .          TC(3,3)          .          TEMP1(3)          .  COMMC
COMMON      T(3,3)      .          TEMP2(3)          .          TEMP3(3)          .  COMMC
*          TEMP3(3)          .          TEMP4(3)          .          TEMP5(3,3)          .  COMMC
*          TEMP6(3,3)          .          TEMP7(3,3)          .          TEMP8(3,3)          .  COMMC
*          TEMP9(3,3)          .          TEMP10(3,3)          .          TEMP11(3,3)          .  COMMC
*          TEMP12(3,3)          .          TEMP13(3,3)          .          TEMP14(3,3)          .  COMMC
*          TEMP15(3,3)          .          TERM1(3)          .          TERM2(3)          .  COMMC
*          TFR1CT          .          THATA(6)          .          THATAD(6)          .  COMMC
*          THETA1          .          THETA3          .          THETA4          .  COMMC
*          THETA          .          TIBO(3,3)          .          TIBOJ(3,3)          .  COMMC
*          TIME          .          TJ          .          TJ1(10)          .  COMMC
*          TJ2(10)          .          TJ3(10)          .          TJ4(10)          .  COMMC
*          TMOTOR          .          TOTMAS          .          T01          .  COMMC
*          TOEF(3)          .          TQOP(3)          .          TQ1G(3)          .  COMMC
*          TQOG(3)          .          TSTART          .          TSTOP          .  COMMC
*          TQ1P(3)          .          TT3DOT          .          TT4DOT          .  COMMC
*          TT1DOT          .          T13          .          T14          .  COMMC
*          TIEF(3)          .          WS          .          W1(3)          .  COMMC
COMMON      V(3)          .          W4(3)          .          XCDOT          .  COMMC
COMMON      W0(3)          .          XC          .          COMMI
*          W3(3)          .          XMU          .          COMMI
COMMON      X(6,7)          .          .          .          .          .          .  COMMI
*          .          .          .          .          .          .          .          .  COMMI

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C
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SINTT1 = SIN(THETA1)          PCON
COSTT1 = COS(THETA1)          PCON
DO 30 M=1,3                    PCON
FS = CGAIN0(M)*W0(M)          PCON
FPT(M) = 2.*ABS(FS)           PCON
TQOP(M) = FS*AOJ(M)           PCON
30 CONTINUE                    PCON
FS = 0.                         PCON
IF (COSTT1 .GT. 0.87)FS = CGAIN1(2)*W0(2) PCON
IF (COSTT1 .LT. 0.87)FS = CGAIN1(2)*W0(2) PCON
IF (SINTT1 .GT. 0.87)FS = CGAIN1(2)*W0(3) PCON
IF (SINTT1 .LT. 0.87)FS = CGAIN1(2)*W0(3) PCON
FPT(4) = 2.*ABS(FS)           PCON
TQ1P(2) = FS*AIJ(2)           PCON
FS = CGAIN1(1)*(OMEGA1 = SP)  PCON
FPT(5) = 2.*ABS(FS)           PCON
TQ1P(1) = FS*AIJ(1)           PCON

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RETURN

PCON
PCON

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*

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END

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SUBROUTINE RECALC

C
C
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C

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*****
COMMON  A(3)          ,          AE(5)          ,          AED(5)          ,          COMMC
*        AFOUR(2)     ,          AII(6,3,3)    ,          ,          COMMC
*        AIO(6,3,3)   ,          AJ1(3)        ,          ALI             ,          COMMC
*        AOCJ(6,3,3)  ,          AOJ(3)       ,          AONE(7)         ,          COMMC
*        ATCPT2(3,3)  ,          ATHREE(5)    ,          ATWO(4)        ,          COMMC
*        A1(3,3)      ,          AJ(2)         ,          ,          COMMC
COMMON  BDMASS        ,          BFOUR(2)        ,          BMOM           ,          COMMC
*        BODYDI(3,3)  ,          BODYOI(3,3)    ,          BODY1I(3,3)   ,          COMMC
*        BOMASS       ,          BONE(7)       ,          BTHREE(5)     ,          COMMC
*        BTWO(4)      ,          B1MASS        ,          B2MASS         ,          COMMC
*        B3MASS       ,          B4MASS        ,          ,          COMMC
COMMON  CA(3)         ,          CB(3)          ,          CGAINO(3)     ,          COMMC
*        CGAIN1(2)    ,          ,          ,          COMMC
*        COSFEJ       ,          COSTTJ        ,          COSTTO         ,          COMMC
*        COSTT1       ,          COSTT3        ,          COSTT4         ,          COMMC
*        CO2T         ,          CP1           ,          CP2           ,          COMMC
*        CST          ,          C1            ,          ,          COMMC
COMMON  DB(3)         ,          DD01(3)        ,          ,          COMMC
*        DELTAT       ,          DO1(3)         ,          DO1DOT(3)     ,          COMMC
*        DTI(3)       ,          ,          ,          COMMC
*        DTIME        ,          D12(3)          ,          D13(3)         ,          COMMC
*        D13DOT(3)    ,          D13YCS          ,          D13YSN         ,          COMMC
*        D13ZCS       ,          D13ZSN          ,          D14(3)         ,          COMMC
*        D14DOT(3)    ,          D14YCS          ,          D14YSN         ,          COMMC
*        D14ZCS       ,          D14ZSN          ,          ,          COMMC
COMMON  EEE(3,3)     ,          EEJ(3,3)       ,          EL2(3)         ,          COMMC
*        EL2DOT(3)    ,          EL2YCS          ,          EL2YSN         ,          COMMC
*        EL2ZCS       ,          EL2ZSN          ,          EL3(3)         ,          COMMC
*        EL3DOT(3)    ,          EL3YCS          ,          EL3YSN         ,          COMMC
*        EL3ZCS       ,          EL3ZSN          ,          EL4(3)         ,          COMMC
*        EL4DOT(3)    ,          EL4YCS          ,          EL4YSN         ,          COMMC
*        EL4ZCS       ,          EL4ZSN          ,          EM(6,6)        ,          COMMC
COMMON  FAT(8)       ,          ,          ,          COMMC
*        FEE(6)       ,          FEED(6)        ,          FFF(3)         ,          COMMC
*        FFJ(3)       ,          FLAG1          ,          FLAG2         ,          COMMC
*        FLAG3        ,          FLAG4          ,          FN            ,          COMMC
*        FO(3)        ,          FO1(3)         ,          FO2(3)         ,          COMMC
*        FO3(3)       ,          F1(3)          ,          F11(3)         ,          COMMC
*        FPT(5)       ,          ,          ,          COMMC
*        F12(3)       ,          F13(3)         ,          ,          COMMC
COMMON  GAIN(10)     ,          G3             ,          ,          COMMC
*        G3DOT        ,          G4             ,          G4DOT          ,          COMMC
COMMON  H(3)         ,          HCMG(3)       ,          HDOT(3)        ,          COMMC
*        HI(3)        ,          HO(3)         ,          HW(6)         ,          COMMC
*        H1(3)        ,          HIPDOT(3)     ,          HIPRIM(3)     ,          COMMC
*        H3PRIM(3)    ,          H4PRIM(3)     ,          ,          COMMC
COMMON  IB2F         ,          ICFA          ,          ICFB           ,          COMMC
*        ICFC         ,          ICFD          ,          IDOCK          ,          COMMC
*        IDOF(6)      ,          ,          ,          COMMC
*        IGRAVF       ,          IPNDLM         ,          IPNTCK         ,          COMMC
*        IPRINT       ,          IPROPF         ,          ,          COMMC
COMMON  NCASE        ,          NCHECK         ,          NDECK          ,          COMMC
*        NGAIN        ,          NUMCMG         ,          ,          COMMC
COMMON  OMEGA1       ,          OMEGA3         ,          OMEGA4         ,          COMMC
COMMON  PEND3L       ,          PEND4L         ,          ,          COMMC
COMMON  Q(4,6)

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COMMON      R      ,      RO(3)      ,      R1(3)      ,      COMMC
*           R1DOT(3) ,      R1YCS      ,      R1YSN      ,      COMMC
*           R1ZCS      ,      R1ZSN      ,      R2(3)      ,      COMMC
*           R2DOT(3)  ,      R2YCS      ,      R2YSN      ,      COMMC
*           R2ZCS      ,      R2ZSN      ,      R3(3)      ,      COMMC
*           R3DOT(3)  ,      R3YCS      ,      R3YSN      ,      COMMC
*           R3ZCS      ,      R3ZSN      ,      R4(3)      ,      COMMC
*           R4DOT(3)  ,      R4YCS      ,      R4YSN      ,      COMMC
*           R4ZCS      ,      R4ZSN      ,      COMMC
COMMON      S      ,      SDOT      ,      SINFEJ      ,      COMMC
*           SINTTJ      ,      SINTTIO      ,      SINTT1      ,      COMMC
*           SINTT2      ,      SINTT3      ,      SINTT4      ,      COMMC
*           SP      ,      SUM1      ,      SUM2      ,      COMMC
*           SUM3      ,      S2(3)      ,      S3(3)      ,      COMMC
*           S4(3)      ,      COMMC
COMMON      T(3,3)  ,      TC(3,3)  ,      TEMP1(3)  ,      COMMC
*           TEMP2(3)  ,      TEMP4(3)  ,      TEMP5(3,3) ,      COMMC
*           TEMP3(3)  ,      TEMP7(3,3) ,      TEMP8(3,3) ,      COMMC
*           TEMP6(3,3) ,      TEMP10(3,3) ,      TEMP11(3,3) ,      COMMC
*           TEMP9(3,3) ,      TEMP13(3,3) ,      TEMP14(3,3) ,      COMMC
*           TEMP12(3,3) ,      TERM1(3)  ,      TERM2(3)  ,      COMMC
*           TEMP15(3,3) ,      THATA(6) ,      THATA(6)  ,      COMMC
*           TFRICT      ,      THETA3      ,      THETA4      ,      COMMC
*           THETA1      ,      TIBO(3,3)  ,      TIBO1(3,3) ,      COMMC
*           THETO      ,      TJ      ,      TJ1(10)   ,      COMMC
*           TIME      ,      TJ3(10)   ,      TJ4(10)   ,      COMMC
*           TJ2(10)   ,      TOTMAS      ,      T01      ,      COMMC
*           TMOTOR      ,      TQOP(3)   ,      TQ1G(3)   ,      COMMC
*           TOEF(3)   ,      TSTART      ,      TSTOP      ,      COMMC
*           TQOG(3)   ,      TT3DOT      ,      TT4DOT      ,      COMMC
*           TQ1P(3)   ,      T13      ,      T14      ,      COMMC
*           TT1DOT      ,      COMMC
*           T1EF(3)   ,      COMMC
COMMON      V(3)   ,      COMMC
COMMON      W0(3)   ,      WS      ,      W1(3)      ,      COMMC
*           W3(3)   ,      W4(3)      ,      COMMC
COMMON      X(6,7) ,      XC      ,      XCDOT      ,      COMMC
*           XMU      ,      COMMC

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*
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SINTT1 = SIN(THETA1)      RECAL
COSTT1 = COS(THETA1)      RECAL
CALL SCALC                RECAL
EL2(1) = D12(1) + S*S2(1) RECAL
EL2(2) = D12(2) + S*S2(2) RECAL
EL2(3) = D12(3) + S*S2(3) RECAL
SINTT3 = SIN(THETA3)      RECAL
COSTT3 = COS(THETA3)      RECAL
EL3(1) = PENDING*SINTT3   RECAL
EL3(2) = PENDING*COSTT3*S3(3) RECAL
EL3(3) = PENDING*COSTT3*S3(2) RECAL
SINTT4 = SIN(THETA4)      RECAL
COSTT4 = COS(THETA4)      RECAL
EL4(1) = PENDING*SINTT4   RECAL
EL4(2) = PENDING*COSTT4*S4(3) RECAL
EL4(3) = PENDING*COSTT4*S4(2) RECAL
R1(1) = (BOMASS/TOTMAS)*D01(1) RECAL

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C
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C

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*      = (B2MASS/TOTMAS)*EL2(1) - (B3MASS/TOTMAS)*(D13(1) + EL3(1)) RECAL
*      = (B4MASS/TOTMAS)*(D14(1) + EL4(1)) RECAL
R1(2) = (B0MASS/TOTMAS)*(D01(2)*COSTT1 + D01(3)*SINTT1) RECAL
*      = (B2MASS/TOTMAS)*EL2(2) RECAL
*      = (B3MASS/TOTMAS)*(D13(2) + EL3(2)) RECAL
*      = (B4MASS/TOTMAS)*(D14(2) + EL4(2)) RECAL
R1(3) = (B0MASS/TOTMAS)*(-D01(2)*SINTT1 + D01(3)*COSTT1) RECAL
*      = (B2MASS/TOTMAS)*EL2(3) RECAL
*      = (B3MASS/TOTMAS)*(D13(3) + EL3(3)) RECAL
*      = (B4MASS/TOTMAS)*(D14(3) + EL4(3)) RECAL
R2(1) = R1(1) + EL2(1) RECAL
R2(2) = R1(2) + EL2(2) RECAL
R2(3) = R1(3) + EL2(3) RECAL
R3(1) = R1(1) + D13(1) + EL3(1) RECAL
R3(2) = R1(2) + D13(2) + EL3(2) RECAL
R3(3) = R1(3) + D13(3) + EL3(3) RECAL
R4(1) = R1(1) + D14(1) + EL4(1) RECAL
R4(2) = R1(2) + D14(2) + EL4(2) RECAL
R4(3) = R1(3) + D14(3) + EL4(3) RECAL
RETURN RECAL

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C
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C

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*****
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*
*
END

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C
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SUBROUTINE SCALC

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*****
COMMON      A (3)          ,          AE (5)          ,          AED (5)          ,          COMMC
*           AF0UR (2)      ,          AII (6,3,3)     ,          COMMC
*           AIO (6,3,3)    ,          AJI (3)      ,          ALIT           ,          COMMC
*           AOCJ (6,3,3)   ,          AOJ (3)      ,          AONE (7)        ,          COMMC
*           ATCPT2 (3,3)   ,          ATHREE (5)   ,          ATWO (4)         ,          COMMC
*           A1 (3,3)       ,          A1J (2)       ,          COMMC
COMMON      BDMASS        ,          BFOUR (2)       ,          BMOM           ,          COMMC
*           BODYDI (3,3)   ,          BODYOI (3,3)   ,          BODY1I (3,3)    ,          COMMC
*           BOMASS        ,          BONE (7)       ,          BTHREE (5)       ,          COMMC
*           BTWO (4)       ,          B1MASS         ,          B2MASS           ,          COMMC
*           B3MASS        ,          B4MASS         ,          COMMC
COMMON      CA (3)        ,          CB (3)         ,          CGAINO (3)      ,          COMMC
*           CGAINI (2)     ,          COMMC
*           COSFEJ        ,          COSTTJ         ,          COSTTO          ,          COMMC
*           COSTT1        ,          COSTT3         ,          COSTT4          ,          COMMC
*           CO2T          ,          CP1            ,          CP2             ,          COMMC
*           CST           ,          C1              ,          COMMC
COMMON      DB (3)        ,          DD01 (3)       ,          COMMC
*           DELTAT        ,          D01 (3)         ,          D01DOT (3)      ,          COMMC
*           DTI (3)       ,          COMMC
*           DTIME         ,          D12 (3)         ,          D13 (3)         ,          COMMC
*           D13DOT (3)    ,          D13YCS         ,          D13YSN         ,          COMMC
*           D13ZCS       ,          D13ZSN         ,          D14 (3)         ,          COMMC
*           D14DOT (3)   ,          D14YCS         ,          D14YSN         ,          COMMC
*           D14ZCS       ,          D14ZSN         ,          COMMC
COMMON      EEE (3,3)    ,          EEJ (3,3)     ,          EL2 (3)         ,          COMMC
*           EL2DOT (3)    ,          EL2YCS         ,          EL2YSN         ,          COMMC
*           EL2ZCS       ,          EL2ZSN         ,          EL3 (3)         ,          COMMC
*           EL3DOT (3)   ,          EL3YCS         ,          EL3YSN         ,          COMMC
*           EL3ZCS       ,          EL3ZSN         ,          EL4 (3)         ,          COMMC
*           EL4DOT (3)   ,          EL4YCS         ,          EL4YSN         ,          COMMC
*           EL4ZCS       ,          EL4ZSN         ,          EM (6,6)        ,          COMMC
COMMON      FAT (8)      ,          COMMC
*           FEE (6)       ,          FEED (6)       ,          FFF (3)         ,          COMMC
*           FFJ (3)       ,          FLAG1          ,          FLAG2          ,          COMMC
*           FLAG3        ,          FLAG4          ,          FNI             ,          COMMC
*           FO (3)        ,          FO1 (3)        ,          FO2 (3)        ,          COMMC
*           FO3 (3)       ,          F1 (3)         ,          F11 (3)        ,          COMMC
*           FPT (5)       ,          COMMC
*           F12 (3)       ,          F13 (3)        ,          COMMC
COMMON      GAIN (10)    ,          G3              ,          COMMC
*           G3DOT        ,          G4              ,          G4DOT          ,          COMMC
COMMON      H (3)        ,          HCMG (3)       ,          HDOT (3)        ,          COMMC
*           HI (3)        ,          HO (3)         ,          HW (6)         ,          COMMC
*           H1 (3)        ,          H1PDOT (3)     ,          H1PRIM (3)     ,          COMMC
*           H3PRIM (3)    ,          H4PRIM (3)     ,          COMMC
COMMON      IB2F         ,          ICFA           ,          ICFB           ,          COMMC
*           ICFC         ,          ICFD           ,          IDOCK          ,          COMMC
*           IDOF (6)     ,          COMMC
*           IGRAVF       ,          IPNDLM         ,          IPNTCK         ,          COMMC
*           IPRINT       ,          IPROPF         ,          COMMC
COMMON      NCASE        ,          NCHECK         ,          NDECK          ,          COMMC
*           NGAIN        ,          NUMCMG         ,          COMMC
COMMON      OMEGA1       ,          OMEGA3         ,          OMEGA4         ,          COMMC
COMMON      PEND3L      ,          PEND4L         ,          COMMC
COMMON      Q (4,4)     ,          COMMC

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COMMON      R          0          R0(3)      0          R1(3)      0  COMM
*          R1DOT(3)    0          R1YCS    0          R1YSN    0  COMM
*          R1ZCS      0          R1ZSN    0          R2(3)     0  COMM
*          R2DOT(3)    0          R2YCS    0          R2YSN    0  COMM
*          R2ZCS      0          R2ZSN    0          R3(3)     0  COMM
*          R3DOT(3)    0          R3YCS    0          R3YSN    0  COMM
*          R3ZCS      0          R3ZSN    0          R4(3)     0  COMM
*          R4DOT(3)    0          R4YCS    0          R4YSN    0  COMM
*          R4ZCS      0          R4ZSN    0          COMM
COMMON      S          0          SDOT      0          SINFEJ    0  COMM
*          SINTTJ     0          SINTIO   0          SINTT1    0  COMM
*          SINTT2     0          SINTT3   0          SINTT4    0  COMM
*          SP         0          SUM1     0          SUM2     0  COMM
*          SUM3       0          S2(3)    0          S3(3)    0  COMM
*          S4(3)      0          COMM
COMMON      T(3,3)    0          TC(3,3)  0          TEMP1(3)  0  COMM
*          TEMP2(3)   0          COMM
*          TEMP3(3)   0          TEMP4(3)  0          TEMP5(3,3) 0  COMM
*          TEMP6(3,3) 0          TEMP7(3,3) 0          TEMP8(3,3) 0  COMM
*          TEMP9(3,3) 0          TEMP10(3,3) 0          TEMP11(3,3) 0  COMM
*          TEMP12(3,3) 0          TEMP13(3,3) 0          TEMP14(3,3) 0  COMM
*          TEMP15(3,3) 0          TERM1(3)  0          TERM2(3)  0  COMM
*          TFRICT     0          THATA(6)  0          THATAD(6) 0  COMM
*          THETA1     0          THETA3    0          THETA4    0  COMM
*          THETO      0          TIB0(3,3) 0          TIB0I(3,3) 0  COMM
*          TIME       0          TJ        0          TJ1(10)   0  COMM
*          TJ2(10)    0          TJ3(10)   0          TJ4(10)   0  COMM
*          TMOTOR     0          COMM
*          TOEF(3)    0          TOTMAS    0          Y01      0  COMM
*          TQOG(3)    0          TQOP(3)   0          TQ1G(3)   0  COMM
*          TQ1P(3)    0          TSTART    0          TSTOP     0  COMM
*          TT1DOT     0          TT3DOT    0          TT6DOT    0  COMM
*          T1EF(3)    0          T13       0          T14      0  COMM
COMMON      V(3)      0          COMM
COMMON      W0(3)     0          WS        0          W1(3)     0  COMM
*          W3(3)      0          W4(3)     0          COMM
COMMON      X(6,7)    0          XC        0          XCDOT     0  COMM
*          XMU        0          COMM

```

```

*****

```

```

THIS SUBROUTINE CALCULATES THE ELEVATOR POSITION

```

```

S = 0
RETURN

```

```

*****

```

```

END

```

```

SCAL
SCAL
SCAL
SCAL
SCAL

```

```

C
C
C
C
C
C
C
C
C
C
C
C

```

SUBROUTINE SDCALC

```

*
*
*****
COMMON      A(3)          ,      AE(5)          ,      AED(5)          ,      COMMC
*            AFOUR(2)     ,      AII(6,3,3)    ,      ALI             ,      COMMC
*            AIO(6,3,3)   ,      AJ1(3)      ,      ADNE(7)        ,      COMMC
*            AOCJ(6,3,3)  ,      AOJ(3)      ,      ATWO(4)        ,      COMMC
*            ATCPT2(3,3)  ,      ATHREE(5)   ,      ALJ(2)         ,      COMMC
*            A1(3,3)      ,      A1J(2)      ,      BFOUR(2)       ,      COMMC
COMMON      BDMASS       ,      BODYOI(3,3) ,      BOMOM           ,      COMMC
*            BODYDI(3,3)  ,      BONE(7)     ,      BODY1I(3,3)   ,      COMMC
*            BOMASS      ,      B1MASS     ,      BTHREE(5)     ,      COMMC
*            BTWO(4)     ,      B4MASS     ,      B2MASS        ,      COMMC
*            B3MASS     ,      CB(3)      ,      CGAINO(3)     ,      COMMC
COMMON      CA(3)       ,      CGAIN1(2)   ,      COSTTJ        ,      COMMC
*            COSFEJ      ,      COSTT1     ,      COSTT3        ,      COMMC
*            COSTT1     ,      CP1        ,      COSTT4        ,      COMMC
*            CO2T       ,      C1         ,      CP2          ,      COMMC
*            CST        ,      DD01(3)   ,      COMMC
COMMON      DB(3)       ,      DO1(3)     ,      D01DOT(3)     ,      COMMC
*            DELTAT     ,      D12(3)    ,      D13(3)        ,      COMMC
*            DTI(3)     ,      D13YCS    ,      D13YSN        ,      COMMC
*            DTIME      ,      D13ZSN    ,      D14(3)        ,      COMMC
*            D13DOT(3)  ,      D14YCS    ,      D14YSN        ,      COMMC
*            D13ZCS     ,      D14ZSN    ,      EEL(3)        ,      COMMC
COMMON      D14DOT(3)  ,      EEJ(3,3)   ,      EL2(3)        ,      COMMC
*            D14ZCS     ,      EL2YCS    ,      EL2YSN        ,      COMMC
*            EEE(3,3)   ,      EL2ZSN    ,      EL3(3)        ,      COMMC
*            EL2DOT(3)  ,      EL3YCS    ,      EL3YSN        ,      COMMC
*            EL2ZCS     ,      EL3ZSN    ,      EL4(3)        ,      COMMC
*            EL3DOT(3)  ,      EL4YCS    ,      EL4YSN        ,      COMMC
*            EL3ZCS     ,      EL4ZSN    ,      EM(6,6)      ,      COMMC
*            EL4DOT(3)  ,      FEED(6)   ,      FFF(3)        ,      COMMC
COMMON      EL4ZCS     ,      FEED(6)   ,      FLAG1         ,      COMMC
*            FAT(8)     ,      FFJ(3)    ,      FLAG2         ,      COMMC
*            FEE(6)     ,      FLAG3     ,      FLAG4         ,      COMMC
*            FFJ(3)     ,      F0(3)     ,      FNI           ,      COMMC
*            FLAG3     ,      F03(3)    ,      F02(3)        ,      COMMC
*            F0(3)     ,      F03(3)    ,      F11(3)        ,      COMMC
*            F03(3)    ,      FPT(5)    ,      F13(3)        ,      COMMC
*            FPT(5)    ,      F12(3)    ,      G3            ,      COMMC
COMMON      F12(3)    ,      G3DOT     ,      G4            ,      COMMC
*            GAIN(10)   ,      H(3)      ,      H4DOT(3)     ,      COMMC
*            G3DOT     ,      HI(3)     ,      H4PRIM(3)    ,      COMMC
COMMON      HI(3)     ,      H1(3)     ,      H1PDOT(3)    ,      COMMC
*            H1(3)     ,      H3PRIM(3) ,      H4PRIM(3)    ,      COMMC
*            H3PRIM(3) ,      IBZF      ,      ICFB          ,      COMMC
COMMON      IBZF      ,      ICFC      ,      IDOCK         ,      COMMC
*            ICFC      ,      IDOF(6)   ,      IPNDLM        ,      COMMC
*            IDOF(6)   ,      IGRAVF    ,      IPNTCK        ,      COMMC
*            IGRAVF    ,      IPRINT    ,      NCHECK        ,      COMMC
COMMON      IPRINT    ,      NCASE     ,      NDECK         ,      COMMC
*            NCASE     ,      NGAIN     ,      NUMCMG        ,      COMMC
COMMON      NGAIN     ,      OMEGA1    ,      OMEGA3        ,      COMMC
*            OMEGA1    ,      PEND3L   ,      OMEGA4        ,      COMMC
COMMON      PEND3L   ,      Q(4,4)    ,      COMMC
COMMON      Q(4,4)

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```

COMMON      R          '          R0(3)          '          R1(3)          '  COMMC
*           R1DOT(3)  '          R1YCS          '          R1YSN          '  COMMC
*           R1ZCS     '          R1ZSN          '          R2(3)          '  COMMC
*           R2DOT(3)  '          R2YCS          '          R2YSN          '  COMMC
*           R2ZCS     '          R2ZSN          '          R3(3)          '  COMMC
*           R3DOT(3)  '          R3YCS          '          R3YSN          '  COMMC
*           R3ZCS     '          R3ZSN          '          R4(3)          '  COMMC
*           R4DOT(3)  '          R4YCS          '          R4YSN          '  COMMC
*           R4ZCS     '          R4ZSN          '          COMMC
COMMON      S          '          SDOT          '          SINFEJ        '  COMMC
*           SINTTJ    '          SINTTO        '          SINTT1        '  COMMC
*           SINTT2    '          SINTT3        '          SINTT4        '  COMMC
*           SP         '          SUM1          '          SUM2          '  COMMC
*           SUM3       '          S2(3)         '          S3(3)         '  COMMC
*           S4(3)     '          COMMC
COMMON      T(3,3)    '          TC(3,3)     '          TEMP1(3)    '  COMMC
*           TEMP2(3)  '          COMMC
*           TEMP3(3)  '          TEMP4(3)     '          TEMP5(3,3)   '  COMMC
*           TEMP6(3,3)'          TEMP7(3,3)   '          TEMP8(3,3)   '  COMMC
*           TEMP9(3,3)'          TEMP10(3,3)  '          TEMP11(3,3)  '  COMMC
*           TEMP12(3,3)'          TEMP13(3,3)  '          TEMP14(3,3)  '  COMMC
*           TEMP15(3,3)'          TERM1(3)     '          TERM2(3)   '  COMMC
*           TFRIC     '          THATA(6)   '          THATAD(6) '  COMMC
*           THETA1    '          THETA3     '          THETA4     '  COMMC
*           THETO     '          TIBO(3,3)  '          TIBO1(3,3)   '  COMMC
*           TIME      '          TJ           '          TJ1(10)      '  COMMC
*           TJ2(10)   '          TJ3(10)    '          TJ4(10)      '  COMMC
*           TMOTOR    '          COMMC
*           TOEF(3)   '          TOTMAS     '          T01          '  COMMC
*           TQOG(3)   '          TQOP(3)    '          TQ1G(3)      '  COMMC
*           TQ1P(3)   '          TSTART     '          TSTOP        '  COMMC
*           TT1DOT    '          TT3DOT     '          TT4DOT      '  COMMC
*           TIEF(3)   '          T13         '          T14          '  COMMC
COMMON      V(3)     '          COMMC
COMMON      W0(3)    '          WS          '          W1(3)        '  COMMC
*           W3(3)     '          W4(3)      '          COMMC
COMMON      X(6,7)   '          XC         '          XCDOT      '  COMMC
*           XMU       '          COMMC

```

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*****

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*****

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```

THIS SUBROUTINE CALCULATES THE ELEVATOR VELOCITY.

```

```

SDOT = 0.

```

```

RETURN

```

```

*****

```

```

END

```

C
C
C
C
C
C
C
C
C

SUBROUTINE TORK01

C
C
C
C

```

*****
COMMON  A (3)          AE (5)          AED (5)          COMM
        AF0UR (2)      AII (6,3,3)         COMM
        AIO (6,3,3)    AJ1 (3)          ALIT            COMM
        AOCJ (6,3,3)   AOJ (3)          AONE (7)       COMM
        ATCPT2 (3,3)   ATHREE (5)        ATHO (4)       COMM
        A1 (3,3)       AIJ (2)          COMM
COMMON  BDMASS         BFOUR (2)         BMMO            COMM
        BODYDI (3,3)   BODYO1 (3,3)      BODY1I (3,3)   COMM
        BOMASS         BONE (7)          BTHREE (5)     COMM
        BTWO (4)       B1MASS           B2MASS         COMM
        B3MASS         B4MASS           COMM
COMMON  CA (3)        CB (3)            CGAINO (3)     COMM
        CGAIN1 (2)     COMM
        COSFEJ         COSTTJ            COSTTO         COMM
        COSTT1         COSTT3            COSTT4         COMM
        CO2T           CP1              CPR            COMM
        CST            CI              COMM
COMMON  DB (3)        DD01 (3)          DD1DOT (3)     COMM
        DELTAT         DO1 (3)            COMM
        DTI (3)        D12 (3)          D13 (3)        COMM
        DTIME          D13YCS           D13YSN         COMM
        D13DOT (3)     D13ZSN           D14 (3)        COMM
        D13ZCS         D14YCS           D14YSN         COMM
        D14DOT (3)     D14ZSN           COMM
        D14ZCS         EEJ (3,3)        EL2 (3)        COMM
COMMON  EEE (3,3)     EL2DOT (3)       EL2YCS         COMM
        EL2ZCS         EL2YSN           EL2ZSN         COMM
        EL3DOT (3)     EL3YCS           EL3 (3)        COMM
        EL3ZCS         EL3YSN           EL3ZSN         COMM
        EL4DOT (3)     EL4YCS           EL4 (3)        COMM
        EL4ZCS         EL4YSN           EL4ZSN         COMM
COMMON  FAT (8)       EL4ZSN           EM (6,6)       COMM
        FEE (6)        FEED (6)         FFF (3)        COMM
        FFJ (3)        FLAG1            FLAG2          COMM
        FLAG3         FLAG4            FNI            COMM
        FO (3)         FO1 (3)          FO2 (3)        COMM
        FO3 (3)        F1 (3)           F11 (3)        COMM
        FPT (5)        F12 (3)          F13 (3)        COMM
COMMON  F12 (3)       F13 (3)          G3              COMM
        GAIN (10)      G4              G4DOT          COMM
COMMON  G3DOT         HCMG (3)         HDOT (3)       COMM
        H (3)          HO (3)          HW (6)         COMM
        HI (3)         H1PDOT (3)      H1PRIM (3)     COMM
        H1 (3)         H4PRIM (3)      COMM
COMMON  H3PRIM (3)   ICFA             ICFS           COMM
        IB2F          ICFC            ICFD           COMM
        ICFC          IDOF (6)        IDOCK          COMM
        IDOF (6)      IGRAVF         IPNDLM         COMM
        IGRAVF        IPROPF         IPNTCK         COMM
COMMON  IPRINT       IPROPF         NDECK          COMM
        NCASE         NCHECK         OMEGA3         COMM
COMMON  NGAIN        NUMCMG         OMEGA4         COMM
COMMON  OMEGA1       OMEGA3         COMM
COMMON  PENS3L       PEND4L         COMM
COMMON  Q (4,4)

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```

COMMON   R      ,      RO(3)      ,      R1(3)      ,      COMM
*        R1DOT(3) ,      R1YCS     ,      R1YSN     ,      COMM
*        R1ZCS     ,      R1ZSN     ,      R2(3)      ,      COMM
*        R2DOT(3)  ,      R2YCS     ,      R2YSN     ,      COMM
*        R2ZCS     ,      R2ZSN     ,      R3(3)      ,      COMM
*        R3DOT(3)  ,      R3YCS     ,      R3YSN     ,      COMM
*        R3ZCS     ,      R3ZSN     ,      R4(3)      ,      COMM
*        R4DOT(3)  ,      R4YCS     ,      R4YSN     ,      COMM
*        R4ZCS     ,      R4ZSN     ,      COMM
COMMON   S      ,      SDOT       ,      SINFEJ     ,      COMM
*        SINTTJ    ,      SINTTO    ,      SINTT1     ,      COMM
*        SINTT2    ,      SINTT3    ,      SINTT4     ,      COMM
*        SP        ,      SUM1      ,      SUM2      ,      COMM
*        SUM3      ,      S2(3)     ,      S3(3)     ,      COMM
*        S4(3)     ,      COMM
COMMON   T(3,3)   ,      TC(3,3)   ,      TEMP1(3)   ,      COMM
*        TEMP2(3)   ,      COMM
*        TEMP3(3)   ,      TEMP4(3)   ,      TEMP5(3,3)  ,      COMM
*        TEMP6(3,3) ,      TEMP7(3,3) ,      TEMP8(3,3)  ,      COMM
*        TEMP9(3,3) ,      TEMP10(3,3) ,      TEMP11(3,3) ,      COMM
*        TEMP12(3,3) ,      TEMP13(3,3) ,      TEMP14(3,3) ,      COMM
*        TEMP15(3,3) ,      TERM1(3)   ,      TERM2(3)   ,      COMM
*        TFRICT     ,      THATA(6)   ,      THATAD(6)  ,      COMM
*        THETA1     ,      THETA3     ,      THETA4     ,      COMM
*        THETO      ,      TIBO(3,3)  ,      TIBO1(3,3)  ,      COMM
*        TIME       ,      TJ         ,      TJ1(10)    ,      COMM
*        TJ2(10)    ,      TJ3(10)    ,      TJ4(10)    ,      COMM
*        TMOTOR     ,      COMM
*        TOEF(3)    ,      TOTMAS     ,      T01        ,      COMM
*        TQOG(3)    ,      TQOP(3)    ,      TQ1G(3)    ,      COMM
*        TQ1P(3)    ,      TSTART     ,      TSTOP      ,      COMM
*        TT1DOT     ,      TT3DOT     ,      TT4DOT     ,      COMM
*        T1EF(3)    ,      T13        ,      T14        ,      COMM
COMMON   V(3)     ,      COMM
COMMON   W0(3)     ,      WS         ,      W1(3)      ,      COMM
*        W3(3)     ,      W4(3)      ,      COMM
COMMON   X(6,7)   ,      XC         ,      XCDOT      ,      COMM
*        XMU       ,      COMM

```

```

*****
*
*
*****

```

THIS SUBROUTINE COMPUTES THE TORQUE BETWEEN BODY 0 AND BODY 1.
THIS TORQUE CONSISTS OF THE CONTROL TORQUE AND FRICTION TORQUE.

```

IF (TIME .NE. TSTART) GO TO 10
XC=-GAIN(2)*OMEGA1
AFOUR(2)=XC
10  CONTINUE
AFOUR(1)=TIME
BFOUR(1)=DELTA T
XCDOT=GAIN(3)*(OMEGA1-SP)
BFOUR(2)=XCDOT
CALL FOMS(AFOUR,BFOUR,2,FLAG4,TJ4)
XC=AFOUR(2)
TMOTOR=GAIN(2)*OMEGA1+XC
TFRICT=GAIN(1)*SIN(OMEGA1)
T01=TMOTOR+TFRICT
RETURN

```

C
C
C
C
C
C
C
C
C
C

C
C
C
C

TORK

*

*

END

SUBROUTINE TORK13(T13,CP1,CP2,THETA3,OMEGA3)

*

*

THIS SUBROUTINE COMPUTES THE TORQUE BETWEEN BODY 1 AND BODY 3.
THIS TORQUE CONSISTS OF THE CONTROL TORQUE AND FRICTION TORQUE.

TORK1

TORK1

TORK1

TORK1

TORK1

TORK1

TORK1

T13 = - CP1*OMEGA3 - CP2*THETA3

RETURN

*

*

END

C
C
C
C
C
C

C
C
C
C

C
C
C
C
C
C
C
C
C
C
C

SUBROUTINE TORQ14(T14,CP1,CP2,THETA4,OMEGA4)

*
*

THIS SUBROUTINE COMPUTES THE TORQUE BETWEEN BODY 1 AND BODY 4.
THIS TORQUE CONSISTS OF THE CONTROL TORQUE AND FRICTION TORQUE.

TORQ1
TORQ1
TORQ1
TORQ1
TORQ1
TORQ1

T14 = CP1*OMEGA4 + CP2*(THETA4 - 3.14159)

RETURN

*
*
END

SUBROUTINE XDOT

C
C
C
C

```

*****
COMMON  A(3)      ,      AE(5)      ,      AED(5)      ,      COMMC
*        AFOUR(2) ,      AII(6,3,3) ,      ALI      ,      COMMC
*        AIO(6,3,3) ,      AJ1(3)   ,      ALI      ,      COMMC
*        AOCJ(6,3,3) ,      AOJ(3)   ,      ADNE(7)   ,      COMMC
*        ATCPT2(3,3) ,      ATHREE(5) ,      ATWO(4)   ,      COMMC
*        A1(3,3)    ,      A1J(2)   ,      COMMC
COMMON  BDMASS    ,      BFOUR(2)   ,      BMOM      ,      COMMC
*        BODYDI(3,3) ,      BODYDI(3,3) ,      BODY1I(3,3) ,      COMMC
*        BOMASS     ,      BONE(7)   ,      BTHREE(5)   ,      COMMC
*        BTWO(4)    ,      B1MASS   ,      B2MASS     ,      COMMC
*        B3MASS     ,      B4MASS   ,      COMMC
COMMON  CA(3)     ,      CB(3)     ,      CGAINO(3)  ,      COMMC
*        CGAIN1(2)  ,      COMMC
*        COSFEJ    ,      COSTTJ   ,      COSTTO    ,      COMMC
*        COSTT1    ,      COSTT3   ,      COSTT4    ,      COMMC
*        CO2T      ,      CP1      ,      CPR       ,      COMMC
*        CST       ,      C1       ,      COMMC
COMMON  DB(3)     ,      DD01(3)  ,      COMMC
*        DELTAT    ,      D01(3)   ,      D01DOT(3)  ,      COMMC
*        DTI(3)    ,      COMMC
*        DTIME     ,      D12(3)   ,      D13(3)    ,      COMMC
*        D13DOT(3) ,      D13YCS   ,      D13YSN    ,      COMMC
*        D13ZCS    ,      D13ZSN   ,      D14(3)    ,      COMMC
*        D14DOT(3) ,      D14YCS   ,      D14YSN    ,      COMMC
*        D14ZCS    ,      D14ZSN   ,      COMMC
COMMON  EEE(3,3)  ,      EEJ(3,3)  ,      EL2(3)    ,      COMMC
*        EL2DOT(3) ,      EL2YCS   ,      EL2YSN    ,      COMMC
*        EL2ZCS    ,      EL2ZSN   ,      EL3(3)    ,      COMMC
*        EL3DOT(3) ,      EL3YCS   ,      EL3YSN    ,      COMMC
*        EL3ZCS    ,      EL3ZSN   ,      EL4(3)    ,      COMMC
*        EL4DOT(3) ,      EL4YCS   ,      EL4YSN    ,      COMMC
*        EL4ZCS    ,      EL4ZSN   ,      EM(6,6)   ,      COMMC
COMMON  FAT(8)    ,      COMMC
*        FEE(6)    ,      FEED(6)  ,      FFF(3)    ,      COMMC
*        FFJ(3)    ,      FLAG1    ,      FLAG2    ,      COMMC
*        FLAG3    ,      FLAG4    ,      FN       ,      COMMC
*        FO(3)     ,      F01(3)   ,      F02(3)   ,      COMMC
*        F03(3)   ,      F1(3)    ,      F11(3)   ,      COMMC
*        FPT(5)    ,      COMMC
*        F12(3)    ,      F13(3)   ,      COMMC
COMMON  GAIN(10)  ,      G3       ,      COMMC
*        G3DOT    ,      G4       ,      G4DOT    ,      COMMC
COMMON  H(3)      ,      HCMG(3)  ,      HDOT(3)  ,      COMMC
*        HI(3)    ,      HO(3)    ,      HW(6)    ,      COMMC
*        H1(3)    ,      H1PDOT(3) ,      H1PRIM(3) ,      COMMC
*        H3PRIM(3) ,      H4PRIM(3) ,      COMMC
COMMON  IB2F      ,      ICFA     ,      ICFB     ,      COMMC
*        ICFC     ,      ICFD     ,      IDOCK    ,      COMMC
*        IDOF(6)  ,      COMMC
*        IGRAVF   ,      IPNDLM   ,      IPNTCK   ,      COMMC
*        IPRINT   ,      IPROPF   ,      COMMC
COMMON  NCASE     ,      NCHECK   ,      NDECK    ,      COMMC
*        NGAIN    ,      NUMCMG   ,      COMMC
COMMON  OMEGA1    ,      OMEGA3   ,      OMEGA4   ,      COMMC
COMMON  PEND3L    ,      PEND4L   ,      COMMC
COMMON  Q(4,4)    ,      COMMC

```



```

W3(3) = OMEGA3*S3(3) + W1(3)
EL3DOT(1) = -W3(3)*EL3(2) + W3(2)*EL3(3)
EL3DOT(2) = W3(3)*EL3(1) - W3(1)*EL3(3)
EL3DOT(3) = -W3(2)*EL3(1) + W3(1)*EL3(2)
W4(1) = W1(1)
W4(2) = OMEGA4*S4(2) + W1(2)
W4(3) = OMEGA4*S4(3) + W1(3)
EL4DOT(1) = -W4(3)*EL4(2) + W4(2)*EL4(3)
EL4DOT(2) = W4(3)*EL4(1) - W4(1)*EL4(3)
EL4DOT(3) = -W4(2)*EL4(1) + W4(1)*EL4(2)
D01DOT(1) = -W0(3)*D01(2) + W0(2)*D01(3)
D01DOT(2) = W0(3)*D01(1) - W0(1)*D01(3)
D01DOT(3) = -W0(2)*D01(1) + W0(1)*D01(2)
D13DOT(1) = -W1(3)*D13(2) + W1(2)*D13(3)
D13DOT(2) = W1(3)*D13(1) - W1(1)*D13(3)
D13DOT(3) = -W1(2)*D13(1) + W1(1)*D13(2)
D14DOT(1) = -W1(3)*D14(2) + W1(2)*D14(3)
D14DOT(2) = W1(3)*D14(1) - W1(1)*D14(3)
D14DOT(3) = -W1(2)*D14(1) + W1(1)*D14(2)
R1DOT(1) = (B0MASS/TOTMAS)*D01DOT(1)
*      = (B2MASS/TOTMAS)*EL2DOT(1)
*      = (B3MASS/TOTMAS)*(D13DOT(1) + EL3DOT(1))
*      = (B4MASS/TOTMAS)*(D14DOT(1) + EL4DOT(1))
R1DOT(2) = (B0MASS/TOTMAS)*(D01DOT(2)*COSTT1 + D01DOT(3)*SINTT1)
*      = (B2MASS/TOTMAS)*EL2DOT(2)
*      = (B3MASS/TOTMAS)*(D13DOT(2) + EL3DOT(2))
*      = (B4MASS/TOTMAS)*(D14DOT(2) + EL4DOT(2))
R1DOT(3) = (B0MASS/TOTMAS)*(-D01DOT(2)*SINTT1 + D01DOT(3)*COSTT1)
*      = (B2MASS/TOTMAS)*EL2DOT(3)
*      = (B3MASS/TOTMAS)*(D13DOT(3) + EL3DOT(3))
*      = (B4MASS/TOTMAS)*(D14DOT(3) + EL4DOT(3))
R2DOT(1) = R1DOT(1) + EL2DOT(1)
R2DOT(2) = R1DOT(2) + EL2DOT(2)
R2DOT(3) = R1DOT(3) + EL2DOT(3)
R3DOT(1) = R1DOT(1) + D13DOT(1) + EL3DOT(1)
R3DOT(2) = R1DOT(2) + D13DOT(2) + EL3DOT(2)
R3DOT(3) = R1DOT(3) + D13DOT(3) + EL3DOT(3)
R4DOT(1) = R1DOT(1) + D14DOT(1) + EL4DOT(1)
R4DOT(2) = R1DOT(2) + D14DOT(2) + EL4DOT(2)
R4DOT(3) = R1DOT(3) + D14DOT(3) + EL4DOT(3)
CALL MULT(H0,BODY0I,W0,DUM,DUM,DUM,1)
CALL MULT(H1,BODY1I,W1,DUM,DUM,DUM,1)
H3PRIM(1) = B3MASS*(-EL3(3)*R3DOT(2) + EL3(2)*R3DOT(3))
H3PRIM(2) = B3MASS*( EL3(3)*R3DOT(1) - EL3(1)*R3DOT(3))
H3PRIM(3) = B3MASS*(-EL3(2)*R3DOT(1) + EL3(1)*R3DOT(2))
H4PRIM(1) = B4MASS*(-EL4(3)*R4DOT(2) + EL4(2)*R4DOT(3))
H4PRIM(2) = B4MASS*( EL4(3)*R4DOT(1) - EL4(1)*R4DOT(3))
H4PRIM(3) = B4MASS*(-EL4(2)*R4DOT(1) + EL4(1)*R4DOT(2))
H1PRIM(2) = H1(2) + H3PRIM(2) + H4PRIM(2)
*      = B2MASS*( -EL2(3)*R2DOT(1) + EL2(1)*R2DOT(3))
*      = B3MASS*( -D13(3)*R3DOT(1) + D13(1)*R3DOT(3))
*      = B4MASS*( -D14(3)*R4DOT(1) + D14(1)*R4DOT(3))
H1PRIM(3) = H1(3) + H3PRIM(3) + H4PRIM(3)
*      = B2MASS*( EL2(2)*R2DOT(1) - EL2(1)*R2DOT(2))
*      = B3MASS*( D13(2)*R3DOT(1) - D13(1)*R3DOT(2))
*      = B4MASS*( D14(2)*R4DOT(1) - D14(1)*R4DOT(2))
IF (TIME .NE. TSTART) GO TO 5
H1PRIM(1) = H1(1) + H3PRIM(1) + H4PRIM(1)
*      = B2MASS*(EL2(3)*R2DOT(2) - EL2(2)*R2DOT(3))
*      = B3MASS*(D13(3)*R3DOT(2) - D13(2)*R3DOT(3))
*      = B4MASS*(D14(3)*R4DOT(2) - D14(2)*R4DOT(3))
LET US DEFINE SOME INTERMEDIATE VALUES NEEDED TO COMPUTE H.

```

C

```

SUM1 = B1MASS*R1DOT(1) + B2MASS*R2DOT(1)
*      + B3MASS*R3DOT(1) + B4MASS*R4DOT(1)
SUM2 = B1MASS*R1DOT(2) + B2MASS*R2DOT(2)
*      + B3MASS*R3DOT(2) + B4MASS*R4DOT(2)
SUM3 = B1MASS*R1DOT(3) + B2MASS*R2DOT(3)
*      + B3MASS*R3DOT(3) + B4MASS*R4DOT(3)
C   CALCULATE H0
DO 4 I=1,3
HCMG(I) = FFF(I)
DO 4 J=1,3
HCMG(I) = EEE(I,J)*HO(J) + HCMG(I)
4 CONTINUE
H(1) = HO(1) + H1PRIM(1)
*      + (-DO1(3)*COSTT1 + DO1(2)*SINTT1)*SUM2
*      + ( DO1(3)*SINTT1 + DO1(2)*COSTT1)*SUM3
*      + HCMG(1)
H(2) = HO(2) + COSTT1*H1PRIM(2) - SINTT1*H1PRIM(3)
*      + DO1(3)*SUM1 - DO1(1)*SINTT1*SUM2 - DO1(1)*COSTT1*SUM3
*      + HCMG(2)
H(3) = HO(3) + SINTT1*H1PRIM(2) + COSTT1*H1PRIM(3)
*      + DO1(2)*SUM1 + DO1(1)*COSTT1*SUM2 - DO1(1)*SINTT1*SUM3
*      + HCMG(3)
5 CONTINUE
C   COMPUTE THE UNIT VECTOR J1.
AJ1(1) = B2MASS*EL2(1)
*      + B3MASS*D13(1) + B3MASS*EL3(1)
*      + B4MASS*D14(1) + B4MASS*EL4(1)
AJ1(2) = B2MASS*EL2(2)
*      + B3MASS*D13(2) + B3MASS*EL3(2)
*      + B4MASS*D14(2) + B4MASS*EL4(2)
AJ1(3) = B2MASS*EL2(3)
*      + B3MASS*D13(3) + B3MASS*EL3(3)
*      + B4MASS*D14(3) + B4MASS*EL4(3)
C   UPDATE THE ORBIT ANGLE
THETO = TIME*WS
IF (IGRAVF .EQ. 0) GO TO 10
C   CALCULATE THE GRAVITY GRADIENT FORCES AND TORQUES.
CALL GGRAD
10 CONTINUE
C   SUM THE FORCES ON BODY ZERO.
FO(1) = FO1(1)
FO(2) = FO1(2)
FO(3) = FO1(3)
C   SUM THE FORCES ON BODY ONE.
F1(1) = F11(1)
F1(2) = F11(2)
F1(3) = F11(3)
C   SUM THE TORQUES ON BODY ZERO.
TOEF(1) = TQOG(1) + TQOP(1)
TOEF(2) = TQOG(2) + TQOP(2)
TOEF(3) = TQOG(3) + TQOP(3)
C   SUM THE TORQUES ON BODY ONE.
T1EF(1) = TQ1G(1) + TQ1P(1)
T1EF(2) = TQ1G(2) + TQ1P(2)
T1EF(3) = TQ1G(3) + TQ1P(3)
C   LET US DEFINE SOME INTERMEDIATE TERMS USED TO CALCULATE HDOT.
TERM1(1) = (BOMASS - TOTMAS)*DO1(1) - AJ1(1)
TERM1(2) = (BOMASS - TOTMAS)*DO1(2)
*      + COSTT1*AJ1(2) + SINTT1*AJ1(3)
TERM1(3) = (BOMASS - TOTMAS)*DO1(3)
*      + SINTT1*AJ1(2) - COSTT1*AJ1(3)
TERM2(1) = BOMASS*DO1(1) - AJ1(1)

```

```

TERM2(2) = BOMASS*( COSTT1*DO1(2) + SINTT1*DO1(3)) - AJ1(2)
TERM2(3) = BOMASS*(-SINTT1*DO1(2) + COSTT1*DO1(3)) - AJ1(3)
ATCPT2(1,1) = 0
ATCPT2(1,2) = -TERM2(3)
ATCPT2(1,3) = TERM2(2)
ATCPT2(2,1) = COSTT1*TERM2(3) + SINTT1*TERM2(2)
ATCPT2(2,2) = -SINTT1*TERM2(1)
ATCPT2(2,3) = -COSTT1*TERM2(1)
ATCPT2(3,1) = SINTT1*TERM2(3) - COSTT1*TERM2(2)
ATCPT2(3,2) = COSTT1*TERM2(1)
ATCPT2(3,3) = -SINTT1*TERM2(1)
HDOT(1) = WO(3)*H(2) - WO(2)*H(3)
*
* (-TERM1(3)*FO(2) + TERM1(2)*FO(3))/TOTMAS
** (ATCPT2(1,1)*F1(1)+ATCPT2(1,2)*F1(2)+ATCPT2(1,3)*F1(3))/TOTMAS
** TOEF(1) + T1EF(1)
HDOT(2) = -WO(3)*H(1) + WO(1)*H(3)
*
* ( TERM1(3)*FO(1) - TERM1(1)*FO(3))/TOTMAS
** (ATCPT2(2,1)*F1(1)+ATCPT2(2,2)*F1(2)+ATCPT2(2,3)*F1(3))/TOTMAS
** TOEF(2) + COSTT1*T1EF(2) - SINTT1*T1EF(3)
HDOT(3) = WO(2)*H(1) - WO(1)*H(2)
*
* (-TERM1(2)*FO(1) + TERM1(1)*FO(2))/TOTMAS
** (ATCPT2(3,1)*F1(1)+ATCPT2(3,2)*F1(2)+ATCPT2(3,3)*F1(3))/TOTMAS
** TOEF(3) + SINTT1*T1EF(2) + COSTT1*T1EF(3)
C
CALCULATE THE TORQUE BETWEEN BODY 0 AND BODY 1. (CONTROL, FRICTION)
CALL TORK01
H1PDOT(1) = -W1(2)*H1PRIM(3) + W1(3)*H1PRIM(2)
*
* R1DOT(2)*(-B2MASS*EL2DOT(3)-B3MASS*(D13DOT(3)+EL3DOT(3))-
* B4MASS*(D14DOT(3)+EL4DOT(3)))-R1DOT(3)*(-B2MASS*EL2DOT(2)-
* B3MASS*(D13DOT(2)+EL3DOT(2))-B4MASS*(D14DOT(2)+EL4DOT(2)))
** -AJ1(2)*(-FO(2)*SINTT1/TOTMAS+FO(3)*COSTT1/TOTMAS)
** +AJ1(3)*( FO(2)*COSTT1/TOTMAS+FO(3)*SINTT1/TOTMAS)
** +AJ1(3)*F1(2)/TOTMAS-AJ1(2)*F1(3)/TOTMAS+T1EF(1)*T01
C
CALCULATE THE TORQUE BETWEEN BODY 1 AND BODY 3. (CONTROL, FRICTION)
CALL TORK13(T13,CP1,CP2,THETA3,OMEGA3)
G3DOT=-S3(2)*(W1(3)*H3PRIM(1)-W1(1)*H3PRIM(3))-S3(3)*(W1(1)*H3PRIM(2)
*(2)-W1(2)*H3PRIM(1))+B3MASS*S3(2)*(EL3DOT(3)+R3DOT(1)-EL3DOT(1)+R3DOT
*(3))+B3MASS*S3(3)*(EL3DOT(1)+R3DOT(2)-EL3DOT(2)+R3DOT(1))-
*(B3MASS/TOTMAS)*S3(2)*(EL3(3)*(FO(1)+F1(1))-EL3(1)*(-FO(2)*SINTT1+
*FO(3)*COSTT1+F1(3)))-(B3MASS/TOTMAS)*S3(3)*(EL3(1)*(-FO(2)*COSTT1+
*FO(3)*SINTT1+F1(2))-EL3(2)*(FO(1)+F1(1)))+T13
C
CALCULATE THE TORQUE BETWEEN BODY 1 AND BODY 4. (CONTROL, FRICTION)
CALL TORK14(T14,CP1,CP2,THETA4,OMEGA4)
G4DOT=-S4(2)*(W1(3)*H4PRIM(1)-W1(1)*H4PRIM(3))-S4(3)*(W1(1)*H4PRIM(2)
*(2)-W1(2)*H4PRIM(1))+B4MASS*S4(2)*(EL4DOT(3)+R4DOT(1)-EL4DOT(1)+R4DOT
*(3))+B4MASS*S4(3)*(EL4DOT(1)+R4DOT(2)-EL4DOT(2)+R4DOT(1))-
*(B4MASS/TOTMAS)*S4(2)*(EL4(3)*(FO(1)+F1(1))-EL4(1)*(-FO(2)*SINTT1+
*FO(3)*COSTT1+F1(3)))-(B4MASS/TOTMAS)*S4(3)*(EL4(1)*(-FO(2)*COSTT1+
*FO(3)*SINTT1+F1(2))-EL4(2)*(FO(1)+F1(1)))+T14
RETURN
*****
*
*
*
END

```

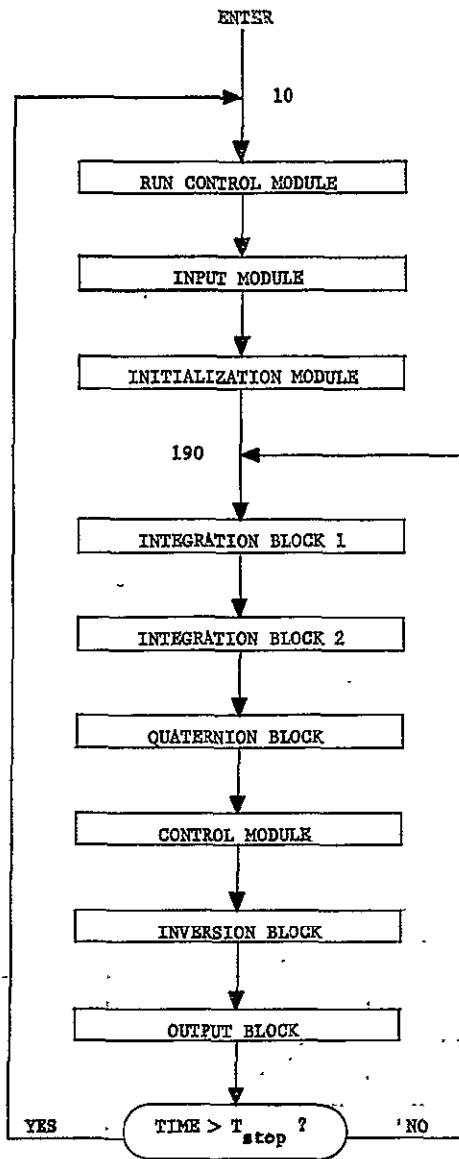
C
C
C
C

APPENDIX D, PROGRAM FLOW CHARTS

FLOW CHART & BLOCK DIAGRAM

FORM DEN 1102-01 (4-64)

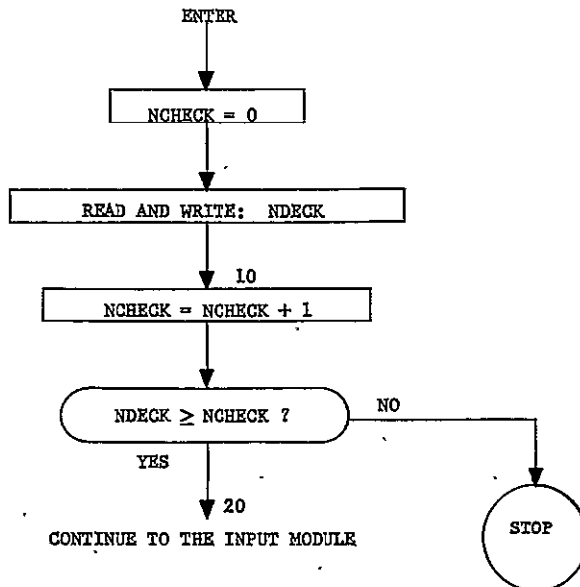
Application MAIN PROGRAM FLOW CHART Date OCTOBER 1970 Page 1 of 1
Procedure _____ Drawn By GARY JOHNSON



FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 14-643

Application RUN CONTROL MODULE Date OCTOBER 1970 Page 1 of 1
Procedure _____ Drawn By GARY JOHNSON



FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application INPUT MODULE Date OCTOBER 1970 Page 1 of 5
 Procedure _____ Drawn By GARY JOHNSON

ENTER
↓

```

----- GAIN(M) = 0. M=1,10
WRITE: NCHECK
READ AND WRITE:
IPNDLM
IPRINT
T_start, T_stop, Δt
ALT
[I, B0]I
wox, woy, woz
m0
[I0]
NUMCMG
    
```

↓
 .NUMCMG = 0 ? YES
 NO

```

DO 110 J = 1, NUMCMG
READ AND WRITE:
IDOF (J)
HwJ
[θ, CJ]
IF (IDOF (J) .EQ. 0) GO TO 110
READ AND WRITE:
[IIJ]
θJ
CJ
βJ = 0.
δJ = 0.
IF (IDOF (J) .EQ. 1) GO TO 110
READ AND WRITE:
[IOJ]
βJ
δJ
110 CONTINUE
    
```

120 ←

CONTINUE TO THE NEXT PAGE

FLOW CHART & BLOCK DIAGRAM

Application: INPUT MODULE CONTINUED

Date: OCTOBER 1970

Page: 2 of 5

Procedure: _____

Drawn By: GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

READ AND WRITE: IPROFF

IPROFF = 0 ?

YES

NO

READ AND WRITE: IATTIF

IATTIF = 0 ?

YES

NO

READ AND WRITE:
CA (1), CA (2), CA (3)

125

DO 130 J = 1, 3
READ AND WRITE:
A_{oJ}, CGAIN_{oJ}
130 CONTINUE

140

CONTINUE TO THE NEXT PAGE

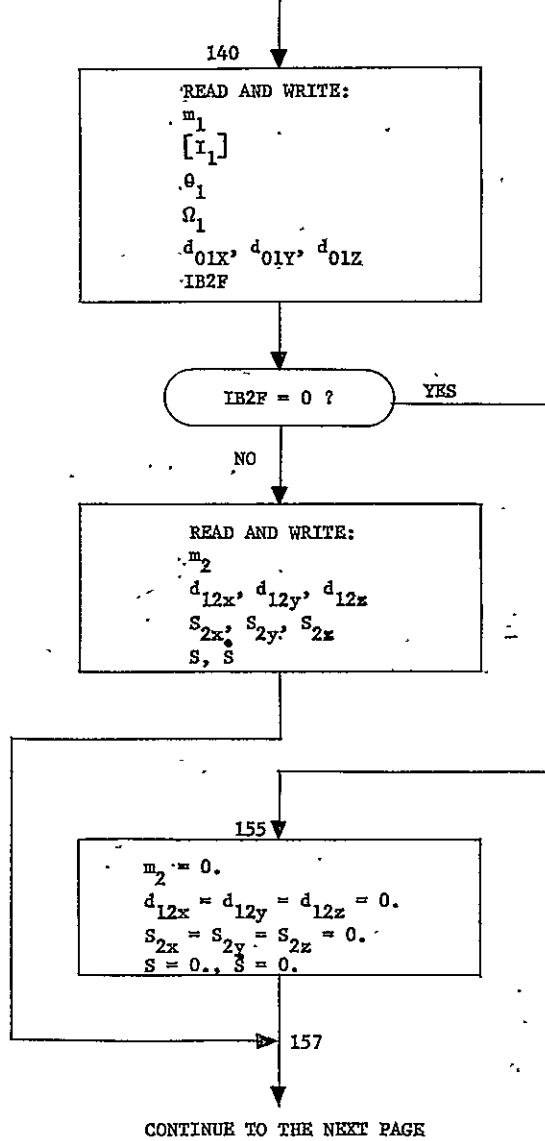
11-1-70

FLOW CHART & BLOCK DIAGRAM

FORM DE 1103-01 (4-64)

Application INPUT MODULE CONTINUED Date OCTOBER 1970 Page 3 of 5
 Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



CONTINUE TO THE NEXT PAGE

FOLD TO PREVIOUS PAGE

FLOW CHART & BLOCK DIAGRAM

FORM DE. 1103-01 (1-64)

Application INPUT MODULE CONTINUED Date OCTOBER 1970 Page 4 of 5

Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

157

I_{PROFF} = 0 ?

YES

NO

```

DO 160 J = 1, 2
READ AND WRITE:
  A1J, CGAIN1J
160 CONTINUE
    
```

170

I_{PNDIM} = 0 ?

YES

NO

```

READ AND WRITE:
CP1
CP2
m3
d13x, d13y, d13z
s3x, s3y, s3z
l3
θ3
Ω3
m4
d14x, d14y, d14z
s4x, s4y, s4z
l4
θ4
Ω4
    
```

172

```

m3 = 0., CP1 = CP2 = 0.
d13x = d13y = d13z = 0.
s3x = s3y = s3z = 0.
l3 = θ3 = Ω3 = 0.
m4 = 0.
d14x = d14y = d14z = 0.
s4x = s4y = s4z = 0.
l4 = θ4 = Ω4 = 0.
    
```

174

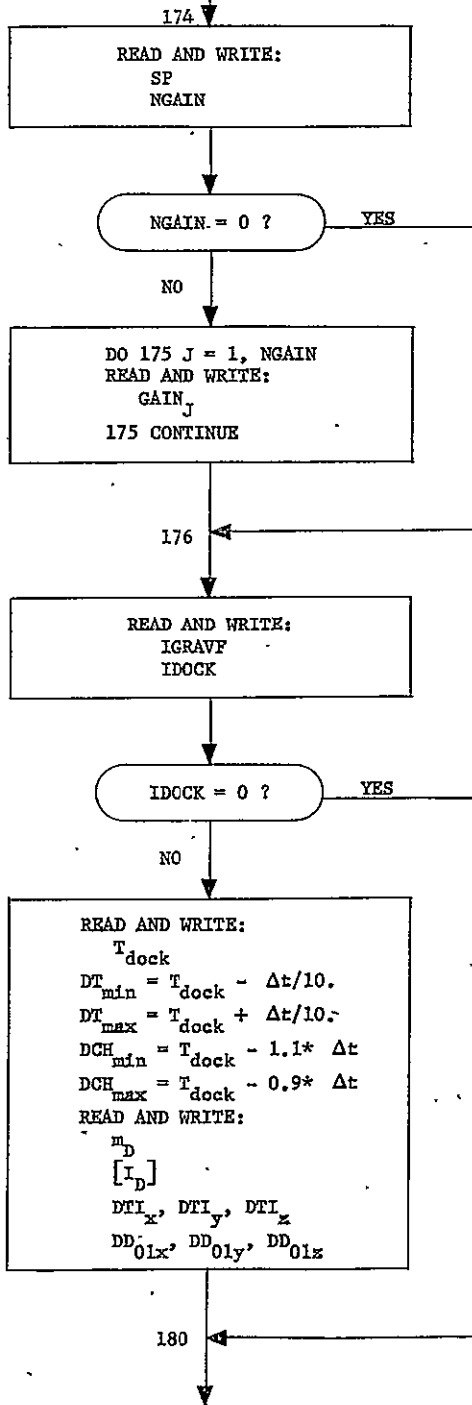
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3 of photos of P151

Fig. 40. FLOWCHART & BLOCK DIAGRAM
FORM NO. 1103-01 (2-64)

Application INPUT MODULE CONTINUED Date OCTOBER 1970 Page 5 of 5
 Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



CONTINUE TO THE INITIALIZATION MODULE

FLOW CHART & BLOCK DIAGRAM

Application INITIALIZATION MODULE

Date OCTOBER 1970

Page 1 of 1

Procedure _____

Drawn By GARY JOHNSON

ENTER

```

m = m0 + m1 + m2 + m3 + m4
ICFA = ICFB = ICFC = ICFD = 0.
FLAG 1 = FLAG 2 = FLAG 3 = FLAG 4 = 0.
λ2 = 1.
λ3 = λ4 = λ5 = 0.
λ̇2 = 1.
λ̇3 = λ̇4 = λ̇5 = 0.
A22 = θ1
A23 = θ3
A24 = θ4
A32 = 1.
A33 = A34 = A35 = 0.
IENTCK = 1
TIME = Tstart
μ = 1.408 × 1016
R = ALT + 3960.
R = 5280 * R
C1 = μ/R3
ws = √C1
F01x = F01y = F01z = 0.
F02x = F02y = F02z = 0.
F0x = F0y = F0z = 0.
F11x = F11y = F11z = 0.
F12x = F12y = F12z = 0.
FLx = FLy = FLz = 0.
TQ0Gx = TQ0Gy = TQ0Gz = 0.
TQ0Px = TQ0Py = TQ0Pz = 0.
TQ1Gx = TQ1Gy = TQ1Gz = 0.
TQ1Px = TQ1Py = TQ1Pz = 0.
TAP = TBP = 0.
FFF(M) = 0. M = 1, 3
    
```

NUMCMG = 0 ? YES

NO

CALL CMG

```

DO 183 J = 1, NUMCMG
θJ = θJ - θ̇J * Δt
φJ = φJ - φ̇J * Δt
183 CONTINUE
    
```

184

CALL XDOT

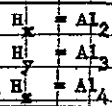
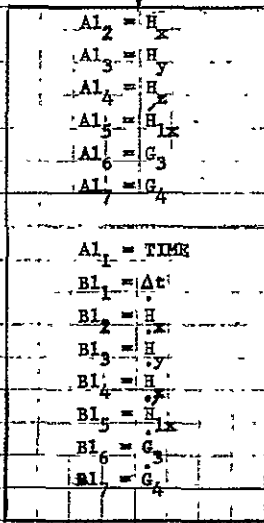
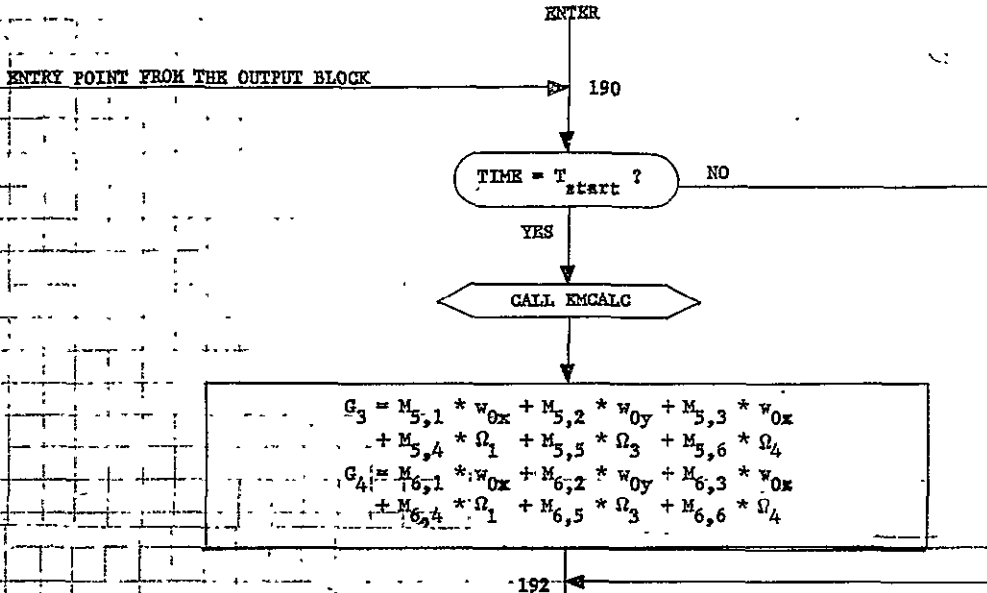
CONTINUE TO INTEGRATION BLOCK 1

FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application INTEGRATION BLOCK 1 Date OCTOBER 1970 Page 1 of 2

Procedure _____ Drawn By GARY JOHNSON



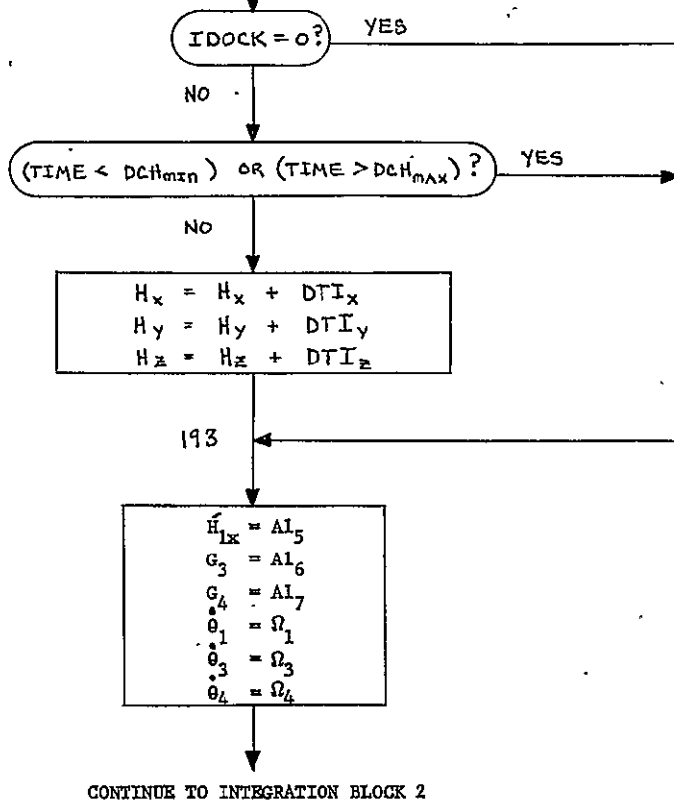
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FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-54)

Application INTEGRATION BLOCK 1 CONTINUED Date OCTOBER 1970 Page 2 of 2
 Procedure _____ Drawn By GARY JOHNSON

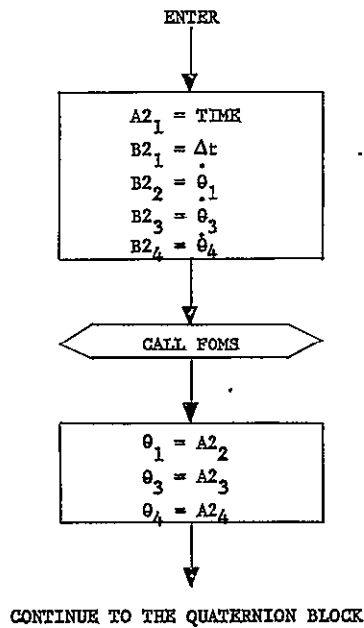
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FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application INTEGRATION BLOCK 2 Date OCTOBER 1970 Page 1 of 1
Procedure _____ Drawn By GARY JOHNSON



FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (2-64)

Application QUATERNION BLOCK Date OCTOBER 1970 Page 1 of 1
 Procedure _____ Drawn By GARY JOHNSON

ENTER

$$[Q] = \frac{1}{2} \begin{bmatrix} 0. & -w_{0x} & -w_{0y} & -w_{0z} \\ w_{0x} & 0. & w_{0z} & -w_{0y} \\ w_{0y} & -w_{0z} & 0. & w_{0x} \\ w_{0z} & w_{0y} & -w_{0x} & 0. \end{bmatrix}$$

$$\begin{bmatrix} x_2 \\ x_3 \\ x_4 \\ x_5 \end{bmatrix} = [Q] \begin{bmatrix} \lambda_2 \\ \lambda_3 \\ \lambda_4 \\ \lambda_5 \end{bmatrix}$$

$A3_1 = \text{TIME}$
 $B3_1 = \Delta t$
 $B3_2 = x_2$
 $B3_3 = x_3$
 $B3_4 = x_4$
 $B3_5 = x_5$

CALL FOMS

$$\begin{aligned} \lambda_2 &= A3_2 \\ \lambda_3 &= A3_3 \\ \lambda_4 &= A3_4 \\ \lambda_5 &= A3_5 \\ F_N &= \sqrt{\lambda_2^2 + \lambda_3^2 + \lambda_4^2 + \lambda_5^2} \\ \lambda_2 &= \lambda_2 / F_N \\ \lambda_3 &= \lambda_3 / F_N \\ \lambda_4 &= \lambda_4 / F_N \\ \lambda_5 &= \lambda_5 / F_N \\ T_{1,1} &= \lambda_2^2 + \lambda_3^2 - \lambda_4^2 - \lambda_5^2 \\ T_{1,2} &= 2 * (\lambda_3 \lambda_4 - \lambda_2 \lambda_5) \\ T_{1,3} &= 2 * (\lambda_3 \lambda_5 + \lambda_2 \lambda_4) \\ T_{2,1} &= 2 * (\lambda_3 \lambda_4 + \lambda_2 \lambda_5) \\ T_{2,2} &= \lambda_2^2 - \lambda_3^2 + \lambda_4^2 - \lambda_5^2 \\ T_{2,3} &= 2 * (\lambda_4 \lambda_5 - \lambda_2 \lambda_3) \\ T_{3,1} &= 2 * (\lambda_3 \lambda_5 - \lambda_2 \lambda_4) \\ T_{3,2} &= 2 * (\lambda_3 \lambda_4 + \lambda_2 \lambda_5) \\ T_{3,3} &= \lambda_2^2 - \lambda_3^2 + \lambda_4^2 + \lambda_5^2 \end{aligned}$$

CALL MULT

(I.E. $[I, B_1] = [I, B_0] [F]$)

CALL MULT

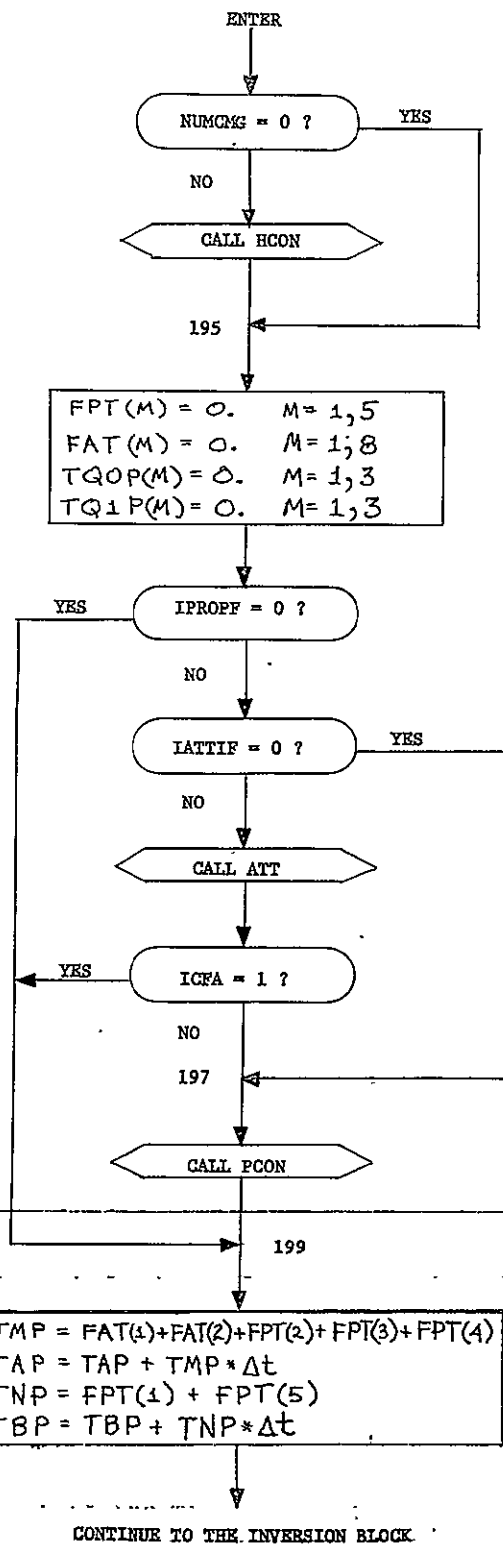
(I.E. $[R_T] = [I, B_1] [R]$)

CONTINUE TO THE CONTROL MODULE

FLOW CHART & BLOCK DIAGRAM

F - V EE - 1102 - 01 10-60

Application CONTROL MODULE Date OCTOBER 1970 Page 1 of 1
 Procedure _____ Drawn By GARY JOHNSON

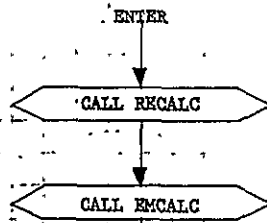


FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application INVERSION BLOCK Date OCTOBER 1970 Page 1 of 2

Procedure _____ Drawn By GARY JOHNSON



| | |
|--|-------------|
| | $[X] = [M]$ |
| STEMP ₁ = $m_2 * s * (-R_{2x} s_{2y} + R_{2y} s_{2x})$ | |
| STEMP ₂ = $m_2 * s * ((R_{2x} s_{2x}) - R_{2y} s_{2x}) C_{G1}$ | |
| STEMP ₃ = $m_2 * s * ((R_{2x} s_{2x}) - R_{2y} s_{2x}) S_{G1}$ | |
| STEMP ₄ = $s * (s_{2y} (-m_2 R_{2x} + (m_2 m_2 / m) * (d_{01y} s_{G1} - d_{01x} C_{G1})))$ | |
| STEMP ₅ = $(m_2 m_3 / m) * s * ((l_{3x} s_{2x} - l_{3y} s_{2x}) * s_{3y}$ | |
| STEMP ₆ = $(m_2 m_4 / m) * s * ((l_{4x} s_{2x} - l_{4y} s_{2x}) s_{4y} + (l_{4y} s_{2x} + l_{4x} s_{2y}) s_{4x})$ | |
| $H_x = H_x - STEMP_1$ | |
| $H_y = H_y - STEMP_2$ | |
| $H_x = H_x - STEMP_3$ | |
| $H_{1x} = H_{1x} - STEMP_4$ | |
| $G_3 = G_3 + STEMP_5$ | |
| $G_4 = G_4 + STEMP_6$ | |

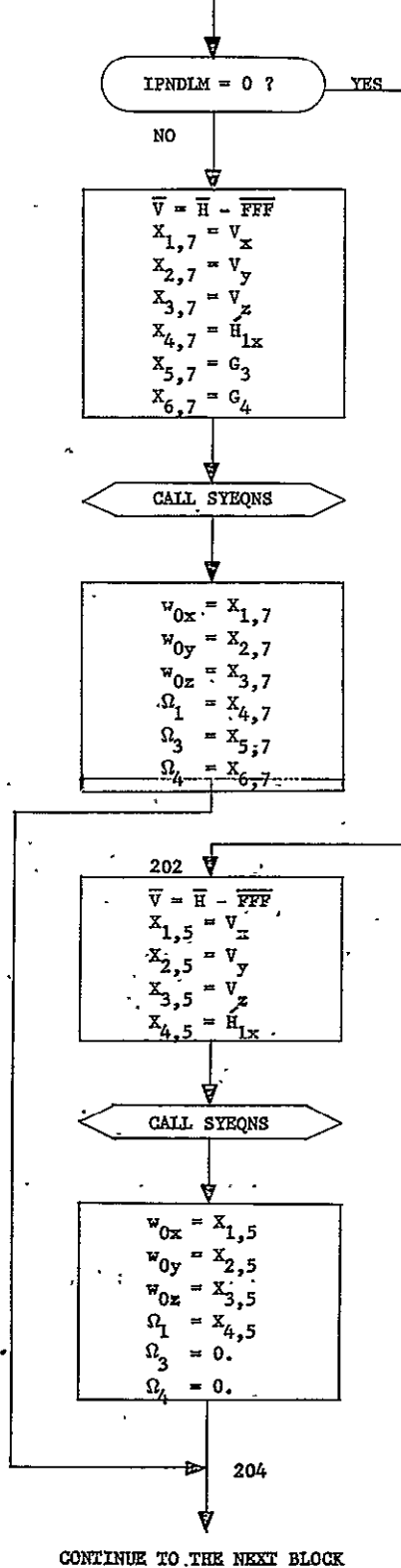
CONTINUE TO THE NEXT PAGE

FLOW CHART & BLOCK DIAGRAM

Application INVERSION BLOCK CONTINUED Date OCTOBER 1970 Page 2 of 2

Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

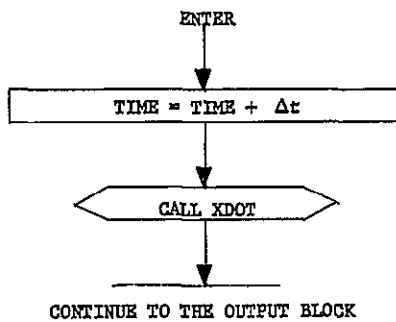


FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

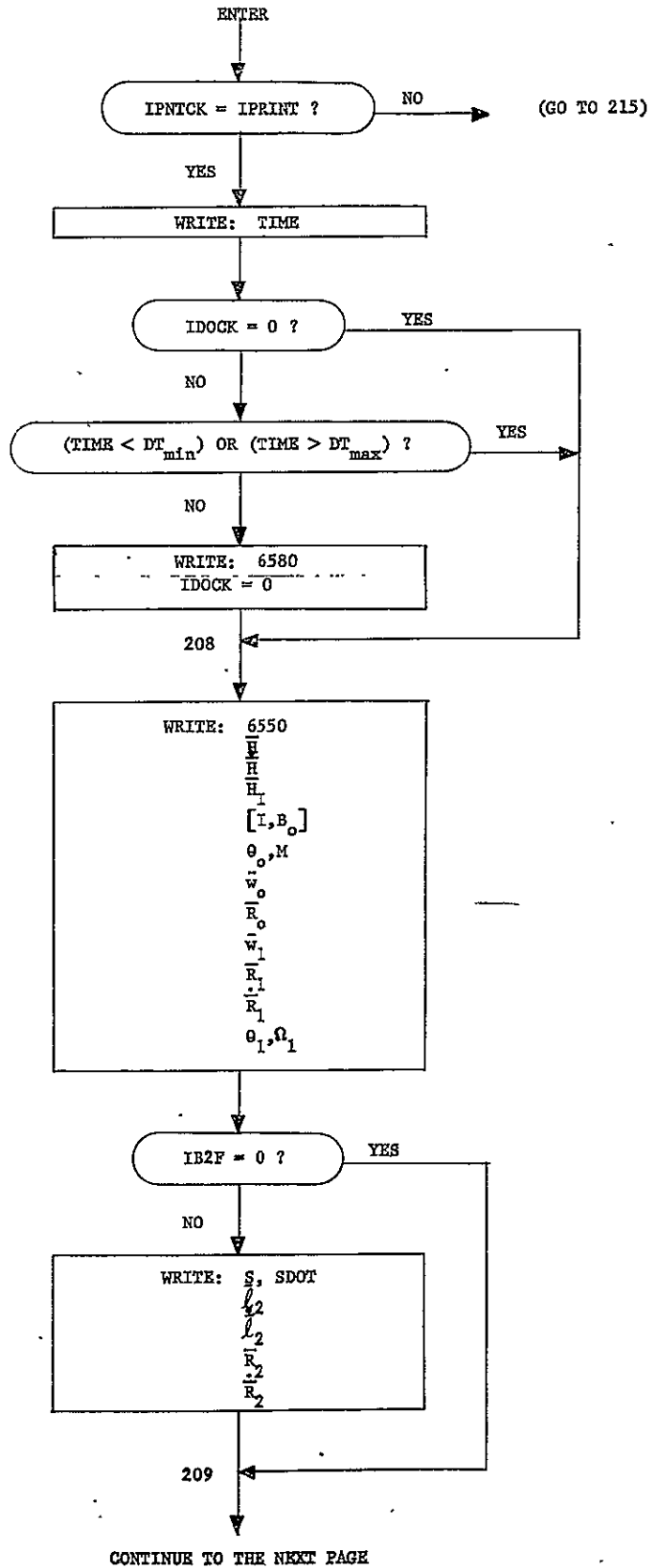
Application TIME UPDATE Date OCTOBER 1970 Page 1 of 1

Procedure _____ Drawn By GARY JOHNSON



FLOW CHART & BLOCK DIAGRAM

Application OUTPUT BLOCK Date OCTOBER 1970 Page 1 of 3
 Procedure _____ Drawn By GARY JOHNSON



FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application OUTPUT BLOCK CONTINUED Date OCTOBER 1970 Page 2 of 2

Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

209

IFNDLM = 0 ?

YES

NO

WRITE:

$$\begin{matrix} \bar{w}_3 \\ \bar{h}_3 \\ \bar{l}_3 \\ \bar{r}_3 \\ \bar{r}_3 \\ \theta_3, \Omega_3 \\ G_3, \dot{G}_3 \\ \bar{w}_4 \\ \bar{h}_4 \\ \bar{l}_4 \\ \bar{r}_4 \\ \bar{r}_4 \\ \theta_4, \Omega_4 \\ G_4, \dot{G}_4 \end{matrix}$$

211

IFPROP = 0 ?

YES

NO

WRITE: TAP, TBP

212

NUMCMG = 0 ?

YES

NO

DO 213 J = 1, NUMCMG
 WRITE: $\theta_j, \dot{\theta}_j$
 IF (IDOF(j) \neq 2) GO TO 213
 WRITE: $\phi_j, \dot{\phi}_j$
 213 CONTINUE

214

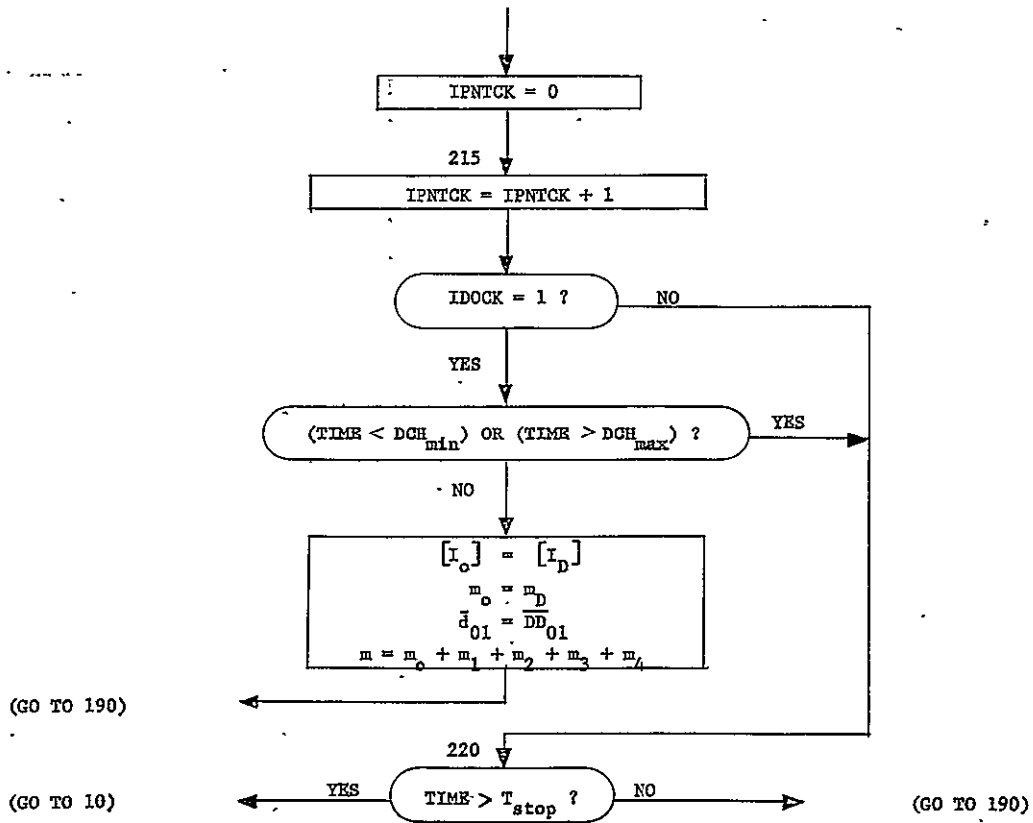
CONTINUE TO THE FOLLOWING PAGE

FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application OUTPUT BLOCK CONTINUED Date OCTOBER 1970 Page 3 of 3
 Procedure _____ Drawn By GARY JOHNSON

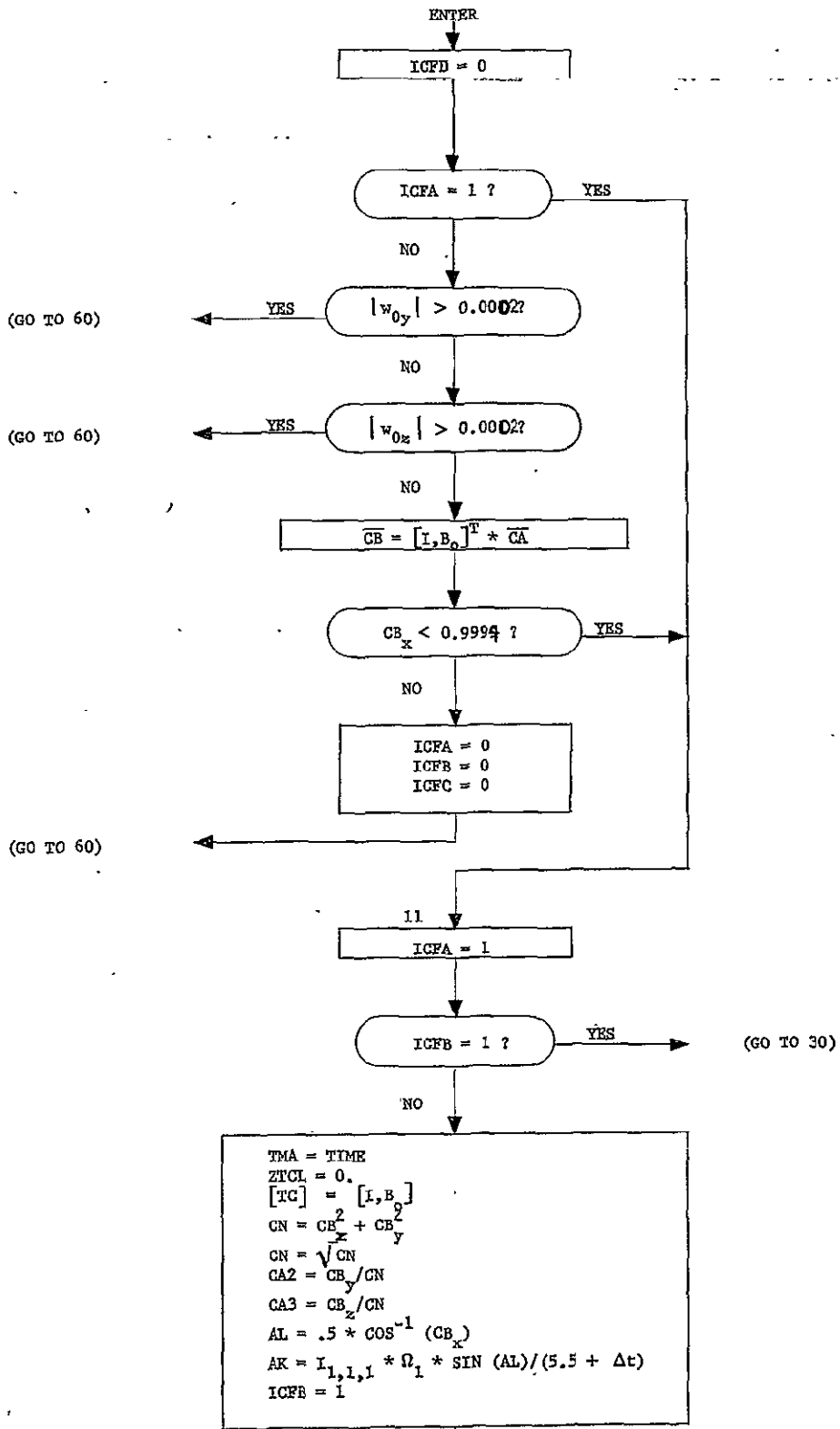
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FLOW CHART & BLOCK DIAGRAM

FORM DEV 1102-01 (4-64)

Application SUBROUTINE ATT Date OCTOBER 1970 Page 1 of 3
 Procedure _____ Drawn By GARY JOHNSON



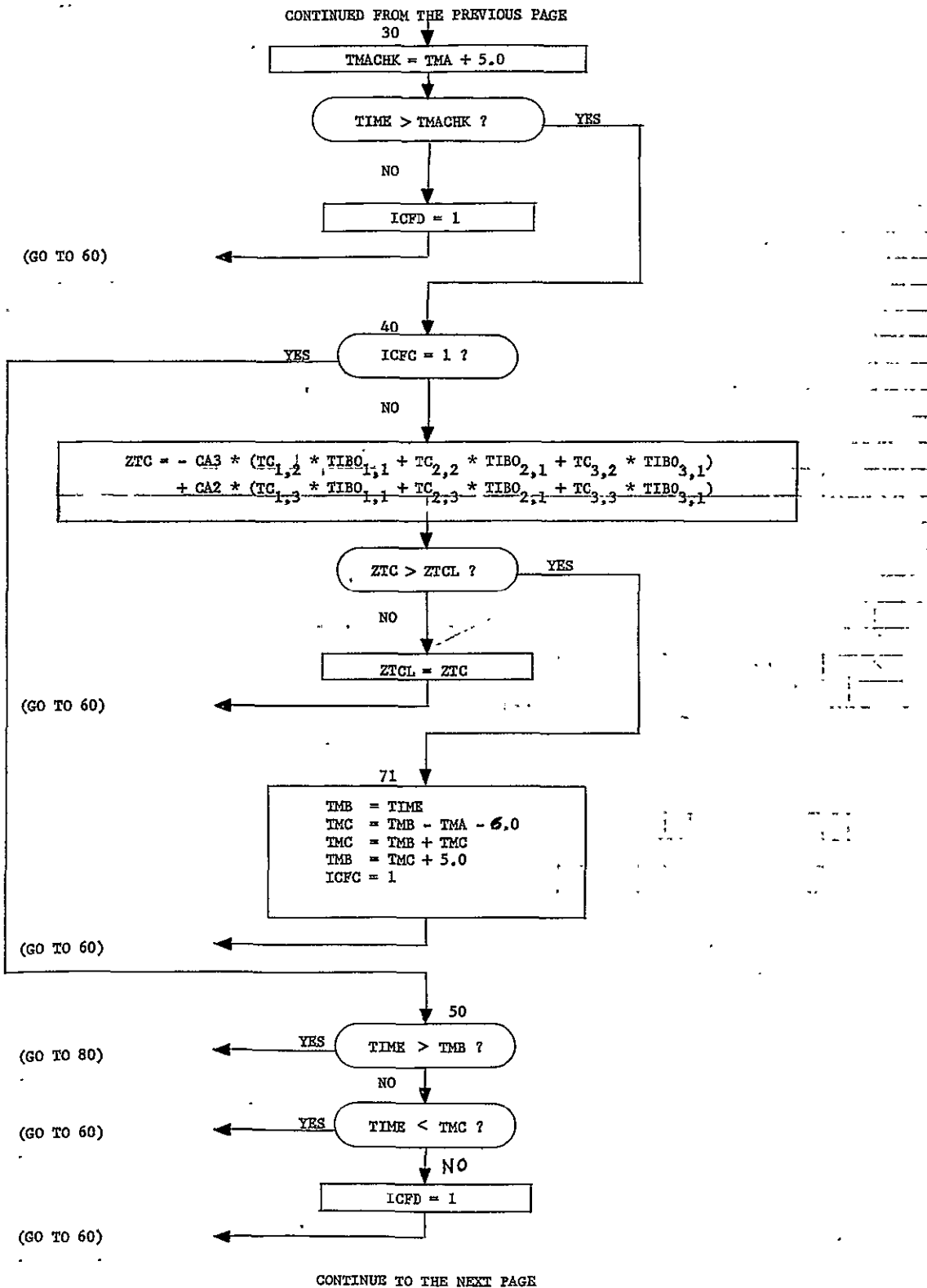
Field

Fold to attach file

FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE ATT CONTINUED Date OCTOBER 1970 Page 2 of 3

Procedure _____ Drawn By GARY JOHNSON



File

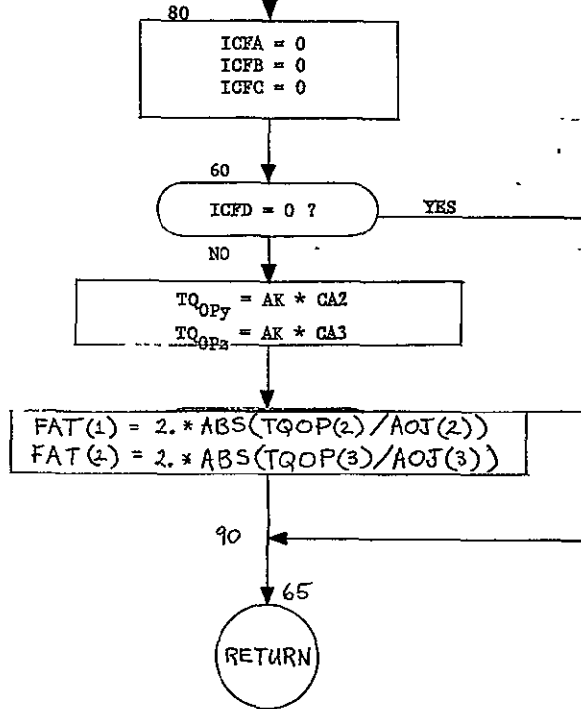
Fold to correct line

FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (1-64)

Application SUBROUTINE ATT CONTINUED Date OCTOBER 1970 Page 3 of 3
Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



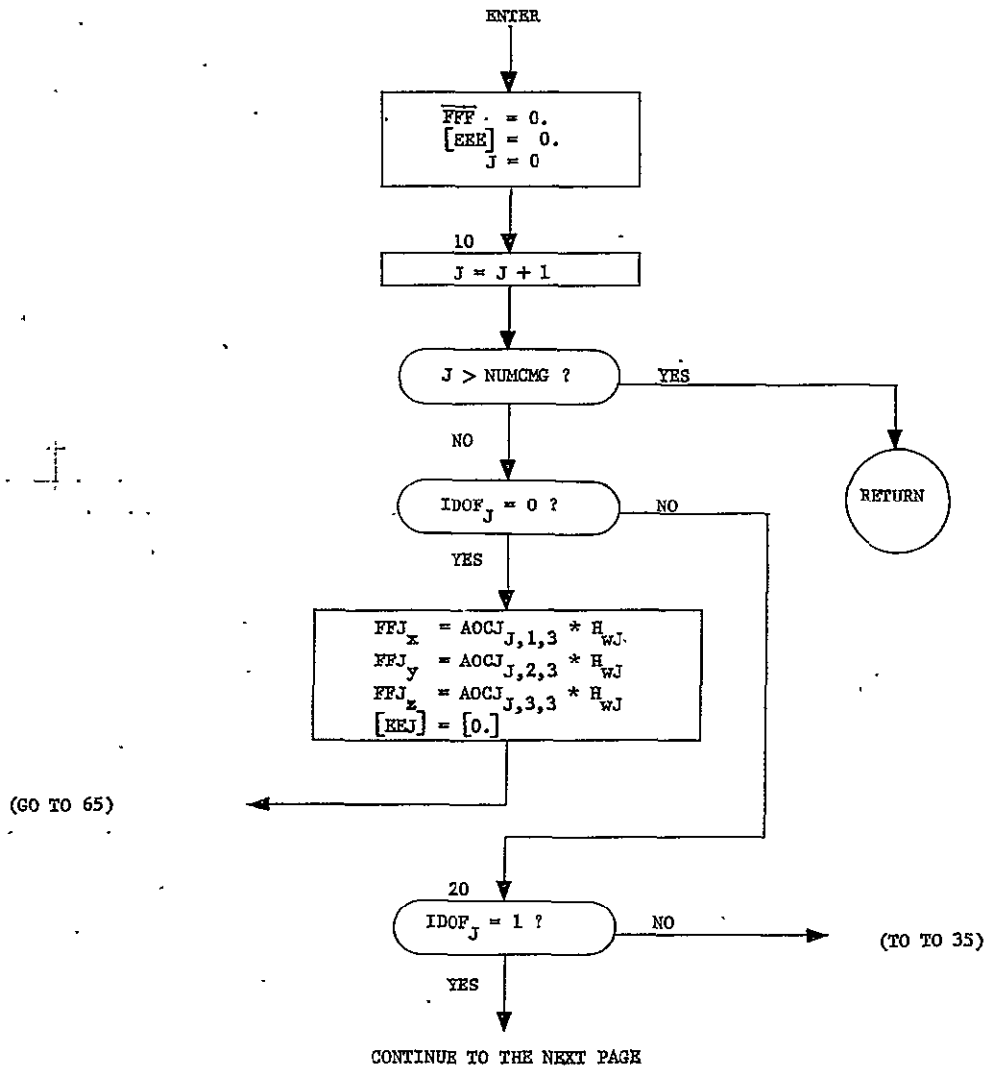
— Fold to extend line

FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application SUBROUTINE CMG Date OCTOBER 1970 Page 1 of 4

Procedure _____ Drawn By GARY JOHNSON



FORM DEN 1103-01 (4-64)

FLOW CHART & BLOCK DIAGRAM

F-4V REF 1163-01 (2-1-67)

Application SUBROUTINE CMG CONTINUED Date OCTOBER 1970 Page 2 of 4

Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

$$\begin{aligned}
 \text{TEMP12}_x &= C\theta_J * \text{ALL}_{J,1,2} * \theta_J + S\theta_J * \text{ALL}_{J,3,2} * \theta_J + S\theta_{H_{WJ}} \\
 \text{TEMP12}_y &= S\theta_J * S\theta_J * \text{ALL}_{J,1,2} * \theta_J + C\theta_J * \text{ALL}_{J,2,2} * \theta_J - S\theta_J * C\theta_J * \text{ALL}_{J,3,2} * \theta_J \\
 \text{TEMP12}_z &= -S\theta_J * C\theta_J * \text{ALL}_{J,1,2} * \theta_J + S\theta_J * \text{ALL}_{J,2,2} * \theta_J \\
 &\quad + C\theta_J * C\theta_J * \text{ALL}_{J,3,2} * \theta_J + H_{WJ} * C\theta_J \\
 \underline{FFJ} &= [0, C_J] * \text{TEMP12} \\
 \text{TEMP13}_{1,1} &= C\theta_J * \text{AOCJ}_{J,1,1} + S\theta_J * S\theta_J * \text{AOCJ}_{J,1,2} - S\theta_J * C\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP13}_{1,2} &= C\theta_J * \text{AOCJ}_{J,2,1} + S\theta_J * S\theta_J * \text{AOCJ}_{J,2,2} - S\theta_J * C\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP13}_{1,3} &= C\theta_J * \text{AOCJ}_{J,3,1} + S\theta_J * S\theta_J * \text{AOCJ}_{J,3,2} - S\theta_J * C\theta_J * \text{AOCJ}_{J,3,3} \\
 \text{TEMP13}_{2,1} &= C\theta_J * \text{AOCJ}_{J,1,2} + S\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP13}_{2,2} &= C\theta_J * \text{AOCJ}_{J,2,2} + S\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP13}_{2,3} &= C\theta_J * \text{AOCJ}_{J,3,2} + S\theta_J * \text{AOCJ}_{J,3,3} \\
 \text{TEMP13}_{3,1} &= S\theta_J * \text{AOCJ}_{J,1,1} - S\theta_J * C\theta_J * \text{AOCJ}_{J,1,2} + C\theta_J * C\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP13}_{3,2} &= S\theta_J * \text{AOCJ}_{J,2,1} - S\theta_J * C\theta_J * \text{AOCJ}_{J,2,2} + C\theta_J * C\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP13}_{3,3} &= S\theta_J * \text{AOCJ}_{J,3,1} - S\theta_J * C\theta_J * \text{AOCJ}_{J,3,2} + C\theta_J * C\theta_J * \text{AOCJ}_{J,3,3} \\
 [\text{TEMP14}] &= [\text{II}_J] * [\text{TEMP13}] \\
 \text{TEMP15}_{1,1} &= C\theta_J * \text{TEMP14}_{1,1} + S\theta_J * \text{TEMP14}_{3,1} \\
 \text{TEMP15}_{1,2} &= C\theta_J * \text{TEMP14}_{1,2} + S\theta_J * \text{TEMP14}_{3,2} \\
 \text{TEMP15}_{1,3} &= C\theta_J * \text{TEMP14}_{1,3} + S\theta_J * \text{TEMP14}_{3,3} \\
 \text{TEMP15}_{2,1} &= S\theta_J * S\theta_J * \text{TEMP14}_{1,1} + C\theta_J * \text{TEMP14}_{2,1} - S\theta_J * C\theta_J * \text{TEMP14}_{3,1} \\
 \text{TEMP15}_{2,2} &= S\theta_J * S\theta_J * \text{TEMP14}_{1,2} + C\theta_J * \text{TEMP14}_{2,2} - S\theta_J * C\theta_J * \text{TEMP14}_{3,2} \\
 \text{TEMP15}_{2,3} &= S\theta_J * S\theta_J * \text{TEMP14}_{1,3} + C\theta_J * \text{TEMP14}_{2,3} - S\theta_J * C\theta_J * \text{TEMP14}_{3,3} \\
 \text{TEMP15}_{3,1} &= -S\theta_J * C\theta_J * \text{TEMP14}_{1,1} + S\theta_J * \text{TEMP14}_{2,1} + C\theta_J * C\theta_J * \text{TEMP14}_{3,1} \\
 \text{TEMP15}_{3,2} &= -S\theta_J * C\theta_J * \text{TEMP14}_{1,2} + S\theta_J * \text{TEMP14}_{2,2} + C\theta_J * C\theta_J * \text{TEMP14}_{3,2} \\
 \text{TEMP15}_{3,3} &= -S\theta_J * C\theta_J * \text{TEMP14}_{1,3} + S\theta_J * \text{TEMP14}_{2,3} + C\theta_J * C\theta_J * \text{TEMP14}_{3,3} \\
 [\text{REJ}] &= [0, C_J] * [\text{TEMP15}]
 \end{aligned}$$

(GO TO 60) ←

CONTINUE TO THE NEXT PAGE

FLOW CHART & BLOCK DIAGRAM

FORM DEV 1103-01 (4-64)

Application SUBROUTINE CMG CONTINUED Date OCTOBER 1970 Page 3 of 4

Procedure _____ Drawn By GARY JOHNSON

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$$\begin{aligned}
 \text{TEMP1}_x &= \text{AIO}_{J,1,1} * \theta_J \\
 \text{TEMP1}_y &= \text{C}\theta_J * \text{AIO}_{J,2,1} * \theta_J - \text{S}\theta_J * \text{AIO}_{J,3,1} * \theta_J \\
 \text{TEMP1}_z &= \text{S}\theta_J * \text{AIO}_{J,2,1} * \theta_J + \text{C}\theta_J * \text{AIO}_{J,3,1} * \theta_J \\
 \text{TEMP2}_x &= \text{C}\theta_J * [\text{AII}_{J,1,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,1,2} * \theta_J + \text{AII}_{J,1,3} * \text{S}\theta_J * \theta_J] \\
 &+ \text{S}\theta_J * [\text{AII}_{J,3,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,3,2} * \theta_J + \text{AII}_{J,3,3} * \text{S}\theta_J * \theta_J] \\
 \text{TEMP2}_y &= \text{S}\theta_J * \text{S}\theta_J * [\text{AII}_{J,1,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,1,2} * \theta_J + \text{AII}_{J,1,3} * \text{S}\theta_J * \theta_J] \\
 &+ \text{C}\theta_J * [\text{AII}_{J,2,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,2,2} * \theta_J + \text{AII}_{J,2,3} * \text{S}\theta_J * \theta_J] \\
 &- \text{S}\theta_J * \text{C}\theta_J * [\text{AII}_{J,3,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,3,2} * \theta_J + \text{AII}_{J,3,3} * \text{S}\theta_J * \theta_J] \\
 \text{TEMP2}_z &= -\text{S}\theta_J * \text{C}\theta_J * [\text{AII}_{J,1,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,1,2} * \theta_J + \text{AII}_{J,1,3} * \text{S}\theta_J * \theta_J] \\
 &+ \text{S}\theta_J * [\text{AII}_{J,2,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,2,2} * \theta_J + \text{AII}_{J,2,3} * \text{S}\theta_J * \theta_J] \\
 &+ \text{C}\theta_J * \text{C}\theta_J * [\text{AII}_{J,3,1} * \text{C}\theta_J * \theta_J + \text{AII}_{J,3,2} * \theta_J + \text{AII}_{J,3,3} * \text{S}\theta_J * \theta_J] \\
 \text{TEMP3}_x &= \text{H}_{\text{WJ}} * \text{S}\theta_J \\
 \text{TEMP3}_y &= -\text{H}_{\text{WJ}} * \text{C}\theta_J * \text{S}\theta_J \\
 \text{TEMP3}_z &= \text{H}_{\text{WJ}} * \text{C}\theta_J * \text{C}\theta_J \\
 \text{TEMP4} &= \text{TEMP1} + \text{TEMP2} + \text{TEMP3} \\
 \text{FFJ} &= [0, \text{C}_J] * \text{TEMP4} \\
 \text{TEMP5}_{1,1} &= \text{AOCJ}_{J,1,1} \\
 \text{TEMP5}_{1,2} &= \text{AOCJ}_{J,2,1} \\
 \text{TEMP5}_{1,3} &= \text{AOCJ}_{J,3,1} \\
 \text{TEMP5}_{2,1} &= \text{C}\theta_J * \text{AOCJ}_{J,1,2} + \text{S}\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP5}_{2,2} &= \text{C}\theta_J * \text{AOCJ}_{J,2,2} + \text{S}\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP5}_{2,3} &= \text{C}\theta_J * \text{AOCJ}_{J,3,2} + \text{S}\theta_J * \text{AOCJ}_{J,3,3} \\
 \text{TEMP5}_{3,1} &= -\text{S}\theta_J * \text{AOCJ}_{J,1,2} + \text{C}\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP5}_{3,2} &= -\text{S}\theta_J * \text{AOCJ}_{J,2,2} + \text{C}\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP5}_{3,3} &= -\text{S}\theta_J * \text{AOCJ}_{J,3,2} + \text{C}\theta_J * \text{AOCJ}_{J,3,3} \\
 \text{TEMP6} &= [\text{I}_J] * \text{TEMP5} \\
 \text{TEMP7}_{1,1} &= \text{TEMP6}_{1,1} \\
 \text{TEMP7}_{1,2} &= \text{TEMP6}_{1,2} \\
 \text{TEMP7}_{1,3} &= \text{TEMP6}_{1,3} \\
 \text{TEMP7}_{2,1} &= \text{C}\theta_J * \text{TEMP6}_{2,1} - \text{S}\theta_J * \text{TEMP6}_{3,1} \\
 \text{TEMP7}_{2,2} &= \text{C}\theta_J * \text{TEMP6}_{2,2} - \text{S}\theta_J * \text{TEMP6}_{3,2} \\
 \text{TEMP7}_{2,3} &= \text{C}\theta_J * \text{TEMP6}_{2,3} - \text{S}\theta_J * \text{TEMP6}_{3,3} \\
 \text{TEMP7}_{3,1} &= \text{S}\theta_J * \text{TEMP6}_{2,1} + \text{C}\theta_J * \text{TEMP6}_{3,1} \\
 \text{TEMP7}_{3,2} &= \text{S}\theta_J * \text{TEMP6}_{2,2} + \text{C}\theta_J * \text{TEMP6}_{3,2} \\
 \text{TEMP7}_{3,3} &= \text{S}\theta_J * \text{TEMP6}_{2,3} + \text{C}\theta_J * \text{TEMP6}_{3,3} \\
 \text{TEMP8}_{1,1} &= \text{C}\theta_J * \text{AOCJ}_{J,1,1} + \text{S}\theta_J * \text{S}\theta_J * \text{AOCJ}_{J,1,2} - \text{S}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP8}_{1,2} &= \text{C}\theta_J * \text{AOCJ}_{J,2,1} + \text{S}\theta_J * \text{S}\theta_J * \text{AOCJ}_{J,2,2} - \text{S}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP8}_{1,3} &= \text{C}\theta_J * \text{AOCJ}_{J,3,1} + \text{S}\theta_J * \text{S}\theta_J * \text{AOCJ}_{J,3,2} - \text{S}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,3,3} \\
 \text{TEMP8}_{2,1} &= \text{C}\theta_J * \text{AOCJ}_{J,1,2} + \text{S}\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP8}_{2,2} &= \text{C}\theta_J * \text{AOCJ}_{J,2,2} + \text{S}\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP8}_{2,3} &= \text{C}\theta_J * \text{AOCJ}_{J,3,2} + \text{S}\theta_J * \text{AOCJ}_{J,3,3} \\
 \text{TEMP8}_{3,1} &= \text{S}\theta_J * \text{AOCJ}_{J,1,1} - \text{S}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,1,2} + \text{C}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,1,3} \\
 \text{TEMP8}_{3,2} &= \text{S}\theta_J * \text{AOCJ}_{J,2,1} - \text{S}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,2,2} + \text{C}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,2,3} \\
 \text{TEMP8}_{3,3} &= \text{S}\theta_J * \text{AOCJ}_{J,3,1} - \text{S}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,3,2} + \text{C}\theta_J * \text{C}\theta_J * \text{AOCJ}_{J,3,3}
 \end{aligned}$$

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FLOW CHART & BLOCK DIAGRAM

FD-207 (Rev. 11-03-59) (4-54)

Application SUBROUTINE CMG CONTINUED Date OCTOBER 1970 Page 4 of 4
 Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

$$[\text{TEMP9}] = [\text{II}_J] [\text{TEMP8}]$$

$$\text{TEMP10}_{1,1} = C\theta_J * \text{TEMP9}_{1,1} + S\theta_J * \text{TEMP9}_{3,1}$$

$$\text{TEMP10}_{1,2} = C\theta_J * \text{TEMP9}_{1,2} + S\theta_J * \text{TEMP9}_{3,2}$$

$$\text{TEMP10}_{1,3} = C\theta_J * \text{TEMP9}_{1,3} + S\theta_J * \text{TEMP9}_{3,3}$$

$$\text{TEMP10}_{2,1} = S\theta_J * S\theta_J * \text{TEMP9}_{1,1} + C\theta_J * \text{TEMP9}_{2,1} - S\theta_J * C\theta_J * \text{TEMP9}_{3,1}$$

$$\text{TEMP10}_{2,2} = S\theta_J * S\theta_J * \text{TEMP9}_{1,2} + C\theta_J * \text{TEMP9}_{2,2} - S\theta_J * C\theta_J * \text{TEMP9}_{3,2}$$

$$\text{TEMP10}_{2,3} = S\theta_J * S\theta_J * \text{TEMP9}_{1,3} + C\theta_J * \text{TEMP9}_{2,3} - S\theta_J * C\theta_J * \text{TEMP9}_{3,3}$$

$$\text{TEMP10}_{3,1} = -S\theta_J * C\theta_J * \text{TEMP9}_{1,1} + S\theta_J * \text{TEMP9}_{2,1} + C\theta_J * C\theta_J * \text{TEMP9}_{3,1}$$

$$\text{TEMP10}_{3,2} = -S\theta_J * C\theta_J * \text{TEMP9}_{1,2} + S\theta_J * \text{TEMP9}_{2,2} + C\theta_J * C\theta_J * \text{TEMP9}_{3,2}$$

$$\text{TEMP10}_{3,3} = -S\theta_J * C\theta_J * \text{TEMP9}_{1,3} + S\theta_J * \text{TEMP9}_{2,3} + C\theta_J * C\theta_J * \text{TEMP9}_{3,3}$$

$$[\text{TEMP11}] = [\text{TEMP7}] + [\text{TEMP10}]$$

$$[\text{EEJ}] = [0, C_J] * [\text{TEMP11}]$$

$$\begin{aligned} \theta_J &= \theta_J + \dot{\theta}_J * \Delta t \\ \phi_J &= \phi_J + \dot{\phi}_J * \Delta t \end{aligned}$$

65

$$\begin{aligned} \overline{\text{FFF}} &= \overline{\text{FFF}} + \overline{\text{FFJ}} \\ [\text{EEE}] &= [\text{EEK}] + [\text{KEJ}] \end{aligned}$$

(GO TO 10) ←

FLOW CHART & BLOCK DIAGRAM

FORM DEC 1103-01 (4-64)

Application SUBROUTINE EMGALC : Date OCTOBER 1970 Page 1 of 4

Procedure _____ Drawn By GARY JOHNSON

ENTER

$$\begin{aligned}
 M_{1,1} = & I_{0,1,1} + I_{1,1,1} + m_1 * d_{01y} * (R_{1y}C_{01} - R_{1x}S_{01}) + m_1 * d_{01x} * (R_{1y}S_{01} + R_{1x}C_{01}) \\
 & + m_2 * (R_{2y}C_{01} - R_{2x}S_{01}) * (d_{01y} + l_{2y}C_{01} - l_{2x}S_{01}) \\
 & + m_2 * (R_{2y}S_{01} + R_{2x}C_{01}) * (d_{01x} + l_{2y}S_{01} + l_{2x}C_{01}) \\
 & + m_3 * (R_{3y}C_{01} - R_{3x}S_{01}) * (d_{01y} + d_{13y}C_{01} - d_{13x}S_{01} + l_{3y}C_{01} - l_{3x}S_{01}) \\
 & + m_3 * (R_{3y}S_{01} + R_{3x}C_{01}) * (d_{01x} + d_{13y}S_{01} + d_{13x}C_{01} + l_{3y}S_{01} + l_{3x}C_{01}) \\
 & + m_4 * (R_{4y}C_{01} - R_{4x}S_{01}) * (d_{01y} + d_{14y}C_{01} - d_{14x}S_{01} + l_{4y}C_{01} - l_{4x}S_{01}) \\
 & + m_4 * (R_{4y}S_{01} + R_{4x}C_{01}) * (d_{01x} + d_{14y}S_{01} + d_{14x}C_{01} + l_{4y}S_{01} + l_{4x}C_{01})
 \end{aligned}$$

$$\begin{aligned}
 M_{1,2} = & I_{0,1,2} + I_{1,1,2} * C_{01} - I_{1,1,3} * S_{01} - m_1 * R_{1x} * d_{01y} \\
 & - m_2 * R_{2x} * (d_{01y} + l_{2y}C_{01} - l_{2x}S_{01}) \\
 & - m_3 * R_{3x} * (d_{01y} + d_{13y}C_{01} - d_{13x}S_{01} + l_{3y}C_{01} - l_{3x}S_{01}) \\
 & - m_4 * R_{4x} * (d_{01y} + d_{14y}C_{01} - d_{14x}S_{01} + l_{4y}C_{01} - l_{4x}S_{01})
 \end{aligned}$$

$$\begin{aligned}
 M_{1,3} = & I_{0,1,3} + I_{1,1,2} * S_{01} + I_{1,1,3} * C_{01} - m_1 * R_{1x} * d_{01x} \\
 & - m_2 * R_{2x} * (d_{01x} + l_{2y}S_{01} + l_{2x}C_{01}) \\
 & - m_3 * R_{3x} * (d_{01x} + d_{13y}S_{01} + d_{13x}C_{01} + l_{3y}S_{01} + l_{3x}C_{01}) \\
 & - m_4 * R_{4x} * (d_{01x} + d_{14y}S_{01} + d_{14x}C_{01} + l_{4y}S_{01} + l_{4x}C_{01})
 \end{aligned}$$

$$\begin{aligned}
 M_{1,4} = & I_{1,1,1} - m_1 * d_{01x} * ((m_0/m) * d_{01x} - R_{1y}S_{01} - R_{1x}C_{01}) \\
 & + m_1 * d_{01y} * (R_{1y}C_{01} - R_{1x}S_{01} - (m_0/m) * d_{01y}) \\
 & - m_2 * (d_{01x} + l_{2y}S_{01} + l_{2x}C_{01}) * ((m_0/m) * d_{01x} - R_{2y}S_{01} - R_{2x}C_{01}) \\
 & + m_2 * (d_{01y} + l_{2y}C_{01} - l_{2x}S_{01}) * (R_{2y}C_{01} - R_{2x}S_{01} - (m_0/m) * d_{01y}) \\
 & - m_3 * (d_{01x} + (d_{13y} + l_{3y})S_{01} + (d_{13x} + l_{3x}) * C_{01}) * ((m_0/m) * d_{01x} - R_{3y}S_{01} - R_{3x}C_{01}) \\
 & + m_3 * (d_{01y} + (d_{13y} + l_{3y})C_{01} - (d_{13x} + l_{3x}) * S_{01}) * (R_{3y}C_{01} - R_{3x}S_{01} - (m_0/m) * d_{01y}) \\
 & - m_4 * (d_{01x} + (d_{14y} + l_{4y})S_{01} + (d_{14x} + l_{4x}) * C_{01}) * ((m_0/m) * d_{01x} - R_{4y}S_{01} - R_{4x}C_{01}) \\
 & + m_4 * (d_{01y} + (d_{14y} + l_{4y})C_{01} - (d_{14x} + l_{4x}) * S_{01}) * (R_{4y}C_{01} - R_{4x}S_{01} - (m_0/m) * d_{01y})
 \end{aligned}$$

$$\begin{aligned}
 M_{1,5} = & -m_3 * R_{3x} * (S_{3x} * l_{3x} - S_{3x} * l_{3x}) \\
 & + m_3 * R_{3y} * (-S_{3y} * l_{3x} + S_{3x} * l_{3y})
 \end{aligned}$$

$$\begin{aligned}
 M_{1,6} = & -m_4 * R_{4x} * (S_{4x} * l_{4x} - S_{4x} * l_{4x}) \\
 & + m_4 * R_{4y} * (-S_{4y} * l_{4x} + S_{4x} * l_{4y})
 \end{aligned}$$

$$\begin{aligned}
 M_{2,1} = & I_{0,2,1} + I_{1,2,1} * C_{01} - I_{1,3,1} * S_{01} - m_1 * d_{01x} * (R_{1y}C_{01} - R_{1x}S_{01}) \\
 & - m_2 * (R_{2y}C_{01} - R_{2x}S_{01}) * (d_{01x} + l_{2x}) \\
 & - m_3 * (R_{3y}C_{01} - R_{3x}S_{01}) * (d_{01x} + d_{13x} + l_{3x}) \\
 & - m_4 * (R_{4y}C_{01} - R_{4x}S_{01}) * (d_{01x} + d_{14x} + l_{4x})
 \end{aligned}$$

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FLOW CHART & BLOCK DIAGRAM

CONTINUED FROM THE PREVIOUS PAGE

$$\begin{aligned}
 M_{2,2} = & I_{0,2,2} + I_{1,2,2} C_1^2 - I_{1,2,3} C_1 S_1 - I_{1,3,2} * C_1 S_1 + I_{1,3,3} * S_1^2 \\
 & + m_1 * R_{1x} * d_{01x} + m_1 * d_{01x} * (R_{1y} S_1 + R_{1z} C_1) \\
 & + m_2 * R_{2x} * (d_{01x} + l_{2x}) + m_2 * (R_{2y} S_1 + R_{2z} C_1) * (d_{01x} + l_{2y} S_1 + l_{2z} C_1) \\
 & + m_3 * R_{3x} * (d_{01x} + d_{13x} + l_{3x}) \\
 & + m_3 * (R_{3y} S_1 + R_{3z} C_1) * (d_{01x} + d_{13y} S_1 + d_{13z} C_1 + l_{3y} S_1 + l_{3z} C_1) \\
 & + m_4 * R_{4x} * (d_{01x} + d_{14x} + l_{4x}) \\
 & + m_4 * (R_{4y} S_1 + R_{4z} C_1) * (d_{01x} + d_{14y} S_1 + d_{14z} C_1 + l_{4y} S_1 + l_{4z} C_1)
 \end{aligned}$$

$$\begin{aligned}
 M_{2,3} = & I_{0,2,3} + I_{1,2,2} C_1 S_1 + I_{1,2,3} * C_1^2 - I_{1,3,2} * S_1^2 - I_{1,3,3} * C_1 S_1 \\
 & - m_1 * d_{01x} * (R_{1y} C_1 - R_{1z} S_1) \\
 & - m_2 * (R_{2y} C_1 - R_{2z} S_1) * (d_{01x} + l_{2y} S_1 + l_{2z} C_1) \\
 & - m_3 * (R_{3y} C_1 - R_{3z} S_1) * (d_{01x} + d_{13y} S_1 + d_{13z} C_1 + l_{3y} S_1 + l_{3z} C_1) \\
 & - m_4 * (R_{4y} C_1 - R_{4z} S_1) * (d_{01x} + d_{14y} S_1 + d_{14z} C_1 + l_{4y} S_1 + l_{4z} C_1)
 \end{aligned}$$

$$\begin{aligned}
 M_{2,4} = & I_{1,1,2} * C_1 - I_{1,1,3} * S_1 - m_1 * d_{01x} * R_{1y} C_1 \\
 & + m_1 * d_{01x} * R_{1z} S_1 + (m_0/m) * m_1 * d_{01x} * d_{01y} \\
 & - m_2 * (d_{01x} + l_{2x}) * (R_{2y} C_1 - R_{2z} S_1 - (m_0/m) * d_{01y}) \\
 & - m_3 * (d_{01x} + d_{13x} + l_{3x}) * (R_{3y} C_1 - R_{3z} S_1 - (m_0/m) * d_{01y}) \\
 & - m_4 * (d_{01x} + d_{14x} + l_{4x}) * (R_{4y} C_1 - R_{4z} S_1 - (m_0/m) * d_{01y})
 \end{aligned}$$

$$\begin{aligned}
 M_{2,5} = & (m_3 * R_{3x} * (-S_{3x} * l_{3y} + S_{3y} * l_{3x}) \\
 & - m_3 * R_{3x} * (-S_{3y} * l_{3x} + S_{3x} * l_{3y})) * C_1 \\
 & - (-m_3 * R_{3y} * (-S_{3x} * l_{3y} + S_{3y} * l_{3x}) \\
 & + m_3 * R_{3x} * (S_{3x} * l_{3x} - S_{3x} * l_{3x})) * S_1
 \end{aligned}$$

$$\begin{aligned}
 M_{2,6} = & (m_4 * R_{4x} * (-S_{4x} * l_{4y} + S_{4y} * l_{4x}) \\
 & - m_4 * R_{4x} * (-S_{4y} * l_{4x} + S_{4x} * l_{4y})) * C_1 \\
 & - (-m_4 * R_{4y} * (-S_{4x} * l_{4y} + S_{4y} * l_{4x}) \\
 & + m_4 * R_{4x} * (S_{4x} * l_{4x} - S_{4x} * l_{4x})) * S_1
 \end{aligned}$$

$$\begin{aligned}
 M_{3,1} = & I_{0,3,1} + I_{1,2,1} * S_1 + I_{1,3,1} * C_1 - m_1 * d_{01x} * (R_{1y} S_1 + R_{1z} C_1) \\
 & - m_2 * (d_{01x} + l_{2x}) * (R_{2y} S_1 + R_{2z} C_1) \\
 & - m_3 * (d_{01x} + d_{13x} + l_{3x}) * (R_{3y} S_1 + R_{3z} C_1) \\
 & - m_4 * (d_{01x} + d_{14x} + l_{4x}) * (R_{4y} S_1 + R_{4z} C_1)
 \end{aligned}$$

$$\begin{aligned}
 M_{3,2} = & I_{0,3,2} + I_{1,2,2} * C_1 * S_1 - I_{1,2,3} * S_1^2 + I_{1,3,2} * C_1^2 - I_{1,3,3} * C_1 * S_1 \\
 & - m_1 * d_{01y} * (R_{1y} S_1 + R_{1z} C_1) \\
 & - m_2 * (R_{2y} S_1 + R_{2z} C_1) * (d_{01y} + l_{2y} C_1 - l_{2x} S_1) \\
 & - m_3 * (R_{3y} S_1 + R_{3z} C_1) * (d_{01y} + d_{13y} C_1 - d_{13x} S_1 + l_{3y} C_1 - l_{3x} S_1) \\
 & - m_4 * (R_{4y} S_1 + R_{4z} C_1) * (d_{01y} + d_{14y} C_1 - d_{14x} S_1 + l_{4y} C_1 - l_{4x} S_1)
 \end{aligned}$$

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$$\begin{aligned}
M_{3,3} = & I_{0,3,3} + I_{1,2,2} * S_0^2 + I_{1,2,3} * C_0 * S_0 + I_{1,3,2} C_0 * S_0 + I_{1,3,3} * C_0^2 \\
& + m_1 * R_{1x} * d_{01x} + m_1 * (R_{1y} C_0 - R_{1z} S_0) * d_{01y} + m_2 * R_{2x} * (d_{01x} + l_{2x}) \\
& + m_2 * (R_{2y} C_0 - R_{2z} S_0) * (d_{01y} + l_{2y} C_0 - l_{2z} S_0) \\
& + m_3 * R_{3x} * (d_{01x} + d_{13x} + l_{3x}) \\
& + m_3 * (R_{3y} C_0 - R_{3z} S_0) * (d_{01y} + d_{13y} C_0 - d_{13z} S_0 + l_{3y} C_0 - l_{3z} S_0) \\
& + m_4 * R_{4x} * (d_{01x} + d_{14x} + l_{4x}) \\
& + m_4 * (R_{4y} C_0 - R_{4z} S_0) * (d_{01y} + d_{14y} C_0 - d_{14z} S_0 + l_{4y} C_0 - l_{4z} S_0)
\end{aligned}$$

$$\begin{aligned}
M_{3,4} = & I_{1,1,2} * S_0 + I_{1,1,3} * C_0 \\
& + m_1 * d_{01x} * ((m_0/m) * d_{01z} - R_{1y} S_0 - R_{1z} C_0) \\
& + m_2 * (d_{01x} + l_{2x}) * ((m_0/m) * d_{01z} - R_{2y} S_0 - R_{2z} C_0) \\
& + m_3 * (d_{01x} + d_{13x} + l_{3x}) * ((m_0/m) * d_{01z} - R_{3y} S_0 - R_{3z} C_0) \\
& + m_4 * (d_{01x} + d_{14x} + l_{4x}) * ((m_0/m) * d_{01z} - R_{4y} S_0 - R_{4z} C_0)
\end{aligned}$$

$$\begin{aligned}
M_{3,5} = & (m_3 * R_{3x} * (-S_{3z} * l_{3y} + S_{3y} * l_{3z}) \\
& - m_3 * R_{3x} * (-S_{3y} * l_{3x} + S_{3z} * l_{3y})) * S_0 \\
& + (-m_3 * R_{3y} * (-S_{3z} * l_{3y} + S_{3y} * l_{3z}) \\
& + m_3 * R_{3x} * (S_{3z} * l_{3x} - S_{3x} * l_{3z})) * C_0
\end{aligned}$$

$$\begin{aligned}
M_{3,6} = & (m_4 * R_{4x} * (-S_{4z} * l_{4y} + S_{4y} * l_{4z}) \\
& - m_4 * R_{4x} * (-S_{4y} * l_{4x} + S_{4z} * l_{4y})) * S_0 \\
& + (-m_4 * R_{4y} * (-S_{4z} * l_{4y} + S_{4y} * l_{4z}) \\
& + m_4 * R_{4x} * (S_{4z} * l_{4x} - S_{4x} * l_{4z})) * C_0
\end{aligned}$$

DEFINE SOME REOCCURRING TERMS

$$SR_3 = m_3 * (d_{13y} + l_{3y})$$

$$SR_4 = m_3 * (d_{13z} + l_{3z})$$

$$SR_5 = m_4 * (d_{14y} + l_{4y})$$

$$SR_6 = m_4 * (d_{14z} + l_{4z})$$

$$SR_1 = I_{1,1,2} - m_2 * l_{2y} * R_{2x} - SR_3 * R_{3x} - SR_5 * R_{4x}$$

$$SR_2 = I_{1,1,3} - m_2 * l_{2z} * R_{2x} - SR_4 * R_{3x} - SR_6 * R_{4x}$$

$$M_{4,1} = I_{1,1,1} + m_2 * (l_{2x} * R_{2x} + l_{2y} * R_{2y}) + SR_4 * R_{3x} + SR_3 * R_{3y} + SR_6 * R_{4x} + SR_5 * R_{4y}$$

$$M_{4,2} = SR_1 * C_0 - SR_2 * S_0$$

$$M_{4,3} = SR_1 * S_0 + SR_2 * C_0$$

REDEFINE SR₁ AND SR₂

$$SR_1 = (m_0/m) * (d_{01y} * C_0 + d_{01z} * S_0)$$

$$SR_2 = (m_0/m) * (-d_{01y} * S_0 + d_{01z} * C_0)$$

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FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE EMCALG CONTINUED

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Procedure _____

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$$M_{4,4} = I_{1,1,1} + m_2 * (l_{2x} * (R_{2z} - SR_2) + l_{2y} * (R_{2y} - SR_1)) \\ + SR_4 * (R_{3z} - SR_2) + SR_3 * (R_{3y} - SR_1) + SR_6 * (R_{4z} - SR_2) + SR_5 * (R_{4y} - SR_1)$$

$$M_{4,5} = m_3 * ((R_{3z} - SR_2) * l_{3x} + (R_{3y} - SR_1) * l_{3y}) * S_{3z} \\ - (R_{3y} - SR_1) * l_{3x} * S_{3y} - (R_{3z} - SR_2) * l_{3x} * S_{3z}$$

$$M_{4,6} = m_4 * ((R_{4z} - SR_2) * l_{4x} + (R_{4y} - SR_1) * l_{4y}) * S_{4z} \\ - (R_{4y} - SR_1) * l_{4x} * S_{4y} - (R_{4z} - SR_2) * l_{4x} * S_{4z}$$

$$M_{5,1} = -m_3 * l_{3x} * (R_{3y} * S_{3y} + R_{3z} * S_{3z})$$

$$M_{5,2} = m_3 * ((l_{3x} * R_{3z} + l_{3x} * R_{3z}) * CO_1 + l_{3x} * R_{3y} * SO_1) * S_{3y} \\ + (-l_{3y} * R_{3z} * CO_1 - (l_{3y} * R_{3y} + l_{3x} * R_{3z}) * SO_1) * S_{3z}$$

$$M_{5,3} = m_3 * ((l_{3x} * R_{3z} + l_{3x} * R_{3z}) * SO_1 - l_{3x} * R_{3y} * CO_1) * S_{3y} \\ + (-l_{3y} * R_{3z} * SO_1 + (l_{3y} * R_{3y} + l_{3x} * R_{3z}) * CO_1) * S_{3z}$$

$$M_{5,4} = m_3 * l_{3x} * ((-R_{3y} + SR_1) * S_{3y} + (-R_{3z} + SR_2) * S_{3z})$$

$$M_{5,5} = m_3 * (1. - m_3/TOTMAS) * (((l_{3x}^2 + l_{3x}^2) * S_{3y} \\ - l_{3x} * l_{3y} * S_{3z}) * S_{3y} + ((l_{3y}^2 + l_{3x}^2) * S_{3z} - l_{3y} * l_{3x} * S_{3y}) * S_{3z})$$

$$M_{5,6} = (m_3 * m_4/m) * ((-l_{3x} * l_{4z} + l_{3x} * l_{4z}) * S_{4y} + l_{3x} * l_{4y} * S_{4z}) * S_{3y} \\ + (-l_{3y} * l_{4y} + l_{3x} * l_{4z}) * S_{4z} + l_{3y} * l_{4x} * S_{4y}) * S_{3z}$$

$$M_{6,1} = -m_4 * l_{4x} * (R_{4y} * S_{4y} + R_{4z} * S_{4z})$$

$$M_{6,2} = m_4 * (((l_{4x} * R_{4z} + l_{4x} * R_{4z}) * CO_1 + l_{4x} * R_{4y} * SO_1) * S_{4y} \\ + (-l_{4y} * R_{4z} * CO_1 - (l_{4y} * R_{4y} + l_{4x} * R_{4z}) * SO_1) * S_{4z})$$

$$M_{6,3} = m_4 * ((l_{4x} * R_{4z} + l_{4x} * R_{4z}) * SO_1 - l_{4x} * R_{4y} * CO_1) * S_{4y} \\ + (-l_{4y} * R_{4z} * SO_1 + (l_{4y} * R_{4y} + l_{4x} * R_{4z}) * CO_1) * S_{4z}$$

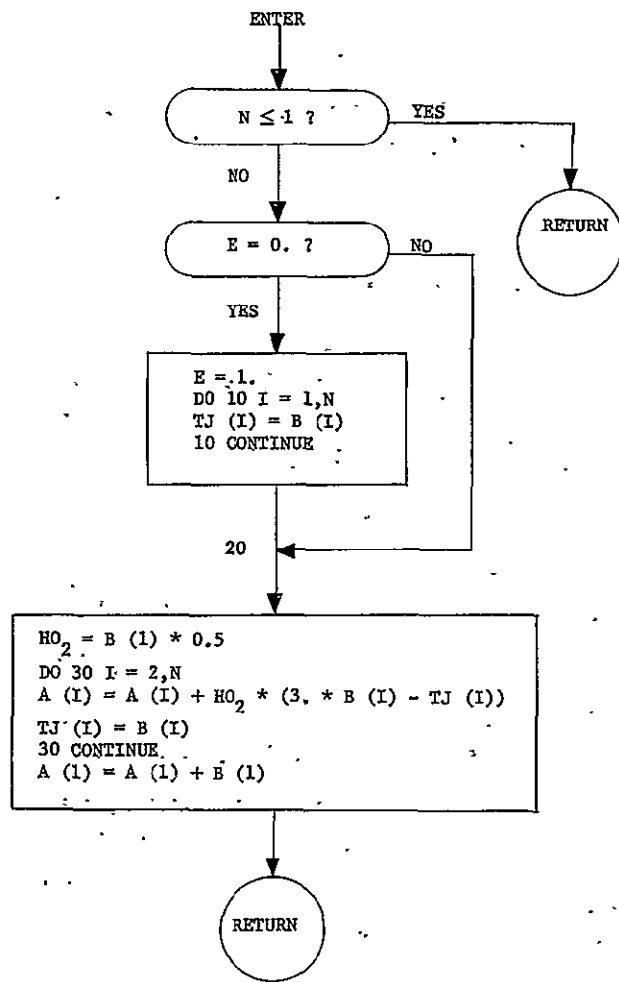
$$M_{6,4} = m_4 * l_{4x} * ((-R_{4y} + SR_1) * S_{4y} + (-R_{4z} + SR_2) * S_{4z})$$

$$M_{6,5} = (m_3 * m_4/m) * ((-l_{4x} * l_{3z} + l_{4x} * l_{3z}) * S_{3y} + l_{4x} * l_{3y} * S_{3z}) * S_{4y} \\ + (-l_{4y} * l_{3y} + l_{4x} * l_{3z}) * S_{3z} + l_{4y} * l_{3x} * S_{3y}) * S_{4z}$$

$$M_{6,6} = m_4 * (1. - m_4/m) * (((l_{4x}^2 + l_{4x}^2) * S_{4y} - l_{4x} * l_{4y} * S_{4z}) * S_{4y} \\ + ((l_{4y}^2 + l_{4x}^2) * S_{4z} - l_{4y} * l_{4z} * S_{4y}) * S_{4z})$$

$$[M] = [M] + [ERE]$$





FLOW CHART & BLOCK DIAGRAM

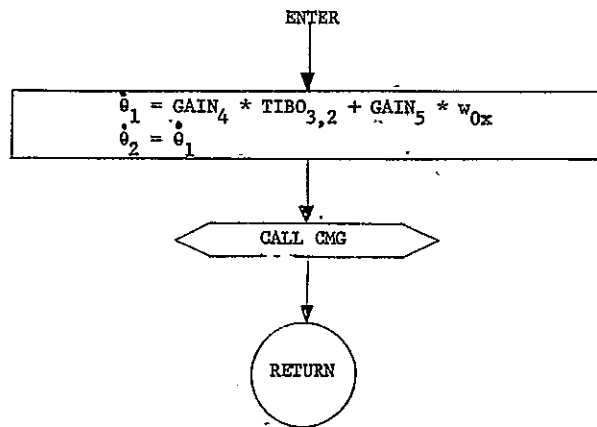
Application SUBROUTINE CGRAD Date OCTOBER 1970 Page 1 of 1
 Procedure _____ Drawn By GARY JOHNSON

ENTER

```

DBx = - S0 * TIBO1,1 + C0 * TIBO2,1
DBy = - S0 * TIBO1,2 + C0 * TIBO2,2
DBz = - S0 * TIBO1,3 + C0 * TIBO2,3
REMP = DBx * Rox + DBy * Roy + DBz * Roz
F01 = C1 * m0 * (3. * REMP * DBz - R0)
Ax = I0,1,1 * DBx + I0,1,2 * DBy + I0,1,3 * DBz
Ay = I0,2,1 * DBx + I0,2,2 * DBy + I0,2,3 * DBz
Az = I0,3,1 * DBx + I0,3,2 * DBy + I0,3,3 * DBz
TQOGx = 3. * C1 * (DBy * Az - DBz * Ay)
TQOGy = 3. * C1 * (DBz * Ax - DBx * Az)
TQOGz = 3. * C1 * (DBx * Ay - DBy * Ax)
DBx = - S0 * TIBO1,1 + C0 * TIBO2,1
DBy = C0 * (- S0 * TIBO1,2 + C0 * TIBO2,2)
      + S0 * (- S0 * TIBO1,3 + C0 * TIBO2,3)
DBz = - S0 * (- S0 * TIBO1,2 + C0 * TIBO2,2)
      + C0 * (- S0 * TIBO1,3 + C0 * TIBO2,3)
REMP = DBx * R1x + DBy * R1y + DBz * R1z
F11 = C1 * m1 * (3. * REMP * DBz - R1)
Ax = I1,1,1 * DBx + I1,1,2 * DBy + I1,1,3 * DBz
Ay = I1,2,1 * DBx + I1,2,2 * DBy + I1,2,3 * DBz
Az = I1,3,1 * DBx + I1,3,2 * DBy + I1,3,3 * DBz
TQ1Gx = 3. * C1 * (DBy * Az - DBz * Ay)
TQ1Gy = 3. * C1 * (DBz * Ax - DBx * Az)
TQ1Gz = 3. * C1 * (DBx * Ay - DBy * Ax)
    
```

RETURN



FLOW CHART & BLOCK DIAGRAM

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Procedure _____ Drawn By GARY JOHNSON

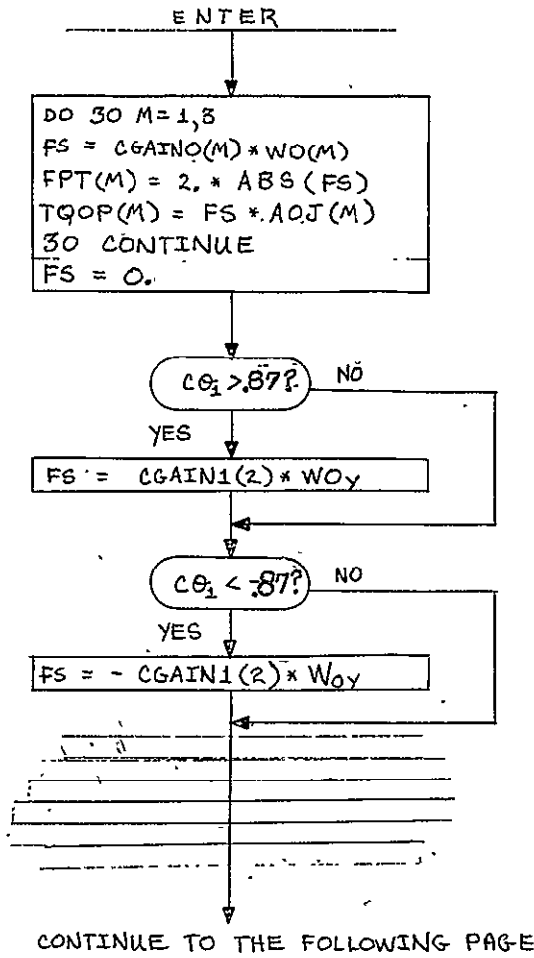
ENTER

| | |
|-----------|---|
| C_x | $= A_{1,1} * B_x + A_{1,2} * B_y + A_{1,3} * B_z$ |
| C_y | $= A_{2,1} * B_x + A_{2,2} * B_y + A_{2,3} * B_z$ |
| C_z | $= A_{3,1} * B_x + A_{3,2} * B_y + A_{3,3} * B_z$ |
| $F_{1,1}$ | $= D_{1,1} * E_{1,1} + D_{1,2} * E_{2,1} + D_{1,3} * E_{3,1}$ |
| $F_{1,2}$ | $= D_{1,1} * E_{1,2} + D_{1,2} * E_{2,2} + D_{1,3} * E_{3,2}$ |
| $F_{1,3}$ | $= D_{1,1} * E_{1,3} + D_{1,2} * E_{2,3} + D_{1,3} * E_{3,3}$ |
| $F_{2,1}$ | $= D_{2,1} * E_{1,1} + D_{2,2} * E_{2,1} + D_{2,3} * E_{3,1}$ |
| $F_{2,2}$ | $= D_{2,1} * E_{1,2} + D_{2,2} * E_{2,2} + D_{2,3} * E_{3,2}$ |
| $F_{2,3}$ | $= D_{2,1} * E_{1,3} + D_{2,2} * E_{2,3} + D_{2,3} * E_{3,3}$ |
| $F_{3,1}$ | $= D_{3,1} * E_{1,1} + D_{3,2} * E_{2,1} + D_{3,3} * E_{3,1}$ |
| $F_{3,2}$ | $= D_{3,1} * E_{1,2} + D_{3,2} * E_{2,2} + D_{3,3} * E_{3,2}$ |
| $F_{3,3}$ | $= D_{3,1} * E_{1,3} + D_{3,2} * E_{2,3} + D_{3,3} * E_{3,3}$ |

RETURN

FLOW CHART & BLOCK DIAGRAM

Procedure: SUBROUTINE PCON Date: OCTOBER 1970 Page: 4 of 2
Drawn By: GARY JOHNSON



FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-6-6)

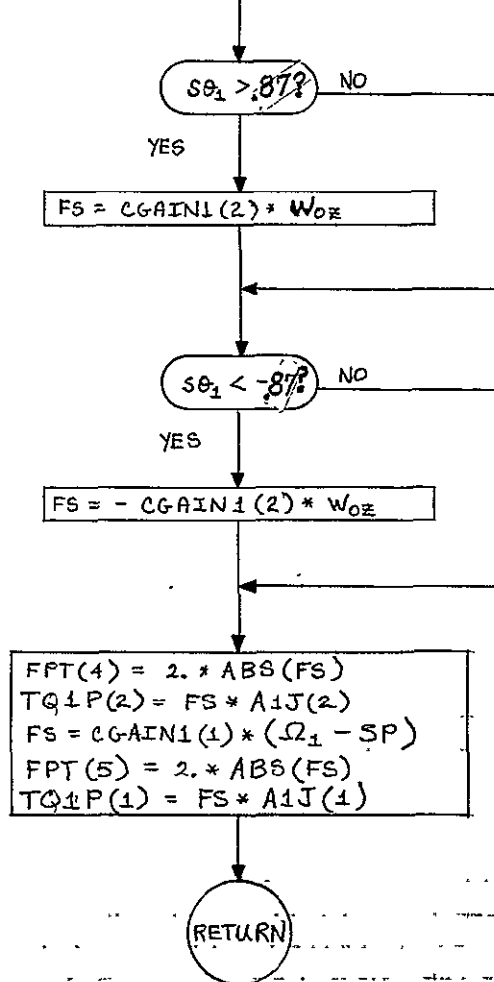
Application SUBROUTINE PCON CONTINUED

Date OCTOBER 1970 Page 2 of 2

Procedure _____

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE RECALC Date OCTOBER 1970 Page 1 of 1
 Procedure _____ Drawn By GARY JOHNSON

ENTER

CALL SCALC

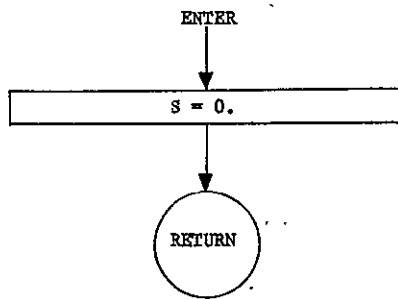
$$\begin{aligned}
 \bar{l}_2 &= \bar{d}_{12} + s * \bar{s}_2 \\
 l_{3x} &= l_3 * s\theta_3 \\
 l_{3y} &= -l_3 * c\theta_3 * s_{3z} \\
 l_{3z} &= l_3 * c\theta_3 * s_{3y} \\
 l_{4x} &= l_4 * s\theta_4 \\
 l_{4y} &= -l_4 * c\theta_4 * s_{4z} \\
 l_{4z} &= l_4 * c\theta_4 * s_{4y} \\
 R_{1x} &= (m_0/m) * d_{01x} - (m_2/m) * l_{2x} \\
 &\quad - (m_3/m) * (d_{13x} + l_{3x}) \\
 &\quad - (m_4/m) * (d_{14x} + l_{4x}) \\
 R_{1y} &= (m_0/m) * (d_{01y} * c\theta_1 + d_{01x} * s\theta_1) \\
 &\quad - (m_2/m) * l_{2y} \\
 &\quad - (m_3/m) * (d_{13y} + l_{3y}) \\
 &\quad - (m_4/m) * (d_{14y} + l_{4y}) \\
 R_{1z} &= (m_0/m) * (-d_{01y} * s\theta_1 + d_{01x} * c\theta_1) \\
 &\quad - (m_2/m) * l_{2z} \\
 &\quad - (m_3/m) * (d_{13z} + l_{3z}) \\
 &\quad - (m_4/m) * (d_{14z} + l_{4z}) \\
 \bar{R}_2 &= \bar{R}_1 + \bar{l}_2 \\
 \bar{R}_3 &= \bar{R}_1 + \bar{d}_{13} + \bar{l}_3 \\
 \bar{R}_4 &= \bar{R}_1 + \bar{d}_{14} + \bar{l}_4
 \end{aligned}$$

RETURN

FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application SUBROUTINE SCALC Date OCTOBER 1970 Page 1 of 1
Procedure _____ Drawn By GARY JOHNSON

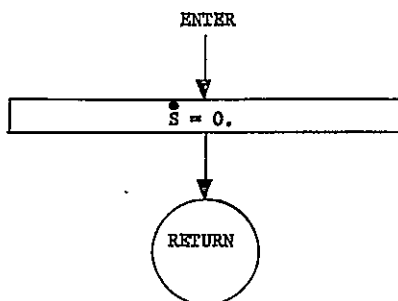


FLOW CHART & BLOCK DIAGRAM

FORM NO. 11-70-31 2-64

Application SUBROUTINE SDGALC Date OCTOBER 1970 Page 1 of 1

Procedure _____ Drawn By GARY JOHNSON

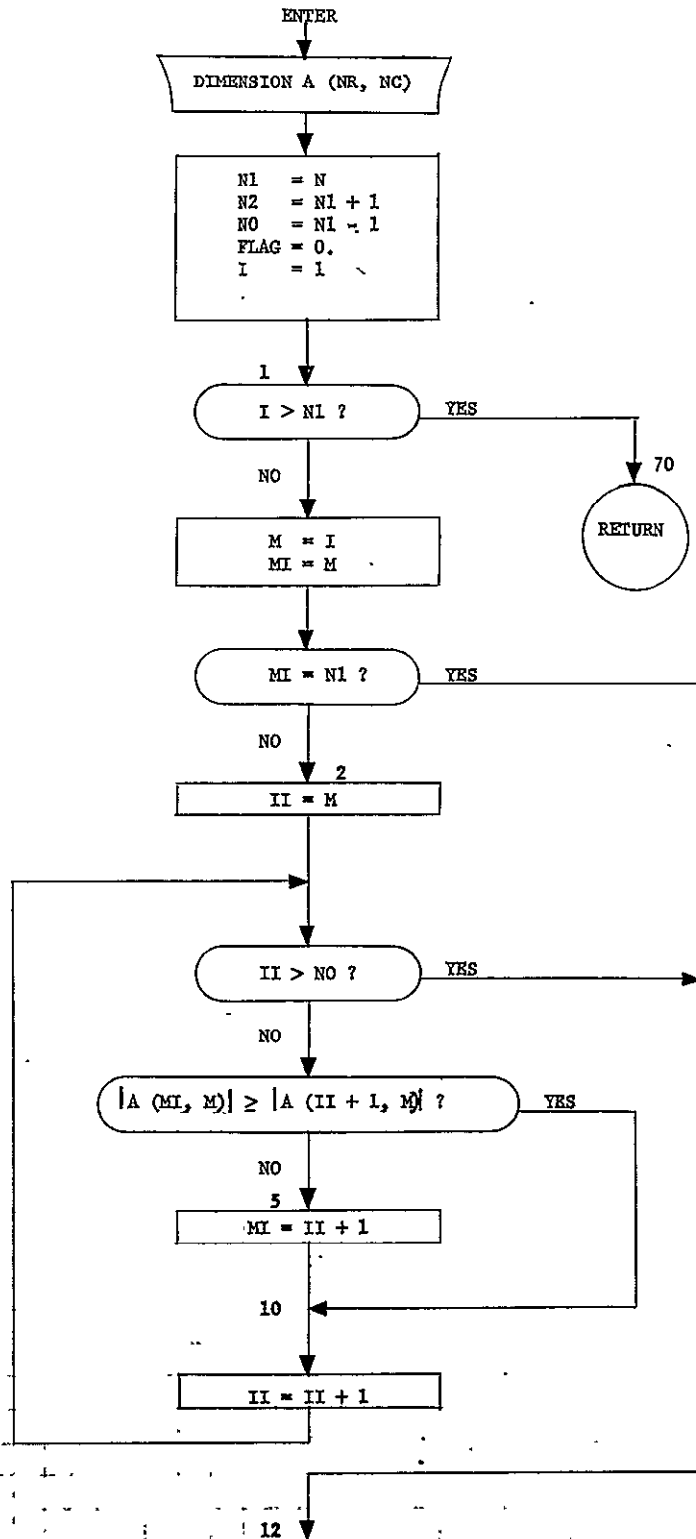


FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application SUBROUTINE SYEQNS Date OCTOBER 1970 Page 1 of 2
 Procedure _____ Drawn By GARY JOHNSON

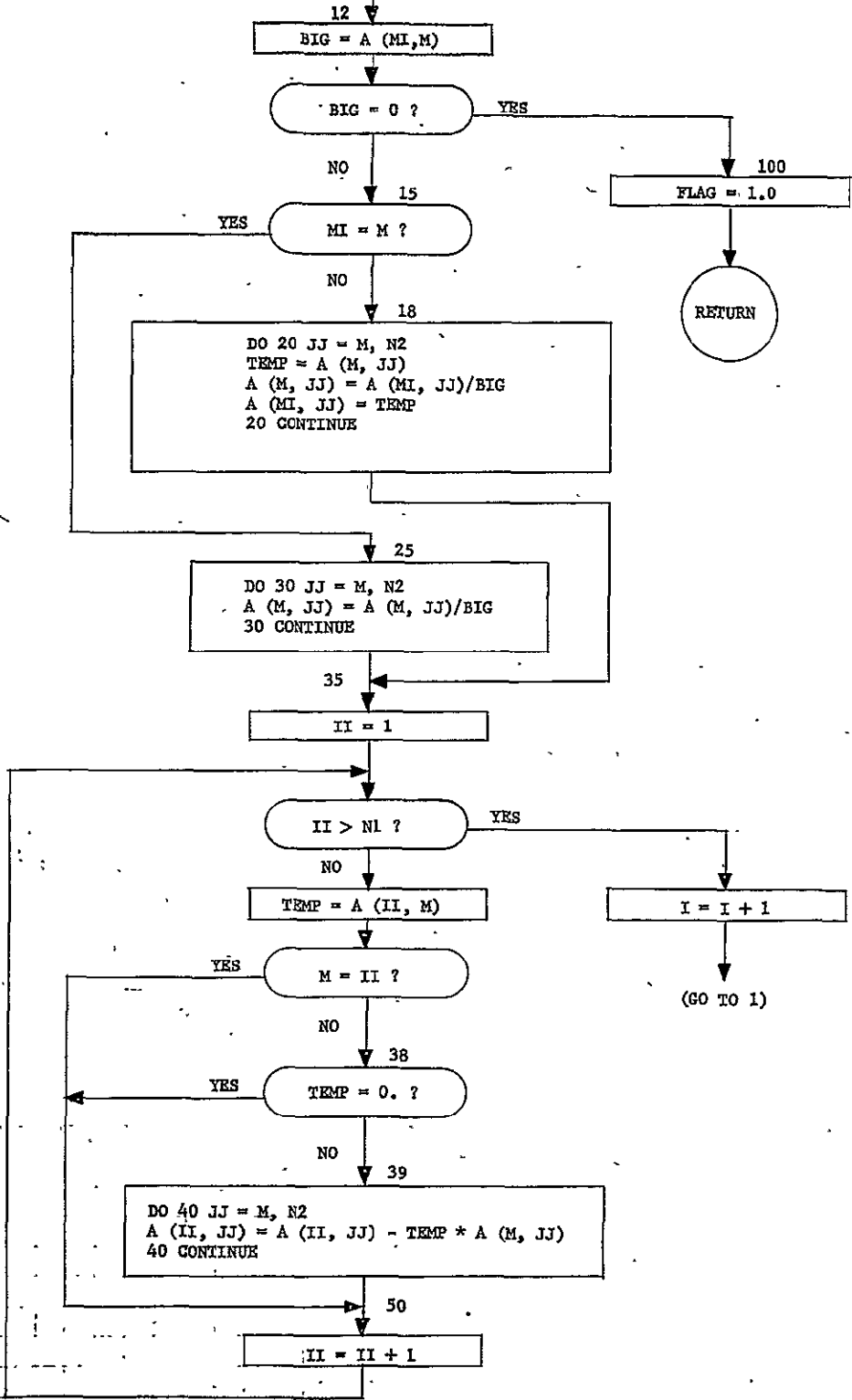
SUBROUTINE SYEQNS (A, N, NR, NC, FLAG)



CONTINUE TO THE NEXT PAGE

FLOW CHART & BLOCK DIAGRAM

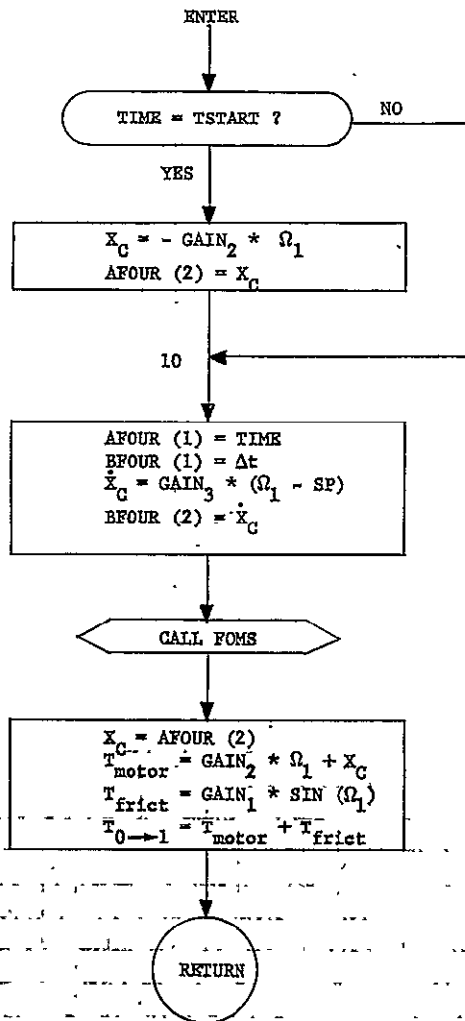
CONTINUED FROM THE PREVIOUS PAGE



FLOW CHART & BLOCK DIAGRAM

FORM 1103-01 (4-64)

Application SUBROUTINE TORQ01 Date OCTOBER 1970 Page 1 of 1
 Procedure _____ Drawn By GARY JOHNSON

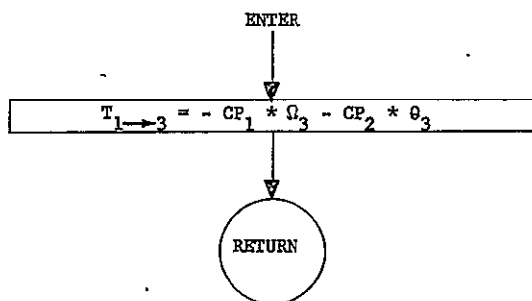


FLOW CHART & BLOCK DIAGRAM

FORM T-11 (3-61) (2-2-63)

Application SUBROUTINE TORK13 Date OCTOBER 1970 Page 1 of 1
Procedure _____ Drawn By GARY JOHNSON

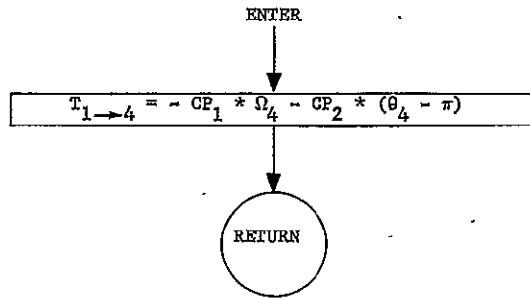
SUBROUTINE TORK13 (T13, CP1, CP2, THETA3, OMEGA3)



FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE TORK14 Date OCTOBER 1970 Page 1 of 1
Procedure _____ Drawn By GARY JOHNSON

SUBROUTINE TORK14 (T14, CP1, CP2, THETA4, OMEGA4)



FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 14-641

Application SUBROUTINE XDOT Date OCTOBER 1970 Page 1 of 5
 Procedure _____ Drawn By _____

ENTER

$$\begin{aligned} w_{1x} &= w_{0x} + \Omega_1 \\ w_{1y} &= w_{0y} * C\theta_1 + w_{0z} * S\theta_1 \\ w_{1z} &= -w_{0y} * S\theta_1 + w_{0z} * C\theta_1 \end{aligned}$$

TIME = T_{start} ?

YES

NO

CALL RECALC

2

CALL SDGALC

$$\begin{aligned} l_{2x} &= -w_{1x} * l_{2y} + w_{1y} * l_{2z} + S_{2x} * S \\ l_{2y} &= w_{1x} * l_{2x} - w_{1y} * l_{2z} + S_{2y} * S \\ l_{2z} &= -w_{1y} * l_{2x} + w_{1x} * l_{2y} + S_{2z} * S \\ \bar{R}_0 &= \bar{R}_1 - d_{01} \\ w_{3x} &= w_{1x} \\ w_{3y} &= \Omega_3 * S_{3y} + w_{1y} \\ w_{3z} &= \Omega_3 * S_{3z} + w_{1z} \\ l_{3x} &= -w_{3z} * l_{3y} + w_{3y} * l_{3z} \\ l_{3y} &= w_{3z} * l_{3x} - w_{3y} * l_{3z} \\ l_{3z} &= -w_{3y} * l_{3x} + w_{3z} * l_{3y} \\ w_{4x} &= w_{1x} \\ w_{4y} &= \Omega_4 * S_{4y} + w_{1y} \\ w_{4z} &= \Omega_4 * S_{4z} + w_{1z} \\ l_{4x} &= -w_{4z} * l_{4y} + w_{4y} * l_{4z} \\ l_{4y} &= w_{4z} * l_{4x} - w_{4y} * l_{4z} \\ l_{4z} &= -w_{4y} * l_{4x} + w_{4z} * l_{4y} \\ d_{01x} &= -w_{0x} * d_{01y} + w_{0y} * d_{01z} \\ d_{01y} &= -w_{0z} * d_{01x} - w_{0x} * d_{01z} \\ d_{01z} &= -w_{0y} * d_{01x} + w_{0x} * d_{01y} \\ d_{13x} &= -w_{1z} * d_{13y} + w_{1y} * d_{13z} \\ d_{13y} &= w_{1z} * d_{13x} - w_{1y} * d_{13z} \\ d_{13z} &= -w_{1y} * d_{13x} + w_{1z} * d_{13y} \\ d_{14x} &= -w_{1x} * d_{14y} + w_{1y} * d_{14z} \\ d_{14y} &= w_{1x} * d_{14z} - w_{1y} * d_{14x} \\ d_{14z} &= -w_{1y} * d_{14x} + w_{1x} * d_{14y} \end{aligned}$$

CONTINUE TO THE NEXT PAGE

FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE XDOT CONTINUED Date OCTOBER 1970 Page 2 of 5
 Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

$$\begin{aligned} \dot{R}_{1x} &= (m_0/m) * \dot{d}_{01x} - (m_2/m) * \dot{l}_{2x} \\ &\quad - (m_3/m) * (\dot{d}_{13x} + \dot{l}_{3x}) - (m_4/m) * (\dot{d}_{14x} + \dot{l}_{4x}) \\ \dot{R}_{1y} &= (m_0/m) * (\dot{d}_{01y} * \cos \theta_1 + \dot{d}_{01z} * \sin \theta_1) - (m_2/m) * \dot{l}_{2y} \\ &\quad - (m_3/m) * (\dot{d}_{13y} + \dot{l}_{3y}) - (m_4/m) * (\dot{d}_{14y} + \dot{l}_{4y}) \\ \dot{R}_{1z} &= (m_0/m) * (-\dot{d}_{01y} * \sin \theta_1 + \dot{d}_{01z} * \cos \theta_1) - (m_2/m) * \dot{l}_{2z} \\ &\quad - (m_3/m) * (\dot{d}_{13z} + \dot{l}_{3z}) - (m_4/m) * (\dot{d}_{14z} + \dot{l}_{4z}) \\ \dot{R}_2 &= \dot{R}_1 + \dot{l}_2 \\ \dot{R}_3 &= \dot{R}_1 + \dot{d}_{13} + \dot{l}_3 \\ \dot{R}_4 &= \dot{R}_1 + \dot{d}_{14} + \dot{l}_4 \end{aligned}$$

CALL MULT

(I.E. $\bar{H}_0 = [I_0] * \bar{w}_0$)

CALL MULT

(I.E. $\bar{H}_1 = [I_1] * \bar{w}_1$)

$$\begin{aligned} h'_{3x} &= m_3 * (-l_{3z} * \dot{R}_{3y} + l_{3y} * \dot{R}_{3z}) \\ h'_{3y} &= m_3 * (l_{3z} * \dot{R}_{3x} - l_{3x} * \dot{R}_{3z}) \\ h'_{3z} &= m_3 * (-l_{3y} * \dot{R}_{3x} + l_{3x} * \dot{R}_{3y}) \\ h'_{4x} &= m_4 * (-l_{4z} * \dot{R}_{4y} + l_{4y} * \dot{R}_{4z}) \\ h'_{4y} &= m_4 * (l_{4z} * \dot{R}_{4x} - l_{4x} * \dot{R}_{4z}) \\ h'_{4z} &= m_4 * (-l_{4y} * \dot{R}_{4x} + l_{4x} * \dot{R}_{4y}) \\ h'_{1y} &= H_{1y} + h'_{3y} + h'_{4y} \\ &\quad - m_2 * (-l_{2z} * \dot{R}_{2x} + l_{2x} * \dot{R}_{2z}) \\ &\quad - m_3 * (-d_{13z} * \dot{R}_{3x} + d_{13x} * \dot{R}_{3z}) \\ &\quad - m_4 * (-d_{14z} * \dot{R}_{4x} + d_{14x} * \dot{R}_{4z}) \\ h'_{1x} &= H_{1x} + h'_{3x} + h'_{4x} \\ &\quad - m_2 * (l_{2y} * \dot{R}_{2x} - l_{2x} * \dot{R}_{2y}) \\ &\quad - m_3 * (d_{13y} * \dot{R}_{3x} - d_{13x} * \dot{R}_{3y}) \\ &\quad - m_4 * (d_{14y} * \dot{R}_{4x} - d_{14x} * \dot{R}_{4y}) \end{aligned}$$

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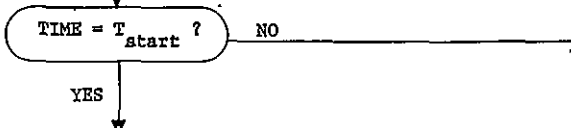
FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (1-64)

Application SUBROUTINE XDOT CONTINUED Date OCTOBER 1970 Page 3 of 5

Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



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$$\begin{aligned} h'_{1x} &= h_{1x} + h'_{3x} + h'_{4x} \\ &\quad - m_2 * (l_{2x} * R_{2y} - l_{2y} * R_{2x}) \\ &\quad - m_3 * (d_{13x} * R_{3y} - d_{13y} * R_{3x}) \\ &\quad - m_4 * (d_{14x} * R_{4y} - d_{14y} * R_{4x}) \\ \text{SUM}_1 &= m_1 * R_{1x} + m_2 * R_{2x} + m_3 * R_{3x} + m_4 * R_{4x} \\ \text{SUM}_2 &= m_1 * R_{1y} + m_2 * R_{2y} + m_3 * R_{3y} + m_4 * R_{4y} \\ \text{SUM}_3 &= m_1 * R_{1z} + m_2 * R_{2z} + m_3 * R_{3z} + m_4 * R_{4z} \\ \text{DO } 4 \text{ I} &= 1, 3 \\ H_{\text{CMGI}} &= \text{FFF}_I \\ \text{DO } 4 \text{ J} &= 1, 3 \\ H_{\text{CMGI}} &= \text{ERR}_{I,J} * w_{0J} + H_{\text{CMGI}} \\ 4 \text{ CONTINUE} \\ H_x &= H_{0x} + h'_{1x} + (-d_{01x} * C\theta_1 + d_{01y} * S\theta_1) * \text{SUM}_2 \\ &\quad + (d_{01x} * S\theta_1 + d_{01y} * C\theta_1) * \text{SUM}_3 + H_{\text{CMGX}} \\ H_y &= H_{0y} + C\theta_1 * h'_{1y} - S\theta_1 * h'_{1z} + d_{01x} * \text{SUM}_1 \\ &\quad - d_{01x} * S\theta_1 * \text{SUM}_2 - d_{01x} * C\theta_1 * \text{SUM}_3 + H_{\text{CMGY}} \\ H_z &= H_{0z} + S\theta_1 * h'_{1y} + C\theta_1 * h'_{1z} - d_{01y} * \text{SUM}_1 \\ &\quad + d_{01x} * C\theta_1 * \text{SUM}_2 - d_{01x} * S\theta_1 * \text{SUM}_3 + H_{\text{CMGZ}} \end{aligned}$$

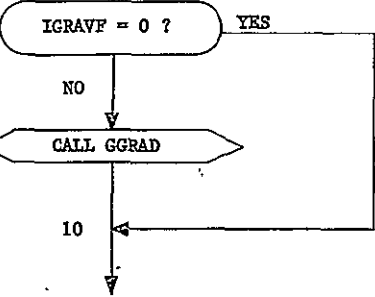

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5

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$$\begin{aligned} \text{AJ}_{1x} &= m_2 * l_{2x} + m_3 * d_{13x} + m_3 * l_{3x} + m_4 * d_{14x} + m_4 * l_{4x} \\ \text{AJ}_{1y} &= m_2 * l_{2y} + m_3 * d_{13y} + m_3 * l_{3y} + m_4 * d_{14y} + m_4 * l_{4y} \\ \text{AJ}_{1z} &= m_2 * l_{2z} + m_3 * d_{13z} + m_3 * l_{3z} + m_4 * d_{14z} + m_4 * l_{4z} \\ \theta_0 &= \text{TIME} * w_8 \end{aligned}$$


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10

CONTINUE TO THE FOLLOWING PAGE

FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE XDOT CONTINUED

Date OCTOBER 1970

Page 4 of 5

Procedure _____

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

$$\begin{aligned} \bar{F}_0 &= \bar{F}_{01} \\ \bar{F}_1 &= \bar{F}_{11} \\ \bar{T}_{OEF} &= \bar{T}_{OEG} + \bar{T}_{OP} \\ \bar{T}_{IEF} &= \bar{T}_{IG} + \bar{T}_{IP} \\ \text{TERM1}(1) &= (m_o - m) * d_{01x} - AJ_{1x} \\ \text{TERM1}(2) &= (m_o - m) * d_{01y} - C\theta_1 * AJ_{1y} + S\theta_1 * AJ_{1z} \\ \text{TERM1}(3) &= (m_o - m) * d_{01z} - S\theta_1 * AJ_{1y} - C\theta_1 * AJ_{1z} \\ \text{TERM2}(1) &= m_o * d_{01x} - AJ_{1x} \\ \text{TERM2}(2) &= m_o * (C\theta_1 * d_{01y} + S\theta_1 * d_{01z}) - AJ_{1y} \\ \text{TERM2}(3) &= m_o * (-S\theta_1 * d_{01y} + C\theta_1 * d_{01z}) - AJ_{1z} \\ \text{ATCPT2}_{1,1} &= 0. \\ \text{ATCPT2}_{1,2} &= -\text{TERM2}(3) \\ \text{ATCPT2}_{1,3} &= \text{TERM2}(2) \\ \text{ATCPT2}_{2,1} &= C\theta_1 * \text{TERM2}(3) + S\theta_1 * \text{TERM2}(2) \\ \text{ATCPT2}_{2,2} &= -S\theta_1 * \text{TERM2}(1) \\ \text{ATCPT2}_{2,3} &= -C\theta_1 * \text{TERM2}(1) \\ \text{ATCPT2}_{3,1} &= S\theta_1 * \text{TERM2}(3) - C\theta_1 * \text{TERM2}(2) \\ \text{ATCPT2}_{3,2} &= C\theta_1 * \text{TERM2}(1) \\ \text{ATCPT2}_{3,3} &= -S\theta_1 * \text{TERM2}(1) \\ H_x &= w_{0z} * H_y - w_{0y} * H_z + (-\text{TERM1}(3) * F_{0y} + \text{TERM1}(2) * F_{0x})/m \\ &+ (\text{ATCPT2}_{1,1} * F_{1x} + \text{ATCPT2}_{1,2} * F_{1y} + \text{ATCPT2}_{1,3} * F_{1z})/m \\ &+ T_{OEFx} + T_{IEFx} \\ H_y &= -w_{0z} * H_x + w_{0x} * H_z + (\text{TERM1}(3) * F_{0x} - \text{TERM1}(1) * F_{0z})/m \\ &+ (\text{ATCPT2}_{2,1} * F_{1x} + \text{ATCPT2}_{2,2} * F_{1y} + \text{ATCPT2}_{2,3} * F_{1z})/m \\ &+ T_{OEFy} + C\theta_1 * T_{IEFy} - S\theta_1 * T_{IEFz} \\ H_z &= w_{0y} * H_x - w_{0x} * H_y + (-\text{TERM1}(2) * F_{0x} + \text{TERM1}(1) * F_{0y})/m \\ &+ (\text{ATCPT2}_{3,1} * F_{1x} + \text{ATCPT2}_{3,2} * F_{1y} + \text{ATCPT2}_{3,3} * F_{1z})/m \\ &+ T_{OEFz} + S\theta_1 * T_{IEFy} + C\theta_1 * T_{IEFz} \end{aligned}$$

CALL TORR01

$$\begin{aligned} \dot{h}_{1x} &= -w_{1y} * \dot{h}_{1z} + w_{1z} * \dot{h}_{1y} \\ &+ R_{1y} * (-m_2 * \dot{l}_{2z} - m_3 * (\dot{d}_{13x} + \dot{l}_{3z})) - m_4 * (\dot{d}_{14x} + \dot{l}_{4z}) \\ &- R_{1z} * (-m_2 * \dot{l}_{2y} - m_3 * (\dot{d}_{13y} + \dot{l}_{3y})) - m_4 * (\dot{d}_{14y} + \dot{l}_{4y}) \\ &- AJ_{1y} * (-F_{0y} * S\theta_1/m + F_{0x} * C\theta_1/m) \\ &+ AJ_{1z} * (F_{0y} * C\theta_1/m + F_{0x} * S\theta_1/m) \\ &+ AJ_{1x} * F_{1y}/m - AJ_{1y} * F_{1z}/m + T_{IEFx} + T_{O\rightarrow 1} \end{aligned}$$

CONTINUE TO THE FOLLOWING PAGE

FLOW CHART & BLOCK DIAGRAM

FORM DEN 1102-01 (4-64)

Application SUBROUTINE XDOT CONTINUED Date OCTOBER 1970 Page 5 of 5

Procedure _____ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

CALL TORK13

$$\begin{aligned}
 \dot{G}_3 = & -S_{3y} * (w_{1x} * h_{3x} - w_{1x} * h_{3z}) \\
 & - S_{3z} * (w_{1x} * h_{3y} - w_{1y} * h_{3x}) \\
 & + m_3 * S_{3y} * (l_{3z} * R_{3x} - l_{3x} * R_{3z}) \\
 & + m_3 * S_{3z} * (l_{3x} * R_{3y} - l_{3y} * R_{3x}) \\
 & - (m_3/m) * S_{3y} * (l_{3z} * (F_{0x} + F_{1x}) - l_{3x} * (-F_{0y} * S\theta_1 + F_{0z} * C\theta_1 + F_{1z})) \\
 & - (m_3/m) * S_{3z} * (l_{3x} * (F_{0y} * C\theta_1 + F_{0z} * S\theta_1 + F_{1y}) \\
 & - l_{3y} * (F_{0z} + F_{1z})) + T_1 \rightarrow 3
 \end{aligned}$$

CALL TORK14

$$\begin{aligned}
 \dot{G}_4 = & -S_{4y} * (w_{1x} * h_{4x} - w_{1x} * h_{4z}) \\
 & - S_{4z} * (w_{1x} * h_{4y} - w_{1y} * h_{4x}) \\
 & + m_4 * S_{4y} * (l_{4z} * R_{4x} - l_{4x} * R_{4z}) \\
 & + m_4 * S_{4z} * (l_{4x} * R_{4y} - l_{4y} * R_{4x}) \\
 & - (m_4/m) * S_{4y} * (l_{4z} * (F_{0x} + F_{1x}) - l_{4x} * (-F_{0y} * S\theta_1 + F_{0z} * C\theta_1 + F_{1z})) \\
 & - (m_4/m) * S_{4z} * (l_{4x} * (F_{0y} * C\theta_1 + F_{0z} * S\theta_1 + F_{1y}) \\
 & - l_{4y} * (F_{0z} + F_{1z})) + T_1 \rightarrow 4
 \end{aligned}$$

RETURN

APPENDIX E, SUBROUTINE DESCRIPTIONS

Subroutine: CMG

Purpose: This subroutine computes the angular momenta produced by the CMGs located on body 0. Either 2 degree of freedom, 1 degree of freedom or reaction wheels can be accommodated.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|---|
| I | NUMCMG | N_{CMG} | The number of CMGs located on body 0 |
| I | IDOF(K) | I_{DOF} | The number of degrees of freedom for the <u>kth</u> CMG |
| I | HW(K) | \bar{H} | The momentum of the <u>kth</u> wheel |
| I | AIJ(J,K,M) | I_I | The inertia matrix of the inner gimbal including wheel. The subscript J refers to the CMG being referenced, K, and M are dimensioned 3 and accommodate the inertia matrix |
| I | AIO(J,K,M) | I_o | The inertia matrix of the outer gimbal. The meaning of the subscripts are the same as AIJ(J,K,M) |
| I | THATA(J) | θ_j | The inner gimbal angle |
| I | FEE(J) | ϕ_j | The outer gimbal angle |
| I | THATA(J) | $\dot{\theta}_j$ | The time-derivative of θ_j |
| I | FEED(J) | $\dot{\phi}_j$ | The time derivative of ϕ_j |
| O | FFF(M) | f | The total angular momentum of the CMGs which is not a function of the angular rates |
| O | EEE(M,N) | E | The total angular momentum of the CMGs which is a function of the angular rates. For further discussion see the Appendix |

Subroutines required: None

Discussion: None

Subroutine ATT

Purpose: This routine simulates the action of an attitude control system using reaction jets.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|--|
| I | WO(3) | $\vec{\omega}_0$ | Angular rates of Body 0 (stator) |
| I | TIBO(3,3) | $[I, B]_0$ | Transformation from Body 0 to inertial frame |
| I | CA(3) | \overline{CA} | Direction cosines of reference direction |
| I | TIME | t | Time |
| I | BODYII(1,1) | I_{11} | Moment of inertia around spin axis of rotor |
| I | OMEGA1 | Ω_1 | Gimbal rate of rotor |
| I | DELTAT | Δt | Time increment per step |
| O | TQOP(3) | | Control torques |
| O | FAT(8) | | Control forces |
| I | AOJ(3) | | Reaction jet lever arms |

Subroutines required: none

Equations programmed: $AK = \Omega_1 L_{11} \sin\beta/2 / (5.5 + \Delta t)$
coordinate transformations

Discussion: A complete description of this routine is given in the final report.

In order to activate the attitude control function it is necessary to set both IPROPF and IATTIF in the input data.

The attitude section also requires designation of the three direction cosines (CA(1), CA(2), CA(3)) of the direction in

inertial space at which control is desired. For a reorientation maneuver the initial orientation of the spin axis in inertial space read in (TIBOI(1,1), TIBOI(2,1), TIBOI(2,3) are the initial direction cosines of the spin axis in inertial space) can be specified different from GA. It is necessary, however, to ensure that the angle between the initial direction of the spin axis and the direction to which it is commanded to be redirected be not greater than 60° for the attitude control routine employed in this program.

The propulsion control section must be supplied with appropriate jet couple lengths and control gains for removal of transverse angular rates (see discussion on PCON subroutine). The control can be on either Body 0 or Body 1 or on both.

Subroutine: EMCALC

Purpose: Subroutine EMCALC assembles the M matrix used in the calculations from which the angular velocities are computed.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|----------------|---|
| I | THETA1 | θ_1 | Angular displacement between bodies 0 and 1 |
| I | R1(3) | \vec{r}_1 | Vector distance from system c.m. to the c.m. of body 1 |
| I | R2(3) | \vec{r}_2 | Vector distance from system c.m. to the c.m. of body 2 |
| I | R3(3) | \vec{r}_3 | Vector distance from system c.m. to the c.m. of body 3 |
| I | R4(3) | \vec{r}_4 | Vector distance from system c.m. to the c.m. of body 4 |
| I | EL2(3) | \vec{l}_2 | Vector position of the movable mass |
| I | EL3(3) | \vec{l}_3 | Vector position of body 3 from hinge line s_3 |
| I | EL4(3) | \vec{l}_4 | Vector position of body 4 from hinge line s_4 |
| I | D01(3) | \vec{d}_{01} | Vector distance from the c.m. of body 0 to the hinge line of body 1 |
| I | D13(3) | \vec{d}_{13} | Vector distance from the c.m. of body 1 to the hinge line of body 3 |
| I | D14(3) | \vec{d}_{14} | Vector distance from the c.m. of body 1 to the hinge line of body 4 |
| I | BOMASS | m_0 | Mass of body 0 |

| | | | |
|-------------|-------------|-------------|--|
| I | B2MASS | m_2 | Mass of body 2 |
| I | B3MASS | m_3 | Mass of body 3 |
| I | B4MASS | m_4 | Mass of body 4 |
| I | TOTMAS | m_3 | Mass of composite body |
| I | | A_1 | Coordinate transformation from body 0 to body 1 |
| I | R1(3) | \vec{r}_1 | Vector distance from system c.m. to the c.m. of body 1 |
| I | R2(3) | \vec{r}_2 | Vector distance from the system c.m. to the c.m. of body 2 |
| I | R3(3) | \vec{r}_3 | Vector distance from the system c.m. to the c.m. of body 3 |
| I | BODY0I(3,3) | I_0 | The inertia matrix of body 0 |
| I | BODY1I(3,3) | I_1 | The inertia matrix of body 1 |
| I | S3(3) | \vec{s}_3 | The hinge line of body 3 |
| I | S4(3) | \vec{s}_4 | The hinge line of body 4 |
| \emptyset | EM(6,6) | m_{ij} | The M matrix |

Subroutines required: None

Equations programmed: The M matrix is related to the angular momenta and the angular velocities by the equation shown below:

$$\begin{bmatrix} H_x \\ H_y \\ H_z \\ h_{1x}^i \\ h_3^i \cdot s_3 \\ h_4^i \cdot s_4 \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} & M_{13} & M_{14} & M_{15} & M_{16} \\ M_{21} & M_{22} & M_{23} & M_{24} & M_{25} & M_{26} \\ M_{31} & M_{32} & M_{33} & M_{34} & M_{35} & M_{36} \\ M_{41} & M_{42} & M_{43} & M_{44} & M_{45} & M_{46} \\ M_{51} & M_{52} & M_{53} & M_{54} & M_{55} & M_{56} \\ M_{61} & M_{62} & M_{63} & M_{64} & M_{65} & M_{66} \end{bmatrix} \begin{bmatrix} \omega_{0x} \\ \omega_{0y} \\ \omega_{0z} \\ \Omega_1 \\ \Omega_3 \\ \Omega_4 \end{bmatrix}$$

Subroutine FOMS

Purpose: This integration routine calculates values of a set of variables at time t_{n+1} from their values at t_n and their derivatives at times t_n and t_{n-1} .

Calling Sequence: FOMS (A, B, N, E, TJ)

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------------|---|
| I | A(I) | $x_{i,n}$ | i th variable at time t_n ; $i = 1, 2, \dots, n$; $I = i + 1$ |
| O | A(I) | $x_{i,n+1}$ | i th variable at time t_{n+1} |
| I | B(I) | $\dot{x}_{i,n}$ | i th derivative at time t_n |
| I | N | m | Number of variables to be integrated; $m = N-1$ |
| I,O | E | | Flag to use current derivatives for past derivatives on first integration |
| I | TJ(I) | $\dot{x}_{i,n-1}$ | i th derivative at time t_{n-1} |
| O | TJ(I) | $\dot{x}_{i,n}$ | i th derivative at time t_n , storage for next step |

Subroutines required: none

Equations programmed: $x_{n+1} = x_n + 1/2 \Delta t (3\dot{x}_n - \dot{x}_{n-1})$

Discussion: The variables and derivatives are indexed over values of I from 2 to N. B(1) is used to bring in Δt . A(1) is set up to be used for time but is not used in this program. On the first integration the current derivatives are also used as past derivatives since no past derivatives are available.

Subroutine GGRAD

Purpose: This subroutine calculates the forces and torques due to gravity gradient on Body 0 and Body 1.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|---------------------|---|
| I | THETO | θ_0 | True anomaly |
| I | TIBO(3,3) | $[I,B]_0$ | Transformation from Body 0 to inertial frame |
| I | BODY0I(3,3) | $[I_0]$ | Moment of inertia matrix of Body 0 |
| I | BODY1I(3,3) | $[I_1]$ | Moment of inertia matrix of Body 1 |
| O | F0I(3) | $\overline{F_{0I}}$ | Force on Body 0 due to gravity gradient |
| O | F1I(3) | $\overline{F_{1I}}$ | Force on Body 1 due to gravity gradient |
| O | TQOG(3) | | Torque on Body 0 due to gravity gradient |
| O | TQIG(3) | | Torque on Body 1 due to gravity gradient |
| I | C1 | | Gravitation constant and earth radius factor |
| I | BOMASS | m_0 | Mass of Body 0 |
| I | B1MASS | m_1 | Mass of Body 1 |
| I | THETA1 | θ_1 | Gimbal angle of Body 1 |
| I | RO(3) | r_0 | Distance between centers of mass of Body 0 and system |
| I | RI(3) | r_1 | Distance between centers of mass of Body 1 and system |

Equations programmed:

$$\text{Torque: } T_G = - \frac{3\mu}{R_0} \bar{R}_0 \times [\bar{I} \cdot \bar{R}_0]$$

$$\text{Force: } F_G = \frac{\mu m}{R_0^3} \left(\bar{r} - \frac{3\bar{R}_0 \cdot \bar{r}}{R_0^2} \bar{R}_0 \right)$$

where R_0 = distance to center of earth

r = distance between center of mass of body and
center of mass of system

Discussion: The translational motion is limited to circular orbits in the X-Y inertial plane in order to simplify transformations and relationships in this subroutine. Gravity gradient effects on Body 2, Body 3 and Body 4 are neglected.

Subroutine: HCON

Purpose: The subroutine contains the control laws in terms of gimbal angle rates for the CMGs. In most cases the user must furnish his own control law.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|---|
| I | | | Any program variables to be used in the control law |
| O | FEED(J) | $\dot{\phi}_J$ | Outer gimbal rate of the <u>J</u> th CMG |
| O | THATAD(J) | $\dot{\theta}_J$ | Inner gimbal rate of the <u>J</u> th CMG |

Subroutines required: CMG

Discussion: None

Subroutine MULT

Purpose: Subroutine MULT multiplies either a 3 x 3 matrix by a 3 x 1 matrix or a 3 x 3 matrix by a 3 x 3 matrix.

Calling sequence: CALL MUTL (C, A, B, F, D, E, MTYPE)

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|---|
| I | A | | A 3 x 3 matrix used in the matrix multiplication $C = A \times B$ |
| I | B | | A 3 x 1 matrix used in the matrix multiplication $C = A \times B$ |
| Ø | C | | A 3 x 1 matrix which is the result of $A \times B$ |
| I | D | | A 3 x 3 matrix used in the matrix multiplication $F = D \times E$ |
| I | E | | A 3 x 3 matrix used in the matrix multiplication $F = D \times E$ |
| Ø | F | | A 3 x 3 matrix which is the result of $D \times E$ |
| I | MTYPE | | A flag which determines the type of matrix multiplication being performed. If MTYPE = 1 then $C = A \times B$ is performed, if MTYPE \neq 1 then $D = E \times F$ is performed. |

Discussion: When subroutine MULT is used to multiply a 3 x 3 matrix by a 3 x 1 matrix variables F, D, E are dummies, when used to multiply two 3 x 3 matrices then variables C, A, B are dummies.

Subroutine PCON

Purpose: To simulate a reaction jet control system for removing transverse components of angular velocity, maintaining the spin rate of the rotor and removing spin axis angular rates of the stator.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|---|
| I | WO | $\bar{\omega}_0$ | Angular rates of Body 0 |
| I | THETA1 | θ_1 | Angle of Body 1 with respect to Body 0 |
| I | OMEGA1 | Ω_1 | Angular velocity of Body 1 with respect to Body 0 |
| I | CGAINO(3) | | Control gains of stator jets |
| I | AOJ(3) | | Stator jet couple arm length |
| I | CGAINI(2) | | Control gains of rotor jets |
| I | ALJ(2) | | Rotor jet couple arm length |
| O | TQOP(3) | | Control torques on stator |
| O | TQIP(3) | | Control torques on rotor |
| O | FPT(5) | | Control forces |

Subroutines required: none

Equations programmed: none

Discussion: Certain restrictions on the configuration of the reaction jets have been assumed.

Associated with the torque around an axis there are four jets. One pair is in a pure couple to produce torque in one direction. The other pair, identical in location and strength, is oppositely directed. No torque is produced around axes other than the one designated.

In setting up input data for the reaction jet controls, the

control gain of the jets of the couple and the distance between the two jets forming the couple must be specified. Since the couples are similar for the two directions, this data is read only once for each axis.

The firing of jets on Body 1 (rotor) must be timed according to alignment with stator axes. Gimbal angle sensing is used in this routine to provide this timing.

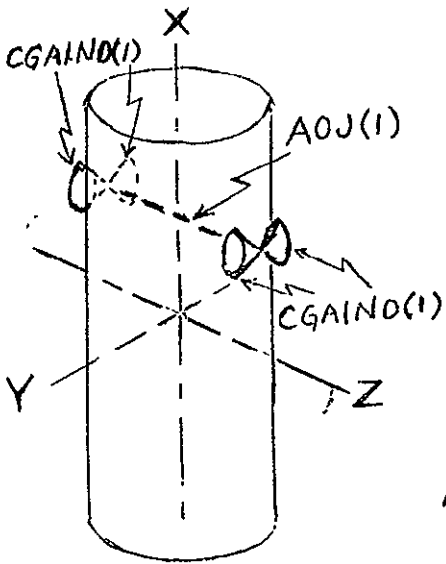
The PCON subroutine simulates a reaction jet control on angular rates. Transverse control torques are made proportional and opposite to transverse velocities. Such a control is similar in effect to an external frictional force acting against transverse motion. For a transverse torque T_T related to the magnitude of transverse rate ω_T by $T_T = -K \omega_T$ some estimate of the decrease in magnitude of transverse rate over a time interval t is given by $\omega_T \approx \omega_{T0} e^{-K/I_T t}$ where ω_{T0} is the initial transverse angular rate and $I_T = \sqrt{(I_{022} + I_{122})(I_{033} + I_{133})}$. This estimate will be good for jets on Body 0 where both transverse axes are controlled. For the single axis jets on the rotor the control will be much slower due to the time that the rotor spends in unfavorable positions.

In Figure jet configurations are illustrated. Note that it is not necessary for jets to be symmetrically located with respect to any coordinate axes or planes. It is necessary, however, that the X-jet couple arm be parallel to the Y-Z plane, the Y-jet couple arm be parallel to the X-Z plane, etc. The data deck is simplified by requiring only magnitudes of jet couple arms without regard for actual directions or components.

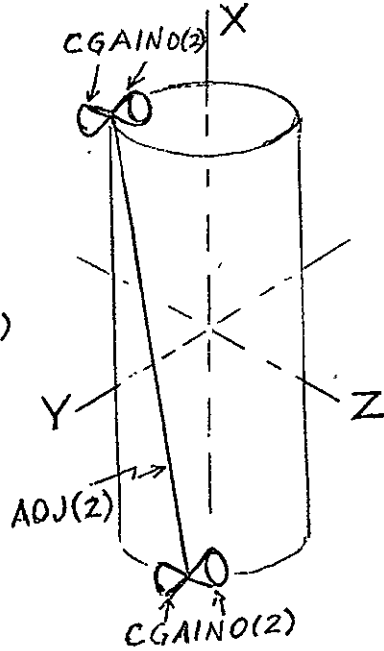
The reaction jets are activated by setting IPROPF = 1 and supplying control gain and couple arm length data. If it is desired to leave a certain axis uncontrolled, the corresponding control gain is set to zero, but the couple arm length should be given some non-zero value in order to prevent division by zero in calculation of impulse contributions.

Body 0

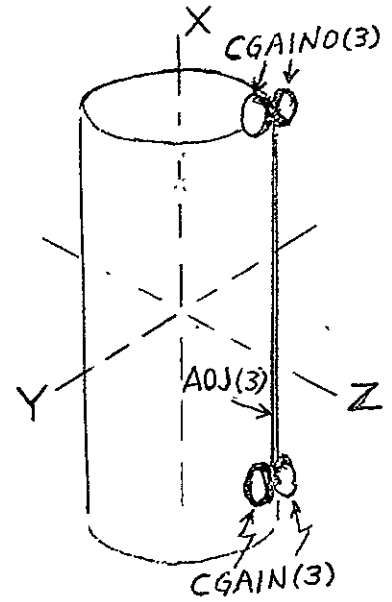
X-Axis Jets



Y-Axis Jets

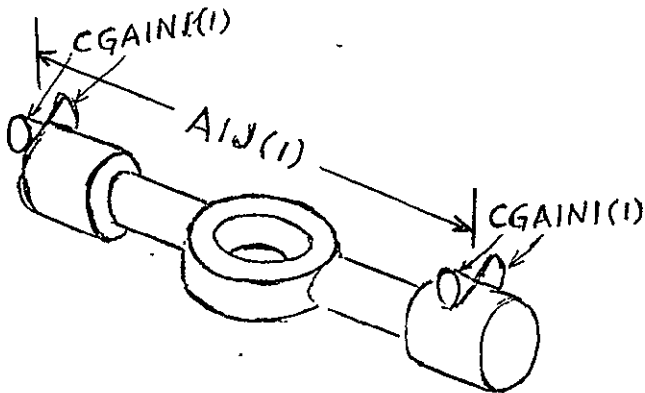


Z-Axis Jets

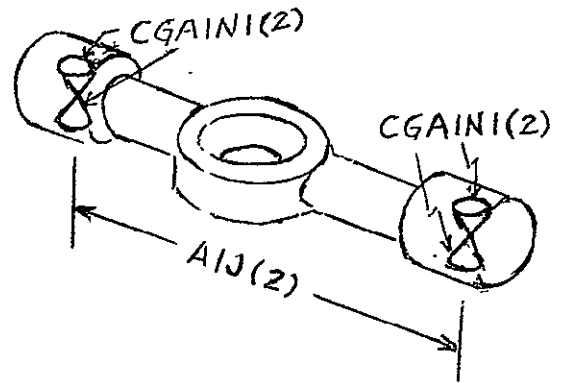


Body 1

X-Axis Jets



Y-Axis Jets



Subroutine: RECALC

Purpose: The purpose of this subroutine is to compute the distance from combined system center of mass to the center of mass of the various bodies.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|----------------|---|
| I | BOMASS | m_0 | Mass of body 0 |
| I | B2MASS | m_2 | Mass of body 2 |
| I | B3MASS | m_3 | Mass of body 3 |
| I | B4MASS | m_4 | Mass of body 4 |
| I | TOTMASS | m | Mass of composite body |
| I | D01(3) | \vec{d}_{01} | Vector distance from the c.m. of body 0 to the hinge line of body 1 |
| I | EL2(3) | $\vec{\ell}_2$ | Vector position of the movable mass. |
| I | D13(3) | \vec{d}_{13} | Vector distance from the c.m. of body 1 to the hinge line of body 3 |
| I | D14(3) | \vec{d}_{14} | Vector distance from the c.m. of body 1 to the hinge line of body 4 |
| I | EL3(3) | $\vec{\ell}_3$ | Vector position of body 3 from the hinge line s_3 |
| I | EL4(3) | $\vec{\ell}_4$ | Vector position of body 4 from the hinge line s_4 |
| O | R1(3) | \vec{r}_1 | Vector distance from system c.m. to the c.m. of body 1 |
| O | R2(3) | \vec{r}_2 | Vector distance from the system c.m. to the c.m. of body 2 |

| | | | |
|---|-------|-------------|--|
| 0 | R3(3) | \bar{r}_3 | Vector distance from the system c.m. to the c.m. of body 3 |
| 0 | R4(4) | \bar{r}_4 | Vector distance from the system c.m. to the c.m. of body 4 |

Subroutines required: None

Equations programmed:

$$r_1 = \frac{m_0}{m} \bar{d}_{01} - \frac{m_2}{m} \bar{l}_2 - \frac{m_3}{m} (\bar{d}_{13} + \bar{l}_3) - \frac{m_4}{m} (\bar{d}_{14} + \bar{l}_4)$$

$$r_2 = \frac{m_0}{m} d_{01} + (1 - \frac{m_2}{m}) l_2 - \frac{m_3}{m} (d_{13} + l_3) - \frac{m_4}{m} (d_{14} + l_4)$$

$$r_3 = \frac{m_0}{m} d_{10} - \frac{m_2}{m} l_2 + (1 - \frac{m_3}{m}) (d_{13} + l_3) - \frac{m_4}{m} (d_{14} + l_4)$$

$$r_4 = \frac{m_0}{m} d_{01} - \frac{m_2}{m} l_2 - \frac{m_3}{m} (d_{13} + l_3) + (1 - \frac{m_4}{m}) (d_{14} + l_4)$$

$m_0, m_2, m_3, m_4, m,$

d_{10}, d_{13}, d_{14}

l_2, l_3, l_4

r_1, r_2, r_3, r_4

Subroutine SCALC

Purpose: This routine supplies the position of the movable mass, Body 2.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|--|
| 0 | S | S | Distance of Body 2 from D12 along direction S2 |

Note: Other I/O variables may be employed depending on the formulation of the subroutine.

Subroutines required: Not specified

Equations programmed: Not specified

Discussion: This subroutine will be constructed to suit the needs of the user. Any variables appearing in the common region can be employed as input/output variables.

Subroutine SDCALC

Purpose: This routine supplies the speed of the movable mass, Body 2.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|---|
| 0 | SDOT | \dot{s} | Magnitude of velocity of Body 2 along direction S2. |

Note: Other I/O variables may be employed depending on the formulation of the subroutine.

Subroutines required: Not specified

Equations programmed: Not specified

Discussion: This subroutine will be constructed to suit the needs of the user. Any variables appearing in the common region can be employed as input/output variables.

Subroutine: SYEQNS (A,N,NR,NC,FLAG)

Purpose: Subroutine SYEQNS solves a set of linear simultaneous equations $AX = c$ to determine the column vector x .

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|--|
| I/O | A | A | A is the system matrix as depicted above. Also the answer x will appear as the $N+1$ at column of matrix A |
| I | N | N | N is the number of linear equations to be solved |
| I | NR | NR | NR is the number of rows in A |
| I | NC | NC | NC is the number of columns in A |
| O | FLAG | FLAG | If FLAG = 0 a solution exists if FLAG = 1 no solution exists |

Subroutines required: None

Discussion: None

Subroutine: TORK01

Purpose: The purpose of this subroutine is to compute the torque acting between bodies 0 and 1. The present version of TORK01 contains a frictional torque as well as torque motor with appropriate control law.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|---|
| I | | | Any of the variables carried through common |
| O | T01 | T_{01} | The torque acting between body 0 and body 1 |

Discussion: None ,

Subroutine: TORK13

Purpose: This subroutine computes the torque between body 1 and body 3.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|---|
| I | THETA3 | θ_3 | Angular displacement of body 3 about the hinge line s_3 |
| I | OMEGA3 | ω_3 | Angular velocity of body 3 about the hinge line s_3 |
| I | CP1 | CP1 | Gain for ω_3 |
| I | CP2 | CP2 | Gain for θ_3 |
| O | T13 | T_{13} | The torque acting between bodies 1 and 3 |

Subroutines required: None

Equations programmed:

$$T_{1 \rightarrow 3} = -CP1 \times \omega_3 - CP2 \times \theta_3$$

Subroutine: TORK14

Purpose: This subroutine computes the torque acting between body 1 and body 4.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|---|
| I | THETA4 | θ_4 | Angular displacement of body 4 about the hinge line s_4 |
| I | OMEGA4 | ω_4 | Angular velocity of body 4 about the hinge line s_4 |
| I | CP1 | CP_1 | Gain for ω_4 |
| I | CP2 | CP_2 | Gain for θ_3 |
| O | T14 | T_{14} | The torque acting between bodies 1 and 4 |

Subroutines required: None

Equation programmed:

$$T_{1 \rightarrow 4} = - CP1 \times \omega_4 - CP2 \times (\theta_4 - \pi)$$

Subroutine XDOT

Purpose: To compute the derivative of the unconstrained components of angular momenta as well as the variable required for these calculations.

Segment 1

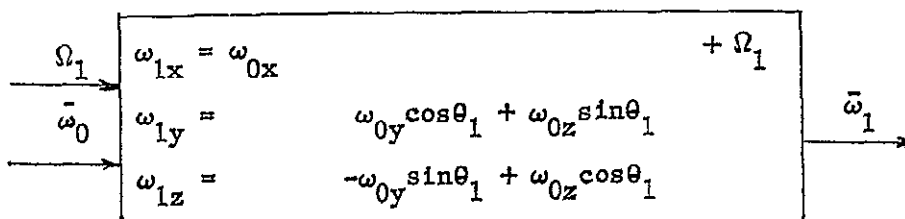
Purpose: To compute the angular velocity of body 1.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|---|
| I | OMEGA1 | Ω_1 | Angular velocity between bodies 1 and 0 |
| I | WO(3) | $\bar{\omega}_0$ | Angular velocity of body 0 |
| Ø | W1(3) | $\bar{\omega}_1$ | Angular velocity of body 1 |
| I | THETA1 | θ_1 | Angular displacement between bodies 1 and 0 |

Subroutines required: None

Equations Programmed:



Discussion: The angular velocity of body 0 ($\bar{\omega}_0$) is transformed to the body 1 coordinate system and is added to the primary gimbal rate to obtain the angular velocity of body 1 ($\bar{\omega}_1$).

Segment 2.

Purpose: To compute the vector position of the movable mass from the center-of-mass (c.m.) of body 1.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|----------------|--|
| I | S | s | Movable mass travel, a specified scalar function of time |
| I | D12(3) | \vec{d}_{12} | Fixed vector (in body 1 coordinates) locating the path of movable mass from c.m. of body 1 |
| I | S2(3) | \vec{s}_2 | Unit vector defining direction in which the movable mass travels |
| Ø | EL2(3) | \vec{l}_2 | Position of movable mass (in body 1 coordinates) from c.m. of body 1 |

Subroutines required: None

Equations programmed:

$$\begin{array}{l}
 \vec{s} \rightarrow \\
 \vec{d}_{12} \\
 \vec{s}_2
 \end{array}
 \rightarrow
 \begin{array}{l}
 l_{2x} = d_{12x} + ss_{2x} \\
 l_{2y} = d_{12y} + ss_{2y} \\
 l_{2z} = d_{12z} + ss_{2z}
 \end{array}
 \rightarrow \vec{l}_2$$

Discussion: The position of the movable mass is computed from the vector equation $\vec{l}_2 = \vec{d}_{12} + \vec{s}_2 s$.

Segment 3

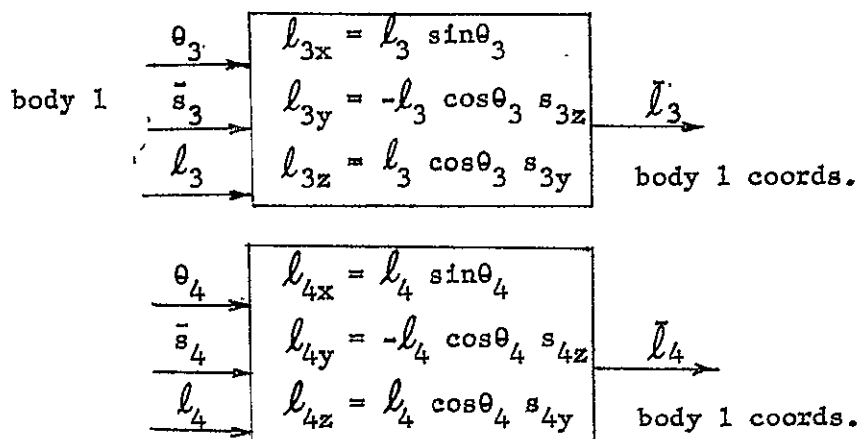
Purpose: To compute the positions of bodies 3 and 4.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|--|
| I | THETA3 | θ_3 | Angular position of pendulum 3 |
| I | S3(3) | \bar{s}_3 | Hinge line of pendulum 3 |
| I | PEND3L | l_3 | Scalar length of pendulum 3 |
| Ø | EL3(3) | \bar{l}_3 | Vector position of pendulum 3 from hinge line \bar{s}_3 |
| I | THETA4 | θ_4 | Angular position of pendulum 4 |
| I | S4(3) | \bar{s}_4 | Hinge line of pendulum 4 in body 1 coordinated (no dimensions) |
| I | PEND4L | l_4 | Scalar length of pendulum 4 |
| Ø | EL4(3) | \bar{l}_4 | Vector position of pendulum 4 |

Subroutines required: None

Equations programmed:



Discussion: None

Segment 4

Purpose: To compute the center of mass equations for bodies 0, 1, 2 and 3. \bar{r}_j is defined as the vector distance from the system center of mass to the center of mass of the jth body.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|----------------|---|
| I | EL2(3) | \bar{l}_2 | Vector position of the movable mass |
| I | EL3(3) | \bar{l}_3 | Vector position of body 3 from hinge line s_3 |
| I | EL4(3) | \bar{l}_4 | Vector position of body 4 from hinge line s_4 |
| I | D01(3) | \bar{d}_{01} | Vector distance from the c.m. of body 0 to the hinge line of body 1 |
| I | D13(3) | \bar{d}_{13} | Vector distance from the c.m. of body 1 to the hinge line of body 3 |
| I | D14(3) | \bar{d}_{14} | Vector distance from the c.m. of body 1 to the hinge line of body 4 |
| I | B0MASS | m_0 | Mass of body 0 (slugs) |
| I | B2MASS | m_2 | Mass of body 2 |
| I | B3MASS | m_3 | Mass of body 3 |
| I | B4MASS | m_4 | Mass of body 4 |
| I | TOTMAS | m | Mass of composite body |
| I | | A_1 | Coordinate transformation from body 0 to body 1 |

| | | | |
|-------------|-------|-------------|--|
| \emptyset | R1(3) | \vec{r}_1 | Vector distance from system c.m. to the c.m. of body 1 |
| \emptyset | R2(3) | \vec{r}_2 | Vector distance from the system c.m. to the c.m. of body 2 |
| \emptyset | R3(3) | \vec{r}_3 | Vector distance from the system c.m. to the c.m. of body 3 |
| \emptyset | R4(3) | \vec{r}_4 | Vector distance from the system c.m. to the c.m. of body 4 |

Subroutines required: None

Equations programmed:

$$\begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} = \frac{m_0}{m} A_1 \begin{bmatrix} d_{01x} \\ d_{01y} \\ d_{01z} \end{bmatrix} - \frac{m_2}{m} \begin{bmatrix} l_{2x} \\ l_{2y} \\ l_{2z} \end{bmatrix} - \frac{m_3}{m} \begin{bmatrix} d_{13x} + l_{3x} \\ d_{13y} + l_{3y} \\ d_{13z} + l_{3z} \end{bmatrix} - \frac{m_4}{m} \begin{bmatrix} d_{14x} + l_{4x} \\ d_{14y} + l_{4y} \\ d_{14z} + l_{4z} \end{bmatrix}$$

$$\begin{bmatrix} r_{2x} \\ r_{2y} \\ r_{2z} \end{bmatrix} = \begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} + \begin{bmatrix} l_{2x} \\ l_{2y} \\ l_{2z} \end{bmatrix}$$

$$\begin{bmatrix} r_{3x} \\ r_{3y} \\ r_{3z} \end{bmatrix} = \begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} + \begin{bmatrix} d_{13x} \\ d_{13y} \\ d_{13z} \end{bmatrix} + \begin{bmatrix} l_{3x} \\ l_{3y} \\ l_{3z} \end{bmatrix}$$

$$\begin{bmatrix} r_{4x} \\ r_{4y} \\ r_{4z} \end{bmatrix} = \begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} + \begin{bmatrix} d_{14x} \\ d_{14y} \\ d_{14z} \end{bmatrix} + \begin{bmatrix} l_{4x} \\ l_{4y} \\ l_{4z} \end{bmatrix}$$

l_2, l_3, l_4

$\bar{d}_{01}, \bar{d}_{13}, \bar{d}_{14}$

A_1

$\bar{r}_1, \bar{r}_2, \bar{r}_3, \bar{r}_4$

(body 1 coords.)

Discussion: None

Segment 5

Purpose: To compute the derivative of \vec{l}_2 , the rate at which to movable mass in moving.

Input/output:

| I/O | Fortran Statement | Math Symbol | Definition |
|-----|-------------------|-------------------|---|
| I | W1(3) | ω_1 | Angular velocity of body 1 |
| I | EL2(3) | \vec{l}_2 | Vector position of the movable mass |
| I | s2(3) | \vec{s}_2 | Unit vector defining the direction of travel of the movable mass (body 2) |
| I | S | s | Movable mass travel, a specified scalar function of time |
| I | SDOT | \dot{s} | The time derivative of s. |
| Ø | EL2DOT(3) | $\dot{\vec{l}}_2$ | The time derivative of \vec{l}_2 |

Subroutines required: SDCALC

Equations programmed:

$$\begin{array}{c}
 \vec{\omega}_1 \\
 \vec{l}_2 \\
 \vec{s}_2, \dot{s}
 \end{array}
 \rightarrow
 \left[\begin{array}{c}
 l_{2x} \\
 \dot{l}_{2y} \\
 l_{2z}
 \end{array} \right]
 =
 \text{CPM } \vec{\omega}_1
 \left[\begin{array}{c}
 l_{2x} \\
 l_{2y} \\
 l_{2z}
 \end{array} \right]
 +
 \left[\begin{array}{c}
 s_{2x} \dot{s} \\
 s_{2y} \dot{s} \\
 s_{2z} \dot{s}
 \end{array} \right]
 \rightarrow
 \dot{\vec{l}}_2$$

where

$$\text{CFM}\vec{\omega}_1 = \begin{bmatrix} 0 & -W1(3) & W1(2) \\ W1(3) & 0 & -W1(1) \\ -W1(2) & W1(1) & 0 \end{bmatrix}$$

Discussion: None

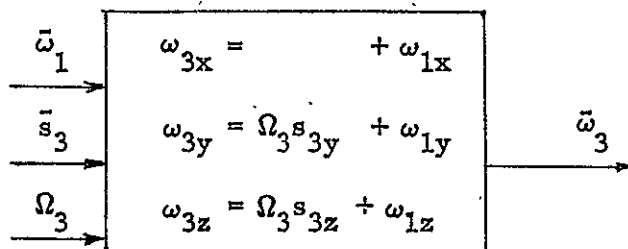
Segment 6

Purpose: To compute the angular velocity of body 3 ($\vec{\omega}_3$).

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|---|
| I | W1(3) | $\vec{\omega}_1$ | Angular velocity of body 1 |
| I | OMEGA3 | Ω_3 | Angular velocity of body 3 about the hinge line s_3 |
| I | s3(3) | \vec{s}_3 | The hinge line about which body 3 rotates |
| Ø | W3(3) | $\vec{\omega}_3$ | The angular velocity of body 3 |

Subroutines required: None

Equations programmed:



Discussion: None

Segment 7

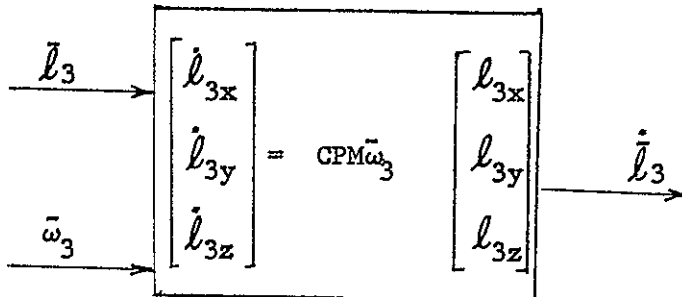
Purpose: To compute the derivative of \vec{l}_3 .

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------------|---|
| I | EL3(3) | \vec{l}_3 | Vector position of body 3 from hinge line \bar{s}_3 |
| I | W3(3) | $\bar{\omega}_3$ | Angular velocity of body 3 |
| Ø | EL3DOT(3) | $\dot{\vec{l}}_3$ | Time derivative of \vec{l}_3 |

Subroutines required: None

Equations programmed:



Discussion: None

Segment 8

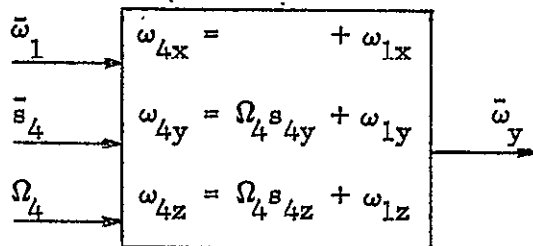
Purpose: To compute the angular velocity of body 4 $\vec{\omega}_4$.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|---|
| I | W1(3) | $\vec{\omega}_1$ | Angular velocity of body 1 |
| I | OMEGA4 | Ω_4 | Angular velocity of body 4 about the hinge line \vec{s}_4 |
| I | S4(3) | \vec{s}_4 | The hinge line about which body 4 rotates |
| Ø | W4(3) | $\vec{\omega}_4$ | Angular velocity of body 4 |

Subroutines required: None

Equations programmed:



Discussion: None

Segment 9

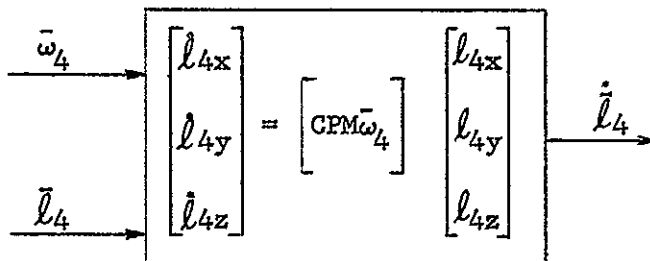
Purpose: To compute the derivative of \bar{l}_4 .

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------------|---|
| I | EL4(3) | \bar{l}_4 | Vector position of body 4 from the hinge line \bar{s}_4 |
| I | W4(3) | $\bar{\omega}_4$ | Angular velocity of body 4 |
| O | EL4DOT(3) | $\dot{\bar{l}}_4$ | Time derivative of \bar{l}_4 |

Subroutines required: None

Equations programmed:



Discussion: None

Segment 10

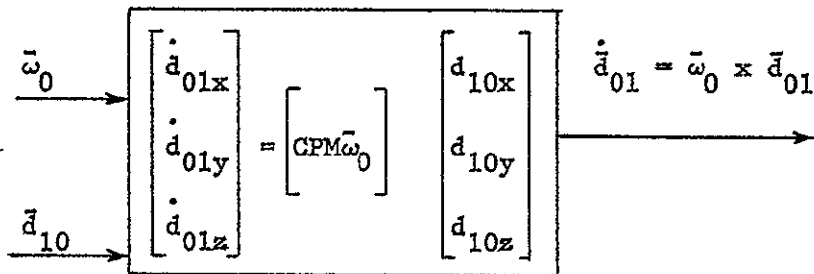
Purpose: To compute the time derivatives of \bar{d}_{01} , \bar{d}_{13} , and \bar{d}_{14} .

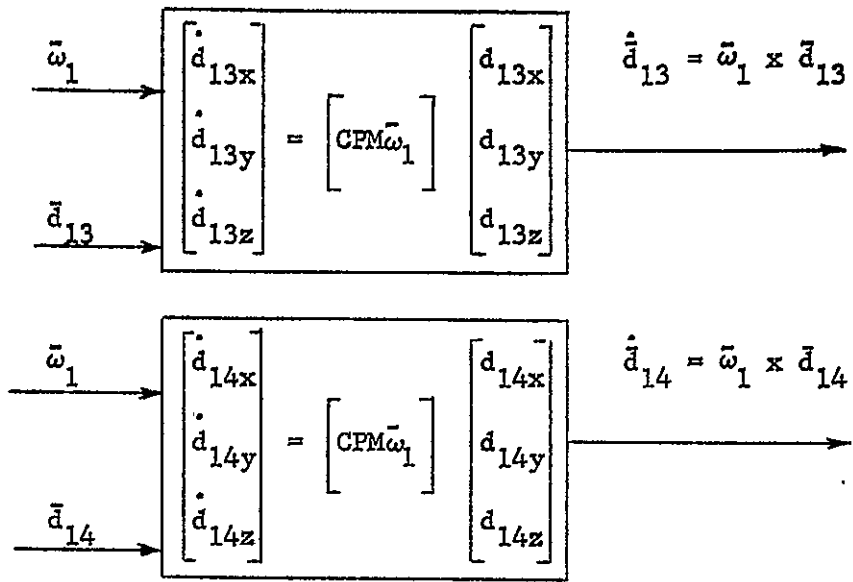
Input/output:

| I/O | Fortran Statement | Math Symbol | Definition |
|-----|-------------------|----------------------|---|
| I | D01(3) | \bar{d}_{01} | Vector distance from the c.m. of body 0 to the hinge line of body 1 |
| I | D13(3) | \bar{d}_{13} | Vector distance from the c.m. of body 1 to the hinge line of body 3 |
| I | D14(3) | \bar{d}_{14} | Vector distance from the c.m. of body 1 to the hinge line of body 4 |
| I | W1(3) | $\bar{\omega}_1$ | Angular velocity of body 1 |
| Ø | D01DOT(3) | $\dot{\bar{d}}_{01}$ | Time derivative of \bar{d}_{01} |
| Ø | D13DOT(3) | $\dot{\bar{d}}_{13}$ | Time derivative of \bar{d}_{13} |
| Ø | D14DOT(3) | $\dot{\bar{d}}_{14}$ | Time derivative of \bar{d}_{14} |

Subroutines required: None

Equations programmed:





Discussion: None

Segment 11

Purpose: To compute the time derivatives to the center of mass variables \bar{r}_1 , \bar{r}_2 , \bar{r}_3 and \bar{r}_4 .

Input/output:

| I/O | Fortran Statement | Math Symbol | Definition |
|-----|-------------------|----------------------|---|
| I | D01DOT(3) | $\dot{\bar{d}}_{01}$ | Time derivatives of \bar{d}_{01} |
| I | EL2DOT(3) | $\dot{\bar{l}}_2$ | Time derivative of \bar{l}_2 |
| I | D13DOT(3) | $\dot{\bar{d}}_{13}$ | Time derivative of \bar{d}_{13} |
| I | EL3DOT(3) | $\dot{\bar{l}}_3$ | Time derivative of \bar{l}_3 |
| I | D14DOT(3) | $\dot{\bar{d}}_{14}$ | Time derivative of \bar{d}_{14} |
| I | EL4DOT(3) | $\dot{\bar{l}}_4$ | Time derivative of \bar{l}_4 |
| I | R1DOT(3) | $\dot{\bar{r}}_1$ | Time derivative of \bar{r}_1 |
| I | B0MASS | m_0 | Mass of body 0 |
| I | B2MASS | m_2 | Mass of body 2 |
| I | B3MASS | m_3 | Mass of body 3 |
| I | B4MASS | m_4 | Mass of body 4 |
| I | TOTMAS | m | Mass of composite body (total mass) |
| I | | A_1 | Coordinate transformation from body 0 to body 1 |
| Ø | R1DOT(3) | $\dot{\bar{r}}_1$ | Time derivative of \bar{r}_1 |
| Ø | R2DOT(3) | $\dot{\bar{r}}_2$ | Time derivative of \bar{r}_2 |
| Ø | R3DOT(3) | $\dot{\bar{r}}_3$ | Time derivative of \bar{r}_3 |
| Ø | R4DOT(3) | $\dot{\bar{r}}_4$ | Time derivative of \bar{r}_4 |

Subroutines required: None

Equations programmed:

$$\begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} = \frac{m_0}{m} [A_1] \begin{bmatrix} \dot{d}_{01x} \\ \dot{d}_{01y} \\ \dot{d}_{01z} \end{bmatrix} - \frac{m_2}{m} \begin{bmatrix} \dot{l}_{2x} \\ \dot{l}_{2y} \\ \dot{l}_{2z} \end{bmatrix} - \frac{m_3}{m} \begin{bmatrix} \dot{d}_{13x} + \dot{l}_{3x} \\ \dot{d}_{13y} + \dot{l}_{3y} \\ \dot{d}_{13z} + \dot{l}_{3z} \end{bmatrix} - \frac{m_4}{m} \begin{bmatrix} \dot{d}_{14x} + \dot{l}_{4x} \\ \dot{d}_{14y} + \dot{l}_{4y} \\ \dot{d}_{14z} + \dot{l}_{4z} \end{bmatrix}$$

$$\begin{bmatrix} \dot{r}_{2x} \\ \dot{r}_{2y} \\ \dot{r}_{2z} \end{bmatrix} = \begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} + \begin{bmatrix} \dot{l}_{2x} \\ \dot{l}_{2y} \\ \dot{l}_{2z} \end{bmatrix}$$

$$\begin{bmatrix} \dot{r}_{3x} \\ \dot{r}_{3y} \\ \dot{r}_{3z} \end{bmatrix} = \begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} + \begin{bmatrix} \dot{d}_{13x} + \dot{l}_{3x} \\ \dot{d}_{13y} + \dot{l}_{3y} \\ \dot{d}_{13z} + \dot{l}_{3z} \end{bmatrix}$$

$$\begin{bmatrix} \dot{r}_{4x} \\ \dot{r}_{4y} \\ \dot{r}_{4z} \end{bmatrix} = \begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} + \begin{bmatrix} \dot{d}_{14x} + \dot{l}_{4x} \\ \dot{d}_{14y} + \dot{l}_{4y} \\ \dot{d}_{14z} + \dot{l}_{4z} \end{bmatrix}$$

\dot{d}_{01} (body 0 coordinates)

$\dot{d}_{10}, \dot{d}_{13}, \dot{d}_{14}, \dot{l}_2, \dot{l}_3, \dot{l}_4$ (body 1 coordinates)

A_1

$\dot{r}_1, \dot{r}_2, \dot{r}_3, \dot{r}_4$

(body 1 coords.)

Discussion: None

Segment 12

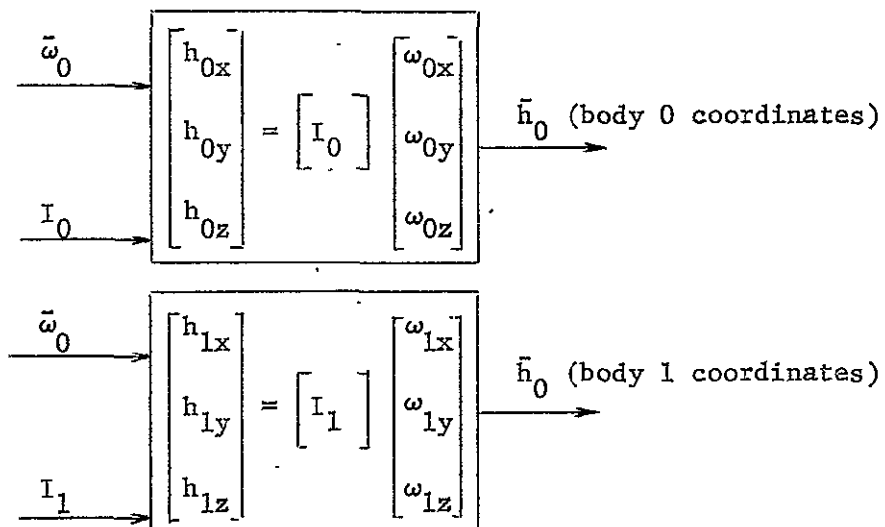
Purpose: To compute the angular momentum of body 0 and body 1.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|--------------------------------|
| I | W0 | $\bar{\omega}_0$ | Angular velocity of body 0 |
| I | W1 | $\bar{\omega}_1$ | Angular velocity of body 1 |
| I | BODY0I | I_0 | The inertia of body 0 |
| I | BODY1I | I_1 | The inertia of body 1 |
| O | H0 | \bar{h}_0 | The angular momentum of body 0 |
| O | H1 | \bar{h}_1 | The angular momentum of body 1 |

Subroutines required: MULT

Equations programmed:



Discussion: None

Segment 13

Purpose: To compute the primed angular momentum of bodies 1, 3 and 4.

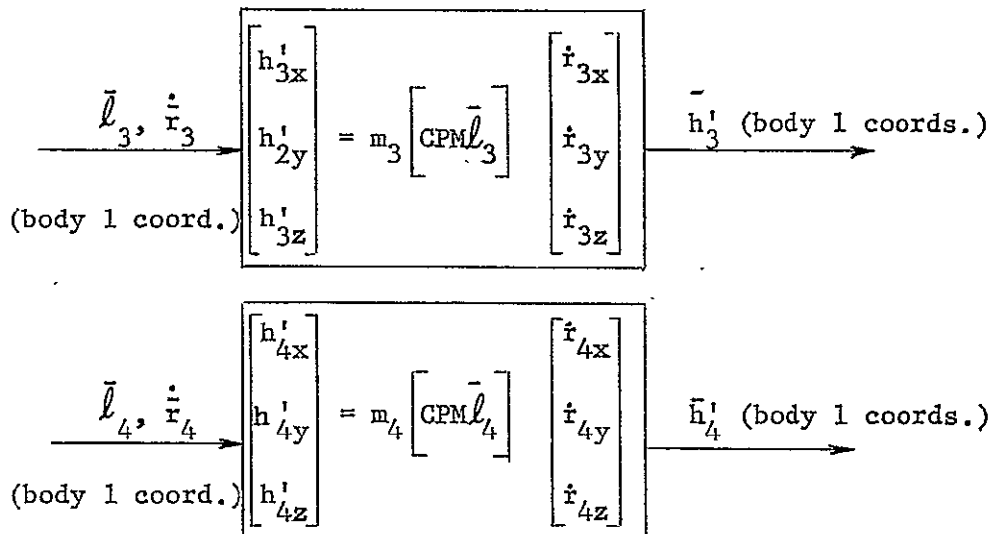
Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------------|---|
| I | B3MASS | m_3 | The mass of body 3 |
| I | EL3(3) | $\vec{\ell}_3$ | Vector position of body 3 from the hinge line \vec{s}_3 |
| I | R3DOT(3) | $\dot{\vec{r}}_3$ | The time derivative of \vec{r}_3 |
| O | H3PRIM(3) | \vec{h}'_3 | The primed angular momentum of body 3 |
| I | B4MASS | m_4 | The mass of body 4 |
| I | EL4(3) | $\vec{\ell}_4$ | Vector position of body 4 from the hinge line \vec{s}_4 |
| I | R4DOT(3) | $\dot{\vec{r}}_4$ | The time derivative of \vec{r}_4 |
| O | H4PRIM(3) | \vec{h}'_4 | The primed angular momentum of body 4 |
| I | H1(3) | \vec{h}_1 | The angular momentum of body 1 |
| I | H3PRIM(3) | \vec{h}'_3 | The primed angular momentum of body 3 |
| I | H4PRIM(3) | \vec{h}'_4 | The primed angular momentum of body 4 |
| I | B2MASS | m_2 | The mass of body 2 |
| I | EL2(3) | $\vec{\ell}_2$ | Vector position of the movable mass |
| I | R2DOT(3) | $\dot{\vec{r}}_2$ | The time derivative of \vec{r}_2 |
| I | B3MASS | m_3 | The mass of body 3 |

| | | | |
|---|-----------|-------------------|--|
| I | R3DOT(3) | $\dot{\bar{r}}_3$ | The time derivative of \bar{r}_3 |
| I | B4MASS | m_4 | The mass of body 4 |
| I | R4DOT(3) | $\dot{\bar{r}}_4$ | The time derivative of \bar{r}_4 |
| I | D13(3) | \bar{d}_{13} | Vector distance from the c.m. of body 1 to the hinge line of body 3 |
| I | D14(3) | \bar{d}_{14} | Vector distances from the c.m. of body 1 to the hinge line of body 4 |
| 0 | H1PRIM(3) | \bar{h}'_1 | The primed angular momentum of body 1 |

Subroutines required: None

Equations programmed:



$$\begin{bmatrix} h'_{1x} \\ h'_{1y} \\ h'_{1z} \end{bmatrix} = \begin{bmatrix} h_{1x} + h'_{3x} + h'_{4x} \\ h_{1y} + h'_{3y} + h'_{4y} \\ h_{1z} + h'_{3z} + h'_{4z} \end{bmatrix} - m_2 \begin{bmatrix} \text{CFM}(-\bar{l}_2) \end{bmatrix} \begin{bmatrix} \dot{r}_{2x} \\ \dot{r}_{2y} \\ \dot{r}_{2z} \end{bmatrix} - m_3 \begin{bmatrix} \text{CFM}(-\bar{l}_3) \end{bmatrix} \begin{bmatrix} \dot{r}_{3x} \\ \dot{r}_{3y} \\ \dot{r}_{3z} \end{bmatrix} - m_4 \begin{bmatrix} \text{CFM}(-\bar{d}_{14}) \end{bmatrix} \begin{bmatrix} \dot{r}_{4x} \\ \dot{r}_{4y} \\ \dot{r}_{4z} \end{bmatrix}$$

$\bar{h}_1, \bar{h}'_3, \bar{h}'_4, \bar{l}_2, \bar{l}_3, \dot{r}_2, \dot{r}_3, \dot{r}_4$
 (body 1 coords.)

\bar{h}'_1 (body 1 coords.)

Discussion: None

Segment 14

Purpose: To compute the angular momentum of the composite vehicle.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------------|---|
| I | H0(3) | \bar{h}_0 | The angular momentum of body 0 |
| I | H1PRIM(3) | h_1' | The primed angular momentum of body 1 |
| I | D01(3) | \bar{d}_{01} | Vector distance from the c.m. of body 0 to the hinge line of body 1 |
| I | | A_0 | Coordinate transformation from body 1 to body 0 |
| I | B1MASS | m_1 | Mass of body 1 |
| I | B2MASS | m_2 | Mass of body 2 |
| I | B3MASS | m_3 | Mass of body 3 |
| I | B4MASS | m_4 | Mass of body 4 |
| I | R1DOT(3) | $\dot{\bar{r}}_1$ | Time derivative of \bar{r}_1 |
| I | R2DOT(3) | $\dot{\bar{r}}_2$ | Time derivative of \bar{r}_2 |
| I | R3DOT(3) | $\dot{\bar{r}}_3$ | Time derivative of \bar{r}_3 |
| I | R4DOT(3) | $\dot{\bar{r}}_4$ | Time derivative of \bar{r}_4 |
| O | H(3) | \bar{H} | The angular momentum of the composite vehicle |

Subroutines required: None

Equations programmed:

$$\begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix} = \begin{bmatrix} h_{0x} \\ h_{0y} \\ h_{0z} \end{bmatrix} + [A_0] \begin{bmatrix} h_{1x}^i \\ h_{1y}^i \\ h_{1z}^i \end{bmatrix} + [GPM(\vec{d}_{01})] [A_0] \begin{bmatrix} m_1 \dot{r}_{1x} + m_2 \dot{r}_{2x} + m_3 \dot{r}_{3x} \\ m_1 \dot{r}_{1y} + m_2 \dot{r}_{2y} + m_3 \dot{r}_{3y} \\ m_1 \dot{r}_{1z} + m_2 \dot{r}_{2z} + m_3 \dot{r}_{3z} \end{bmatrix}$$

\vec{h}_0 (body 0 coords.)

$\vec{h}_1^i, \dot{\vec{r}}_1, \dot{\vec{r}}_2, \dot{\vec{r}}_3, \dot{\vec{r}}_4$ (body 1 coords.)

\vec{H} (body 0 coords.)

Discussion: None

Segment 15

Purpose: To compute in body 1 coordinates, the unit vector \bar{j} . This is done as a matter of computational convenience and is used in setting up the angular momentum derivatives.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|----------------|---|
| I | EL2(3) | \bar{l}_2 | Vector position of the movable mass |
| I | D13(3) | \bar{d}_{13} | Vector distance from the c.m. of body 1 to the hinge line of body 3 |
| I | EL3(3) | \bar{l}_3 | Vector position of body 3 |
| I | D14(3) | \bar{d}_{14} | Vector distance from the c.m. of body 1 to the hinge line of body 4 |
| I | EL4(3) | \bar{l}_4 | Vector position of body 4 |
| I | BMASS2 | m_2 | Mass of body 2 |
| I | BMASS3 | m_3 | Mass of body 3 |
| I | BMASS4 | m_4 | Mass of body 4 |
| 0 | AJ1(3) | \bar{j}_1 | Unit vector defined in body 1 |

Subroutines required: None

Equations programmed:

$$\begin{array}{l}
 \bar{l}_2, \bar{l}_3, \bar{l}_4 \\
 m_2, m_3, m_4 \\
 \bar{d}_{13}, \bar{d}_{14}
 \end{array}
 \rightarrow
 \begin{array}{c}
 \begin{bmatrix} j_{1x} \\ j_{1y} \\ j_{1z} \end{bmatrix}
 = m_2 \begin{bmatrix} l_{2x} \\ l_{2y} \\ l_{2z} \end{bmatrix}
 + m_3 \begin{bmatrix} d_{13x} + l_{3x} \\ d_{13y} + l_{3y} \\ d_{13z} + l_{3z} \end{bmatrix}
 + m_4 \begin{bmatrix} d_{14x} + l_{4x} \\ d_{14y} + l_{4y} \\ d_{14z} + l_{4z} \end{bmatrix}
 \end{array}
 \rightarrow \bar{j}_1 \text{ (body 1 coords.)}$$

Discussion: None

Segment 16

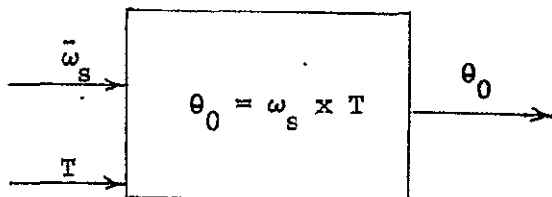
Purpose: To update the orbit angle θ_0 and to compute the external forces and moments.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|------------------------------|
| I | TIME | T | The time in seconds |
| I | Ws | ω_s | The orbital rate |
| O | THETO | θ_0 | The orbital angular position |
| O | TQ1G(3) | TQ_{1G} | The gravity gradient torques |
| O | TQ1P(3) | TQ_{1P} | The propulsion torques |

Subroutines required: GGRAD, PCON

Equations programmed:



Discussion: None

Segment 17

Purpose: To sum to forces and moments acting on bodies 0 and 1.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-------------|--|
| I | F01(3) | F_{01} | Force acting on body 0 due to gravity gradient |
| I | F11(3) | F_{11} | Force acting on body 1 due to gravity gradient |
| I | TQOG(3) | TQ_{OG} | The torque acting on body 0 due to gravity gradient |
| I | TQOP(3) | TQ_{OP} | The torque acting on body 0 due to propulsion forces |
| I | TQ1G(3) | TQ_{1G} | The torque acting on body 1 due to gravity gradient |
| I | TQ1P(3) | TQ_{1P} | The torque acting on body 1 due to propulsion forces |
| ∅ | TOEF(3) | T_{0eF} | The summation of the torques acting on body 0 |
| ∅ | T1EF(3) | T_{1eF} | The summation of the torques acting on body 1 |

Subroutines required: None

Equations programmed:

Segment 18

Purpose: To calculate the time derivatives of the angular momentum of the composite vehicle.

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|------------------|---|
| I | WO(3) | $\bar{\omega}_0$ | Angular velocity of body 0 |
| I | H(3) | \bar{H} | Angular momentum of the composite body |
| I | TOTMAS | m | Mass of the composite body |
| I | BOMASS | m_0 | Mass of body 0 |
| I | D01(3) | \bar{d}_{01} | Vector distance from the c.m. of body 0 to the hinge line of body 1 |
| I | AJ1(3) | \bar{j}_1 | A vector, defined in body 1 coordinates used only for computational convenience |
| I | F0(3) | \bar{F}_0 | Summation of the forces acting on body 0 |
| | | A_0 | Coordinate transformation from body 1 to body 0 |
| I | TOEF(3) | \bar{T}_{OEF} | Summation of the torques acting on body 0 |
| I | T1EF(3) | \bar{T}_{1EF} | Summation of the torques acting on body 1 |
| O | HDOT(3) | $\frac{dH}{dt}$ | The time derivative of H |

Subroutines required: None

Equations programmed:

$$\begin{aligned}
 & \begin{bmatrix} \frac{dH_x}{dt} \\ \frac{dH_y}{dt} \\ \frac{dH_z}{dt} \end{bmatrix} + \text{CPM}(\bar{\omega}_0) \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix} = \frac{1}{m} \text{CPM}\{(m_0 - m)\} \begin{bmatrix} \dot{d}_{01x} \\ \dot{d}_{01y} \\ \dot{d}_{01z} \end{bmatrix} - A_0 \begin{bmatrix} j_{1x} \\ j_{1y} \\ j_{1z} \end{bmatrix} \begin{bmatrix} F_{0x} \\ F_{0y} \\ F_{0z} \end{bmatrix} \\
 & + \frac{1}{m} A_0 \text{CPM}\{m_0\} \begin{bmatrix} A_1 \\ \begin{bmatrix} \dot{d}_{01x} \\ \dot{d}_{01y} \\ \dot{d}_{01z} \end{bmatrix} - \begin{bmatrix} j_{1x} \\ j_{1y} \\ j_{1z} \end{bmatrix} \end{bmatrix} \cdot \begin{bmatrix} F_{1x} \\ F_{1y} \\ F_{1z} \end{bmatrix} + \begin{bmatrix} T_{OEFx} \\ T_{OEFy} \\ T_{OEFz} \end{bmatrix} + A_0 \begin{bmatrix} T_{1EFx} \\ T_{1EFy} \\ T_{1EFz} \end{bmatrix}
 \end{aligned}$$

$\bar{\omega}_0, \bar{H}, \bar{F}_0, \bar{T}_{OEF}, \bar{d}_{01}$ (body 0 coords.)
 \bar{j}_1, F_1, T_{1EF} (body 1 coords.)
 A_1, A_0

$\frac{d\bar{H}}{dt}$ (body 0 coords.)

INTEGRATION SUBROUTINE

Discussion: The following vector equation is programmed in this segment:

$$\frac{d\bar{H}}{dt} + \bar{\omega}_0 \times \bar{H} = \left\{ -(m - m_0) \dot{\bar{d}}_{01} - \bar{j}_2 \right\} \times \frac{\bar{F}_0}{m} + \left\{ m_0 \dot{\bar{d}}_{01} - \bar{j}_1 \right\} \times \frac{\bar{F}_0}{m} + \bar{T}_{OEF} + \bar{T}_{1EF}$$

Segment 19

Purpose: To calculate the time derivative of \bar{h}'_1 about the unconstrained axis \bar{x}_1 .

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|-----------------------------|---|
| I | W1(3) | $\bar{\omega}_1$ | Angular velocity of body 1 |
| I | H1PRIM(3) | \bar{h}_1 | The primed angular momentum of body 1 |
| I | B2MASS | m_2 | Mass of body 2 |
| I | EL2DOT(3) | $\dot{\bar{l}}_2$ | Time derivative of \bar{l}_2 |
| I | R2DOT(3) | $\dot{\bar{r}}_2$ | Time derivative of \bar{r}_2 |
| I | B3MASS | m_3 | Mass of body 3 |
| I | D13DOT(3) | $\dot{\bar{d}}_{13}$ | Time derivative of \bar{d}_{13} |
| I | EL3DOT(3) | $\dot{\bar{l}}_3$ | Time derivative of \bar{l}_3 |
| I | R3DOT(3) | $\dot{\bar{r}}_3$ | Time derivative of \bar{r}_3 |
| I | B4MASS | m_4 | Mass of body 4 |
| I | D14DOT(3) | $\dot{\bar{d}}_{14}$ | Time derivative of \bar{d}_{14} |
| I | EL4DOT(3) | $\dot{\bar{l}}_4$ | Time derivative of \bar{l}_4 |
| I | R4DOT(3) | $\dot{\bar{r}}_4$ | Time derivative of \bar{r}_4 |
| I | AJ1(3) | \bar{j}_1 | A vector, defined in body 1 coordinates, used for computational convenience |
| I | T1EF(3) | \bar{T}_{1EF} | Summation of the torques acting on body 1 |
| I | T01 | $\bar{T}_{0 \rightarrow 1}$ | The torque acting between bodies 0 and 1 |
| O | H1PDOT(1) | $\dot{\bar{h}}'_{1x}$ | Time derivative of \bar{h}'_{1x} |

Subroutines required: TORK01

Equations programmed:

Unconstrained component along $\bar{x}_0 = \bar{x}_1$ (axis)

$$\begin{aligned} \frac{dh'_{1x}}{dt} + \omega_{1y} h'_{1z} - \omega_{1z} h'_{1y} = & \dot{r}_{1y} (-m_2 \dot{l}_{2z} - m_3 (\dot{d}_{13z} + \dot{l}_{3z}) - m_4 (\dot{d}_{14z} + \dot{l}_{4z})) \\ & - \dot{r}_{1z} (-m_2 \dot{l}_{2y} - m_3 (\dot{d}_{13y} + \dot{l}_{3y}) - m_4 (\dot{d}_{14y} + \dot{l}_{4y})) \\ & + j_{1y} \left(\frac{F_{0y}}{m} \sin\theta_1 - \frac{F_{0z}}{m} \cos\theta_1 \right) + j_{1z} \left(\frac{F_{0y}}{m} \cos\theta_1 + \frac{F_{0z}}{m} \sin\theta_1 \right) \\ & + j_{1z} \frac{F_{1y}}{m} - j_{1y} \frac{F_{1z}}{m} + T_{1EFx} + T_{(0 \rightarrow 1)x} \end{aligned}$$

$\bar{h}'_1, \bar{\omega}_1, \dot{\bar{r}}_1, \dot{\bar{r}}_2, \dot{\bar{r}}_3, \dot{\bar{r}}_4, \dot{\bar{l}}_2, \dot{\bar{l}}_3, \dot{\bar{l}}_4, \bar{j}_1, \bar{F}_1, \bar{T}_{1EF}, \bar{T}_{(0 \rightarrow 1)x}$
(body 1 coords.)

\bar{F}_0 (body 0 coords.)

h'_{1x} - (body 1 coords.)

Discussion: None

Segment 20

Purpose: To calculate the time derivatives of the primed angular momenta about the unconstrained axes \bar{s}_3 and \bar{s}_4 .

Input/output:

| I/O | Fortran Name | Math Symbol | Definition |
|-----|--------------|---|--|
| I | H3PRIM(3) | \bar{h}'_3 | The primed angular momentum of body 3 |
| I | S3(3) | \bar{s}_3 | The hinge line of body 3 |
| I | W1(3) | $\bar{\omega}_1$ | The angular velocity of body 1 |
| I | B3MASS | m_3 | Mass of body 3 |
| I | EL3DOT(3) | $\dot{\bar{l}}_3$ | Time derivative of \bar{l}_3 |
| I | R3DOT(3) | $\dot{\bar{r}}_3$ | Time derivative of \bar{r}_3 |
| I | EL3(3) | \bar{l}_3 | Vector position of body 3 from the hinge line \bar{s}_3 |
| I | B4MASS | m_4 | Mass of body 4 |
| I | TOTMAS | m | Mass of composite vehicle |
| I | F0(3) | \bar{F}_0 | Summation of the forces acting on body 0 |
| I | F1(3) | \bar{F}_1 | Summation of the forces acting on body 1 |
| I | T13 | $\bar{T}_{1 \rightarrow 3}$ | Torque acting between bodies 1 and 3 |
| ∅ | G3DOT | $\frac{d}{dt} (\bar{h}'_3 \cdot \bar{s}_3)$ | Time derivative of the unconstrained component of \bar{h}'_3 |
| I | H4PRIM(3) | \bar{h}'_4 | The primed angular momentum of body 4 |

| | | | |
|---|-----------|--|---|
| I | S4(3) | \bar{s}_4 | The hinge line of body 4 |
| I | EL4DOT(3) | $\dot{\bar{l}}_4$ | Time derivative of \bar{l}_4 |
| I | R4DOT(3) | $\dot{\bar{r}}_4$ | Time derivative of \bar{r}_4 |
| I | EL4(3) | \bar{l}_4 | Vector position of body 4 from the hinge line \bar{s}_4 |
| I | T14 | $\bar{T}_{1 \rightarrow 4}$ | Torque acting between bodies 1 and 4 |
| O | G4DOT | $\frac{d}{dt} (\bar{h}_4^i \cdot \bar{s}_4)$ | Time derivative of the unconstrained component of \bar{h}_4^i |

Subroutines required: TORK13, TORK14

Equations programmed:

$$\begin{aligned}
 & \frac{d}{dt} (\bar{h}'_3 \cdot \bar{s}_3) + s_{3y} (\omega_{1z} h'_{3x} - \omega_{1x} h'_{3z}) + s_{3z} (\omega_{1x} h'_{3y} - \omega_{1y} h'_{3x}) = \\
 & m_3 s_{3y} (\dot{l}_{3z} \dot{r}_{3x} - \dot{l}_{3x} \dot{r}_{3z}) + m_3 s_{3z} (\dot{l}_{3x} \dot{r}_{3y} - \dot{l}_{3y} \dot{r}_{3x}) \\
 & + \frac{m_3}{m} s_{3y} l_{3z} (F_{0x} + F_{1x}) - l_{3x} (-F_{0y} \sin \theta_1 + F_{0z} \cos \theta_1 + F_{1z}) \\
 & + \frac{m_3}{m} s_{3z} l_{3z} (F_{0y} \cos \theta_1 + F_{0z} \sin \theta_1 + F_{1y}) - l_{3y} (F_{0x} + F_{1x}) \\
 \\
 & \frac{d(\bar{h}'_4 \cdot \bar{s}_4)}{dt} + s_{4y} (\omega_{1z} h'_{4x} - \omega_{1x} h'_{4z}) + s_{4z} (\omega_{1x} h'_{4y} - \omega_{1y} h'_{4x}) \\
 & = m_4 s_{4y} (\dot{l}_{4z} \dot{r}_{4x} - \dot{l}_{4x} \dot{r}_{4z}) + m_4 s_{4z} (\dot{l}_{4x} \dot{r}_{4y} - \dot{l}_{4y} \dot{r}_{4x}) \\
 & + \frac{m_4}{m} s_{4y} l_{4z} (F_{0x} + F_{1x}) - l_{4x} (-F_{0y} \sin \theta_1 + F_{0z} \cos \theta_1 + F_{1z}) \\
 & + \frac{m_4}{m} s_{4z} l_{4x} (F_{0y} \cos \theta_1 + F_{0z} \sin \theta_1 + F_{1y}) - l_{4y} (F_{0x} + F_{1x}) + T_{1 \rightarrow 4}
 \end{aligned}$$

$\bar{\omega}_1, \bar{h}'_3, \bar{h}'_4, \bar{l}_3, \bar{l}_4, \dot{\bar{l}}_3, \dot{\bar{l}}_4$
 $\dot{\bar{r}}_3, \dot{\bar{r}}_4, \bar{F}_1, \bar{T}_{1 \rightarrow 3}, \bar{T}_{1 \rightarrow 4}$
 (body 1 coords.)

\bar{F}_0 (body 0 coords.)

$$\frac{d}{dt} (\bar{h}'_3 \cdot \bar{s}_3) = \frac{d}{dt} (h'_{3y} s_{3y} + h'_{3z} s_{3z})$$

$$\frac{d}{dt} (\bar{h}'_4 \cdot \bar{s}_4) = \frac{d}{dt} (h'_{4y} s_{4y} + h'_{4z} s_{4z})$$

(body 1 coords.)

Discussion: None