

X-547-65-222

NASA TMX-55271

FACILITY FORM 602

165-29805

(ACCESSION NUMBER)

114

(PAGES)

(NASA OR OR TMX OR AD NUMBER)

(THRU)

1

(CODE)

08

(CATEGORY)

A MUTUAL VISIBILITY COMPUTER PROGRAM FOR COMMUNICATION SATELLITES

GPO PRICE \$ _____

CFSTI PRICE(S) \$ _____

Hard copy (HC) 4.00

Microfiche (MF) .75

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ff 653 July 65

MAY 1965



GODDARD SPACE FLIGHT CENTER
GREENBELT, MARYLAND

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COMMUNICATION SATELLITES

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G. D. Repass and R. G. Chaplick

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INTRODUCTION

As more and more ground stations are constructed around the world to operate with communication satellites, the problems of scheduling the experiments become more complex. Many factors, e.g., is the attitude of the satellite correct, must be considered simultaneously in order for decisions to be made. Although many pieces of data were on hand during tests with Telstar I and Relay I, the information was presented randomly in three or more books, and much human effort was needed to extract and analyze the pertinent data. The obvious solution was to compute only the necessary data and to present them as concisely as possible. This report will describe such a program which has been developed by members of the Theory and Analysis Office.

PROGRAM CRITERIA

The following criteria were used to design the program:

(a) Data should be printed only for passes during which the spacecraft was visible to a "control" station. Because the Relay spacecraft can be operated by only two or three stations, it must be visible to one of those stations when experiments are made.

(b) Data should be presented in two books, one graphs of mutual visibility and the other the actual numerical data.

MUTUAL VISIBILITY

Bar graphs appeared to be the most legible form for presentation of time intervals of mutual visibility. In addition, indications of elevation angles from 0° to 5° , from 5° to 10° , and from 10° to 90° ; of ranges higher or lower than a prescribed input value; of spacecraft look angle; and of orbit number were necessary.

NUMERICAL DATA

This volume consists of all the numerical data used to produce the mutual visibility graphs. These data are spacecraft longitude, latitude, height and sun-light indicator; and for each station the spacecraft look angle (the angle between the spin axis and the slant range), azimuth, elevation, and slant range. The last set of data in this book is a complete time history of entry into and exit from the earth's shadow.

THEORY

The program can be described simply as an orbit generator with associated subroutines necessary to perform needed calculations. Experience at Goddard has indicated that the theory developed by Brouwer (1959) is adaptable for the purposes of this program. The American Institute of Physics has granted permission to the authors to reproduce certain pages of Brouwer (1959) herein. Appendix I consists of pages 393 to 396. To aid the reader the pertinent equations have been rewritten and the equivalent Fortran II variable names for some of the terms have been superimposed on the equations. These equations are reproduced in Appendix II.

A brief explanation of how the orbit generator has been programmed will help the reader.

Secular terms. These equations were rewritten as:

$$l'' = l_0'' + S_1 t + S_{1,2} t^2$$

$$g'' = g_0'' + S_2 t$$

$$h'' = h_0'' + S_3 t$$

where S_1 , S_2 , S_3 are constant for any given set of a_0'' , e_0'' , I_0'' , and earth constants and $S_{1,2}$ is the anomalistic acceleration computed by the GSFC differential correction programs. If $S_{1,2}$ is unavailable, the added term can be dropped by inputting it as zero.

Long Period terms. These equations were rewritten as:

$$\ell' = \ell'' + L_1 \sin 2g'' + L_2 \cos g'' + L_3 \cos 3g''$$

$$g' = g'' + L_4 \sin 2g'' + L_5 \cos g'' + L_6 \cos 3g''$$

$$h' = h'' + L_7 \sin 2g'' + L_8 \cos g'' + L_9 \cos 3g''$$

$$\delta_1 e = L_{10} \cos 2g'' + L_{11} \sin g'' + L_{12} \sin 3g''$$

$$\delta_1 I = L_{13} \delta_1 e$$

where L_i , $1 \leq i \leq 13$ are constant for any given set of a_0'' , e_0'' , I_0'' , and earth constants.

EARTH'S GRAVITATIONAL POTENTIAL

The force function used is that of Brouwer, page 393, where k_2 , k_3 , k_4 , k_5 represent the zonal harmonics. However, Vinti's notation of J_n should be adopted. Either set of harmonics can be used by means of the following equations:

$$k_2 = + \frac{1}{2} J_2 R_e^2$$

$$k_3 = - J_3 R_e^3$$

$$k_4 = - \frac{3}{8} J_4 R_e^4$$

$$k_5 = - J_5 R_e^5$$

The program has been designed either to use constants stored in memory or to read new constants along with other input data.

COMPUTER PROGRAM

The computer program, written in Fortran II for the IBM 7094, was designed typically is a main program with subroutines called when needed. The orbit generator has been designed to compute in one subroutine all quantities which are functions of mean elements and earth constants. Another subroutine computes only those quantities which are either explicit or implicit functions of time. Terms that occur at least twice in the equations are assigned a variable name and actually are computed only once.

Main Program. The requirement that data be printed only for passes when the spacecraft is visible at a control station implies, unfortunately, that data must be computed and stored before a decision can be made to discard the data. The authors recognize that "shortcuts" were available to avoid computing data which were to be thrown away. However, the requirement for an accurate eclipse history did not allow such methods to be used.

Main Program One. This program fulfills the requirements described previously herein. Its characteristics are (a) an IBM 7094 with a 65K memory is required and (b) the complete sunlight history is computed. Computer running time could be reduced if (a) and (b) can be eliminated.

Main Program Two. This program is similar to Main Program One except that the control station requirements, the complete sunlight history, and the numerical data on bar graphs were deleted. A computer with at least a 20K memory (dependent on memory needed for library subroutines) is required.

Subroutines. The subroutines for each of the main programs are identical.

Operation Instructions. Instructions for operating the two programs are given in Appendix III.

Input deck instructions. Instructions for punching the input deck for each program are given in Appendix III.

Flow Charts. The flow chart for Main Program Two is contained in Appendix IV.

Source Decks. Source decks for Main Program One, Main Program Two, and Subroutines are reproduced in Appendices V, VI, and VII respectively.

Sample Problems. Inputs to and outputs of each program are given in Appendix VIII. The outputs have been abbreviated.

Results

Main Program One has been used extensively and successfully for planning experiments with Relay I and II and Echo I and II. Main program Two, which is less sophisticated and is easy to change, has been used for a variety of special studies, e.g., travel time of light from station to spacecraft back to station; angles between slant ranges from a single station to two different spacecraft, etc.

REFERENCE

1. "Solution of the Problem of Artificial Satellite Theory without Drag," D. Brouwer, *Astronomical Journal* 64, 9, Nov. 1959, pp. 393-396.

APPENDIX I

Reproduction of Pages 393 to 396 of Brouwer (1959)

Formulas for Computation. For convenience of computation the perturbations in the Keplerian elements a , e , I are given instead of those in L , G , H .

The adopted force function is

$$\begin{aligned}
 U = & \frac{\mu}{r} + \frac{\mu k_2}{r^2} (1 - 3 \sin^2 \beta) + \frac{\mu k_4}{r^6} \left(1 - 10 \sin^2 \beta + \frac{35}{3} \sin^4 \beta \right) \\
 & + \frac{\mu A_{3,0}}{r^4} \left(-\frac{3}{2} \sin \beta + \frac{5}{2} \sin^3 \beta \right) + \frac{\mu A_{5,0}}{r^6} \left(\frac{15}{8} \sin \beta - \frac{35}{4} \sin^3 \beta + \frac{63}{8} \sin^5 \beta \right),
 \end{aligned}$$

in which k_2 is a small quantity, and k_4 , $A_{3,0}$, $A_{5,0}$ are assumed to be of order k_2^2 .

The secular motions have been computed to $O(k_2^2)$, the coefficients of periodic terms to $O(k_2)$.

Basic constants:

a'' = semi-major axis constant

e'' = eccentricity constant

I'' = inclination constant

$n_0 = \mu^{1/2} a''^{-3/2} = 17.04337 (a''/R)^{-3/2}$ rev./day

R = equatorial radius

Abbreviations:

$$\eta = (1 - e'^2)^{1/2} \quad \theta = \cos I''$$

$$\gamma_2 = \frac{k_2}{a'^{1/2}} \quad \gamma_4 = \frac{k_4}{a'^{3/4}} \quad \gamma_3 = \frac{A_{3,0}}{a'^{3/8}} \quad \gamma_5 = \frac{A_{5,0}}{a'^{5/8}}$$

$$\gamma_2' = \gamma_2 \eta^{-4} \quad \gamma_4' = \gamma_4 \eta^{-8} \quad \gamma_3' = \gamma_3 \eta^{-6} \quad \gamma_5' = \gamma_5 \eta^{-10}$$

It is customary to use for the second harmonic the coefficient J; Jeffreys (1954) used for the fourth harmonic the coefficient D. The relations between J, D and γ_2, γ_4 are

$$\gamma_2 = \frac{1}{3} J \left(\frac{R}{a''} \right)^2, \quad \gamma_4 = \frac{3}{35} D \left(\frac{R}{a''} \right)^4.$$

Strictly speaking, $e'' + \delta_1 e$, $\theta' = \cos(I'' + \delta_1 I)$, $\eta' = [1 - (e'' + \delta_1 e)^2]^{1/2}$ should be used in the computation of the periodic terms, but since the short-period terms are obtained to $O(k_2)$, it is of no consequence if contributions of $O(k_2)$ are omitted in expressions that have γ_2 as a factor. Similarly, ℓ'' , g'' might be used in computing f' , r' ; but since ℓ' , γ' are available, their use does not complicate the calculation.

The formulas are applicable for any eccentricity $e < 1$ and any inclination with the exception of inclinations near the critical inclination, for which $1 - 5 \cos^2 I$ appears as a small divisor.

The appearance of e'' as a divisor in the short-period terms in e is apparent only. The expressions that are multiplied by e''^{-1} contain e'' as a factor, either implicitly or explicitly.

In the short-period terms in ℓ and g a divisor e'' occurs also, but for the calculation of the position only $g + \ell$ + equation of the center is needed. In $g + \ell$ the divisor e'' is not present.

Singularities in some of the elements also occur for very small inclinations; again, no singularity is present in the coordinates. In such cases it may be found convenient to modify the formulas and obtain expressions for the perturbations in coordinates.

Secular terms:

l'' = "mean" mean anomaly

$$= n_0 t \left\{ 1 + \frac{3}{2} \gamma_2' \eta (-1 + 3\theta^2) + \frac{3}{32} \gamma_2'^2 \eta [-15 + 16\eta + 25\eta^2 + (30 - 96\eta - 90\eta^2)\theta^2] \right. \\ \left. + (105 + 144\eta + 25\eta^2)\theta^4 \right\} + \frac{15}{16} \gamma_4' \eta e''^2 [3 - 30\theta^2 + 35\theta^4] + l_0''$$

g'' = mean argument of perigee

$$= n_0 t \left\{ \frac{3}{2} \gamma_2' (-1 + 5\theta^2) + \frac{3}{32} \gamma_2'^2 [-35 + 24\eta + 25\eta^2 + (90 - 192\eta - 126\eta^2)\theta^2] \right. \\ \left. + (385 + 360\eta + 45\eta^2)\theta^4 \right\} + \frac{5}{16} \gamma_4' [21 - 9\eta^2 + (-270 + 126\eta^2)\theta^2 + (385 - 189\eta^2)\theta^4] + g_0''$$

h'' = mean longitude of ascending node

$$= n_0 t \left\{ -3\gamma_2' \theta + \frac{3}{8} \gamma_2'^2 [(-5 + 12\eta + 9\eta^2)\theta + (-35 - 36\eta - 5\eta^2)\theta^2] \right. \\ \left. + \frac{5}{4} \gamma_4' (5 - 3\eta^2)\theta(3 - 7\theta^2) \right\} + h_0''$$

Long-period terms:

$$\begin{aligned} \delta_{1e} = & \left\{ \frac{1}{8} \gamma_2' e'' \eta^3 [I - 11\theta^2 - 40\theta^4 (I - 5\theta^2)^{-1}] - \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} e'' \eta^3 [I - 3\theta^2 - 8\theta^4 (I - 5\theta^2)^{-1}] \right\} \cos 2g'' \\ & + \left\{ \frac{1}{4} \frac{\gamma_3'}{\gamma_2'} \eta^3 \sin I'' + \frac{5}{64} \frac{\gamma_6'}{\gamma_2' \eta^2} \sin I'' (4 + 3e''^2) [I - 9\theta^2 - 24\theta^4 (I - 5\theta^2)^{-1}] \right\} \sin g'' \\ & - \frac{35}{384} \frac{\gamma_6'}{\gamma_2'} e''^2 \eta^3 \sin I'' [I - 5\theta^2 - 16\theta^4 (I - 5\theta^2)^{-1}] \sin 3g'' \end{aligned}$$

$$\delta_{1I} = - \frac{e'' \delta_{1e}}{\eta^2 \tan I''}$$

$$\begin{aligned} I' = I'' + & \left\{ \frac{1}{8} \gamma_2' \eta^3 [I - 11\theta^2 - 40\theta^4 (I - 5\theta^2)^{-1}] - \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} \eta^3 [I - 3\theta^2 - 8\theta^4 (I - 5\theta^2)^{-1}] \right\} \sin 2g'' \\ & + \left\{ - \frac{1}{4} \frac{\gamma_3'}{\gamma_2'} \frac{\eta^3}{e''} \sin I'' - \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \frac{\eta^3}{e''} \sin I'' (4 + 9e''^2) [I - 9\theta^2 - 24\theta^4 (I - 5\theta^2)^{-1}] \right\} \cos g'' \\ & + \frac{35}{384} \frac{\gamma_6'}{\gamma_2'} \eta^3 e'' \sin I'' [I - 5\theta^2 - 16\theta^4 (I - 5\theta^2)^{-1}] \cos 3g'' \end{aligned}$$

$$\begin{aligned} g' = g'' + & \left\{ - \frac{1}{16} \gamma_2' [(2 + e''^2) - 11(2 + 3e''^2)\theta^2 - 40(2 + 5e''^2)\theta^4 (I - 5\theta^2)^{-1}] \right. \\ & - 400e''^2 \theta^6 (I - 5\theta^2)^{-2}] + \frac{5}{24} \frac{\gamma_4'}{\gamma_2'} [2 + e''^2 - 3(2 + 3e''^2)\theta^2 - 8(2 + 5e''^2)\theta^4 (I - 5\theta^2)^{-1}] \\ & \left. - 80e''^2 \theta^6 (I - 5\theta^2)^{-2}] \right\} \sin 2g'' + \left\{ \frac{1}{4} \frac{\gamma_3'}{\gamma_2'} \left(\frac{\sin I''}{e''} - \frac{e'' \theta^2}{\sin I''} \right) + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \right. \\ & \times \left[\left(\frac{\eta^2 \sin I''}{e''} - \frac{e'' \theta^2}{\sin I''} \right) (4 + 3e''^2) + e'' \sin I'' (26 + 9e''^2) \right] [I - 9\theta^2 - 24\theta^4 (I - 5\theta^2)^{-1}] \\ & - \frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e'' \theta^2 \sin I'' (4 + 3e''^2) [3 + 16\theta^2 (I - 5\theta^2)^{-1} + 40\theta^4 (I - 5\theta^2)^{-2}] \left. \right\} \cos g'' \\ & + \left\{ - \frac{35}{1152} \frac{\gamma_6'}{\gamma_2'} \left[e'' \sin I'' (3 + 2e''^2) - \frac{e''^2 \theta^2}{\sin I''} \right] [I - 5\theta^2 - 16\theta^4 (I - 5\theta^2)^{-1}] \right. \\ & \left. + \frac{35}{576} \frac{\gamma_6'}{\gamma_2'} e''^2 \theta^2 \sin I'' [5 + 32\theta^2 (I - 5\theta^2)^{-1} + 80\theta^4 (I - 5\theta^2)^{-2}] \right\} \cos 3g'' \end{aligned}$$

$$\begin{aligned}
h' = h'' + & \left\{ -\frac{1}{8} \gamma_2 e'' \theta [11 + 80\theta^2(1 - 5\theta^2)^{-1} + 200\theta^4(1 - 5\theta^2)^{-2}] \right. \\
& + \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} e'' \theta [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \left. \right\} \sin 2g'' \\
& + \left\{ \frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \frac{e'' \theta}{\sin I''} + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \frac{e'' \theta}{\sin I''} (4 + 3e''^2) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \right. \\
& + \left. \frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e'' \theta \sin I'' (4 + 3e''^2) [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos g'' \\
& + \left\{ -\frac{35}{1152} \frac{\gamma_6'}{\gamma_2'} \frac{e'' \theta}{\sin I''} [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] \right. \\
& \quad \left. - \frac{35}{576} \frac{\gamma_2'}{\gamma_2'} e'' \theta \sin I'' [5 + 32\theta^2(1 - 5\theta^2)^{-1} + 80\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos 3g''
\end{aligned}$$

Short-period terms included:

$$\begin{aligned}
a &= a'' \left\{ 1 + \gamma_2 \left[(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} - \eta^{-3} \right) + 3(1 - \theta^2) \frac{a''^2}{r'} \cos (2g' + 2f') \right] \right\} \\
e &= e'' + \delta_1 e + \frac{\eta^2}{2e''} \left\{ \gamma_2 \left[(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} - \eta^{-3} \right) + 3(1 - \theta^2) \left(\frac{a''^2}{r'^2} - \eta^{-4} \right) \cos (2g' + 2f') \right] \right. \\
& \quad \left. - \gamma_2' (1 - \theta^2) [3e'' \cos (2g' + f') + e'' \cos (2g' + 3f')] \right\} \\
I &= I'' + \delta_1 I + \frac{1}{2} \gamma_2' \theta (1 - \theta^2)^2 [3 \cos (2g' + 2f') + 3e'' \cos (2g' + f') + e'' \cos (2g' + 3f')] \\
l &= l' - \frac{\eta^2}{4e''} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' \right. \\
& \quad \left. + 3(1 - \theta^2) \left[\left(-\frac{a''^2}{r'^2} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
g &= g' + \frac{\eta^2}{4e''} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' \right. \\
& \quad \left. + 3(1 - \theta^2) \left[\left(-\frac{a''^2}{r'^2} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
& \quad + \frac{1}{2} \gamma_2' \{ 6(-1 + 5\theta^2)(f' - l' + e'' \sin f') \\
& \quad \quad + (3 - 5\theta^2)[3 \sin (2g' + 2f') + 3e'' \sin (2g' + f') + e'' \sin (2g' + 3f')] \} \\
h &= h' - \frac{1}{2} \gamma_2' \theta [6(f' - l' + e'' \sin f') - 3 \sin (2g' + 2f') \\
& \quad \quad - 3e'' \sin (2g' + f') - e'' \sin (2g' + 3f')].
\end{aligned}$$

f', r' are to be computed from

$$\begin{aligned}
E' - e'' \sin E' &= l' \\
\tan \frac{1}{2} f' &= \left(\frac{1 + e''}{1 - e''} \right)^{\frac{1}{2}} \tan \frac{1}{2} E' & \frac{r'}{a''} \sin f' &= (1 - e''^2)^{\frac{1}{2}} \sin E' \\
\frac{a''}{r'} &= \frac{1 + e'' \cos f'}{1 - e''^2} & \text{or} & \frac{r'}{a''} \cos f' &= \cos E' - e'' \\
& & & \frac{r'}{a''} &= 1 - e'' \cos E'
\end{aligned}$$

For the calculation of the coordinates at any time the complete values of e and l should be used for the solution of Kepler's equation,

$$E - e \sin E = l$$

and subsequently r and f , which may then be used in the formulas:

$$x = r[\cos(g + f) \cos h - \sin(g + f) \sin h \cos I]$$

$$y = r[\cos(g + f) \sin h + \sin(g + f) \cos h \cos I]$$

$$z = r \sin(g + f) \sin I$$

A convenient alternative form is:

$$x = A_x (\cos E - e) + B_x \sin E$$

$$y = A_y (\cos E - e) + B_y \sin E$$

$$z = A_z (\cos E - e) + B_z \sin E$$

$$A_x = a [\cos g \cos h - \sin g \sin h \cos I]$$

$$B_x = -a(1 - e^2)^{\frac{1}{2}} [\sin g \cos h$$

$$+ \cos g \sin h \cos I]$$

$$A_y = a [\sin g \cos h \cos I + \cos g \sin h]$$

$$B_y = a(1 - e^2)^{\frac{1}{2}} [\cos g \cos h \cos I - \sin g \sin h]$$

$$A_z = a \sin g \sin I$$

$$B_z = a(1 - e^2)^{\frac{1}{2}} \cos g \sin I$$

Noted added in proof. The lack of uniformity in notation of the coefficients of the second and fourth harmonics of the earth's potential in papers dealing with the motion of artificial satellites calls for a comment on this subject.

The table below contains a listing of some of the designations used and their relations to the coefficients B_p in the expression of the force function of a body with rotational symmetry,

$$F = \frac{\mu}{r} \left[1 + \sum_{p=2}^{\infty} \frac{B_p P_p(\sin \beta)}{r^p} \right],$$

in which B_p are Legendre polynomials and $\mu = GM$. The expression is an adaptation of the Laplacian expression given by Tisserand.

In addition to the equivalents of B_2 and B_4 the table gives those of the ratio B_4/B_2^2 , which is unity for the special case treated by Vinti (1959), in which the terms with small divisors near the critical inclination vanish. No effort has been made to make the tabulation complete.

Laplace	B_2	B_4	B_4/B_2^2	Tisserand, <i>Méc. Céleste</i> 11, 320, 1890
H. Struve	$-\frac{2}{3}k$	$\frac{2}{3}l$	$\frac{3}{2}l/k^2$	<i>Suppl. I, Obs. Pulkovo</i> 1888
W. de Sitter	$-\frac{2}{3}JK^2$	$\frac{4}{15}KR^2$	$\frac{3}{5}K/J^2$	<i>B. A. N.</i> 2, 97, 1924
D. Brouwer	$-2k_2$	$\frac{8}{3}k_4$	$\frac{2}{3}k_4/k_2^2$	<i>J. J.</i> 51, 223, 1946
H. Jeffreys	$-\frac{2}{3}JK^2$	$\frac{8}{35}DK^2$	$\frac{18}{35}D/J^2$	<i>M. N.</i> 14, 433, 1954
Y. Kozai	$-\frac{2}{3}A_2$	$\frac{8}{35}A_4$	$\frac{18}{35}A_4/A_2^2$	
P. Herget and P. Mussen	$-2k_2$	$8k_4$	$2k_4/k_2^2$	<i>J. J.</i> 63, 430, 1958
J. O'Keefe et al.	$+ .12\omega/\mu$	$+ .14\omega/\mu$	$\mu .14\omega/A_2\omega^2$	<i>J. J.</i> 64, 235, 1959
B. Garfinkel	$-2k$	k'	$\frac{1}{4}k'/k^2$	This issue
J. Vinti	$-J_2R^2$	$-J_4R^4$	J_4/J_2^2	<i>J. of Res. Nat. Bureau of Standards</i> 62B, 105, 1959

In the table R represents the earth's equatorial radius. Ignoring the presence of R^2 and differences in sign, essentially three different coefficients for the second

harmonic have been used in recent papers. For the coefficients of the fourth harmonic six different choices are listed. I now regret that I introduced k_2 , k_4 in my paper in 1946. The principal reason was that they give a particularly simple form for the expression of the potential in the equatorial plane. If I could have foreseen the increase in interest in the subject and the confusion to which I was contributing, I would have chosen the coefficients B_p or the alternative form

$$V = \frac{\mu}{r} \left[1 - \sum_{p=2}^{\infty} J_p \left(\frac{R}{r} \right)^p P_p (\sin \beta) \right],$$

which was used by Vinti (1959). I intend to revert to this form and recommend this to other authors.

APPENDIX II

Short Period Term for a

From Brouwer, SPT is

$$1 + \gamma_2 \left[(-1 + 3\theta^2) \left(\frac{a^{n3}}{r'^3} - \eta^{-3} \right) + 3(1 - \theta^2) \frac{a^{n3}}{r'^3} \cos(2g' + 2f') \right]$$

Rewrite

$$1 + \gamma_2 \left[\underbrace{(-1 + 3\theta^2)}_{D(6)} \underbrace{\left(\frac{a^{n3}}{r'^3} - \eta^{-3} \right)}_{\substack{X(11) \\ B(8)}} + \frac{a^{n3}}{r'^3} \underbrace{3(1 - \theta^2)}_{D(19)} \underbrace{\cos(2g' + 2f')}_{X(21)} \right]$$

$\underbrace{\hspace{10em}}_{X(22)} \qquad \underbrace{\hspace{10em}}_{X(23)}$

$$SPT = 1. + C(1) * (X(22) + X(11) * X(23))$$

Short Period Term for e

$$\frac{\eta^2}{2e''} \left\{ \gamma_2 \left[\underbrace{(-1 + 3\theta^2)}_{C(1)} \underbrace{\left(\frac{a^{n3}}{r'^3} - \eta^{-3} \right)}_{X(22)} + \underbrace{\left(\frac{a^{n3}}{r'^3} - \eta^{-4} \right)}_{\substack{X(11) \\ B(9)}} \underbrace{3(1 - \theta^2) \cos(2g' + 2f')}_{X(23)} \right] - \gamma_2' (1 - \theta^2) \underbrace{[3e'' \cos(2g' + f') + e'' \cos(2g' + 3f')]}_{X(24)} \right\}$$

$\underbrace{\hspace{10em}}_{D(23)} \qquad \underbrace{\hspace{10em}}_{X(24)}$

$$SPT_e = G(12) * (C(1) * (X(22) + X(23)) * (X(11) - B(9))) - D(23) * X(24)$$

Short Period Term for Inclination

$$\frac{1}{2} \gamma_2' \theta (1 - \theta^2)^{1/2} \underbrace{[3 \cos(2g' + 2f')]}_{D(22)} + e'' \underbrace{[3 \cos(2g' + f') + \cos(2g' + 3f')]}_{X(24)}$$

$\underbrace{\hspace{10em}}_{X(21)}$

$$SPT_i = D(22) * (3 * X(21) + X(24))$$

Short Period Term for l

$$\begin{array}{c}
 \frac{\eta^2}{4e''} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' + 3(1 - \theta^2) \left[\left(-\frac{a''^2}{r'^2} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
 \begin{array}{cccccccc}
 \uparrow & & & & \uparrow & & & \uparrow \\
 \text{B(2)*G(13)} & \text{D(20)} & \text{X(25)} & \text{X(12)} & \text{D(19)} & \text{X(25)} & \text{X(19)} & \text{X(25)} & \text{X(20)} \\
 & & & & & & & & \vdots \\
 & & & & & & & & \text{X(26)}
 \end{array}
 \end{array}$$

$$\text{SPT}_M = \text{B(2)*X(26)}$$

Short Period Term for g

$$\begin{array}{c}
 + \frac{\eta^2}{4e''} \gamma_2' \left\{ 2(-1 + 3\theta^2) \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + 1 \right) \sin f' \right. \\
 \left. + 3(1 - \theta^2) \left[\left(-\frac{a''^2}{r'^2} \eta^2 - \frac{a''}{r'} + 1 \right) \sin (2g' + f') + \left(\frac{a''^2}{r'^2} \eta^2 + \frac{a''}{r'} + \frac{1}{3} \right) \sin (2g' + 3f') \right] \right\} \\
 \text{X(26)} \\
 \begin{array}{cccccccc}
 & & & \uparrow & & & & & \\
 & & & \text{C(9)} & \text{D(7)} & \text{X(27)/6} & \text{D(21)} & \text{X(17)} & \text{X(19)} & \text{X(20)} \\
 & & & & & & & & & \vdots \\
 & & & & & & & & & \text{X(28)}
 \end{array} \\
 + \frac{1}{4} \gamma_2' \left\{ 6(-1 + 5\theta^2) (f' - l' + e'' \sin f') + (3 - 5\theta^2) [3 \sin (2g' + 2f') + 3e'' \sin (2g' + f') + e'' \sin (2g' + 3f')] \right\}
 \end{array}$$

$$\text{SPT} = \text{X(26)} + \text{C(9)} * (\text{D(7)} * \text{X(27)} + \text{D(21)} * \text{X(28)})$$

Short Period Terms for h

$$\frac{1}{2}\gamma_2'\theta[6(f' - l' + e'' \sin f') - 3 \sin(2g' + 2f') - 3e'' \sin(2g' + f') - e'' \sin(2g' + 3f')], \quad (27)$$

\uparrow
 C(10) X(27) X(28)

$$\text{SPT} = \text{C}(10) * (\text{X}(27) - \text{X}(28))$$

Secular terms:

$l'' =$ "mean" mean anomaly

$$= n_0 \left\{ 1 + \frac{3}{2}\gamma_2'\eta(-1 + 3\theta^2) + \frac{3}{32}\gamma_2'^2\eta[-15 + 16\eta + 25\eta^2 + (30 - 96\eta - 90\eta^2)\theta^2 + (105 + 144\eta + 25\eta^2)\theta^4] + \frac{15}{16}\gamma_4'\eta e''^2[3 - 30\theta^2 + 35\theta^4] \right\} l + l_0''$$

S(1)

$g'' =$ mean argument of perigee

$$= n_0 \left\{ \frac{3}{2}\gamma_2'\eta(-1 + 5\theta^2) + \frac{3}{32}\gamma_2'^2[-35 + 24\eta + 25\eta^2 + (90 - 192\eta - 126\eta^2)\theta^2 + (385 + 360\eta + 45\eta^2)\theta^4] + \frac{5}{16}\gamma_4'[21 - 9\eta^2 + (-270 + 126\eta^2)\theta^2 + (385 - 189\eta^2)\theta^4] \right\} l + g_0''$$

S(2)

$h'' =$ mean longitude of ascending node

$$= n_0 \left\{ -3\gamma_2'\theta + \frac{3}{8}\gamma_2'^2[(-5 + 12\eta + 9\eta^2)\theta + (-35 - 36\eta - 5\eta^2)\theta^2] + \frac{5}{4}\gamma_4'(5 - 3\eta^2)\theta(3 - 7\theta^2) \right\} l + h_0''$$

S(3)

Long-period terms:

EL(10)

$$\delta_1 e = \left\{ \frac{1}{8}\gamma_2'e''\eta^2[1 - 11\theta^2 - 40\theta^4(1 - 5\theta^2)^{-1}] - \frac{5}{12}\frac{\gamma_4'}{\gamma_2'}e''\eta^2[1 - 3\theta^2 - 8\theta^4(1 - 5\theta^2)^{-1}] \right\} \cos 2g'' + \left\{ \frac{1}{4}\frac{\gamma_6'}{\gamma_2'}\eta^2 \sin I'' + \frac{5}{64}\frac{\gamma_6'}{\gamma_2'\eta^2} \sin I'' (4 + 3e''^2)[1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \right\} \sin g''$$

EL(11)

$$- \frac{35}{384}\frac{\gamma_6'}{\gamma_2'}e''^2\eta^2 \sin I'' [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] \sin 3g''$$

EL(12)

$$\delta_1 I = -\frac{e'' \delta_1 e}{\eta^2 \tan I''} = \text{EL}(13) * \delta_1 e$$

Long Period Terms

$$l' = l'' + \left\{ \frac{1}{8} \gamma_2' \eta' [1 - 11\theta^2 - 40\theta^4(1 - 5\theta^2)^{-1}] - \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} \eta^2 [1 - 3\theta^2 - 8\theta^4(1 - 5\theta^2)^{-1}] \right\} \sin 2g'' + \left\{ -\frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \frac{\eta^2}{e''} \sin I'' - \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \frac{\eta^2}{e''} \sin I'' (4 + 9e''^2) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \right\} \cos g'' + \frac{35}{384} \frac{\gamma_6'}{\gamma_2'} \eta^2 e'' \sin I'' [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] \cos 3g''$$

\uparrow A11(6) \uparrow C(5) \uparrow B(3) \uparrow D(10) \uparrow X(3) \uparrow C(7) \uparrow F(5) \uparrow X(4) \uparrow X(5)

$\underbrace{\hspace{15em}}_{D(11)} \quad \underbrace{\hspace{15em}}_{EL(2)} \quad \underbrace{\hspace{15em}}_{EL(3)}$

$\underbrace{\hspace{15em}}_{B(3) * D(11)} \quad \underbrace{\hspace{15em}}_{EL(1)}$

$$l' = l'' + EL(1) * X(3) + EL(2) * X(4) + EL(3) * X(5)$$

$$g' = g'' + \left[\begin{array}{l} -\frac{1}{16} \gamma_2' [(2 + e''^2) - 11(2 + 3e''^2)\theta^2 - 40(2 + 5e''^2)\theta^4(1 - 5\theta^2)^{-1}] \\ -400e''^2\theta^6(1 - 5\theta^2)^{-2} + \frac{5}{24} \frac{\gamma_4'}{\gamma_2'} [2 + e''^2 - 3(2 + 3e''^2)\theta^2 - 8(2 + 5e''^2)\theta^4(1 - 5\theta^2)^{-1}] \\ -80e''^2\theta^6(1 - 5\theta^2)^{-2} \end{array} \right] \sin 2g'' + \left[\begin{array}{l} \frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \left(\frac{\sin I''}{e''} - \frac{e''\theta^2}{\sin I''} \right) + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \\ \left(\frac{\eta^2 \sin I''}{e''} - \frac{e''\theta^2}{\sin I''} \right) (4 + 3e''^2) + e'' \sin I'' (26 + 9e''^2) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] \\ -\frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e''\theta^2 \sin I'' (4 + 3e''^2) [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \end{array} \right] \cos g''$$

\uparrow EL(4) \uparrow X(3) \uparrow EL(5) \uparrow X(4)

$$g' = g'' + EL(4) * X(3) + EL(5) * X(4) + EL(6) * X(5)$$

\uparrow A1(5) \uparrow A11(5) \uparrow EL(6) \uparrow X(5)

$$h' = h'' + \left\{ \frac{1}{8} \gamma_2' e''^2 \theta [11 + 80\theta^2(1 - 5\theta^2)^{-1} + 200\theta^4(1 - 5\theta^2)^{-2}] + \frac{5}{12} \frac{\gamma_4'}{\gamma_2'} e''^2 \theta [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \right\} \sin 2g'' + \left\{ \frac{1}{4} \frac{\gamma_2'}{\gamma_2'} \frac{e''\theta}{\sin I''} + \frac{5}{64} \frac{\gamma_6'}{\gamma_2'} \frac{e''\theta}{\sin I''} (4 + 3e''^2) [1 - 9\theta^2 - 24\theta^4(1 - 5\theta^2)^{-1}] + \frac{15}{32} \frac{\gamma_6'}{\gamma_2'} e''\theta \sin I'' (4 + 3e''^2) [3 + 16\theta^2(1 - 5\theta^2)^{-1} + 40\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos g'' + \left\{ -\frac{35}{1152} \frac{\gamma_6'}{\gamma_2'} \frac{e''^2 \theta}{\sin I''} [1 - 5\theta^2 - 16\theta^4(1 - 5\theta^2)^{-1}] - \frac{35}{576} \frac{\gamma_6'}{\gamma_2'} e''^2 \theta \sin I'' [5 + 32\theta^2(1 - 5\theta^2)^{-1} + 80\theta^4(1 - 5\theta^2)^{-2}] \right\} \cos 3g''$$

\uparrow EL(7) \uparrow X(3) \uparrow EL(8) \uparrow X(4) \uparrow EL(9) \uparrow X(5)

$$h' = h'' + EL(7) * X(3) + EL(8) * X(4) + EL(9) * X(5)$$

APPENDIX III (PART A)

PROGRAM OPERATING INSTRUCTIONS
FOR MAIN PROGRAM ONE

```

@PPRATING INSTRUCTIONS
      FOR
      MUSTAP PROGRAM
@PPRATING NOTES FOR MUSTAP PROGRAM.
PURPOSE--
      THE MUSTAP PROGRAM IS ONE DESIGNED TO COMPUTE MUTUAL VISIBILITY
, LOCAL STATION PREDICTIONS, SPACECRAFT LOOK ANGLES, AND WORLD MAPS OF
COMMUNICATION SATELLITES.
INPUT--
      INPUT TO THE PROGRAM CONSISTS OF CONTROL OPTIONS, TEST CRITERIA,
EPOCH, ORBITAL ELEMENTS OR POSITION AND VELOCITY VECTORS, START AND STOP
TIMES WITH PREDICTION INTERVAL, ATTITUDE DATA, AND STATION COORDINATES.
METHOD--
      THE PATH OF THE SATELLITE IS COMPUTED BY AN INTERNAL ORBIT
GENERATOR. THE POSITION OF THE SPACECRAFT WITH RESPECT TO EACH STATION
IS COMPUTED AND TESTED AGAINST THE SPECIFIED CRITERIA. OUTPUT STATEMENTS
ARE ARRANGED TO PRESENT THE DATA IN THE MOST USEFUL MANNER TO THE PROJECT.
OUTPUT--
      OUTPUT DATA ARE WRITTEN ON TWO MAGNETIC TAPES--(1) MUTUAL VISIBILITY
(2) WORLD MAP, PREDICTIONS AND TIME THE SATELLITE IS IN SHADOW. THE MUTUAL
VISIBILITY DATA ARE PRESENTED IN GRAPHICAL FORM. THE OTHER DATA ARE S/C
LATITUDE, LONGITUDE, HEIGHT, AZIMUTH, ELEVATION, RANGE, AND SPACECRAFT
LOOK ANGLE (THE ANGLE BETWEEN THE S/C SPIN AXIS AND THE LINE TO THE STATION).
FOR CHECKOUT PURPOSES A SENSE SWITCH CAN BE DOWN AND THE INPUT WILL BE
WRITTEN ON--LINE.
PROGRAM INPUT DATA INSTRUCTIONS.
INPUT DATA--
      ALL INPUT DATA ARE ON CARDS (READ ON--LINE).
CARD 1-- IDENTIFICATION CARD (FORMAT 2(6A6))--ANY DESCRIPTIVE DATA
NOTE ---
      THIS IDENTIFICATION IS OUTPUT ON 2 LINES --
      LINE 1 --CONTENTS OF COLUMNS 1-36
      LINE 2 --CONTENTS OF COLUMNS 37-72
CARD 2--CONTROL CARD (FORMAT 8(3,F10,1))
COLUMN
1-3 TYPE OF INPUT +01 = OSCULATING ORBITAL ELEMENTS
+03 = INERTIAL R AND V VECTORS, CANONICAL UNITS
+04 = BROWNER MEAN ELEMENTS
4-6 WORLD MAP +01 = COMPUTE WORLD MAP AND PREDICTIONS
+00 = DO NOT COMPUTE WORLD MAP AND PREDICTIONS
-01 = DO NOT COMPUTE WORLD MAP AND PREDICTIONS
7-9 LOOK ANGLE +01 ALWAYS
10-12 EARTH CONST. -03 = USE INTERNATIONAL CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-02 = USE GODDARD EARTH CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-01 = USE SIRY PACKAGE CONSTANTS
+00 = USE GODDARD EARTH CONSTANTS
+01 = READ A NEW SET OF EARTH CONSTANTS
([INPUT ON CARDS 4-5])
13-15 TRUNCATION -01 = USE INTERNAL VALUE
+00 = USE INTERNAL VALUE
+01 = READ NEW TRUNCATION FACTOR -- CARD 3
(USED AS CRITERIA TO SOLVE KPFLER'S EQ.)
16-18 BROWNER TRUNCATION -01 = USE INTERNAL VALUES
+00 = USE INTERNAL VALUES
+01 = READ NEW TRUNCATION FACTORS FOR
SUBROUTINE BBRWR -- CARD 6
19-21 BLANK -- USED INTERNALLY
22-24 POSITIVE N -- N CONTROL STATIONS (THEY ARE THE FIRST N

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STATIONS.)
N MUST BE LFSS THAN OR EQUAL TO THE NUMBER OF STATIONS GIVEN
ON CARD 11.

25-34 MAXIMUM RANGE FOR STATIONS IN NAUTICAL MILES. A T IS PRINTED
ON THE MUTUAL VISIBILITY OUTPUT,WHFN THE RANGE IS LARGER
THAN THIS VALUF.

CARD 3 -- NEW TRUNCATION FACTØR (ØMIT THIS CARD UNLESS CØLUMNS 13-15
OF CARD 2 ARF = +01) (FØRMT FØ.2)

CØLUMN
1-8 NFW TRUNCATION FACTØR

CARD 4 -- EARTH CØNSTANTS (ØMIT UNLESS CØLUMNS 10-12 ØF
CARD 2 = +01) (FØRMT F12.6,F12.5)

CØLUMN
1-12 NFW ØF THE EARTH (KM, CUBFD/ SFCØNDS SQUARED)
13-24 J2)
25-36 J3) HARMØNICS ØF THE GRAVITATIONAL PØTENTIAL ØF
37-48 J4) THE EARTH
49-60 J5)

CARD 5 -- EARTH CØNSTANTS CØNTINUED (ØMIT UNLESS CØLUMNS 10-12
ØF CARD 2 = +01) (FØRMT 2F12.4)

CØLUMN
1-12 INVRSØ OF FLATTENING
13-24 EQUATORIAL RADIUS ØF THE EARTH IN KM

CARD 6 -- NEW TRUNCATION FACTØRS FOR SUBRØUTINE BØRNR (ØMIT UNLESS
CØLUMNS 10-18 ØF CARD 2 ARE = +01) (FØRMT ØF12.8)
TRUNCATION FACTØRS USED IN CØMPUTING BRØUWER MEAN
ELEMENTS FRØM ØSCULATING ELFHNENTS ---

CØLUMN
1-12 (SEMI-MAJØR AXIS - KM
13-24 (ECCFNTPICITY - KM
25-36 FACTØR FOR (INCLINATION - DEGRFS
37-48 (R.A. ASC. NØDF - DEGRFS
49-60 (ARG. ØF PFRIGFF - DEGRFS
61-72 (MEAN ANØVALY - DEGRFS

CARD 7 -- EPOCH CARD (TIME AT WHICH PARAMETERS APPLY)
FØRMT 1X,A5,X,3I2,X,2I2,X,F4.2,39X,15)

CØLUMN
1 PLANK
2-6 SATELLITE IDENTIFICATION NUMBER
8-9 YFAP (ABBØFVIATF)
10-11 MONTH
12-13 DAY
15-16 HOUR)
17-18 MINUTE) UNIVRSAL TIME
20-24 SFCØNDS)
63-67 ØRBIT NUMBER AT THE START TIME GIVEN ØN CARD 10

CARD 8 -- PARAMETER CARD (THFSE DATA MUST BE CØHØEN IN ACCØRDANCE
WITH THE INSTRUCTION ØN CARD 2, CØLUMNS 1-3)
(FØRMT ØF12.8) +XXXXXXXXXX

--ØØ NØT LEAVE THE SIGN ØF THE EXPØNENT BLANK--

VECTØRS (+Ø3) REQUIRF THE FØLLØWING

CØL
1-12 X VUL
13-24 Y VUL
25-36 Z VUL
37-48 X-DØT VUL/VUT
49-60 Y-DØT VUL/VUT
61-72 Z-DØT VUL/VUT

ELFHNENTS (+Ø1 AND +Ø4) REQUIRF THE FØLLØWING

CØL
1-12 SEMI-MAJØR AXIS VUL
13-24 ECCENTRICITY
25-36 INCLINATION RADIANS
37-48 MEAN ANØVALY RADIANS
49-60 ARGUMENT ØF PFRIGFF RADIANS
61-72 R.A. ØF ASCENDING NØDF RADIANS
ØNE VUL = 6378.388 KILØMETERS
ØNE VUL/VUT = 6378.388 KM / ØØØ.Ø22 SEC
RECTANGULAR CØØRDINATES ARE ØFFINED TO BE IN AN INERTIAL,
EQUATORIAL, GØCØNTRIC SYSTEM. X GØES THROUGH ARIES, Y IS
IN EQUATORIAL PLANE, Z IS ALØNG PØLAR AXIS TØ FØRM A RIGHT
HANDED SYSTEM.

CARD 9 -- DRAG CARD (FØRMT A46.1X,E12.8)

CØL
1-24 SAME AS EPOCH CARD
25 PLANK
26-37 ACCELERATION ØF MEAN ANØVALY(N2 DRAG TERM AT GSFC) IN
UNITS ØF RADIANS / VUT SQUARFD. +XXXXXXXXXX

CARD 10 -- PREDICTION AND MUTUAL VISIBILITY REQUEST CARD
(FØRMT 2I1I2I,1X,14,2I3,F7.3,13,1X,12,1X,1,2I3,
F7.3,F11.3)

CØL FØRMT
2-3 MONTH IZ

5-6 DAY)) I2
 8-11 YEAR (DO NOT ABRFVIATF)) START I4
 13-14 HOUR)) TIME I2
 16-17 MINUTE) UNIVERSAL TIME) I2
 19-24 SECOND)) F6.3
 26-27 MONTH)) I2
 29-30 DAY)) I2
 32-35 YEAR (DO NOT ABRFVIATF)) END I4
 37-38 HOUR)) TIME I2
 40-41 MINUTE) UNIVERSAL TIME) I2
 43-48 SECOND)) F6.3
 49-59 PREDICTION INTERVAL, SECOND) F11.3

CARD 11--STATION CONTROL CARD (FORMAT 313,F10,0,51X,I2)

COL
 1-3 NO. OF STATION COORDINATE CARDS TO BE LOADED
 N.B., THE MAXIMUM NUMBER OF STATIONS THAT CAN BE CONSIDERED IS NINETY (19).
 4-6 = BLANK OR +00
 7-9 = +XX LOWEST ELEVATION ANGLE FOR WHICH THE STATIONS CAN OBSERVE THE SPACECRAFT.
 10-19= BLANK (READ BUT NOT USED)
 20-70= BLANK (NOT READ)
 71-72= BLANK FOR NORMAL RUNS. OUTPUT FOR A PASS IS GIVEN WHEN THERE IS MUTUAL VISIBILITY BETWEEN AT LEAST TWO STATIONS (ONE OF WHICH IS A CONTROL STATION) DURING THE PASS.
 +XX UNEQUAL TO ZERO -- KILLS MUTUAL VISIBILITY REQUIREMENT-- GIVES OUTPUT ANYTIME THE SPACECRAFT IS VISIBLE TO ANY OF THE STATIONS.

(WHEN COLUMNS 1-3 OF THIS CARD ARE LESS THAN OR EQUAL TO ZERO, A NEW JOB IS STARTED BY READING CARD 1.)

CARD 12--ATTITUDE DATA CARD (FORMAT 4F6,1,I6)

COL
 1-12 READ BUT NOT USED
 13-18 RIGHT ASCENSION OF S/C SPIN AXIS, DEGREES
 19-24 DECLINATION OF S/C SPIN AXIS, DEGREES
 25-30 +00 USE THE INPUT VALUES OF RT, ASCENSION AND DECLINATION TO DEFINE SPIN AXIS DIRECTION
 +XX (POSITIVE) ASSUME SPIN AXIS IS ALONG THE INITIAL INERTIAL VELOCITY VECTOR

N.B., RIGHT ASCENSION AND DECLINATION ARE AT THE EPOCH GIVEN ON CARD 3. THESE ANGLES ARE ASSUMED CONSTANT.

CARD 13 -- STATION COORDINATE CARD (S)

COL	NAME	FORMAT
2-7	LONGITUDE, DEGREES (+FAST)	A6
9-12	LONGITUDE, MINUTES	I4
14-15	LONGITUDE, SECONDS	I2
17-22	LATITUDE, DEGREES (+NORTH)	F6.3
24-26	LATITUDE, MINUTES	I3
28-29	LATITUDE, SECONDS	I2
31-36	ALTITUDE, METERS	F6.3
37-47	ALTITUDE, METERS	F11.2

N.B., THERE MUST BE AS MANY STATION COORDINATE CARDS AS INDICATED BY CARD 11.

THE STATION COORDINATE CARDS ARE FOLLOWED BY ANOTHER STATION CONTROL CARD OR BY A BLANK. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS NEGATIVE OR ZERO, A NEW JOB IS STARTED BY READING CARD 1. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS POSITIVE, NEW ATTITUDE DATA AND COORDINATE CARDS ARE READ. MUTUAL VISIBILITY AND PREDICTIONS ARE THEN COMPUTED FOR THE NEW STATIONS AND ATTITUDE FOR TIMES GIVEN ON CARD 10.

JOB'S MAY BE STACKED BY PLACING A BLANK CARD AFTER THE LAST STATION COORDINATE CARD. CARD 1 OF THE NEW JOB THEN FOLLOWS THIS BLANK CARD.

PLACE 3 BLANK CARDS AFTER THE LAST STATION COORDINATE CARD IN THE LAST INPUT DECK OF THE JOB. THIS WILL RESULT IN THE CORRECT FINAL HALT -- HPR 77777.

PUT SENSE SWITCH 3 DOWN TO TERMINATE RUN BEFORE THE END TIME IS REACHED.

VALUF	EARTH CONSTANTS STORED IN THE PROGRAM		
	INTERNATIONAL	STANDARD	SIRY
GM	+3.986268730E+05	+3.986032000E+05	+3.986268800E+05
J2	0.0	+1.0823E-03	+1.08219E-03
J3	0.0	+2.3F-06	-2.88E-06
J4	0.0	-1.8E-06	-2.123F-06
J5	0.0	0.0	-2.32F-07
F	297.0	298.3	297.0
A	6378.388	6378.165	6378.388

RUNNING INSTRUCTIONS.

0
0
0
0
0
0
0

Mount PROGRAM SYSTEM TAPE ON A1
Mount BLANK TAPES ON A3, A5, A8
No KEYS ON SENSE SWITCHES.
PUT INPUT CARDS IN READER AND READER READER.
CLEAR AND LOAD TAPE.
FINAL STOP IS HPR 77777

HALTS --

HPR 00010 MACHINE IS NOT IN 65K
HPR 54321 MORE THAN 19 CONTROL STATIONS ARE BEING USED. THE
PROGRAM CAN NOT RUN.
HPR 54333 THE NUMBER OF CONTROL STATIONS IS LARGER THAN THE NUMBER
OF STATIONS.
HPR 66666 MORE THAN 19 STATIONS ARE BEING USED. THE PROGRAM
CAN NOT RUN.
HPR 77774 SENSE SWITCH 2 IS DOWN FOR TIMING PURPOSES -- END OF
PREDICTIONS. HIT START TO CONTINUE.
HPR 77775 SENSE SWITCH 2 IS DOWN FOR TIMING PURPOSES -- BEGINNING
OF PREDICTIONS. HIT START TO CONTINUE.
HPR 77777 FINAL (END OF JOB)

PRINT OUTPUT TAPE A3
(1) NARROW PAPER WHEN THERE ARE 15 OR LESS STATIONS
(2) WIDE PAPER WHEN THERE ARE 16 TO 19 STATIONS
PRINT OUTPUT TAPE A8 ON NARROW PAPER.

APPENDIX III (PART B)
PROGRAM OPERATING INSTRUCTIONS
FOR MAIN PROGRAM TWO

OPERATING INSTRUCTIONS

FOR

MUSTAP PROGRAM

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0
0 OPERATING NOTES FOR MUSTAP PROGRAM.
0
0 PURPOSE--
0 THE MUSTAP PROGRAM IS ONE DESIGNED TO COMPUTE MUTUAL VISIBILITY,
LOCAL STATION PREDICTIONS, SPACECRAFT LOOK ANGLES, AND WORLD MAPS OF
COMMUNICATION SATELLITES.
0
0 INPUT--
0 INPUT TO THE PROGRAM CONSISTS OF CONTROL OPTIONS, TEST CRITERIA,
EPOCH, ORBITAL ELEMENTS OR POSITION AND VELOCITY VECTORS, START AND STOP
TIMES WITH PREDICTION INTERVAL, ALTITUDE DATA, AND STATION COORDINATES.
0
0 METHOD--
0 THE PATH OF THE SATELLITE IS COMPUTED BY AN INTERNAL ORBIT
GENERATOR. THE POSITION OF THE SPACECRAFT WITH RESPECT TO EACH STATION
IS COMPUTED AND TESTED AGAINST THE SPECIFIED CRITERIA. OUTPUT STATEMENTS
ARE ARRANGED TO PRESENT THE DATA IN THE MOST USEFUL MANNER TO THE PROJECT.
0
0 OUTPUT--
0 OUTPUT DATA ARE WRITTEN ON TWO MAGNETIC TAPES--(1) MUTUAL VISIBILITY
AND WORLD MAP (2) PREDICTIONS. FOR CHECKOUT PURPOSES A SENSE SWITCH CAN BE
DOWN AND ALL DATA WILL BE WRITTEN ON-LINE. THE MUTUAL VISIBILITY DATA ARE
PRESENTED IN GRAPHICAL FORM. THE OTHER DATA ARE S/C LATITUDE, LONGITUDE,
AND HEIGHT FOR EACH TIME STEP, AZIMUTH, ELEVATION, RANGE, AND SPACECRAFT
LOOK ANGLE (THE ANGLE BETWEEN THE S/C SPIN AXIS AND THE LINE TO THE STATION)
FOR EACH STATION.
0
0 PROGRAM INPUT DATA INSTRUCTIONS.
0
0 INPUT DATA--
0 ALL INPUT DATA ARE ON CARDS (READ ON-LINE).
0
0 CARD 1--IDENTIFICATION CARD (FORMAT 12A6)--ANY DESCRIPTIVE DATA
0
0 CARD 2--CONTROL CARD (FORMAT 713)
0
0 COLUMN
0 1-3 TYPE OF INPUT +01 = OSCILLATING ORBITAL ELEMENTS
+02 = INERTIAL R AND V VECTORS, KGS SYSTEM
+03 = INERTIAL R AND V VECTORS, CANONICAL UNITS
+04 = BROWNER MEAN ELEMENTS
0 4-6 WORLD MAP +01 = COMPUTE WORLD MAP
+00 = DO NOT COMPUTE MAP
-01 = DO NOT COMPUTE MAP
0 7-9 LOOK ANGLE +01 = COMPUTE MUTUAL VISIBILITY
+00 = DO NOT COMPUTE MUTUAL VISIBILITY
-01 = DO NOT COMPUTE MUTUAL VISIBILITY
0 10-12 EARTH CONST. -03 = USE INTERNATIONAL CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-02 = USE GODDARD EARTH CONSTANTS WITH
HARMONICS EQUAL TO ZERO.
-01 = USE SIRY PACKAGE CONSTANTS
+00 = USE GODDARD EARTH CONSTANTS
+01 = READ A NEW SET OF EARTH CONSTANTS
(INPUT ON CARDS 4-5)
0 13-15 TRUNCATION -01 = USE INTERNAL VALUE
+00 = USE INTERNAL VALUE
+01 = READ NEW TRUNCATION FACTOR -- CARD 3
(USED AS CRITERIA TO SOLVE KEPLER'S EQ.)
0 16-18 BBRWR TRUNCATION -01 = USE INTERNAL VALUES
+00 = USE INTERNAL VALUES
+01 = READ NEW TRUNCATION FACTORS FOR
SUBROUTINE BBRWR -- CARD 6
0
0 CARD 3 -- NEW TRUNCATION FACTOR ( OMIT THIS CARD UNLESS COLUMNS 13-15
OF CARD 2 ARE = +01 ) (FORMAT E8.2)

```

COLUMN
1-8 NFW TRUNCATION FACTOR

CARD 4 -- EARTH CONSTANTS (OMIT UNLESS COLUMNS 10-12 OF
CARD 2 = +01) (FORMAT F12.6,4E12.5)

COLUMN
1-12 NEW GM OF THE EARTH (KM. CUBED/ SECONDS SQUARED)
13-24 J2)
25-36 J3) HARMONICS OF THE GRAVITATIONAL POTENTIAL OF
37-48 J4) THE EARTH
49-60 J5)

CARD 5 -- EARTH CONSTANTS CONTINUED (OMIT UNLESS COLUMNS 10-12
OF CARD 2 = +01) (FORMAT 2F12.4)

COLUMN
1-12 INVERSE OF FLATTENING
13-24 EQUATORIAL RADIUS OF THE EARTH IN KM

CARD 6 -- NEW TRUNCATION FACTORS FOR SUBROUTINE BBRWR (OMIT UNLESS
COLUMNS 16-18 OF CARD 2 ARE = +01) (FORMAT 6F12.8)
TRUNCATION FACTORS USED IN COMPUTING BROUWER MEAN
ELEMENTS FROM OSCULATING ELEMENTS ---

COLUMN
1-12 (SEMI-MAJOR AXIS - KM
13-24 (ECCENTRICITY
25-36 FACTOR FOR (INCLINATION - DEGREES
37-48 (R.A. ASC. NODE - DEGREES
49-60 (ARG. OF PERIGEE - DEGREES
61-72 (MEAN ANOMALY - DEGREES

CARD 7 -- EP@CH CARD (TIME AT WHICH PARAMETERS APPLY)

COL.	MONTH	DAY	YEAR (DO NOT ABBREVIATE)	HOUR	MINUTE	SECOND
2-3						
5-6						
8-11						
13-14						
16-17						
19-24						

FORMAT
12
12
14
12
12
F5.3

CARD 8 -- PARAMETER CARD (THESE DATA MUST BE CHOSEN IN ACCORDANCE
WITH THE INSTRUCTION ON CARD 2, COLUMNS 1-3) (FORMAT 6F12.6)
ELEMENTS (+01 OR +04) REQUIRE THE FOLLOWING

COL	SEMI-MAJOR AXIS, KILOMETERS	ECCENTRICITY	INCLINATION	R.A. OF ASCENDING NODE	ARGUMENT OF PERIGEE	MEAN ANOMALY
1-12						
13-24						
25-36						
37-48						
49-60						
61-72						

VECTORS (+02 OR +03) REQUIRE THE FOLLOWING

COL	X	Y	Z	X-DOT	Y-DOT	Z-DOT
1-12						
13-24						
25-36						
37-48						
49-60						
61-72						

ONE VUL = 6378.388 KILOMETERS
ONE VUL/VUT = 6378.388 KM/ 806.832 SEC
RECTANGULAR COORDINATES ARE DEFINED TO BE IN AN INERTIAL,
EQUATORIAL, GEOCENTRIC SYSTEM. X GOES THROUGH ARIES, Y IS
IN EQUATORIAL PLANE, Z IS ALONG POLAR AXIS TO FORM A RIGHT
HANDED SYSTEM.

CARD 9 -- WORLD MAP REQUEST CARD.
THIS CARD IS NEEDED ONLY WHEN THE NUMBER IN COLUMNS 4-6
OF CARD 2 IS GREATER THAN ZERO.
(FORMAT 2(1X12),1X,14+213,F7.3,13,1X,12+1X,14+213,
F7.3,F11.3)

COL	MONTH	DAY	YEAR (DO NOT ABBREVIATE)	HOUR	MINUTE	SECOND	MONTH	DAY	YEAR (DO NOT ABBREVIATE)	HOUR	MINUTE	SECOND	PREDICTION INTERVAL, SECOND
7-3													
4-6													
8-11													
13-14													
16-17													
19-24													
26-27													
29-30													
32-35													
37-38													
40-41													
43-48													
49-59													

FORMAT
12
12
14
12
12
F6.3
12
12
14
12
12
F6.3
F11.3

N.B., IF THE NUMBER IN COLUMNS 7-9 OF CARD 2 IS ZERO OR
NEGATIVE, A NEW JOB IS STARTED BY PEADING CARD 1.

N.B., IF CONTROL ON CARD 2 REQUESTS BOTH MAP AND PREDICTIONS,
TWO REQUEST CARDS ARE NECESSARY.

CARD 10 -- PREDICTION AND MUTUAL VISIBILITY REQUEST CARD
THIS CARD IS NEEDED ONLY WHEN THE NUMBER IN COLUMNS 7-9
OF CARD 2 IS GREATER THAN ZERO.

(SAME FORMAT AS CARD 9)

CARD 11 -- STATION CONTROL CARD (FORMAT 313,F10.0)

COL.
1-3 NO. OF STATION COORDINATE CARDS TO BE LOADED

N.B., THE MAXIMUM NUMBER OF STATIONS THAT CAN BE CONSIDERED IS TWELVE (12).
4-6 = +1 COMPUTE PREDICTIONS, OUTPUT WILL BE ON TAPE A6.
+00 DO NOT OUTPUT PREDICTIONS (ON TAPE A6)
7-9 = MINIMUM ELEVATION ANGLE (DEGREES). NO OUTPUT IS GIVEN IF ELEVATION IS LESS THAN THIS VALUE.
10-20 = MAXIMUM RANGE (KILOMETERS). NO OUTPUT IS GIVEN WHEN THE RANGE IS LARGER THAN THIS VALUE.

(WHEN COLUMNS 1-3 OF THIS CARD ARE LESS THAN OR EQUAL TO ZERO A NEW JOB IS STARTED BY READING CARD 1.)

CARD 12 -- ATTITUDE DATA CARD (FORMAT 4F6.1)

COL.
1-6 MAXIMUM SPACECRAFT LOOK ANGLE, DEGREES
7-12 MINIMUM SPACECRAFT LOOK ANGLE, DEGREES
13-18 RIGHT ASCENSION OF S/C SPIN AXIS, DEGREES
19-24 DECLINATION OF S/C SPIN AXIS, DEGREES

NO MUTUAL VISIBILITY OUTPUT IS GIVEN WHEN THE SPACECRAFT LOOK ANGLE IS OUTSIDE THE LIMITS OF THE MAXIMUM AND MINIMUM VALUES ON THIS CARD.

N.B., MAXIMUM AND MINIMUM LOOK ANGLES, RIGHT ASCENSION, AND DECLINATION ARE CONSTANTS.

CARD 13 -- STATION COORDINATE CARD (S)

COL	NAME	FORMAT
2-7	NAME	A6
9-12	LONGITUDE, DEGREES (+EAST)	I4
14-15	LONGITUDE, MINUTES	I2
17-22	LONGITUDE, SECONDS	F6.3
24-26	LATITUDE, DEGREES (+NORTH)	I3
28-29	LATITUDE, MINUTES	I2
31-36	LATITUDE, SECONDS	F6.3
37-47.	ALTITUDE, METERS	F11.2

N.B., THERE MUST BE AS MANY STATION COORDINATE CARDS AS INDICATED BY CARD 11.
THE STATION COORDINATE CARDS ARE FOLLOWED BY ANOTHER STATION CONTROL CARD OR BY A BLANK. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS NEGATIVE OR ZERO, A NEW JOB IS STARTED BY READING CARD 1. IF THE NUMBER IN COLUMNS 1-3 OF THIS CARD IS POSITIVE, NEW ATTITUDE DATA AND COORDINATE CARDS ARE READ. MUTUAL VISIBILITY AND PREDICTIONS ARE THEN COMPUTED FOR THE NEW STATIONS AND ATTITUDE FOR TIMES GIVEN ON CARD 10.

JOBS MAY BE STACKED BY PLACING A BLANK CARD AFTER THE LAST STATION COORDINATE CARD. CARD 1 OF THE NEW JOB THEN FOLLOWS THIS BLANK CARD.

PLACE 3 BLANK CARDS AFTER THE LAST STATION COORDINATE CARD IN THE LAST INPUT DECK OF THE JOB. THIS WILL RESULT IN THE CORRECT FINAL HALT -- HPR 77777.

	EARTH CONSTANTS STORED IN THE PROGRAM		
VALUF	INTERNATIONAL	GODDARD	SIRY
GH	+3.986268730E+05	+3.986032000E+05	+3.986268800E+05
J2	0.0	+1.0823E-03	+1.08219E-03
J3	0.0	-2.3E-06	-2.285E-06
J4	0.0	-1.8E-06	-2.123E-06
J5	0.0	0.0	-2.32E-07
F	297.0	298.3	297.0
A	6378.388	6376.165	6376.388

RUNNING INSTRUCTIONS.

RUN UNDER MONITOR SYSTEM
MOUNT BLANK TAPES ON A3 AND A6. IF CONTROL ON CARD 6 CALLS FOR A6

NO KEYS OR SPNSE SWITCHES.

PUT INPUT CARDS IN READER AND READY READER.

FINAL STOP IS -- HPR 77777

PRINT OUTPUT TAPES A3 AND A6 ON NARROW PAPER WITH PROGRAM CONTROL

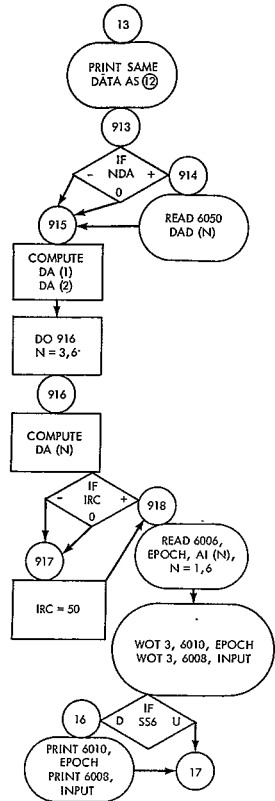
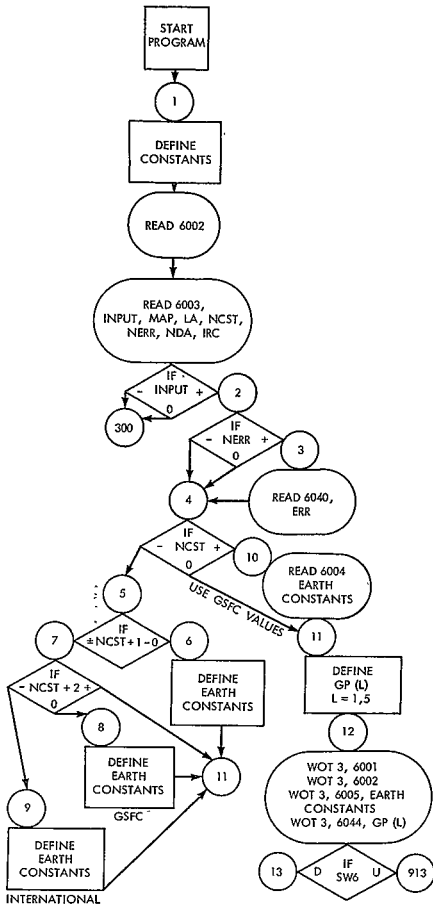
SAMPLE PROGRAM INPUT DECK FOLLOWS. THE DECK WILL COMPUTE THE MUTUAL VISIBILITY OF 12 STATIONS FOR ABOUT ONE DAY. SOME OF THE

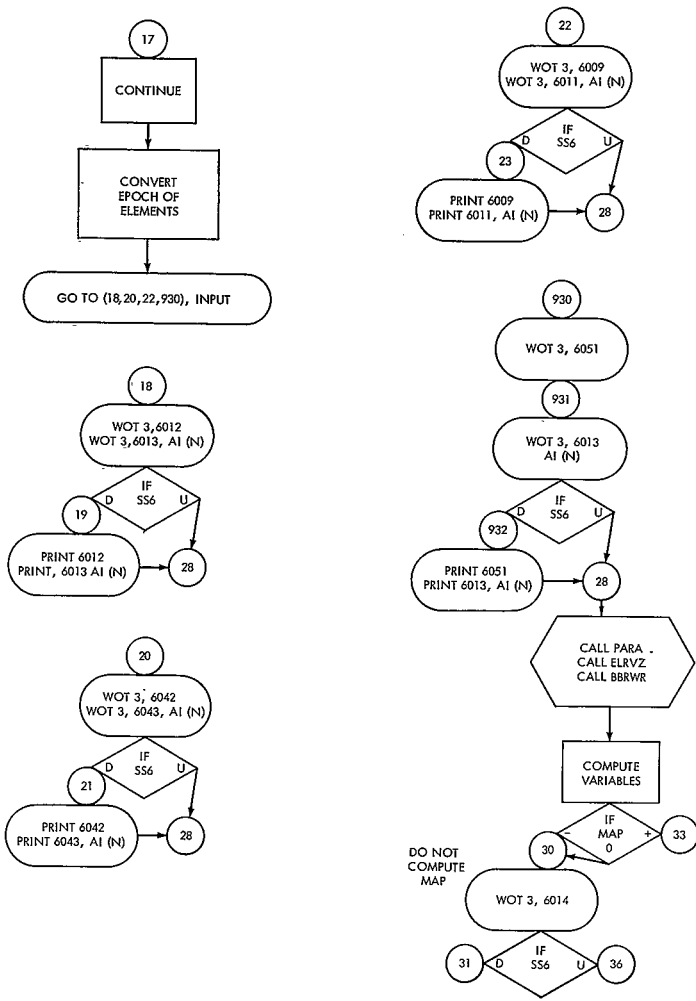
STATIONS WILL BE DUPLICATED. NOTE THAT BOTH MUTUAL VISIBILITY AND
 A WORLD MAP ARE REQUESTED.

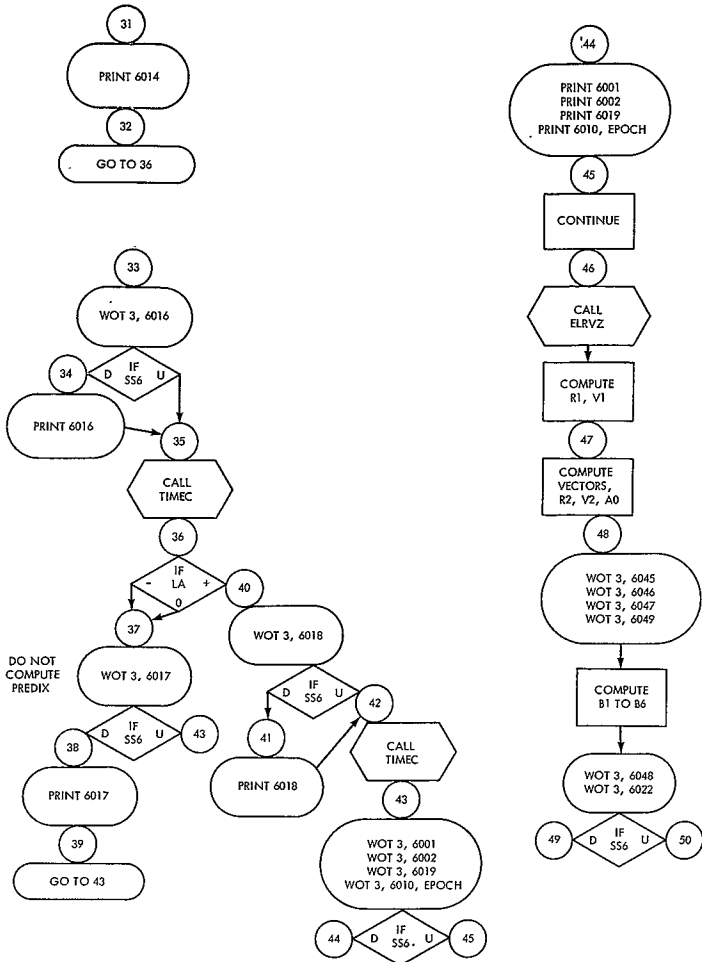
RELAY TEST 12 STATIONS
 +04+01+01-01
 01/14/1964 21 57
 +11143.084 +0.23653052 +46.497757 +220.62688 +186.36665 +359.95097
 01/15/1964 20 00 00.000 01/16/1964 20 00 00.000 +120.
 01/15/1964 19 00 00.000 01/16/1964 19 00 00.000 +120.
 +12+01+00
 90.0 0.0 178. 25.
 CCMNUT -75 00 0.000 +40 00 0.000 0.0
 CCMAND -068 40 00.000 +44 54 00.000 38.
 CCMHIL -05 10 29.0 +50 02 58.0 350.0
 CCMGFR +10 00 00.000 +51 00 00.000 50.
 CCMTEL +13 36 5.000 +41 58 41.000 2168.6
 CCMRIF -43 22 7.000 -22 57 9.000 0.8
 CCMNUT -75 00 0.000 +40 00 0.000 0.0
 CCMAND -068 40 00.000 +44 54 00.000 38.
 CCMHIL -05 10 29.0 +50 02 58.0 350.0
 CCMNUT -75 00 0.000 +40 00 0.000 0.0
 CCMAND -068 40 00.000 +44 54 00.000 38.
 CCMHIL -05 10 29.0 +50 02 58.0 350.0

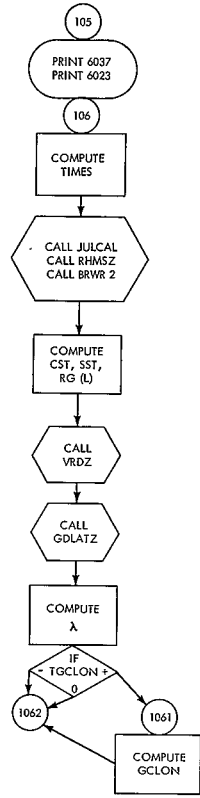
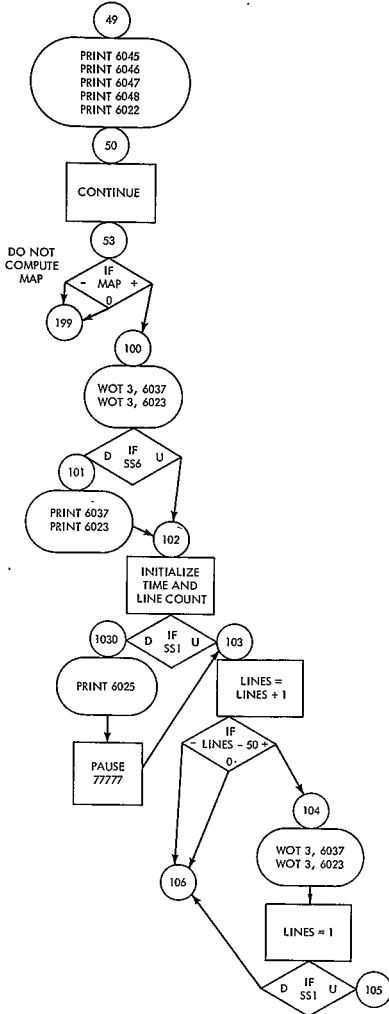
APPENDIX IV

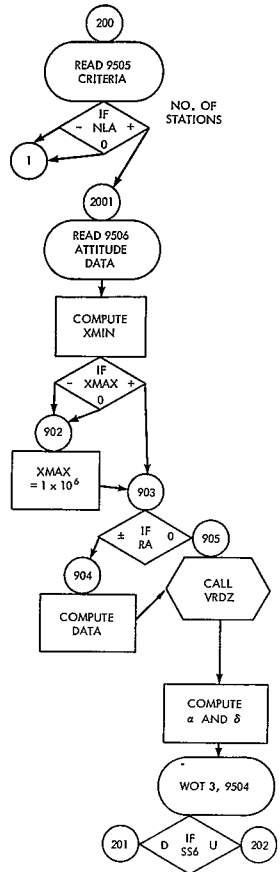
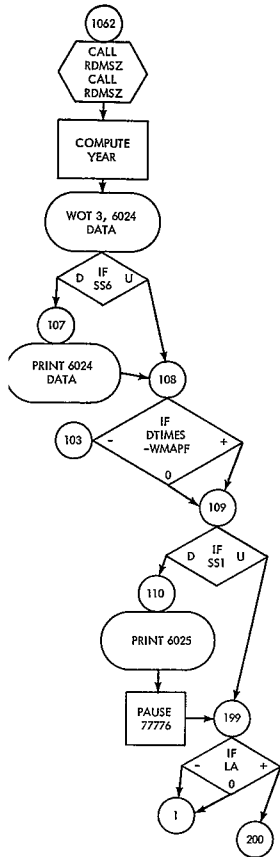
FLOW CHART FOR MAIN PROGRAM TWO

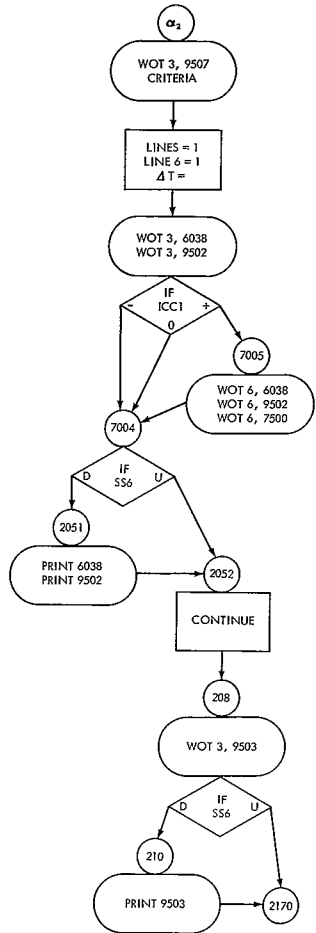
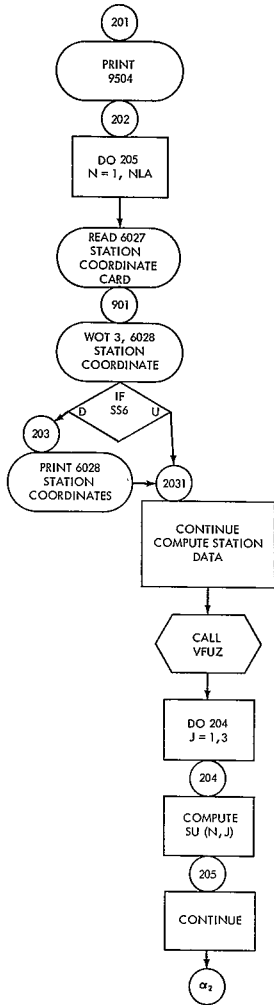


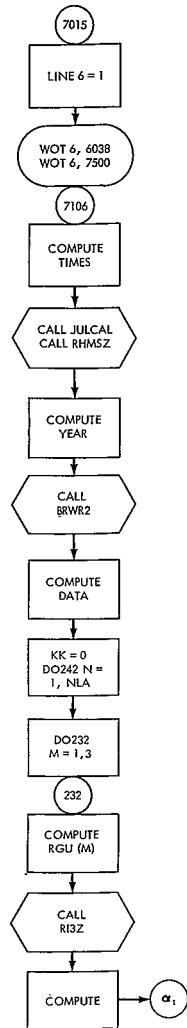
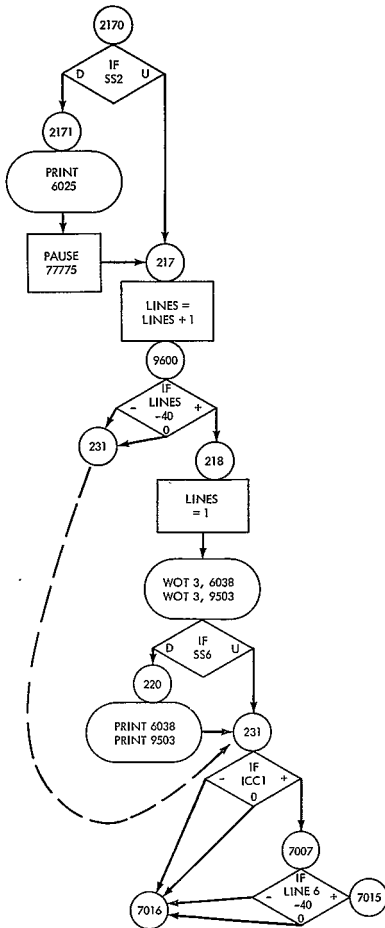


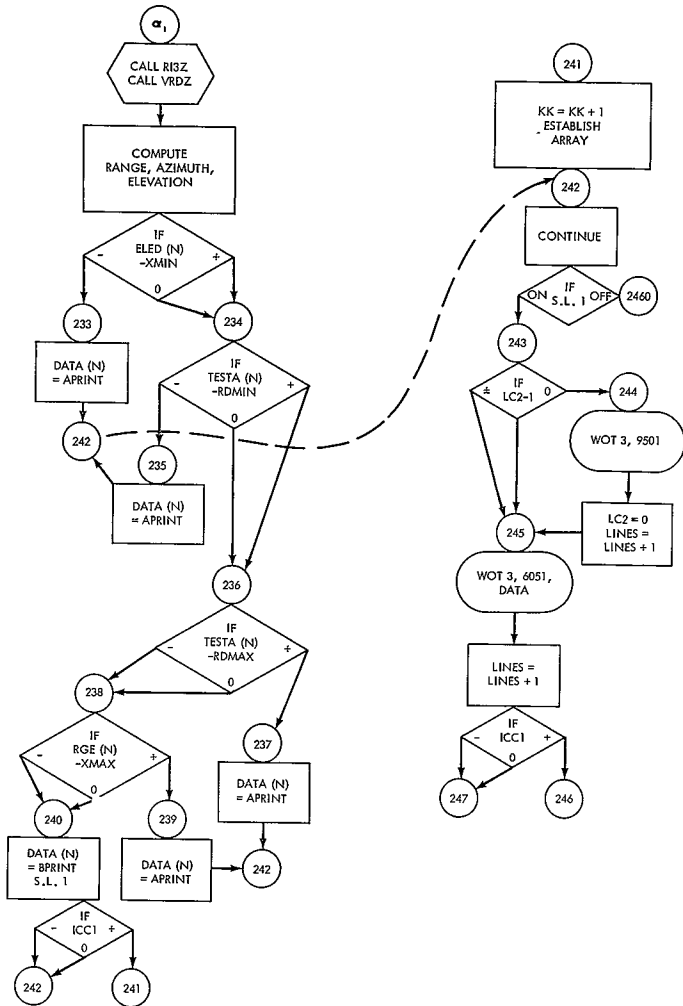


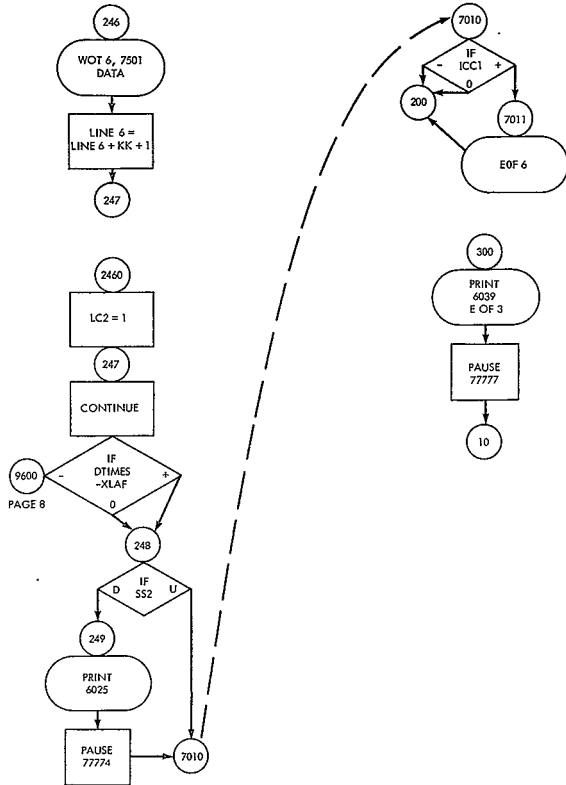












APPENDIX V
SOURCE DECK FOR MAIN PROGRAM ONE

```

*      DATE 9/6/65
*      C N RPPASC
*      DATE
*      CARD# COLUMN
*      LIST#
*      LABEL
*      MUSTAP PROGRAM VERSION 2 THEORY AND ANALYSIS OFFICE - GSFC
C
C      GENERALIZED WORLD MAP AND LOCAL STATION PREDICTIONS PROGRAM.
C
C      1A. CONVERTS OSCILLATING ORBITAL ELEMENTS TO INERTIAL POSITION
C           AND VELOCITY RECTANGULAR COORDINATES.
C      1B. CONVERTS INERTIAL POSITION AND VELOCITY RECTANGULAR
C           COORDINATES TO OSCILLATING ORBITAL ELEMENTS.
C      2.  COMPUTES WORLD MAP ON REQUEST.
C      3.  COMPUTES LOCAL STATION PREDICTIONS (LOOK ANGLES) ON REQUEST.
C
C      ALL INTERNAL CALCULATIONS ARE PERFORMED USING THE KILOMETER AS
C      THE UNIT OF LENGTH AND THE SECOND AS THE UNIT OF TIME. IF ANY
C      OF THE OPTIONAL INPUT PARAMETERS ARE DEFINED IN OTHER UNITS,
C      THEY ARE CONVERTED TO THESE UNITS AS SOON AS THEY ARE READ IN
C      AND ARE SUBSEQUENTLY USED IN THE CALCULATIONS IN KILOMETERS
C      AND SECONDS.
C
C      THE ORBIT REQUIRED FOR THE WORLD MAP AND LOCAL STATION PREDICTIONS
C      IS GENERATED BY SUBROUTINES BRW1 AND BRW2 (DIRK BRUGER -
C      SOLUTION OF THE PROBLEM OF ARTIFICIAL SATELLITE THEORY WITHOUT
C      MAPS)
C
C      REQUIRED SUBROUTINES AND FUNCTIONS
C
C      ALLOT
C      ALLOTZ
C      ARKTAN
C      ATANQ
C      ATAN7
C      RACS
C      GRGRN
C      RRWR1
C      RRWR2
C      CH65C
C      DJUL
C      DMSR2
C      DNTZ
C      FLRV
C      FLRVZ
C      FQN
C      GASTZ
C      GDLATZ
C      HNSPZ
C      JULCAL
C      PARA
C      PM6Z
C      RM6Z
C      RVFZ
C      R137
C      TFSOV
C      TIMFC
C      TIMF4
C      STASH
C      SIN
C      VFI7
C      VPD7
C      XKFP
C      XKFPZ
C
C      Z END OF NAME OF FUNCTION OR SUBROUTINE INDICATES THAT INPUT,
C      OUTPUT, AND INTERNAL ARITHMETIC ARE PERFORMED IN DOUBLE PRECISION.
C
C      DEFINITION OF SYMBOLS
C
C      ERR = TRUNCATION FACTOR (IN RADIANS) USED IN SOLUTION OF
C      KPFLR5 EQUATION
C      GM = PRODUCT OF G (=GAUSSIAN CONSTANT SQUARED) AND M, THE MASS OF
C      THE EARTH, IN UNITS OF KM. CUBED/SEC SQUARED
C      FJ2=J2 )
C      FJ3=J3 ) HARMONICS OF EARTH'S GRAVITATIONAL POTENTIAL
C      FJ4=J4 ) (DIMENSIONLESS)
C      FJ5=J5 )
C      FL=INVERSE OF FLATTENING
C      RE= EQUATORIAL RADIUS OF EARTH IN KM.
C
C      SENSE SWITCH 6 IS USED IN THE MAIN PROGRAM TO PROVIDE AN OPTION TO
C      GET THE INPUT PRINTED ON LINE.
C
C      ALL FORMATS USED IN PROGRAM FOLLOW IMMEDIATELY.
C
C      6002 FORMAT (12A6)
C      6003 FORMAT (8I3,F10.1)
C      6004 FORMAT (E12.6,4E12.5/2F12.4)
C      6005 FORMAT (/ 1X1PE14.8,9X23H FFET PER NAUTICAL MILE//
C      1XDPF8.3,9X33H EQUATORIAL RADIUS OF EARTH IN KM /2XFS.1,11X22H IN
C      2VERSE OF FLATTENING/1X,1PE14.8,3X31H GM (KM, CUBED/SECONDS SQUARED

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```

C
C   TEST FOR 65K SFTTING.
5041 CALL CH65K(NP)
      IF(NW)5038,5042,5038
5038 PRINT 5040
      WRITE OUTPUT TAPE 3,5040
5040 FORMAT (15H0 NOTE TO OPERATOR / 72H PUT MACHINE IN 65K + REWIND AL
      1L TAPFS , AND START JOB FROM BEGINNING . )
      REWIND 1
      PAUSE 00010
      GO TO 5038
5042 IF(SFNSF LIGHT 2) 1,1
n 1 FRR=1,OF=8
      FRRB=1,OF=7
      ITAPP4 = 8
      LPAS = 0
      NPAG3 = 0
C
C   DEFINE TRUNCATION FACTORS FOR SUBROUTINE BRUNFR ( USED TO CONVERT
C   OSCILLATING FLPMENTS TO BRUNFR MFA4 ELEMNTS)
C
      NAD(1)=5,OF=4
      NAD(2)=5,OF=6
      NAD(3)=5,OF=6
      NAD(4)=5,OF=6
      NAD(5)=5,OF=6
      NAD(6)=5,OF=6
C
C   LCP=0
      LCP=0
      ICFD = 0
R   APRINT=60 60 60 60 60 60
R   RPRINT = 60 21 60 60 60 60
B   DPRINT = 60 05 60 60 60 60
R   FPRINT = 60 11 60 60 60 60
R   XRX = 74 77 77 77 77 77
      XNWT = 60B.
      NUMNUM = 0
      XST00 = 0.
      IZWI = 0
      DO 4002 I = 1,12
R4002 XHP(1) = 60452612760
C   ASSUMF VFHICLF STARTS OFF IN SHADOW
      IVA = 0
      IFCY = 0
      IFCM = 0
      IFSO = 0
      IFSH = 0
      IFSM = 0
C
C   DFFINF GENDARD EARTH CONSTANTS
C
      GM=3.986032F+5
      FJ2=1.4873F-3
      FJ3=-7.7E-6
      FJ4=-1.8F-6
      FJ5=0.0
      FL=298.15
      RF=6378.165
C
C   CARD 1 - READ IN I.D. CARD - ANY INFORMATION IN COLS. 2 - 72
C
      RFAD 6002,(XHFAD(1),I = 1,12)
C
C   CARD 2 - READ IN CONTROL CARD
C
      COLS. 1-3 TYPE OF INPUT (+03 = INERTIAL POSITION AND VELOCITY
      IN VANGUARD UNITS
      +01 = OSCILLATING ELEMENTS-CU AND RAD
      +04 = BRUNFR VFA4 FLPMENTS )
      COLS. 4-6 COMPUTE WORLD MAP AND PREDICTIONS - YES OR NO
      ( YES IF MAP=+XX, NO IF MAP=+00 OR -XX )
      COLS. 7-9 +XX ALWAYS
      COLS. 10-12 CHANGE EARTH CONSTANTS
      COLS. 13-15 CHANGE TRUNCATION FACTOR
      COLS. 16-18 BRUNFR TRUNCATION CONTROL
      COLS. 19-21 BLANK - USED INTERNALLY
      COLS. 22-24 NUMBER OF CONTROL STATIONS
      COLS. 25-34 MAXIMUM RANGE TEST VALUF NAUTICAL MILES
      READ 6003,INPUT,MAP,LA,NCST,NERR,NOA,IRC,I2CT,RGMA
C
C   I2CT IS THE NUMBER OF CONTROL STATIONS.
C   TEST - HAVE ALL CASES BEEN RUN - YES OR NO
C
      IF(I2CT - 19) 5034,5034,3010
3010 PRINT 5033,I2CT
      WRITE OUTPUT TAPE 3,5033,I2CT
5033 FORMAT(15H0YOU ARE USING 16,60H CONTROL STATIONS. THE PROGRAM CAN
      1ONLY HANDLE 19 STATIONS. )
      68 PAUSE 54321
      GO TO 68
5034 IF(1INPUT)300,300+2
C   IF INPUT=+00 OR -XX, ALL CASES HAVE BFEN RUN. GO TO 300 (END

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C
C TEST - CHANGE TRUNCATION FACTOR - YES OR NO
C
C 2 IF (NFRF) 4,4,3
C
C CARD 2A- (OPTIONAL) READ IN NEW VALUE OF TRUNCATION FACTOR IF
C NERR=+XX. IF NERR=+00 OR -XX, PROCEED TO NEXT
C OPTI@N TFST.
C
C 3 READ 6040,ERR
C
C TEST - CHANGE EARTH CONSTANTS - YES OR NO
C
C 4 IF (NCST) 5,11,10
C
C TO NEXT STEP.
C
C 5 IF (NCST+1) 7,6,7
C
C USE SJRY PACKAGE CONSTANTS IF NCST = -1
C
C 6 GM=3.9862688F+05
C FJ2=1.0F219F-03
C FJ3=-2.285F-06
C FJ4=-2.123F-06
C FJ5=-2.32F-07
C FL=297.0
C RF=6374.388
C GM T@ 11
C
C 7 IF (NCST+2) 9,8,11
C
C USE GODDARD EARTH CONSTANTS WITH HARMONICS = 0 IF NCST = -2
C
C 8 FJ2=0.0
C FJ3=0.0
C FJ4=0.0
C FJ5=0.0
C GM T@ 11
C
C USE INTERNATIONAL CONSTANTS WITH HARMONICS = 0 IF NCST = -3
C
C 9 GM=3.98626873F+5
C FJ2=0.0
C FJ3=0.0
C FJ4=0.0
C FJ5=0.0
C FL=297.0
C RF=6374.388
C GM T@ 11
C
C CARDS 2B AND 2C- (OPTIONAL) READ IN NEW SET OF EARTH CONSTANTS
C IF NCST=+XX.
C
C 10 READ 6004,GM,FJ2,FJ3,FJ4,FJ5,FL,RF
C
C CONVERT EARTH CONSTANTS
C
C 11 GP(1)=GM
C GP(2)=-.5*FJ2*RF**2
C GP(3)=-FJ3*RF**3
C GP(4)=-.375*FJ4*RF**4
C GP(5)=-FJ5*RF**5
C
C PRINT ALL QUANTITIES @4 @OUTPUT TAPP A3.
C
C 12 WRITE @OUTPUT TAPP 3,3089
C WRITE @OUTPUT TAPE ITAPP4,3089
C WRITE @OUTPUT TAPE 3,3087,(IXHFAD(1),I = 1,12)
C WRITE @OUTPUT TAPP ITAPP4,3087,(IXHFAD(1), I = 1,12)
C WRITE @OUTPUT TAPE 3,3089
C WRITE @OUTPUT TAPE 3,5025,(IXHFAD(1),I = 1,12)
3087 @FORMAT (////////// ?(21X6A6/))
3088 @FORMAT (1HP)
5025 @FORMAT (////////// 2(54X,6A6/))
WRITE @OUTPUT TAPE 3,3089
3089 @FORMAT (1H1)
WRITE @OUTPUT TAPP 3,3088
WRITE @OUTPUT TAPE ITAPP4,3088
WRITE @OUTPUT TAPE ITAPP4,3088
WRITE @OUTPUT TAPE 3,6005,(XNMFT,RE,FL,GM,FJ2,FJ3,FJ4,FJ5)
WRITE @OUTPUT TAPE ITAPP4,6005,(XNMFT,RE,FL,GM,FJ2,FJ3,FJ4,FJ5)
IF (SFNSF SWITCH 6) 13,915
C
C PRINT SAVE INFORMATION @N LINE IF SENSE SWITCH 6 IS DOWN.
C
C 13 PRINT 6002
C PRINT 6005,XNMFT,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
913 IF (NDA) 915,915,914
914 READ 6050, (DAN(N), N=1,6)
915 DA(1)=DAN(1)
DA(2)=DAN(2)
DA 916 N=3,6

```

```

916 NAI(N)=NAD(N)*0.917453292
IF (IRC) 917,917,918
917 IRC=50
CARD 4 - READ IN PARAMETERS
TAKES STANDARD EP0CH AND ELEMENT CARDS
ALL PARAMETERS USE STANDARD FORMAT (6E12,8)
918 READ 6006,IDSAT,NYE,NME,NDE,NHE,NMNE,TSE,NORBIT,(AI(N), N = 1,6)
NYE = 1900 + NYE
PRINT FP0CH AND INPUT OPTI0N 0N OUTPUT TAPF A3
15 WRITE OUTPUT TAPE 3,6010,NYE,NME,NDE,NHE,NMF,NMNE,TSF
WRITE OUTPUT TAPE ITAPE4,6010,NYE,NME,NDE,NHE,NMNE,TSE
IF (SFNSF SWITCH 6) 16,17
PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS 00WN
16 PRINT 6010,NYE,NME,NDE,NHE,NMNE,TSE
17 CONTINUE
READ THE FP0CH AND DRAG TERM. THE UNITS 0F THE DRAG TERM ARE
RADIAN5 PER CUT**2.
CHANGE DRAG TO RADIAN5 PER SECOND**2 BY DIVIDING BY 806.832**2.
READ 5028,IDG1,IDG2,IDG3,IDG4,IDG5,IDG6,ENZ
5028 FORMAT (7X,3I2,X,2I2,X,1I2,4X,E12.8)
CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
TO FP0CH UNIVERSAL TIME IN RADIAN5.
TIME0=HMSRZ(NHF,NMNE,TSE)
CONVERT EP0CH CALENDAR DATE TO FP0CH JULIAN DATE AT 0 HOURS
UNIVERSAL TIME.
NJO=NJUL(NME,NDF,NYE)
CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
TO SFC0NDS.
THF=NHF*3600
TMNF=NMNF*60
TSFP=THF+TMNF+TSE
GO TO (18,1,22,930), INPUT
18 WRITE OUTPUT TAPF 3,6012
INPUT OPTI0N 1 - OSCILLATING ELEMENTS IN VANGUARD UNITS AND RADIAN5
WRITE OUTPUT TAPE ITAPE4,6012
WRITE OUTPUT TAPE 3,6051
WRITE OUTPUT TAPE ITAPE4,6051
WRITE OUTPUT TAPE 3,6011, (AI(N),N = 1,6)
WRITE OUTPUT TAPF ITAPE4,6011,(AI(N),N = 1,6)
IF (SFNSF SWITCH 6) 19,3002
19 PRINT 6012
PRINT 6051
PRINT 6011, (AI(N),N=1,6)
GO TO 3002
PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTI0N 3
INERTIAL POSITION AND VELOCITY RECTANGULAR COORDINATES -
IN VANGUARD UNITS.
22 WRITE OUTPUT TAPE 3,6009
WRITE OUTPUT TAPE ITAPE4,6009
WRITE OUTPUT TAPE 3,6011,(AI(N),N=1,6)
WRITE OUTPUT TAPE ITAPE4,6011,(AI(N),N = 1,6)
IF (SFNSF SWITCH 6) 23,28
PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS 00WN
23 PRINT 6000
PRINT 6011,(AI(N),N=1,6)
GO TO 24
PRINT INPUT PARAMETERS - INPUT OPTI0N 4 - BROUWER MEAN ELEMENTS
930 WRITE OUTPUT TAPE 3,6051
WRITE OUTPUT TAPE ITAPE4,6051
931 WRITE OUTPUT TAPE 3,6011,(AI(N),N = 1,6)
WRITE OUTPUT TAPE ITAPE4,6011,(AI(N),N = 1,6)
IF (SFNSF SWITCH 6) 932,3002
PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS 00WN
932 PRINT 6051
PRINT 6011,(AI(N),N = 1,6)
CONVERT TO KM AND DGRFFS
N0002 A1(1) = A1(1) * 6378.388
AAMA = A1(4) * 57.2957795130823
A1(4) = A1(6) * 57.2957795130823
A1(5) = A1(5) * 57.2957795130823
A1(6) = AAMA * 57.2957795130823

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```

C
C      CONVERT INPUT PARAMETERS TO OSCILLATING ELEMENTS
C
C 28 CALL PARA(INPUT,AT+A,GN)
5027 FORMAT(13HODRAG EFFECTS ,6X,7H(P,0),8X,7H(N(2,0),9X,7H(N(3,0)
      1 14X,2(X,3)2),2(3X+E15,8)
      WRITE OUTPUT TAPE ITAPE4,5027,1DG1,1DG2,1DG3,1DG4,1DG5,1DG6,EN2
      WRITE OUTPUT TAPE          3,5027,1DG1,1DG2,1DG3,1DG4,1DG5,1DG6,EN2
n
n      FN2 = FN2 / 806.832**2
D      CALL FLRVZ(RX,VX,A,PER,FM,GM,ERR)
      CALL BRNR(DA,A,IRC,MN)
n
n      VX(1)=VX(1)
n      VX(2)=VX(2)
n      VX(3)=VX(3)
      FN=S*(1)
      DP=S*(2)
      DN=S*(3)
n
n      PFR=6.2831853*718/EN
n      PFRM=PFR/60.0
n      PFRH=PFR/3600.0
n      FN1=FN*206264.806247096
n      DN*PFR=DN*4950355.3499303
n      DN*PFR1=DN*4950355.3499303
C
C      TFST = 14 WRPLD MAP DFS1PFD
C
C
C 29 IF (MAP) 30,30,33
30 WRITE OUTPUT TAPE 3,6014
      IF (SFNSF SWITCH 6) 31,36
C
C 31 PRINT 6014
32 GO TO 36
33 CONTINUE
C
C
C 36 CONTINUE
C
C      CARD 10 - STATION PREDICTIONS AND WORLD MAP ARE REQUIRED, READ
C      CALENDAR DATE AND UNIVERSAL TIME AT WHICH THE START
C      OF THE CALCULATION IS DESIRED, CALENDAR DATE AND
C      UNIVERSAL TIME AT WHICH THE TERMINATION OF THE
C      CALCULATION IS DESIRED, AND THE DESIRED TIME INCREMENT
C      OF THE CALCULATION IN SECONDS.
C
C 40 WRITE OUTPUT TAPE 3,6018
      WRITE OUTPUT TAPE ITAPF4,6018
C
C      PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
C      IF (SFNSF SWITCH 6) 41,42
C 41 PRINT 6018
C 42 CALL TIME4(IDJ0,TSEP,XLAS,XLAF,DTLA)
C
C      PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
C 43 CONTINUE
C
C      CONVERT OSCILLATING ORBITAL ELEMENTS TO INERTIAL POSITION AND
C      VELOCITY CORONATES IN KM AND KV/SEC
C
C 46 CALL FLRVZ(RX,VX,A,PER,EN,GM,ERR)
      R1=SQRT(RX(1)**2+RX(2)**2+RX(3)**2)
      V1=SQRT(VX(1)**2+VX(2)**2+VX(3)**2)
C
C      CONVERT TO VANGUARD UNITS OF LENGTH AND VELOCITY
C
C 47 X01=RX(1)/6378.388
n      X02=RX(2)/6378.388
n      X03=RX(3)/6378.388
n      V01=VX(1)/7.9054722668
n      V02=VX(2)/7.9054722668
n      V03=VX(3)/7.9054722668
n      P2=SQRT(X01**2+X02**2+X03**2)
n      V2=SQRT(V01**2+V02**2+V03**2)
C
C      CONVERT ANGLFS (RADIAN) TO ANGLFS (DEGREES)
C
C      A01=A(1)
n      A02=A(2)
n      A03=A(3)*57.2957795130923
n      A04=A(4)*57.2957795130923
n      A05=A(5)*57.2957795130923
n      A06=A(6)*57.2957795130923
n      R1=110(1)
n      R2=110(2)
n      R3=110(3)*57.2957795
n      R4=110(4)*57.2957795
n      R5=110(5)*57.2957795
n      R6=110(6)*57.2957795
C
C      BEGIN LOCAL STATION PREDICTIONS CALCULATION

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200 IF(IIRD)13001,3000,3001
3000 READ 9505,NLA,ICCL1,MINV,XMAX,MUTE
      IRFD = 5
      IF(NLA - 18) 73,73,70
70 PRINT 71,NLA
   WRITE OUTPUT TAPE 3,71,NLA
71 FORMAT(16H0 YOU ARE USING 19,
          1 47H STATIONS. PROGRAM CAN ONLY HANDLE 19 STATIONS.
72 PAUSE 66666
   GO TO 72
C   WIDE PAPER FORM IF MBRF THAN 15 STATIONS ARE USED
73 IF(NLA - 15) 60,60,61
60 NLSPP = 40
   GO TO 62
61 NLSPP = 58
62 IF (NLA) 1,1,2001
C   MAKE ISVEL POSITIVE IF SPIN AXIS IS ALONG INERTIAL VELOCITY VECTOR
2001 READ 9506,RDMAX,RDMIN,RA,DEC,ISVEL
C   STORE BLANKS
      IF(NLA - 12CT) 5035,5037,5037
5035 PRINT 5036
      WRITE OUTPUT TAPE 3,5036
5036 FORMAT(72H0THE NUMBER OF CONTROL STATIONS IS LARGER THAN THE NUMBE
          1FR OF STATIONS.
67 PAUSE 54333
   GO TO 67
5047 IF(NLA - 18) 5004,5004,5006
5004 NFL = (NLA*2) + 7
      DR 5005 I = NFL,44
5005 MUV(1) = APRINT
5006 CONTINUE
      XMIN=MINV
      XMAX = RGMA * XMMET * 0.30480061F-03
      903 IF(ISVEL)905,904,905
n904  RAR=RA*,0176532925
n     DECR=DFC*.0176532925
n     VXF(1) = COSF(DFCR) * COSF(IRAR)
n     VXF(2) = COSF(DFCR) * SINF(IRAR)
n     VXF(3) = SINF(DFCR)
      GO TO 5026
D905  CALL VRD(1,VXF+DECR,RAR,XXX)
      S4= RAR*57.2957795
      DFC=DFCR*57.2957795
5026 WRITE OUTPUT TAPE 3,9504
      IF (SFNSF SWITCH 6) 201,202
201 PRINT 9504
202 DR 205 N1,NLA
      READ 6027,STAT(N),STAT1(N),LOND,LONM,XLONS,LATD,LATM,
          1 XLATS,HGT
901 WRITE OUTPUT TAPE 3,6028,STAT(N),STAT1(N),LOND,LONM,XLONS,LATD,
          1LATM,XLAT5,HGT
      IF (SFNSF SWITCH 6) 203,2031
203 PRINT 6028,STAT(N),LOND,LONM,XLONS,LATD,LATM,XLAT5,HGT
2031 CONTINUE
D     C@ORD(1)=DMSRZ(LATD,LATM,XLAT5)
D     C@ORD(2)=DMSRZ(LOND,LONM,XLONS)
D     C@ORD(3)=HGT/1000.0
D     RLAT(N)=C@ORD(1)
n     RLON(N)=C@ORD(2)
D     CALL VFUZ(C@ORD,RE,FL,U)
      DR 204 J=1,3
204 SU(N,J)=U(J)
705 CONTINUE
      N = 1
      IF(12CT) 3095,3095,3094
3094 N= 17CT
3095 WRITE OUTPUT TAPE 3,3093,(STAT(J),STAT1(J),J = 1,N)
      WRITE OUTPUT TAPE 1TAPE4,3093,(STAT(J),STAT1(J), J = 1,N)
3093 FORMAT(//15X21H CONTROL STATIONS ARE /+4(20X23/1)
          WRITE OUTPUT TAPE 3,9507,MINV,MINV,RGMA
          WRITE OUTPUT TAPE 3,3013,RA,DEC
          WRITE OUTPUT TAPE 1TAPF4,3091
3091 FORMAT(54H0 5 IS PRINTED WHEN THE SATELLITE IS IN THE SUNLIGHT )
          WRITE OUTPUT TAPE 3,3092
3092 FORMAT(80H0 THE 3 DIGIT NUMBERS UNDER THE STATION NAMES ARE THE 5
          1P4CFRCRAFT LOOK ANGLES.
          )
C
C   INITIALIZE LINE COUNT AND DELTA T (DIFFERENCE BETWEEN
C   LOCAL STATION PREDICTIONS STARTING TIME AND EPOCH OF INPUT
C   PARAMETERS IN SECONDS)
C
C   3001 LINF5 = 1
C       LINF6=1
D       DTIMF5=XLAS-DTLA
C
C
C   2170 IF (SFNSF SWITCH 2) 2171,217
C   2171 PRINT 6025
C       PAUSE 77775
C   217 LINF5=LINF5+1
C
C   SKIP A PAGE AND PRINT HEADING IF 50 LINES OF CALCULATION

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C      HAVF BFFN PPINTED
C
0601 JJ = 1
      NPPRFD = 0
      LIN11 = 0
      LIN12 = 0
      IALAX = 0
      IMRS = '2767'
0600 CONTINUE
07016 DTIMES = DTIMES + DTLA
D      TIME=TIME0+DTIMES*0.727220521664304E-4
D      DDJO=INT( TIME/6.283185307179586)
D      DJ=DDJO*DJ0
D      TIME=ALLDTZ(TIME)
C
C      COMPUTE GFRENWICH APPARENT SIDEREAL TIME AT TO + DELTA T
C
D      UT = TIME * 2.81071863471
D      FOR = FON(DJ,UT,XDX,XDX,FCOM)
D      ST = GAST7(DJ,UT,EOR)
D      CALL JULCAL(DJ,NR,ND,NY)
C
C      CONVERT UNIVERSAL TIME IN RADIANS TO HOURS, MINUTES, AND SECONDS
C
D      CALL RHP5Z(TIME,II,II,14,TS)
D      NYM19=NY-1900
C
D      CALL RRWR2(DTIMES,ENZ)
D      CST=SIGN(*T)
D      RR(1)=RXR(1)*FCST+RXR(2)*SST
D      RG(2)=RXB(2)*CST-RX(1)*SST
D      RG(3)=RXB(3)
D      CALL VRN2(1,RG,GCLAT,GCLON,R)
C
C      COMPUTE GEOPTIC LATITUDE OF SUBSATELLITE POINT
C
D      GDLAT = GDLATZ(GCLAT,R,RE,FL,ALTT)
C
C      COMPUTE HEIGHT OF SATELLITE ABOVE COMPUTATIONAL ELLIPSOID ALONG
D      NORVAL FROM SATELLITE TO FLLIPSOID
C
C      CONVERT LATITUDE AND LONGITUDE IN RADIANS TO DEGREES, MINUTES,
D      AND SECONDS
C
D      TGCLON=GCLON-3.141592653589793
D      IF (TGCLON) 1062,1062,1061
01061 GCLON=TGCLON-3.141592653589793
C
01062 CONTINUE
C      TEST FOR VEHICLE IN SUNLIGHT
C      AN S WILL BE PRINTED IF IN SUNLIGHT
D      IFFSNSF LIGHT 2) 3000,3011
03011 CALL SUN(DJ,TIME,SLC)
D      SLC = SLC - 0.99241E-04
D      CFCO = COS(FCOM)
D      SFCO = SIN(FCOM)
D      SSLC = SIN(SLC)
C      COMPUTE COMPONENTS OF SUN
D      XSU = COS(SLC)
D      YSU = SSLC * CFCO
D      ZSU = SCLC * SFCO
D      RINTO = RXB(1)**2 + RXB(2)**2 + RXB(3)**2
D      RINT = SORTF(RINTO)
D      IF(RINT)3015,3015,3016
3015 IFR = 0
D      PRINT 3024,IFR,1
3024 FORMAT(2I6)
D      GO TO 3007
3016 CPSI = (XSU*RXB(1) + YSU*RXB(2) + ZSU*RXB(3)) / RINT
3017 IFCPSI)3005,3006,3006
3005 DFMX = RINTO - RF**2
D      DFMX = SORTF(DFMX)
D      IF(DFMX)3018,3018,3019
3018 IFR = 1
D      PRINT 3024,IFR,1
D      GO TO 3007
03019 TNN = RF / DFMX
D      CALL ARKTAN(RE,DFMX,XNU,1)
D      SPS1 = 1.-CPSI**2
D      IFCPSI)3020,3021,3021
3020 IFR = 2
D      PRINT 3024,IFR,1
D      GO TO 3007
3021 SPS1 = SORTF(SPS1)
D      CPS1 =-CPS1
D      CALL ARKTAN(SPS1,CPS1,PSVA,1)
D      X90DG = 1.5707963
D      GULX = X90DG - PSVA
D      TFNN = GULX + XNU - X90DG
D      IF(TFNN) 3006,3006,3007
R3006 SUNN = 62 60 60 60 60 60

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      IGRD = 2
C     VFHICLF IN SUN
      NUMSUN = NUMSUN + 1
      GR TO 3008
93007 SUNN = 60 60 60 60 60 60
      IGRD = 1
C     VFHICLF IN SHAD0W
93008 CONTINUF
      IF(1VA) 3026,3025,3026
9025 IVA = 2
      DTFSH = DTIMFS
      GR TO 3030
      3026 IF(IIGR - IGRM)3027,3030,3028
9027 IFSY = NY419
      IFSM0 = NV
      IFSN = ND
      IFSM = IH
      IFSM = IV
      DTFSH = DTIMFS
      GR TO 3030
93028 PERCENT = 100. - (DTIMFS - DTFSH) / (36. * PPRH)
      DRAT = DTIMFS - DTESH) / 60.
      WRITE OUTPUT TAPE 5,3029,IESY,IESM0,IESD,IFSH,IESM,NY19,NY,ND,
      IIM,IM,DRAT,PERCENT
9029 FORMAT (5X,312,X,212,13X,312,X,212,5X,FT,1,11X,FT,2)
9031 FORMAT(11H,20X,22H SUNLIGHT HISTORY OF A5//5X63HSATELLITE WILL BE
      11N SUNLIGHT AT ALL TIMFS EXCEPT WHEN IT WILL /5X,
      24DHNTFR SHAD0W AT AND LEAVE SHAD0W AT /5X,
      37SHYMNDD HHHM          YMNDD HHHM DURATION (MIN) PERCENT IN
      4, SUNLIGHT )
9030 IGRM = IGRD
C
      IF(XS700)3070,3069,3079
3069 XGLAST = GDLT
      GR TO 3074
9070 IF(GDLAT)3073,3071,3071
3071 IF(XGLAST)3072,3073,3073
3072 NDRAT = NDRAT + 1
3073 XGLAST = GDLAT
9074 XS700 = X5700 + 1.
      IF(IJJ - 113078,3077,3078
9077 IGRDPR = NDRAT
9078 CONTINUF
      IF(XS700 - 300.)3064,3063,3063
9063 X5700 = 1.
      PRINT 5050,NY419,NM,ND,IH,IV
9050 FORMAT(3X,312,2X,212)
3064 KK = 0
      N0 3081 I = 1,19
9081 XPESTA(I) = APRINT
      N0 247 N=1,NLA
      N0 232 M=1,5
      N 232 QGU(M)=RG(M)-SU(N,M)
      N CALL R13Z(RTX,0,-ST,QGU)
      N NUPC=NR7(RTX,XX)
      N TESTA(N)=NUM*57,295780
      N R13A1=1,57079632679-RLAT(N)
      N R13A2=1,57079632679+RLON(N)
      N CALL R13Z(I,R13A1,R13A2,RGU)
      N CALL WRZ(I,2,2,ELEVAT,AZ,INUT,RANG)
      N FLFD(N)=57,29578*ELEVAT
      N AZID(N)=57,29578*AZINUT
      N RGF(N)=PANG
      N DATA(N) = PRINT
      N IF(FLFD(N))1293,319,318
318 IF(FLFD(N) - 5,0) 319,321,320
319 DATA(N) = PRINT
      GR TO 238
320 IF(FLFD(N) - 10,1321,238,238
321 DATA(N) = PRINT
328 IF(RGF(N) - XMAX)239,239,902
233 DATA(N) = APRINT
      GR TO 242
      N 902 DATA(N) = DATA(N) + (- XRRX)
      N 240 IDATA = APRINT
3004 QNSF LIGHT 1
4009 FRRMAT (1515,F16,8)
4001 FRRMAT (4F16,8,215)
322 IF(NPRFD) 241,310,241
310 N0 3009 III = 1,12CT
      INAT = DATA(III)
      IF(IIDAT - IDATA)311,3009,311
9009 CONTINUF
      GR TO 241
311 NPRFD = 1
241 KK = KK + 1
      IF(IALAX - 1) 3061,3061,3062
9061 IALAX = KK
9062 CONTINUF
      XRG(KK) = RGF(N)
      XAZ(KK) = AZID(N)
      XFL(KK) = FLFD(N)

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Y0(KK) = TFSTA(N)
STAT3(KK) = STAT(N)
STAT4(KK) = STAT1(N)
IN(KK) = N
IZ(KK) = TFSTA(N)
242 CONTINUE
C CONVERT S/C ANGLE TO BCD
I*(KK)3090,3090,3082
3082 DO 3083 I = 1,KK
CALL TFSCBVI(IZ(I),XZ(I))
3083 CONTINUE
DO 3085 I = 1,KK
INVA = IN(I)
3085 XSTAT(INVA) = XZ(I)
3090 GCLN = GCLRN * 57.29577951
N GOLT = GDLAT * 57.29577951
243 IF (SPNSF LIGHT 1) 243,2460
244 LC2 = 0
245 JJ = JJ + 1
17NJ = 10
C SFT HP WPIV APPRY
WPIV(1) = NY*19
UPIV(2) = NY
WPIV(3) = ND
WPIV(4) = IH
WPIV(5) = IM
VPIV(6) = NFRQIT
DO 5003 I = 1,NLA
NXD = (I*2) * 5
WPIV(NXD) = XSTAT(I)
NXD = NYD + 1
5003 WPIV(NXD) = DATA(I)
C STORF WPIV
IPRS = 12900 - LIN11 * 44
IF (IPRS - 44)5019,5021,5021
5019 DTIMFS = DTIMFS - DTLA
SFNSF LIGHT 3
GO TO 2460
5021 CALL STASH(WPIV+44,IPRS)
IF(MAP)3079,3079,3080
C SFT HP FOR 65 K.
3080 PRF(1) = KK
PRF(2) = STAT3(I)
PRF(3) = STAT4(I)
PRF(4) = XPG(I)
PRF(5) = XZ(I)
PRF(6) = XFL(I)
PRF(7) = XR(I)
PRF(8) = GOLT
PRF(9) = GCLN
PRF(10) = ALIT
PRF(11) = SINW
LIN12 = LIN12 + 1
NXD = 11
IF(KK - 1)5002,5002,5000
5000 DO 5001 K = 2,KK
NXD = (K*7) - 2
PRF(NXD) = STAT3(K)
NXD = NXD + 1
PRF(NXD) = STAT4(K)
NXD = NXD + 1
PRF(NXD) = XRG(K)
NXD = NXD + 1
PRF(NXD) = XAZ(K)
NXD = NXD + 1
PRF(NXD) = XFL(K)
NXD = NXD + 1
PRF(NXD) = XR(K)
NXD = NXD + 1
5001 PRF(NXD) = SINW
5002 IF(IMBS - 12090 - NXD) 5020,5022,5022
5020 DTIMFS = DTIMFS - DTLA
LL11 = LL11 - 1
SFNSF LIGHT 4
GO TO 2460
C STORF PRF
5022 CALL STASH(PRF+NXD,IMPS)
IMPS = IMPS - NXD
IX = IX + 1
3051 FFORMAT (13X,2A3,F9.1,2F6.1,F7.1,5A6)
3070 LIN11 = LIN11 + 1
GO TO 247
2460 IF(INLA - 1)3059,3060+63
63 IF(IMUTF)313,5031,313
5031 IF(IJLAK - 1)3059,3059+3060
3060 IF(INPRE)313,3059,313
313 JWX = JJ - 1
LPAS = 10
WRITE OUTPUT TAPE 3,3076,1BG5RB
3076 FFORMAT (1H1,27X,13H ORBIT NUMBER 16)
WRITE OUTPUT TAPE 3,330,1NSAT

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      LL11 = 2
      LASORR = JRGORB
C   RETURN WPUV
      DR 3054 K = 1,LL11
      LOK = I2000 - (K-1) * 44
      CALL BACK(WPUV,44,LOK)
      DA 5007 I = 1,5
5007 MVI(1) = WPUV(1)
      IF(LL11 = 2) 5032,64,5032
      64 IF(NPAG2)65,5029,65
      65 NPAG3 = 0
      LL11 = LL11 + 1
      MVI(7) = WPUV(6)
      WRITE OUTPUT TAPE 3,66,MVI(7)
      66 FORMAT (2RX,13H ORBIT NUMBER I6 )
5029 WRITE OUTPUT TAPE 3,5030,MVI(2),MVI(3),MVI(1)
5030 FORMAT (2RX,18H DATE(HH,MM,YY) = 2(12,1H),12)
      WRITE OUTPUT TAPE 3,331,(STAT(1)),I = 1,4LA)
5032 MVI(7) = WPUV(6)
      IF(LASORR = MVI(7)) 5016,5017,5017
5016 LASORR = MVI(7)
      WRITE OUTPUT TAPE 3,5018,LASORR
      WRITE OUTPUT TAPE ITAPF4,5018,LASORR
5018 FORMAT (1H0,27X13H ORBIT NUMBER I6)
      WRITE OUTPUT TAPE 3,4006,APRINT
      LL11 = LL11 + 3
      LL12 = LL12 + 2
5017 NFND = (NLA*2) + 6
      WRITE OUTPUT TAPE 3,6052,(MVI(1)),I = 4,5),(MVI(1)),I = 7,NEND)
      IF(MAP) 5014,5014,102
      102 LINF4 = 1
      IF(K-1) 5009,5008,5009
5008 IMOS = 32767
      WRITE OUTPUT TAPE ITAPF4,3076,IBGORB
      WRITE OUTPUT TAPE ITAPF4,332,IDSAT
      LL12 = 3
5009 CALL BACK(PRF,11,IMOS)
C   RETURN PRF
      IMOS = IMOS - 11
      MVI(6) = PRF(1)
      WRITE OUTPUT TAPE ITAPF4,4006,APRINT
      4006 FORMAT (114X,A6)
      WRITE OUTPUT TAPE ITAPF4,323,(MVI(K),K = 1,5),(PRE(K),K = 2,11)
      LL12 = LL12 + 2
      IF(LL12 = 40) 5024,5024,5023
5023 WRITE OUTPUT TAPE ITAPF4,3076,MVI(7)
      WRITE OUTPUT TAPE ITAPF4,4005
      LL12 = 3
5024 IF(MVI(6) - 1) 5014,5014,5010
5010 IPPP = MVI(6)
      DR 3056 I = 2,IPPP
      CALL BACK(PRF,7,IMOS)
      IMOS = IMOS - 7
      WRITE OUTPUT TAPE ITAPF4,3051,(PRF(K), K = 1,6)
      LINF2 = LINF2 + 1
      LL12 = LL12 + 1
      IF(LL12 = 40)3056,3056,4004
4004 WRITE OUTPUT TAPE ITAPF4,3076,MVI(7)
      WRITE OUTPUT TAPE ITAPF4,4005
4005 FORMAT ( 20XSHRANG,4X,4HAZ1,2X,5HELEV,2X,8HSC/L 00K,2X,4HLAT,
      1,2X,5HLONG,2X6HFHEIGHT /
      210H YYMMDD HHHM STAT,3X,4H(K),4X,35H-----DEGREES-----
      3-----,3X,4H(K) )
      LL12 = 2
3056 CONTINUE
5014 LL11 = LL11 + 1
      IF(LL11 = NLSPP) 3054,3054,4003
4003 WRITE OUTPUT TAPE 3,3089
      LL11 = 2
      NPAGF = 10
3054 CONTINUE
      WRITE OUTPUT TAPE 3,9501
      WRITE OUTPUT TAPE ITAPF4,9501
      LC2 = 3
C
C   PUT SENSF SWITCH 3 DOWN TO TERMINATE RUN BEFORE THE END TIME.
C
      IF(SFNSF SWITCH 3)5012,3059
3059 CONTINUE
      323 FORMAT I,X,3I2,X,2I2,X,2A3,F9.1,2F6.1,F7.1,F10.1,F7.1,F9.1,X,A3)
      332 FORMAT (15H LOCAL STATION PREDICTIONS AND SATELLITE WORLD MAP FOR
      1A5/20XSHRANG,4X,4HAZ1,2X,5HELEV,2X,8HSC/L 00K,2X,4HLAT,2X,
      25HLONG,2X6HFHEIGHT /
      310H YYMMDD HHHM STAT,3X,4H(K),4X,35H-----DEGREES-----
      4-----,3X,4H(K) )
      317 IF(OTIMFS = XLAF)9601,248,248
      247 CONTINUE
      IF(OTIMFS = XLAF) 9600,5015,5C15
      5015 IF(LL11 = 2) 1,248,248,2460
      248 IF (SFNSF SWITCH 2) 249,7C10
      249 PRINT 6025
      PAUSE 77774

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```

7010 IF(LPAS) 5012,5011,5012
5011 LPAS = 10
    GO TO 2460
5012 JMX = 9
    WRITE OUTPUT TAPE ITAPF4,3031,IDSAT
    WRITE OUTPUT TAPE 5,3032,JMX
    FND FILE 5
    RETURN 5
3033 READ INPUT TAPF 5,3032,JMX,(SA(I),I = 1,12)
3032 FORMAT (11,11(A6),A3)
    IF(JMX - 9)3036,3035,3034
3034 WRITE OUTPUT TAPE ITAPF5,3036,(SA(I),I = 1,12)
3036 FORMAT (11,11(A6),A3)
    GO TO 3033
3035 RETURN 5
    GO TO 3000
C
C
C
390 PRINT 6039
    FND FILE 3
    PAUSE 77777
    GO TO 10
    FND

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APPENDIX VI
SOURCE DECK FOR MAIN PROGRAM TWO

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* DATE 10/19/64
* GDR
* PAUSE
* XEQ
* CARDS COLUMN
* LIST8
* LABEL
* FORMAP
C HWAPLA
C
C GENERALIZED WORLD MAP AND LOCAL STATION PREDICTIONS PROGRAM.
C
C 1A. CONVERTS OSCILLATING ORBITAL ELEMENTS TO INERTIAL POSITION
C AND VELOCITY RECTANGULAR COORDINATES.
C 1B. CONVERTS INERTIAL POSITION AND VELOCITY RECTANGULAR
C COORDINATES TO OSCILLATING ORBITAL ELEMENTS.
C 2. COMPUTES WORLD MAP ON REQUEST.
C 3. COMPUTES LOCAL STATION PREDICTIONS (LOOK ANGLES) ON REQUEST.
C PROCESSES 1, 2, 3, OR 4 STATIONS SIMULTANEOUSLY ON REQUEST.
C
C ALL INTERNAL CALCULATIONS ARE PERFORMED USING THE KILOMETER AS
C THE UNIT OF LENGTH AND THE SECOND AS THE UNIT OF TIME. IF ANY
C OF THE OPTIONAL INPUT PARAMETERS ARE DEFINED IN OTHER UNITS,
C THEY ARE CONVERTED TO THESE UNITS AS SOON AS THEY ARE READ IN
C AND ARE SUBSEQUENTLY USED IN THE CALCULATIONS IN KILOMETERS
C AND SECONDS.
C
C
C REQUIRED SUBROUTINES AND FUNCTIONS
C
C ALLOT
C ALL0TZ
C ATANO
C ATANZ
C BRWR
C BRWR1
C BRWR2
C DJUL
C DMSRZ
C DOTZ
C ELRV
C ELRVZ
C F0N
C GASTZ
C GOLATZ
C HMSRZ
C JULCAL
C PARA
C RDMSZ
C RHMSZ
C RVELZ
C R13Z
C TIMEC
C VFUZ
C VRDZ
C XKEP
C XKEPZ
C
C Z END OF NAME OF FUNCTION OR SUBROUTINE INDICATES THAT INPUT,
C OUTPUT, AND INTERNAL ARITHMETIC ARE PERFORMED IN DOUBLE PRECISION.
C
C DEFINITION OF SYMBOLS
C
C ERR = TRUNCATION FACTOR (IN RADIAN) USED IN SOLUTION OF
C KEPLER'S EQUATION
C GM = PRODUCT OF G (=GAUSSIAN CONSTANT SQUARED) AND M, THE MASS OF
C THE EARTH, IN UNITS OF KM. CUBED/SEC SQUARED
C FJ2=J2 )
C FJ3=J3 ) HARMONICS OF EARTH'S GRAVITATIONAL POTENTIAL
C FJ4=J4 ) (DIMENSIONLESS)
C FJ5=J5 )
C FL=INVERSE OF FLATTENING
C RE= EQUATORIAL RADIUS OF EARTH IN KM.
C
C SENSE SWITCH 6 IS USED IN THE MAIN PROGRAM TO PROVIDE AN OPTIONAL
C OUTPUT ON LINE. IF SENSE SWITCH 6 IS DOWN, THE SAME INFORMATION
C WHICH IS PRINTED ON TAPE A3 IS ALSO PRINTED ON LINE. IF SENSE
C SWITCH 6 IS UP, OUTPUT IS PRINTED ON A3 ONLY.
C
C ALL FORMATS USED IN PROGRAM FOLLOW IMMEDIATELY.
C
C 6001 FORMAT (36HISANDTRACKS ORBITAL COMPUTING SYSTEM //)
C 6002 FORMAT (72H
C 1
C 6003 FORMAT (713)
C 6004 FORMAT (E12.6,4E12.5/2F12.4)
C 6005 FORMAT (/ IX1PE8.1,9X39H TOLERANCE REQUIRED FOR KEPZ SUBROUTINE//
C 1 X0PF8.3,9X39H EQUATORIAL RADIUS OF EARTH IN KM /2XF5.1,11X22H IN
C 2VERSE OF FLATTENING/1X,1PE14.8,3X31H GM (KM. CUBED/SECONDS SQUARED
C 3 /18X44H HARMONICS OF EARTH'S GRAVITATIONAL POTENTIAL /1XE19.6,
C 4 4X3H J2/1X,E13.6,4X3H J3/1X,E13.6,4X3H J4 /1X,E13.6,4X3H J5 )
C 6006 FORMAT (21X12,1X14,213,F7.3/6F12.6)
C 6008 FORMAT (/1X13,14X20H INPUT @PT10N NUMBER/18X24H INPUT PARAMETERS A

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1RF--- //)
6009 FORMAT /46H GEOCENTRIC EQUATORIAL RECTANGULAR COORDINATES/70H REQU
IRED UNITS - CENZY MIXED UP VANGUARD UNITS OF LENGTH AND VELOCITY/
6010 FORMAT // 1X12+1H/12+1H/14,7X29H EPOCH DATE OF PARAMETERS/21X12),
1 F7.3,5X29H EPOCH TIME OF PARAMETERS-UT2 )
6011 FORMAT /16X,F12.9, 20H X1 - VANGUARD UNITS/6X,F12.9, 3H X2/
1 6X,F12.9, 3H X3/6X,F12.9, 20H VX1- VANGUARD UNITS/6X,F12.9,
2 4H VX2/6X,F12.9, 4H VX3 )
6012 FORMAT /30H ORBITAL ELEMENTS - OSCULATING/69H PEQUIRED UNITS - ALL
1 ANGLES IN DEGREES/SEMI-MAJOR AXIS IN KILOMETERS )
6013 FORMAT // 2X/F11.4,5X,27H SEMI-MAJOR AXIS-KILOMETERS/6X,F11.8,
1 14H ECCENTRICITY/5X,F12.6,3X,12H INCLINATION/3X,9H -DEGREES/3X,
2 F12.6,3X,24H R.A. ASC. NODE -DEGREES/3X,F12.6,3X,24H ARG. OF PERI
3 GEE-DEGREES/3X,F12.6,3X,24H MEAN ANOMALY -DEGREES )
6014 FORMAT (/18X,25H NO WORLD MAP CALCULATION )
6016 FORMAT (/45H WORLD MAP CALCULATIONS - START AND END TIMES//)
6017 FORMAT (/18X,26H NO LOOK ANGLE CALCULATION )
6018 FORMAT (/46H LOOK ANGLE CALCULATIONS - START AND END TIMES//)
6019 FORMAT (/ 32H QUANTITIES COMPUTED FROM INPUT )
6020 FORMAT (/ 1X/F13.5,4X,16H X1 - KILOMETERS/1X,F13.5,4X,3H X2/1X,
1 F13.5,4X,3H X3/5X,F12.8,20H VX1- KILOMETERS/SEC./5X,F12.8,
2 5H VX2/5X,F12.8,5H VX3 )
6021 FORMAT (/ 2X/F11.4,5X,27H SEMI-MAJOR AXIS-KILOMETERS/6X,F11.8,
1 14H ECCENTRICITY/3X,F12.6,3X,12H INCLINATION/3X,9H -DEGREES/3X,
2 F12.6,3X,24H R.A. ASC. NODE -DEGREES/3X,F12.6,3X,24H ARG. OF PERI
3 GEE-DEGREES/3X,F12.6,3X,24H MEAN ANOMALY -DEGREES )
6022 FORMAT (/ 4X,F11.6,3X,7H PERIOD/8X,7H -HOURS/2X/F11.4,20X,9H -MINUT
1 ES/4X,F11.6,3X,12H MEAN MOTION/3X,14H -DEGREES/HOUR/4X,F11.6,3X,
2 15H MOTION OF NODE/8X,14H -DEGREES/DAY/4X,F11.6,3X,18H NOTION OF
3 PERIGEE/5X,14H -DEGREES/DAY )
6023 FORMAT /5H DATE,6X14HUNIVERSAL TIME,16X20HGEODETIC COORDINATES/
1 9H MO/DY/YR,3X4HH M,3X4HSEC.,9X39HLATITUDE-DMS LONGITUDE-DMS H
2 FIGHT-KM, //)
6024 FORMAT (/1X/12+1H/,12+1H/,12,2X213+P7.3,8X213+P6.2,2X14+,13+P6.2,
1 F11.3 )
6025 FORMAT (11H PUSH START //)
6026 FORMAT (1H1//15X39H LOCAL STATION PREDICTIONS FOR -- //8H STATION,
1 5X10H LONGITUDE,5X10H LATITUDE,4X16H HEIGHT (METERS) //)
6027 FORMAT (1X2A3,15,13+F7.3,14,13+F7.3,F11.2 )
6028 FORMAT (1X,2A3,5X14,13+F7.3,15,13+F7.3,4XF10.2 )
6037 FORMAT (1H1/4510H WORLD MAP //)
6038 FORMAT (27HLOCAL STATION PREDICTIONS )
6039 FORMAT (13H JOB FINISHED //)
6040 FORMAT (E8.2)
6041 FORMAT (28HIEXCUTE MAIN PROGRAM-WMAPLA/1H)
6042 FORMAT /1C EQUATORIAL INERTIAL COORDINATES/
1 90H REQUIRED UNITS - KILOMETERS AND KILOMETERS/SECOND/
6043 FORMAT (1X,F13.5,4X,17H X1 - KILOMETERS/1X,F13.5,4X,
1 17H X2 - KILOMETERS/1X,F13.5,4X,17H X3 - KILOMETERS//5X,F12.8,
2 1X,13H VX1 - KM/SEC/5X,F12.8,1X,13H VX2 - KM/SEC/5X,F12.8,1X,
3 13H VX3 - KM/SEC)
6044 FORMAT (/18X,50H BROUWER HARMONICS COMPUTED FROM J2,J3,J4, AND J5
1 /1X,1PE14+8,3X,24H K2 (KILOMETERS SQUARED)/1X,E14+8,3X,
2 22H K3 (KILOMETERS CUBED)/1X,E14+8,3X,
3 29H K4 (KILOMETERS FOURTH POWER)/1X,E14+8,3X,
4 28H K5 (KILOMETERS FIFTH POWER)//)
6045 FORMAT (/4X,63H POSITION AND VELOCITY VECTORS - GEOCENTRIC EQUATOR
1 IAL INERTIAL)
6046 FORMAT (/1X,F13.5,4X,17H X1 - KILOMETERS,3X,F12.8,1X,
1 21H X1 - VANGUARD UNITS/1X,F13.5,4X,17H X2 - KILOMETERS,3X,
2 F12.8,1X,21H X2 - VANGUARD UNITS/1X,F13.5,4X,
3 17H X3 - KILOMETERS,3X,F12.8,1X,21H X3 - VANGUARD UNITS)
6047 FORMAT (/5X,F13.5,4X,17H X1 - KILOMETERS,7X,F12.8,1X,
1 21H VX1 - VANGUARD UNITS/5X,F12.8,1X,13H VX2 - KM/SEC,7X,F12.8,
2 1X,21H VX2 - VANGUARD UNITS/5X,F12.8,1X,13H VX3 - KM/SEC,7X,
3 F12.8,1X,21H VX3 - VANGUARD UNITS//1X,F13.5,4X,
4 17H R - KILOMETERS,3X,F12.8,1X,21H R - VANGUARD UNITS/5X,
5 F12.8,1X,13H V - KM/SEC,7X,F12.8,1X,
6 21H V - VANGUARD UNITS)
6048 FORMAT (/26X,17H ORBITAL ELEMENTS/20H OSCULATING ELEMENTS,2X,
1 22H BROUWER MEAN ELEMENTS/1X,F12.4,11X,F12.4,7X,
2 29H SEMI-MAJOR AXIS - KILOMETERS/6X,F11.8,12X,F11.8,3X,
3 13H ECCENTRICITY/4X,F11.6,12X,F11.6,5X,
4 26H INCLINATION - DEGREES/4X,F11.6,12X,F11.6,5X,
5 26H R.A. ASC. NODE - DEGREES/4X,F11.6,12X,F11.6,5X,
6 26H ARG. OF PERIGEE - DEGREES/4X,F11.6,12X,F11.6,5X,
7 26H MEAN ANOMALY - DEGREES)
6049 FORMAT (/45H TRUNCATION FACTORS USED IN COMPUTING BROUWER /
1 39H MEAN ELEMENTS FROM OSCULATING ELEMENTS//1X,1PE8+1,9X,
2 29H SEMI-MAJOR AXIS - KILOMETERS/1X,E8.1,9X,13H ECCENTRICITY/1X,
3 E8.1,9X,26H INCLINATION - DEGREES/1X,E8.1,9X,
4 26H R.A. ASC. NODE - DEGREES/1X,E8.1,9X,
5 26H ARG. OF PERIGEE - DEGREES/1X,E8.1,9X,
6 26H MEAN ANOMALY - DEGREES )
6050 FORMAT (F12.8)
6051 FORMAT (22H BROUWER MEAN ELEMENTS/69H REQUIRED UNITS - ALL ANGLES
1 IN DEGREES+SEMI-MAJOR AXIS IN KILOMETERS )
6052 FORMAT /1X/12+1H/12,1X,213+,F7.3,5X,12(2XA3)
9501 FORMAT (1H0,8H *****)
9502 FORMAT (1H0,17HMUTUAL VISIBILITY//)
9503 FORMAT (/SHODATE,5X15H UNIVERSAL TIME/23H MO/DY/YR H M SEC.,
1 5X,12(2XA3))

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9504 FORMAT(1H1//15X33H LOCAL STATION PREDICTIONS FOR -- //8H STATION,
15X10H LONGITUDE ,6X9H LATITUDE,4X16H HEIGHT (METERS)//)
9505 FORMAT (3I3,F10.0)
9506 FORMAT(A#6,1)
9507 FORMAT(1//17X26HNO STATION PRINT OUT IF ---//
11X,25H1. ELEVATION IS LESS THAN,14X,13. 8H DEGREES/
21X,25H2. RANGE IS GREATER THAN ,7X,F9.0,12H KILOMETERS/
31X,30H3. RADAR ANGLE IS GREATER THAN,6X,F6.1,8H DEGREES/
419X,12HOR LESS THAN,6X,F6.1,8H DEGREES//)
54X,25H5HIN AXIS COORDINATES ARE,8X,F6.1,24H DEGREES RIGHT ASCENSIN@
6N/37X,F6.1,20H DEGREES DECLINATION )
7500 FORMAT(5HODATE,7X3HUTZ,15X5HRRANGE,3X2HAZ,3X2HEL,3X5HRRADAR/
1 9H M@D@Y/YR,16H . H M STATION,6X4H(KM),12H (DEG) (DEG) .
2 12H ANGLE F (DEG) //)
7501 FORMAT(XI2,2(1H/12),1X,2(13),2X,2A3,3XF8.1,1XF5.1,XF4.1,2XF5.1/
118X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2X
2F5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1
3 , 2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1
4 ,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1
5 ,XF5.1,XF4.1,2XF5.1/18X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1/18X,2A3,3X
6 F8.1,XF5.1,XF4.1,2XF5.1/
718X,2A3,3XF8.1,XF5.1,XF4.1,2XF5.1)
C
C ALL DIMENSION STATEMENTS FOLLOW IMMEDIATELY.
C
C DIMENSION RX(3),VX(3),A(6),AI(6),RG(3),VG(3),RLAT(12),RLON(12)
D
D DIMENSION RGU(3),Z(3),C@GRD(3),U(3),SU(12,3)
D DIMENSION ELED(12),AZID(12),RGE(12),TESTA(12),STAT1(12),STAT2(12)
D DIMENSION RGE1(12),ELED1(12),AZID1(12),TESTA1(12),STAT3(12)
D DIMENSION GP(5),DA(6),DAD(6),A110(6),XX(12),AD(6),RXB(3)
D
D DIMENSION VXE(3),RTX(3)
D DIMENSION STATA(12),DATA(12),VXB(3),XXX(10),SS(3)
D DIMENSION DUM1(100)
COMMON DUM1,A110,GP,ERRB,XX,AB,RXB,VXB,XXX,SS
C
C PRINT 6041
C
C DEFINE TRUNCATION FACTOR (RADIAN5)
C
C 1 FRR=1,DE-8
D FRRB=3,DE-7
D EN2 = 0,0
C
C DEFINE TRUNCATION FACTORS FOR SUBROUTINE BBRWR I USED TO CONVERT
C @SCULATING ELEMENTS TO BROWNER MEAN ELEMENTS)
C
C DAD(1)=5,OF-4
C DAD(2)=5,OF-6
C DAD(3)=5,OF-6
C DAD(4)=5,OE-6
C DAD(5)=5,OF-6
C DAD(6)=5,OE-6
C
C LC2=0
B APRINT=60 60 60 60 60 60
B BPRINT = 60 60 54 60 60 60
C
C DEFINE GODDARD EARTH CONSTANTS
C
C GM=3.986032E+5
D FJ2=1.0823E-3
D FJ3=-2.3E-6
D FJ4=-1.8E-6
D FJ5=0,0
D FL=298.3
D RE=6378.165
C
C CARD 1 - READ IN I.D. CARD - ANY INFORMATION IN COLS. 2 - 72
C
C RFAD 6002
C
C CARD 2 - READ IN CONTROL CARD
C
C COLS. 1- 3 TYPE OF INPUT +01 = @SCULATING @ORBITAL ELEMENTS
C +02 = INERTIAL POSITION AND VELOCITY
C IN KILOMETERS AND KM/SEC
C +03 = INERTIAL POSITION AND VELOCITY
C IN VANGUARD UNITS
C +04 = BROWNER MEAN ELEMENTS )
C
C COLS. 4- 6 COMPUTE WORLD MAP - YES OR NO ( YES IF MAP=+XX, NO IF
C MAP=+00 OR -XX)
C COLS. 7- 9 COMPUTE LOOK ANGLES - YES OR NO (YES IF LA=+XX, NO IF
C LA=+00 OR -XX)
C
C COLS. 10-12 CHANGE EARTH CONSTANTS
C COLS. 13-16 CHANGE TRUNCATION FACTOR
C
C READ 6003,INPUT,MAP,LA,MCST,NERR,HDA,IRC
C
C TEST - HAVE ALL CASES BEEN RUN - YES OR NO
C
C IF (INPUT) 300,300,2

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C      IF INPUT=+00 OR -XX, ALL CASES HAVE BEEN RUN. GO TO 300 (END
C      FILE, REWIND AND UNLOAD A3). IF INPUT =+XX, PROCEED TO NEXT CASE.
C
C      TEST - CHANGE TRUNCATION FACTOR - YES OR NO
C
C      2 IF (NERR) 4,4,3
C
C      CARD 2A- (OPTIONAL) READ IN NEW VALUE OF TRUNCATION FACTOR IF
C      NERR=+XX. IF NERR=+00 OR -XX, PROCEED TO NEXT
C      OPTION TEST.
C
C      3 READ          6040,ERR
C
C      TEST - CHANGE EARTH CONSTANTS - YES OR NO
C
C      4 IF (NCST) 5,11,10
C
C      IF NCST=+00, RETAIN STANDARD GODDARD EARTH CONSTANTS AND PROCEED
C      TO NEXT STEP.
C
C      5 IF (NCST+1) 7,6,7
C
C      USE S1RY PACKAGE CONSTANTS IF NCST = -1
C
C      6 GM=3,9862688E+05
C      D FJ2=1,08219E-03
C      D FJ3=-2,285E-06
C      D FJ4=-2,123F-06
C      D FJ5=-2,32F-07
C      D FL=297,0
C      D RE=6378,388
C      GO TO 11
C      7 IF (NCST+2) 9,8,11
C
C      USE GODDARD EARTH CONSTANTS WITH HARMONICS = 0 IF NCST = -2
C
C      8 FJ2=0,0
C      D FJ3=0,0
C      D FJ4=0,0
C      D FJ5=0,0
C      GO TO 11
C
C      USE INTERNATIONAL CONSTANTS WITH HARMONICS = 0 IF NCST = -3
C
C      9 GM=3,98626873E+5
C      D FJ2=0,0
C      D FJ3=0,0
C      D FJ4=0,0
C      D FJ5=0,0
C      D FL=297,0
C      D RF=6378,388
C      GO TO 11
C
C      CARDS 2B AND 2C- (OPTIONAL) READ IN NEW SET OF EARTH CONSTANTS
C      IF NCST=+XX.
C
C      10 READ          6004,GM,FJ2,FJ3,FJ4,FJ5,FL,RE
C
C      CONVERT EARTH CONSTANTS
C
C      11 GP(1)=GM
C      GP(2)=.5*FJ2*RE**2
C      GP(3)=-FJ3*RE**3
C      GP(4)=-.375*FJ4*RE**4
C      GP(5)=-FJ5*RE**5
C
C      PRINT ALL QUANTITIES ON OUTPUT TAPE A3.
C
C      12 WRITE OUTPUT TAPE 3,6001
C      WRITE OUTPUT TAPE 3,6002
C      WRITE OUTPUT TAPE 3,6005,ERR,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
C      WRITE OUTPUT TAPE 3,6044,GP(2),GP(3),GP(4),GP(5)
C      IF (SFNSF SWITCH 6) 13,913
C
C      PRINT SAME INFORMATION ON LINE IF SENSE SWITCH 6 IS DOWN.
C
C      13 PRINT 6001
C      PRINT 6002
C      PRINT 6005,ERR,RE,FL,GM,FJ2,FJ3,FJ4,FJ5
C      PRINT 6044,GP(2),GP(3),GP(4),GP(5)
C      913 IF (NDA) 915,915,914
C      914 READ          6050, (DAD(N), N=1,6)
C      915 DA(1)=DAD(1)
C      DA(2)=DAD(2)
C      DO 916 N=3,6
C      916 DA(N)=DAD(N)*0.017453292
C      IF (IRCI 917,917,918
C      917 IRC=50 -
C
C      CARD 3 - READ IN EPOCH OF INPUT PARAMETERS-CALENDAR DATE (MONTH,
C      DAY, AND YEAR) AND UNIVERSAL TIME (HOURS, MINUTES, AND
C      SECONDS TO 3 DECIMALS OF A SECOND).

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C   CARD 4 - READ IN PARAMETERS
C
C   918 READ          6006,NME,NDE,NYE,NHE,NMNE,TSE,(AI(N),N=1,6)
C
C   PRINT EP0CH AND INPUT OPTION 0N OUTPUT TAPE A3
C
C   15 WRITE OUTPUT TAPE 3,6010,NME,NDE,NYE,NHE,NMNE,TSE
C   WRITE OUTPUT TAPE 3,6008,INPUT
C   IF (SENSE SWITCH 6) 16,17
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   16 PRINT 6010,NME,NDE,NYE,NHE,NMNE,TSE
C   PRINT 6008,INPUT
C   17 CONTINUE
C
C   CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
C   TO EP0CH UNIVERSAL TIME IN RADIANs.
C
C   TIME0=HMSRZ(NHE,NMNE,TSE)
C
C   CONVERT EP0CH CALENDAR DATE TO EP0CH JULIAN DATE AT 0 HOURS
C   UNIVERSAL TIME.
C   DJ0=DJUL(NME,NDE,NYE)
C
C   CONVERT EP0CH UNIVERSAL TIME IN HOURS, MINUTES, AND SECONDS
C   TO SECONDS.
C
C   THE=NHE*3600
C   TMNE=NMNE*60
C   TSEP=THE+TMNE+TSE
C   GO TO (18,20,22,930) , INPUT
C
C   PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTION 1
C   OSCULATING ORBITAL ELEMENTS -
C   1. SEMI-MAJOR AXIS IN KM 2. ECCENTRICITY 3. INCLINATION 4. RIGHT
C   ASCENSION OF ASCENDING NODE 5. ARGUMENT OF PERIGEE 6. MEAN ANOMALY
C   (ALL ANGLES I.E. 3,4,5, AND 6 ARE IN DEGREES).
C
C   18 WRITE OUTPUT TAPE 3,6012
C   WRITE OUTPUT TAPE 3,6013,(AI(N),N=1,6)
C   IF (SENSE SWITCH 6) 19,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   19 PRINT 6012
C   PRINT 6013,(AI(N),N=1,6)
C   GO TO 28
C
C   PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTION 2
C   INERTIAL POSITION AND VELOCITY RECTANGULAR COORDINATES -
C   IN KILOMETERS AND KILOMETERS PER SECOND.
C
C   20 WRITE OUTPUT TAPE 3,6042
C   WRITE OUTPUT TAPE 3,6043,(AI(N),N=1,6)
C   IF (SENSE SWITCH 6) 21,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   21 PRINT 6042
C   PRINT 6043,(AI(N),N=1,6)
C   GO TO 28
C
C   PRINT INPUT PARAMETERS 0N OUTPUT TAPE A3 - INPUT OPTION 3
C   INERTIAL POSITION AND VELOCITY RECTANGULAR COORDINATES -
C   IN VANGUARD UNITS.
C
C   22 WRITE OUTPUT TAPE 3,6009
C   WRITE OUTPUT TAPE 3,6011,(AI(N),N=1,6)
C   IF (SENSE SWITCH 6) 23,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   23 PRINT 6009
C   PRINT 6011,(AI(N),N=1,6)
C   GO TO 28
C
C   PRINT INPUT PARAMETERS - INPUT OPTION 4 - BROUWER MEAN ELEMENTS
C
C   930 WRITE OUTPUT TAPE 3,6051
C   931 WRITE OUTPUT TAPE 3,6013,(AI(N),N = 1,6)
C   IF (SENSE SWITCH 6) 932,28
C
C   PRINT SAME INFORMATION 0N-LINE IF SENSE SWITCH 6 IS DOWN
C
C   932 PRINT 6051
C   PRINT 6013,(AI(N), N = 1,6)
C
C   CONVERT INPUT PARAMETERS TO OSCULATING ELEMENTS

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D 28 CALL PARA(INPUT,AI,A,GM)
D CALL ELRVZ(RX,VX,A,PER,EN,GM,ERR)
D CALL BBRWR(DA,A,IRC,NN)
D VX(1)=VX(1)
D VX(2)=VX(2)
D VX(3)=VX(3)
D FN=SS(1)
D DP=SS(2)
D DN=SS(3)
D PER=6.28318530718/EN
D PERM=PER/60.0
D PERH=PER/3600.0
D EN1=EN*206264.806247096
D DN0DE=DN*4950355.3499303
D DPERI=DP*4950355.3499303
C
C TEST - IS WORLD MAP DESIRFO
C
D 29 IF (MAP) 30,30,33
D 30 WRITE OUTPUT TAPE 3,6014
D IF (SENSE SWITCH 6) 31,36
D 31 PRINT 6014
D 32 GO TO 36
C
C CARD 5A - WORLD MAP IS DESIRED. READ IN CALENDAR DATE (DAY,
C MONTH, AND YEAR) AND UNIVERSAL TIME (HOURS, MINUTES,
C AND SECONDS TO 3 DECIMALS OF A SECOND) AT WHICH THE
C START OF CALCULATION IS DESIRED, CALENDAR DATE AND
C UNIVERSAL TIME AT WHICH THE TERMINATION OF THE
C CALCULATION IS DESIRED, AND THE DESIRED TIME INCREMENT
C OF THE CALCULATION IN SECONDS TO 3 DECIMALS OF A SECOND.
C
D 33 WRITE OUTPUT TAPE 3,6016
C
C PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
D IF (SENSE SWITCH 6) 34,35
D 34 PRINT 6016
D 35 CALL TIMEC(DJO,TSEP,WMAPS,WMAPI,WMAPI)
C
C TEST - ARE STATION PREDICTIONS (LOOK ANGLES) DESIRED
C
D 36 IF (LA) 37,37,40
D 37 WRITE OUTPUT TAPE 3,6017
D IF (SENSE SWITCH 6) 38,43
D 38 PRINT 6017
D 39 GO TO 43
C
C CARD 5B - STATION PREDICTIONS (LOOK ANGLES) ARE REQUIRED. READ
C IN CALENDAR DATE AND UNIVERSAL TIME AT WHICH THE START
C OF THE CALCULATION IS DESIRED, CALENDAR DATE AND
C UNIVERSAL TIME AT WHICH THE TERMINATION OF THE
C CALCULATION IS DESIRED, AND THE DESIRED TIME INCREMENT
C OF THE CALCULATION IN SECONDS.
C
D 40 WRITE OUTPUT TAPE 3,6018
C
C PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
D IF (SENSE SWITCH 6) 41,42
D 41 PRINT 6018
D 42 CALL TIMEC(DJO,TSEP,XLAS,XLAF,DTLA)
D 43 WRITE OUTPUT TAPE 3,6001
D WRITE OUTPUT TAPE 3,6002
D WRITE OUTPUT TAPE 3,6019
D WRITE OUTPUT TAPE 3,6010,NME,NDE,NYE,NHE,NMNE,TSE
C
C PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
D IF (SENSE SWITCH 6) 44,45
D 44 PRINT 6001
D PRINT 6002
D PRINT 6019
D PRINT 6010,NME,NDE,NYE,NHE,NMNE,TSE
D 45 CONTINUE
C
C CONVERT OSCILLATING ORBITAL ELEMENTS TO INERTIAL POSITION AND
C VELOCITY COORDINATES IN KM AND KM/SEC
C
D 46 CALL ELRVZ(RX,VX,A,PER,EN,GM,ERR)
D R1=SORTF(RX(1)**2+RX(2)**2+RX(3)**2)
D V1=SORTF(VX(1)**2+VX(2)**2+VX(3)**2)
C
C CONVERT TO VANGUARD UNITS OF LENGTH AND VELOCITY
C
D 47 X01=RX(1)/6378.388
D X02=RX(2)/6378.388
D X03=RX(3)/6378.388
D V01=VX(1)/7.9054722668
D V02=VX(2)/7.9054722668
D V03=VX(3)/7.9054722668

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D      R2=SQRT(X01**2+X02**2+X03**2)
D      V2=SQRT(V01**2+V02**2+V03**2)
C
C      CONVERT ANGLES (RADIAN) TO ANGLES (DEGREES)
C
D      A01=A(1)
D      A02=A(2)
D      A03=A(3)*57.2957795130823
D      A04=A(4)*57.2957795130823
D      A05=A(5)*57.2957795130823
D      A06=A(6)*57.2957795130823
48 WRITE OUTPUT TAPE 3,6045
WRITE OUTPUT TAPE 3,6046,RX(1),X01,RX(2),X02,RX(3),X03
WRITE OUTPUT TAPE 3,6047,VX(1),V01,VX(2),V02,VX(3),V03,R1,R2,V1,V2
WRITE OUTPUT TAPE 3,6049,(DAD(I) , I = 1,6)
B1=A110(1)
B2=A110(2)
B3=A110(3)*57.2957795
B4=A110(4)*57.2957795
B5=A110(5)*57.2957795
B6=A110(6)*57.2957795
WRITE OUTPUT TAPE 3,6048,A01,B1,A02,B2,A03,B3,A04,B4,A05,B5,A06,B6
WRITE OUTPUT TAPE 3,6022,PERH,PERM,EN1,DNODE,DPERI
IF (SENSE SWITCH 6) 49,50
C
C      PRINT SAME INFORMATION ON-LINE IF SENSE SWITCH 6 IS DOWN
C
C
49 PRINT 6045
PRINT 6046,RX(1),X01,RX(2),X02,RX(3),X03
PRINT 6047,VX(1),V01,VX(2),V02,VX(3),V03,R1,R2,V1,V2
PRINT 6048,A01,B1,A02,B2,A03,B3,A04,B4,A05,B5,A06,B6
PRINT 6022,PERH,PERM,EN1,DNODE,DPERI
50 CONTINUE
53 IF (MAP) 199,199,100
C
C      BEGIN WORLD MAP CALCULATION (NO CALCULATION IF MAP = 0)
C      SKIP A PAGE AND PRINT HEADING FOR WORLD MAP CALCULATIONS
C
100 WRITE OUTPUT TAPE 3,6037
WRITE OUTPUT TAPE 3,6023
IF (SENSE SWITCH 6) 101,102
101 PRINT 6037
PRINT 6023
C
C      INITIALIZE LINE COUNT AND DELTA T (DIFFERENCE BETWEEN
C      WORLD MAP STARTING TIME AND EPOCH OF INPUT PARAMETERS IN SECONDS)
C
C
102 LINES=1
DTIMES=WMAPS-WMAPDT
IF (SENSE SWITCH 1) 1030,103
1030 PRINT 6025
PAUSE 7777
103 LINES=LINES+1
C
C      SKIP A PAGE AND PRINT HEADING IF 50 LINES OF CALCULATION
C      HAVF BEEN PRINTED
C
IF (LINES-50) 106,106,104
104 WRITE OUTPUT TAPE 3,6037
WRITE OUTPUT TAPE 3,6023
LINES=1
IF (SENSE SWITCH 6) 105,106
105 PRINT 6037
PRINT 6023
D 106 DTIMES=DTIMES+WMAPDT
D TIME=TIME+DTIMES*0.727220521664304E-4
D DDJO=INTF(TIME/6.283185307179586)
D DJ=DJO+DDJO
D TIME=ALL0TZ(TIME)
C
C      COMPUTE GREENWICH APPARENT SIDEREAL TIME AT TO + DELTA T
C
C
D EPHR = TIME * 3.81971863421
D EQR=EON(DJ,EPHR,XX,XX,XX)
D ST=GASTZ(DJ,EPHR,EQR)
D CALL JULCAL(DJ,NM,ND,NY)
C
C      CONVERT UNIVERSAL TIME IN RADIAN TO HOURS, MINUTES, AND SECONDS
C
D CALL RHMSZ(TIME,II,IH,IM,TS).
C
C      CALL BRWR2(DTIMES,EN2)
C      SST=SINF(ST)
C      CST=COSF(ST)
C      RG(1)=RXB(1)*CST+RXB(2)*SST
C      RG(2)=RXB(2)*CST-RXB(1)*SST
C      RG(3)=RXB(3)
C      CALL VROZ(I,RG,GCLAT,GCLON,R)
D
C
C      COMPUTE GEODETIC LATITUDE OF SUBSATELLITE POINT
C

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C      COMPUTE HEIGHT OF SATELLITE ABOVE COMPUTATIONAL ELLIPSOID ALONG
C      NORMAL FROM SATELLITE TO ELLIPSOID
C
C      GDLAT = GDLATZ(GCLAT,R,RE,FL,ALT)
C
C      CONVERT LATITUDE AND LONGITUDE IN RADIANS TO DEGREES, MINUTES,
C      AND SECONDS
C
C      TGCLON=GCLON-3,141592653589793
C      IF (TGCLON) 1062,1062,1061
D1061 GCLON=TGCLON-3,141592653589793
C      1062 CONTINUE
D      CALL RDMSZ(GDLAT,I,IPD,IPM,TPS)
D      CALL RDMSZ(GCLON,II,ILD,ILM,TLS)
C
C      OUTPUT PREPARATION
C
C      NYM19=NY-1900
C      WRITE OUTPUT TAPE 3,6024,NM,ND,NYM19,IH,IM,TS,IPD,IPM,TPS,ILD,
C      1 ILM,TLS,ALT
C      IF (SENSE SWITCH 6) 107,108
107 PRINT 6024,NM,ND,NYM19,IH,IM,TS,IPD,IPM,TPS,ILD,ILM,TLS,ALT
108 IF (DTIMES-WMAPF) 103,109,109
109 IF (SENSE SWITCH 1) 110,199
110 PRINT 6025
C      PAUSE 77776
C
C      END WORLD MAP CALCULATION
C
C      199 IF (LA) 1,1,200
C
C      BEGIN LOCAL STATION PREDICTIONS CALCULATION
C      (NO CALCULATION IF LA=0)
C
C      200 READ          9505,NLA,ICCI,MINV,XMAX
C      IF (NLA) 1,1,2001
2001 READ          9506,RDMAX,RDMIN,RA,DEC
C      XMIN=MINV
C      IF(XMAX) 902,902,903
902 XMAX=1000000.0
903 IF(RA) 904,905,904
D904 RAR=RA*.0174532925
D      DECR=DEC*.0174532925
D      VXE(1) = COSF(DECR) * COSF(RAR)
D      VXF(2) = COSF(DECR) * SINF(RAR)
D      VXF(3) = SINF(DECR)
D905 CALL VRDZ(1,VXE+DECR,RAR,XXX)
C      RA = RAR*57.2957795
C      DECR=DECR*57.2957795
C      WRITE OUTPUT TAPE 3,9504
C      IF (SENSE SWITCH 6) 201,202
201 PRINT 9504
202 DO 205 N=1,NLA
C      READ          6027,STAT1(N),STAT2(N),LOND,LONM,XLONS,LATD,
901  LATM,XLATS,HGT
C      WRITE OUTPUT TAPE 3,6028,STAT1(N),STAT2(N),LOND,LONM,XLONS,LATD,
C      1LATM,XLATS,HGT
C      IF (SENSE SWITCH 6) 203,2031
203 PRINT 6028,STAT1(N),STAT2(N),LOND,LONM,XLONS,LATD,LATM,XLATS,HGT
2031 CONTINUE
D      C@ORD(1) = DMSRZ(LATD,LATM,XLATS)
D      C@ORD(2) = DMSRZ(LOND,LONM,XLONS)
D      C@ORD(3)=HGT/1000.0
D      RLAT(N)=C@ORD(1)
D      RLON(N)=C@ORD(2)
D      CALL VFUZ(C@ORD,RE,FL,U)
D      DO 204 J=1,J
204 SUIN,J)=J(J)
205 CONTINUE
C      WRITE OUTPUT TAPE 3,9507,MINV,XMAX,RDMAX,RDMIN,RA,DEC
C
C      INITIALIZE LINE COUNT AND DELTA T DIFFERENCE BETWEEN
C      LOCAL STATION PREDICTIONS STARTING TIME AND EPOCH OF INPUT
C      PARAMETERS IN SECONDS)
C
C      LINES=1
C      LINE6=1
D      DTIMES=XLAS-DTIA
C
C      SKIP A PAGE AND PRINT HEADING FOR LOCAL STATION PREDICTIONS
C      PRINT 607
C
C      WRITE OUTPUT TAPE 3,6038
C      WRITE OUTPUT TAPE 3,9502
C      IF(ICCI) 7004,7004,7005
7005 WRITE OUTPUT TAPE 6,6038
C      WRITE OUTPUT TAPE 6,9502
C      WRITE OUTPUT TAPE 6,7500
7004 IF(SENSE SWITCH 6) 2051,2052
2051 PRINT 6038
207 PRINT 9502
2052 CONTINUE

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208 WRITE OUTPUT TAPE 3,9503,(STAT2(I),I = 1,NLA)
    IF (SENSE SWITCH 6) 210,2170
210 PRINT          9503,(STAT2(I),I = 1,NLA)
2170 IF (SENSE SWITCH 2) 2171,217
2171 PRINT 6025
    PAUSE 77775
217 LINES=LINFS+1
C
C   SKIP A PAGE AND PRINT HEADING IF 50 LINES OF CALCULATION
C   HAVE BEEN PRINTED
C
9600 IF (LINES-40) 231,231,218
218 LINFS=1
    WRITE OUTPUT TAPE 3,6038
    WRITE OUTPUT TAPE 3,9503,(STAT2(I),I = 1,NLA)
    IF (SENSE SWITCH 6) 220,231
220 PRINT 6038
    PRINT          9503,(STAT2(I),I = 1,NLA)
231 IF (ICCL) 7016,7016,7007
7007 IF (LINE6-40) 7016,7016,7015
7015 LINE6=1
    WRITE OUTPUT TAPE 6,6038
    WRITE OUTPUT TAPE 6,7500
D7016 DTIMES=DTIMFS+DTLA
D   TIME=TIME0+DTIMES*0.727220521664304E-4
D   DJO=INT(F TIME/6.283185307179586)
D   DJ=DJ0+ND*10
D   TIME=ALL0TZ(TIME)
C
C   COMPUTE GREENWICH APPARENT SIDEREAL TIME AT TO + DELTA T
C
D   EPHR = TIME * 3.81971863421
D   EOR=EON(DJ,EPHR,XX,XX,XX)
D   ST = GAST7(DJ,EPHR,EOR)
D   CALL JULCAL(DJ,NM,ND,NY)
C
C   CONVERT UNIVERSAL TIME IN RADIAN TO HOURS, MINUTES, AND SECONDS
C
C   CALL RHMSZ(TIME,II,IH,IM,TS)
C   NYM19=NY-1900
C
C   CALL BRWR2(DTIMES,EN2)
    SST=SNP(ST)
    CST=COSF(ST)
    RG(1)=RXB(1)*CST+RXB(2)*SST
    RG(2)=RXB(2)*CST-RXB(1)*SST
    RG(3)=RXB(3)
C
C   KK=0
D0 242 N=1,NLA
D0 232 M=1,3
D   PCU(N)=RG(N)-SU(N,M)
D   CALL R13Z(RTX,0,-ST,RGU)
D   DUMX=DOTZ(RTX,VXE)
D   TESTA(N)=DUMX*57.295780
D   R13A1=1.57079632679-RLAT(N)
D   R13A2=1.57079632679+RLON(N)
D   CALL R13Z(Z,R13A1,R13A2,RGU)
D   CALL VRDZ(Z,Z,ELEVAT,AZIMUT,RANG)
D   ELED(N)=57.29578*ELEVAT
D   AZID(N)=57.29578*AZIMUT
D   RGE(N)=RANG
    IF (ELED(N)-XMIN) 233,234,234
B 233 DATA(N)=APRINT
    G0 T0 242
234 IF (TESTA(N)-RDMIN) 235,236,236
B 235 DATA(N)=APRINT
    G0 T0 242
236 IF (TESTA(N)-RDMAX) 238,238,237
B 237 DATA(N)=APRINT
    G0 T0 242
238 IF (RGE(N)-XMAX) 240,240,239
B 239 DATA(N)=APRINT
    G0 T0 242
B 240 DATA(N)=BPRINT
    SENSE LIGHT 1
    IF (ICCL) 242,242,241
241 KK=KK+1
    RGE1(KK)=RGE(N)
    ELED1(KK)=ELED(N)
    AZID1(KK)=AZID(N)
    TESTA1(KK)=TESTA(N)
B   STAT3(KK) = STAT1(N)
B   STAT4(KK) = STAT2(N)
242 CONTINUE
    IF (SENSE LIGHT 1) 243,2460
243 IF (LC2-1) 245,244,245
244 WRITE OUTPUT TAPE 3,9501
    LC2=0
    LINES =LINES+1
245 WRITE OUTPUT TAPE 3,6052,NM,ND,NYM19,IH,IM,TS, (DATA(N), N=1,NLA)
    LINES= LINES+1

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```

      IF (ICCL) 247,247,246
246  WRITE OUTPUT TAPE 6,7501,NM,NO,NYM19,IH,IM,(STAT3(I),STAT4(I),
      IRGF1(I),AZ101(I),ELED1(I),TESTA1(I), I =1,KK)
      LINE6=LINE6+KK+1
      GO TO 247
2460 LC2=1
247  CONTINUE
      IF (DTIMFS-XLAF) 9600,248,248
248  IF (SENSF SWITCH 2) 249,7010
249  PRINT 6025
      PAUSE 77774
7010 IF (ICCL) 200,200,7011
7011 FND FILF 6
      GO TO 200

C
C   END LOCAL STATION PREDICTIONS CALCULATION
C
300 PRINT 6039
      FND FILE 3
      PAUSE 77777
      GO TO 10
      END

```

APPENDIX VII
SOURCE DECKS OF SUBROUTINES

```

*   DATE 2/25/65
*   FUNCTION ALLOT FORTRAN SOURCE PROGRAM
*   CARDS COLUMN
*   LISTS
*   LABEL
*   FUNCTION ALLOT(X)
*
*   VERSION OF 07/22/63
*   FORTRAN FUNCTION
*   FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
*
*   PURPOSE
*   REDUCES AN ANGLE OF ANY MAGNITUDE AND SIGN BY MODULUS 2 PI
*   AND ADDS 2 PI IF ANGLE IS NEGATIVE. THE RESULTING ANGLE IS
*   POSITIVE BETWEEN 0 AND +2 PI RADIANS.
*
*   CALLING SEQUENCE
*   NAME = ALLOT(X)
*
*   INPUT
*   X = ANGLE IN RADIANS
*
*   OUTPUT
*   NAME = ANGLE IN RADIANS BETWEEN 0 AND + 2 PI RADIANS
*
*   REFERENCE
*   *****
*
*   METHOD
*   *****
*
*   RESTRICTIONS
*   *****
*
*   ACCURACY
*   *****
*
*   REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
*   NONE
*
*   REQUIRED SUBPROGRAMS - OTHER
*   NONE
*
*   STORAGE REQUIREMENTS
*   41
*
*   TIMING
*   NO ESTIMATE AVAILABLE
*
*   PROGRAM MODIFICATIONS
*   NO MODIFICATIONS TO DATE
*
* ***** START PROGRAM *****
2 ALLOT=MODF(X,6.2831853)
3 IF (ALLOT) 4,5,5
4 ALLOT=ALLOT+6.2831853
5 RETURN
END
*   FUNCTION ALLJZ FORTRAN SOURCE PROGRAM
*   CARDS COLUMN
*   LISTS
*   LABEL
*   FUNCTION ALLJZ(X)
*
*   VERSION OF 07/22/63
*   FORTRAN FUNCTION
*   FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
*
*   PURPOSE
*   REDUCES AN ANGLE OF ANY MAGNITUDE AND SIGN BY MODULUS 2 PI
*   AND ADDS 2 PI IF ANGLE IS NEGATIVE. THE RESULTING ANGLE IS
*   POSITIVE BETWEEN 0 AND +2 PI RADIANS.
*
*   CALLING SEQUENCE
*   D NAME = ALLJZ(X)
*
*   INPUT
*   X = ANGLE IN RADIANS
*
*   X MUST BE AVAILABLE IN CALLING PROGRAM IN DOUBLE PRECISION
*   FORM.
*
*   OUTPUT
*   NAME = ANGLE IN RADIANS BETWEEN 0 AND + 2 PI RADIANS
*
*   NAME IS RETURNED TO CALLING PROGRAM IN DOUBLE PRECISION
*   FORM.
*
*   REFERENCE
*   *****

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ALLJZ000
ALLJZ001
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ALLJZ099
ALLJZ100

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METHOD	ALL0T232
*****	ALL0T233
RESTRICTIONS	ALL0T234
*****	ALL0T235
ACCURACY	ALL0T236
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.	ALL0T237
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR	ALL0T238
DMOD, (DFAD)	ALL0T239
REQUIRED SUBPROGRAMS - OTHER	ALL0T240
NONE	ALL0T241
STORAGE REQUIREMENTS	ALL0T242
64 WITHOUT REQUIRED SUBPROGRAMS	ALL0T243
TIMING	ALL0T244
NO ESTIMATE AVAILABLE	ALL0T245
PROGRAM MODIFICATIONS	ALL0T246
NO MODIFICATIONS TO DATE	ALL0T247
***** START PROGRAM *****	ALL0T248
U 2 ALL0T2=MOD(X,6.283185307179586)	ALL0T249
3 IF (ALL0T2) 4,5,5	ALL0T250
D 4 ALL0T2=ALL0T2+6.283185307179586	ALL0T251
5 RETURN	ALL0T252
END	ALL0T253
* FUNCTION ATANQ FORTRAN SOURCE PROGRAM	ALL0T254
* CARDS COLUMN	ALL0T255
* LISTB	ALL0T256
* LABEL	ALL0T257
* FUNCTION ATANQ(S,C)	ALL0T258
VERSION OF 03/03/64	ALL0T259
FORTRAN FUNCTION	ALL0T260
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094	ALL0T261
PURPOSE	ALL0T262
COMPUTES THE ARCTANGENT OF AN ANGLE WITH PROPER ALLOCATION OF QUADRANT TO THE ANGLE BETWEEN 0 AND + 2 PI RADIANS.	ALL0T263
CALLING SEQUENCE	ALL0T264
NAME = ATANQ (S,C)	ALL0T265
INPUT	ALL0T266
S = D*SIN(A)	ALL0T267
C = D*COS(A)	ALL0T268
WHERE D IS AN ARBITRARY POSITIVE CONSTANT (USUALLY 1)	ALL0T269
D = +1.0)	ALL0T270
OUTPUT	ALL0T271
NAME = ANGLE A IN RADIANS BETWEEN 0 AND + 2 PI RADIANS	ALL0T272
REFERENCE	ALL0T273
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP	ALL0T274
METHOD	ALL0T275
USES FORTRAN MONITOR FUNCTION ATANF. TESTS THE SIGNS OF SINE AND COSINE, THEY ADDS OR SUBTRACTS APPROPRIATE FRACTIONS OF 2 PI RADIANS TO ASSIGN ANGLE TO PROPER QUADRANT BETWEEN 0 AND + 2 PI RADIANS.	ALL0T276
RESTRICTIONS	ALL0T277
ATANQ(0/0) = 0 BY DEFINITION	ALL0T278
ACCURACY	ALL0T279
*****	ALL0T280
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR	ALL0T281
ATAN	ALL0T282
REQUIRED SUBPROGRAMS - OTHER	ALL0T283
NONE	ALL0T284
STORAGE REQUIREMENTS	ALL0T285
173 WITHOUT REQUIRED SUBPROGRAMS	ALL0T286
TIMING	ALL0T287
NO ESTIMATE AVAILABLE	ALL0T288
PROGRAM MODIFICATIONS	ALL0T289
***** START PROGRAM *****	ALL0T290
IF (C) 108,100,116	ALL0T291

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100 IF (S) 102,104,106
102 ATANQ=4.712 388 98
RETURN
104 ATANQ=0.0
RETURN
-----
106 ATANQ=1.570 796 33
RETURN
108 IF (S) 110,112,114
110 ADD=3.141 592 65
GO TO 124
112 ATANQ=3.141 592 65
RETURN
114 ADD=3.141 592 65
GO TO 132
-----
116 IF (S) 118,120,122
118 ADD=6.283 185 31
GO TO 132
-----
120 ATANQ=0.0
RETURN
122 ADD=0.0
124 IF (ABS(F(S)-ABS(F(C))) 126,128,130
126 ATANQ=ATANF(S/C)+ADD
RETURN
128 ATANQ=0.785 398 163+ADD
RETURN
130 ATANQ=1.570 796 33-ATANF(C/S)+ADD
RETURN
132 IF (ABS(F(S)-ABS(F(C))) 126,134,136
134 ATANQ=-0.785 398 163+ADD
RETURN
136 ATANQ=-1.57079633-ATANF(C/S)+ADD
RETURN
END
FUNCTION ATANZ FURTRAN SOURCE PROGRAM
CARDS COLUMN
LISTB
LABEL
FUNCTION ATANZ(S,C)
VERSION OF 07/22/63
FORTRAN FUNCTION
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
COMPUTES AN ANGLE FROM ITS SINE AND COSINE AND PLACES THE
THE ANGLE IN A POSITIVE QUADRANT BETWEEN 0 AND + 2 PI
RADIANS.
CALLING SEQUENCE
D NAME = ATANZ(S,C)
INPUT
S = SINE OF ANGLE (+ OR -)
C = COSINE OF ANGLE (+ OR -)
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN
DOUBLE PRECISION FORM.
OUTPUT
NAME = ANGLE IN RADIANS BETWEEN 0 AND + 2 PI RADIANS
NAME IS RETURNED TO CALLING PROGRAM IN DOUBLE PRECISION
FORM.
REFERENCE
*****
METHOD
USES FORTRAN MONITOR FUNCTION ATANZF. IF ARGUMENT
RETURNED BY ATANZF IS -, 2 PI RADIANS ARE ADDED .
RESTRICTIONS
*****
ACCURACY
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
DATANZ,DFAD)
REQUIRED SUBPROGRAMS - OTHER
NONE
STORAGE REQUIREMENTS
67 WITHOUT REQUIRED SUBPROGRAMS
TIMING
NO ESTIMATE AVAILABLE
PROGRAM MODIFICATIONS
NO MODIFICATIONS TO DATE

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ATANQ058
ATANQ059
ATANQ070
ATANQ071
ATANQ072
ATANQ073
ATANQ074
ATANQ075
ATANQ076
ATANQ077
ATANQ078
ATANQ079
ATANQ080
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ATANZ056
ATANZ057
ATANZ058
ATANZ059

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C
C ***** START PROGRAM *****
D 2 ATANZ=ATANZ(S,C)
D 3 IF (ATANZ1,4,5,6)
D 4 ATANZ=ATANZ+6.283185307179586
D 5 RETURN
END
SUBROUTINE BBRWR FORTRAN SOURCE PROGRAM
*
* PAUSE
* CARDS COLUMN
* LISTB
* LABEL
SUBROUTINE BBRWR(DA,AT,J,K)
VERSION OF 10/02/63
FORTRAN SUBROUTINE
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
COMPUTES BROUWER MEAN ORBITAL ELEMENTS FROM OSCULATING
ORBITAL ELEMENTS BY MEANS OF AN ITERATIVE PROCESS.
CALLING SEQUENCE
DIMENSION DA(6),AT(6)
CALL BBRWR(DA,AT,J,K)
INPUT
J = MAXIMUM NUMBER OF ITERATIONS ALLOWED
DA(1) = TRUNCATION FACTOR FOR SEMI-MAJOR AXIS - KILOMETERS
DA(2) = TRUNCATION FACTOR FOR ECCENTRICITY - DIMENSIONLESS
DA(3) = TRUNCATION FACTOR FOR INCLINATION - RADIANS
DA(4) = TRUNCATION FACTOR FOR RIGHT ASCENSION OF ASCENDING
NODE - RADIANS
DA(5) = TRUNCATION FACTOR FOR ARGUMENT OF PERIGEE - RADIANS
DA(6) = TRUNCATION FACTOR FOR MEAN ANOMALY - RADIANS
TRUE VALUES OF OSCULATING ORBITAL ELEMENTS
AT(1) = SEMI-MAJOR AXIS - KILOMETERS
AT(2) = ECCENTRICITY - DIMENSIONLESS
AT(3) = INCLINATION - RADIANS
AT(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS
AT(5) = ARGUMENT OF PERIGEE - RADIANS
AT(6) = MEAN ANOMALY - RADIANS
OUTPUT
K = NUMBER OF ITERATIONS REQUIRED FOR CONVERGENCE
OUTPUT VIA COMMON
BROUWER MEAN ELEMENTS
ALL(1) = SEMI-MAJOR AXIS - KILOMETERS
ALL(2) = ECCENTRICITY - DIMENSIONLESS
ALL(3) = INCLINATION - RADIANS
ALL(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS
ALL(5) = ARGUMENT OF PERIGEE - RADIANS
ALL(6) = MEAN ANOMALY - RADIANS
REFERENCE
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP
METHOD
FOR THE 1ST APPROXIMATION, THE MEAN ELEMENTS ARE ASSUMED
TO BE EQUAL TO THE TRUE OSCULATING ELEMENTS. IN SUBSEQUENT
APPROXIMATIONS, THE MEAN ELEMENTS ARE SET EQUAL TO THE
MEAN ELEMENTS OF THE PREVIOUS APPROXIMATION PLUS THE
ALGEBRAIC DIFFERENCE BETWEEN THE VALUES OF THE TRUE
OSCULATING ELEMENTS MINUS THE VALUES OF THE OSCULATING
ELEMENTS COMPUTED BY SUBROUTINES BRWR1 AND BRWR2.
SUBROUTINES BRWR1 AND BRWR2 COMPUTE OSCULATING ELEMENTS
ACCORDING TO DIRK BROWDER'S ARTIFICIAL SATELLITE THEORY
WITHOUT DRAG.
THIS METHOD SUGGESTED BY DR. HANS HERTZ, DATA SYSTEMS
DIVISION, GODDARD SPACE FLIGHT CENTER.
RESTRICTIONS
FOR SMALL ECCENTRICITIES, THIS SUBROUTINE WILL NOT
CONVERGE. ERROR WARNING IS PRINTED IN LINE AND IN TAPE
UNIT 43 BEFORE RETURNING TO CALLING PROGRAM IF CONVERGENCE
IS NOT OBTAINED AFTER J ITERATIONS.
ACCURACY
SEVERAL TEST CASES WERE RUN WITH ECCENTRICITIES IN THE
NEIGHBORHOOD OF 1 AND CONVERGENCE WAS REACHED AFTER 4 OR
5 ITERATIONS.
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
(ISTH),(FIL),(SPH)
REQUIRED SUBPROGRAMS - OTHER
07/22/63 ALLOT
07/22/63 ALLOTZ
ATANZ066
ATANZ067
ATANZ068
ATANZ069
ATANZ070
ATANZ071
ATANZ072
ATANZ073
BBRW000
BBRW001
BBRW002
BBRW003
BBRW004
BBRW005
BBRW006
BBRW007
BBRW008
BBRW009
BBRW010
BBRW011
BBRW012
BBRW013
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BBRW083

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C      03/03/64. ATANQ      BBRW086
C      07/17/63. BRWRL      BBRW085
C      01/31/64 BRWRL      BBRW086
C      03/02/64. ELRV      BBRW087
C      09/12/63. XKPE      BBRW088
C      -----            BBRW089
C      STORAGE REQUIREMENTS BBRW090
C      . . . 146 WITHOUT REQUIRED SUBPROGRAMS. BBRW091
C      -----            BBRW092
C      TITING              BBRW093
C      . . . NO ESTIMATE AVAILABLE. BBRW094
C      -----            BBRW095
C      PROGRAM MODIFICATIONS BBRW099
C      -----            BBRW102
C      ***** START PROGRAM ***** BBRW103
C      100 FORMAT (//24H ***** WARNING ***** //7TH NO CONVERGENCE IN BBRWBWR109 BBRW106
C      1R SUBROUTINE, BROWWER MEAN ELEMENTS ARE NOT ACCURATE...//11//). BBRW107
C      -----            BBRW108
C      DIMENSION DUML(100) BBRW111
C      DIMENSION DA(6),AT(6),AL(6),A1(6),DUML(100),AF(6),DA(16),DTAT(6) BBRW112
C      -----            BBRW113
C      COMMON DUML,A110,DUHX,AC BBRW114
C      -----            BBRW115
C      K = 0 BBRW116
C      DO 10 N=1,6 BBRW117
C      10 A110(N) = AT(N) BBRW118
C      -----            BBRW119
C      1 CALL BRWRL BBRW120
C      CALL BRWRL(0.0,0.0) BBRW121
C      -----            BBRW122
C      K = K + 1 BBRW123
C      IF (K-J) 4,4,3 BBRW124
C      3 WRITE OUTPUT TAPE 3,100 BBRW125
C      PRINT 100 BBRW126
C      RETURN BBRW127
C      -----            BBRW128
C      4 DO 5 N=1,6 BBRW129
C      DAT(N) = AT(N) - AC(N) BBRW130
C      5 TDAT(N) = ABSF(DAT(N)) BBRW131
C      -----            BBRW132
C      6 CONTINUE BBRW133
C      7 RETURN BBRW134
C      -----            BBRW135
C      8 DO 9 N=1,6 BBRW136
C      9 A110(N) = A110(N) + DAT(N) BBRW137
C      A110(3) = ALL0T(A110(3)) BBRW138
C      A110(4) = ALL0T(A110(4)) BBRW139
C      A110(5) = ALL0T(A110(5)) BBRW140
C      A110(6) = ALL0T(A110(6)) BBRW141
C      GO TO 1 BBRW142
C      END BBRW143
C      SUBROUTINE BRWRL BBRW144
C      * CARDS COLUMN BBRW145
C      * LIST8 BBRW146
C      * LABEL BBRW147
C      * SUBROUTINE BRWRL BBRW148
C      -----            BBRW149
C      VERSION OF 07/17/63 BBRW150
C      FORTRAN SUBROUTINE BBRW151
C      FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094 BBRW152
C      -----            BBRW153
C      PURPOSE BBRW154
C      BRWRL AND BRWR2 CONVERT BROWWER MEAN ORBITAL ELEMENTS TO BBRW155
C      OSCILLATING ORBITAL ELEMENTS AND TO POSITION AND VELOCITY BBRW156
C      COMPONENTS. SECULAR AND LONG PERIOD COEFFICIENTS AND OTHER BBRW157
C      INTERMEDIATE QUANTITIES WHICH ARE FUNCTIONS OF THE MEAN BBRW158
C      ELEMENTS AND THE EARTH'S GRAVITATIONAL HARMONICS ONLY (I.E., DO NOT BBRW159
C      VARY WITH TIME AND ARE CONSTANT FOR ANY GIVEN SET OF MEAN BBRW160
C      ELEMENTS) ARE COMPUTED IN BRWRL AND PLACED IN COMMON. BRWR2 CAN BBRW161
C      THEN BE USED TO CALCULATE OSCILLATING ORBITAL ELEMENTS FOR ANY BBRW162
C      SPECIFIED VALUE OF DT (TIME ELAPSED FROM EPOCH OF MEAN BBRW163
C      ELEMENTS). COMMON IS USED TO TRANSFER INPUT TO SUBROUTINE BRWR2 BBRW164
C      FROM CALLING PROGRAM, CONSTANTS AND INTERMEDIATE CALCULATIONS FROM BBRW165
C      BRWRL TO BRWR2, AND TO RETURN OUTPUT FROM BRWR2 TO CALLING PROGRAM. BBRW166
C      -----            BBRW167
C      DUML IS A DUMMY VARIABLE INSERTED AS FIRST VARIABLE IN COMMON IN BBRW168
C      BRWRL AND BRWR2 TO PERMIT SHIFTING OF VARIABLES IN COMMON AREA IF BBRW169
C      DESIRED. THE DIMENSION OF DUML MAY BE CHANGED BUT SHOULD BE THE BBRW170
C      SAME IN SUBROUTINES BRWRL,BRWR2, AND THE CALLING PROGRAM. BBRW171
C      -----            BBRW172
C      CALLING SEQUENCE BBRW173
C      CALL BRWRL BBRW174
C      -----            BBRW175
C      INPUT VIA COMMON BBRW176
C      BROWWER MEAN ELEMENTS BBRW177
C      A110(1) = SEMI-MAJOR AXIS - KILOMETERS BBRW178
C      A110(2) = ECCENTRICITY BBRW179
C      A110(3) = INCLINATION - RADIANS BBRW180
C      A110(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS BBRW181

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C          AL10(5) = ARGUMENT OF PERIGEE.           - RADIANs         BRWR1037
C          A110(6) = MEAN ANOMALY                    - RADIANs         BRWR1038
C          BRWR1039
C          EARTHS GRAVITATIONAL CONSTANTS           BRWR1040
C          GP(1) = GM(PRODUCT OF G,THE GAUSSIAN CONSTANT SQUARED, AND     BRWR1042
C             M, THE MASS OF THE EARTH) - KM. CUBED/SEC. SQUARED           BRWR1043
C          GP(2) = K2. ZONAL HARMONIC              - KM. SQUARED           BRWR1045
C          GP(3) = K3 ) COEFFICIENTS OF THE         - KM. CUBED           BRWR1045
C          GP(4) = K4 ) EARTHS GRAVITATIONAL        - KM. 4TH POWER           BRWR1046
C          GP(5) = K5 ) FIELD                       - KM. 5TH POWER           BRWR1047
C          BRWR1048
C          ERR = TRUNCATION FACTOR REQUIRED IN       BRWR1049
C             FUNCTION XK6P ----- RADIANs         BRWR1050
C          BRWR1051
C          OUTPUT VIA COMMON                          BRWR1052
C          REFERENCE                                BRWR1053
C          DIRK BROWER - SOLUTION OF THE PROBLEM OF ARTIFICIAL           BRWR1055
C             SATELLITE THEORY WITHOUT DRAG -                               BRWR1057
C             THE ASTRONOMICAL JOURNAL, VOL. 64, NO. 9,                   BRWR1058
C             NOVEMBER 1959, PAGES 378 - 397                               BRWR1059
C          METHOD                                     BRWR1060
C          REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP     BRWR1061
C          BRWR1062
C          RESTRICTIONS                              BRWR1063
C          ***** BRWR1064
C          BRWR1065
C          ACCURACY                                  BRWR1066
C          BRWR1067
C          REQUIRED SUBPROGRAMS - FORTRAY 2 MONITOR           BRWR1068
C          SORT,CDS,STN BRWR1069
C          BRWR1070
C          REQUIRED SUBPROGRAMS - OTHER                      BRWR1071
C          NONE BRWR1072
C          BRWR1073
C          STORAGE REQUIREMENTS                        BRWR1074
C          666 WITHOUT REQUIRED SUBPROGRAMS               BRWR1075
C          BRWR1076
C          BRWR1077
C          TIMING                                     BRWR1078
C          NO ESTIMATE AVAILABLE BRWR1079
C          BRWR1080
C          BRWR1085
C          BRWR1086
C          PROGRAM MODIFICATIONS                     BRWR1087
C          NO MODIFICATIONS TO DATE BRWR1088
C          ***** START PROGRAM ***** BRWR1090
C          BRWR1092
C          BRWR1093
C          2 DIMENSIOND DUMI(100) BRWR1095
C          3 DIMENSION AL10(6),GP(5),AL1(6),A1(6),A(6),R,X(3),YX(3),EL(13),F(9), BRWR1096
C             I(9),C(12),D(23),G(13),X(28),S(3) BRWR1100
C          BRWR1106
C          4 COMMON DUMI,AL10,GP,ERR,AL1,A1,A,R,X,VX,EVD,CAI,DI,CII,ALI,UL, BRWR1107
C             I GI,UG,A1,UH,S,EL,A2,A3,R,C,D,5,X,F BRWR1109
C          BRWR1120
C          COMPUTE INTERMEDIATE QUANTITIES
C          BRWR1101
C          BRWR1102
C          BRWR1103
C          BRWR1104
C          BRWR1105
C          BRWR1107
C          BRWR1108
C          BRWR1109
C          BRWR1110
C          BRWR1111
C          BRWR1112
C          BRWR1113
C          BRWR1114
C          BRWR1115
C          BRWR1116
C          BRWR1117
C          BRWR1118
C          BRWR1119
C          BRWR1120
C          BRWR1121
C          BRWR1122
C          BRWR1123
C          BRWR1124
C          BRWR1125
C          BRWR1126
C          BRWR1127
C          BRWR1128
C          BRWR1129
C          BRWR1130
C          BRWR1131
C          BRWR1132
C          BRWR1133
C          BRWR1134
C          BRWR1135
C          BRWR1136

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39 D(8)=8.*D(4)/D(7) . . . . .BRWR1137
40 D(9)=5.*D(8)/D(7) . . . . .BRWR1138
41 D(10)=D(8)-D(6) . . . . .BRWR1139
42 D(11)=C(5)*I(5)*D(10)-4.*4.*D(5)-F(6)*D(10) . . .BRWR1140
43 D(12)=1.6666667*C(8)*(3.*D(10)-2.) . . . . .BRWR1141
44 D(13)=1.9444444+C(8)*I(10)+D(10)-D(5) . . . . .BRWR1142
45 D(14)=3.-15.*D(13)/D(7)+D(9) . . . . .BRWR1143
46 D(15)=G(8)*D(14) . . . . .BRWR1144
47 D(16)=F(6)*D(15) . . . . .BRWR1145
48 D(17)=0.33333333*D(13) . . . . .BRWR1146
49 D(18)=1.2962963*(D(15)+D(15)-C(8)) . . . . .BRWR1147
50 D(19)=3.*D(5) . . . . .BRWR1148
51 D(20)=D(6)+D(6) . . . . .BRWR1149
52 D(21)=2.-D(7) . . . . .BRWR1150
53 D(22)=C(10)*SQRT(F(10(51))) . . . . .BRWR1151
54 D(23)=4.*C(9)*D(1) . . . . .BRWR1152
55 F(8)=D(3)*2.*F(4) . . . . .BRWR1153
56 F(9)=(2.+5.*F(2))*D(8)-D(9)+F(3)*D(3).. . . .BRWR1154
57 G(1)=SINF(A11(10(3))) . . . . .BRWR1155
58 G(2)=B(1)*G(1) . . . . .BRWR1156
59 G(3)=A11(2)+D(1) . . . . .BRWR1157
60 G(4)=G(3)*D(1) . . . . .BRWR1158
61 G(5)=G(3)/G(1) . . . . .BRWR1159
62 G(6)=G(4)/G(1) . . . . .BRWR1160
63 G(7)=B(1)*G(1) . . . . .BRWR1161
64 G(8)=G(7)/A11(2) . . . . .BRWR1162
65 G(9)=A11(2)*G(1) . . . . .BRWR1163
66 G(10)=G(3)+D(3) . . . . .BRWR1164
67 G(11)=B(1)/A11(2) . . . . .BRWR1165
68 G(12)=5.*G(11) . . . . .BRWR1166
69 G(13)=G(11)*C(9) . . . . .BRWR1167
C C C C C
      COMPUTE *MEAN* MEAN MOTION
C C C C C
70 ENO=SQRTF(GP(1)/A3)
C C C C C
      COMPUTE COEFFICIENTS OF SECULAR TERMS
C C C C C
71 S(1)=ENO*(1.+8*(2)+C(2)*D(6)+C(3)*(16.-8*(2)-15.+8(6)+130.-96.*8(2)*
1.-90.*8(1)+D(3)+105.+144.*8(2)+8(6)*D(4)+C(4)*F(2)+3.-30.*D(3))
2*35.*D(4)) . . . . .BRWR1177
72 S(2)=ENO*(C(2)+D(7)+C(3)*(24.*8(2)-35.*8(6)+90.-192.*8(2)-8(7))+
10(3)+385.*36.*8(1)+49.*8(11)+D(4))+3333333*C(4)*(21.-8(5)+
2(8(7)-2(7))*D(3)+385.-189.*8(1))+D(6)) . . . . .BRWR1178
73 S(3)=ENO*(4.*D(11)+C(3)*8(5)-5.+12.*8(2)-D(3)+35.*36.*8(2)+5.*
18(11))+.3333333*C(4)*(5.-3.*8(11))*(3.-7.*D(3))-C(2)*D(2)) . . .BRWR1181
C C C C C
      COMPUTE COEFFICIENTS OF LONG PERIOD TERMS
C C C C C
74 EL(1)=8(3)+D(11) . . . . .BRWR1182
75 EL(2)=8(2)+G(6)*I(-C(7)-4.*F(5)+D(12)) . . . . .BRWR1183
76 EL(3)=G(3)+8(3)*D(13) . . . . .BRWR1184
77 EL(4)=5.*C(6)*F(7)-3.*F(8)+F(9)-.41666667E-14C(2)*F(7)-11.*
I(8)+5.*F(9) . . . . .BRWR1185
78 EL(5)=C(7)+G(11)/F(1)-G(6)+D(12)+((G(8)-G(6))*F(6)+3(9)+(25.0+
IF(5)))-G(4)+G(11)+D(16) . . . . .BRWR1186
79 EL(6)=G(9)*D(18)+G(10)-D(17)*(3.0+F(3)-G(10)/G(2)) . . . . .BRWR1187
80 EL(7)=G(3)+A11(2)*(C(6)+D(14)-C(5)+15.*D(14)-4.) . . . . .BRWR1194
81 EL(8)=G(5)*C(7)+F(6)+D(12)+G(2)+D(16) . . . . .BRWR1195
82 EL(9)=G(5)*F(2)+(-D(17)-D(18)+G(2)) . . . . .BRWR1196
83 EL(10)=B(1)*F(1)+D(11) . . . . .BRWR1197
84 EL(11)=G(7)+C(7)+F(6)+D(12) . . . . .BRWR1198
85 EL(12)=F(12)*D(13)+D(13) . . . . .BRWR1199
86 EL(13)=-G(3)/G(7) . . . . .BRWR1200
87 RETURN
C C C C C
      END
      SUBROUTINE BRWR2 FORTRAN SOURCE PROGRAM
      * CARDS COLUMN
      * LISTB
      * LABEL
      * SUBROUTINE BRWR2(OT,EN2)
C C C C C
      VERSION OF 01/31/64
      FORTRAN SUBROUTINE
      FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
      PURPOSE
      CALLING SEQUENCE
      CALL BRWR2(OT,EN2)
      INPUT
      DT = TIME ELAPSED FROM EPOCH OF MEAN ELEMENTS - SECONDS
      SEE SUBROUTINE BRWR1 FOR INPUT VIA COMMON
      OUTPUT VIA COMMON
      OSCILLATING ORBITAL ELEMENTS AT TIME T = EPOCH TIME + DT
      A(1) = SEMI-MAJOR AXIS - KILOMETERS
      A(2) = ECCENTRICITY - DIMENSIONLESS
      A(3) = INCLINATION - RADIAN
      A(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIAN
      A(5) = ARGUMENT OF PERIGEE - RADIAN
      A(6) = MEAN ANOMALY - RADIAN
C C C C C

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	37 X(12)=X(6)*X(9)+B(2)		BRWR2130
	38 X(13)=X(9)*X(7)-A110(21)		BRWR2131
	X12 = X(12)		BRWR2132
D	DX12 = X12		BRWR2133
D	X13 = X(13)		BRWR2134
	DX13 = X13		BRWR2135
	X(14) = ATANQ(DX12,DX13)		BRWR2136
	40 X(15)=G1+G1		BRWR2137
	41 X(16)=X(15)*X(14)		BRWR2138
	42 X(17)=X(16)*X(14)		BRWR2139
	43 X(18)=X(17)*X(14)		BRWR2140
	44 X(19)=SINF(X(16))		BRWR2141
	45 X(20)=SINF(X(18))		BRWR2142
	46 X(21)=COSF(X(17))		BRWR2143
	47 X(22)=D(6)+X(11)-B(8)		BRWR2144
	48 X(23)=D(19)*X(21)		BRWR2145
	49 X(24)=A110(2)*13.+COSF(X(16))+COSF(X(18))		BRWR2146
	50 X(25)=X(9)+B(1)*X(10)		BRWR2147
	51 X(26)=G(13)+D(20)*X(12)+X(25)*1.+D(19)*((-X(25))*X(19)+		BRWR2148
	1(X(25)+.33333333)*X(20))		BRWR2149
	52 X(27)=6.+X(14)-A110(2)*X(12)		BRWR2150
	53 X(28)=5.+SINF(X(17))+A110(2)*X(19))+A110(2)*X(20)		BRWR2151
C	COMPUTE OSCILLATING ELEMENTS		BRWR2152
C			BRWR2153
C	54 A(1)=A110(1)+1.+C(1)*X(22)+X(11)*X(23))		BRWR2154
C	55 A(2) = A110(2)+D(6)+G(12)+C(1)+X(22)+X(23)+X(11)-B(9))-D(23)+		BRWR2155
	1X(24))		BRWR2157
	56 A(3)=A110(3)+D(1)+D(22)+13.+X(21)*X(25))		BRWR2158
	57 U(1)=A110(2)+X(26)		BRWR2159
	58 U(2)=G1+X(26)+C(9)+D(7)*X(27)+D(21)*X(28)		BRWR2150
	59 U(3)=H1-C(10)+X(27)-X(28)		BRWR2151
	60 A(6)=ALLTOT(L)		BRWR2152
	61 A(5)=ALLTOT(U)		BRWR2153
	62 A(4)=ALLTOT(W)		BRWR2154
			BRWR2155
C	COMPUTE POSITION AND VELOCITY COMPONENTS		BRWR2156
			BRWR2157
	63 CALL ELRV (RX,VX,A,P,EN,GP(1),ERR)		BRWR2158
	RETURN		BRWR2159
	END		BRWR2170
*	FUNCTION DJUL FORTRAN SOURCE PROGRAM		DJUL 000
*	CARDS COLUMN		DJUL 001
*	LISTB		DJUL 002
*	LABEL		
	FUNCTION DJUL(NM,ND,NY)		DJUL 003
	VERSION OF 07/22/63		DJUL 004
	FORTRAN FUNCTION		DJUL 005
	FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094		DJUL 006
	PURPOSE		DJUL 007
	COMPUTES JULIAN DATE AT 0 HOURS UNIVERSAL TIME (OR		DJUL 008
	0 HOURS EPHEMERIS TIME).		DJUL 009
	CALLING SEQUENCE		DJUL 010
	NAME = DJUL(NM,ND,NY)		DJUL 011
	INPUT		DJUL 012
	NM = CALENDAR MONTH		DJUL 013
	ND = CALENDAR DAY		DJUL 014
	NY = CALENDAR YEAR		DJUL 015
	OUTPUT		DJUL 016
	NAME = JULIAN DATE AT 0 HOURS UNIVERSAL TIME		DJUL 017
	REFERENCE		DJUL 018
	REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP		DJUL 019
	METHOD		DJUL 020
	THE NUMBER OF DAYS WHICH HAVE ELAPSED FROM 12 HOURS		DJUL 021
	UNIVERSAL TIME JAN. 0, 1800 ARE COUNTED AND ADDED TO THE		DJUL 022
	JULIAN DATE OF 12 HOURS UNIVERSAL TIME OF JAN. 0, 1800.		DJUL 023
	RESTRICTIONS		DJUL 024
	DATE RESTRICTED TO LIE BETWEEN JANUARY 1, 1801 AND DECEMBER		DJUL 025
	31, 2000.		DJUL 026
	ACCURACY		DJUL 027
	EXACT BINARY REPRESENTATION WITHIN DATE LIMITATIONS.		DJUL 028
	REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR		DJUL 029
	NONE		DJUL 030
	REQUIRED SUBPROGRAMS - OTHER		DJUL 031
	NONE		DJUL 032
	STORAGE REQUIREMENTS		DJUL 033
	153		DJUL 034
	TIMING		DJUL 035
	NONE ESTIMATE AVAILABLE		DJUL 036
			DJUL 037
			DJUL 038
			DJUL 039
			DJUL 040
			DJUL 041
			DJUL 042
			DJUL 043
			DJUL 044
			DJUL 045
			DJUL 046
			DJUL 047
			DJUL 048
			DJUL 049
			DJUL 050
			DJUL 054

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C      PROGRAM_MODIFICATIONS
C      NO MODIFICATIONS TO DATE
C ***** START PROGRAM *****
C      2 DIMENSION RM(12)
C      5 RM(1)=0.0
C      6 RM(2)=31.0
C      7 RM(3)=28.0
C      8 RM(4)=31.0
C      9 RM(5)=30.0
C     10 RM(6)=31.0
C     11 RM(7)=30.0
C     12 RM(8)=31.0
C     13 RM(9)=3.0
C     14 RM(10)=30.0
C     15 RM(11)=31.0
C     16 RM(12)=30.0
C
C     17 Y=NY-1800
C     18 YL=INTF((Y-1.0)/4.0)
C     19 YC=INTF((Y+99.0)/100.0)-1.0
C     20 RY=Y-YL
C     21 DJUL=RY*365.0+YL*366.0-YC+2378495.5
C     22 TD=ND
C     23 DD 24, N=1, NM
C     24 DJUL=DJUL+RM(N)
C     25 IF (NM-2) 29, 29, 26
C     26 IF (Y-100.0) 27, 29, 27
C     27 IF (XMOD(NY,4)) 29, 28, 29
C     28 DJUL=DJUL+1.0
C     29 DJUL=DJUL+TD
C     RETURN
C     END
C
C * FUNCTION DMSRZ  FORTRAN SOURCE PROGRAM
C * CARDS COLUMN
C * LISTD
C * LABEL
C * FUNCTION DMSRZ(ID,IM,AS)
C
C     VERSION OF 07/22/63
C     FORTRAN FUNCTION
C     FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
C
C     PURPOSE
C     CONVERTS DEGREES, MINUTES, AND SECONDS OF ANGLE OR ARC TO
C     RADIANS (360 DEGREES = 2 PI RADIANS).
C
C     CALLING SEQUENCE
C     D  NAME = DMSRZ(ID,IM,AS)
C
C     INPUT
C     ID = NUMBER OF DEGREES IN ANGLE OR ARC
C     IM = NUMBER OF MINUTES IN ANGLE OR ARC
C     AS = NUMBER OF SECONDS IN ANGLE OR ARC
C
C     SIGN OF THE INPUT ANGLE OR ARC NEED ONLY BE
C     ASSOCIATED WITH THE NUMBER OF DEGREES (ID).
C
C     OUTPUT
C     NAME = ANGLE OR ARC IN RADIANS
C
C     NAME IS RETURNED TO CALLING PROGRAM IN DOUBLE PRECISION
C     FORM.
C
C     REFERENCE
C     *****
C
C     METHOD
C     *****
C
C     RESTRICTIONS
C     *****
C
C     ACCURACY
C     WHEN NECESSARY, INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE
C     PRECISION SO THAT THE VALUE OF THE OUTPUT ARGUMENT IS
C     AVAILABLE TO CALLING PROGRAM IN DOUBLE PRECISION.
C
C     REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
C     (DFMP),(DFAD)
C
C     REQUIRED SUBPROGRAMS - OTHER
C     NONE
C
C     STORAGE REQUIREMENTS
C     135 WITHOUT REQUIRED SUBPROGRAMS
C
C     TIMING
C     NO ESTIMATE AVAILABLE

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DJUL 257
DJUL 258
DJUL 260
DJUL 261
DJUL 262
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DJUL 292
DJUL 293
DMSRZ030
DMSRZ031
DMSRZ032
DMSRZ033
DMSRZ034
DMSRZ035
DMSRZ036
DMSRZ037
DMSRZ038
DMSRZ039
DMSRZ040
DMSRZ041
DMSRZ042
DMSRZ043
DMSRZ044
DMSRZ045
DMSRZ046
DMSRZ047
DMSRZ048
DMSRZ049
DMSRZ050
DMSRZ051
DMSRZ052
DMSRZ053
DMSRZ054
DMSRZ055
DMSRZ059

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DMSR2062
C PROGRAM MODIFICATIONS ..DMSR2063
C NO MODIFICATIONS TO DATE ..DMSR2065
C ***** START PROGRAM ***** ..DMSR2067
DMSR2068
2 AD=ID ..DMSR2069
3 AM=IN ..DMSR2070
4 AM=SIGN(IAH,AD) ..DMSR2071
5 ARS= SIGN(AS,AD) ..DMSR2072
D 6 DMSRZ=AD*.1748329251994330E-1 C AM*.290888208657216E-3 ..DMSR2073
1 + ARS*.4848136811095360E-5 ..DMSR2074
RETURN
END ..DMSR2076
* FUNCTION DOTZ FORTRAN_SOURCE PROGRAM
* CARDS COLUMN
* LISTS
* LABEL
1 FUNCTION DOTZ(X,Y)
VERSION OF 7/22/63
COMPUTES THE ANGLE BETWEEN VECTORS X AND Y.
INPUT, OUTPUT, AND INTERNAL ARITHMETIC OPERATIONS
ARE ALL PERFORMED IN DOUBLE PRECISION.
INPUT
VECTOR X IN ANY UNITS.
VECTOR Y IN ANY UNITS, NOT NECESSARILY THE SAME
UNITS AS VECTOR X.
OUTPUT
DOTZ = ANGLE IN RADIANS BETWEEN X AND Y.
DOTZ LIES BETWEEN 0 AND PI RADIANS.
REQUIRED SUBPROGRAMS
NONE
D 2 DIMENSION X(3),Y(3)
D 3 C=(X(1)*Y(1)+X(2)*Y(2)+X(3)*Y(3))/((SORTF(X(1)**2+X(2)**2+X(3)**2)
D 1 )*(SORTF(Y(1)**2+Y(2)**2+Y(3)**2)))
D A = 1.0 - C*C
D A = ABS(FIA)
D 4 S = SORT(FIA)
D 5 DOTZ=ATAN2(F(S,C))
D 6 RETURN
D 7 END
* SUBROUTINE ELRV FORTRAN SOURCE PROGRAM ELRV 000
* CARDS COLUMN ELRV 031
* LISTS ELRV 032
* LABEL
* SUBROUTINE ELRV(X,VX,A,P,EN,GM,ERR) ELRV 033
VERSION OF 03/02/64 ELRV 034
FORTRAN SUBROUTINE ELRV 035
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094 ELRV 036
PURPOSE ELRV 039
CONVERTS OSCULATING ORBITAL ELEMENTS INTO GEOCENTRIC ELRV 010
EQUATORIAL INERTIAL RECTANGULAR COORDINATES OF POSITION ELRV 111
AND VELOCITY. ELRV 112
ELRV 113
CALLING SEQUENCE ELRV 114
DIMENSION X(3),VX(3),A(6) ELRV 115
CALL ELRV(X,VX,A,P,EN,GM,ERR) ELRV 116
ELRV 117
INPUT ELRV 118
A(1) = SEMI-MAJOR AXIS - ELRV 020
A(2) = ECCENTRICITY - DIMENSIONLESS ELRV 020
A(3) = INCLINATION - RADIANS ELRV 021
A(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS ELRV 022
A(5) = ARGUMENT OF PERIGEE - RADIANS ELRV 023
A(6) = MEAN ANOMALY - RADIANS ELRV 024
ELRV 025
GM = THE PRODUCT OF G, THE GAUSSIAN CONSTANT SQUARED, ELRV 026
AND R, THE MASS OF THE EARTH ELRV 027
ERR = TRUNCATION FACTOR REQUIRED IN FUNCTION XKEP ELRV 029
IN RADIANS ELRV 030
OUTPUT ELRV 031
X(1) ELRV 032
X(2) THE 3 RECTANGULAR COORDINATES OF POSITION ELRV 033
X(3) ELRV 034
VX(1) ELRV 035
VX(2) THE 3 RECTANGULAR COMPONENTS OF VELOCITY ELRV 036
VX(3) ELRV 037
P = ANOMALISTIC PERIOD ELRV 041
EN = MEAN ANGULAR MOTION ELRV 042
ELRV 043

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UNIT'S OF INPUT ARGUMENTS A(1) AND GM ARE ARBITRARY          ERLV 044
BUT MUST BE MUTUALLY CONSISTENT.                            ERLV 045
-----
UNIT'S OF OUTPUT ARGUMENTS X, VX, P, AND EN WILL DEPEND    ERLV 046
UPON THE UNITS EMPLOYED FOR A(1) AND GM.                    ERLV 047
-----
REFERENCE                                                     ERLV 048
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP    ERLV 049
METHOD                                                         ERLV 050
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP    ERLV 051
RESTRICTIONS                                                  ERLV 052
ECCENTRICITY MUST BE LESS THAN 1.0.                          ERLV 053
ACCURACY                                                       ERLV 054
REFER TO ACCURACY TESTS IN SUBPROGRAM WRITEUP.              ERLV 055
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR                      ERLV 056
  SQRT,SIN,COS                                                ERLV 057
REQUIRED SUBPROGRAMS - OTHER                                  ERLV 058
  D9/12/63 XKEP .                                             ERLV 059
STORAGE REQUIREMENTS                                         ERLV 060
290 WITHOUT REQUIRED SUBPROGRAMS                              ERLV 061
TIMING                                                         ERLV 062
NO ESTIMATE AVAILABLE .                                       ERLV 063
PROGRAM MODIFICATIONS                                         ERLV 064
***** START PROGRAM *****
DIMENSION X(3),VX(3),A(6)
3 E=XKEP(A(6),A(2),SE,CE,ERR)
4 X1=1.0-A(2)*CE
5 X2=1.0/X1
6 R=A(1)*X1
7 X3=SQRT(1.0-A(2)**2)
8 RTGM=SQRT(GM*A(1))
SA = SIN(A(5))
SB = SIN(A(3))
SC = SIN(A(4))
CA = COS(A(5))
CB = COS(A(3))
CC = COS(A(4))
COMPUTE POSITION COORDINATES
Q1 = A(1)+(CE-A(2))
Q2 = A(1)+X3*SE
V = Q1*CA - Q2*SA
W = Q2*CA + Q1*SA
Z = CB*W
X(1) = CC*V - SC*Z
X(2) = CC*Z + SC*V
X(3) = SB*W
COMPUTE VELOCITY COMPONENTS
QD1 = -RTGM*SE/R
QD2 = RTGM*X3*CE/R
V = QD1*CA - QD2*SA
W = QD2*CA + QD1*SA
Z = CB*W
VX(1) = CC*V - SC*Z
VX(2) = CC*Z + SC*V
VX(3) = SB*W
RTGM = SQRT(GM)
RTA = SQRT(A(1))
FV = RTGM/(RTA*A(1))
P = 6.283 185 31/EN
RETURN
END
SUBROUTINE ERLV2 FORTRAN SOURCE PROGRAM                      ERLV200
CARDS COLUMN                                               ERLV201
LISTS                                                       ERLV202
LABEL                                                       ERLV203
SUBROUTINE ERLV2(X,VX,A,P,CY,GM,ERR)                       ERLV204
VEASION DF 33/32/64                                         ERLV205
FORTRAN SUBROUTINE                                         ERLV206
FOR USE WITH FORTRAN 2 MONITOR Z MONITOR JN 04 7093, 7094 ERLV207
PURPOSE                                                      ERLV208
CONVERTS OSCILLATING ORBITAL ELEMENTS INTO GEOCENTRIC     ERLV209
EQUATORIAL INERTIAL RECTANGULAR COORDINATES OF POSITION    ERLV210
AND VELOCITY.                                               ERLV211
CALLING SEQUENCE                                             ERLV212

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C
D DIMENSION X(3), VX(3), A(6) ELRVZ215
D CALL ELRVZ(A, VX, A, P, EN, GH, ERR) ELRVZ216
C ELRVZ217
C ELRVZ218
C INPUT ELRVZ219
C A(1) = SEMI-MAJOR AXIS ELRVZ220
C A(2) = ECCENTRICITY, DIMENSIONLESS ELRVZ221
C A(3) = INCLINATION, RADIANS ELRVZ222
C A(4) = RIGHT ASCENSION OF ASCENDING NODE, RADIANS ELRVZ223
C A(5) = ARGUMENT OF PERIGEE, RADIANS ELRVZ224
C A(6) = MEAN ANOMALY, RADIANS ELRVZ225
C GH = THE PRODUCT OF G, THE GAUSSIAN CONSTANT SQUARED, ELRVZ226
C AND H, THE MASS OF THE EARTH ELRVZ227
C ERR = TRUNCATION FACTOR REQUIRED IN XKEPZ FUNCTION ELRVZ229
C IN RADIANS ELRVZ230
C ELRVZ231
C UNITS OF INPUT ARGUMENTS A(1) AND GH ARE ARBITRARY ELRVZ232
C BUT MUST BE MUTUALLY CONSISTENT. ELRVZ233
C INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN ELRVZ234
C DOUBLE PRECISION FORM. ELRVZ235
C OUTPUT ELRVZ237
C X(1) ELRVZ238
C X(2) THE 3 RECTANGULAR COORDINATES OF POSITION ELRVZ239
C X(3) ELRVZ240
C ELRVZ241
C VX(1) ELRVZ242
C VX(2) THE 3 RECTANGULAR COMPONENTS OF VELOCITY ELRVZ243
C VX(3) ELRVZ244
C ELRVZ245
C P = ANOMALISTIC PERIOD ELRVZ246
C EN = MEAN ANGULAR MOTION ELRVZ247
C ELRVZ248
C UNITS OF OUTPUT ARGUMENTS X, VX, P, AND EN WILL DEPEND ELRVZ249
C UPON THE UNITS EMPLOYED FOR A(1) AND GH. ELRVZ250
C OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE ELRVZ251
C FORM. ELRVZ252
C ELRVZ253
C REFERENCE ELRVZ254
C REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP ELRVZ255
C ELRVZ256
C METHOD ELRVZ257
C REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP ELRVZ258
C ELRVZ259
C RESTRICTIONS ELRVZ260
C ECCENTRICITY MUST BE LESS THAN 1.0. ELRVZ261
C ELRVZ262
C ACCURACY ELRVZ263
C REFER TO ACCURACY TESTS IN SUBPROGRAM WRITEUP. ELRVZ264
C INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION. ELRVZ265
C ELRVZ266
C REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR ELRVZ267
C (DFMP), (DFAD), (DFOP), DEXPT2, DSORT, DSTN, DCOS, (D=SB) ELRVZ268
C ELRVZ269
C REQUIRED SUBPROGRAMS - OTHER ELRVZ270
C 09/12/63 XKEPZ ELRVZ271
C ELRVZ272
C STORAGE REQUIREMENTS ELRVZ273
C 843 WITHOUT REQUIRED SUBPROGRAMS ELRVZ274
C ELRVZ275
C TIMING ELRVZ276
C NO ESTIMATE AVAILABLE ELRVZ277
C ELRVZ278
C PROGRAM MODIFICATIONS ELRVZ279
C ELRVZ280
C ELRVZ281
C ***** START PROGRAM ***** ELRVZ282
C ELRVZ283
C DIMENSION V(3), VX(3), A(6) ELRVZ284
C ELRVZ285
C A1=A(1) ELRVZ286
C A2=A(2) ELRVZ287
C A3=A(3) ELRVZ288
C A4=A(4) ELRVZ289
C A5=A(5) ELRVZ290
C A6=A(6) ELRVZ291
C 4 E=XKEPZ(A6, A2, SE, CE, ERR) ELRVZ292
C 7 X1=1.0-A(2)*CE ELRVZ293
C 8 X2=1.0/X1 ELRVZ294
C 9 R=A(1)*X1 ELRVZ295
C 10 DUM(1)=3-A2**2 ELRVZ296
C 11 RTGMA=SQRTF(GMA*1) ELRVZ297
C SA = SINP(A5) ELRVZ298
C SB = SINP(A3) ELRVZ299
C SC = SINP(A4) ELRVZ300
C CA = COSF(A5) ELRVZ301
C CB = COSF(A3) ELRVZ302
C CC = COSF(A4) ELRVZ303
C COMPUTE POSITION COORDINATES ELRVZ304
C ELRVZ305

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D Q1 = A(1)*(CE-A(2))
D Q2 = A(1)*X3+SE
D V = Q1*CA - Q2*SA
D W = Q2*CA + Q1*SA
D Z = CB*W
D X(1) = CC*V - SC*Z
D X(2) = CC*Z + SC*V
D X(3) = SB*W
C
C COMPUTE VELOCITY COMPONENTS
C
D QD1 = -RTGMA*SE/R
D QD2 = RTGMA*X3+CE/R
D V = QD1*CA - QD2*SA
D W = QD2*CA + QD1*SA
D Z = CB*W
D VX(1) = CC*V - SC*Z
D VX(2) = CC*Z + SC*V
D VX(3) = SB*W
C
C RTGM=SQRTF(GM)
C RTA=SQRTF(A1)
C ENH=RTGM/RTA*A(1)
D P=6.283185307179586/EN
C RETURN
C
* FUNCTION EQN FORTRAN SOURCE PROGRAM
* CARDS COLUMN
* LISTB
* LABEL
* FUNCTION EQN(DJ,ET,DPSI,DE,E)
C
C VERSION OF 02/27/64
C FORTRAN FUNCTION
C FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
C
C PURPOSE
C COMPUTES NUTATION IN LONGITUDE, NUTATION
C IN OBLIQUITY, TRUE OBLIQUITY OF DATE AND NUTATION
C IN RIGHT ASCENSION (EQUATION OF THE EQUINOXES).
C
C CALLING SEQUENCE
C NAME = EQN(DJ,ET,DPSI,DE,E)
C
C INPUT
C DJ = JULIAN DATE AT 0 HOURS EPHEMERIS TIME
C ET = EPHEMERIS TIME IN HOURS
C
C OUTPUT
C DPSI = NUTATION IN LONGITUDE - RADIANS
C DE = NUTATION IN OBLIQUITY - RADIANS
C C = TRUE OBLIQUITY OF DATE - RADIANS
C .NAME = NUTATION IN RIGHT ASCENSION - RADIANS
C (EQUATION OF THE EQUINOXES)
C
C REFERENCE
C THE FORMULATION BY EDGAR W. WOOLARD MAY BE FOUND IN
C 4 PUBLICATIONS -
C
C 1. ASTRONOMICAL PAPERS PREPARED FOR THE USE OF THE
C AMERICAN EPHEMERIS AND NAUTICAL ALMANAC - VOLUME 15,
C PART 1, PAGE 153 (THEORY OF THE ROTATION OF THE
C EARTH AROUND ITS CENTER OF MASS - BY FOSAR H.
C WOOLARD)
C
C 2. IMPROVED LUNAR EPHEMERIS 1952-1959 - A JOINT
C SUPPLEMENT TO THE AMERICAN EPHEMERIS AND THE
C (BRITISH) NAUTICAL ALMANAC - PAGES IX AND X.
C
C AND THE AMERICAN EPHEMERIS AND NAUTICAL ALMANAC -
C PAGES 44 AND 45.
C
C 3. ASTRONOMICAL JOURNAL, 1953 FEBRUARY, VOL. 58, NO. 1
C PAGES 1-3 (A DEVELOPMENT OF THE THEORY OF NUTATION)
C - BY EDGAR W. WOOLARD)
C
C METHOD
C
C RESTRICTIONS
C ALL PERIODIC TERMS IN WOOLARD'S THEORY WITH COEFFICIENTS
C LESS THAN 0.001 SECONDS OF ARC HAVE BEEN NEGLECTED. ALL
C SECULAR PORTIONS OF THE COEFFICIENTS HAVE BEEN NEGLECTED
C WHENEVER THE SECULAR COEFFICIENTS ARE LESS THAN 0.001
C SECONDS OF ARC.
C
C REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
C (DFAD), (DFSH), (DFHP), (DFDP), DADD, COS, SIN
C
C REQUIRED SUBPROGRAMS - OTHER
C NONE
C
C TIMING
C 9.4 MILLISECONDS ON 7094
C
C STORAGE REQUIREMENTS

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ELRVZ118
ELRVZ119
ELRVZ120
ELRVZ121
ELRVZ122
ELRVZ123
ELRVZ124
ELRVZ125
ELRVZ126
ELRVZ127
ELRVZ128
ELRVZ129
ELRVZ130
ELRVZ131
ELRVZ132
ELRVZ133
ELRVZ134
ELRVZ135
ELRVZ136
ELRVZ137
ELRVZ138
ELRVZ139
ELRVZ140
ELRVZ141
ELRVZ142
ELRVZ143
EQV 000
EQV 001
EQV 002
EQV 003
EQV 004
EQV 005
EQV 006
EQV 007
EQV 008
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EQV 054
EQV 055
EQV 056

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----- EQN 367
1096 WITHOUT REQUIRED SUBPROGRAMS EQN 368
1329 WITH REQUIRED SUBPROGRAMS EQN 369
----- EQN 370
PROGRAM MODIFICATIONS EQN 371
----- EQN 372
NOTE: A 7094 FAP VERSION OF EQN IS AVAILABLE USING THE SAME EQN 384
CALLING SEQUENCE AS THE FORTRAN VERSION. THE FAP VERSION EQN 385
REQUIRES 725 STORAGE LOCATIONS WITHOUT REQUIRED SUBPROGRAMS EQN 386
AND 830 LOCATIONS WITH REQUIRED SUBPROGRAMS. COMPUTING EQN 388
TIME FOR THE FAP VERSION IS 6.6 MILLISECOND ON 7094. EQN 389
----- EQN 390
***** START PROGRAM ***** EQN 391
----- EQN 392
DIMENSION SCF(36),S(36),CCE(19),C(19) EQN 393
----- EQN 394
COMPUTE NUMBER OF JULIAN CENTURIES OF 36525.0 DAYS EXACTLY WHICH EQN 395
HAVE ELAPSED FROM 1900 JAN. 0.5 DAYS EPHEMERIS TIME. EQN 396
----- EQN 397
PRT1=DJ-2415020.0 EQN 398
PRT2=ET/24.0 EQN 399
T=(PRT1+PRT2)/36525.0 EQN 400
T2=T*T EQN 401
T3=T*T2 EQN 402
----- EQN 403
COMPUTE FUNDAMENTAL ARGUMENTS EQN 404
----- EQN 405
MEAN ANOMALY - MOON EQN 406
----- EQN 407
X = 0.160 424 847 E-3 *T2 + 0.251 133 E-6 * T3 EQN 408
EL = 5.168 000 345 745 + X + 8328.691 103 668 024 * T EQN 409
----- EQN 410
MEAN ANOMALY - SUN EQN 411
----- EQN 412
X = 0.261 799 4 E-5 *T2 + 0.581 78 E-7 * T3 EQN 413
EL1 = 6.256 583 580 497 - X + 628.301 945 726 742 * T EQN 414
----- EQN 415
MEAN ARGUMENT OF LATITUDE - HDON EQN 416
----- EQN 417
X = 0.560 444 62 E-4 *T2 + 0.581 8 E-8 * T3 EQN 418
F = 0.196 365 054 887 - X + 8433.466 291 171 947 * T EQN 419
----- EQN 420
MEAN ELONGATION OF MOON FROM SUN EQN 421
----- EQN 422
X = 0.250 648 67 E-4 *T2 - 0.329 67 E-7 * T3 EQN 423
D = 6.121 523 942 807 - X + 7771.377 193 934 485 * T EQN 424
----- EQN 425
LONGITUDE OF MEAN ASCENDING NODE - HDON EQN 426
----- EQN 427
X = 0.362 640 63 E-4 *T2 + 0.387 85 E-7 * T3 EQN 428
D = 4.523 601 514 852 + X - 33.757 146 246 552 * T EQN 429
----- EQN 430
REDUCE ALL ANGLES BY MODULUS 2 PI. EQN 431
----- EQN 432
EL = MODF(EL,6.283 185 307 179 586) EQN 433
EL1 = MODF(EL1,6.283 185 307 179 586) EQN 434
F = MODF(F,6.283 185 307 179 586) EQN 435
D = MODF(D,6.283 185 307 179 586) EQN 436
U = MODF(U,6.283 185 307 179 586) EQN 437
----- EQN 438
COMPUTE SINES AND COSINES OF FUNDAMENTAL ARGUMENTS AND EQN 439
COMBINATIONS OF THE FUNDAMENTAL ARGUMENTS. EQN 440
----- EQN 441
S(1) = SIN(F) EQN 442
C(1) = COS(F) EQN 443
S(3) = 2.0*S(1)*C(1) EQN 444
C(3) = C(1)**2-S(1)**2 EQN 445
SF = SIN(F) EQN 446
CF = COS(F) EQN 447
S(25) = 2.0*SF*CF EQN 448
C2F = CF**2-SF**2 EQN 449
SD = SIN(D) EQN 450
CD = COS(D) EQN 451
S(14) = 2.0*SD*CD EQN 452
C2D = CD**2-SD**2 EQN 453
S(4) = S(25)*C(3)+C2F *S(3) EQN 454
C(4) = C2F *C(3)-S(25)*S(3) EQN 455
AL = S(4)*C2D EQN 456
AL1 = C(4)*S(14) EQN 457
AL2 = S(4)*S(14) EQN 458
AL3 = C(4)*C2D EQN 459
S(2) = AL -AL1 EQN 460
C(2) = AL3*AL2 EQN 461
S(21) = AL +AL1 EQN 462
C(16) = AL3-AL2 EQN 463
S(5) = SIN(EL1) EQN 464
CL1 = COS(EL1) EQN 465
S(28) = 2.0*S(5)*CL1 EQN 466
C2L1 = CL1**2-S(5)**2 EQN 467
S(6) = SIN(EL) EQN 468
CL = COS(EL) EQN 469
S(22) = 2.0*S(6)*CL EQN 470

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C2L = CL**2-S(6)**2
S(8) = S(25)*C(11)+C2F *S(11)
C(6) = C2F *C(11)-S(25)*S(11)
BE = S(2)*CL1
BE1 = C(2)+S(5) --
BE2 = S(2)+S(5)
BE3 = C(2)+C1
S(7) = BE +BE1
C(5) = BE3-BE2
S(10) = BE -BE1
C(8) = BE3+BE2
GA = S(4)*CL
GA1 = C(4)+S(6)
GA2 = S(4)+S(6) --
GA3 = C(4)+CL
S(9) = GA +GA1
C(7) = GA3-GA2
S(13) = GA -GA1
C(10) = GA3+GA2
S(11) = S(6)*C2D-CL *S(14)
CT = CL *C2D+S(6)*S(14)
S(12) = S(8)*C2D-C(6)*S(14)
C(9) = C(6)+C2D*S(8)+S(12)
DE = S(1)*CL
DE1 = C(1)*S(6)
DE2 = S(1)*S(6)
DE3 = C(1)*CL
S(15) = DE +DE1
C(11) = DE3-DE2
S(16) = DE -DE1
C(12) = DE3+DE2
S(17) = S(21)*CL -C(16)*S(6)
C(15) = C(16)*CL +S(21)*S(6)
S(18) = S(8)*C2L-C(6)*S(22)
C(13) = C(6)*C2L+S(8)*S(22)
S(19) = S(22)*C2D-C2L *S(14)
EP = S(8)*CL
EP1 = C(6)*S(6)
EP2 = S(8)*S(6)
EP3 = C(6)*CL
S(20) = EP +EP1
C(14) = EP3-EP2
S(27) = EP -EP1
C(19) = EP3+EP2
S(23) = S(2)*CL +C(2)*S(6)
C(17) = C(2)*CL -S(2)*S(6)
S(24) = S(4)+C2L +C(4)+S(22)
C(18) = C(4)+C2L -S(4)+S(22)
S(26) = S(25)*C2D-S(14)*C2F
S(29) = S(2)*C2L+C(2)*S(26)
ZE = S(11)*CL
ZE1 = C(11)*S(5)
S(30) = ZE+ZE1
S(13) = ZE-ZE1
AMU = S(11)*CT
AMU1 = C(11)*S(11)
S(31) = AMU-AMU1
S(32) = AMU+AMU1
S(34) = S(22)*C2F-C2L*S(25)

```

C
P
C

DEFINE C,H,STANT COEFFICIENTS OF SINE AND COSINE TERMS ON FIRST
PASS ONLY

```

IF (TEST) 2,1,2
1 TEST = * 1.0
SCF(2) = - 1.2729
SCF(3) = * 0.2088
SCF(4) = - 0.2037
SCF(5) = + 0.1261
SCF(6) = + 0.0675
SCF(7) = - 0.0497
SCF(8) = - 0.0342
SCF(9) = - 0.0261
SCF(10) = + 0.0214
SCF(11) = - 0.0149
SCF(12) = + 0.0124
SCF(13) = + 0.0114
SCF(14) = + 0.0060
SCF(15) = + 0.0058
SCF(16) = - 0.0057
SCF(17) = - 0.0052
SCF(18) = + 0.0045
SCF(19) = + 0.0045
SCF(20) = - 0.0044
SCF(21) = - 0.0032
SCF(22) = + 0.0028
SCF(23) = + 0.0026
SCF(24) = - 0.0026
SCF(25) = + 0.0025
SCF(26) = - 0.0021
SCF(27) = + 0.0019
SCF(28) = + 0.0016
SCF(29) = - 0.0015
SCF(30) = - 0.0015

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EQN 171
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EQN 262
EQN 263
EQN 264


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FORTRAN OR FAP_FUNCTION_EQN. : ..... GASTZ035
3. JULIAN DATE AT 0 HOURS UNIVERSAL TIME MAY BE COMPUTED GASTZ036
BY MEANS OF FORTRAN_OR_FAP_FUNCTION_DJUL. GASTZ037
METHOD. GASTZ039
GREENWICH MEAN SIDEREAL TIME AT 0 HOURS UNIVERSAL TIME IS GASTZ040
COMPUTED ACCORDING TO THE FORMULA CONTAINED IN THE AMERICAN GASTZ041
EPHEMERIS AND NAUTICAL ALMANAC. GREENWICH APPARENT SIDEREAL GASTZ042
TIME IS OBTAINED BY ADDING TO THIS QUANTITY, THE NUTATION GASTZ043
IN RIGHT ASCENSION PLUS UT1 TIMES THE RATIO OF THE SIDEREAL GASTZ044
DAY TO THE MEAN SOLAR DAY. GASTZ045
RESTRICTIONS GASTZ046
ANY VALUE OF DJ AND UT1 MAY BE USED AS INPUT. GASTZ047
NO RESTRICTIONS OTHER THAN THOSE INHERENT IN THE GASTZ048
FORMULATIONS OF THE GREENWICH MEAN SIDEREAL TIME AND GASTZ049
THE NUTATION IN RIGHT ASCENSION. GASTZ050
ACCURACY GASTZ051
WHEN NECESSARY, INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE GASTZ052
PRECISION IN ORDER THAT THE VALUE OF THE ARGUMENT RETURNED GASTZ053
TO THE CALLING PROGRAM HAVE AN ACCURACY IN RADIANS GASTZ054
EQUIVALENT TO .001 SECONDS OF TIME. GASTZ055
AN EPHEMERIS HAS BEEN GENERATED LISTING GREENWICH APPARENT GASTZ056
SIDEREAL TIME AT 0 HOURS UNIVERSAL TIME, DAILY FROM GASTZ057
01/01/1801 TO 12/31/2000. DAILY COMPARISONS WERE MADE WITH GASTZ058
THE AMERICAN EPHEMERIS FOR THE INTERVAL 1959-1963. GASTZ059
FOR THE TIMES COMPARED, COMPARISON WITH AMERICAN EPHEMERIS GASTZ060
WAS EXACT TO AN ACCURACY OF .001 SECONDS. GASTZ061
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR... GASTZ062
(DDFP),(DFMP),(DFAD),DMOD GASTZ063
REQUIRED SUBPROGRAMS - OTHER GASTZ064
NDNE GASTZ065
STORAGE REQUIREMENTS GASTZ066
126 WITHOUT REQUIRED SUBPROGRAMS GASTZ067
TIMING GASTZ068
NO ESTIMATE AVAILABLE GASTZ069
PROGRAM MODIFICATIONS GASTZ070
***** START PROGRAM ***** GASTZ071
DT=0J-2415020.0 GASTZ072
T=DT/36525.0 GASTZ073
C=1+40.67558786E-5+EQ GASTZ074
GASTZ=1.739935893717+628.331950990910*T+C+0.26251617071*UT1 GASTZ075
GASTZ=MODF(GASTZ,6.283185307179586) GASTZ076
RETURN GASTZ077
END GASTZ078
FUNCTION GDLATZ FORTRAN SOURCE PROGRAM GASTZ079
CARDS COLUMN GDLATZ01
L1S18 GDLATZ02
LABEL GDLATZ03
FUNCTION GDLATZ(ALL,RS,RE,F1,ALTZ) GDLATZ04
VERSION OF 07/19/63 GDLATZ05
FORTRAN FUNCTION GDLATZ06
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094 GDLATZ07
PURPOSE GDLATZ08
COMPUTES - GDLATZ09
1. GEODETIC LATITUDE OF SUBSATELLITE POINT FROM GDLATZ10
GEOCENTRIC DISTANCE AND GEOCENTRIC LATITUDE GDLATZ11
(DECLINATION) OF SATELLITE. GDLATZ12
2. HEIGHT OF SATELLITE ABOVE COMPUTATIONAL SPHEROID GDLATZ13
ALONG THE NORMAL FROM SATELLITE TO SPHEROID. GDLATZ14
CALLING SEQUENCE GDLATZ15
NAME = GDLATZ(ALL,RS,RE,F1,ALTZ) GDLATZ16
INPUT GDLATZ17
ALL = GEOCENTRIC LATITUDE (DECLINATION) OF SATELLITE GDLATZ18
IN RADIANS GDLATZ19
RS = GEOCENTRIC DISTANCE IN KILOMETERS GDLATZ20
RE = EQUATORIAL RADIUS OF COMPUTATIONAL SPHEROID IN GDLATZ21
KILOMETERS GDLATZ22
F1 = INVERSE OF FLATTENING OF COMPUTATIONAL SPHEROID GDLATZ23
(DIMENSIONLESS) - E.G. IF FLATTENING = 1/298.3, GDLATZ24
THEY *F1 = 298.3 GDLATZ25
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN GDLATZ26
DOUBLE PRECISION FORM. GDLATZ27
OUTPUT GDLATZ28
NAME = GEODETIC LATITUDE OF SUBSATELLITE POINT - RADIANS GDLATZ29
ALTZ = HEIGHT OF SATELLITE ABOVE COMPUTATIONAL SPHEROID GDLATZ30
ALONG NORMAL FROM SATELLITE TO SPHEROID - KILOMETERS GDLATZ31
GDLATZ32
GDLATZ33
GDLATZ34
GDLATZ35

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      GDLAT237
      OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE GDLAT238
      FORM. GDLAT239
      GDLAT240
      REFERENCE GDLAT241
      ***THE REDUCTION FROM GEOCENTRIC TO GEODETTIC COORDINATES** GDLAT242
      BY JOHN HARRISON AND SAMUEL PLUMES GDLAT243
      THE ASTRONOMICAL JOURNAL, VOL. 86, NO. 1, FEBRUARY 1961. GDLAT244
      PAGES 15 AND 16. GDLAT245
      GDLAT246
      METHOD GDLAT247
      AN APPROXIMATION BY MEANS OF LAGRANGE'S EXPANSION FORMULA. GDLAT248
      GDLAT249
      RESTRICTIONS GDLAT250
      ***** GDLAT251
      GDLAT252
      ACCURACY GDLAT253
      INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION. GDLAT254
      GDLAT255
      THE APPROXIMATION GIVES AN ACCURACY OF 8 SIGNIFICANT GDLAT256
      FIGURES. GDLAT257
      THE 8 FIGURE ACCURACY CLAIMED BY THE AUTHORS WAS VERIFIED GDLAT258
      BY USING THE INVERSE PROBLEM (GEODETTIC TO GEOCENTRIC GDLAT259
      COORDINATES), WHICH CAN BE SOLVED RIGOROUSLY, TO SUPPLY GDLAT260
      THE INPUT FOR THIS FUNCTION. THE OUTPUT FROM THIS FUNCTION GDLAT261
      WAS THEN COMPARED WITH THE INITIAL DATA FOR YAB3QU3. GDLAT262
      INITIAL CONDITIONS. GDLAT263
      GDLAT264
      REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR GDLAT265
      (DFDP), (DFMP), (DFAD), (DFSB), DSIN, DCOS, DSQRT GDLAT266
      GDLAT267
      REQUIRED SUBPROGRAMS - OTHER GDLAT268
      NONE GDLAT269
      GDLAT270
      STORAGE REQUIREMENTS GDLAT271
      1110 WITHOUT REQUIRED SUBPROGRAMS GDLAT272
      GDLAT273
      TIMING GDLAT274
      NO ESTIMATE AVAILABLE GDLAT275
      GDLAT276
      GDLAT277
      PROGRAM MODIFICATIONS GDLAT278
      NO MODIFICATIONS TO DATE GDLAT279
      GDLAT280
      GDLAT281
      GDLAT282
      GDLAT283
      GDLAT284
      GDLAT285
      GDLAT286
      GDLAT287
      GDLAT288
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      GDLAT316
      GDLAT317
      GDLAT318
      GDLAT319
      GDLAT320
      GDLAT321
      GDLAT322
      GDLAT323
      GDLAT324
      * FUNCTION HMSRZ FORTRAN SOURCE PROGRAM *MSR2333
      * CARDS COLUMN *MSR2334
      * LIST *MSR2335
      * LABEL *MSR2336
      * FUNCTION HMSRZ(TH, IH, TS) *MSR2337
      * *MSR2338
      * *MSR2339
      * *MSR2340
      VERSION OF 07/22/63 *MSR2341
      FORTRAN FUNCTION *MSR2342
      FOR USE WITH FORTRAN 2 MONITOR ON 104 7090, 7094 *MSR2343
      *MSR2344
      PURPOSE *MSR2345
      CONVERTS HOURS, MINUTES, AND SECONDS OF TIME TO RADIAN

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..... (24 HOURS = 2 PI RADIANS).....
CALLING SEQUENCE
D NAME = HMSRZ(IH, TH, TS)
INPUT
IH = NUMBER OF HOURS IN TIME
TH = NUMBER OF MINUTES IN TIME
TS = NUMBER OF SECONDS IN TIME
SIGN OF THE INPUT TIME NEED ONLY BE ASSOCIATED WITH
THE NUMBER OF HOURS (IHL)
OUTPUT
NAME = TIME IN RADIANS
NAME IS RETURNED TO CALLING PROGRAM IN DOUBLE
PRECISION FORM.
REFERENCE
*****
METHOD
*****
RESTRICTIONS:
*****
ACCURACY
WHEN NECESSARY, INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE
PRECISION SO THAT THE VALUE OF THE OUTPUT ARGUMENT IS
AVAILABLE TO CALLING PROGRAM IN DOUBLE PRECISION,
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
(DFM2); (DFAD2)
REQUIRED SUBPROGRAMS - OTHER
NONE
STORAGE REQUIREMENTS
125 WITHOUT REQUIRED SUBPROGRAMS.
TIMING
NO ESTIMATE AVAILABLE.
PROGRAM MODIFICATIONS
NO MODIFICATIONS TO DATE
***** START PROGRAM *****
2 TH=IH
3 TH=TH
4 TH=SIGNF(TH,TH)
5 TRS=SIGNF(TS,TH)
0 6 HMSRZ=TH*.2617993877991494 + TH*4.363323129985824E-3
1 +TRS*7.272205216643040E-5
RETURN
END
SUBROUTINE JULCAL FORTRAN SOURCE PROGRAM
CARDS COLUMN
LISTB
LABEL
SUBROUTINE JULCAL(DJ, NM, ND, NY)
VERSION OF 07/22/63
FORTRAN SUBROUTINE
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
PURPOSE
COMPUTES CALENDAR DATE FROM JULIAN DATE AT 0 HOURS
UNIVERSAL TIME (OR 0 HOURS EPHEMERIS TIME).
CALLING SEQUENCE
CALL JULCAL(DJ, NM, ND, NY)
INPUT
DJ = JULIAN DATE AT 0 HOURS UNIVERSAL TIME
OUTPUT
NM = CALENDAR MONTH
ND = CALENDAR DAY
NY = CALENDAR YEAR
REFERENCE
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP
METHOD
THE NUMBER OF DAYS FROM 12 HOURS UNIVERSAL TIME JAN. 0,
1800 IS CALCULATED. THE INTEGRAL NUMBER OF YEARS IN THIS
NUMBER IS ADDED TO 1800 TO GIVE THE CURRENT CALENDAR YEAR
AND THE NUMBER OF DAYS CONTAINED IN THE INTEGRAL NUMBER
OF YEARS ELAPSED SINCE JAN. 0, 1800 IS SUBTRACTED FROM THE

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HMSRZ011
HMSRZ012
HMSRZ013
HMSRZ014
HMSRZ015
HMSRZ016
HMSRZ017
HMSRZ018
HMSRZ019
HMSRZ020
HMSRZ021
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HMSRZ096
HMSRZ097
HMSRZ098
HMSRZ099
HMSRZ100

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AND, M.L. THE MASS OF THE EARTH. . . . . PARA 324
----- PARA 325
OUTPUT OSCULATING ORBITAL ELEMENTS. . . . . PARA 326
----- PARA 327
A(1) = SEMI-MAJOR AXIS. . . . . PARA 328
A(2) = ECCENTRICITY. . . . . - DIMENSIONLESS PARA 329
A(3) = INCLINATION. . . . . - RADIANS. . . . . PARA 330
A(4) = RIGHT ASCENSION OF ASCENDING NODE. . . . . - RADIANS PARA 331
A(5) = ARGUMENT OF PERIGEE. . . . . - RADIANS PARA 333
A(6) = MEAN ANOMALY. . . . . - RADIANS. . . . . PARA 334
----- PARA 335
REFERENCE. . . . . PARA 336
***** PARA 337
METHOD. . . . . PARA 338
***** PARA 339
RESTRICTIONS. . . . . PARA 340
***** PARA 341
ACCURACY. . . . . PARA 342
***** PARA 343
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
. . . . . {DEMP} PARA 344
. . . . . PARA 345
. . . . . PARA 346
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. . . . . PARA 351
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. . . . . PARA 379
***** START PROGRAM *****
D DIMENSION A(6),A(6),RX(3),VX(3) PARA 381
D DIMENSION DUM1(100),A1(6) PARA 382
D DIMENSION XX(18),AB(6) PARA 383
D COMMON DUM1,A1(6),XX,AB PARA 384
D GO TO (1,2,3,4), INPUT PARA 385
D INPUT OPTION 1. AI = OSCULATING ORBITAL ELEMENTS, ALL ANGLES IN PARA 386
D DEGREES PARA 387
D 1 A(1)=A(1) PARA 388
D A(2)=A(2) PARA 389
D DD 101 N=3,6 PARA 390
D 101 A(N)=A1(N)+0.0174532925199433 PARA 391
D GO TO 9999 PARA 392
D INPUT OPTION 2. AI = POSITION AND VELOCITY VECTORS IN PARA 393
D KILOMETERS AND KILOMETERS/SEC^2) PARA 394
D 2 DD 201 N=1,3 PARA 395
D RX(N)=A1(N) PARA 396
D 201 VX(N)=A1(N+3) PARA 397
D CALL RVELZ(RX,VX,A,PER,EN,GM) PARA 398
D GO TO 9999 PARA 399
D INPUT OPTION 2. AI = POSITION AND VELOCITY VECTORS IN PARA 400
D VANGUARD UNITS PARA 401
D 3 DD 301 N=1,3 PARA 402
D RX(N)=A1(N)+6378.388 PARA 403
D 301 VX(N)=A1(N+3)+7.905472668 PARA 404
D CALL RVELZ(RX,VX,A,PER,EN,GM) PARA 405
D GO TO 9999 PARA 406
D INPUT OPTION 4. AI = BROWER MEAN ELEMENTS, ALL ANGLES IN DEGREES PARA 407
D 4 A1(0(1))=A(1) PARA 408
D A1(0(2))=A(2) PARA 409
D DD 401 N=3,6 PARA 410
D BA=A1(N)+0.0174532925199433 PARA 411
D 401 A1(0(N))=BA PARA 412

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CALL BRHR1	PARA 123
D DT=0.0	PARA 124
D CALL BRHR2(0Y,0.0)	
DD 402 N=1,6	PARA 126
402 SIN=ABIN)	PARA 127
9999 RETURN	PARA 128
END	PARA 129
* SUBROUTINE RDMSZ...EDTRAN_SOURCE_PROGRAM	RDMS2000
* CARDS COLUMN	RDMS2001
* LISTS	RDMS2002
* LABEL	
SUBROUTINE RDMSZ(AR,IR,JD,IM,AS)	RDMS2003
C	RDMS2004
C VERSION OF 03/02/64	RDMS2005
C FORTRAN SUBROUTINE	RDMS2006
C FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094	RDMS2007
C	RDMS2008
C PURPOSE	RDMS2009
CONVERTS AN ANGLE OR ARC IN RADIANS INTO THE INTEGRAL	RDMS2010
NUMBER OF REVOLUTIONS, NUMBER OF DEGREES, NUMBER OF	RDMS2011
MINUTES, AND NUMBER OF SECONDS AND DECIMALS OF A SECOND	RDMS2012
CONTAINED IN THE ANGLE OR ARC.	RDMS2013
CALLING SEQUENCE	RDMS2014
D CALL RDMSZ(AR,IR,JD,IM,AS)	RDMS2015
INPUT	RDMS2016
AR = ANGLE OR ARC IN RADIANS	RDMS2017
AR MUST BE AVAILABLE IN CALLING PROGRAM IN DOUBLE PRECISION	RDMS2018
FORM.	RDMS2019
OUTPUT	RDMS2020
IR = INTEGRAL NUMBER OF REVOLUTIONS IN THE ANGLE OR ARC	RDMS2021
JD = NUMBER OF DEGREES	RDMS2022
IM = NUMBER OF MINUTES	RDMS2023
AS = NUMBER OF SECONDS AND DECIMALS OF A SECOND	RDMS2024
REFERENCE	RDMS2025
*****	RDMS2026
METHOD	RDMS2027
*****	RDMS2028
RESTRICTIONS	RDMS2029
*****	RDMS2030
ACCURACY	RDMS2031
CONVERSION IS ACCURATE TO AT LEAST .001 SECONDS OF ARC.	RDMS2032
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR	RDMS2033
(DFDP),DMDD,(DFMP),(DFSB)	RDMS2034
REQUIRED SUBPROGRAMS - OTHER	RDMS2035
NONE	RDMS2036
STORAGE REQUIREMENTS	RDMS2037
337 WITHOUT REQUIRED SUBPROGRAMS	RDMS2038
TIMING	RDMS2039
NO ESTIMATE AVAILABLE	RDMS2040
ANALYSIS	RDMS2041
PROGRAM MODIFICATIONS	RDMS2042
03/02/64 MOD. 1 BY S. STATEV - CHANGED UPPER LIMIT OF	RDMS2043
AS FROM 99.0005 TO 59.9995	RDMS2044
***** START PROGRAM *****	RDMS2045
D 5 IR=AR/6.283185307179586	RDMS2046
D 6 AR=MODF(AR,6.283185307179586)	RDMS2047
D 7 ID=AR*57.2957795130823	RDMS2048
D 8 AI=ID	RDMS2049
D 9 A=A1/57.2957795130823	RDMS2050
D 10 B=AR-A	RDMS2051
D 11 IM=B/3437.746770784938	RDMS2052
D 12 A2=IM	RDMS2053
D 13 IM=XBSF(IM)	RDMS2054
D 14 C=A2/3437.746770784938	RDMS2055
D 15 D=B-C	RDMS2056
D 16 AS=BSF(D+206264.806247096)	RDMS2057
D 17 IF (AS=99.9995) 20,18,18	RDMS2058
D 18 AS=ABSF(AS-63.)	RDMS2059
D 19 IM=IM+1	RDMS2060
D 20 IF (IM=63) 23,21,21	RDMS2061
D 21 IM=IM-60	RDMS2062
D 22 ID=ID+XSIGNF(1,ID)	RDMS2063
D 23 IF (XBSF(ID)=360) 26,24,24	RDMS2064
D 24 ID=ID-XSIGNF(360,ID)	RDMS2065
D 25 IR=IR+XSIGNF(1,IR)	RDMS2066
D 26 RETURN	RDMS2067

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END
SUBROUTINE RHMSZ FORTRAN SOURCE PROGRAM
CARDS COLUMN
LISTB
LABEL
SUBROUTINE RHMSZ(TR,IO,IM,TS)

VERSION OF 03/02/64
FORTRAN SUBROUTINE
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094

PURPOSE
CONVERTS TIME IN RADIANs (24_HOURS = 2 PI RADIANs) INTO
THE INTEGRAL NUMBER OF DAYS, NUMBER OF HOURS, NUMBER OF
MINUTES, AND NUMBER OF SECONDS AND DECIMALS OF A SECOND
CONTAINED IN THE TIME.

CALLING SEQUENCE
D CALL RHMSZ(TR,IO,IM,TS)

INPUT
TR = TIME IN RADIANs
TIME MUST BE AVAILABLE IN CALLING PROGRAM IN
DOUBLE PRECISION FORM.

OUTPUT
IO = INTEGRAL NUMBER OF DAYS CONTAINED IN THE TIME
IM = NUMBER OF HOURS
IN = NUMBER OF MINUTES
TS = NUMBER OF SECONDS AND DECIMALS OF A SECOND

REFERENCE
*****

METHOD
*****

RESTRICTIONS
*****

ACCURACY
CONVERSION IS ACCURATE TO AT LEAST .001 SECONDS OF TIME.

REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
(DFDP),DMDD,(DFHP),(DFSB)

REQUIRED SUBPROGRAMS - OTHER
NONE

STORAGE REQUIREMENTS
316 WITHOUT REQUIRED SUBPROGRAMS

TIMING
NO ESTIMATE AVAILABLE

ANALYSIS

PROGRAM MODIFICATIONS
03/02/64 MOD. 1 BY S. STATEN - CHANGED UPPER LIMIT OF
TS FROM 59.0005 TO 59.9995

***** START PROGRAM *****
D 5 ID=TR/6.283185307179586
D 6 TR=MODF(TR,6.283185307179586)
D 7 IM=TR-5.9171863420548
D 8 I1=IM
D 9 A=I1/3.81971863420548
D 10 B=TK-A
D 11 IM=B+229.183118052329
D 12 T2=IM
D 13 IM=XABSF(IM)
D 14 C=T2/229.183118052329
D 15 D=B-C
D 16 TS=ABSF(D+13750.98700831397)
D 17 IF (TS-59.9995) 20,18,18
D 18 TS=ABSF(TS-62.)
D 19 IM=IM+1
D 20 IF (IM-62) 23,21,21
D 21 IM=IM-60
D 22 IM=(IXSIGNF(1,IM)
D 23 IF (XABSF(IM)-24) 26,24,24
D 24 IM=(IXSIGNF(24,IM)
D 25 IO=ID+XSIGNF(1,IO)
D 26 RETURN
END
SUBROUTINE RVELZ FORTRAN SOURCE PROGRAM
CARDS COLUMN
LISTB
LABEL
SUBROUTINE RVELZ(X,VX,A,P,EY,GH)

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R0HSZ090
R4HSZ090
R4HSZ091
R4HSZ092
R4HSZ093
R4HSZ094
R4HSZ095
R4HSZ096
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R4HSZ203
R4HSZ204

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VERSION OF 07/22/63
FORTRAN SUBROUTINE
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094
RVELZ005
RVELZ006
RVELZ007
RVELZ008
RVELZ009

PURPOSE
CONVERTS GEOCENTRIC EQUATORIAL INERTIAL RECTANGULAR
COORDINATES OF POSITION AND COMPONENTS OF VELOCITY INTO
OSCILLATING ORBITAL ELEMENTS
RVELZ010
RVELZ011
RVELZ012
RVELZ013

CALLING SEQUENCE
D DIMENSION X(3),VX(3),A(6)
D CALL RVELZ(X,VX,A,P,EH,GH)
RVELZ014
RVELZ015
RVELZ016
RVELZ017
RVELZ018

INPUT
X(1)
X(2) THE 3 RECTANGULAR COORDINATES OF POSITION
X(3)
RVELZ019
RVELZ020
RVELZ021
RVELZ022
RVELZ023
RVELZ024
RVELZ025
RVELZ026
RVELZ027
RVELZ028
RVELZ029
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RVELZ113
RVELZ114

UNITS OF INPUT ARGUMENTS X, VX, AND GH ARE ARBITRARY BUT
MUST BE MUTUALLY CONSISTENT
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN
DOUBLE PRECISION FORM.

OUTPUT
A(1) = SEMI-MAJOR AXIS - DIMENSIONLESS
A(2) = ECCENTRICITY - DIMENSIONLESS
A(3) = INCLINATION - RADIANS
A(4) = RIGHT ASCENSION OF ASCENDING NODE - RADIANS
A(5) = ARGUMENT OF PERIGEE - RADIANS
A(6) = MEAN ANOMALY - RADIANS
P = ANOMALISTIC PERIOD
EV = MEAN ANGULAR MOTION
UNITS OF OUTPUT ARGUMENTS A(1), P, AND EV WILL DEPEND UPON
THE UNITS EMPLOYED FOR X, VX, AND GH.
ALL ANGLES ARE IN RADIANS.
OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE
FORM.

REFERENCE
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP

METHOD
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP

RESTRICTIONS
ECCENTRICITY MUST BE LESS THAN 1.0.

ACCURACY
REFER TO ACCURACY TESTS IN SUBPROGRAM WRITEUP.
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.

REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR
DEXPT2, (DFAD), DSQRT, (DFMP), (DFSB), (DFDP)

REQUIRED SUBPROGRAMS - OTHER
07/22/63 ALLOTZ
07/22/63 ATANZ

STORAGE REQUIREMENTS
1015 WITHOUT REQUIRED SUBPROGRAMS

TIMING
NO ESTIMATE AVAILABLE

PROGRAM MODIFICATIONS
NO MODIFICATIONS TO DATE

***** START PROGRAM *****
D DIMENSION X(3),VX(3),A(6),Y(3),VY(3)
500 DO 502 N=1,3
D 501 Y(N)=X(N)
D 502 VY(N)=VX(N)
D 3 R=SQRTF(R2)
D 4 VZ=VY(1)**2+VY(2)**2+VY(3)**2
D 5 V1=SQRTF(VZ)
D 6 RDOT=Y(1)*VY(1)+Y(2)*VY(2)+Y(3)*VY(3)
D 7 H1=Y(2)*VY(3)-Y(3)*VY(2)
D 8 H2=Y(3)*VY(1)-Y(1)*VY(3)
D 9 H3=Y(1)*VY(2)-Y(2)*VY(1)

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D 10	C2=H1**2+H2**2 .	RVELZ105
D 11	C1=SQRTF(C2)	RVELZ106
D 12	H=SQRTF(H3**2+C2)	RVELZ107
D 13	RC1=R#C1	RVELZ108
D 14	RTGM=SQRTF(GH)	RVELZ109
D 15	A(1)=GM#R/(GM+GM-R#V2)	RVELZ110
D 16	RTA=SQRTF(A(1))	RVELZ111
D 17	F1=RODOTZ(RTGM#RTA)	RVELZ112
D 18	AR=A(1)/R	RVELZ113
D 19	F2=1.0-R/A(1)	RVELZ114
D 20	F2=F1**2+F2**2	RVELZ115
D 21	A(2)=SQRTF(F2)	RVELZ116
D 22	S1=C1/H	RVELZ117
D 23	C1=H3/H	RVELZ118
D 24	SN=H1/C1	RVELZ119
D 25	CN=H2/C1	RVELZ120
D 26	SU=H#Y(3)/RC1	RVELZ121
D 27	CU= (Y(2)*H1-Y(1)*H2)/RC1	RVELZ122
D 28	SE=F1/A(2)	RVELZ123
D 29	CE=F2/A(2)	RVELZ124
D	SF=AR#SE#SQRTF(1.0-E2)	RVELZ125
D	CF=AR*(CE-A(2))	RVELZ126
D 30	A(3)=ATANZ(S1,CF)	RVELZ127
D 31	A(4)=ATANZ(SN,CN)	RVELZ128
D 32	U=ATANZ(SU,CU)	RVELZ129
D	F=ATANZ(SF,CF)	RVELZ130
D 33	E=ATANZ(SE,CE)	RVELZ131
D	AS=U-F	RVELZ132
D	A(5)=ALLOTZ(A5)	RVELZ133
D 34	A6=E-A(2)*SE	RVELZ134
D 35	A(6)=ALLOTZ(A6)	RVELZ135
D 36	EN=RTGM/(RTA#A(1))	RVELZ136
D 37	P=6.283185307179586/EN	RVELZ137
	RETURN	RVELZ138
	END	RVELZ139
*	SUBROUTINE R13Z 'FORTRAN SOURCE PROGRAM	R13Z 000
*	CARDS COLUMN	R13Z 001
*	.LISTB	R13Z 002
*	LABEL	
*	SUBROUTINE R13Z(Y,B,A,X)	R13Z 003
		R13Z 004
	VERSION OF 07/10/63	R13Z 005
	FORTRAN SUBROUTINE	R13Z 006
	FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094	R13Z 007
		R13Z 008
	PURPOSE	R13Z 009
	SOLVES THE MATRIX EQUATION -	R13Z 010
	Y = R1(B) R3(A) X	R13Z 011
	WHERE -	R13Z 012
		R13Z 013
		R13Z 014
		R13Z 015
		R13Z 016
		R13Z 017
		R13Z 018
		R13Z 019
		R13Z 020
		R13Z 021
		R13Z 022
		R13Z 023
	CALLING SEQUENCE	R13Z 024
	D DIMENSION Y(3),X(3)	R13Z 025
	D CALL R13Z(Y,B,A,X)	R13Z 026
		R13Z 027
	INPUT	R13Z 028
	VECTOR X IN ANY UNITS	R13Z 029
	ROTATION ANGLES A AND B IN RADIANS	R13Z 030
		R13Z 031
	INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN	R13Z 032
	DOUBLE PRECISION FORM.	R13Z 033
		R13Z 034
		R13Z 035
	OUTPUT	R13Z 036
	VECTOR Y IN SAME UNITS AS VECTOR X	R13Z 037
	OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE	R13Z 038
	FORM.	R13Z 039
		R13Z 040
	REFERENCE	R13Z 041
	REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP	R13Z 042
		R13Z 043
	METHOD	R13Z 044
	REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP	R13Z 045
		R13Z 046
	RESTRICTIONS	R13Z 047
	*****	R13Z 048
		R13Z 049
	ACCURACY	R13Z 050
	INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.	R13Z 051
		R13Z 052
	REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR	R13Z 053
	DSIN,DCOS,(DFMP),(DFSB),(DFAD).	R13Z 054
		R13Z 055
	REQUIRED SUBPROGRAMS - OTHER	R13Z 056
	NONE	R13Z 057

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C
C----- STORAGE REQUIREMENTS ----- R13Z 058
C----- 248 WITHOUT REQUIRED SUBPROGRAMS ----- R13Z 059
C----- TIMING ----- R13Z 060
C----- NO ESTIMATE AVAILABLE. ----- R13Z 061
C----- ANALYSIS ----- R13Z 062
C----- PROGRAM MODIFICATIONS ----- R13Z 063
C----- NO MODIFICATIONS TO DATE ----- R13Z 064
C----- START PROGRAM ----- R13Z 065
C----- R13Z 066
C----- R13Z 067
C----- R13Z 068
C----- R13Z 069
C----- R13Z 070
C----- R13Z 071
C----- R13Z 072
C----- R13Z 073
C----- R13Z 074
C----- R13Z 075
C----- R13Z 076
C----- R13Z 077
C----- R13Z 078
C----- R13Z 079
C----- R13Z 080
C----- R13Z 081
C----- R13Z 082
C----- R13Z 083
C----- R13Z 084
C----- R13Z 085
C----- R13Z 086
C----- R13Z 087
C----- R13Z 088
C----- R13Z 089
C----- TIMEC
C----- CARDS COLUMN
C----- LISTB
C----- LABEL
C----- SUBROUTINE TIMEC(DJO,TSEP,S,E,DT)
C----- USES TAPE A3
C-----
C----- VERSION OF 7/22/63
C-----
C----- READS A CARD FROM CARD READER CONTAINING CALENDAR DATE AND UT2 OF
C----- DESIRED START AND END TIMES FOR CALCULATION OF AN EPHEMERIS, AND
C----- THE TIME INCREMENT OF THE EPHEMERIS IN SECONDS. CALCULATES TIME
C----- INTERVAL IN SECONDS FROM SOME EPOCH (DJO,TSEP) TO THE START AND
C----- END TIMES.
C----- WRITES CALENDAR DATE AND UT2 ON TAPE UNIT A3.
C-----
C----- INPUT FROM CALLING SEQUENCE
C----- DJO = EPOCH JULIAN DATE AT 0 HOURS UT2.
C----- TSEP = EPOCH UT2 IN SECONDS
C-----
C----- INPUT FROM CARD READER
C----- NMS,NDS,NYS = MONTH, DAY, YEAR OF START DATE
C----- NMF,NDF,NYF = MONTH, DAY, AND YEAR OF END DATE
C-----
C----- NMS,NMNS,TSS = HOUR, MINUTE, SECOND (UT2) OF START TIME
C----- NMF,NMNF,TSF = HOUR, MINUTE, SECOND (UT2) OF END DATE
C----- DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
C-----
C----- OUTPUT
C----- S = TIME IN SECONDS FROM EPOCH TO START TIME
C----- F = TIME IN SECONDS FROM EPOCH TO END TIME
C----- DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
C-----
C----- REQUIRED SUBPROGRAMS
C-----
C----- DJUL, JULCAL 37/22/60 - FAP DOUBLE ENTRY PROGRAM
C-----
5015 FORNAT (2(1X)I2) ,1X,14,2I3,F7.3,I3,1X,12,1X,14,2I3,F7.3,F11.3 )
6016 FORNAT (1X)I2,1H)I2,1H)I4,7X)I1H START DATE(1X)I2,I3,F7.3,2X,
1 15H START TIME-UT2(1X)F12.3,5X)23H TIME INCREMENT-SECONDS(1X)I2,
2 1H)I2,1H)I4,7X)9H END DATE(1X)I2,I3,F7.3,5X)13H END TIME-UT2
READ 6015,NMS,NDS,NYS,NMS,NMNS,TSS,NMF,NDF,NYF,NMF,
1 NMF,NDF,DT
WRITE OUTPUT TAPE 3,6016,NMS,NDS,NYS,NMS,NMNS,TSS,DT,NMF,NDF,NYF,
1 NMF,NMNF,TSF
IF (SENSE SWITCH 6) 1,2
PRHT 6016,NMS,NDS,NYS,NMS,NMNS,TSS,DT,NMF,NDF,NYF,NMF,NMNF,TSF
2 DJSO=DJUL(NMS,NDS,NYS)
DJFO=DJUL(NMF,NDF,NYF)
TSS=NMS*3600
TMNS=NMS*60
TS=TMNS+TSS-TSEP
TMF=NMF*3600
TMNF=NMF*60
TF=TMF+TMNF+TSF-TSEP
DJS=DJSO-DJO
DJF=DJFO-DJO
S=DJS+86400.+TS
F=DJF+86400.+TF
RETURN
END
SUBROUTINE VFUZ FORTRAN SOURCE PROGRAM VFUZ 000
CARDS COLUMN VFUZ 001
LISTB VFUZ 002
LABEL VFUZ 003
SUBROUTINE VFUZ(SC,RE,F,U) VFUZ 004
VFUZ 005
C

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VERSION OF 07/22/63.....VFUZ 005
FORTRAN SUBROUTINE.....VFUZ 006
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094VFUZ 007
VFUZ 008
PURPOSE.....VFUZ 009
CONVERTS GEODETIC LATITUDE, LONGITUDE, AND HEIGHT OF A
STATION ABOVE A COMPUTATIONAL SPHEROID (ALONG A NORMAL TO
THE SPHEROID) INTO GEOCENTRIC RECTANGULAR COORDINATES OF
POSITION. THE ORIGIN OF THE RECTANGULAR COORDINATE SYSTEM
(THE U SYSTEM) IS LOCATED AT THE GEOMETRICAL CENTER OF THE
COMPUTATIONAL SPHEROID. THE U1 AXIS IS DIRECTED INWARDS
THE INTERSECTION OF THE GREENWICH MERIDIAN AND THE
EQUATORIAL PLANE. THE U3 AXIS IS PERPENDICULAR TO THE
EQUATORIAL PLANE AND IS DIRECTED NORTH. THE U2 AXIS IS
LOCATED IN THE EQUATORIAL PLANE 90 DEGREES EAST OF THE U1
AXIS.
VFUZ 010
VFUZ 011
VFUZ 012
VFUZ 013
VFUZ 014
VFUZ 015
VFUZ 016
VFUZ 017
VFUZ 018
VFUZ 019
VFUZ 020
VFUZ 021
VFUZ 022
CALLING SEQUENCE.....VFUZ 023
0 DIMENSION SC(3),U(3)VFUZ 024
0 CALL VEUZ(SC,RE,F,UI)VFUZ 025
VFUZ 026
INPUT.....VFUZ 027
SC(1)= GEODETIC LATITUDE - RADIANSVFUZ 028
SC(2)= GEODETIC LONGITUDE - RADIANSVFUZ 029
SC(3)= HEIGHT ABOVE COMPUTATIONAL SPHEROID ALONG A NORMAL
TO THE SPHEROID.VFUZ 030
VFUZ 031
RE = EQUATORIAL RADIUS OF COMPUTATIONAL SPHEROIDVFUZ 032
F = [INVERSE OF FLATTENING OF COMPUTATIONAL SPHEROID]VFUZ 033
(DIMENSIONLESS) - E.G. IF FLATTENING = 1/298.3,
THEN F = 298.3VFUZ 034
VFUZ 035
VFUZ 036
UNITS OF INPUT ARGUMENTS SC(3) AND RE ARE ARBITRARY BUT
MUST BE MUTUALLY CONSISTENT.VFUZ 037
INPUT ARGUMENTS MUST BE AVAILABLE IN CALLING PROGRAM IN
DOUBLE PRECISION FORM.VFUZ 038
VFUZ 039
VFUZ 040
VFUZ 041
OUTPUT.....VFUZ 042
U(1)VFUZ 043
U(2) THE 3 RECTANGULAR COORDINATES OF POSITIONVFUZ 044
U(3)VFUZ 045
VFUZ 046
UNITS OF OUTPUT ARGUMENTS, U WILL DEPEND UPON THE UNITS
EMPLOYED FOR SC(3) AND RE.VFUZ 047
VFUZ 048
OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE
FORM.VFUZ 049
VFUZ 050
VFUZ 051
VFUZ 052
REFERENCE.....VFUZ 053
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUPVFUZ 054
VFUZ 055
METHOD.....VFUZ 056
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUPVFUZ 057
VFUZ 058
RESTRICTIONS.....VFUZ 059
*****VFUZ 060
VFUZ 061
ACCURACY.....VFUZ 062
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION.VFUZ 063
VFUZ 064
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITORVFUZ 065
DSIN,DCOS,(DFOP),(DFS8),DEXP(2,DSQRT,(DFMB),(DFAD)VFUZ 066
VFUZ 067
REQUIRED SUBPROGRAMS - OTHERVFUZ 068
NONEVFUZ 069
VFUZ 070
STORAGE REQUIREMENTS.....VFUZ 071
305 WITHOUT REQUIRED SUBPROGRAMSVFUZ 072
VFUZ 073
TIMING.....VFUZ 074
NO ESTIMATE AVAILABLEVFUZ 075
VFUZ 076
VFUZ 077
VFUZ 078
VFUZ 079
PROGRAM MODIFICATIONS.....VFUZ 080
NO MODIFICATIONS TO DATEVFUZ 081
VFUZ 082
***** START PROGRAM *****VFUZ 083
VFUZ 084
VFUZ 085
2 DIMENSION SC(3),U(3)VFUZ 086
VFUZ 087
VFUZ 088
3 SAL=SINF(SC(1))VFUZ 089
4 CAL=COSF(SC(1))VFUZ 090
5 C1=(1.0-1./F)**2VFUZ 091
6 EN=RE*SQRTF(CAL**2+C1*SAL**2)VFUZ 092
7 C2=(EN*SC(3))+CALVFUZ 093
8 U(1)=C2*COSF(SC(2))VFUZ 094
9 U(2)=C2*SINF(SC(2))VFUZ 095
10 U(3)=(EN*C1+SC(3))*SALVFUZ 096
VFUZ 097
RETURNVFUZ 098
ENDVFUZ 099
VFUZ 100
* SUBROUTINE VADZ FORTRAN SOURCE PROGRAMVFUZ 101
*VFUZ 102
* CARDS COLUMNVFUZ 103
* LIST8VFUZ 104
* LABELVFUZ 105

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SUBROUTINE VRDZ(N,Z,E,A,R) VRDZ 003
C----- VRDZ 006
VERSION OF 07/16/63 VRDZ 005
FORTRAN SUBROUTINE VRDZ 004
FOR USE WITH FORTRAN 2 MONITOR ON IBM 7090, 7094 VRDZ 007
C----- VRDZ 008
PURPOSE VRDZ 009
C----- VRDZ 010
CONVERTS RECTANGULAR POSITION COORDINATES OF A POINT TO THE
SPHERICAL COORDINATES OF THE POINT. VRDZ 011
C----- VRDZ 012
C----- VRDZ 013
CALLING SEQUENCE VRDZ 014
D DIMENSION Z(3) VRDZ 015
D CALL VRDZ(1,Z,E,A,R) VRDZ 016
D CALL VRDZ(2,Z,E,A,R) VRDZ 017
C----- VRDZ 018
INPUT VRDZ 019
Z(1) VRDZ 020
Z(2) THE 3 RECTANGULAR COORDINATES OF POSITION VRDZ 021
Z(3) VRDZ 022
N = OPTION NUMBER TO DETERMINE TYPE OF SPHERICAL
COORDINATE DESIRED. VRDZ 024
VRDZ 025
OUTPUT VRDZ 027
R = MAGNITUDE OF POSITION VECTOR VRDZ 028
E = ANGULAR DISTANCE IN RADIANS OF VECTOR FROM Z1-Z2 VRDZ 029
PLANE (E.G. ELEVATION, DECLINATION, LATITUDE) VRDZ 030
E IS RESTRICTED TO LIE BETWEEN 0 AND + PI/2 RADIANS VRDZ 031
OR BETWEEN 0 AND - PI/2 RADIANS VRDZ 032
VRDZ 033
N=1 A = ANGULAR DISTANCE IN RADIANS OF PROJECTION OF VECTOR VRDZ 034
ONTO THE Z1-Z2 PLANE, MEASURED POSITIVELY COUNTER- VRDZ 035
CLOCKWISE FROM THE Z1 AXIS (E.G. RIGHT ASCENSION, VRDZ 036
LONGITUDE MEASURED POSITIVE EAST FROM GREENWICH) VRDZ 037
VRDZ 038
N=2 A = ANGULAR DISTANCE IN RADIANS OF PROJECTION OF VECTOR VRDZ 039
ONTO THE Z1-Z2 PLANE, MEASURED POSITIVELY CLOCKWISE VRDZ 040
FROM THE Z2 AXIS (E.G. AZIMUTH MEASURED POSITIVE VRDZ 041
CLOCKWISE FROM NORTH) VRDZ 042
VRDZ 043
A IS RESTRICTED TO LIE BETWEEN 0 AND + 2 PI RADIANS VRDZ 044
VRDZ 045
OUTPUT ARGUMENTS ARE RETURNED TO CALLING PROGRAM IN DOUBLE
FORM. VRDZ 047
VRDZ 048
VRDZ 049
REFERENCE VRDZ 050
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP VRDZ 051
VRDZ 052
METHOD VRDZ 053
REFER TO MATHEMATICAL DESCRIPTION IN SUBPROGRAM WRITEUP VRDZ 054
VRDZ 055
RESTRICTIONS VRDZ 056
***** VRDZ 057
VRDZ 058
ACCURACY VRDZ 059
INTERNAL ARITHMETIC IS PERFORMED IN DOUBLE PRECISION. VRDZ 060
VRDZ 061
REQUIRED SUBPROGRAMS - FORTRAN 2 MONITOR VRDZ 062
DSQRT,DEXP(2),(DFA0),(DFDP),(DFMP),DATAN VRDZ 063
VRDZ 064
REQUIRED SUBPROGRAMS - OTHER VRDZ 065
07/22/63 ATANZ VRDZ 066
VRDZ 067
STORAGE REQUIREMENTS VRDZ 068
298 WITHOUT REQUIRED SUBPROGRAMS VRDZ 069
VRDZ 070
TIMING VRDZ 071
NO ESTIMATE AVAILABLE VRDZ 072
VRDZ 073
VRDZ 074
VRDZ 075
PROGRAM MODIFICATIONS VRDZ 081
NO MODIFICATIONS TO DATE VRDZ 082
VRDZ 083
***** START PROGRAM ***** VRDZ 085
C----- VRDZ 086
2 DIMENSION Z(3) VRDZ 087
C----- VRDZ 088
3 R=SQRTF(Z(1)**2+Z(2)**2+Z(3)**2) VRDZ 089
4 SE=Z(3)/R VRDZ 090
5 CE=SQRTF(1.0-SE**2) VRDZ 091
6 C=R*CE VRDZ 092
GO TO (7,9), N VRDZ 093
7 CA=Z(1)/C VRDZ 094
8 SA=Z(2)/C VRDZ 095
GO TO 11 VRDZ 096
9 SA=Z(1)/C VRDZ 097
10 CA=Z(2)/C VRDZ 098
11 E=ATAN2F(SE,CF) VRDZ 099
12 A=ATANZ(SA,CA) VRDZ 100
RETURN VRDZ 101
END VRDZ 102

```

```

*      FUNCTION XKEP                                     XKEP
*      CARDS COLUMN
*      LISTB
*      LABEL
*      FUNCTION XKEP(AM,ECC,SE,CE,ERR)
*      E1 = AM + (ECC * SINP(AM) )
*      N = 0
*      1 E2 = E1
*      N = N + 1
*      SE = SINP(E1)
*      CE = COSP(E1)
*      E1 = E1 + ((AM - E1 + ECC*SE) / (1.0 - ECC*CE))
*      G = ABSF(E1 - E2) / E1
*      IF( N = 2) 2,2,3
*      2 IF(G - ERR ) 5,5,1
*      3 PRINT 4
*      PRINT 6,AM,E1,E2,G,N
*      4 FORMAT (36H0ND CONVERGENCE IN KEPLERS EQUATION
*      6 FORMAT (4E16,8,I5)
*      SENSE LIGHT 2
*      5 XKEP = E1
*      RETURN
*      END
*      FUNCTION XKCP2                                     XKEPZ
*      CARDS COLUMN
*      LISTB
*      LABEL
*      FUNCTION XKCP2(AM,ECC,SE,CE,ERR)
*      D .. E1 = AM + (ECC * SINP(AM) )
*      N = 0
*      D 1 E2 = E1
*      N = N + 1
*      D SE = SINP(E1)
*      D CE = COSP(E1)
*      D .. E1 = E1 + ((AM - E1 + ECC*SE) / (1.0 - ECC*CE))
*      D G = ABSF(E1 - E2) / E1
*      D IF( N = 2) 2,2,3
*      D 2 IF(G - ERR ) 5,5,1
*      3 PRINT 4
*      PRINT 6,AM,E1,E2,G,N
*      4 FORMAT (36H0ND CONVERGENCE IN KEPLERS EQUATION
*      6 FORMAT (4E16,8,I5)
*      SENSE LIGHT 2
*      D 5 XKCP2 = E1
*      RETURN
*      END
*      SUBROUTINE BACK
*      CARDS COLUMN
*      LISTB
*      FAP
*      COUNT 82
*      LBL BACK,X
*      REM SUBROUTINE BACK
*      REM PROGRAM IN CORE A. MOVES AN ARRAY FROM CORE B TO
*      REM DESIGNATED LOCATIONS CORE A.
*      ENTRY BACK
*      BACK EFT TEST FOR A OR B CORE
*      TRA ERROR ERROR - B CORE
*      SXA STOR1,1 STORE MACHINE CONDITIONS
*      SXO STOR1,2 X
*      STI STOIND X
*      AXT 0,2 ZERO I.R. 2
*      CAL* 3,4 FORTRAN ADDRESS BLOCK FROM CORE B
*      ARS 18 SHIFT TO ADDRESS PORTION OF WORD
*      STA ARRAY STORED FOR REFERENCE
*      SUB ADDR1 SETTING UP TRANSFER OF THREE WORDS
*      STA ARRAY+1 AT A TIME
*      SUB ADDR1 X
*      STA ARRAY+2 X
*      CAL* 2,4 ARRAY LENGTH
*      PDX 0,1 PLACED IN I.R. 1
*      TXL SHLARY,1,2 SMALL ARRAY, LENGTH EQUAL TO 1 OR 2
*      CAL 1,4 FORTRAN ADDRESS BLOCK IN CORE A
*      STA STORE STORED FOR REFERENCE
*      SUB ADDR1 WILL BE STORING THREE WORDS AT A TIME
*      STA STORE+1 X
*      SUB ADDR1 X
*      STA STORE+2 X
*      RESET SEB X
*      ARRAY CLA **2 TRANSFER OF WORDS
*      LDO **2 X
*      LDI **2 X
*      SEA X
*      STORE STO **2 STORED
*      STO **2 X
*      STI **2 X
*      TXI **1,2,3 MOVE DOWN THROUGH BLOCK
*      TIX RESET,1,3 REDUCE BLOCK BY 3
*      TXH ARRAY3,1,2 IF 3 WORDS, SET I.R. 1 = 0
*      TXH THWDS,1,1 TEST FOR REMAINING (1 OR 2) WORDS
*      TXL RETURN,1,0 X
*      ONEWD CAL* 3,4 TRANSFERRING TOTAL OF 1 WORD, OR
*      ARS 18 REMAINING WORD FROM A TO B CORE
*      STA ARRAY1 REMAINING WORD FROM A TO B CORE

```


	CAL	1,4	X
	STA	STORE1	X
	SEB		X
ARRAY1	CLA	**,2	X
	SEA		X
STORE1	STO	**,2	X
RETURN	LXA	STOIR,1	RETURN TO FORTRAN
	LXD	STOIR,2	X
	LDI	STOIND	X
	TRA	4,4	X
SMLARY	TXL	ONEWD,1,2	TEST FOR 1 OR 2 WORDS IN ARRAY
TWOADS	CAL*	3,4	TRANSFERRING TOTAL OF 2 WORDS, OR
	ARS	18	REMAINING 2 WORDS FROM A TO B CORE
	STA	ARRAY2	X
	SUB	ADDR1	X
	STA	ARRAY2+1	X
	CLA	1,4	X
	STA	STORE2	X
	SUB	ADDR1	X
	STA	SJOB2+1	X
	SEB		X
ARRAY2	CLA	**,2	X
	LQ	**,2	X
	SEA		X
STORE2	STO	**,2	X
	STQ	**,2	X
	TRA	RETURN	X
ARRAY3	AXT	0,1	3 WORDS, ZERO I.R. 1
	TRA	RESET	X
ERROR	WTOA	3	
	RCHA	READ	
	TCOA	*	
	TRA	4,4	
READ	IDCD	WORDS,1,9	
WORDS	BCI	9,1**	SUBROUTINE BACK CANNOT BE EXECUTED FROM B CORE **
	ADDR1	OCT	1
STOIND	BSS	1	
STOIR	BSS	1	
	END		
*	SUBROUTINE	STASH	
*	CARDS	COLUMN	
*	LIST		
*	FAP		
	COUNT	80	
	LBL	STASH,X	
	REM	SUBROUTINE	STASH
	REM	PROGRAM	IN CORE A, MOVES AN ARRAY FROM CORE A TO
	REM	DESIGNATED	LOCATIONS CORE B.
	ENTRY	STASH	
STASH	FT	STASH	
	TRA	ERROR	TEST FOR A OR B CORE
	SXA	STOIR,1	ERROR - B CORE
	SXD	STOIR,2	STORE MACHINE CONDITIONS
	STI	STOIND	X
	AXT	0,2	ZERO I.R. 2
	CAL	1,4	FORTTRAN ADDRESS BLOCK FROM
	STA	ARRAY	STORED FOR REFERENCE
	SUB	ADDR1	SETTING UP TRANSFER OF THREE WORDS
	STA	ARRAY+1	AT A TIME
	SUB	ADDR1	X
	STA	ARRAY+2	X
	CAL*	2,4	ARRAY LENGTH
	PDX	0,1	PLACED IN I.R. 1
	TXL	SMLARY,1,2	SMALL ARRAY, LENGTH EQUAL TO 1 OR 2
	CAL*	3,4	FORTRAY ADDRESS BLOCK TO
	ARS	18	SHIFT TO ADDRESS PORTION OF WORD
	STA	STORE	STORED FOR REFERENCE
	SUB	ADDR1	WILL BE STORING THREE WORDS AT A TIME
	STA	STORE+1	X
	SUB	ADDR1	X
	STA	STORE+2	X
ARRAY	CLA	**,2	TRANSFER OF WORDS
	LDA	**,2	X
	LDI	**,2	X
	SEB		X
STORE	STO	**,2	STORED
	STQ	**,2	X
	STJ	**,2	X
	TXI	**1,2,3	MOVE DOWN THROUGH BLOCK
	SEA		X
	TEX	ARRAY,1,3	REDUCE BLOCK BY 3
	TXH	ARRAY3,1,2	IF 3 WORDS, SET I.R. 1 = 0
	TXH	TWOADS,1,1	TEST FOR REMAINING (1 OR 2) WORDS
	TXL	RETURN,1,0	X
ONEWD	CAL	1,4	TRANSFERRING TOTAL OF 1 WORD, OR
	STA	ARRAY1	REMAINING WORD FROM A TO B CORE
	CAL*	3,4	X
	ARS	18	X
	STA	STORE1	X
ARRAY1	CLA	**,2	X
	SEB		X
STORE1	STO	**,2	X
	RESET	SEA	X
RETURN	LXA	STOIR,1	RETURN TO FORTRAN

```

LXD STOR1+2 ----X
LDL STOR1D ----X
TRA 4,4 ----X
SMARY TXL ONEHD;L;J .. TEST FOR 1 OR 2 WORDS IN ARRAY
THWDS CAL 1,4 .. TRANSFERRING TOTAL OF 2 WORDS; DR
STA ARRAY2 .. REMAINING 2 WORDS FROM A TO B CORE
SUB ADDR1 ----X
STA ARRAY2+1 ----X
CLA# 3,4 ----X
ARS 18 ----X
STA STOR2 ----X
SUB ADDR1 ----X
STA STOR2+1 ----X
ARRAY2 CLA ##;2 ----X
LDQ ##;2 ----X
SEB ----X
STOR2 STO ##;2 ----X
STQ ##;2 ----X
TRA RESET ----X
ARRAY3 AXT 0,1 .. 3 WORDS; ZERO I,R, 1
TRA ARRAY X
ERROR WTD 3
RCHR READ
TCOA *
TRA 4,4
READ JDCD .. WORDS;L;R
WORDS BCI 9,1+ SUBROUTINE STASH CANNOT BE EXECUTED FROM B CORE
ADDR1 OCT 1
STOIN BSS 1
STOIN BSS 1
END
* SUBROUTINE TIMC4
* CARDS COLUMN
* LISTB
* LABEL
SUBROUTINE TIMC4(DJO,TSEP,S;F,DT)
USES SUBROUTINE TIMEC AND GIVES OUTPUT ON
TAPES A3 AND A8
VERSION OF 7/22/63
READS A CARD FROM CARD READER CONTAINING CALENDAR DATE AND UT2 OF
DESIRED START AND END TIMES FOR CALCULATION OF AN EPHEMERIS, AND
THE TIME INCREMENT OF THE EPHEMERIS IN SECONDS. CALCULATES TIME
INTERVAL IN SECONDS FROM SOME EPOCH (DJO,TSEP) TO THE START AND
END TIMES.
WRITES CALENDAR DATE AND UT2 ON TAPE UNIT A3.
INPUT FROM CALLING SEQUENCE
DJO = EPOCH JULIAN DATE AT 0 HOURS UT2.
TSEP = EPOCH UT2 IN SECONDS
INPUT FROM CARD READER
NMS,NDS,NYS = MONTH, DAY, YEAR OF START DATE
NMF,NDF,NYF = MONTH, DAY, AND YEAR OF END DATE
NHS,NMNS,TSS = HOUR, MINUTE, SECOND (UT2) OF START TIME
NHF,NMNF,TSF = HOUR, MINUTE, SECOND (UT2) OF END DATE
DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
OUTPUT
S = TIME IN SECONDS FROM EPOCH TO START TIME
F = TIME IN SECONDS FROM EPOCH TO END TIME
DT = TIME INCREMENT OF EPHEMERIS IN SECONDS
REQUIRED SUBPROGRAMS
DJUL, JULCAL 07/22/60 - FAP DOUBLE ENTRY PROGRAM
6015 FORMAT (2I1X12),1X,I4,2I3,F7.3,13,1X,I2,1X,I4,2I3,F7.3,F11.3 )
6016 FORMAT (1X12,1H/12,1H/14,7X11H START DATE/1X12,13,F7.3,5X,
1 15H START TIME-UT2/1X12,3,5X23H TIME INCREMENT-SECONDS//1X12,
2 1H/12,1H/14,7X9H END DATE/1X12,13,F7.3,5X13H END TIME-UT2 )
READ 6015,NMS,NDS,NYS,NHS,NMNS,TSS,NMF,NDF,NYF,NHF
1 NMNF,TSF,DT
WRITE OUTPUT TAPE 3,6016,NMS,NDS,NYS,NHS,NMNS,TSS,DT,NMF,NDF,NYF,
1 NMF,NMNF,TSF
WRITE OUTPUT TAPE 8,6016,NMS,NDS,NYS,NHS,NMNS,TSS,DT,NMF,NDF,NYF,
1 NMF,NMNF,TSF
PRINT 6016,NMS,NDS,NYS,NHS,NMNS,TSS,DT,NMF,NDF,NYF,NHF,NMNF,TSF
IF ISENSE SWITCH 0) 1;2
1 PRINT 6016,NMS,NDS,NYS,NHS,NMNS,TSS,DT,NMF,NDF,NYF,NHF,NMNF,TSF
2 DJSO=DJUL(NMS,NDS,NYS)
DJFO=DJUL(NMF,NDF,NYF)
THS=NMS*3600
TMNS=NMNS*60
TS=THS+TMNS+TSS-TSEP
THF=NMF*3600
TMNF=NMNF*60
TF=THF+TMNF+TSF-TSEP
DJS=DJSO-DJO
DJF=DJFO-DJO
S=DJS+86400.*TS
F=DJF+86400.*TF

```

```

RETURN
END
SUBROUTINE SUN
  CARDS COLUMN
  LISTB
  LABEL
  SUBROUTINE SUN(DJ,ET,CL)

```

```

THEORY AND ANALYSIS OFFICE - GSEC
ONLY COMPUTES LONGITUDE IN RADIANs - ECLIPTIC
VERSION OF 9/15/64

```

```

WOOLARD'S ABBREVIATED VERSION OF NEWCOMB'S THEORY OF THE SUN.

```

```

INPUT
  DJ = JULIAN DATE AT 0 HOUR'S EPHEMERIS TIME.
  ET = EPHEMERIS TIME IN RADIANs [24 HOURS = 2 PI RADIANs].
  ET IS RESTRICTED TO LIE BETWEEN 0 AND +2 PI RADIANs.

```

```

OUTPUT
  GEOMETRIC COORDINATES OF THE SUN, TRUE EQUINOX
  AND ECLIPTIC OF DATE.
  CL = LONGITUDE IN RADIANs.

```

```

REFERENCES
  ASTRONOMICAL PAPERS PREPARED FOR THE USE OF THE AMERICAN
  EPHEMERIS AND NAUTICAL ALMANAC. VOLUME 15, PART 1 (THEORY
  OF THE ROTATION OF THE EARTH AROUND ITS CENTER OF MASS -
  BY EDGAR N. WOOLARD - PAGES 53, 64 - 66 ).

```

```

RESTRICTIONS
  WOOLARD HAS USED NEWCOMB'S THEORY OF THE SUN, NEGLECTING
  ALL PERIODIC TERMS WITH COEFFICIENTS GREATER THAN .001
  SECONDS OF ARC IN LONGITUDE AND LATITUDE, AND GREATER
  THAN 7 UNITS IN THE 8TH DECIMAL OF THE LOGARITHM
  OF THE RADIUS VECTOR.

```

```

COMPUTE TIME IN JULIAN CENTURIES ELAPSED SINCE 1900 JAN. 0.5 ET

```

```

DIMENSION S(35),C(35),C(123),E(23),S(28),H(28),C(41),G(45)
PRT1=DJ-2419020.0
PRT2=ET/6.28318531
T=PRT1+PRT2/36525.0
T2=T*T
T3=T2*T

```

```

COMPUTE FUNDAMENTAL ARGUMENTS

```

```

MEAN LONGITUDE - SUN
  X = 3.5284469 E-5 *T2
  CL1 = 4.881627934112 + 628.331950990909*T + X

```

```

MEAN ANOMALY - VENUS
  X = 0.22446873 E-4 *T2
  G1 = 3.710626228126 + 1021.328348655046*T + X

```

```

MEAN ANOMALY - EARTH
  X = 0.2617994 E-5 *T2 + 0.58178 E-7 *T3
  G2 = 6.256583580497 + 628.301945726741*T - X

```

```

MEAN ANOMALY - MARS
  X = 0.3156137 E-5 *T2
  G3 = 5.57684377809 + 334.053549190822*T + X

```

```

MEAN ANOMALY - JUPITER
  G4 = 3.932889060231 + 52.965367620264*T

```

```

MEAN ANOMALY - SATURN
  G5 = 3.062637351924 + 21.320095075899*T

```

```

MEAN ANOMALY - MOON
  X = 0.163424846 E-3 *T2 + 0.251133 E-6 *T3
  SL = 5.158000345744 + 8328.691103668024*T + X

```

```

MEAN ANOMALY - SUN
  X = 0.2617994 E-5 *T2 + 0.58178 E-7 *T3
  SL1 = 6.256583590497 + 628.301945726741*T - X

```

```

MEAN ARGUMENT OF LATITUDE - MOON
  X = 0.56344461E-4*T2 + 0.5818E-8*T3
  F = 0.196365054887 + 8433.466291171947*T - X

```

```

MEAN ELONGATION OF MOON FROM SUN
  X = 0.32967E-7*T3 - 0.25064867E-4*T2

```

```

D. D = 6.121523942807 ± 777L377193934895 *T+X
C
C LONGITUDE OF MEAN ASCENDING NODE - PDDN
C
C X = 0.36284063E-4+T2 + 0.38785E-7+T3
C W = 4.523601514852 - 33.757146246651T + X
C
C REDUCE ALL ANGLES BY MODULUS 2 PI
C
C
C CL1 = MODF (CL1,6.283185307179586)
D G1 = MODF (G1,6.283185307179586)
D G3 = MODF (G3,6.283185307179586)
D G4 = MODF (G4,6.283185307179586)
D G5 = MODF (G5,6.283185307179586)
D SL = MODF (SL,6.283185307179586)
D SL1 = MODF (SL1,6.283185307179586)
D D = MODF (D,6.283185307179586)
D F = MODF (F,6.283185307179586)
D W = MODF (W,6.283185307179586)
C
C COMPUTE EXCEPTIONAL ARGUMENTS
C
1400 EA1 = 8.0*S11-15.0*G3
EA2 = 3.0*G4-3.0*G3+4.0*S11
EA3 = .785398163327446E-1+T-R*0*G1+13.0*S11
EA4 = 7.0*S11-(3.0*G1+4.0*G3)
EA5 = (F+W)+(F+W)
EA6 = EA5-(D*2)
C COMPUTE SINES AND/OR COSINES OF 16 ARGUMENTS
1500 S11 = SINP(SL1)
CS11 = COSP(SL1)
S1 = SINP(SL)
CS1 = COSP(SL)
S01 = SINE(G1)
C01 = COSP(G1)
S03 = SINP(G3)
C03 = COSP(G3)
S04 = SINP(G4)
C04 = COSP(G4)
S05 = SINP(G5)
C05 = COSP(G5)
S0 = SINP(F)
C0 = COSP(D)
S0W = SINP(W)
C0W = COSP(W)
C28 = COSP(EA1)
S49 = SINP(EA2)
C49 = COSP(EA2)
S51 = SINP(EA3)
C51 = COSP(EA3)
S52 = COSP(EA4)
S46 = SINP(EA5)
S47 = SINP(EA6)
S44A = S11*CD
S44B = C11*SD
S44 = S44A+S44B
S45 = S44A-S44B
C45A = C11*CD
C45B = S11*SD
C45 = C45A+C45B
C75 = C45A-C45B
C76 = C45A*(4.0*CD+CD-3.0)+C45B*(3.0-4.0*SD+SD)
C EVALUATE ALL OTHER SINES AND COSINES IN TERMS OF ABOVE
X = 2.0*CS11
S01 = X *S11
C01 = X *CS11-1.0
X = 2.0*C01
S02 = (X +1.0)*S11
C02 = (X -1.0)*CS11
S03 = 2.0*S0*CW
S04 = S11*C01-CS11*S01
C04 = CS11*C01+S11*S01
S05 = S04 *C01-C04 *S01
C05 = C04 *C01+S04 *S01
X = 2.0*C04
S06 = X *S04
C06 = X *C04-1.0
S07 = S11*C06+CS11*S06
C07 = CS11*C06-S11*S06
X = 2.0*C06
S08 = (X +1.0)*S04
C08 = (X -1.0)*C04
S09 = S11*C08+CS11*S08
C09 = CS11*C08-S11*S08
S10 = S611*C09+CS11*S09
C10 = CS11*C09-S11*S09
X = 2.0*C08
S11 = X *S06
C11 = X *C06-1.0
S12 = S11*C11+CS11*S11
S13 = S01 *C11+C01 *S11
C13 = C01 *C11-S01 *S11

```

```

S14 =S11 *CG4+C11 *S04.
C14 =C11 *CG4-C11 *S04.
S15 =S01 *C14+C01 *S14
C16 =CG0 *C14-S02 *S14
C17 =CG4 *C14-S04 *S14
S18 =SS11*CG3-C20*S02
C18 =C011*CG3+SS11*S03
S19 =S18 *CG3-C18 *SG3
C19 =C18 *CG3+S18 *SG3
X =2.0*C18
S20 =X *S18
C20 =X *C18-1.0
S21 =S20*CG3-C20*S03
C21 =CG29*CG3-C20*S02
C22 =C18*C20-S18*S20
S23 =S21*CG3-C21*S03
C23 =C21*CG3+S21*S03
S24 =SS11*CG3-C21*S03
C24 =C011*CG3-SS11*S23
S25 =S24 *CG3-C24 *SG3
C25 =C24 *CG3+S24 *SG3
C26 =C011*CG3-SS11*S25
S27 =S18*CG3+C18*S25
C27 =C18*C25-S18*S25
S29 =SS11*CG4-C511*S04
C29 =C511*CG4+SS11*S04
S30 =SS11*CG9-C511*S29
C30 =C511*CG9-SS11*S29
S31 =S29 *CG4-C29 *SG4
C31 =CG29 *CG4+S29 *SG4
X =2.0 *CG29
S32 =X *S29
C32 =X *CG29-1.0
C33 =C011*CG3-C511*S32
S34 =S31 *CG4-C31 *SG4
C34 =C31 *CG4+S31 *SG4
S35 =S32 *CG4-C32 *SG4
C35 =C32 *CG4+S32 *SG4
S36 =S29 *CG3-C29 *S32
C36 =C29 *CG3-S29 *S32
C37 =C35 *CG4+S35 *SG4
S38 =S35 *CG4-C36 *SG4
C39 =C511*CG4-SS11*S04
S40 =SS11*CG5-C511*S05
C40 =C511*CG5+SS11*S05
C41 =C40 *CG5+S40 *SG5
X =2.0 *C40
C42 =X *C40-1.0
S43 =SS11*CG -C511*S0
C77A =C511*CG
C77B =SS11*S0
C77 =C77A-C77B
C78 =C77A+C77B
X =C511*C49
Y =SS11*S49
C48 =X +Y
C50 =X -Y

```

C COMPUTE LOG611JDE OF SUN (HEAN LUNG. + TABLE 8) 4000LD 2P1

```

1800 C11 J=SS11*(+33502.E-6)
C12 J=S01 *(+ 351.E-6)
C13 J=S02 *(+ 5.E-6)
C14 J=S49 *(+ 25.E-6)
C15 J=S04 *(+ 20.E-6)
C16 J=S05 *(+ 14.E-6)
C17 J=S07 *(+ 9.E-6)
C18 J=S09 *(+ 2.E-6)
C19 J=S12 *(+ 3.E-6)
C110)=S51 *(+ 7.E-6)
C111)=S19 *(+ 1.E-6)
C112)=S23 *(+ 3.E-6)
C113)=S19 *(+ 3.E-6)
C114)=S21 *(+ 1.E-6)
C115)=S24 *(+ 2.E-6)
C116)=S23 *(+ 1.E-6)
C117)=S29 *(+ 1.E-6)
C118)=S04 *(+ 13.E-6)
C119)=S32 *(+ 13.E-6)
C120)=S31 *(+ 7.E-6)
C121)=S35 *(+ 3.E-6)
C122)=S34 *(+ 1.E-6)
C123)=S40 *(+ 2.E-6)
C124)=S05 *(+ 2.E-6)
C125)=SS11*(+ 8358.E-8)*T
C126)=S01 *(+ 175.E-8)*T
C127)=SS11*(+ 29.E-8)*T+T
C128)=S0 *(+ 31.E-6)
C129)=S44 *(+ 1.E-6)
C130)=S45 *(+ 2.E-6)
C131)=S43 *(+ 1.E-6)
C132)=S0 *(+ 84.E-6)
C133)=S03 *(+ 1.C-6)
C134)=S47 *(+ 6.C-6)
C135)=S45 *(+ 1.E-6)
1900 C11 J=C04 *(+ 11.1.C-6)

```

```

E(2 )=C06 *(- 23.E-6)
E(3 )=C07 *(+ 9.E-6)
E(4 )=C08 *(- 3.E-6)
E(5 )=C09 *(+ 7.L-6)
E(6 )=C10 *(+ 4.E-6)
E(7 )=C11 *(- 1.E-6)
E(8 )=C13 *(+ 1.E-6)
E(9 )=C15 *(+ 1.E-6)
E(10)=C51 *(+ 6.E-6)
E(11)=C49 *(+ 18.E-6)
E(12)=C18 *(- 1.E-6)
E(13)=C20 *(+ 10.E-6)
E(14)=C13 *(- 8.E-6)
E(15)=C21 *(+ 2.E-6)
E(16)=C23 *(+ 3.E-6)
E(17)=C28 *(+ 1.E-6)
E(18)=C30 *(- 1.E-6)
E(19)=C29 *(- 35.E-6)
E(20)=C04 *(- 1.E-6)
E(21)=C31 *(- 3.E-6)
E(22)=C36 *(- 1.E-6)
E(23)=C52 *(- 1.E-6)
T8S = C(1)
DO 1930 J=2,35
1930 T8S = T8S+C(J)
      T8C = E(1)
1940 T8C = T8C+E(J)
      T488 = T8S + T8C
1950 CL =MDDF(T488*CL1, 6.283185307179586)
9000 RETURN
      END
      * SUBROUTINE ARKTAN
      * CARDS COLUMN
      * LIST8
      * LABEL
      * SUBROUTINE ARKTAN(Y,X,Z,N)
      * IF (X) 6,5,6
      * 5 IF (Y) 7,8,9
      * 7 IF (N) 10,11,10
      * 11 Z = -90.
      * GO TO 500
      * 10 Z = -1.5707964
      * GO TO 500
      * 8 Z = 0.
      * GO TO 500
      * 9 IF (Y) 12,13,12
      * 13 Z = 90.
      * GO TO 500
      * 12 Z = 1.5707964
      * GO TO 500
      * 6 IF (Y) 15,15,14
      * 15 IF (X) 15,17,17
      * 16 IF (N) 18,19,18
      * 19 Z = 180.
      * GO TO 500
      * 18 Z = 3.1415927
      * GO TO 500
      * 17 Z = 0.
      * GO TO 500
      * 14 IF ACCUMULATOR OVERFLOW 30,30
      * 30 IF JOTIEVF JVERFLOW 31,31
      * 31 IF DIVIDE CHECK 32,32
      * 32 A = ARSF (Y)
      * B = ARSF (X)
      * Z = A/B
      * IF DIVIDE CHECK 33,34
      * 33 Z = 0.
      * GO TO 500
      * 34 Z = ATANF(Z)
      * IF (Y) 50,51,51
      * 50 IF (X) 52,53,53
      * 52 Z = Z-3.1415927
      * GO TO 500
      * 53 Z = -Z
      * GO TO 600
      * 51 IF (X) 54,600,600.
      * 54 Z = 3.1415927-Z
      * GO TO 600
      * 600 IF (N) 500,55,500
      * 55 Z = (180./3.1415927)*Z
      * 500 RETURN
      * END
      * SUBROUTINE TESCOV CONVERTS 3 DIGIT INTEGER INTO BCD FORM
      * CARDS COLUMN
      * LIST8
      * FAP
      * COUNT 20
      * LBL TESCOV,X
      * ENTRY TESCOV
      * TESCOV CLA= 1,4
      * RCYDEC ARS= 18
      * ANA, IBADR
      * LDQ BLNKS

```

ALLOT001
ALLOT002

```

VDP      RCVDI+6
VDP      BCVDI+1+6
VDP      BCVDI+3+6
VDP      BCVDI+3+6
VDP      BCVDI+3+6
RQL      18
STQ*     2,4
TRA      3,4
BCVDI DEC -840000,-6096000,-26214400,-167772160,-1073741824
ISADR DCT 00000007777
BLNKS BCL 1
END
* SUBROUTINE CH65K      TESTS FOR 65K.
* CARDS COLUMNS
* LISTB
* FAP
COUNT 20
LBL CH65K*
ENTRY CH65K
CH65K SEB
EFT
TRA **4
XN32K CLA B32
STQ* 1,4
TRA 2,4
SEA
EFT
TRA XN32K
STQ* 1,4
TRA 2,4
B32 DCT 00000400000

```

```

-----
_FORTRAN CALLING SEQUENCE =
CALL CH65K(N)

```

```

MACHINE IS IN 32K -- N

```

```

MACHINE IS IN 65K -- N = 0

```

APPENDIX VIII (PART A)
SAMPLE INPUT
FOR MAIN PROGRAM ONE

RELAY 2 12 STATION TEST

+04+01+01-01 +4 5000.
 33333 640114 2157 00000 00000
 +17470063+01+23653052+00+81153895+00+62823296+01+32527117+01+38506655+01 TEST
 33333 640114 2157 00000 +00000000+00
 01/15/1964 20 00 00,000 01/16/1964 20 00 00,000 +120.
 +12+00+00
 90.0 0.0 178. 25.
 CBMNUIT -75 00 0.000 +40 00 0.000 0.0
 CBMAND -068 40 00.000 +44 54 00.000 38.
 CBMHIL -05 10 29.0 +50 02 58.0 350.0
 CBMGER +10 00 00.000 +51 00 00.000 50.
 CBMTEL +13 36 5.000 +41 58 41.000 2168.6
 CBMRI9 -43 22 7.000 -22 57 9.000 0.0
 CBMNUIT -75 00 0.000 +40 00 0.000 0.0
 CBMAND -068 40 00.000 +44 54 00.000 38.
 CBMHIL -05 10 29.0 +50 02 58.0 350.0
 CBMNUIT -75 00 0.000 +40 00 0.000 0.0
 CBMAND -068 40 00.000 +44 54 00.000 38.
 CBMHIL -05 10 29.0 +50 02 58.0 350.0

APPENDIX VIII (PART B)
MAIN PROGRAM ONE OUTPUT

BAR GRAPHS
TAPE A3

RELAY 2 12 STATION TEST

RELAY 2 12 STATION TEST

5.0799999E 03 FEET PER NAUTICAL MILE

5376.388 EQUATORIAL RADIUS OF EARTH IN KM
297.0 INVERSE OF FLATTENING
3.98626870E 05 GM (KM. CUBED/SECONDS SQUARED)

HARMONICS OF EARTHS GRAVITATIONAL POTENTIAL

1.082190E-03 J2
-2.285000E-06 J3
-2.123000E-06 J4
-2.320000E-07 J5

EPOCH 54 1 14 21 57 .00

A E I M OMEGA THETA
1.7470063E 00 2.3693052E-01 8.1153895E-01 6.2823295E 00 3.2527117E 00 3.8505655E 00

DRAG EFFECTS T (P,0) N (2,0) N (3,0)
64 114 2157 0 0.

LOOK ANGLE CALCULATIONS - START AND END TIMES

1/15/1964 START DATE
20 0 0. START TIME-UT2
120.000 TIME INCREMENT-SECONDS

1/16/1964 END DATE
20 0 0. END TIME-UT2

LOCAL STATION PREDICTIONS FOR --

STATION	LONGITUDE	LATITUDE	HEIGHT (METERS)
COMNUT	-75 0 0.	40 0 0.	0.
COMAND	-68 40 0.	44 54 0.	38.00
COMHIL	-5 10 29.000	50 2 58.000	350.00
COMGER	10 0 0.	51 0 0.	50.00
COMTEL	13 36 54.000	41 58 41.000	2168.50
COMRIO	-43 22 7.000	-22 57 9.000	0.
COMNUT	-75 0 0.	40 0 0.	0.
COMAND	-68 40 0.	44 54 0.	38.00
COMHIL	-5 10 29.000	50 2 58.000	350.00
COMNUT	-75 0 0.	40 0 0.	0.
COMAND	-68 40 0.	44 54 0.	38.00
COMHIL	-5 10 29.000	50 2 58.000	350.00

CONTROL STATIONS ARE

COMNUT
COMAND
COMHIL
COMGER

NO STATION PRINT OUT IF --

ELEVATION IS LESS THAN 0 DEGREES

5 IS PRINTED IF THE ELEVATION IS GREATER THAN OR EQUAL TO 0 AND LESS THAN 5 DEGREES
9 IS PRINTED IF THE ELEVATION IS GREATER THAN OR EQUAL TO 5 AND LESS THAN 10 DEGREES
A IS PRINTED IF THE ELEVATION IS GREATER THAN OR EQUAL TO 10 DEGREES

A T IS PRINTED OF RANGE IS GREATER THAN 0.50300000E 00NAUTICAL MILES

SPIN AXIS COORDINATES ARE
178.0 DEGREES RIGHT ASCENSION
25.0 DEGREES DECLINATION

THE 3 DIGIT NUMBERS UNDER THE STATION NAMES ARE THE SPACECRAFT LOOK ANGLES.

ORBIT NUMBER 0
MUTUAL VISIBILITY OF 33333 FOR THE FOLLOWING STATIONS
DATE(EHH/00/YY) = 1/15/64

HHMM	NUT	AND	HIL	GER	TEL	RIO	NUT	AND	HIL	NUT	AND	HIL
20 0	068	A	072	A			068	A	072	A		
20 2	071	A	075	A			071	A	075	A		
20 4	075	A	079	A			075	A	079	A		
20 6	078	A	083	A			078	A	083	A		
20 8	083	A	087	A			083	A	087	A		
20 10	088	A	093	A			088	A	093	A		
20 12	094	A	099	A			094	A	099	A		
20 14	101	A	106	A	114	5	101	A	106	A	114	5
20 16	108	A	114	A	119	5	108	A	114	A	119	5
20 18	116	A	123	A	124	5	116	A	123	A	124	5
20 20	123	A	132	A	131	5	123	A	132	A	131	5
20 22	128	A	139	A	137	5	128	A	139	A	137	5
20 24	131	A	142	A	144	5	131	A	142	A	144	5
20 26	132	A	143	A	152	5	132	A	143	A	152	5
20 28	131	A	141	A	160	5	131	A	141	A	160	5
20 30	128	A	137	A	168	5	128	A	137	A	168	5
20 32	126	9	133	9	177	5	126	9	133	9	177	5
20 34			129	5			087	5	126	9	133	9
20 36							088	9				
20 38							088	A				
20 40							087	A				
20 42							086	A				
20 44							083	A				
20 46							081	A				
20 48							078	A				
20 50							075	9				
20 52							072	5				
20 54							070	5				

TAPE A8
WORLD MAP
LOCAL STATION PREDICTIONS
SUN LIGHT HISTORY

RELAY 2 12 STATION TEST

5.07999998E 03 FEET PER NAUTICAL MI.±
5378.388 EQUATORIAL RADIUS OF EARTH IN KM
297.0 INVERSE OF FLATTENING
3.98626876E 05 G⁴ (KM. CUBED/SECONDS SQUARED)
HARMONICS OF EARTHS GRAVITATIONAL POTENTIAL
1.082190E-03 J2
-2.285000E-06 J3
-2.123000E-06 J4
-2.320000E-07 J5
EPOCH 64 1 14 21 57 0.
A E I H OMEGA THETA
1.7470063E 00 2.3653052E-01 8.1193895E-01 6.2823296E 00 3.2527117E 00 3.8506655E 00
DRAG EFFECTS I (P.0) N (2.0) N (3.0)
64 114 2157 0 0.
LOOK ANGLE CALCULATIONS - START AND END TIMES
1/15/1964 START DATE
20 0 0. START TIME-UT2
120.000 TIME INCREMENT-SECONDS
1/16/1964 END DATE
20 0 0. END TIME-UT2

CONTROL STATIONS ARE
COMMUT
COMAND
COMHIL
COMGER

S IS PRINTED WHEN THE SATELLITE IS IN THE SUNLIGHT

		ORBIT NUMBER		0				
LOCAL STATION PREDICTIONS AND SATELLITE WORLD MAP FOR 33333								
YNNKDD	HMMN	STAY.	RANGE (KM)	AZI.	ELEV.	S/C LOOK ANGLE DEGREES	LAT. LONG. HEIGHT (KM)	
64	115	20	0	CONNUT	6619.0	295.1	29.8 68.9	46.0 -116.7 4853.8 S
				COMAND	6854.6	289.3	26.2 72.9	
				CONNUT	6619.0	295.1	29.8 68.9	
				COMAND	6854.6	289.3	26.2 72.9	
				CONNUT	6619.0	295.1	29.8 68.9	
				COMAND	6854.6	289.3	26.2 72.9	
64	115	20	2	CONNUT	6166.2	295.8	33.9 71.9	46.4 -112.1 4594.3 S
				COMAND	6402.8	288.6	30.1 76.0	
				CONNUT	6166.2	295.8	33.9 71.9	
				COMAND	6402.8	288.6	30.1 76.0	
				CONNUT	6166.2	295.8	33.9 71.9	
				COMAND	6402.8	288.6	30.1 76.0	
64	115	20	4	CONNUT	5715.0	296.5	38.6 75.2	46.5 -107.2 4522.5 S
				COMAND	5941.3	287.5	34.4 79.5	
				CONNUT	5715.0	296.5	38.6 75.2	
				COMAND	5941.3	287.5	34.4 79.5	
				CONNUT	5715.0	296.5	38.6 75.2	
				COMAND	5941.3	287.5	34.4 79.5	
64	115	20	6	CONNUT	5270.4	297.3	43.9 79.0	46.5 -102.2 4348.9 S
				COMAND	5484.4	286.0	39.3 83.4	
				CONNUT	5270.4	297.3	43.9 79.0	
				COMAND	5484.4	286.0	39.3 83.4	
				CONNUT	5270.4	297.3	43.9 79.0	
				COMAND	5484.4	286.0	39.3 83.4	
64	115	20	8	CONNUT	4839.1	298.4	50.0 83.4	46.2 -97.0 4174.3 S
				COMAND	5038.4	283.9	44.8 88.0	
				CONNUT	4839.1	298.4	50.0 83.4	
				COMAND	5038.4	283.9	44.8 88.0	
				CONNUT	4839.1	298.4	50.0 83.4	
				COMAND	5038.4	283.9	44.8 88.0	
64	115	20	10	CONNUT	4430.5	299.8	57.0 88.4	45.6 -91.7 3999.5 S
				COMAND	4611.7	280.5	51.1 93.3	

SUNLIGHT HISTORY OF 33333

SATELLITE WILL BE IN SUNLIGHT AT ALL TIMES EXCEPT WHEN IT WILL
ENTER SHADOW AT AND LEAVE SHADOW AT

YNNKDD HMMN YNNKDD HMMN DURATION (MIN) PERCENT IN SUNLIGHT

NO OUTPUT INDICATES THAT SPACECRAFT IS IN SUNLIGHT 100% OF TIME

APPENDIX VIII

PART C

OUTPUT OF MAIN PROGRAM TWO

TAPE A3
WORLD MAP AND BAR GRAPHS

SANDTRACKS, ORBITAL COMPUTING SYSTEM

DELAY TEST 12 STATIONS

```

10.0E-09      TOLERANCE REQUIRED FOR KEPLER SUBROUTINE
6378.388      EQUATORIAL RADIUS OF EARTH IN KM
297.0         INVERSE OF FLATTENING
3.98626876E 05 GM (KM. CUBED/SECONDS SQUARED)

             HARMONICS OF EARTHS GRAVITATIONAL POTENTIAL
1.082190E-03  J2
-2.285000E-06 J3
-2.123000E-06 J4
-2.320000E-07 J5

2.20138180E 04 BRUWER HARMONICS COMPUTED FROM J2, J3, J4, AND J5
5.92951238E 05 K2 (KILOMETERS SQUARED)
1.31772552E 09 K3 (KILOMETERS CUBED)
2.44950354E 12 K4 (KILOMETERS FOURTH POWER)
                K5 (KILOMETERS FIFTH POWER)

1/14/1964     EPOCH DATE OF PARAMETERS
21 57 -0.    EPOCH TIME OF PARAMETERS-UT2
                INPUT OPTION NUMBER
                INPUT PARAMETERS ARE---

BRUWER MEAN ELEMENTS
REQUIRED UNITS - ALL ANGLES IN DEGREES, SEMI-MAJOR AXIS IN KILOMETERS
11143.3840    SEMI-MAJOR AXIS-KILOMETERS
0.23653051    ECCENTRICITY
46.497756     INCLINATION -DEGREES
220.526879    RA. ASC. NODE -DEGREES
166.386648    ARC. OF PERIGEE-DEGREES
359.950966    MEAN ANOMALY -DEGREES

WORLD MAP CALCULATIONS - START AND END TIMES
1/15/1964     START DATE
20 0 0.       START TIME-LT2
120.000       TIME INCREMENT-SECONDS

1/16/1964     END DATE
20 0 0.       END TIME-UT2

LECK ANGLE CALCULATIONS - START AND END TIMES
1/15/1964     START DATE
10 0 0.       START TIME-LT2
120.000       TIME INCREMENT-SECONDS

1/16/1964     END DATE
10 0 0.       END TIME-UT2

```

SANDFACKS ORBITAL COMPUTING SYSTEM

RELAY TEST 12 STATIONS

QUANTITIES COMPUTED FROM INPUT

1/14/1964	EPOCH DATE OF PARAMETERS	---	---	---
21 57 -0.	EPOCH TIME OF PARAMETERS	UT2		
POSITION AND VELOCITY VECTORS - GEOCENTRIC EQUATORIAL INERTIAL				
5966.52051	X1 - KILOMETERS	0.94013103	X1 - VAN GUARD UNITS	
5966.32159	X2 - KILOMETERS	0.94009985	X2 - VAN GUARD UNITS	
-682.69296	X3 - KILOMETERS	-0.10703221	X3 - VAN GUARD UNITS	
-4.02792885	VX1 - KM/SEC	-0.50951149	VX1 - VAN GUARD UNITS	
3.40607376	VX2 - KM/SEC	-0.43085013	VX2 - VAN GUARD UNITS	
-5.48964036	VX3 - KM/SEC	-0.69441018	VX3 - VAN GUARD UNITS	
8507.65540	R - KILOMETERS	1.33382532	R - VAN GUARD UNITS	
7.61325824	V - KM/SEC	0.96303649	V - VAN GUARD UNITS	

TRUNCATION FACTORS USED IN COMPUTING BROWER MEAN ELEMENTS FROM OSCILLATING ELEMENTS

5.0E-04	SEMI-MAJOR AXIS - KILOMETERS
5.0E-06	ECCENTRICITY
5.0E-06	INCLINATION - DEGREES
5.0E-06	R.A. ASC. NODE - DEGREES
5.0E-06	ARC. OF PERIGEE - DEGREES
5.0E-06	MEAN ANOMALY - DEGREES

CRITICAL ELEMENTS

OSCILLATING ELEMENTS BROWER MEAN ELEMENTS

11150.8829	11143.0640	SEMI-MAJOR AXIS - KILOMETERS
0.23704214	0.23653051	ECCENTRICITY
46.509814	46.497756	INCLINATION - DEGREES
220.619161	220.626875	R.A. ASC. NODE - DEGREES
186.266777	186.366640	ARC. OF PERIGEE - DEGREES
0.050050	359.950958	MEAN ANOMALY - DEGREES
3.251240	PERIOD	-HOURS
155.0744		-MINUTES
110.726969	MEAN MOTION	-DEGREES/HOUR
-1.042296	MOTION OF NODE	- DEGREES/DAY
1.085400	MOTION OF PERIGEE	- DEGREES/DAY
		WORLD MAP

DATE MO/DY/YR	UNIVERSAL TIME		GEODEIC COORDINATES		
	H	M SEC.	LATITUDE-DMS	LONGITUDE-DMS	HEIGHT-KM.
1/15/64	20	0 C.CCC	45 58 3.44	-116 41 9.76	4863.764
1/15/64	20	1 C.CCC	46 23 44.15	-112 3 20.31	4694.303
1/15/64	20	4 0.000	46 35 36.75	-107 12 31.30	4522.467
1/15/64	20	6 C.CCC	46 32 5.89	-102 10 21.52	4348.900
1/15/64	20	8 C.CCC	46 11 43.08	-76 59 43.31	4174.323
1/15/64	20	10 C.CCC	45 33 11.46	-91 43 48.92	3999.537
1/15/64	20	12 0.CCC	44 35 30.19	-96 26 5.46	3825.429
1/15/64	20	14 C.CCC	43 17 57.62	-81 9 58.17	3652.979
1/15/64	20	16 0.CCC	41 40 12.74	-75 58 33.43	3483.259
1/15/64	20	18 C.CCC	39 62 15.16	-70 54 25.40	3317.437
1/15/64	20	20 C.CCC	37 24 23.77	-65 59 27.44	3156.770
1/15/64	20	22 0.CCC	34 47 14.74	-61 14 49.10	3002.603
1/15/64	20	24 C.CCC	31 51 39.51	-56 40 58.13	2856.350
1/15/64	20	26 0.CCC	28 38 43.12	-52 17 45.57	2719.480
1/15/64	20	28 C.CCC	25 9 43.10	-48 4 32.26	2593.492
1/15/64	20	30 C.CCC	21 26 9.20	-44 0 15.90	2479.878
1/15/64	20	32 C.CCC	17 25 43.00	-40 3 35.58	2380.086
1/15/64	20	34 0.CCC	13 22 18.25	-36 13 2.11	2295.473
1/15/64	20	36 C.CCC	9 6 0.61	-32 26 51.37	2227.256
1/15/64	20	38 0.CCC	4 43 7.11	-28 43 16.92	2176.462
1/15/64	20	40 C.CCC	0 16 5.05	-25 0 26.26	2143.803
1/15/64	20	42 0.CCC	-4 12 30.38	-21 16 23.33	2130.034
1/15/64	20	44 0.CCC	-8 39 57.52	-17 29 9.25	2135.135
1/15/64	20	46 0.CCC	-13 3 31.88	-13 36 42.88	2159.090
1/15/64	20	48 C.CCC	-17 25 28.68	-9 37 2.52	2201.505
1/15/64	20	50 C.CCC	-21 28 5.68	-5 28 0.20	2261.690
1/15/64	20	52 0.CCC	-25 23 45.58	-1 8 5.78	2338.718
1/15/64	20	54 C.CCC	-29 4 58.28	3 24 47.24	2431.448
1/15/64	20	56 0.CCC	-32 29 23.01	8 11 52.97	2536.579
1/15/64	20	58 0.CCC	-35 34 56.78	13 14 2.16	2658.705
1/15/64	21	0 C.CCC	-38 19 27.46	18 31 21.17	2790.355
1/15/64	21	2 0.CCC	-40 41 37.96	24 2 59.79	2932.042
1/15/64	21	4 C.CCC	-42 46 11.25	29 46 56.24	3082.288
1/15/64	21	6 C.CCC	-44 14 25.80	35 40 4.06	3239.665

1/15/64	21 8	0.000	-45 24 14.38	41 38 0.97	3402.803
1/15/64	21 10	0.000	-46 10 6.21	47 36 18.24	3570.416
1/15/64	21 12	0.000	-46 33 7.64	53 29 18.83	3741.303
1/15/64	21 14	0.000	-46 34 54.49	59 12 19.32	3914.355
1/15/64	21 16	0.000	-46 17 27.11	64 41 12.54	4088.586
1/15/64	21 18	0.000	-45 52 35.28	69 52 53.88	4262.983
1/15/64	21 20	0.000	-44 53 45.54	74 45 26.98	4436.798
1/15/64	21 22	0.000	-43 52 12.25	79 17 58.76	4609.247
1/15/64	21 24	0.000	-42 40 12.84	83 30 28.57	4779.653
1/15/64	21 26	0.000	-41 19 58.53	87 23 34.53	4947.410
1/15/64	21 28	0.000	-39 52 23.97	90 58 20.69	5111.977
1/15/64	21 30	0.000	-38 19 36.97	94 16 6.06	5272.871
1/15/64	21 32	0.000	-36 42 33.88	97 18 16.56	5429.663
1/15/64	21 34	0.000	-35 2 13.38	100 6 18.94	5581.974
1/15/64	21 36	0.000	-33 19 23.70	102 41 37.30	5729.465

LOCAL STATION PREDICTIONS FOR

STATION	LONGITUDE	LATITUDE	HEIGHT (METERS)
COMNUT	-75 0 0	40 0 0	0
COMANC	-68 40 0	44 54 0	350.00
COMHIL	-5 10 25.000	50 2 58.000	350.00
COMGEF	10 0 0	51 0 0	50.00
COMTEL	13 26 5.000	41 56 41.000	2168.60
COMRKC	-43 22 7.000	-22 57 5.000	0
COMNUT	-75 0 0	40 0 0	0
COMANC	-68 40 0	44 54 0	350.00
COMHIL	-5 10 25.000	50 2 58.000	350.00
COMNUT	-75 0 0	40 0 0	0
COMANC	-68 40 0	44 54 0	350.00
COMHIL	-5 10 25.000	50 2 58.000	350.00

NO STATION PRINT OUT IF --

- ELEVATION IS LESS THAN 0 DEGREES
- RANGE IS GREATER THAN 100000. KILOMETERS
- RADAR ANGLE IS GREATER THAN 50.0 DEGREES OR LESS THAN 0. DEGREES

SPIN AXIS COORDINATES ARE 175.0 DEGREES RIGHT ASCENSION
25.0 DEGREES DECLINATION

LOCAL STATION PREDICTIONS

MUTUAL VISIBILITY

DATE	UNIVERSAL TIME	NUT	AND	HIL	GER	TEL	RID	NUT	AND	HIL	NUT	AND	HIL
1/15/64	10 0 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 2 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 4 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 6 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 8 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	10 10 C.000	*	*	*	*	*	*	*	*	*	*	*	*

1/15/64	11 52 0.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	11 54 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	11 56 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	11 58 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 0 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 2 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 4 0.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 6 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 8 0.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 10 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 12 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 14 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 16 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 18 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 20 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 22 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 24 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 26 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 28 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 30 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 32 0.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 34 C.000	*	*	*	*	*	*	*	*	*	*	*	*
1/15/64	12 36 C.000	*	*	*	*	*	*	*	*	*	*	*	*

1/15/64	12 38	0.000	*	*						*	*
1/15/64	12 40	0.000	*	*						*	*
1/15/64	12 42	0.000	*	*						*	*
1/15/64	12 44	0.000	*	*						*	*
1/15/64	12 46	0.000	*	*						*	*
1/15/64	12 48	0.000	*	*						*	*
1/15/64	12 50	0.000	*	*						*	*
1/15/64	12 52	0.000	*	*						*	*
1/15/64	12 54	0.000	*	*						*	*

LOCAL STATION PRECISIONS

DATE			UNIVERSAL TIME													
MO/DY/YR	H	M	SEC.	NUT	AND	HIL	GER	TEL	RIO	NIT	AND	HIL	NUT	AND	HIL	
1/15/64	12	56	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	12	58	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	0	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	2	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	4	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	6	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	8	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	10	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	12	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	14	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	16	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	18	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	20	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	22	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	24	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	26	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	28	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	30	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	32	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	34	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	36	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	13	38	0.000	*	*	*	*	*	*	*	*	*	*	*	*	

1/15/64	15	46	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	48	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	50	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	52	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	54	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	56	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	15	58	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	0	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	2	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	4	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	6	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	8	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	10	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	12	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	14	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	16	0.000	*	*	*	*	*	*	*	*	*	*	*	*	
1/15/64	16	18	0.000	*	*	*	*	*	*	*	*	*	*	*	*	

TAPE A6
LOCAL STATION PREDICTIONS

LOCAL STATION PREDICTIONS
MUTUAL VISIBILITY

DATE MO/DY/YR	UTZ		STATION	RANGE			AZ EL RADAR		
	H	M		(KM)	(DEG)	(DEG)	ANGLE	(DEG)	
1/15/64	10	0	COMFIL	6356.7	149.5	62.6	84.3		
			CONCER	6368.5	201.7	62.2	75.7		
			CONTEL	6144.1	249.3	72.2	69.0		
			COMHIL	6356.7	149.5	62.6	84.3		
			COMFIL	6356.7	149.5	62.6	84.3		
1/15/64	10	2	COMHIL	6214.4	138.5	62.6	87.9		
			CONCER	6141.3	193.8	65.5	79.0		
			CONTEL	5931.2	246.3	77.3	72.3		
			COMHIL	6214.4	138.5	62.6	87.9		
			COMHIL	6214.4	138.5	62.6	87.9		
1/15/64	10	4	CONCER	5931.5	182.7	68.4	82.6		
			CONTEL	5736.9	248.2	82.7	75.9		
1/15/64	10	6	CONCER	5743.3	167.9	70.3	86.6		
			CONTEL	5565.1	261.2	88.4	79.8		
1/15/64	10	8	CONTEL	5420.3	59.9	85.4	84.0		
1/15/64	10	10	CONTEL	5307.1	63.6	79.0	88.5		
1/15/64	11	52	COMRIC	10353.6	244.9	0.4	55.9		
1/15/64	11	54	COMRIC	10285.1	247.3	2.5	53.0		
1/15/64	11	56	COMRIC	10225.0	249.8	4.5	50.2		
1/15/64	11	58	COMRIC	10173.0	252.3	6.4	47.4		
1/15/64	12	0	COMRIO	10128.8	254.9	8.2	44.7		
1/15/64	12	2	COMRIO	10092.0	257.5	9.9	42.0		
1/15/64	12	4	COMRIO	10062.2	260.2	11.5	39.5		
1/15/64	12	6	COMRIC	10038.9	262.9	13.0	37.0		
1/15/64	12	8	COMNUI	11465.3	201.0	0.1	71.4		
			COMRIO	10021.8	265.7	14.3	34.6		
			COMNUT	11465.3	201.0	0.1	71.4		
			COMNUT	11465.3	201.0	0.1	71.4		

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APPLICATION TO THE AEROSPACE INDUSTRY IN
ST. LOUIS

Se-Hark Park

Washington University
St. Louis, Missouri

June 1965