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# TIME VARYING SOLAR CYCLE PROTONS PROGRAM MANUAL

BY

R. A. DEVANEY  
R. C. BLANCHARD  
J. ANDARY

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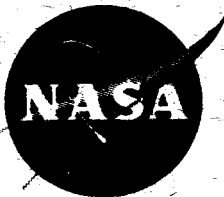
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GODDARD SPACE FLIGHT CENTER

GREENBELT, MD.

**TIME VARYING SOLAR CYCLE PROTONS  
PROGRAM MANUAL**

by

R. A. Devaney  
R. C. Blanchard  
J. Andary

Theoretical Division  
National Aeronautics and Space Administration  
GODDARD SPACE FLIGHT CENTER  
Greenbelt, Maryland

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# TIME VARYING SOLAR CYCLE PROTONS PROGRAM MANUAL

## INTRODUCTION

The purpose of this manual is to provide a detailed description of the programs employed in calculating the variation of the proton population in the earth's radiation belt due to solar cycle atmospheric and source changes. This report makes no attempt to make detail explanations of the theory involved in the calculations. An adequate list of references is provided for those interested in the explanation of the methods and the results to be expected. The entire process involves several interdependent steps. For example, the diurnal averaged atmosphere and the rings output from the B-L search routine are input to the longitudinal averaging processor. The output from this program is then used as input to the "bounce" average program and so forth. Each program description includes the equations used, a flow chart and Fortran listing of the program, input and output specifications, card descriptions, sample input and output data and running time. The code is written in Fortran II language and assembled under GSFC-NASA Theoretical Division monitor system on the IBM-7094 computer.

## I. DIURNAL AVERAGED ATMOSPHERE

Contained here are tables of number density vs. altitude and solar flux number. Separate tables of He, O, O<sub>2</sub>, N<sub>2</sub> and H are contained in Tables 1-5. The models are those generated by Harris and Priester.<sup>(2)</sup> Each model refers to a given solar radiation flux in units of 10<sup>-22</sup> watts/m<sup>2</sup>/cycle/sec. The link between solar flux, S, and time is given by Figure 1 (reproduced from reference 2 with the permission of Harris and Priester). This data is included for continuity and is used as input for the longitudinal averaging processor. The Harris and Priester atmosphere and solar flux vs. time curve is the data used and is subject to change as soon as better data becomes available. Such changes can be performed without effecting the logic of the following programs.

Table 1  
 Diurnal Averaged Number Densities of He as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	2.500E07	2.500E07	2.500E07	2.500E07	2.500E07
200	4.413E06	4.872E06	5.484E06	6.319E06	6.982E06
300	2.642E06	2.843E06	3.050E06	3.205E06	3.212E06
400	1.945E06	2.007E06	2.012E06	1.885E06	1.689E06
500	1.499E06	1.477E06	1.390E06	1.154E06	9.272E05
600	1.176E06	1.107E06	9.646E05	7.236E05	5.231E05
700	9.327E05	8.387E05	6.842E05	4.607E05	3.021E05
800	7.461E05	6.422E05	4.916E05	3.004E05	1.783E05
900	6.016E05	4.964E05	3.574E05	1.984E05	1.074E05
1000	4.886E05	3.871E05	2.628E05	1.331E05	6.593E04
1100	3.995E05	3.044E05	1.953E05	9.050E04	4.119E04
1200	3.287E05	2.411E05	1.466E05	6.238E04	2.616E04
1300	2.721E05	1.925E05	1.110E05	4.353E04	1.687E04
1400	2.265E05	1.547E05	8.482E04	3.074E04	1.104E04
1500	1.895E05	1.251E05	6.537E04	2.195E04	7.328E03
1600	1.595E05	1.019E05	5.078E04	1.584E04	4.925E03
1700	1.348E05	8.346E04	3.974E04	1.155E04	3.351E03
1800	1.145E05	6.875E04	3.133E04	8.497E03	2.306E03
1900	9.774E04	5.696E04	2.487E04	6.308E03	1.605E03
2000	8.378E04	4.743E04	1.988E04	4.724E03	1.128E04

Table 2  
 Diurnal Averaged Number Densities of O as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	7.600E10	7.600E10	7.600E10	7.600E10	7.600E10
200	3.600E09	3.457E09	3.209E09	2.795E09	2.416E09
300	8.870E08	7.134E08	5.124E08	2.809E08	1.564E08
400	3.054E08	2.054E08	1.112E08	4.025E07	1.471E07
500	1.168E08	6.616E07	2.788E07	6.771E06	1.675E06
600	4.749E07	2.287E07	7.708E06	1.273E06	2.183E05
700	2.024E07	8.364E06	2.232E06	2.611E05	3.153E04
800	8.983E06	3.207E06	6.918E05	5.747E04	4.946E03
900	4.130E06	1.282E06	2.252E05	1.342E04	8.320E02
1000	1.960E06	5.312E05	7.645E04	3.301E03	1.488E02
1100	9.567E05	2.275E05	2.696E04	8.502E02	2.810E01
1200	4.791E05	1.003E05	9.834E03	2.284E02	5.381E00
1300	2.456E05	4.538E04	3.701E03	6.379E01	1.162E00
1400	1.287E05	2.106E04	1.434E03	1.848E01	2.527E-1
1500	6.878E04	9.997E03	5.706E02	5.541E00	5.729E-2
1600	3.746E04	4.849E03	2.330E02	1.717E00	1.352E-2
1700	2.077E04	2.399E03	9.744E01	5.486E-1	3.312E-3
1800	1.170E04	1.210E03	4.170E01	1.806E-1	8.412E-4
1900	6.700E03	6.216E02	1.824E01	6.079E-2	2.212E-4
2000	3.893E03	3.247E02	8.149E00	2.128E-2	6.010E-5

Table 3  
 Diurnal Averaged Number Densities of O<sub>2</sub> as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	1.200E11	1.200E11	1.200E11	1.200E11	1.200E11
200	9.900E08	7.910E08	5.699E08	3.438E08	2.151E08
300	7.683E07	4.269E07	1.791E07	4.503E06	1.188E06
400	1.020E07	4.069E06	1.048E06	1.191E05	1.427E04
500	1.217E06	4.886E05	7.983E04	4.808E03	2.444E02
600	3.142E05	6.758E04	7.106E03	1.857E02	5.155E00
700	6.428E04	1.033E03	7.062E02	9.135E00	1.265E-1
800	1.364E04	1.714E03	7.688E01	5.002E-1	3.528E-3
900	3.242E03	3.031E02	8.962E00	3.010E-2	1.102E-4
1000	7.981E02	5.682E01	1.122E00	1.975E-3	3.821E-6
1100	2.056E02	1.122E01	1.493E-1	1.403E-4	1.459E-7
1200	5.526E01	2.322E00	2.106E-2	1.074E-5	5.274E-9
1300	1.544E01	5.028E-1	3.139E-3	8.835E-7	2.788E-10
1400	4.474E00	1.136E-1	4.927E-4	7.772E-8	1.382E-11
1500	1.342E00	2.778E-2	8.124E-5	7.292E-9	7.412E-13
1600	4.157E-1	6.520E-3	1.405E-5	7.277E-10	4.288E-14
1700	1.328E-1	1.653E-3	2.541E-6	7.702E-11	2.667E-15
1800	4.370E-2	4.342E-4	4.800E-7	8.627E-12	1.777E-16
1900	1.478E-2	1.177E-4	9.452E-8	1.200E-12	1.267E-17
2000	5.142E-3	2.906E-5	1.937E-8	1.270E-13	9.626E-19

Table 4  
 Diurnal Averaged Number Densities of  $N_2$  as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	5.800E11	5.800E11	5.800E11	5.800E11	5.800E11
200	7.393E09	6.180E09	4.743E09	3.136E09	2.124E09
300	7.630E08	4.639E08	2.210E08	6.739E07	2.113E07
400	1.278E08	5.777E07	2.151E07	2.682E06	4.225E05
500	2.562E07	8.798E06	1.810E06	1.407E05	1.156E04
600	5.730E06	1.521E06	3.239E05	8.800E03	3.844E02
700	1.403E06	2.884E05	2.763E04	6.190E02	1.471E01
800	3.664E05	5.883E04	3.899E03	4.802E01	6.320E-1
900	1.012E05	1.276E04	5.894E02	4.057E00	3.006E-2
1000	2.932E04	2.918E03	9.470E01	3.702E-1	1.570E-3
1100	8.862E03	6.994E02	1.609E01	3.627E-2	8.936E-5
1200	2.783E03	1.725E02	2.878E00	3.798E-3	1.016E-5
1300	9.053E02	4.558E01	5.404E-1	4.237E-4	3.674E-7
1400	3.041E02	1.233E01	1.063E-1	5.017E-5	2.633E-8
1500	1.075E02	3.456E00	2.183E-2	6.287E-6	2.023E-9
1600	3.768E01	1.002E00	4.677E-3	8.321E-7	1.661E-10
1700	1.380E01	3.001E-1	1.042E-3	1.160E-7	1.454E-11
1800	5.211E00	9.268E-2	2.313E-4	1.699E-8	1.353E-12
1900	2.005E00	2.949E-2	5.746E-5	2.612E-9	1.334E-13
2000	7.927E-1	9.654E-3	1.431E-5	4.619E-10	1.393E-14

Table 5  
 Diurnal Averaged Number Densities of H as a  
 Function of Altitude for Five Solar Flux Numbers.

S h(km.)	250	200	150	100	70
120	4.356E04	4.356E04	4.356E04	4.356E04	4.356E04
200	1.071E04	1.224E04	1.447E04	1.790E04	2.104E04
300	8.035E03	9.323E03	1.114E04	1.380E04	1.611E04
400	7.205E03	8.328E03	9.837E03	1.189E04	1.352E04
500	6.690E03	7.660E03	8.898E03	1.046E04	1.157E04
600	6.272E03	7.102E03	8.107E03	9.263E03	9.974E03
700	5.904E03	6.609E03	7.415E03	8.214E03	8.638E03
800	5.573E03	6.168E03	6.803E03	7.360E03	7.518E03
900	5.272E03	5.769E03	6.260E03	6.597E03	6.571E03
1000	4.996E03	5.408E03	5.774E03	5.933E03	5.768E03
1100	4.742E03	5.079E03	5.339E03	5.352E03	5.083E03
1200	4.502E03	4.778E03	4.947E03	4.843E03	4.495E03
1300	4.291E03	4.503E03	4.594E03	4.395E03	3.989E03
1400	4.090E03	4.250E03	4.275E03	3.998E03	3.552E03
1500	3.903E03	4.018E03	3.986E03	3.647E03	3.173E03
1600	3.730E03	3.804E03	3.723E03	3.335E03	2.843E03
1700	3.568E03	3.606E03	3.484E03	3.057E03	2.555E03
1800	3.417E03	3.424E03	3.266E03	2.809E03	2.303E03
1900	3.276E03	3.255E03	3.066E03	2.587E03	2.081E03
2000	3.144E03	3.098E03	2.884E03	2.387E03	1.886E03

## II. B-L SEARCH

### A. Introduction

This program produces contours of constant B and L as a function of longitude, latitude and altitude in both the northern and southern hemispheres. The desired initial values of B and L are read into the program along with an approximate corresponding latitude,  $\lambda$ , which can easily be obtained by the use of Figure 2. The dipole equation  $r_0 = L_0 \cos^2 \lambda$  relating the initial L and the geocentric distance  $r_0$  is used with the radius of the earth,  $r_e$ , and the equation  $h_1 = r_e (r_0 - 1)$  to provide an approximation of the altitude. This is fed, together with a longitude of 180 degrees and latitude  $\lambda$ , into subroutine INVAR which calculates B and L for a given longitude, latitude and altitude. This subroutine makes use of the transformation developed by McIlwain<sup>(3)</sup> using the 48 spherical harmonic coefficients of Jenson and Cain<sup>(4)</sup>. INVAR numerically integrates the longitudinal invariant I using a series expansion for the magnetic field. Then L is calculated as a function of both B and I by using a dipole representation of the earth. The B and L obtained in this manner are returned to the main program. Here the accuracy of the initial approximation is checked. If the computed L is found to be within an accuracy of  $10^{-4}$  of the initial L the program will enter into a search routine with linear interpolation in latitude and altitude in order to arrive at a correct B. The search parameters  $\Delta h$  (increment in altitude) and  $\Delta \lambda$  (increment in latitude) are prefixed and must remain small in order that interpolation may hold. Once B is found, it is checked, together with the value of L, to insure an accuracy of  $10^{-3}$  in comparison with the initial values. If the accuracy is sufficient the subroutine RING will be called for the northern hemisphere. This subroutine takes a given latitude and altitude and computes the B and L contour map for longitudes of 10 degree increment for the full 360 degrees. The program then computes the contour map for the southern hemisphere at the same B and L, increments B by .01 gauss and returns to the northern hemisphere. It will continue in this manner until the altitude drops below 100 kilometers, at which point the next initial B, L and  $\lambda$  will be read until input data is exhausted. The entire process prepares input for the longitudinal averaging processor.

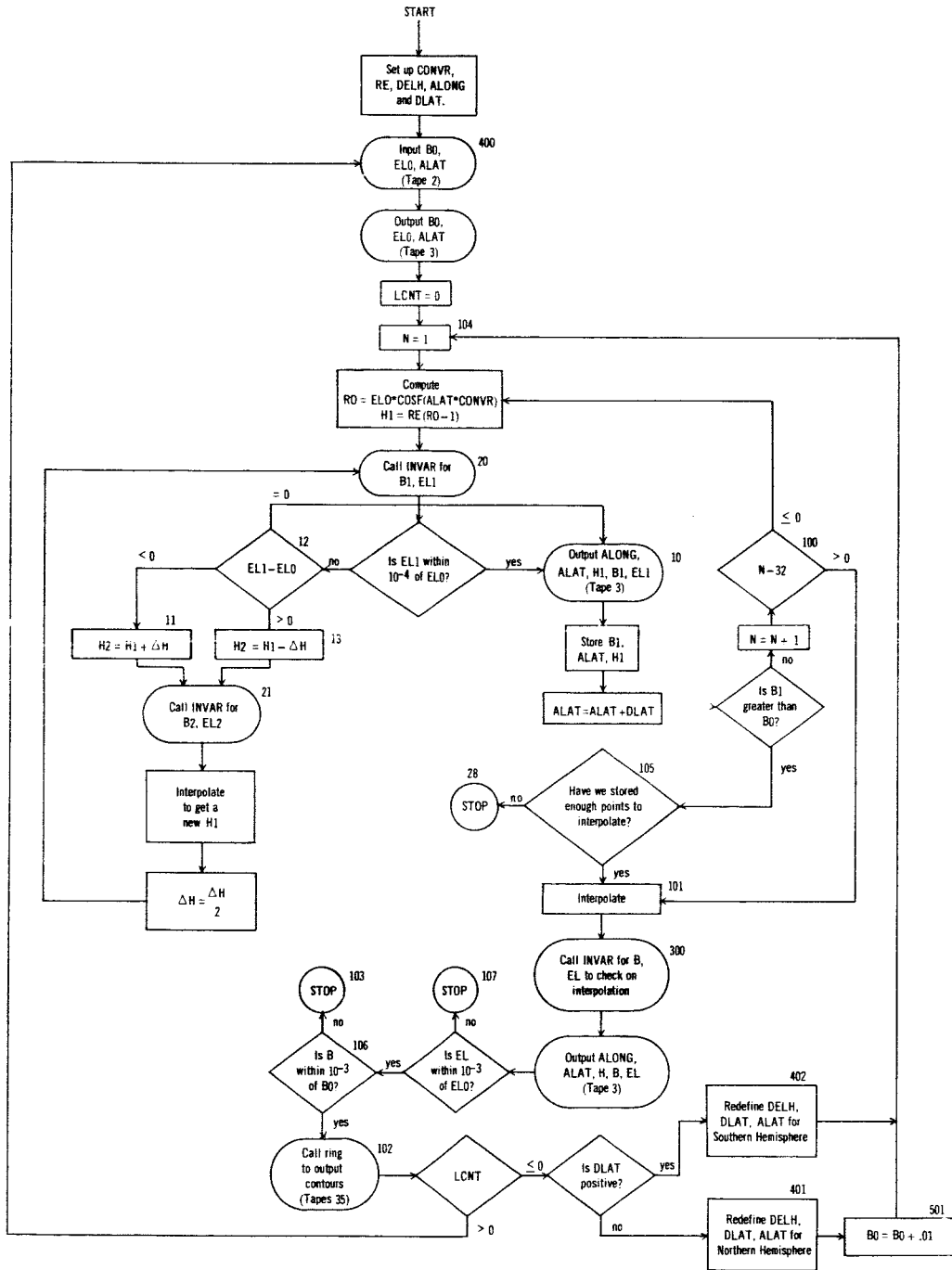


B. Mnemonics

Quantity	Description	Units
CONVR	conversion factor – degrees to radians	--
RE	radius of the earth	km.
DELH	delta altitude	km.
ALONG	geocentric longitude	degrees
DLAT	delta latitude	"
ALAT	geocentric latitude	"
B	magnetic induction	gauss
EL	magnetic field line	earth radii
R	geocentric distance	"
H	altitude	km.
SAVB	temporary storage of B	gauss
SAVH	temporary storage of H	km.
SAVLAT	temporary storage of ALAT	degrees
LCNT	an indicator used to indicate when the altitude has dropped below 100 km.	--

## C. Flow Charts

### 1. Main Program





D. Fortran Listing

```

C      B-L SEARCH
      DIMENSION SAVB(32),SAVLAT(32),SAVH(32)
      1  FORMAT(2F12.5,F8.5)
      2  FORMAT(5F12.5)
      3  FORMAT (5X,42H INTERMEDIATE RESULTS--NORTHERN HEMISPHERE)
      4  FORMAT (8X,4HLONG,8X,3HLAT,9X,3HALT,10X,1HB,11X,1HL)
      5  FORMAT (4H180-1F8.5,4X,4H L0=1F8.5,4X,13H INITIAL LAT=1F8.5)
      6  FORMAT (1H1,5X,42H INTERMEDIATE RESULTS--SOUTHERN HEMISPHERE)
      7  FORMAT (1H1,5X,42H INTERMEDIATE RESULTS--NORTHERN HEMISPHERE)
      8  FORMAT (36HO)VALUE OF B IS NOT WITHIN .CO1 OF RO)
      9  FORMAT (60HO)INTERPOLATION CANNOT PROCEED--MAKE INITIAL LATITUDE SM
      10  FORMAT (37HO)VALUE OF L IS NOT WITHIN .CO1 OF ELO)
      400 READ INPUT TAPE 2,1,80,ELO,ALAT
      WRITE OUTPUT TAPE 3,5,80,ELO,ALAT
      WRITE OUTPUT TAPE 3,3
      WRITE OUTPUT TAPE 3,4
      CONVR=.01745333
      RE=6378.2
      DELH=100.
      ALONG=186.
      CLAT=2.
      ALAT0=ALAT
      LCNT=C
      104 DO 100 N=1,32
      80=ELO*COSE(ALAT*CONVR)**2
      H1=RE*(RO-1.)
      20 CALL INVAR(ALAT,ALONG,H1,.01,01,ELL1)
      CKEL=ELL1-EL0
      IF(ABS(CKEL)-1.E-4)14,14,12
      12 IF(CKEL) 11,14,13
      13 H2=H1-DELH
      21 CALL INVAR(ALAT,ALONG,H2,.01,02,ELL2)
      H1=H1-(ELL1-ELL0)*(H1-H2)/(ELL1-ELL2)
      DELH=DELH/2.
      GO TO 20
      11 H2=H1+DELH
      GO TO 21
      14 WRITE OUTPUT TAPE 3,2,ALONG,ALAT,H1,B1,ELL1
      SAVB(N)=B1
      SAVLAT(N)=ALAT
      SAVH(N)=H1
      ALAT=ALAT+ULAT
      IF(RI-60) 100,100,105
      100 CONTINUE
      105 IF (N-1) 28,28,101
      28 WRITE OUTPUT TAPE 3,9
      CALL EXIT
      101 DO 200 I=1,32
      IF(SAVB(I)-B0) 200,30,31
      31 AL2=SAVLAT(I)
      B2=SAVB(I)
      H2=SAVH(I)
      AL1=SAVLAT(I-1)
      B1=SAVB(I-1)

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```

HI=SAVH(I-1)
ALAT=AL2-(AL2-AL1)*(B2-B0)/(B2-B1)
H=H1-(C0-B1)*(H1-F2)/(B2-B1)
GO TO 300
30 B=SAVH(I)
ALAT=SAVLAT(I)
H=SAVH(I)
GO TO 300
2A0 CONTINUE
300 CALL INVAR(ALAT,ALONG,H,.01,B,EL)
WRITE OUTPUT TAPE 3,2,ALONG,ALAT,H,B,EL
CKL=EL-EL0
IF (ABS(FCKL)-1.E-3) 106,106,107
107 WRITE OUTPUT TAPE 3,10
CALL EXIT
106 CRD=B-B0
IF (ABS(FCKB)-1.E-3) 107,102,103
103 WRITE OUTPUT TAPE 3,8
CALL EXIT
102 CALL RING(ALAT,H,LCNT)
IF (LCNT) 403,403,400
403 IF (PLAT) 401,401,402
402 DELH=100.
PLAT=-2.
IF (ALATC-11.) 500,501,501
500 ALAT=-1.
GO TO 502
501 ALAT=-ALATC+11.
502 WRITE OUTPUT TAPE 3,6
WRITE OUTPUT TAPE 3,4
GO TO 104
401 PLAT=2.
DELH=100.
ALAT=ALATC+1.
ALAT0=ALAT
BC=80+.C1
WRITE OUTPUT TAPE 3,7
WRITE OUTPUT TAPE 3,4
GO TO 104
END(1,1,0,0,0,0,0,0,0,0,0,0,0,0)

```

STORAGE NOT USED BY PROGRAM

DEC	UCT	DEC	UCT
624	01160	32561	77461

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	UCT	DEC	UCT
623	01157	559	01057
SAVB	SAVB	SAVLAT	591 01117

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	UCT	DEC	UCT	DEC	UCT
527	01017	526	01016	525	01015
AL1	AL2	AL3	AL4	AL5	AL6
522	01012	521	01011	520	01010
CKL	CKL	CKL	CKL	CKL	CKL
517	01005	516	01004	515	01003
LL1	LL1	LL1	LL1	LL1	LL1
512	01000	511	00777	510	00776
H2	H	H	H	H	H
507	00773	506	00772	505	00771
RO	RE	RE	RE	RE	RE
502	00766	501	00765	500	00764

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN	LCC	LUC	EFN	LCC	EFN	LCC	
1	00757	2	00754	3	00752	4	00741
6	00720	7	00706	8	00674	9	00665

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	UCT	DEC	UCT
496	00760	399	00617
C)60	C)61	C)62	C)63
459	00763	500	00764
185	00275	14	00016
188	00274	202	00312
330	00512	345	00531

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	UCT	DEC	UCT
5	00005	7	00007
0	00000	2	00002

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

DEC	UCT	DEC	UCT
403	00523	402	00522
84	00525	85	00533
94	00566	95	00567

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	LCC	EFN	LCC	EFN	LCC
13	00023	26	00111	20	00134
35	00167	40	00222	42	00227
51	00302	53	00315	55	00325
59	00413	75	00457	77	00471
84	00525	85	00533	86	00543
94	00566	95	00567	96	00577



```

12 IF(AUSF(RLN)-ERRL) 50,50,30
30 PHI=PHIN
   L=BN
   ALT=ALTN
   LL=ELN
   RR=REN
   RL=RLN
40 CONTINUE
   WRITE OUTPUT TAPE 3,102
   PRLNG=PRLNG+10.
   IF(PRLNG-180.5) 5,3,3
50 PHI=PHIN
   B=BN
   ALT=ALTN
   LL=ELN
   WRITE OUTPUT TAPE 3,103,PRLNG,PHI,ALT,B,LL
   WRITE OUTPUT TAPE 5,103,PRLNG,PHI,ALT,B,LL
   IF(ALT-100.) 70,70,71
71 PRLNG=PRLNG+10.
   IF(PRLNG-170.5) 9,3,3
3 RETURN
70 LCNT=LCNT+1
   RETURN
LAD(1,1,0,0,0,0,0,0,1,0,0,0,0,0,0,0)

```









```

SUBROUTINE LINES (R1,R2,R3,B,ARC,ERR,J,VP,VN)
DIMENSION B(200),ARC(200),R1(3),R2(3),R3(3),VN(3),VP(3),RA(3)
CRE=0.25
IF(ERR=0.15625)74,75,75
74 CRE=(CRK*0.333333333)
75 A3=ARC(3)
AAB=ARF(A3)
SNA=A3/AAB
A1=ARC(1)
A2=ARC(2)
AG6=A3*A3/6.0
J=3
ILP=1
IS=1
GO TO 87
66 IS=1
J=J+1
AUG=A3*A3/6.0
ARCJ=A1+A2+A3
AD=(ASUM+A1)/AA
BD=ASUM/BB
CU=A1/CC
36 DO 5 I=1,3
DD=R1(I)/AA-R2(I)/BB+R3(I)/CC
GO TO 16,87,IS
6 RT=R1(I)-(AD*R1(I)-BD*R2(I)+CD*R3(I))-DD*ARCJ)*ARCJ
RA(I)=R1(I)
R1(I)=R2(I)
R2(I)=R3(I)
R3(I)=RT
VP(I)=VN(I)
8 RGAR=(R2(I)+R3(I))/2.-DD*AD6
5 VN(I)=VP(I)+A3*GBAR
87 IF(VN(2))76,77,77
76 VN(2)=-VN(2)
77 IF(VN(2))-3.14159265378,78,79
79 VN(2)=0.283185307-VN(2)
GO TO 77
78 IF(VN(3))80,81,81
80 VN(3)=VN(3)+6.283185307
GO TO 78
81 IF(VN(3))-6.283185307182,82,83
83 VN(3)=VN(3)-6.283185307
GO TO 81
82 GO TO (9,10),IS
9 SIT=ARF(SINF(VN(2)))
PRE1=VN(1)
PRE2=PRE1*VN(2)
PRE3=PRE1*SIT*VN(3)
SSQ=SIT*SIT
DER=(6356.912*SSQ*(21.3677+.108*SSQ))/6371.2
AER=VN(1)-DER
CALL MAGNET(AER,SIT,VN(3),BR,BT,BP,B(J),VN(2))
R3(I)=BR/B(J)
DN=B(J)*VN(1)

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LINES000
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LINES053

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R3(2)=BT/DN
R3(3)=BP/(UN*SIT)
ASUM=A2*A2
AA=ASUM*A2
RR=A3*A2
CC=ASUM*A3
IS=2
GO TO 36
10 SIT=ABSF(SINF(VN(2)))
R(J)=B(J)*((PREL/VN(1))**3)
59 CRT=.5*ABSF(R3(1))/(.1*ABSF(R3(2))*VN(1)))
X=(ABSF(VR(1)-PRE1)*CRT*ABSF(VN(1))*VN(2)-PRE2)+ABSF(VN(1))*SIT*VN(3)
1)-PRE3)/(AAE*ERR*SQRT(.1+CRT*CRT))
GC TO (90,93,90),ILP
73 IF(X-2.3)90,89,89
89 A3=A3*.2*(8.C+X)/(0.8+X)
J=J-1
ILP=3
ASUM=A2*A1
AA=ASUM*A1
RR=A2*A1
CC=ASUM*A2
DE 91 1=1,3
VN(1)=VP(1)
R3(1)=R2(1)
R2(1)=R1(1)
91 R1(1)=RA(1)
GO TO 73
90 IF(J-200)67,60,60
67 A1=A2
49 IF(B(J)-b(2))49,45,60
A2=A3
A3=A3*.2*(8.C+X)/(.8+X)
AM=(2.-R3(2))*VN(1))*VN(1)*CRE
IF(ABS(A3)-AM)84,84,72
72 A3=SNA*AM
84 IF(SNA*R3(1)+.5)85,85,73
85 AM=-.5*SNA*VN(1)/R3(1)
IF(ABS(A3)-AM)73,73,86
86 A3=SNA*AM
73 ARC(J+1)=A3
AA8=ABSF(A3)
GO TO 66
60 RETURN
END(1,1,0,0,0,0,1,0,0,0,0,0,0,0,0)

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LINE5054
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LINE5099

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STORAGE NOT USED BY PROGRAM

DEC OCT  
650 01212  
32561 77461

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC LCI DEC OCT DEC OCT DEC OCT  
RA 649 01211

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
AI	646 01206	A2	645 01205	A3	644 01204	AAH	643 01203
AD	641 01201	AER	640 01200	AM	639 01177	AC6	638 01176
ASUM	636 01174	BB	635 01173	PD	634 01172	RP	633 01171
BT	631 01167	CC	630 01166	CC	629 01165	CRE	628 01164
EN	624 01162	ILP	625 01161	IS	624 01160	DER	623 01157
PRE2	621 01159	PRE3	620 01154	GRT	619 01153	RBAR	618 01152
SIT	614 01150	SNA	615 01147	SSC	614 01146	X	613 01145

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
I)	604 01134	2)	572 01074	3)	576 01100	6)	594 01122
C1G2	610 01142	C1G3	611 01143	C1G4	612 01144	E11	155 02233
E1E	292 00444	E1K	444 00674	E1G	493 00755	E1P	498 00762

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
EXP(3	0 00000	MAGNET	2 00002	SIN	1 00001	SORT	3 00003

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

EXP(3	MAGNET	SIN	SORT
-------	--------	-----	------

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS											
EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
74	6	00234	75	7	00240	66	17	00274	36	24	00327
8	31	00403	5	34	00414	87	35	00422	76	36	00426
79	38	00435	78	40	00441	80	41	00445	81	43	00451
82	46	00462	9	47	00464	10	66	00574	59	68	00614
89	72	00702	91	83	00750	90	85	00756	67	86	00764
72	93	01033	84	94	01036	85	95	01043	86	97	01057
60	101	01070							6	27	00346
									77	37	00430
									83	44	00456
									93	71	00675
									49	88	00772
									73	98	01062

```

SUBROUTINE START (R1,R2,R3,B,ARC,ERR,V)
DIMENSION b(200),ARC(200),V(3,3),R1(3),R2(3),R3(3)
SIT=ARCSF(SINF(V(2,2)))
AER=V(1,2)
SSQ=SIT*SIT
DER=(6.356*912+SSQ*(21.3677+.108*SSQ))/6371.2
V(1,2)=AER+DER
10 IF(V(3,2))11,12,12
11 V(3,2)=V(3,2)+6.2e3185307
GO TO 10
12 CALL MAGNET(AEP,SIT,V(3,2),BR,BT,BP,B(2),V(2,2))
R2(1)=BR/B(2)
DN=B(2)*V(1,2)
R2(2)=BT/DN
R2(3)=BP/(DN*SIT)
IS=0
1 DO 2 I=1,3
2 V(I,1)=V(I,2)-ARC(2)*R2(I)
SIT=ARCSF(SINF(V(2,1)))
3 SSQ=SIT*SIT
DER=(6.356*912+SSQ*(21.3677+.108*SSQ))/6371.2
AER=V(1,1)-DER
CALL MAGNET(AEK,SIT,V(3,1),BR,BT,BP,B(1),V(2,1))
IF(B(1)-B(2))4,5,5
4 ARC(2)=-ARC(2)
GO TO 1
5 R1(1)=BR/B(1)
ARC(3)=ARC(2)
DN=B(1)*V(1,1)
R1(2)=BT/DN
R1(3)=BP/(DN*SIT)
DO 6 I=1,3
6 V(I,1)=V(I,2)-ARC(2)*(R1(I)+R2(I))/2.
SIT=ARCSF(SINF(V(2,1)))
IS=IS+1
GO TO (3,7),IS
7 DO 8 I=1,3
8 V(I,3)=V(I,2)+ARC(3)*((1.5)*R2(I)-.5*R1(I))
RETURN
END(1,1,0,C,0,0,0,0,0,0,0,0,0)

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STARTC00
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STORAGE NOT USED BY PROGRAM

DEC	UCT	DEC	UCT
293	00445	325E1	77461

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	UCT	DEC	UCT	DEC	UCT
AER	297	00444	BP	291	00443
IS	287	00437	UER	286	00436
			RR	290	00442
			SIT	283	00435
			SSO	284	00434
			DN	288	00440

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	UCT	DEC	UCT	DEC	UCT
11	280	00430	2)	257	00401
CIG2	283	00433	F38	193	00301
			3)	259	00403
			6)	267	00413
			9)	273	00421

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	UCT	DEC	UCT	DEC	UCT
MAGNET	1	00001	SIN	0	00000

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

MAGNET	SIN
--------	-----

INTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC
10	9	00164	11	10	00167	12	12	00173
3	27	00245	4	28	00302	5	30	00305
8	41	00357				6	36	00330
						1	19	00227
						6	36	00330
						7	40	00355
						2	20	00231
						7	40	00355



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MAGNT054

SUBROUTINE MAGNET (R,S,PHI,PR,BTHET,APHI,OB,THET)  
DIMENSION DP(49),P(49),G(49),H(49),CCNST(49),ACR(7),SP(7),GP(7)  
IF(RIP)151,150,150

150 KIP=-1

DL 152 N=1,49

G(N)=C.C

H(N)=G.O

JENSEN AND GAIN COEFFICIENTS FOR 1560 (JUNE 1962)

G(I) = G(I,N) AND H(I) = H(I,N) WHERE I = N+7\*(M-1)

G( 2) = 3.0411209CL-01

G( 3) = 2.1473858E-02

G( 4) = 2.40253671E-02

G(10) = -5.1253379E-02

G(17) = -1.3811969E-02

G( 4) = -3.15178631E-02

G(11) = 6.2130066E-02

G(18) = -2.4898133E-02

G(25) = -6.49565905E-03

G( 5) = -4.17943639E-02

G(12) = -4.52283660E-02

G(19) = -2.17947447E-02

G(26) = 7.00825465E-03

G(33) = -2.04395562E-03

G( 6) = 1.62556271E-02

G(13) = -3.44067606E-02

G(20) = -1.9447026E-02

G(27) = -6.08211374E-04

G(34) = 2.77833549E-03

G( 7) = -1.95231736E-02

G(14) = -4.85326147E-03

G(21) = 3.21172429E-03

G(28) = 2.14128228E-02

G(35) = 1.05051275E-03

G(42) = 2.26829448E-04

G(49) = 1.11471358E-03

H( 9) = -5.79890501E-02

H(10) = 3.31246714E-02

H(17) = -1.57893822E-03

H(11) = 1.48656943E-02

H(18) = -4.0748158E-03

H(25) = 2.10318235E-04

H(12) = -1.18245466E-02

H(19) = 1.0097732E-02

H(26) = 4.30380863E-04

H(33) = 1.38503490E-03

H(13) = -7.95897466E-04

H(20) = -2.0044021E-03

H(27) = 4.5971859E-03

H(34) = 2.42063078E-03

H(41) = -1.21806522E-03

H(14) = -5.75830293E-03

H(21) = -8.75461401E-03

H(28) = -3.46664073E-03

H(35) = -1.18162456E-04

```

H(42)=-1.1423013E-03
H(49)=-3.24831891E-04
P(1)=1.0
DP(1)=0.0
SP(1)=0.0
CP(1)=1.0
CONST(9)=0.0
CONST(16)=0.0
DO 80 N=3,7
FN=N
DU 80 M=1,N
FM=M
I=N+7*(M-1)
80 CONST(I)=-((FN-2.0)**2-(FM-1.0)**2)/((FN+FN-3.0)*(FN+FN-5.0))
151 C=SQRT(ABSF(1.0-S*S))
IF(THET-1.570796327) 154,154,156
156 C=-C
154 AR=1./(1.+K)
155 SP(2)=SINF(PHI)
CP(2)=COSF(PHI)
AGR(1)=AK*AR
ADR(2)=AK*ADR(1)
DO 90 M=3,7
N=M-1
SP(M)=SP(2)*CP(N)+CP(2)*SP(N)
CP(M)=CP(2)*CP(N)-SP(2)*SP(N)
90 AGR(M)=AR*ADR(N)
BK=0.0
BTHT=0.0
BPHI=0.0
DO 32 N=2,7
FN=N
SUMR=0.0
SUMP=0.0
DO 33 M=1,N
IF(M-M)87,88,87
88 I=8*N-7
L=I-8
P(I)=S*P(L)
DP(I)=S*DP(L)+C*P(L)
GO TO 89
87 I=N+7*(M-1)
J=I-1
K=I-2
P(I)=C*P(J)-CONST(I)*P(K)
DP(I)=C*DP(J)-S*P(J)-CONST(I)*DP(K)
89 FM=M-1
IS=GI)*CP(M)+H(I)*SP(M)
SUMR=SUMR+P(I)*YS
SUMP=SUMP+DP(I)*TS
33 SUMP=SUMP+FM*P(I)*(-G(I)*SP(M)+H(I)*CP(M))
BR=BR+ADR(N)*FN*SUMP
BTHT=BTHT+ADR(N)*SUMT
32 BPHI=BPHI/S

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MAGNT055
MAGNT056
MAGNT057
MAGNT058
MAGNT059
MAGNT060
MAGNT061
MAGNT062
MAGNT063
MAGNT064
MAGNT065
MAGNT066
MAGNT067
MAGNT068
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MAGNT070
MAGNT071
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MAGNT073
MAGNT074
MAGNT075
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MAGNT077
MAGNT078
MAGNT079
MAGNT080
MAGNT081
MAGNT082
MAGNT083
MAGNT084
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MAGNT089
MAGNT090
MAGNT091
MAGNT092
MAGNT093
MAGNT094
MAGNT095
MAGNT096
MAGNT097
MAGNT098
MAGNT099
MAGNT100
MAGNT101
MAGNT102
MAGNT103
MAGNT104
MAGNT105
MAGNT106
MAGNT107
MAGNT108
MAGNT109
MAGNT110

```

```
BB=SQRT(BR**2+RTHEI**2+BPFI**2)
KLTURN
END(1,1,0,0,0,0,1,0,0,0,0,0,0)
```

```
MAGNT111
MAGNT112
```

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
830 01476		32561 77461	

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS									
ADR	DEC	OCT	DEC	OCT					
H	584 01110	CONST	633 01171	CP	570 01072	DP	829 01475	G	731 01333
	682 01252	P	780 01414	SP	577 01101				

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

AR	DEC	OCT	DEC	OCT					
J	563 01063	C	562 01062	FM	561 01061	FN	560 01060	I	559 01057
N	558 01056	KIP	557 01055	K	556 01054	L	555 01053	M	554 01052
	553 01051	SUMP	552 01050	SUMP	551 01047	SUMT	550 01046	TS	549 01045

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

1)	DEC	OCT	DEC	OCT					
C162	537 01031	2)	472 00730	3)	477 00735	6)	531 01023	C160	542 01036
C1201	548 01044	C163	544 01040	D1404	173 00255	C1408	230 00346	C166	547 01043

LOCATIONS OF NAMES IN TRANSFER VECTOR

COS	DEC	OCT	DEC	OCT	
	2 00002	SIN	1 00001	SQRT	0 00000

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

CCS	SIN	SQRT			
EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS					
EFN	IFN	LOC	EFN	IFN	LOC
150	5 00064	152	8 00071	68	00307
154	72 00367	155	73 00375	80	81 00443
89	102 00607	33	106 00635	32	109 00672
				151	69 00347
				88	92 00512
				156	71 00365
				87	97 00541

```

INTEG001
INTEG002
INTEG003
INTEG004
INTEG005
INTEG006
INTEG007
INTEG008
INTEG009
INTEG010
INTEG011
INTEG012
INTEG013
INTEG014
INTEG015
INTEG016
INTEG017
INTEG018
INTEG019
INTEG020
INTEG021
INTEG022
INTEG023
INTEG024
INTEG025
INTEG026
INTEG027
INTEG028
INTEG029
INTEG030
INTEG031
INTEG032
INTEG033
INTEG034
INTEG035
INTEG036
INTEG037
INTEG038

SUBROUTINE INTEG (ARC,BEG,BEND,B,JEP,ECC,FI)
DIMENSION ARC(200),BEG(200),BEND(200),B(200),ECC(200)
4 KK=JEP
6 IF(KK-4)14,11,20
11 KK=KK-1
14 A=B(KK-1)/B(2)
X2=B(KK)/B(2)
X3=B(KK+1)/B(2)
ASUM=ARC(KK)+ARC(KK+1)
DN=ARC(KK)*ARC(KK+1)*ASUM
BB=(-A*ARC(KK+1)*(ARC(KK)+ASUM)+X2*ASUM**2-X3*ARC(KK)*2)/DN
C=(A*ARC(KK+1)-X2*ASUM+X3*ARC(KK))/DN
FI=1.570796326*(1.-A+BB*BB/(4.*C))/SQRTF(ABSF(C))
RETURN
20 T=SQRTF(1.-BEND(2)/B(2))
FI=(2.*T-LOGF((1.+T)/(1.-T)))/ECC(2)
IF(B(2)-BEND(KK))21,21,25
25 KK=KK+1
21 T=SQRTF(ABSF(1.-BEG(KK)/B(2)))
FI=FI-(2.*T-LOGF((1.+T)/(1.-T)))/ECC(KK)
KK=KK-1
22 DO 5 I=3,KK
ARGI=1.-BEND(I)/B(2)
IF(ARGI)26,26,27
26 TE=1.E-5
GO TO 28
27 TE=SQRTF(ARGI)
28 ARG1=1.-BEG(I)/B(2)
IF(ARG1)29,29,31
31 TB=SQRTF(ARG1)
GO TO 32
29 TB=1.E-5
32 IF(ABSF(ECC(I))-2.E-5) 23,23,24
23 FI=FI+((TE+TB)*(ARC(I)+ARC(I+1)))/4.
GO TO 5
24 FI=FI+(2.*(TE-TB)-LOGF((1.+TE)*(1.-TB))/((1.-TE)*(1.+TB))))/ECC(I)
5 CONTINUE
30 RETURN
END(1,1,0,0,0,0,1,0,0,0,0,0,0,0,0,0)

```

STORAGE ACT USED BY PROGRAM

DFC	LCT	DEC	OCT						
371	00263	32561	77461						

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

ANG1	DN	X2	DEC	OCT	ASUM	DEC	OCT	HH	DEC	OCT	C	
			370	00562	A	369	00561	368	00560	367	00557	366
			365	00555	KK	364	00554	363	00553	362	00552	361
			360	00550	X3	359	00547	358	00546	357	00545	356

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

1)	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
C160	350	00536	329	00511	31	323	00515	309
	358	00546	32	00134	E15	202	00312	305

LOCATIONS OF NAMES IN TRANSFER VECTOR

LOG	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
	1	00001	0	00000				

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

LCC SORT

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC
4	4	00117	6	5	00122	11	6	00127
25	20	00305	21	21	00313	22	24	00355
28	30	00401	31	32	00414	29	34	00421
24	30	00445	5	39	00503	30	40	00505
						14	7	00135
						26	27	00371
						32	35	00423
						20	27	00246
						27	29	00374
						23	36	00430

```

C
SUBROUTINE CARMEL (R,XI,VL)
COMPUTE L
XX=LO, F((XI**3)*R)/0.311653)
IF((XX+2.11)*8
8 IF((XX+3.1)*2.49
9 IF((XX-3.1)*3.10
10 IF((XX-12.1)*4.11
11 IF((XX-23.1)*5.16
1 GO=.332338*XX+.30062102
66 TO /
2 GO=((((( (-4.1537735E-14*XX+8.3232531E-15)*XX+1.0066362E-9)*XX+
18.1045063E-3)*XX+3.2916354E-6)*XX+8.2711056E-2)*XX+1.3714067E-3)*
2XX+.015017245)*XX+.43432642)*XX+.62337651
66 TO /
3 GO=((((( (2.6047023E-10*XX+2.3025767E-9)*XX-2.1997963E-8)*XX-
15.397764E-7)*XX-3.3498822E-6)*XX+3.6379917E-2)*XX+1.1784734E-3)*
2XX+1.4452441E-2)*XX+.43352788)*XX+.6228644
66 TO /
4 GO=((((( (6.3271665E-10*XX-3.958566E-8)*XX+3.5766148E-07)*XX-
11.2531732E-5)*XX+7.9451313E-5)*XX-3.2077022E-4)*XX+2.1680398E-3)*
2XX+1.2e17956E-2)*XX+.43510525)*XX+.6222359
66 TO /
5 GO=((((( (2.3212095E-8*XX-3.8049276E-6)*XX+.2.170224E-4)*XX-.7310339CARMLO22
1E-3)*XX+.12036224)*XX-.18461796)*XX+2.000187
66 TO /
6 GO=XX-3.0460681
7 VL=((01.04+EXP F(GO))*C.311653)/R)**(1./3.)
END COMPUTE L
RETURN
END(1,1,0,0,0,0,1,0,0,0,0,0,0,0)
CARMLO0
CARMLO1
CARMLO2
CARMLO3
CARMLO4
CARMLO5
CARMLO6
CARMLO7
CARMLO8
CARMLO9
CARMLO10
CARMLO11
CARMLO12
CARMLO13
CARMLO14
CARMLO15
CARMLO16
CARMLO17
CARMLO18
CARMLO19
CARMLO20
CARMLO21
CARMLO22
CARMLO23
CARMLO24
CARMLO25
CARMLO26
CARMLO27
CARMLO28

```





## E. Restrictions

ALAT must be remotely close to the correct latitude corresponding to the initial B in order to save machine time and to insure the accuracy of the answers. ALAT must always be positive and greater than the geomagnetic equator at geocentric longitude of  $180^\circ$ . This means that ALAT must be greater than  $4^\circ$ .

## F. Input

Cards containing the initial values of B, L and  $\lambda$  are all the data necessary for the execution of this program. This data is entered on logical tape number two. Each card represents a single case.

### 1. Card Description

Columns	Mode	Quantity	Units	Description
1-12	F	BO	gauss	initial magnetic induction
13-24	F	ELO	earth radii	initial magnetic field line
25-32	F	ALAT	degrees	initial latitude

2. Sample

GENERAL PURPOSE DATA SHEET

Problem		Date		Page	
INPUT B-L SEARCH (INITIAL B, L, λ)				of	
Sponsor		Date		Page	
TAPE 2		SAMPLE		of	
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
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99					
100					

## G. Output

Output from this program appears on logical tapes 3 and 5. Both tapes contain the same information with the exception that tape 3 also contains the intermediate results of the search routine. Tape 5 is the output to be used in the longitudinal averaging processor. This tape is punched onto cards which can be combined with similar output from other runs. All this data can then be used as input to the longitudinal averaging processor, but it is important that a blank card follow the last of the data cards. This arrangement is discussed in the next section.

1. Tape 3 Sample

B0= 0.11000      L0= 1.75000      INITIAL LAT=26.00000

INTERMEDIATE RESULTS--NORTHERN HEMISPHERE

LCNG	LAT	ALT	B	L
180.00000	26.00000	3533.22839	0.10159	1.75000
180.00000	28.00000	3257.93344	0.11298	1.75000
180.00000	27.47628	3330.02185	0.10985	1.74955

B= 0.10985

L= 1.74955

FINAL RESULTS

-180.00	27.48	3330.02	0.10985	1.74955
-180.00	27.48	3330.02	0.10985	1.74955
-170.00	25.79	3309.07	0.10987	1.75027
-160.00	23.86	3298.23	0.10987	1.75043
-150.00	21.82	3293.89	0.10987	1.75049
-140.00	19.74	3290.96	0.10986	1.74966
-130.00	17.71	3287.41	0.10986	1.74966
-120.00	15.73	3279.11	0.10986	1.74966
-110.00	13.83	3263.27	0.10987	1.75054
-100.00	11.97	3234.47	0.10987	1.75049
-90.00	10.27	3190.87	0.10987	1.75052
-80.00	8.93	3132.92	0.10986	1.75014
-70.00	8.27	3067.73	0.10986	1.74978
-60.00	8.66	3009.01	0.10985	1.74947
-50.00	10.36	2972.82	0.10985	1.74926
-40.00	13.12	2964.85	0.10985	1.74926
-30.00	16.35	2979.89	0.10985	1.74933
-20.00	19.48	3011.16	0.10985	1.74939
-10.00	22.19	3052.95	0.10985	1.74927
-0.	24.34	3101.34	0.10985	1.74913
10.00	25.90	3153.89	0.10985	1.74914
20.00	26.92	3210.03	0.10985	1.74922
30.00	27.49	3269.30	0.10985	1.74940
40.00	27.80	3331.19	0.10986	1.74874
50.00	28.10	3397.64	0.10987	1.74857
60.00	28.53	3466.52	0.10985	1.74941
70.00	29.03	3528.77	0.10985	1.74939
80.00	29.55	3579.90	0.10985	1.74936
90.00	29.99	3614.76	0.10985	1.74941
100.00	30.27	3629.99	0.10985	1.74857
110.00	30.48	3626.67	0.10985	1.74880
120.00	30.63	3605.07	0.10986	1.74932
130.00	30.67	3566.43	0.10987	1.74938
140.00	30.64	3517.70	0.10987	1.74968
150.00	30.42	3464.00	0.10988	1.75053
160.00	29.83	3410.37	0.10986	1.74985
170.00	28.87	3364.67	0.10986	1.75002

2. Tape 5

INTERMEDIATE RESULTS--SOUTHERN HEMISPHERE

LONG	LAT	ALT	B	L
180.00000	-15.00000	3695.08514	0.10030	1.74998
180.00000	-17.00000	3433.09256	0.11171	1.74995
180.00000	-16.70013	3472.37378	0.10990	1.74989
B= 0.10990	L= 1.74989			

FINAL RESULTS

-180.00	-16.70	3472.37	0.10990	1.74989
-180.00	-16.70	3472.37	0.10990	1.74989
-170.00	-18.67	3441.67	0.10990	1.75006
-160.00	-20.70	3407.85	0.10990	1.75001
-150.00	-22.78	3370.58	0.10990	1.75002
-140.00	-24.86	3327.75	0.10990	1.75005
-130.00	-26.87	3277.04	0.10988	1.74890
-120.00	-28.92	3219.97	0.10987	1.74896
-110.00	-30.96	3153.88	0.10987	1.74892
-100.00	-32.95	3077.77	0.10987	1.74908
-90.00	-34.76	2990.94	0.10987	1.74901
-80.00	-36.23	2895.15	0.10988	1.74917
-70.00	-37.17	2794.22	0.10989	1.74943
-60.00	-37.39	2694.25	0.10990	1.74975
-50.00	-36.73	2603.75	0.10991	1.75009
-40.00	-35.09	2533.92	0.10991	1.75021
-30.00	-32.47	2497.69	0.10991	1.75013
-20.00	-29.06	2503.03	0.10987	1.74902
-10.00	-25.47	2545.84	0.10990	1.74915
-0.	-22.21	2615.13	0.10990	1.74996
10.00	-19.60	2695.72	0.10990	1.75003
20.00	-17.80	2780.87	0.10990	1.75013
30.00	-16.70	2870.66	0.10990	1.75012
40.00	-15.98	2969.88	0.10990	1.75012
50.00	-15.29	3079.53	0.11000	1.74901
60.00	-14.53	3205.88	0.10990	1.75006
70.00	-13.64	3328.53	0.10990	1.75010
80.00	-12.77	3437.57	0.10990	1.75010
90.00	-12.08	3524.42	0.10990	1.75011
100.00	-11.65	3585.00	0.10990	1.75007
110.00	-11.42	3618.98	0.10990	1.74908
120.00	-11.44	3631.77	0.10990	1.74995
130.00	-11.60	3624.71	0.10991	1.75053
140.00	-11.89	3601.71	0.10990	1.74967
150.00	-12.51	3570.65	0.10989	1.74957
160.00	-13.51	3536.55	0.10989	1.74939
170.00	-14.92	3503.21	0.10988	1.74915

a. Card Description

Columns	Mode	Quantity	Units	Description
1-12	F	PRLNG	degrees	geocentric longitude
13-24	F	PHI	degrees	geocentric latitude
25-36	F	ALT	km.	altitude
37-48	F	B	gauss	magnetic induction
49-60	F	EL	earth radii	magnetic field line



## H. Running Time

This program takes about ten minutes for each 100 kilometers in altitude. The initial minimum altitude is required in order to estimate the number of kilometers for a particular run. Use Figure 2 and the initial values of  $B$ ,  $L$  and  $\lambda$  to arrive at an estimate of the initial altitude  $h$ . Subtracting 800 kilometers from this value will give the approximate initial minimum altitude of the first ring. This is the altitude used in figuring the running time.



### III. LONGITUDINAL AVERAGING PROCESSOR

#### A. Introduction

Input to this program are the five diurnal average number density tables (Tables 1-5) and the B-L contour rings output from the B-L search routine. The tables are interpolated (extrapolated) in order to obtain a density value for every ten degrees of longitude in the B-L contours. The densities are then added together for each of the five flux models, and the resulting sum is divided by 36 to arrive at the longitudinally averaged number density. This is done for the northern and southern hemispheres separately and then these values are added together and divided by two in order to obtain one number density for each B and L and each of the five flux models. These final values are used as input to the lambda punch program.

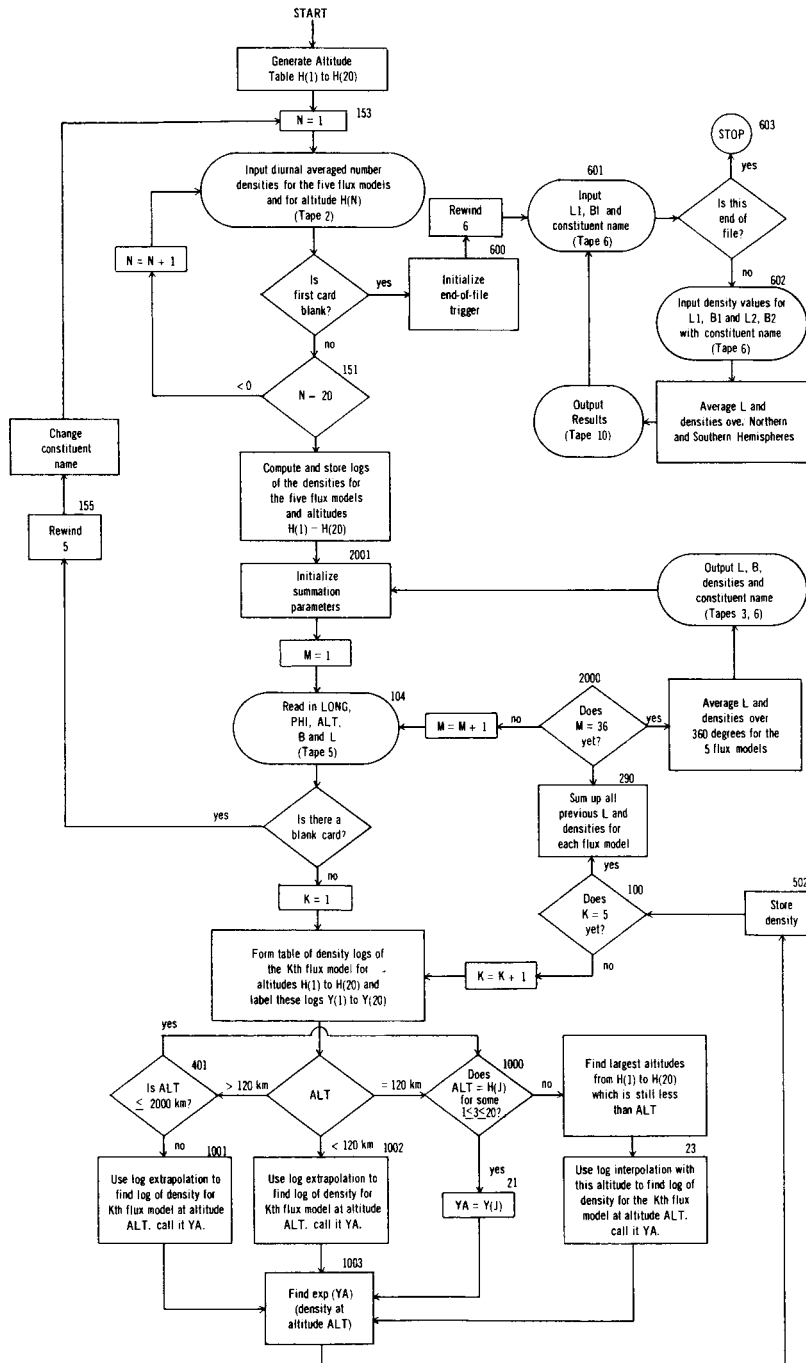
#### B. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
H(J)	J <sup>th</sup> altitude from the diurnal averaged atmosphere tables, Tables 1-5	km.
S1(J), . . . , S5(J)	diurnal averaged atmosphere densities for the J <sup>th</sup> altitude and fluxes of 250, 200, 150, 100 and $70 \times 10^{-22}$ watts/m <sup>2</sup> /cycle/sec from Tables 1-5	atoms/cm <sup>3</sup>
A1, . . . , A5	temporary storage of S1(J), . . . , S5(J)	"
SS1(J), . . . , SS5(J)	natural logarithms of S1(J), . . . , S5(J)	- -
AVHA	sum of EL	earth radii
AVBN1, . . . , AVBN5	density summation for the five flux models	atoms/cm <sup>3</sup>
LONG	geocentric longitude	degrees
PHI	geocentric latitude	degrees

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
ALT	altitude	km.
B	magnetic induction	gauss
EL	magnetic field line	earth radii
Y(I)	temporary storage of SSK(J) at altitude I = J depending on whether K = 1, 2, 3, 4 or 5	- -
HA	temporary storage of altitude	km.
YA	natural logarithm of density at altitude ALT	- -
BARN	density at altitude ALT	atoms/cm <sup>3</sup>
BARNAV(K)	temporary storage of BARN for flux model K	"
JUNK	temporary storage of K	- -
AVERH1	average longitudinal value of EL for only one hemisphere	earth radii
AVERN1,...,AVERN5	averaged densities for the five flux models and one hemisphere	atoms/cm <sup>3</sup>
FINI	end of file trigger for tape 6	- -
EL1	EL for northern hemisphere	earth radii
EL2	EL for southern hemisphere	"
B1	B for northern hemisphere	gauss
B2	B for southern hemisphere	"

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
EN1, . . . , EN5	the first time this designation appears it represents the northern hemisphere densities for the five flux models. The second time it appears it represents the densities for the north and south averaged together.	atoms/cm <sup>3</sup>
EN12, . . . , EN52	averaged southern hemisphere densities for the five flux models	"
ITT	counter to keep track of which hemisphere is being considered	- -
ITTI	counter to keep track of which atmospheric constituent is being considered	- -
XLA(ITTI)	first six letters of the constituent name designated by ITTI	- -
XLB(ITTI)	last two letters of the constituent name designated by ITTI	- -
TSA	first six letters of constituent name	- -
TSB	last two letters of constituent name	- -

# C. Flow Chart



D. Fortran Listing

```

C      LONGITUDINAL AVERAGING PROCESSOR
DIMENSION S1(20),S2(20),S3(20),S4(20),S5(20),H(20),S51(20),S52(20)
1  S53(20),S54(20),S55(20),Y(20),RANVA(5),XLA(5),XLB(5)
2  FORMAT(8X,3FAVERAGE NUMBER DENSITIES FOR DIFF S / IIX,
3  FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
4  FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
5  FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
6  FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
7  FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
8  FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
9  FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
10 FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
11 FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
12 FURMAT(8X,12FAVERAGE L=1F6.3,3X,2HB=1F6.5)
13 FURMAT(3F12.2+2F12.5)
14 FURMAT(5E12.6)
XLA(1)=6PFELIUM
XLA(2)=6HGXGEN
XLA(3)=6H C 2
XLA(4)=6HITRGG
XLB(1)=2H
XLB(2)=2H
XLB(3)=2H
XLB(4)=2F.2N
XLB(5)=2F.2N
IT=1
ITTI=1
WRITE OUTPUT TAPE 3,5,XLA(ITTI),XLB(ITTI)
H(1)=L20.
H(2)=2C0.
DO 150 N=2,15
H(N)=F(N)+1C0.
CONTINUE
150 READ INPUT TAPE 2,152,S1(N),S2(N),S3(N),S4(N),S5(N)
IF(S1(I)) 151,6C0,151
CONTINUE
DO 10 I=1,20
A1=S1(I)
A2=S2(I)
A3=S3(I)
A4=S4(I)
A5=S5(I)
S51(I) = LGGF(A1)
S52(I) = LGGF(A2)
S53(I) = LGGF(A3)
S54(I) = LGGF(A4)
S55(I) = LGGF(A5)
CONTINUE
10 AVHA=0.
AVB1=0.
AVB2=0.
AVB3=0.
AVB4=0.
AVB5=0.

```

```

2000 M=1,26
104 READ INPUT TAPE 5, 103,LCNG,PHI,ALTI,P,EL
IF (8) 153,155,505
155 REWIND 5
ITTI=ITTI+1
IF (ITTI-5) 157,157,153
157 WRITE OUTPUT TAPE 3,5,XLA(ITTI),XLR(ITTI)
GC TC 193
505 DO 100 K=1,5
GC TC (200,201,202,203,204),K
200 DC 300 I=1,20
Y(I) =S1(I)
300 CONTINUE
GC TC 400
201 DC 301 I=1,20
Y(I) =S2(I)
301 CONTINUE
GC TC 400
202 DC 302 I=1,20
Y(I) =S3(I)
302 CONTINUE
GC TC 400
203 DC 303 I=1,20
Y(I) =S4(I)
303 CONTINUE
GC TC 400
204 DC 304 I=1,20
Y(I) =S5(I)
304 CONTINUE
400 HA=ALT
IF(HA-120.) 1002,1000,401
401 IF(HA-2000.) 1000,1000,1001
1000 DC 20 J=1,20
IF( H(J)-HA ) 20,21,22
21 YA=Y(J)
GC TC 30
22 H1=H(J)
Y1=Y(J)
HG=H(J-1)
YG=Y(J-1)
GC TC 23
20 CONTINUE
23 YA=Y1-(Y1-YG)*(H1+A)/(H1+G)
30 GC TC 1003
1001 YA=Y(20)*(H-A-F(2C))*(Y(20)-Y(19))/(H(2C)-H(19))
GC TC 1003
1002 YA=Y(2)-(H(2)-HA)*(Y(2)-Y(1))/(H(2)-H(1))
1003 BARN=FAF(YA)
502 BARNAV(K)=BARN
JUNK=K
IF(JUNK-5) 100,290,100
290 AVHA=EL+AVFA
AVB1 = BARNAV(1)+AVB*1
AVB2 = BARNAV(2)+AVB*2
AVB3 = BARNAV(3)+AVB*3
AVB4 = BARNAV(4)+AVB*4

```







EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

IFN	LCC	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC	IFN	LCC
150	31 00067	153	32 00071	151	36 00123	10	48 00174	2001	49 00176	200	67 00316	302	77 00337	86 00356
154	56 00220	155	59 00245	157	64 00266	505	65 00305	200	67 00316	302	77 00337	400	86 00356	98 00425
200	69 00321	201	71 00325	201	73 00330	202	75 00334	400	86 00356	1003	104 00501	35	125 00606	145 00752
203	79 00343	303	81 00346	204	83 00351	304	85 00354	400	86 00356	1003	104 00501	35	125 00606	145 00752
401	88 00365	1000	85 00373	21	91 00403	22	93 00412	20	98 00425	1003	104 00501	35	125 00606	145 00752
23	95 00427	30	100 00446	1001	101 00447	1002	103 00464	1003	104 00501	1003	104 00501	35	125 00606	145 00752
202	105 00506	290	108 00517	100	114 00541	2000	115 00544	35	125 00606	602	145 00752			
36	128 00616	37	130 00624	600	138 00706	601	142 00730							
603	163 01151													

## E. Restrictions

Input tables must have densities for altitudes starting at 120 kilometers and followed by each 100-kilometer level up to 2000 kilometers. If the tables are changed then the program must be modified. The tables must be input in the following order:

- (1) helium,
- (2) oxygen,
- (3) molecular oxygen,
- (4) nitrogen,
- (5) hydrogen.

## F. Input

Input to this program is handled by two tapes. On tape 2 are entered the diurnal averaged atmosphere tables (Tables 1-5). These tables are punched on cards and placed one behind the other at the end of the Fortran deck. These tables must be input in the following order: helium, oxygen, molecular oxygen, nitrogen and hydrogen. This is necessary in order that the constituent names may be correctly punched on the output. It is also important that a blank card follow the last table in order to notify the program when it has reached the end of the file.

On tape 5 are placed the B-L contours which were produced by the B-L search program. As with the tables, the last card must be blank in order to designate an end of file.

### 1. Tape 2

#### a. Input Card Description

#### ATMOSPHERE TABLES

<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
1-12	E	S1(N)	atoms/cm <sup>3</sup>	density for flux model 1, altitude N
13-24	E	S2(N)	"	" " 2, "
25-36	E	S3(N)	"	" " 3, "
37-48	E	S4(N)	"	" " 4, "
49-60	E	S5(N)	"	" " 5, "



2. Tape 5

a. Input Card Description

B-L CONTOURS

<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
1-12	F	LONG	degrees	geocentric longitude
13-24	F	PHI	degrees	geocentric latitude
25-36	F	ALT	km	altitude
37-48	F	B	gauss	magnetic induction
49-60	F	EL	earth radii	magnetic field line

b. Sample

# GENERAL PURPOSE DATA SHEET

Problem		INPUT - LONGITUDINAL AVERAGING PROCESSOR (B-L CONTOURS)		SAMPLE		Page	
Spencer		TAPE 5		Date		of	
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## G. Output

Output for this program appears on logical tapes 3 and 10. Tape 3 will contain the averaged densities for each of the five flux models at a particular B and L for both northern and southern hemispheres and for each of the five constituents. The constituents (He, O, O<sub>2</sub>, N<sub>2</sub>, H) follow each other in the same order as they exist in the tables which are input on tape 2. Tape 3 is printed with appropriate headings.

Tape 10 also contains densities for the five flux models at each B and L but here the northern and southern hemispheres are averaged together to give one final value for each B and L. Tape 10 contains no headings but each card is labeled with the appropriate constituent name. This tape is punched in order to be used as input to the lambda punch.

A scratch tape must be set up on logical tape unit 6. Although no data appears on this tape at the completion of the program it is used in intermediate steps to store data.

1. Tape 3 Sample

ATMOSPHERIC CONSTITUENT--HELIUM

AVERAGE L= 1.142 B=.23891  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.8300E 06 0.7508E 06 0.6289E 06 0.4600E 06 0.3382E 06

AVERAGE L= 1.142 B=.23890  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1346E 08 0.1210E 08 0.1064E 08 0.9134E 07 0.8207E 07

AVERAGE L= 1.142 B=.22741  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7137E 06 0.6282E 06 0.5063E 06 0.3493E 06 0.2433E 06

AVERAGE L= 1.142 B=.22736  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1428E 07 0.1402E 07 0.1357E 07 0.1293E 07 0.1250E 07

AVERAGE L= 1.142 B=.23465  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7842E 06 0.7021E 06 0.5795E 06 0.4145E 06 0.2984E 06

AVERAGE L= 1.142 B=.23466  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5205E 07 0.4932E 07 0.4608E 07 0.4235E 07 0.3986E 07

AVERAGE L= 1.142 B=.21968  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6485E 06 0.5615E 06 0.4423E 06 0.2952E 06 0.1996E 06

AVERAGE L= 1.142 B=.21968  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8665E 06 0.8125E 06 0.7325E 06 0.6253E 06 0.5477E 06

AVERAGE L= 1.170 B=.23992  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7300E 06 0.6415E 06 0.5134E 06 0.3472E 06 0.2351E 06

AVERAGE L= 1.170 B=.23991  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1571E 08 0.1399E 08 0.1217E 08 0.1032E 08 0.9197E 07

AVERAGE L= 1.170 B=.23468  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6785E 06 0.5881E 06 0.4614E 06 0.3026E 06 0.1990E 06

AVERAGE L= 1.170 B=.23467  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5025E 07 0.4766E 07 0.4459E 07 0.4106E 07 0.3874E 07

AVERAGE L= 1.170 B=.22957  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6319E 06 0.5403E 06 0.4158E 06 0.2647E 06 0.1693E 06

AVERAGE L= 1.170 B=.22956  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1975E 07 0.1940E 07 0.1885E 07 0.1810E 07 0.1758E 07

AVERAGE L= 1.170 B=.21976  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.5513E 06 0.4595E 06 0.3410E 06 0.2052E 06 0.1246E 06

AVERAGE L= 1.170 B=.21977  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8559E 06 0.8062E 06 0.7343E 06 0.6406E 06 0.5740E 06

AVERAGE L= 1.170 B=.20975  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4812E 06 0.3913E 06 0.2804E 06 0.1600E 06 0.9249E 05

AVERAGE L= 1.170 B=.20972  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.6456E 06 0.5736E 06 0.4764E 06 0.3555E 06 0.2730E 06

AVERAGE L= 1.170 B=.20474  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4513E 06 0.3629E 06 0.2560E 06 0.1428E 06 0.8090E 05

AVERAGE L= 1.170 B=.20475  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5692E 06 0.4911E 06 0.3896E 06 0.2688E 06 0.1907E 06

AVERAGE L= 1.170 B=.20141  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4332E 06 0.3460E 06 0.2419E 06 0.1333E 06 0.7469E 05



AVERAGE L= 1.170 B=.20134  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5207E 06 0.4399E 06 0.3375E 06 0.2199E 06 0.1474E 06

AVERAGE L= 1.188 B=.23382  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6179E 06 0.5248E 06 0.3992E 06 0.2485E 06 0.1550E 06

AVERAGE L= 1.188 B=.23383  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.3782E 07 0.3632E 07 0.3447E 07 0.3229E 07 0.3084E 07

AVERAGE L= 1.188 B=.21177  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4507E 06 0.3605E 06 0.2517E 06 0.1373E 06 0.7561E 05

AVERAGE L= 1.188 B=.21175  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.6639E 06 0.5964E 06 0.5050E 06 0.3904E 06 0.3108E 06

AVERAGE L= 1.188 B=.25851  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.8776E 06 0.7972E 06 0.6687E 06 0.4846E 06 0.3495E 06

AVERAGE L= 1.188 B=.25853  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8554E 09 0.6005E 09 0.3943E 09 0.2397E 09 0.1695E 09

AVERAGE L= 1.188 B=.24959  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7733E 06 0.6856E 06 0.5550E 06 0.3807E 06 0.2603E 06

AVERAGE L= 1.188 B=.24954  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1175E 09 0.9275E 08 0.7004E 08 0.5030E 08 0.3995E 08

AVERAGE L= 1.188 B=.23938  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6690E 06 0.5769E 06 0.4486E 06 0.2890E 06 0.1862E 06

AVERAGE L= 1.188 B=.23934  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1212E 08 0.1095E 08 0.9695E 07 0.8383E 07 0.7571E 07

AVERAGE L= 1.188 B=.21981  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.5056E 06 0.4133E 06 0.2976E 06 0.1702E 06 0.9799E 05

AVERAGE L= 1.188 B=.21981  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8335E 06 0.7838E 06 0.7133E 06 0.6223E 06 0.5579E 06

AVERAGE L= 1.188 B=.20482  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4087E 06 0.3211E 06 0.2185E 06 0.1146E 06 0.6086E 05

AVERAGE L= 1.188 B=.20481  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.5597E 06 0.4837E 06 0.3855E 06 0.2689E 06 0.1932E 06

AVERAGE L= 1.200 B=.24991  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.7400E 06 0.6498E 06 0.5184E 06 0.3469E 06 0.2312E 06

AVERAGE L= 1.200 B=.24992  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1125E 09 0.8896E 08 0.6733E 08 0.4849E 08 0.3861E 08

AVERAGE L= 1.200 B=.23952  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.6373E 06 0.5438E 06 0.4160E 06 0.2608E 06 0.1634E 06

AVERAGE L= 1.200 B=.23948  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1122E 08 0.1018E 08 0.9049E 07 0.7866E 07 0.7131E 07

AVERAGE L= 1.200 B=.22940  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.5508E 06 0.4569E 06 0.3357E 06 0.1976E 06 0.1166E 06

AVERAGE L= 1.200 B=.22938  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.1666E 07 0.1638E 07 0.1594E 07 0.1536E 07 0.1496E 07

AVERAGE L= 1.200 B=.21979  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4790E 06 0.3869E 06 0.2735E 06 0.1516E 06 0.8459E 05

AVERAGE L= 1.200 B=.21980  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.8144E 06 0.7642E 06 0.6936E 06 0.6031E 06 0.5390E 06

AVERAGE L= 1.200 B=.20970  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.4136E 06 0.3249E 06 0.2207E 06 0.1151E 06 0.6061E 05

AVERAGE L= 1.200 B=.20971  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.6189E 06 0.5489E 06 0.4559E 06 0.3416E 06 0.2637E 06

AVERAGE L= 1.200 B=.18974  
AVERAGE NUMBER DENSITIES FOR DIFF S  
NORTHERN HEMISPHERE  
0.3116E 06 0.2325E 06 0.1468E 06 0.6859E 05 0.3260E 05

AVERAGE L= 1.200 B=.18975  
AVERAGE NUMBER DENSITIES FOR DIFF S  
SOUTHERN HEMISPHERE  
0.3818E 06 0.3026E 06 0.2112E 06 0.1179E 06 0.6790E 05

2. Tape 10

a. Output card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
B, L Card	1-8	F	EL	earth radii	averaged magnetic field line
	9-16	F	B	gauss	magnetic induction
	72-80	-	-	-	constituent name
Density Card	1-12	E	EN1	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	EN2	atoms/cm <sup>3</sup>	den " 2
	25-36	E	EN3	"	" " 3
	37-48	E	EN4	"	" " 4
	49-60	E	EN5	"	" " 5
	72-80	-	-	-	constituent name

b. Sample

# GENERAL PURPOSE DATA SHEET

Problem		OUTPUT - LONGITUDINAL AVERAGING PROCESSOR (NORTH-SOUTH AVERAGE)	
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## H. Running Time

An allowance of 8 seconds for each B-L line will give a close estimate of the running time for this program.

## IV. LAMBDA PUNCH

### A. Introduction

This program takes the cards from the longitudinal averaging processor and punches the latitude in degrees on every B-L card. This value is necessary in the execution of the "bounce" average calculation.

Computing the latitude is done by the method of false position using the equation.

$$B = \frac{M}{r_e^3} \frac{\sqrt{4 - 3 \cos^2 \lambda}}{L^3 \cos^6 \lambda} \quad (1)$$

where  $M$  is the earth's magnetic dipole moment,  $r_e$  is the radius of the earth and  $\lambda$  is the latitude.  $B$  is traded to the right hand side of equation (1) and the resulting function is evaluated for zero at a fixed  $B$  and  $L$ :

$$\text{BFUNF}(B, L, \lambda) = \frac{M}{r_e^3} \frac{\sqrt{4 - 3 \cos^2 \lambda}}{L^3 \cos^6 \lambda} - B$$

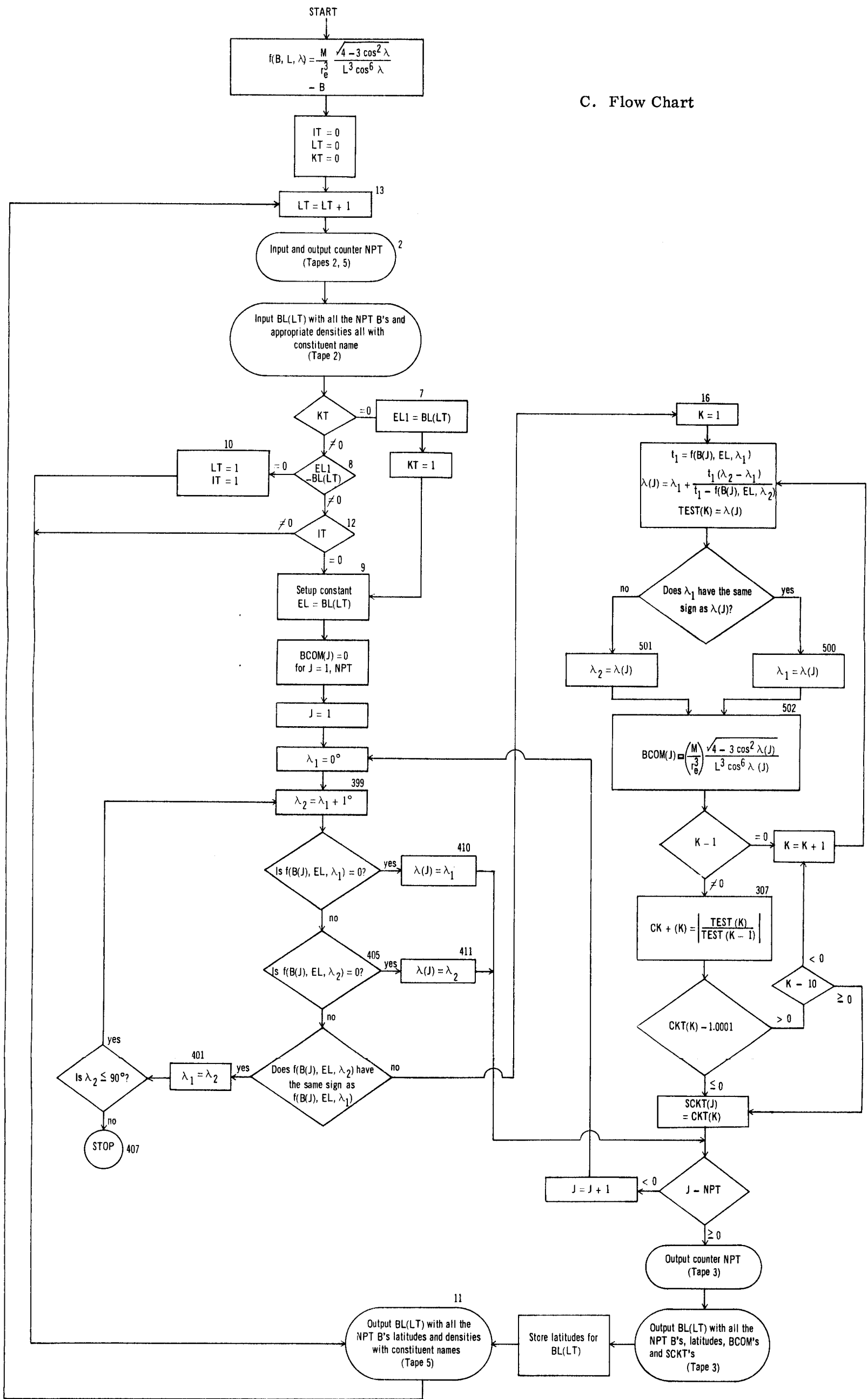
### B. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
IT	counter to eliminate repetition in computation	-
LT	L counter	-
KT	counter to determine whether a particular L is the first L considered	-
RTD	conversion factor - radians to degrees	-
DTR	" " - degrees to radians	-

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
RE	radius of the earth ( $6378.16 \times 10^5$ )	cm
EM	the earth's magnetic dipole moment ( $8.1 \times 10^{25}$ gauss cm <sup>3</sup> ) divided by the radius of the earth cubed	gauss
NPT	count of the number of B's to a given L	-
BL(J)	J <sup>th</sup> magnetic field line	earth radii
B(I)	I <sup>th</sup> magnetic induction for a given L	gauss
SS1(I),..., SS5(I)	longitudinally averaged number densi- ties for the five flux models and the I <sup>th</sup> B.	atoms/cm <sup>3</sup>
RATIO(I)	ratio of the upper limit on the latitude XLW2 to the lower limit on the latitude XLW1 for the I <sup>th</sup> B.	-
BCOM(I)	B computed for the final latitude XLAMP(I) at B(I)	gauss
XLW1	lower limit on the latitude	radians
XLW2	upper limit on the latitude	"
FXLW1	BFUNF computed for XLW1	-
FXLW2	" " " XLW2	-
XLAMP(I)	final selected latitude for B(I)	radians/ degrees
TERM 1	BFUNF computed for XLW1	-
TBLAM(J, I)	latitude for the I <sup>th</sup> B of the J <sup>th</sup> L	degrees
TEST(K)	temporary storage of XLAMP(J)	radians
CKT(K)	the absolute value of TEST(K)/TEST(K-1)	-
SCKT(J)	temporary storage of final CKT(K)	-



C. Flow Chart



D. Fortran Listing

```

LAMPUN
C   LAMPDA PUNCH
DIMENSION B(25),T,LAM(25,25),SS1(25),SS2(25),SS3(25),SS4(25),
ISS(25),CCOM(25),BL(25),TEST(20),CKI(20),SCKI(25),XLAMP(25)
BFUNFU,EM,EL,XLW1=EM*SGRT(4.0-3.0*CCSF(XLAMP)**2)/((FL**2)*
ICCSF(XLAMP)**6)-3
C   -RACR 1 = LAMPDA GREATER THAN 9C,0 DLG.
C   FORMATS
100 FORMAT(12)
101 FORMAT(2F0.5,56X,A6,A2)
102 FORMAT(5E12.4,12X,A6,A2)
103 FORMAT(6F EROR,I2)
104 FORMAT(5H1 NPT,5X,1H1,2X,1H8,6X,6HLAMPDA,4X,9HF CUMP. ,12X,5H RATI
(0)
105 FORMAT(14)
106 FORMAT(4X,2F10.5,F10.1,2E15.7)
107 FORMAT(2F6.5,F8.3,4E8,A6,A2/5E12.4,12X,A6,A2)
IT=0
LT=0
KT=0
13 LI=LI+1
2 READ INPUT TAPE 2,100,NPT
WRITE OUTPUT TAPE 5,100,NPT
DO 18 I=1,NPT
READ INPUT TAPE 2,101,BL(I),B(I),XLA,XLB
18 READ INPUT TAPE 2,102,SS1(I),SS2(I),SS3(I),SS4(I),SS5(I),XLA,XLB
IF(KT) 8,7,8
7 ELI=BL(I)
KT=1
GO TO 4
8 IF (ELI-BL(I)) 12,10,12
12 IF (I) 11,9,11
C   SOLVE FOR LAMPDA BY METHOD OF FALSE POSITION
C   DETERMINE APPROX. SOLN. USING 1 DEG. INCREMENTS
9 RTD=57.29578
DIR=0.01/45329
RE=6378.165E5
EM=8.1E25/RE**3
EL=BL(I)
DO 199 I1=1,NPT
199 BCOM(I1)=0.0
DC 200 J=1,NPT
XLW1=0.0
399 XLW2=XLW1*CTR
FXLW1=BFUNF(BL(I),EM,EL,XLW1)
FXLW2=BFUNF(BL(I),EM,EL,XLW2)
IF(FXLW1) 405,410,405
405 IF(FXLW2) 406,411,406
406 IF(FXLW1-SIGNF(FXLW1,FXLW2)) 16,401,16
401 XLW1=XLW2
407 IF(XLW2-1.5707961) 399,399,407
1ERR=1
WRITE OUTPUT TAPE 3,103,1ERR
CALL EXIT
410 XLAMP(J)=XLW1
GO TO 200

```

```

411 XLAMP(J)=XLRZ
    GC TC 2CC
    C      MFTDZ LF FALSE POSITION
    16 DC 15C K=1,1C
    TMRX=FCDF(RC(J),RNC(1,XLRZ))
    XLAMP(J)=XLRZ+TMRX/(1E0PI-2*FUNCFC(J),FM,L,XLRZ)
    I*(XLRZ-XLRZ)
    TEST(R)=XLAMP(J)
    IF(XLAMP(J)-SIGN(XLAMP(J),XLRZ)) 501,5CC,501
500 XLRZ=XLAMP(J)
502 BCDK(J)=FM*SGRTE(4-C-3*0*GUSE(XLAMP(J))*2)/(EL**3)*
    JGUSE(XLAMP(J))*6)
    IF (K=1) 307,15C,307
307 CRT(K)=463FTTEST(R)/T*STK-1))
    IF (CRT(K)-1.C001) 200,309,15C
501 XLRZ=XLAMP(J)
    GC TC 502
150 CONTINUE
309 SNT(J)=CRT(K)
200 CONTINUE
    WRITE OUTPUT TAPE 3,104
    WRITE OUTPUT TAPE 3,105,NPI
    DC 201 L=1,NPI
    XLAMP(L)=XLAMP(L)*RTO
201 WRITE OUTPUT TAPE 3,106,BL(L),XLAMP(L),BCCK(L),SCKT(L)
    DC 15 J=1,NPI
    15 TBLAP(LT,J)=XLAMP(J)
    GC TC 11
    10 LT=1
    11=1
    11 DC 17 L=1,NPI
    17 WRITE OUTPUT TAPE 5,107,BL(LT),BL(L),TBLAP(LT,L),XLA,XLB,SL(L),
    15S2(L),SS3(L),SS4(L),SS5(L),XLA,XLE
    GC TC 13
    END(1,1,0,0,0,0,1,0,0,0,0,0,0)

```

STORAGE NOT USED BY PROGRAM

DEC LCT  
1446 02546  
DEC CCT  
32561 77461

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC LCT	DEC CCT	DLC DLT	DLC CCT	DLC CCT
1294 02417	BL 1270 02366	B 1445 02445	CAT 1225 02311	SUKT 1205 02265
SS1 1420 02614	SS2 1395 02583	SS3 1370 02532	SS4 1345 02501	SS5 1320 02450
TBLAP 1155 02203	TEST 1245 02335	XLAMP 1180 02234		

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC LCT	DEC CCT	DEC DLT	DEC CCT	DEC CCT
530 01022	CLI 529 01021	EL 528 01020	EM 527 01017	FXLW1 526 01016
525 01015	ERR 524 01014	IT 523 01013	K 522 01012	KI 521 01011
LF 520 01010	NPT 519 01007	RE 518 01006	RTC 517 01005	TENM1 516 01004
ALA 515 01003	ALB 514 01002	ALW1 513 01001	ALW2 512 01000	

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN LCC	EFN LCC	EFN LCC	EFN LCC	EFN LCC
8134 100 00754	8135 101 00753	8136 102 00750	8137 103 00745	8138 104 00742
8139 105 00727	813A 106 00726	813B 107 00722		

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC LCT	DEC CCT	DEC DLT	DEC CCT	DEC CCT
494 00755	111 489 00763	21 439 00467	31 445 00675	41 32167 77777
511 504 00770	61 454 00708	71 508 00774	C160 505 00775	C163 510 00776
C164 511 00777	D140A 118 00164	D140C 297 00451	E14 76 00114	E16 85 00125
C17E 158 00736	E1H 183 00267	E1K 234 00352	E1C 291 00443	E1P 296 00450
I15 302 00456				

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC LCT	DEC CCT	DEC CCT	DEC CCT	DEC CCT
1 00001	EXIT 7 00007	SCRT 2 00002	(FIL) 6 00006	(FPT) 0 00000
4 00004	(STH) 5 00005	(TSH) 3 00003		

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

CCS	EXIT	SCRT	(FIL)	(FPT)	(RTN)	(STH)	(TSH)
-----	------	------	-------	-------	-------	-------	-------

NAMES AND LOCATIONS OF ARITHMETIC STATEMENT FUNCTIONS

DEC LCT	DEC CCT	DEC CCT	DEC CCT
401 00021			

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND LOCAL LOCATIONS

FFN	IFN	LLC	FFN	IFN	LLC	FFN	IFN	LLC	FFN	IFN	LLC	FFN	IFN	LLC
13	14	00029	2	16	00031	18	23	00024	7	26	00119	8	29	00122
12	30	00126	9	31	00132	159	37	00155	399	40	00167	405	44	00224
006	49	00226	401	46	00240	407	48	00247	410	52	00264	411	54	00270
14	58	00273	500	61	00354	502	62	00356	307	64	00426	501	66	00440
130	67	00445	309	69	00452	200	70	00454	201	76	00505	15	79	00535
10	81	00543	11	83	00591	17	84	00555						

## E. Restrictions

Before the first card of a new L line section a counter card must be inserted in order to inform the computer of the number of B's connected with that L.

## F. Input

There are three different cards in the input deck for this program. A counter card is followed by the designated number of card pairs for each L line of every constituent. The card pairs consist of a B-L card and a density card in that order. These are the cards output from the longitudinal averaging processor.

### 1. (Tape 2)

#### CARD DESCRIPTION

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
Counter Card	1-2	I	NPT	-	B-L, density card pair counter
B-L Card	1-8	F	EL	earth radii	magnetic field line
	9-16	F	B	gauss	magnetic induction
	73-80	-	-	-	constituent name
Density Card	1-12	E	SS1	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	SS2	"	" " " " 2
	25-36	E	SS3	"	" " " " 3
	37-48	E	SS4	"	" " " " 4
	49-60	E	SS5	"	" " " " 5
	73-80	-	-	-	constituent name



## G. Output

Output for this program occurs on logical tapes 3 and 5. Tape 3 contains the results of the latitude calculation. The counter NPT is printed along with L, B,  $\lambda$ , BCOMP and the ratio RATIO. BCOMP is the new B computed by inserting the values of L and  $\lambda$  into equation (1). It should compare with the initial B. RATIO is the ratio of  $\lambda$  to a former value of the latitude computed in the intermediate steps. It is the same as SCKT (refer to the mnemonics listing). RATIO should be within .0001 of unity.

Tape 5 contains the same data that was input on tape 2 with the exception that latitudes were added. This tape is punched and used as input for the "bounce" average calculation.



1. Tape 3 Sample

NPT	L	B	LAMBDA	B COMP.	RATIO
4	1.14200	0.23890	9.836	0.2389000E-00	0.1000009E 01
	1.14200	0.22738	7.740	0.2273800E-00	0.1000034E 01
	1.14200	0.23465	9.129	0.2346499E-00	0.1000039E 01
	1.14200	0.21968	5.867	0.2196800E-00	0.1000023E 01

NPT	L	B	LAMBDA	B COMP.	RATIO
7					
	1.17005	0.23991	12.444	0.2399099E-00	0.1000030E 01
	1.17005	0.23467	11.752	0.2346700E-00	0.1000012E 01
	1.17005	0.22956	11.022	0.2295600E-00	0.1000005E 01
	1.17005	0.21976	9.420	0.2197599E-00	0.1000056E 01
	1.17005	0.20973	7.346	0.2097300E-00	0.1000005E 01
	1.17005	0.20474	6.014	0.2047400E-00	0.1000015E 01
	1.17005	0.20137	4.894	0.2013700E-00	0.1000025E 01

2. Tape 5

a. Output card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
Counter Card	1-2	I	NPT	-	B-L- $\lambda$ and density card pair counter
B-L- $\lambda$ Card	1-8	F	EL	earth radii	magnetic field line
	9-16	F	B	gauss	magnetic induction
	17-24	F	XLAM	degrees	latitude
	73-80	-	-	-	constituent name
Density Card	1-12	E	SS1	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	SS2	"	" " " " 2
	25-36	E	SS3	"	" " " " 3
	37-48	E	SS4	"	" " " " 4
	49-60	E	SS5	"	" " " " 5
	73-80	-	-	-	constituent name

b. Sample

GENERAL PURPOSE DATA SHEET

Problem		OUTPUT - LAMBDA PUNCH		Date		SAMPLE		Page		of	
Spensor		TAPE 5									
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## H. Running Time

This program will take close to a minute for every two L lines evaluated.

## V. "BOUNCE" AVERAGE CALCULATION

### A. Introduction

The "bounce" average of the number density is defined<sup>(5)</sup> by the equation

$$\bar{\rho} = \frac{\int_{\lambda_s}^{\lambda_n} \rho(B, L) ds}{\int_{\lambda_s}^{\lambda_n} ds} \quad (1)$$

In other words, for a given mirror point  $\lambda_0$  and a given field line L, the "bounce" average of the number density is the average number of atoms/cm<sup>3</sup> that a particle encounters while spiraling about a field line from the northern to the southern mirror points (see Figure 5). The earth is assumed to be a dipole. This gives symmetry to the magnetic field, permitting the integrals in equation (1) to be evaluated over a fourth of a complete oscillation (see page 189, reference 1, for a discussion of the motion of trapped particles in a magnetic field.)

The output from the lambda punch becomes input to this program. Results are printed and punched for use in later programs. Subroutine TABLE is included to interpolate (extrapolate) the density table to supply the appropriate density at any latitude specified by the main program.

### B. Equations

To calculate equation (1) we project the element of arc length ds onto the field line L. Next we eliminate L from the equation and use the dipole representation

$$B = \frac{M}{r^3} (1 + 3 \sin^2 \lambda)^{1/2} \quad (2)$$

to express B in terms of  $\lambda$ . This gives the "bounce" average  $\bar{\rho}$  weighted over latitude for a given field line as

$$\text{RHOAV} = \frac{\int_0^{\lambda_0} \rho(\lambda) A(\lambda) d\lambda}{\int_0^{\lambda_0} A(\lambda) d\lambda} \quad (3)$$

where the "weighing" factor is

$$A(\lambda) = \frac{\cos^4 \lambda \sqrt{4 - 3 \cos^2 \lambda}}{\sqrt{\cos^6 \lambda \sqrt{4 - 3 \cos^2 \lambda_0} - \cos^6 \lambda_0 \sqrt{4 - 3 \cos^2 \lambda}}}$$

This factor allows for the fact that particles spiraling about the field line stay longer at the mirror latitudes  $\lambda_0$  (see page 189, reference 1, for a complete treatment of the derivation). Figure 6 is a plot of  $A(\lambda)$  versus  $\lambda$  for different mirror latitudes. Since  $A(\lambda)$  becomes undefined at  $\lambda_0$  we divided equation (3) into two cases:

$$\text{RHOAV} = \frac{\int_0^{\lambda_0 - 2h} \rho(\lambda) A(\lambda) d\lambda + \int_{\lambda_0 - 2h}^{\lambda_0} \rho(\lambda) A(\lambda) d\lambda}{\int_0^{\lambda_0 - 2h} A(\lambda) d\lambda + \int_{\lambda_0 - 2h}^{\lambda_0} A(\lambda) d\lambda}$$

Next we designate the square of the denominator of  $A(\lambda)$  by  $q(\lambda)$ . Expanding about  $\lambda_0$  by Taylor's series gives us

$$g(\lambda) = (\lambda - \lambda_0) \sum_{i=1}^{\infty} \frac{q^{(i)}(\lambda_0)}{i!} (\lambda - \lambda_0)^{i-1}$$

where  $q^{(i)}(\lambda_0)$  is the  $i^{\text{th}}$  derivative of  $q$  evaluated at  $\lambda_0$ . To approximate the infinite series we define

$$S(\lambda) = \text{SLAMF}(\lambda, \lambda_0) = - \sum_{i=1}^3 \frac{q^{(i)}(\lambda_0)}{i!} (\lambda - \lambda_0)^{i-1}$$

where the minus sign is inserted in order to avoid the square root of a negative number. In the program we let S1LAMF( $\lambda, \lambda_0$ ), S2LAMF( $\lambda, \lambda_0$ ) and S3LAMF( $\lambda, \lambda_0$ ) represent the first, second and third terms of SLAMF( $\lambda, \lambda_0$ ) respectively and we define

$$\text{WLAMF}(\lambda, \lambda_0) = \frac{\cos^4 \lambda \sqrt{4 - 3 \cos^2 \lambda}}{\sqrt{\text{SLAMF}(\lambda, \lambda_0)}}$$

This gives

$$\int_{\lambda_0 - 2h}^{\lambda_0} \rho(\lambda) A(\lambda) d\lambda = \int_{\lambda_0 - 2h}^{\lambda_0} \frac{\rho(\lambda) \text{WLAMF}(\lambda, \lambda_0)}{\sqrt{\lambda_0 - \lambda}} d\lambda \quad (4)$$

and

$$\int_{\lambda_0 - 2h}^{\lambda_0} A(\lambda) d\lambda = \int_{\lambda_0 - 2h}^{\lambda_0} \frac{\text{WLAMF}(\lambda, \lambda_0)}{\sqrt{\lambda_0 - \lambda}} d\lambda \quad (5)$$

which are linearly approximated by the equations

$$\begin{aligned} \text{ADDNUM} = \sqrt{2h} & \left[ \frac{4}{5} \rho(\lambda_0) \text{WLAMF}(\lambda_0, \lambda_0) + \frac{16}{15} \rho(\lambda_0 - h) \text{WLAMF}(\lambda_0 - h, \lambda_0) \right. \\ & \left. + \frac{2}{15} \rho(\lambda_0 - 2h) \text{WLAMF}(\lambda_0 - 2h, \lambda_0) \right] \end{aligned}$$

and

$$\text{ADDEN} = \sqrt{2h} \left[ \frac{4}{5} \text{WLAMF}(\lambda_0, \lambda_0) + \frac{16}{15} \text{WLAMF}(\lambda_0 - h, \lambda_0) + \frac{2}{15} \text{WLAMF}(\lambda_0 - 2h, \lambda_0) \right]$$



respectively. The final step is to integrate by Simpson's rule<sup>(6)</sup> and add on ADDNUM and ADDDEN to get the correct density  $\bar{\rho}$ .

Additional equations used in this program are listed below:

$$AAAF(\lambda) = \sqrt{4 - 3 \cos^2 \lambda}$$

$$BBBF(\lambda) = \cos^6 \lambda$$

$$MONEF(\lambda) = 3 \cos^4 \lambda \sin 2\lambda \quad \text{the first derivative of } BBBF(\lambda) \text{ used in computing } S1LAMF(\lambda, \lambda_0)$$

$$MTWOF(\lambda) = \frac{15}{2} (\cos \lambda \sin 2\lambda)^2 - 6 \cos^6 \lambda \quad \text{the second derivative of } BBBF(\lambda) \text{ used in computing } S2LAMF(\lambda, \lambda_0)$$

$$MTHRF(\lambda) = 48 \cos^4 \lambda \sin 2\lambda - 15 \sin^3 2\lambda \quad \text{the third derivative of } BBBF(\lambda), \text{ used in computing } S3LAMF(\lambda, \lambda_0)$$

$$ETAF(\lambda) = 10 \cos 2\lambda - 3 \sin^2 2\lambda - 6 \cos^2 2\lambda \quad \text{a factor which appears in the second and third derivatives of } AAAF(\lambda)$$

$$NONEF(\lambda) = \frac{3 \sin 2\lambda}{2 AAAF(\lambda)} \quad \text{the first derivative of } AAAF(\lambda) \text{ used in computing } S1LAMF(\lambda, \lambda_0).$$

$$NTWOF(\lambda) = \frac{3 ETAF(\lambda)}{4(4 - 3 \cos^2 \lambda)^{3/2}} \quad \text{the second derivative of } AAAF(\lambda) \text{ used in computing } S2LAMF(\lambda, \lambda_0).$$

$$NTHRF(\lambda) = \frac{3}{4} \frac{-20 \sin \lambda - 6 \sin 4\lambda - \frac{9 ETAF(\lambda) \sin 2\lambda}{4 - 3 \cos^2 \lambda}}{(4 - 3 \cos^2 \lambda)^{3/2}} \quad \text{the third derivative of } AAAF(\lambda), \text{ used in computing } S3LAMF(\lambda, \lambda_0)$$

WGTF( $\lambda, \lambda_0$ ) the designation for  $A(\lambda)$  when integrating by Simpson's rule

ALAM the value of the denominator in equation (3) but without equation (5)

RHOAS the value of the numerator in equation (3) but without equation (4)

BSUBO  $B_0$  computed by equation (2) for  $\lambda_0$ .

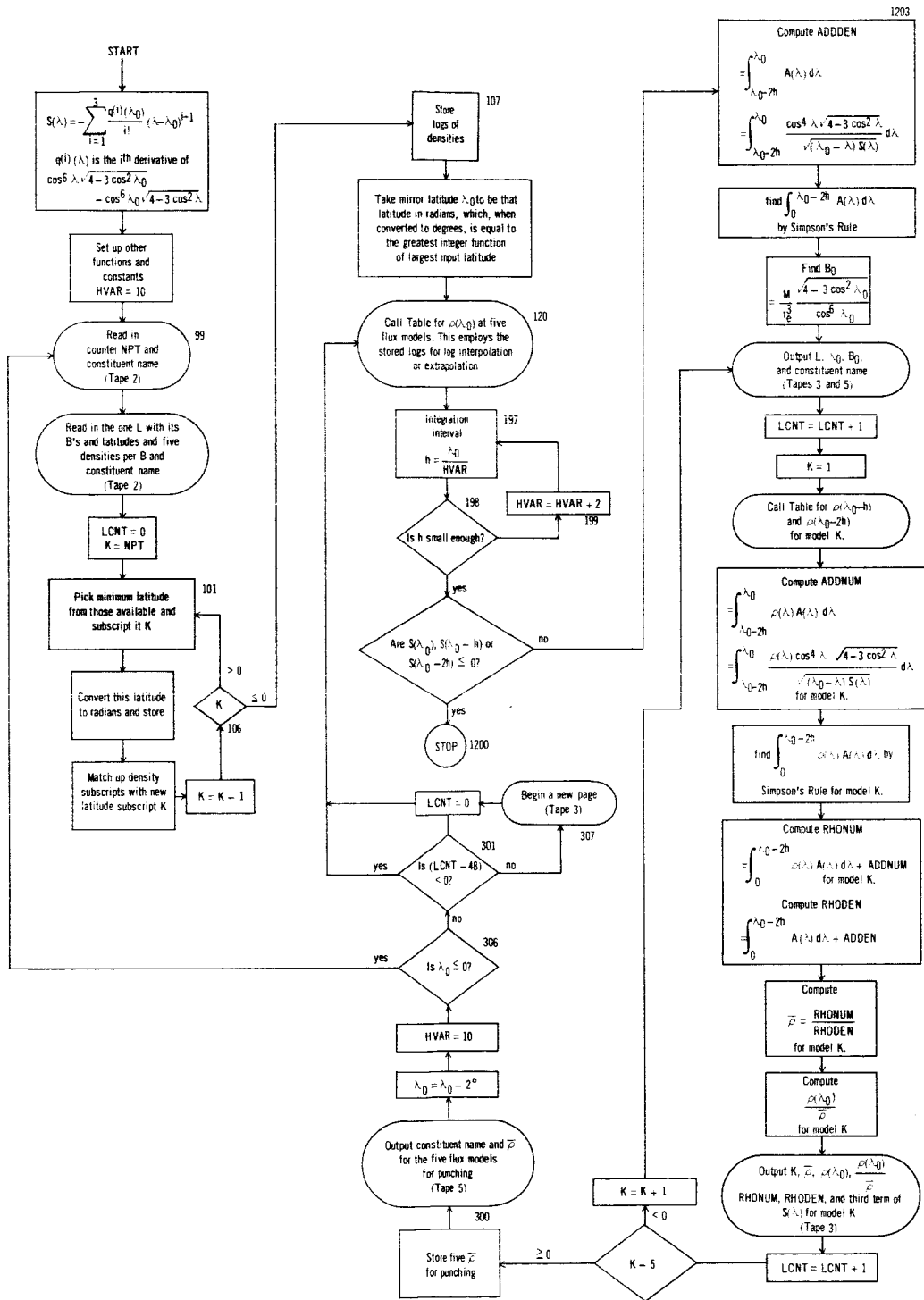
### C. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
DTR	Conversion factor - degrees to radians	-
RTD	Conversion factor - radians to degrees	-
RE	radius of the earth, $6378.165 \times 10^5$ cm.	cm.
EM	earth's magnetic dipole moment, $8.1 \times 10^{25}$ gauss cm <sup>3</sup> , divided by the radius of the earth cubed.	gauss
HVAR	number of partitions in Simpson's rule	-
NPT	counter of the B's for a given L	-
XLAB1	first six letters of constituent identification name	-
XLAB2	remaining two letters of constituent identification name	-
EL	magnetic field line L	earth radii
B(I)	I <sup>th</sup> magnetic induction for a given L	gauss
SS(I,J)	(a) the first time this designation is used it represents the longitudinally averaged density for the I <sup>th</sup> solar flux model and the J <sup>th</sup> magnetic induction	atoms/cm <sup>3</sup>
	(b) the second time this designation is used it represents the log of the densities in (a)	-
LCNT	line counter for output on tape 3	-
XMIN	storage of the smallest available latitude	degrees
XLAMW(K)	latitude in radians, sorted in decreasing order	radians
XLAMRF	storage of maximum value of the latitude	radians

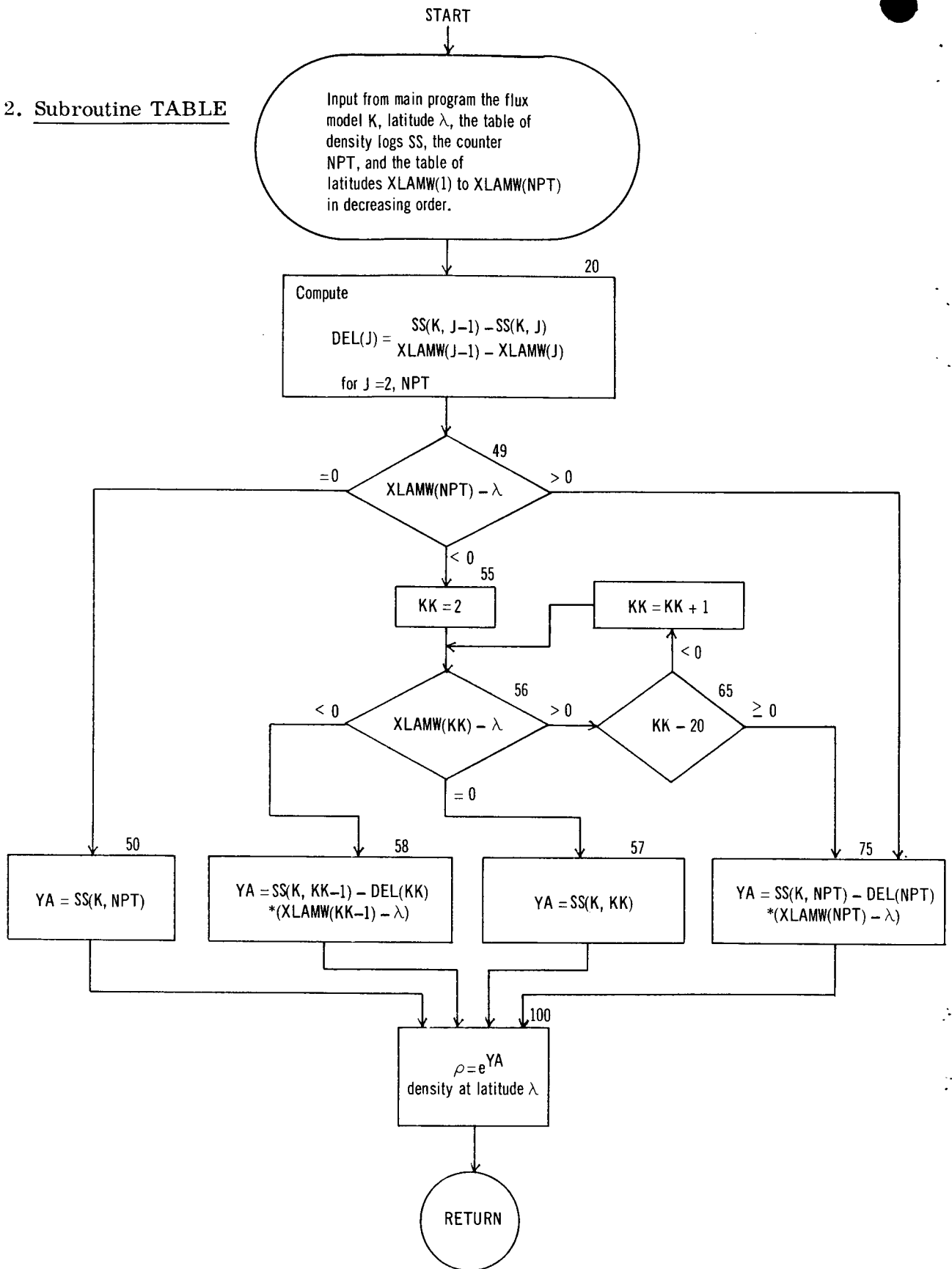
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
XLAMO	mirror latitude $\lambda_0$	radians
RHOLO(I)	density for I <sup>th</sup> flux model at mirror latitude	atoms/cm <sup>3</sup>
HS	integration interval h for Simpson's rule	radians
RHOAV	"bounce" average density	atoms/cm <sup>3</sup>
RATRHO	ratio of density at mirror latitude to density RHOAV	-
RHOLOP	density at mirror latitude	atoms/cm <sup>3</sup>
DENB(K)	temporary storage of "bounce" average density at K <sup>th</sup> flux model for tape 5 punch	atoms/cm <sup>3</sup>

# D. Flow Chart

## 1. Main Program



2. Subroutine TABLE



# E. Fortran Listing

```

BOUNCE
C      BOUNCF AVERAGE CALCULATION
C      PROGRAM TO COMPUTE RHO TRIPLE BAR AS FUNCTION OF L,LAMBDA AND FLUX
C      DIMENSION B(20),XL*(20),S(5,20),
1XLAM*(20),S15*(20),DENM*(20),RFO(LC(5)),DEL(5)
C      FREQUENCY IUT(10),IC6(10),I07(10),I03(15,0,5),I98(1,0,100)
1,30(15,0),J,308(1,0,10),I20(10,0,5),I205(100),Z11(99),Z59(100),
2261(59),I119(C,1,10),I201(C,1,10),I202(C,1,10)
C FORMATS
1 FORMAT(1Z,7CX,46,4Z)
2 FORMAT(2F8.5,F8.3,48X,A6,4Z)
3 FORMAT(5L12.4,12X,A6,4Z)
4 FORMAT(16R1CCASSTTUENT L,5X,11F1PROR C,4X,8DHFLUX AVERAGE R
1HC RHO AT MIRROR RHO/AV, RHO INTEGRAL OF INTEGRAL OF S3 (LA
2M.) F0R/22,4HLAT,31X,8HLATITUDE,19A,21F,4HC*4 CLAP A ULAP,4CX,
3I3HINT, INTERVAL//)
5 FORMAT(3X,A6,4Z,F8.4,F8.3,F8.4)
6 FORMAT(36X,12,1P6E14.4)
7 FORMAT(32HC ERROR - S(LAM) IS NEG, OR ZERO/6H SLL =E15.5,
16F SL2 =E15.5,6H SL3 =E15.5,8H XLAMO =E15.5,5H PS =E15.5)
8 FORMAT (25HLCIVIDE CHLCK HAS OCCURED)
9 FORMAT (30HQUOTIENT OVERFLOW HAS OCCURED)
C ARITHMETIC FUNCTIONS
AAAF(XL)=SORTF(4,C-3,0*(CCSF(XL)**2))
BBBF(XL)=CCSF(XL)**6
E1F(XL)=10.0*(CCSF(2.0*XL))-3.0*(SINF(2.0*XL)**2)
1-6.0*(CCSF(2.0*XL)**2)
MONEF(XL)=-3.0*(CCSF(XL)**4)*SINF(2.0*XL)
M1WDF(XL)=7.5*(CCSF(XL)*SINF(2.0*XL)**2-6.0*(CCSF(XL)**6)
M1TRF(XL)=4.0*(CCSF(XL)**4)*(SINF(2.0*XL))
1-15.0*(SINF(2.0*XL)**3)
N1WCF(XL)=1.5*SINF(2.0*XL)/AAAF(XL)
N1WDF(XL)=0.75*E1F(XL)/(14.0-3.0*(CCSF(XL)**2)**1.5)
N1TRF(XL)=(0.75*(1-20.0*(SINF(2.0*XL))-6.0*(SINF(4.0*XL))
1-(14.0-3.0*(CCSF(XL)**2)**1.5)
2/(14.0-3.0*(CCSF(XL)**2)**1.5)
S1LAMF(XL,XLC)=-1.0*(AAAF(XLC)*MONEF(XLC)-BBBF(XLC)*M1WDF(XLC))
S2LAMF(XL,XLC)=(AAAF(XLC)*M1TRF(XLC)-BBBF(XLC)*M1WCF(XLC))
2*(XL-XLC)/(1-2.0)
S3LAMF(XL,XLC)=(AAAF(XLC)*M1TRF(XLC)-BBBF(XLC)*M1TRF(XLC))
2*(14L-XLC)**2/(1-6.0)
SLAMF(XL,XLC)=S1LAMF(XL,XLC)+S2LAMF(XL,XLC)+S3LAMF(XL,XLC)
W1LAMF(XL,XLC)=(CCSF(XL)**4)*AAAF(XL)/SCRIF(SLAMF(XL,
1XLC))
W2TF(XL,XLC)=(CCSF(XL)**4)*AAAF(XL)/SORTF(
1AAAF(XLC)*BBBF(XL)-BBBF(XLC)*AAAF(XL))
C TURN OFF DIVIDE CHECK LIGHT
C AND QUOTIENT OVERFLOW LIGHT
30 IF QUOTIENT OVERFLOW 31,31
C PROGRAM CONSTANTS
31 DTR=1.7456293E-2
RTD=57.2957795
RFR=0.79,10.2E5
RMR=1.0297E-3
FVAR=10.0

```

```

99 IF CIVIDL CHECK 32,98
98 IF QUOTIENT OVERFLOW 34,32
97 WRITE OUTPUT TAPE 3,8
CALL EXIT
96 WRITE OUTPUT TAPE 3,9
CALL EXIT
C READ IN TABLES OF DENSITY FOR GIVEN L AND VARIOUS LAMBDA-S
C DENSITY - FIRST SUBSCRIPT = FLUX NO., SECOND SUBS. = LATITUDE IN C.
95 READ INPUT TAPE 2,1,NPT,XLAB1,XLAB2
DO 100 I=1,NPT
READ INPUT TAPE 2,2,EL,8(1),XL M(1),XLAEL,XLAB2
100 READ INPUT TAPE 2,3,(SS(IF,I),IF=1,5),XLAG1,XLAB2
WRITE OUTPUT TAPE 3,4
LCNT=0
EL3=EL*EL*EL
C SORT LAMBDA-S IN DECREASING ORDER
C SUBSCRIPT = I = MAX VALUE UP TO SUBSCRIPT = NPT = MIN VALUE
K=NPT
101 XMIN=50.0
102 DO 105 I=1,NPT
103 IF(XMIN-XL M(I)) 105,105,104
104 XMIN=XL M(I)
JJ=I
105 CONTINUE
C XLAM(K)=WORKING VALUE OF LAMBDA (IN RAD.) SORTED IN DECREASING ORDER
C DENSITY SUBSCRIPTS MATCHED UP WITH SORTED LAMBDA-S
XLAM(K)=XMIN*DIR
DO 1105 KF=1,5
1105 S(KF,K)=SS(RF,JJ)
XL P(JJ)=CC.C
K=K-1
106 IF(K) 107,107,101
C STORE LOG OF DENSITIES
107 DO 108 I=1,NPT
DO 1100 IL=1,5
1100 SS(IL,I)=LOG(S(IL,I))
108 CONTINUE
C MIRROR LATITUDE
XLAMR=XLAM(I)
XLAMD=C.C174
1300 IF(XLAMC-XLAMR) 1301,120,1302
1301 XLAG=ALAG.C.C174
GO TO 1305
1302 XLAG=ALAG.C.C174
C LINEAR INTERP. (EXTRAP.) TO FIND DENSITY (FROM TABLE) ASSOCIATED WITH
C MIRROR LATITUDE
1200 IF 1140 XI=1,5
CALL TABLE(XI,XLAMC,SS,RFC,S,NPT,XLAMW)
1140 RHOLOG(KI)=RHOS
C FIND INTEGRATION INTERVAL FOR SIMPSON-S RULE (HS)
117 HS=XLAMC/HSAP
TADP=.6485
S3FUA=3XLAMF(XLAMC+TADP,XLAMC)
118 IF(CARSF(S3FUA)-1.CE-7) 200,200,199
119 HVAR=HVAR+2.C
GO TO 197

```

```

C COMPUTE ADDEND FUNCTION FOR FINAL INTEGRATION STEPS
200 S2ZHS=SQRT(TACH)
HA=FS
TMAH=TACH
RHO3=H/3-C
C TEST IF SLAMP NEG.
SL1=SLAMP(XLAMU,XLAMU)
SL2=SLAMP(XLAMU-HS,XLAMU)
SL3=SLAMP(XLAMU-TWCF,XLAMU)
1199 IF(SL1) L200,L200,L201
1200 WRITE OUTPUT TAPE 3,7,SL1,SL2,SL3,XLAMU,HS
CALL FKIT
1201 IF(SL2) L200,L200,L202
1202 IF(SL3) L200,L200,L203
1203 ADDEN=S2ZHS*IC*8*XLAMP(XLAMU,XLAMU)+1.0666667*
1XLAMP(XLAMU-HA,XLAMU)+0.13333333*XLAMP(XLAMU-TMAH,
2XLAMP)
C INTEGRATE DENOMINATOR BY SIMPSON-S RULE (A(LAM) FUNCTION)
XLIMIT=XLAMU-TMAH
XN=(XLIMIT/TACH)+0.1
NEXN
NFI=N
NM2=N-1
A4=0.0
A2=0.0
XLAM=FS
209 DO 210 IS=1,NM1
XLAM=XLAM+TACH
210 A4=A4+WGTF(XLAM,XLAM)
XLAMP=0.0
211 DO 212 ISS=1,NM2
XLAM=XLAM+TRCH
212 A2=A2+NGJF(XLAM,XLAM)
ALAMP=FSJ *(WGTF(0.0,XLAMU)+4.0*A4+2.0*A2+WGTF(XLIMIT,
1XLAMU))
C END SIMPSON-S RULE FOR A(LAMBDA)
PSUBC=M*AAAF(XLAMU)/(EL3*8*PF(XLAMU))
ALAMP=ALAMP+PSUBC
WRITE OUTPUT TAPE 3,5,XLAB2,EL,XLAMP,PSUBC
WRITE OUTPUT TAPE 5,2,EL,PSUBC,XLAMP,XLAB1,XLAB2
LCNT=LCNT+1
C INTEGRATE FIVE DENSITY MODELS
DO 300 K=1,5
RHO1=RHO0(K)
C ADDEND FUNCTION FOR NUMERATOR
CALL TABLE(K,XLAMU-HA,SS,RHCW2,NPT,XLAMU)
CALL TABLE(K,XLAMU-TMAH,SS,RHCW3,NPT,XLAMU)
ADONUP=SL2H*IC*8*RHCW1*XLAMP(XLAMU,XLAMU)+1.0666667*
1RHO2*XLAMP(XLAMU-HA,XLAMU)+0.13333333*RHCW3*
2XLAMP(XLAMU-TMAH,XLAMU)
RHO4=RHO0
RHO2=G.0
RHOA2=G.0
XLAM=HS
259 DO 260 KS=1,NM1
XLAM=XLAM+TRCH

```



```

CALL TABLE (K,XLAM,SS,RHCTAB,NPT,XLAMW)
250 RFOA4=RFOA4+RHOTAB*WGTF(XLAM,XLAMU)
XLAM=1.0
251 DO 262 KSS=1,NM2
XLAM=XLAM+TRF
CALL TABLE (K,XLAM,SS,RHCTAB,NPT,XLAMW)
262 RFOA2=RFOA2+RFOTAB*WGTF(XLAM,XLAMU)
CALL TABLE (K,G,C,SS,HCASC,NPT,XLAMW)
CALL TABLE (K,XLIMIT,SS,RHCASN,NPT,XLAMW)
RHDA5=RSUS *(RFOA5*WGTF(G+0,XLAMC)+4.0*RFOA4+2.0*RFOA2
I+RHDA5*WGTF(XLIMIT,XLAMC))
C END SIRPSCA-5 RULE FOR RHO*A (LAMBDA)
C COMPUTE BOUNCE AVERAGE
RHOEN=ALAM*ACDEN
RHODEN=RHODEN/RHOEN
RHOEN=ALAM*ACDEN
RHOEN=RHODEN/RHOEN
C COMPUTE RATIO OF SOURCE DENSITY TO INITIAL
RATRHO=RHOLO(K)/RHOAV
RHOLOP=RHOLO(K)
WRITE OUTPUT TAPE 3,6,K,RFOAV,2*HOLCP,RATRHO,RHCNUM,RHODEN,S3FCA
LCNT=LCNT+1
C STORE SOURCE AVERAGE DENSITIES FOR A-5 PUNCH
300 DENB(K)=RHOAV
WRITE OUTPUT TAPE 5,3,DENE(1),DENE(2),DENS(3),DENS(4),DENS(5),
IXLAI,XLAI2
XLANO=ALAM*G-C.03450653
HVAR=10.0
306 IF (XLAM) 99,99,301
301 IF (LCNT-4) 120,307,307
307 WRITE OUTPUT TAPE 3,4
LCNT=C
GO TO 120
END(1,1,0,0,0,0,0,0,0,0,0,0,0,0,0)

```

STORAGE NOT USED BY PROGRAM

DEC	LCT	DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT
173	03305	32561	77461	1647	03157	1872	03210	1652	03164
				4PULG					
SS	1642	03152		ALM	1712	03260			

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	LCT	DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT
1732	03304	1647	03157	1872	03210	1652	03164	1542	03006
		ALMPA	1852	03234					

SEPARATE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT		
A2	1482	02642	AM	1441	02641	ALADDN	1439	02637	ALAM	1438	02636
RSUBC	1437	02635	GR	1436	02634	EL	1434	02632	EM	1433	02631
HA	1432	02630	F503	1431	02627	HVAR	1429	02625	I	1428	02624
JJ	1427	02623	KI	1426	02622	K	1425	02621	NM1	1423	02617
NM2	1422	02616	MPT	1421	02615	N	1420	02614	RE	1418	02612
RHOA2	1417	02611	RHOA4	1416	02610	RLCASN	1415	02607	RFCAS	1413	02605
RHOA4	1411	02604	RHOEN	1411	02603	RFLCPC	1410	02602	RFCAS	1408	02600
RFCAB	1407	02597	RHOE1	1405	02576	RFCW2	1405	02575	RFCAS	1403	02573
S3FUN	1402	02572	SL1	1401	02571	SL2	1400	02570	RFCAS	1398	02567
TWHA	1397	02565	TROH	1396	02564	ALAB1	1395	02563	SL2F	1393	02561
ALAMP	1392	02560	ALAPRF	1351	02557	ALAM	1390	02556	XLAMP	1388	02554
XN	1387	02553									

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN	LCC	LFN	LCC	EFN	LCC	EFN	LCC	EFN	LCC		
811	1	02467	812	2	02464	813	3	02460	814	4	02455
816	6	02404	817	7	02401	818	8	02395	819	9	02347

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT		
11	1336	02470	111	1343	02477	112	1343	02505	113	1356	02516
115	1366	02526	21	1209	02471	31	1217	02501	41	12767	77777
412	1369	02531	413	1371	02533	414	1373	02535	415	1375	02537
71	1377	02541	711	1378	02542	712	1379	02543	713	1380	02544
C1G1	1382	02546	C1G2	1383	02547	C11C1	1384	02550	C11C2	1385	02551
C11C3	119	00167	D120R	223	00237	E13C8	222	00336	L14C0	127	00177
C150H	167	00247	E1C	118	00166	E1P	212	00324	E1C	217	00331

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT		
CCS	1	00001	EXIT	7	00007	EXP(J	4	00004	LOG	10	00012
SURT	2	00002	TABLE	11	00013	(FIL)	6	00006	(FPT)	0	00000
(ISTH)	5	00005	(TSH)	8	00010						

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

DEC	GCT	DEC	GCT	DEC	GCT	DEC	GCT
3	00003	SIN		9	00011	(RTN)	

CCS (STH) (X11) (ISF) EXP(2) LCC STH SORT TABLE (FIL) (FPI) (RTN)

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

DEC	COI	DEC	COI	DEC	COI	DEC	COI
749	01394	764	01374	780	01314	810	01452
834	01362	803	01607	942	01026	917	01623
1031	02807	1067	02653	1100	02122	1163	02213

IFN	LCC	IFN	LCC	IFN	LCC	IFN	LCC
30	00023	31	00026	32	00066	33	00054
34	00021	35	00200	36	00124	37	00170
103	00200	104	00205	105	00213	106	00266
107	00271	1108	00300	108	00210	1301	00325
1302	00332	120	00340	1190	00354	86	00376
159	00404	200	00410	1199	00446	100	00472
1702	00470	1203	00502	209	00376	211	00621
212	00627	259	01061	260	01100	262	01141
300	01300	306	01334	301	01340	146	01141

```

C SUBROUTINE TABLE
SUBROUTINE TO INTERP. (EXTRAP.) IN DENSITY TABLE FOR GIVEN S
SUBROUTINE TABLE (K,XLAM,SS,RHUS,NPT,XLAM*)
DIMENSION SS(5,20),Y(20),DEL(20),XLAM(20)
FREQUENCY15(10),4Y(10,0,5),56(5,0,5)
15 DO 20 J=2,NPT
20 DEL(J)=(SS(K,J-1)-SS(K,J))/(XLAM(J-1)-XLAM(J))
49 IF(XLAM(NPT)-XLAM) 55,5C,75
50 YA=SS(K,NPT)
GG TO 1CU
55 DC 65 KK=2,2G
56 IF(XLAM(KK)-XLAM) 58,57,65
57 YA=SS(K,KK)
GG TO 1CU
58 YA=SS(K,KK-1)-DEL(KK)*(XLAM(KK-1)-XLAM)
GG TO 1CU
65 CONTINUE
C EXTRAPOLATE
75 YA=SS(K,NPT)-DEL(NPT)*(XLAM(NPT)-XLAM)
100 RHUS=EXPF(YA)
RETURN
END(1,1,0,0,0,0,0,0,0,0,0,0,0,0,0)

```

STORAGE NOT USED BY PROGRAM

DEC	LOC	DEC	LOC
204	00314	32961	77461

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	LOC	DEC	LOC
183	00267	203	00313

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	LOC	DEC	LOC
163	00243	162	00242

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	LOC	DEC	LOC
154	00232	144	00220
158	00236	159	00237
121	00171	72	00110

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	LOC	DEC	LOC
0	00000		

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

EXP

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND LOCAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC
15	9	00062	49	7	00103
38	11	00125	58	14	00137
100	18	00172	57	12	00132
			20	6	00071
			57	12	00132
			49	7	00103
			50	8	00112
			65	16	00152
			55	10	00116
			75	17	00157

## F. Input

The input to this program are simply the cards output from the lambda punch. Each constituent can be run separately or they can all be run at the same time. Any number of L lines may be run also. A counter card must state the number of points to each L line which is run. Counter cards are included in the output from the lambda punch but they must be corrected if the number of points per L line are changed before running this program. Input occurs on tape 2.

### 1. Input card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
Counter Card	1-2	I	NPT	-	B-L- $\lambda$ , density card pair counter
B-L- $\lambda$ Card	1-8	F	EL	earth radii	magnetic field line
	9-16	F	B(I)	gauss	magnetic induction
	17-24	F	XLAM(I)	degrees	latitude
	73-80	-	-	-	constituent name
Density Card	1-12	E	SS(1,I)	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	SS(2,I)	"	" " 2
	25-36	E	SS(3,I)	"	" " 3
	37-48	E	SS(4,I)	"	" " 4
	49-60	E	SS(5,I)	"	" " 5
	73-80	-	-	-	constituent name



## G. Output

Output from this program appears on logical tapes 3 and 5. Tape 3 gives results which are to be printed. Each page is devoted to a single L line for a specific constituent. Of the eleven columns which cross the page, the first contains the constituent name. This is followed by the value of L, the mirror latitude  $\lambda_0$ , the corresponding value of B, the flux model number, the "bounce" average number density, the longitudinally averaged number density, the ratio of the longitudinally averaged number density to the "bounce" averaged number density, the value of  $\int_0^{\lambda_0} \rho(\lambda)A(\lambda) d\lambda$ , the value of  $\int_0^{\lambda_0} A(\lambda)d\lambda$  and the third term of SLAMF( $\lambda_0 + 2h, \lambda_0$ ). All these additional values are included as an intermediate check on the process.

Tape 5 contains the data to be punched. The counter card has been eliminated and all that remains are the B-L- $\lambda$  card and the "bounce" average density card with constituent names punched to the right of each card.



1. Tape 3 Sample

CONSTITUENT	L	MIRREN LAT.	δ	FLUX	AVERAGE REFU	RHC AT MIRREN LATITUDE	RNU/AV. RFO	INTEGRAL CF RHO* CLAM	INTEGRAL CF A CLAM	S3 (LAM.) FOR INT. INTERVAL
HELIUM	1.1420	0.973	0.2338	1	1.0423E 06	2.6674E 00	2.4419E 00	8.2198E 05	7.5248E-01	-9.9948E-08
				2	1.0098E 06	2.5110E 00	2.4866E 00	7.5985E 05	7.5248E-01	-9.9948E-08
				3	8.9910E 05	2.3114E 00	2.5707E 00	6.7656E 05	7.5248E-01	-9.9948E-08
				4	7.6346E 05	2.0679E 00	2.7084E 00	5.7449E 05	7.5248E-01	-9.9948E-08
				5	6.7422E 05	1.9022E 00	2.8213E 00	5.0734E 05	7.5248E-01	-9.9948E-08
HELIUM	1.1420	0.973	0.2239	1	0.2956E 05	9.2931E 05	1.4054E 00	4.6787E 05	7.4783E-01	-9.9891E-08
				2	5.5098E 05	8.6498E 05	1.5474E 00	4.1802E 05	7.4783E-01	-9.9891E-08
				3	4.6031E 05	7.7118E 05	1.6467E 00	3.5022E 05	7.4783E-01	-9.9891E-08
				4	3.5807E 05	6.4768E 05	1.8088E 00	2.6778E 05	7.4783E-01	-9.9891E-08
				5	2.8677E 05	5.6219E 05	1.9204E 00	2.1446E 05	7.4783E-01	-9.9891E-08
HELIUM	1.1420	0.973	0.2168	1	4.7748E 05	6.4203E 05	1.3446E 00	3.5538E 05	7.4428E-01	-9.9846E-08
				2	4.1045E 05	5.7017E 05	1.3891E 00	3.0549E 05	7.4428E-01	-9.9846E-08
				3	3.2762E 05	4.7128E 05	1.4008E 00	2.4012E 05	7.4428E-01	-9.9846E-08
				4	2.2101E 05	3.4903E 05	1.5795E 00	1.6449E 05	7.4428E-01	-9.9846E-08
				5	1.5864E 05	2.6042E 05	1.6920E 00	1.1807E 05	7.4428E-01	-9.9846E-08
HELIUM	1.1420	0.973	0.2122	1	3.6833E 05	4.4396E 05	1.2042E 00	2.7325E 05	7.4185E-01	-9.9703E-08
				2	3.0540E 05	3.7594E 05	1.2306E 00	2.2656E 05	7.4185E-01	-9.9703E-08
				3	2.2019E 05	2.8801E 05	1.2733E 00	1.6780E 05	7.4185E-01	-9.9703E-08
				4	1.3590E 05	1.8809E 05	1.3445E 00	1.0378E 05	7.4185E-01	-9.9703E-08
				5	9.0097E 04	1.2816E 05	1.4130E 00	6.7283E 04	7.4185E-01	-9.9703E-08
HELIUM	1.1420	0.973	0.2039	1	2.8749E 05	3.0644E 05	1.0059E 00	2.1293E 05	7.4064E-01	-9.9809E-08
				2	2.3060E 05	2.4774E 05	1.0743E 00	1.7079E 05	7.4064E-01	-9.9809E-08
				3	1.5177E 05	1.7601E 05	1.0880E 00	1.1981E 05	7.4064E-01	-9.9809E-08
				4	9.1254E 04	1.0136E 05	1.1107E 00	6.7586E 04	7.4064E-01	-9.9809E-08
				5	5.4019E 04	0.1189E 04	1.1327E 00	4.0009E 04	7.4064E-01	-9.9809E-08

CONSTITUENT	L	MIRROR LAT.	B	FLUX	AVERAGE RHO	RHO AT MIRROR LATITUDE	RHO/AV. RHO	INTEGRAL OF RHO*ΔLAM	INTEGRAL OF ΔLAM	A CLAM	INTEGRAL OF S3 (LAM.) FOR INT. INTERVAL
HELIUM	1.1700	11.963	C.2362	1	1.1605E 06	3.9406E 06	3.3955E 00	8.0337E 05	7.6118E-01	7.6118E-01	-9.9974E-08
				2	1.0554E 06	3.6392E 06	3.4480E 00	8.0338E 05	7.6118E-01	7.6118E-01	-9.9974E-08
				3	9.2413E 05	3.2852E 06	3.5549E 00	7.0342E 05	7.6118E-01	7.6118E-01	-9.9974E-08
				4	7.7353E 05	2.8870E 06	3.7523E 00	5.8879E 05	7.6118E-01	7.6118E-01	-9.9974E-08
				5	6.7968E 05	2.6315E 06	3.8716E 00	5.1736E 05	7.6118E-01	7.6118E-01	-9.9974E-08
HELIUM	1.1700	9.963	C.2229	1	5.7759E 05	8.6715E 05	1.5013E 00	4.3617E 05	7.5516E-01	7.5516E-01	-9.9922E-08
				2	4.9057E 05	7.9498E 05	1.5945E 00	3.7650E 05	7.5516E-01	7.5516E-01	-9.9922E-08
				3	3.9651E 05	6.9577E 05	1.7460E 00	3.0093E 05	7.5516E-01	7.5516E-01	-9.9922E-08
				4	2.8489E 05	5.7327E 05	2.0123E 00	2.1513E 05	7.5516E-01	7.5516E-01	-9.9922E-08
				5	2.1614E 05	4.9280E 05	2.2800E 00	1.6322E 05	7.5516E-01	7.5516E-01	-9.9922E-08
HELIUM	1.1700	7.963	C.2124	1	4.9387E 05	6.0193E 05	1.2188E 00	3.7041E 05	7.5001E-01	7.5001E-01	-9.9847E-08
				2	4.1153E 05	5.2295E 05	1.2708E 00	3.0865E 05	7.5001E-01	7.5001E-01	-9.9847E-08
				3	3.0989E 05	4.2009E 05	1.3556E 00	2.3242E 05	7.5001E-01	7.5001E-01	-9.9847E-08
				4	1.9767E 05	2.9864E 05	1.5108E 00	1.4826E 05	7.5001E-01	7.5001E-01	-9.9847E-08
				5	1.3185E 05	2.2157E 05	1.6805E 00	9.8892E 04	7.5001E-01	7.5001E-01	-9.9847E-08
HELIUM	1.1700	5.963	C.2046	1	4.4908E 05	5.0863E 05	1.1326E 00	3.3497E 05	7.4590E-01	7.4590E-01	-9.9979E-08
				2	3.6544E 05	4.2540E 05	1.1641E 00	2.7259E 05	7.4590E-01	7.4590E-01	-9.9979E-08
				3	2.6457E 05	3.2122E 05	1.2142E 00	1.9734E 05	7.4590E-01	7.4590E-01	-9.9979E-08
				4	1.5665E 05	2.0438E 05	1.3047E 00	1.1684E 05	7.4590E-01	7.4590E-01	-9.9979E-08
				5	9.5689E 04	1.3457E 05	1.4034E 00	7.1524E 04	7.4590E-01	7.4590E-01	-9.9979E-08
HELIUM	1.1700	3.963	C.1931	1	4.1452E 05	4.5089E 05	1.0678E 00	3.0794E 05	7.4290E-01	7.4290E-01	-9.9457E-08
				2	3.3077E 05	3.6665E 05	1.1085E 00	2.4573E 05	7.4290E-01	7.4290E-01	-9.9457E-08
				3	2.3198E 05	2.6479E 05	1.1414E 00	1.7234E 05	7.4290E-01	7.4290E-01	-9.9457E-08
				4	1.2947E 05	1.5521E 05	1.2011E 00	9.6186E 04	7.4290E-01	7.4290E-01	-9.9457E-08
				5	7.4132E 04	9.3876E 04	1.2663E 00	5.5073E 04	7.4290E-01	7.4290E-01	-9.9457E-08
HELIUM	1.1700	1.963	C.1939	1	3.8512E 05	3.5909E 05	1.0432E 00	2.8393E 05	7.4110E-01	7.4110E-01	-9.9592E-08
				2	2.5599E 05	3.1601E 05	1.0934E 00	2.2233E 05	7.4110E-01	7.4110E-01	-9.9592E-08
				3	2.0408E 05	2.1828E 05	1.0695E 00	1.5125E 05	7.4110E-01	7.4110E-01	-9.9592E-08
				4	1.0770E 05	1.1833E 05	1.0987E 00	7.9820E 04	7.4110E-01	7.4110E-01	-9.9592E-08
				5	5.7930E 04	6.5489E 04	1.1305E 00	4.2932E 04	7.4110E-01	7.4110E-01	-9.9592E-08

2. Tape 5

a. Output card description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
B-L-\	1-8	F	EL	earth radii	magnetic field line
Card	9-16	F	BSUBO	gauss	magnetic induction
	17-24	F	XLAMP	degrees	latitude
	73-80	-	-	-	constituent name
Density	1-12	E	DENB(1)	atoms/cm <sup>3</sup>	density for flux model 1
Card	13-24	E	DENB(2)	"	" " 2
	25-36	E	DENB(3)	"	" " 3
	37-48	E	DENB(4)	"	" " 4
	49-60	E	DENB(5)	"	" " 5
	73-80	-	-	-	constituent name





## H. Running Time

This program will take about twenty minutes for every two L lines if five constituents are run together.

## VI. R, $\Sigma$ CALCULATION AND FLUX ELIMINATION

### A. Introduction

This program computes the atmospheric scale factor R and the atmospheric loss parameter  $\Sigma$ . The scale factor is used in the next program in order to relate the energy loss of the atmosphere with the measured energy loss data.<sup>(7)</sup> The atmospheric loss parameter appears in the calculation of the proton loss term of the conservation equation in the next section. Solar flux S is eliminated from both R and  $\Sigma$  by subroutine ELIM. This subroutine logarithmically interpolates Figure 9 to yield R and  $\Sigma$  as functions of time rather than solar flux S. B, L, and  $\lambda$  and the "bounce" averaged number densities are input to this program. B, L,  $\lambda$ , R and  $\Sigma$  are output for use in the conservation equation calculation.

### B. Equations

For a given B and solar flux model, the "bounce" average number densities of the five constituents are put together to form an average number of equivalent oxygen atoms/cm<sup>3</sup> by the equation  $OXY = RHO/8$  where

$$RHO = 14\bar{n}^{(N_2)} + 8\bar{n}^{(O)} + 2\bar{n}^{(He)} + 16\bar{n}^{(O_2)} + \bar{n}^{(H)}$$

and  $\bar{n}^{(J)}$  is the "bounce" average number density for the J<sup>th</sup> constituent.

The scale factor R is given by the equation

$$R(L, B, t) = \frac{(\text{OXYGEN ATOMS}/\text{CM}^3)\text{ATMOS}}{(\text{OXYGEN ATOMS}/\text{CM}^3)\text{NTP}}$$

where (oxygen atoms/cm<sup>3</sup>) ATMOS is OXY and (oxygen atoms/cm<sup>3</sup>) NTP comes from the following relationship of an ideal gas:

$$22414 \text{ cm}^3/\text{K mole} = .60249 \times 10^{24} \text{ atoms}/\text{K mole}$$

or  $(\text{oxygen atoms}/\text{cm}^3)_{\text{NTP}} = 2.69 \times 10^{19}$ . Figure 7 is an example of the output from this program. It shows the time dependence of the atmosphere in terms of the scale factor R.

Sigma is given by the equation

$$\Sigma = \frac{\bar{n}(\text{He})}{2} \sigma(\text{He}) + \left[ \frac{\bar{n}^{(0)} + 2\bar{n}^{(O_2)}}{8} + \frac{2\bar{n}^{(N_2)}}{7} \right] \sigma(0) \text{ atoms/cm.}$$

where  $\sigma(\text{He})$  and  $\sigma(0)$  are the interaction cross sections of helium and oxygen respectively. Figure 8 again illustrates output from this program. It shows  $\log_e \Sigma$  as a function of time for various values of B at an L of 1.25 earth radii.

### C. Mnemonics

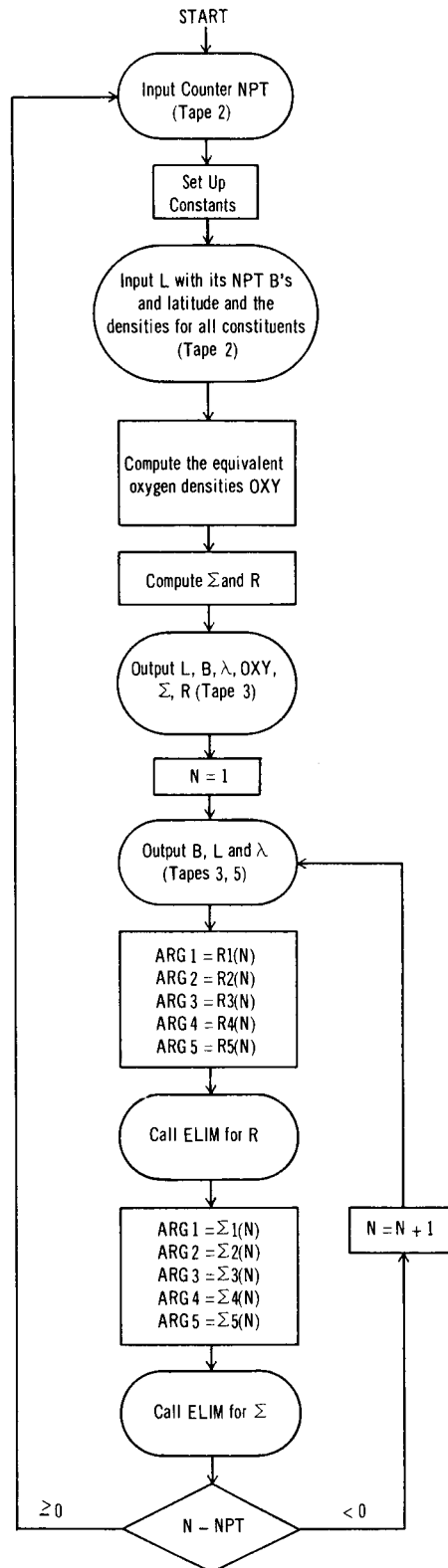
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
NPT	counter of the number of B's to a given L	-
C	(oxygen atoms/cm <sup>3</sup> ) NTP = $2.69 \times 10^{19}$	atoms/cm <sup>3</sup>
SIGHE	$\sigma(\text{He}) = .143 \times 10^{-24}$	cm <sup>2</sup>
SIGO	$\sigma(0) = .36 \times 10^{-24}$	"
EL	magnetic field line L	earth radii
B(N)	N <sup>th</sup> magnetic induction B for a given L line	gauss
ALATO(N)	latitude corresponding to B(N)	degrees
HE1(N), ..., HE5(N)	helium "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
O1(N), ..., O5(N)	oxygen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
O21(N), ..., O25(N)	molecular oxygen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
AN21(N), ..., AN25(N)	nitrogen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
H1(N), ..., H5(N)	hydrogen "bounce" averaged densities for B(N) and the five flux models	atoms/cm <sup>3</sup>
RHO1(N), ..., RHO5(N)	RHO for B(N) and the five flux models (see equation on page 105)	atoms/cm <sup>3</sup>
OXY1(N), ..., OXY5(N)	OXY for B(N) and the five flux models (see equation on page 105)	atoms/cm <sup>3</sup>
SIG1(N), ..., SIG5(N)	atmospheric loss parameter $\Sigma$ for B(N) and the five flux models	atoms/cm
RAT1(N), ..., RAT5(N)	scale factor R for B(N) and the five flux models	-
LCNT	counter to notify subroutine whether it is working with R or $\Sigma$	-
ARG1	temporary storage of RAT1 or SIG1 depending on LCNT	depends on LCNT
ARG2	temporary storage of RAT2 or SIG2 depending on LCNT	depends on LCNT
ARG3	temporary storage of RAT3 or SIG3 depending on LCNT	depends on LCNT
ARG4	temporary storage of RAT4 or SIG4 depending on LCNT	depends on LCNT
ARG5	temporary storage of RAT5 or SIG5 depending on LCNT	depends on LCNT

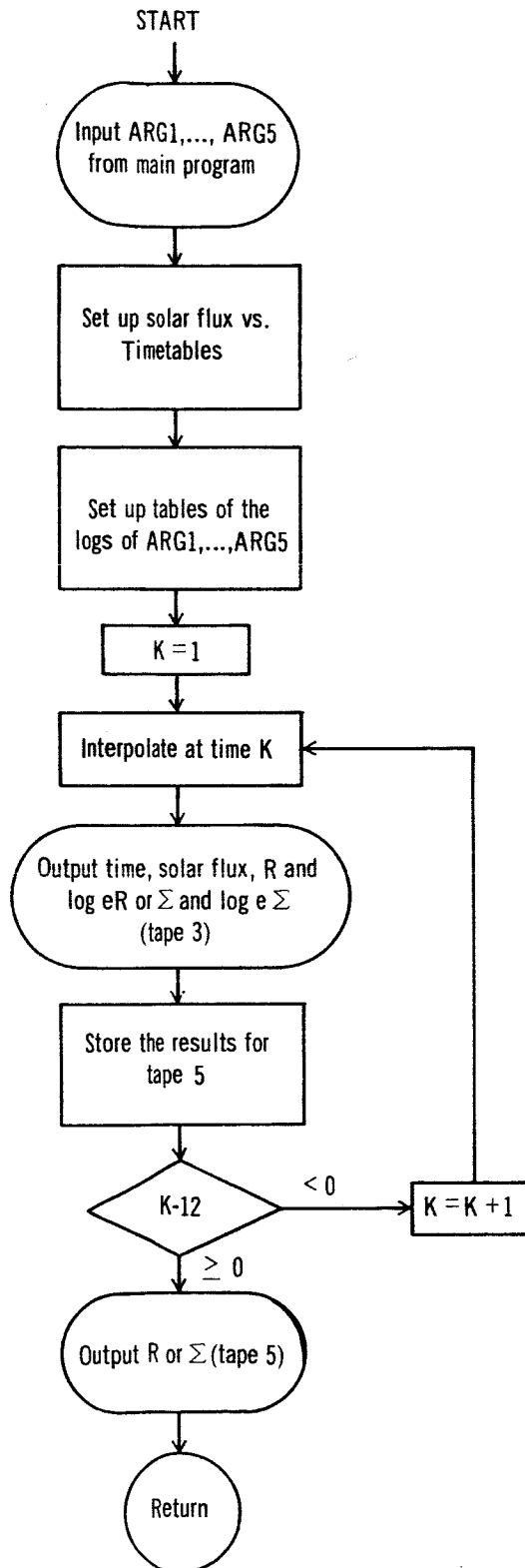


## D. Flow Charts

### 1. Main program



2. Subroutine Elim.



E. Fortran Listing

```

RATIO
C    RATIO, SIGMA CALCULATION AND FLUX ELIMINATION
DIMENSION W(12), RHC1(12), RHC2(12), RHC3(12), RHC4(12), RHC5(12), CXY1
1017, CXY2(12), CXY3(12), CXY4(12), CXY5(12), RAT1(12), RAT2(12), RAT3(12)
21, RAT4(12), RAT5(12), ALATG(12)
DIMENSION ST(12), R(5), Y(5), S(3)
DIMENSION AN21(12), AN22(12), AN23(12), AN24(12), AN25(12)
DIMENSION C1(12), C2(12), C3(12), C4(12), C5(12)
DIMENSION F1(12), F2(12), HE3(12), HE4(12), HE5(12)
DIMENSION G21(12), G22(12), G23(12), G24(12), G25(12)
DIMENSION H1(12), H2(12), F3(12), H4(12), F5(12), X5(12)
DIMENSION SIG1(12), SIG2(12), SIG3(12), SIG4(12), SIG5(12)
COMMON LUNT, ARG1, ARG2, ARG3, ARG4, ARG5
1  FORMAT (2F5.5, F8.3)
2  FORMAT (4F 0XY, 5X15C12.4)
3  FORMAT (1H1)
4  FORMAT (5E12.6)
5  FORMAT (12X, 2HL=F8.5, 4X, 2H8=F8.5, 4X, 4HLAT=F6.3)
6  FORMAT (6H RATIO, 4X, 5E12.4)
7  FORMAT (6F  SIGMA, 4X, 5E12.4//)
8  FORMAT (5E12.4)
9  FORMAT (12)
10 FORMAT (14X, 5FS=250, 7X, 5FS=200, 7X, 5FS=150, 7X, 5FS=100, 7X, 4HS=70)
11 FORMAT (5HLAT=F8.4, 4X, 2HL=F8.4, 4X, 2H8=F8.4)
12 FORMAT (3FE.4)
13 FORMAT (//)
100 READ INPUT TAPE 2, 9, NPT
WRITE OUTPUT TAPE 3, 3
C=2.65E19
SIGDE=.145E-24
SIGG=.36E-24
CC 16 N=1, NPT
READ INPUT TAPE 2, 1, EL, H(N), ALATG(N)
READ INPUT TAPE 2, 3, F1(N), F2(N), F3(N), F4(N), F5(N)
CONTINUE
CC 17 N=1, NPT
READ INPUT TAPE 2, 1, EL, H(N), ALATG(N)
READ INPUT TAPE 2, 5, G1(N), G2(N), G3(N), G4(N), G5(N)
CONTINUE
CC 18 N=1, NPT
READ INPUT TAPE 2, 1, EL, H(N), ALATG(N)
READ INPUT TAPE 2, 8, A21(N), A22(N), A23(N), A24(N), A25(N)
CONTINUE
CC 19 N=1, NPT
READ INPUT TAPE 2, 1, EL, H(N), ALATG(N)
READ INPUT TAPE 2, 8, A21(N), A22(N), A23(N), A24(N), A25(N)
CONTINUE
CC 14 N=1, NPT
READ INPUT TAPE 2, 1, FL, F(N), ALATG(N)
READ INPUT TAPE 2, 8, FL(1), F2(N), F3(N), F4(N), F5(N)
CONTINUE
CC 15 N=1, NPT
RF01(N)=14.*AN21(N)+8.*C1(N)+2.*HE1(N)+16.*C21(N)+H1(N)
RF02(N)=16.*AN22(N)+8.*G2(N)+2.*HE2(N)+16.*C22(N)+H2(N)
RF03(N)=14.*AN23(N)+8.*G3(N)+2.*FL3(N)+16.*C23(N)+F3(N)

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RH04(N)=14.*AN24(N)+8.*04(N)+2.*HL4(N)+16.*C24(N)+H4(N)
RH05(N)=14.*AN25(N)+8.*05(N)+2.*HE5(N)+16.*C25(N)+H5(N)
CONTINUE
15
DC 20 N=1,NPT
OXY1(N)=RF01(N)/8.
OXY2(N)=RF02(N)/8.
OXY3(N)=RF03(N)/8.
OXY4(N)=RF04(N)/8.
OXY5(N)=RF05(N)/8.
CONTINUE
20
DC 25 J=1,NPT
SIG1(J)=FEL(J)*SIGFE/2.+(IG1(J)+2.*G21(J))/8.+2.*AN21(J)/(.)*SIGC
SIG2(J)=FEL(J)*SIGFE/2.+(IG2(J)+2.*G22(J))/8.+2.*AN22(J)/(.)*SIGC
SIG3(J)=FEL(J)*SIGFE/2.+(IG3(J)+2.*G23(J))/8.+2.*AN23(J)/(.)*SIGC
SIG4(J)=FEL(J)*SIGFE/2.+(IG4(J)+2.*G24(J))/8.+2.*AN24(J)/(.)*SIGC
SIG5(J)=FEL(J)*SIGFE/2.+(IG5(J)+2.*G25(J))/8.+2.*AN25(J)/(.)*SIGC
CONTINUE
25
DC 30 N=1,NPT
RAT1(N)=CAY1(N)/C
RAT2(N)=CAY2(N)/C
RAT3(N)=CAY3(N)/C
RAT4(N)=CAY4(N)/C
RAT5(N)=CAY5(N)/C
CONTINUE
30
DC 40 N=1,NPT
WRITE OUTPUT TAPE 3,5,EL,0(N),ALATO(N)
WRITE OUTPUT TAPE 3,2,GXY1(N),OXY2(N),OXY3(N),OXY4(N),OXY5(N)
WRITE OUTPUT TAPE 3,6,RAT1(N),RAT2(N),RAT3(N),RAT4(N),RAT5(N)
WRITE OUTPUT TAPE 3,7,SIG1(N),SIG2(N),SIG3(N),SIG4(N),SIG5(N)
CONTINUE
40
DC 50 N=1,NPT
LCNT=0
WRITE OUTPUT TAPE 3,11,ALATO(N),EL,0(N)
WRITE OUTPUT TAPE 3,2,GXY1(N)
WRITE OUTPUT TAPE 3,6,RAT1(N)
WRITE OUTPUT TAPE 3,13
LCNT=1
ARG1=5101(N)
ARG2=5102(N)
ARG3=5103(N)
ARG4=5104(N)
ARG5=5105(N)
CALL ULIB
CONTINUE
50
END(1,1,0,0,0,0,1,0,0,0,0,0,0,0)

```

STORAGE NOT USED BY PROGRAM

DEC	LOC	DEC	LOC	DEC	LOC
1194	02252	32555	77453	32555	77454

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

ARG1	32560	77460	ARG3	32558	77456	ARG4	32557	77455	ARG5	32556	77454
LCNT	32561	77461									

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	LOC	DEC	LOC	DEC	LOC	DEC	LOC							
ALATO	1001	01751	ANZ1	562	01602	ANZ2	550	01666	ANZ3	938	01652	ANZ4	926	01636
A125	914	01622	B	1155	02251	H1	722	01322	H2	710	01306	H3	698	01272
H4	686	01256	H5	674	01242	HE1	842	01512	HE2	830	01476	HE3	818	01462
HE4	606	01446	H24	794	01432	C1	902	01506	U21	782	01416	U22	770	01402
U23	758	01366	U24	746	01352	C25	734	01336	C2	850	01572	C3	878	01556
O4	866	01542	O5	854	01526	QX1	1121	02154	QX2	1105	02125	QX3	1097	02111
CXY4	1085	02075	CXY5	1073	02061	RAT1	1061	02045	RAT2	1049	02031	RAT3	1037	02015
RAT4	1025	02001	RAT5	1013	01765	RH1	1181	02235	RH2	1169	02221	RH3	1157	02205
RPQ4	1145	02171	RPQ5	1133	02155	R	977	01721	SIG1	650	01212	SIG2	638	01176
SIG3	626	01162	SIG4	614	01146	SIG5	602	01132	S	967	01707	ST	989	01735
XS	652	01226	Y	972	01714									

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC	LOC	DEC	LOC	DEC	LOC									
C	580	01116	EL	589	01115	NPT	588	01114	SIGHE	587	01113	SIGD	586	01112

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN	LOC	EFN	LOC	EFN	LOC	EFN	LOC							
011	1	01104	012	2	01101	013	3	01075	014	4	01074	015	5	01072
016	6	01063	017	7	01057	018	8	01052	019	9	01050	01A	10	01047
01B	11	01035	01C	12	01026	01D	13	01024						

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	LOC	DEC	LOC	DEC	LOC									
1)	581	01105	2)	513	01001	3)	518	01006	4)	32767	77777	6)	526	01016

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	LOC	DEC	LOC	DEC	LOC									
ELIM	5	00005	(FIL)	4	00004	(FPT)	0	00000	(RTN)	2	00002	(STP)	3	00003
(TSH)	1	00001												

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

ELIP	(FIL)	(FPT)	(RTN)	(STP)	(TSH)
------	-------	-------	-------	-------	-------



```

C SUBROUTINE IG_ELIMINATE SOLAR FLUX
SUBROUTINE ELIM
DIMENSION ST(12),R(5),Y(5),S(5),XS(12)
COMMON LUNT,ARG1,ARG2,ARG3,ARG4,ARG5
1 FORMAT (//////)
2 FORMAT(5E12.6)
3 FORMAT(I3,4X,IF10,2,2E20.5)
4 FORMAT (5H TIME,7X,5HSOLAR,12X,6HLOG OF,13X,5HRATIO/6H (YRS),6X,4F
1FLUX,13X,5HRATIO)
5 FORMAT (5H TIME,7X,5HSOLAR,12X,6HLOG OF,13X,5HSIGMA/6H (YRS),6X,4F
1FLUX,13X,5HSIGMA)
6 FORMAT(6E10.4)
R(1) = ARG1
R(2) = ARG2
R(3) = ARG3
R(4) = ARG4
R(5) = ARG5
ST(1) = 70.
ST(2) = 75.
ST(3) = 130.
ST(4) = 230.
ST(5) = 250.
ST(6) = 220.
ST(7) = 185.
ST(8) = 140.
ST(9) = 105.
ST(10) = 90.
ST(11) = 75.
ST(12) = 70.
S(1) = 250.
S(2) = 200.
S(3) = 150.
S(4) = 100.
S(5) = 70.
IF (LUNT) 14,14,17
GO TO 18
17 WRITE OUTPUT TAPE 3,5
18 DO 20, J=1,5
A=R(J)
Y(J)=LUGF(A)
CONTINUE
DO 30, K=1,12
HA=ST(K)
IF(HA-250.)40,41,41
IF(HA-70.)42,42,43
40 ANS=Y(1)
41 GO TO 1000
42 ANS=Y(5)
43 GO TO 1000
44 DO 50, J=1,5
IF(HA-S(J))50,51,52
51 ANS=Y(J)
52 GO TO 1000
53 HI=S(J)

```

```

YI=Y(J)
HO=S(J-1)
YO=Y(J-1)
ANS=YI-(YI-YO)*(H1-HA)/(H1-HO)
GO TO 1000
50 CONTINUE
1000 X=EXP(ANS)

ITIME=A-1
WRITE OUTPUT TAPE 3,3,ITIME,HA,ANS,X
XS(K)=X
CONTINUE
WRITE OUTPUT TAPE 3,1
WRITE OUTPUT TAPE 5,6,XS(1),XS(2),XS(3),XS(4),XS(5),XS(6)
WRITE OUTPUT TAPE 5,6,XS(7),XS(8),XS(9),XS(10),XS(11),XS(12)
RETURN
END(1,1,0,0,0,0,0,0,0,0,0,0)

```



STORAGE NOT USED BY PROGRAM

```

DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT
324  C0304    32555  77453    ARG2  32559  77457    ARG3  32558  77456    ARG4  32557  77455    ARG5  32556  77454
LONT 32561  77461

```

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

```

DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT
ARG1 32560  77460    ARG2  32559  77457    ARG3  32558  77456    ARG4  32557  77455    ARG5  32556  77454
LONT 32561  77461

```

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

```

DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT
R    311  C0467    S    301  00455    ST   323  00503    XS   296  C0450    Y    306  00462

```

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

```

DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT
ANS  284  C0434    A    283  00433    F0   282  00432    F1   281  C0431    HA   280  00430
ITIRE 279  C0427    J    278  C0426    K    277  00425    X    276  C0424    YC   275  C0423
Y1    274  C0422

```

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

```

EFN  LCC      EFN  LCC      EFN  LCC      EFN  LCC      EFN  LCC
011   1  C0414    012   2  00412    013   3  00410    014   4  C0404    015   5  00367
016   6  C0352

```

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

```

DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT
011   1  C0414    012   2  00412    013   3  00410    014   4  C0404    015   5  00367
016   6  C0352

```

LOCATIONS OF NAMES IN TRANSFER VECTOR

```

DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT      DEC  CCT
EXP  3  C0003    LOG  2  C0002    (FIL) 1  00001    (STH) 0  C0000

```

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

```

EXP  LOG      (FIL)      (STH)

```

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

```

EFN  LCC      EFN  LCC      EFN  LCC      EFN  LCC      EFN  LCC      EFN  LCC
14   34  C0074    17   36  C0101    18   37  00105    20   40  C0115    40   44  C0131
41   43  C0136    42   47  C0141    43   49  00144    51   51  00154    52   53  00161
50   55  C0212    1000  60  C0216    30   65  C0250

```

## F. Input

Input to this program are the "bounce" average density cards together with the B-L- $\lambda$  cards output from the last program. The cards are rearranged by L line rather than by constituent as they have been arranged in previous programs. A counter card must again be inserted in order to inform the computer of the number of card pairs per constituent for a given L-line. All input is on tape 2. For a given L-line the constituents must be in the following order:

- (1) helium,
- (2) oxygen,
- (3) molecular oxygen,
- (4) nitrogen,
- (5) hydrogen.

### 1. Input Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
Counter Card	1-2	I	NPT	-	B-L- $\lambda$ and density card pair counter
B-L- $\lambda$ Card	1-8	F	EL	earth radii	magnetic field line
	9-16	F	B	gauss	magnetic induction
	17-24	F	ALATO	degrees	latitude
	73-80	-	-	-	constituent name
Density Card	1-12	E	*	atoms/cm <sup>3</sup>	density for flux model 1
	13-24	E	*	"	density for flux model 2
	25-36	E	*	"	density for flux model 3
	37-48	E	*	"	density for flux model 4
	49-60	E	*	"	density for flux model 5
	73-80	-	-	-	constituent name

\* All of the five constituents use the same card format here. Therefore the quantity on a given density card (HE, O, O<sub>2</sub>, N<sub>2</sub> or H) will depend on the constituent name listed in columns 73-80 of that same card.



## G. Output

Output for this program occurs on tapes 3 and 5. Tape 3 contains two groups of data for each L. The first group lists the values of R,  $\Sigma$  and OXY as functions of position and flux model. The second group contains R,  $\log_e R$ ,  $\Sigma$ ,  $\log_e \Sigma$  and solar flux as functions of position and time.

On tape 5 is the data to be punched for use in the conservation equation calculation. Each B-L- $\lambda$  card is followed by two R cards which are followed in turn by two  $\Sigma$  cards.

### 1. Tape 3 Sample

	S=250	S=200	S=150	S=100	S=70
	L= 1.14200	B= 0.25376	LAT= 8.973		
OXY	0.5479E-11	0.5975E-11	0.6824E-11	0.8475E-11	0.1046E-12
RATIO	0.2037E-08	0.2221E-08	0.2537E-08	0.3151E-08	0.3889E-08
SIGMA	0.3331E-14	0.3303E-14	0.3765E-14	0.4672E-14	0.5757E-14

	S=250	S=200	S=150	S=100	S=70
	L= 1.14200	B= 0.22394	LAT= 6.973		
OXY	0.3250E-09	0.2545E-09	0.1835E-09	0.1138E-09	0.7492E-09
RATIO	0.1208E-10	0.9452E-11	0.6822E-11	0.4231E-11	0.2765E-11
SIGMA	0.1765E-15	0.1379E-16	0.9706E-17	0.6101E-17	0.3984E-17

	S=250	S=200	S=150	S=100	S=70
	L= 1.14200	B= 0.21680	LAT= 4.973		
OXY	0.1631E-08	0.9954E-07	0.5278E-07	0.2141E-07	0.1007E-07
RATIO	0.6065E-12	0.3700E-12	0.1962E-12	0.7958E-13	0.3744E-13
SIGMA	0.8406E-18	0.5144E-18	0.2747E-18	0.1145E-18	0.5633E-19

	S=250	S=200	S=150	S=100	S=70
	L= 1.14200	B= 0.21215	LAT= 2.973		
OXY	0.1731E-07	0.8997E-06	0.3982E-06	0.1296E-06	0.5424E-05
RATIO	0.6435E-13	0.3345E-13	0.1480E-13	0.4816E-14	0.2016E-14
SIGMA	0.1023E-18	0.5969E-19	0.3173E-19	0.1425E-19	0.7878E-20

	S=250	S=200	S=150	S=100	S=70
	L= 1.14200	B= 0.20988	LAT= 0.973		
OXY	0.3371E-06	0.1677E-05	0.7598E-05	0.2981E-05	0.1557E-05
RATIO	0.1253E-13	0.6232E-14	0.2624E-14	0.1108E-14	0.5789E-15
SIGMA	0.3255E-19	0.2143E-19	0.1314E-19	0.6810E-20	0.3927E-20

LAT= 8.9730 L= 1.1420 B= 0.2338

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.19365E 02	0.38892E-08
1	75.00	-0.19400E 02	0.37550E-08
2	130.00	-0.19706E 02	0.27666E-08
3	230.00	-0.19977E 02	0.21087E-08
4	250.00	-0.20012E 02	0.20368E-08
5	220.00	-0.19960E 02	0.21457E-08
6	185.00	-0.19885E 02	0.23118E-08
7	140.00	-0.19749E 02	0.26492E-08
8	105.00	-0.19597E 02	0.30832E-08
9	90.00	-0.19505E 02	0.33798E-08
10	75.00	-0.19400E 02	0.37550E-08
11	70.00	-0.19365E 02	0.38892E-08

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.32788E 02	0.57570E-14
1	75.00	-0.32823E 02	0.55601E-14
2	130.00	-0.33126E 02	0.41067E-14
3	230.00	-0.33396E 02	0.31370E-14
4	250.00	-0.33430E 02	0.30307E-14
5	220.00	-0.33378E 02	0.31915E-14
6	185.00	-0.33304E 02	0.34365E-14
7	140.00	-0.33169E 02	0.39339E-14
8	105.00	-0.33019E 02	0.45726E-14
9	90.00	-0.32928E 02	0.50088E-14
10	75.00	-0.32823E 02	0.55601E-14
11	70.00	-0.32788E 02	0.57570E-14

LAT= 6.9730 L= 1.1420 B= 0.2239

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.26607E 02	0.27852E-11
1	75.00	-0.26537E 02	0.29862E-11
2	130.00	-0.25902E 02	0.56356E-11
3	230.00	-0.25237E 02	0.10957E-10
4	250.00	-0.25139E 02	0.12083E-10
5	220.00	-0.25286E 02	0.10434E-10
6	185.00	-0.25482E 02	0.85774E-11
7	140.00	-0.25806E 02	0.62006E-11
8	105.00	-0.26141E 02	0.44381E-11
9	90.00	-0.26328E 02	0.36806E-11
10	75.00	-0.26537E 02	0.29862E-11
11	70.00	-0.26607E 02	0.27852E-11

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.40064E 02	0.39844E-17
1	75.00	-0.39993E 02	0.42776E-17
2	130.00	-0.39347E 02	0.81603E-17
3	230.00	-0.38675E 02	0.15991E-16
4	250.00	-0.38576E 02	0.17648E-16
5	220.00	-0.38724E 02	0.15221E-16
6	185.00	-0.38922E 02	0.12488E-16
7	140.00	-0.39250E 02	0.89911E-17
8	105.00	-0.39590E 02	0.64039E-17
9	90.00	-0.39780E 02	0.52931E-17
10	75.00	-0.39993E 02	0.42776E-17
11	70.00	-0.40064E 02	0.39844E-17

LAT= 4.9730 L= 1.1420 B= 0.2168

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.30916E 02	0.37441E-13
1	75.00	-0.30790E 02	0.42455E-13
2	130.00	-0.29620E 02	0.13677E-12
3	230.00	-0.28329E 02	0.49772E-12
4	250.00	-0.28131E 02	0.60649E-12
5	220.00	-0.28428E 02	0.45089E-12
6	185.00	-0.28815E 02	0.30591E-12
7	140.00	-0.29440E 02	0.16382E-12
8	105.00	-0.30072E 02	0.87100E-13
9	90.00	-0.30413E 02	0.61897E-13
10	75.00	-0.30790E 02	0.42455E-13
11	70.00	-0.30916E 02	0.37441E-13

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.44323E 02	0.56327E-19
1	75.00	-0.44205E 02	0.63395E-19
2	130.00	-0.43089E 02	0.19356E-18
3	230.00	-0.41817E 02	0.69067E-18
4	250.00	-0.41620E 02	0.84064E-18
5	220.00	-0.41915E 02	0.62604E-18
6	185.00	-0.42300E 02	0.42613E-18
7	140.00	-0.42914E 02	0.23059E-18
8	105.00	-0.43526E 02	0.12495E-18
9	90.00	-0.43850E 02	0.90378E-19
10	75.00	-0.44205E 02	0.63395E-19
11	70.00	-0.44323E 02	0.56327E-19

LAT= 2.9730 L= 1.1420 B= 0.2121

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.33838E 02	0.20163E-14
1	75.00	-0.33692E 02	0.23311E-14
2	130.00	-0.32293E 02	0.94462E-14
3	230.00	-0.30636E 02	0.49528E-13
4	250.00	-0.30374E 02	0.64346E-13
5	220.00	-0.30767E 02	0.43452E-13
6	185.00	-0.31273E 02	0.26189E-13
7	140.00	-0.32069E 02	0.11824E-13
8	105.00	-0.32855E 02	0.53884E-14
9	90.00	-0.33257E 02	0.36028E-14
10	75.00	-0.33692E 02	0.23311E-14
11	70.00	-0.33838E 02	0.20163E-14

TIME (YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.46290E 02	0.78783E-20
1	75.00	-0.46191E 02	0.86967E-20
2	130.00	-0.45217E 02	0.23039E-19
3	230.00	-0.43942E 02	0.82457E-19
4	250.00	-0.43727E 02	0.10228E-18
5	220.00	-0.44050E 02	0.74037E-19
6	185.00	-0.44455E 02	0.49381E-19
7	140.00	-0.45057E 02	0.27037E-19
8	105.00	-0.45617E 02	0.15442E-19
9	90.00	-0.45895E 02	0.11698E-19
10	75.00	-0.46191E 02	0.86967E-20
11	70.00	-0.46290E 02	0.78783E-20

LAT= 0.9730 L= 1.1420 B= 0.2099

TIME (YRS)	SOLAR FLUX	LOG OF RATIO	RATIO
0	70.00	-0.35085E 02	0.57888E-15
1	75.00	-0.34977E 02	0.64504E-15
2	130.00	-0.33875E 02	0.19426E-14
3	230.00	-0.32290E 02	0.94762E-14
4	250.00	-0.32011E 02	0.12530E-13
5	220.00	-0.32430E 02	0.82409E-14
6	185.00	-0.32946E 02	0.49151E-14
7	140.00	-0.33688E 02	0.23424E-14
8	105.00	-0.34343E 02	0.12167E-14
9	90.00	-0.34653E 02	0.89241E-15
10	75.00	-0.34977E 02	0.64504E-15
11	70.00	-0.35085E 02	0.57888E-15



TIME YRS)	SOLAR FLUX	LOG OF SIGMA	SIGMA
0	70.00	-0.46986E 02	0.39268E-20
1	75.00	-0.46895E 02	0.43043E-20
2	130.00	-0.46041E 02	0.10104E-19
3	230.00	-0.45039E 02	0.27541E-19
4	250.00	-0.44872E 02	0.32550E-19
5	220.00	-0.45122E 02	0.25333E-19
6	185.00	-0.45436E 02	0.18509E-19
7	140.00	-0.45910E 02	0.11524E-19
8	105.00	-0.46370E 02	0.72732E-20
9	90.00	-0.46619E 02	0.56685E-20
10	75.00	-0.46855E 02	0.43043E-20
11	70.00	-0.46986E 02	0.39268E-20

2. Tape 5

a. Output Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
B-L- $\lambda$	1-8	F	ALATO	degrees	latitude
	9-16	F	EL	earth radii	magnetic field line
	17-24	F	B	gauss	magnetic induction
1st R Card	1-10	E	XS(1)	-	R for time 0
	11-20	E	XS(2)	-	R for time 1
	21-30	E	XS(3)	-	R for time 2
	31-40	E	XS(4)	-	R for time 3
	41-50	E	XS(5)	-	R for time 4
	51-60	E	XS(6)	-	R for time 5
2nd R Card	1-10	E	XS(7)	-	R for time 6
	11-20	E	XS(8)	-	R for time 7
	21-30	E	XS(9)	-	R for time 8
	31-40	E	XS(10)	-	R for time 9
	41-50	E	XS(11)	-	R for time 10
	51-60	E	XS(12)	-	R for time 11
1st $\Sigma$ Card	1-10	E	XS(1)	atoms/cm	$\Sigma$ for time 0
	11-20	E	XS(2)	"	$\Sigma$ for time 1
	21-30	E	XS(3)	"	$\Sigma$ for time 2
	31-40	E	XS(4)	"	$\Sigma$ for time 3
	41-50	E	XS(5)	"	$\Sigma$ for time 4
	51-60	E	XS(6)	"	$\Sigma$ for time 5

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
2nd $\Sigma$ Card	1-10	E	XS(7)	atoms/cm	$\Sigma$ for time 6
	11-20	E	XS(8)	"	$\Sigma$ for time 7
	21-30	E	XS(9)	"	$\Sigma$ for time 8
	31-40	E	XS(10)	"	$\Sigma$ for time 9
	41-50	E	XS(11)	"	$\Sigma$ for time 10
	51-60	E	XS(12)	"	$\Sigma$ for time 11

This five card group is repeated for each new B and L.

b. Sample

GENERAL PURPOSE DATA SHEET

Problem		OUTPUT - R, Σ CALCULATION AND FLUX ELIMINATION	
Spencer	TAPE 5	Date	SAMPLE
			Page of
1			
2			
3			
4			
5			
6			
7			
8	9730	1.1420	0.2338
9	0.3889E-080	0.3755E-080	0.2767E-080
10	0.2312E-080	0.2649E-080	0.3083E-080
11	0.5757E-140	0.5560E-140	0.4107E-140
12	0.3437E-140	0.3934E-140	0.4573E-140
13	6.9730	1.1420	0.2239
14	0.2785E-110	0.2986E-110	0.5636E-110
15	0.8577E-110	0.6201E-110	0.4438E-110
16	0.3984E-170	0.4278E-170	0.8160E-170
17	0.1249E-160	0.8991E-170	0.6404E-170
18	4.9730	1.1420	0.2168
19	0.3744E-130	0.4245E-130	0.1368E-120
20	0.3059E-120	0.1638E-120	0.8710E-130
21	0.5633E-190	0.6339E-190	0.1936E-180
22	0.4261E-180	0.2306E-180	0.1250E-180
23	2.9730	1.1420	0.2121
24	0.2016E-140	0.2331E-140	0.9446E-140
25	0.2619E-130	0.1182E-130	0.5388E-140
26	0.7878E-200	0.8697E-200	0.2304E-190
27	0.4938E-190	0.2704E-190	0.1544E-190
28	0.9730	1.1420	0.2099
29	0.5789E-150	0.6450E-150	0.1943E-140
30	0.4915E-140	0.2342E-140	0.1217E-140
31	0.3927E-200	0.4304E-200	0.1010E-190
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71			
72			
73			
74			
75			
76			
77			
78			
79			
80			

## H. Running Time

The running time for this program will be about three minutes for every L line.

## VII. CONSERVATION EQUATION CALCULATION

### A. Introduction

This program studies the build-up of proton density by use of the conservation equation (see equation (1)). Several lines of action are available. Either a transient or a time-averaged steady state solution can be calculated for any of 15 desired energy levels without altering the program.

In the transient steady-state solution the conservation equation is integrated as a function of time for a particular energy level until maximum and minimum values of the densities start repeating from one solar cycle to another. At this point the cycle number is recorded together with the time of the maximum and minimum densities. These values are printed with the maximum and minimum density and flux values as well as with the ratio of the maximum flux to the minimum flux. In addition, when calculating the transient steady-state solution, one may have the time history of any one of the energy levels printed on tape 5 with as many points as desired.

In the time-averaged steady-state solution the condition  $dN_p/dt = 0$  yields a density equation for density  $N_p$  which is solved using the relative neutron source strength  $\Phi$  together with  $\Sigma$  and  $R$  from the last program. All these values are averaged over time for this solution of the conservation equation.

Three subroutines assist the main program: subroutine RUNGE is used in integrating by the Runge Kutta technique, subroutine DERIV is used to evaluate  $dN_p/dt$  for a given  $t$  and  $N_p$  and subroutine TABLE interpolates any given table either logarithmically or linearly.

### B. Equations

The form of the particle conservation equation used for the study of the proton population as a function of time is given by

$$\frac{dN_p}{dt} = C_0 \Phi - C_1 N_p \left( \frac{dE}{dx} \right) - C_2 N_p \frac{d}{dE} \left( \frac{dE}{dx} \right) - C_2 N_p \Sigma \quad (1)$$

where  $\frac{dE}{dx}$ ,  $\frac{d}{dE} \left( \frac{dE}{dx} \right)$ ,  $\Phi$  and  $\Sigma$  are the quantities to be supplied and where:

$N_p$  = density

$$C_0 = A_0 / L^2 E^{B_0} \cos^4 \lambda_0$$

$$C_1 = A_1 / E^{B_1}$$

$$C_2 = A_2 E^{B_2}$$

$E$  = Energy

$A_0, \dots, A_2$  = high or low energy conservation equation coefficients depending on whether  $E > 80$  Mev. or  $E \leq 80$  Mev. respectively

$B_0, \dots, B_2$  = " " " " " " " " " " " " "

$\lambda_0$  = mirror latitude

The condition  $dN_p/dt = 0$  yields the equation for the time averaged steady state proton density:

$$N_p = \frac{A_0 \Phi}{L^2 E^{B_0} \left[ \frac{A_1}{E^{B_1}} \left( \frac{dE}{dX} \right) + A_2 E^{B_2} \frac{d}{dE} \left( \frac{dE}{dX} \right) + A_2 E^{B_2} \Sigma \right] \cos^4 \lambda_0}$$

where  $\Phi$ ,  $\Sigma$  and the scale factor  $R$  used in calculating  $dE/dx$  and  $d/dE (dE/dx)$  are all averaged over time.

The density  $N_p$  gives a flux by the equation:

$$\text{Flux} = 2C_2 N_p = N_p v$$

where  $v$  is the neutron velocity factor.

### C. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
TIME(J)	Abscissa of time in increments of years for 12 years	years
ELOSS(J)	dE/dk corresponding to E(J) (see Figure 11)	Mev/cm.
E(J)	energy corresponding to ELOSS(J) "	Mev.
CONVM	conversion factor - months to seconds	-
ALO	$A_0$ for $E \leq 80$ Mev. (see page 130)	$\frac{\# \text{ protons}}{\text{cm. sec. Mev.}}$
AL1	$A_1$ " " "	cm./sec.
AL2	$A_2$ " " "	cm./Mev <sup>2</sup> /sec.
AH0	$A_0$ for $E > 80$ Mev. (see page 130)	$\frac{\# \text{ protons}}{\text{cm. sec. Mev.}}$
AH1	$A_1$ " " "	cm./sec.
AH2	$A_2$ " " "	cm./Mev <sup>2</sup> /sec.
BL0	$B_0$ for $E \leq 80$ Mev. (see page 130)	-
BL1	$B_1$ " " "	-
BL2	$B_2$ " " "	-
BH0	$B_0$ for $E > 80$ Mev. (see page 130)	-
BH1	$B_1$ " " "	-
BH2	$B_2$ " " "	-
DELOSS(J)	d(dE/dx)/dE corresponding to DE(J) (see Figure 12)	cm. <sup>-1</sup>
DE(J)	energy corresponding to DELOSS(J) (see Figure 12)	Mev.



<u>Quantity</u>	<u>Description</u>	<u>Units</u>
PREL(J)	$\phi$ for TIME(J) (see page 130 and Figure 11)	-
AVPRL	simple average of PREL(1), ..., PREL(12)	-
ALAT	mirror latitude $\lambda_0$	degrees
EL	magnetic field line L	earth radii
B	magnetic induction B	gauss
CONVR	conversion factor - degrees to radians	-
ALATO	ALAT in radians	radians
CSLAT4	$\cos^4(\text{ALATO})$	-
ELEL	$L^2$	(earth radii) <sup>2</sup>
R(I)	atmospheric scale factor R for TIME(I)	-
SIG(I)	atmospheric loss parameter $\Sigma$ for TIME(I)	atoms/cm.
ENO	initial density $N_{p_0}$ for integration	# protons/cm <sup>3</sup>
TSUBO	initial time $t_0$ for integration	months
DT1	integration interval for ICSUBO	months
DT2	integration interval for all other cycles	months
TEND	end limit on integration	months
IEST	initial energy level subscript	-
IEDEL	increment for energy level subscript	-
IEEND	final energy level subscript	-
IEPR	subscript of energy level whose time history is desired	-

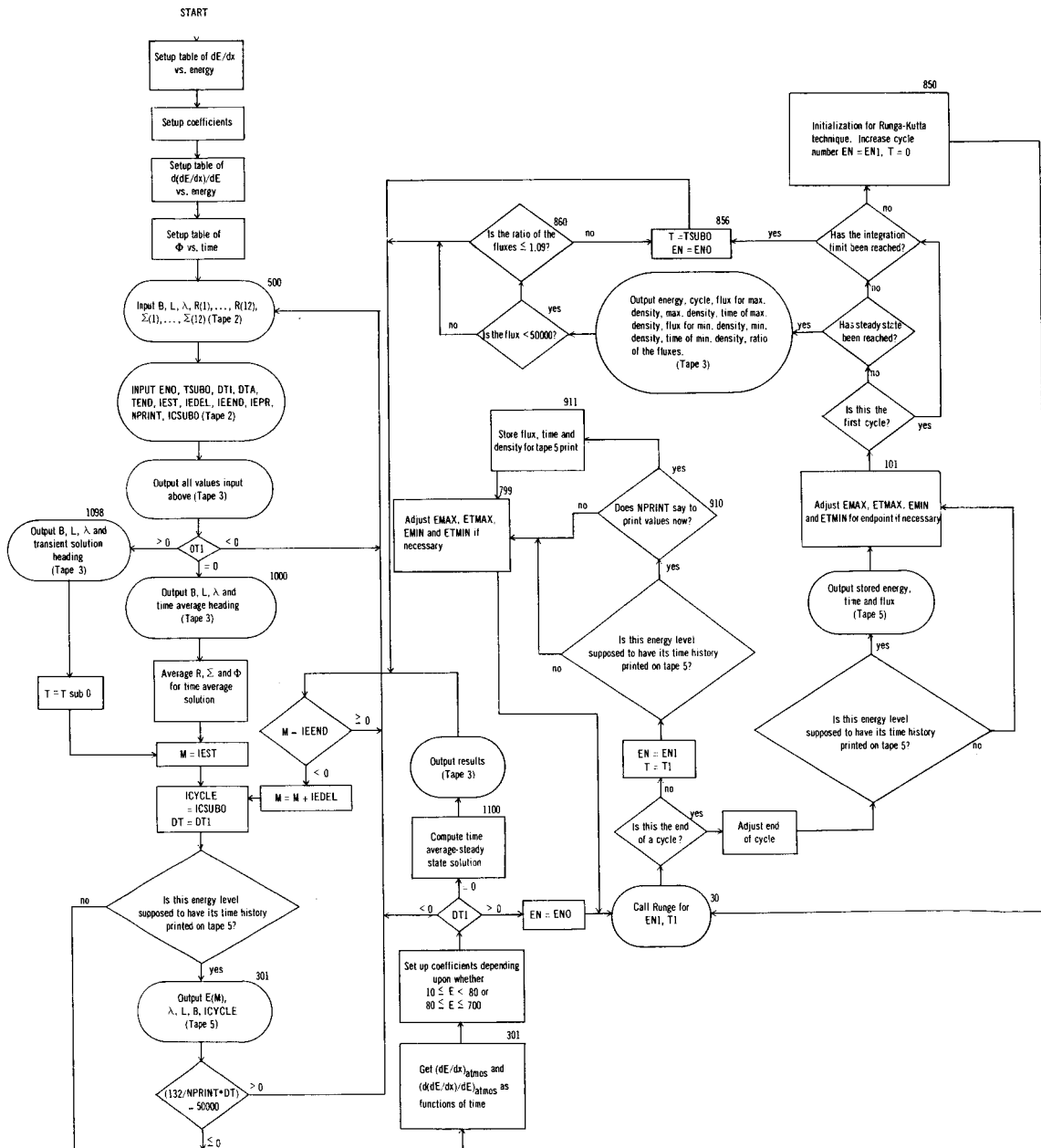
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
NPRINT	a control factor for the time history print on tape 5. Density and flux are given for every NPRINT increments in time. (See Restriction (1)).	-
ICSUBO	initial cycle number corresponding to ENO and TSUBO	-
SUMR	sum of R(1), ..., R(12)	-
AVR	simple average of R(1), ..., R(12)	-
SUMSIG	sum of SIG(1), ..., SIG(12)	atoms/cm
AVSIG	simple average of SIG(1), ..., SIG(12)	atoms/cm
T	time	months
TMAX	time of an eleven year cycle - 132 months	months
TCK	time check to see if TEND has been reached	months
DT	increment in time	months
ICYCLE	cycle number	-
EMAX(J)	maximum density for cycle J	atoms/cm <sup>3</sup>
EMIN(J)	minimum density for cycle J	atoms/cm <sup>3</sup>
ETMAX(J)	time at EMAX(J)	months
ETMIN(J)	time at EMIN(J)	months
M	subscript to indicate the energy level which is under consideration	-
ENER	energy level M under consideration	Mev.
ITEST3	test value to see if the energy level under consideration is to have its time history printed on tape 5	-

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
ALOSS	temporary storage of ELOSS(M)	Mev./cm.
X(1), ...,		
X(15)	temporary storage of DE(1), ..., DE(15)	Mev
Y(1), ...,		
Y(15)	temporary storage of DELOSS(1), ..., DELOSS(15)	cm <sup>-1</sup>
ALOSSA(J)	(dE/dx) × R(J) for energy ENER	Mev./cm.
DLOSSA(J)	(d(dE/dx)/dE) × R(J) for energy ENER	cm <sup>-1</sup>
A0	temporary storage of ALO or AHO	$\frac{\# \text{ protons}}{\text{cm. sec. Mev.}}$
A1	temporary storage of AL1 or AH1	cm/sec
A2	temporary storage of AL2 or AH2	cm/Mev <sup>2</sup> sec
B0	temporary storage of BL0 or BH0	-
B1	temporary storage of BL1 or BH1	-
B2	temporary storage of BL2 or BH2	-
C0	conservation equation coefficient (see page 129)	$\frac{\# \text{ protons/cm}^3}{\text{sec Mev.}}$
C1	conservation equation coefficient (see page 129)	cm/sec. Mev.
C2	conservation equation coefficient (see page 129)	cm/sec. Mev.
DEDX	temporary storage of ALOSSA(J)	Mev./cm.
DDEDX	temporary storage of DLOSSA(J)	cm <sup>-1</sup>

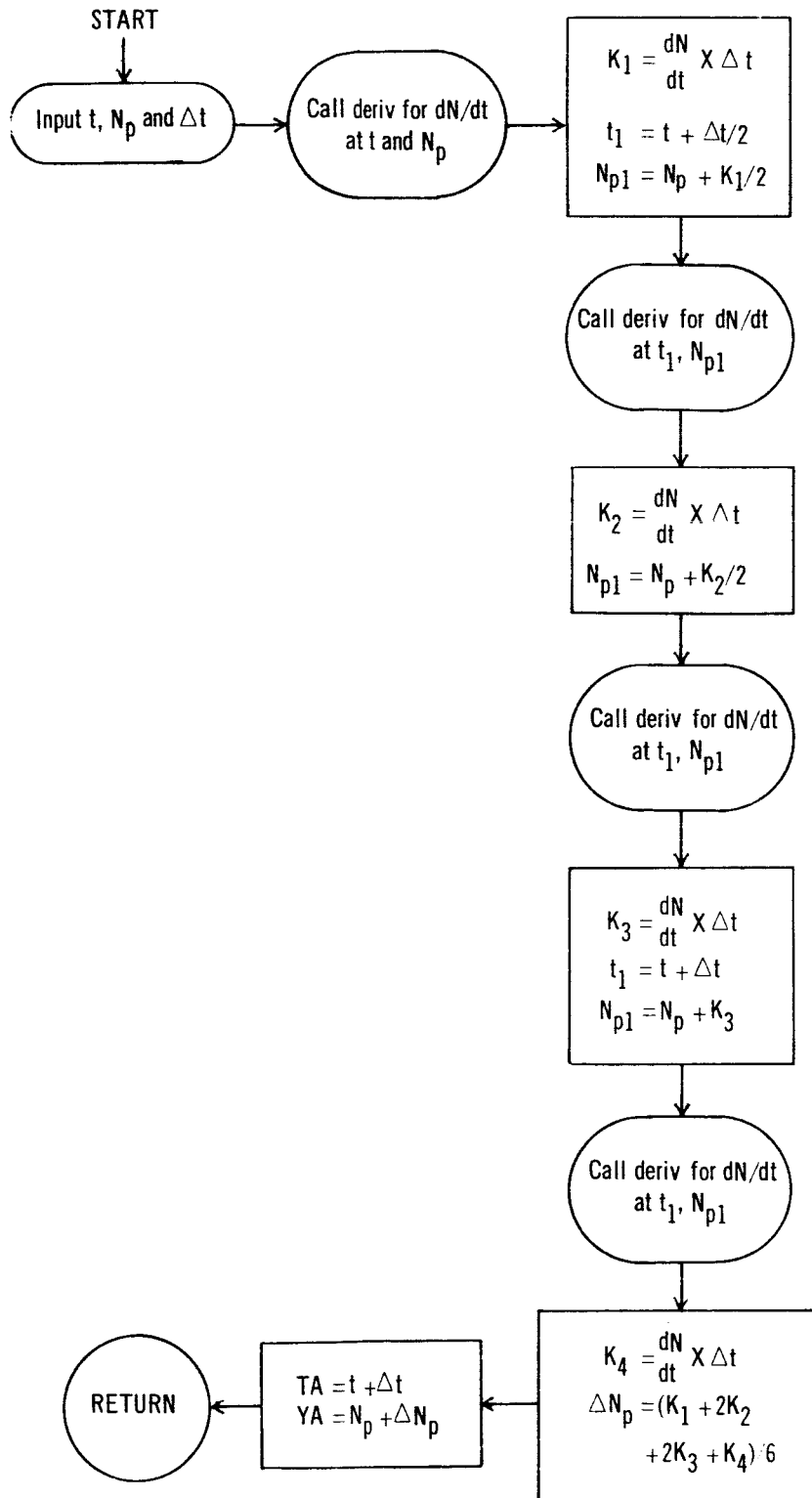
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
DENS	proton density $N_p$	# protons/cm <sup>3</sup> Mev.
FLUX	proton flux	# protons/cm <sup>2</sup> sec. Mev.
NP	counter of the increments in time; used as a check for NPRINT	-
N5	counter of the number of prints on tape 5	-
EN	proton density $N_p$	atoms/cm <sup>3</sup> Mev
ICYM1	the value ICYCLE-1 used in testing for steady-state	-
TEST1	test to see if steady state has been reached	-
TEST2	test to see if steady state has been reached	-
EPR1	minimum density in cycle ICYM1	# protons/cm <sup>3</sup> Mev.
FLPR1	flux for EPR1	# protons/cm <sup>2</sup> sec. Mev.
TPR1	time of EPR1	months
EPR2	maximum density in cycle ICYM1	# protons/cm <sup>3</sup> Mev.
FLPR2	flux for EPR2	# protons/cm <sup>2</sup> sec. Mev.
TPR2	time of EPR2	months
RATIO	ratio of FLPR2 to FLPR1	-

## D. Flow Chart

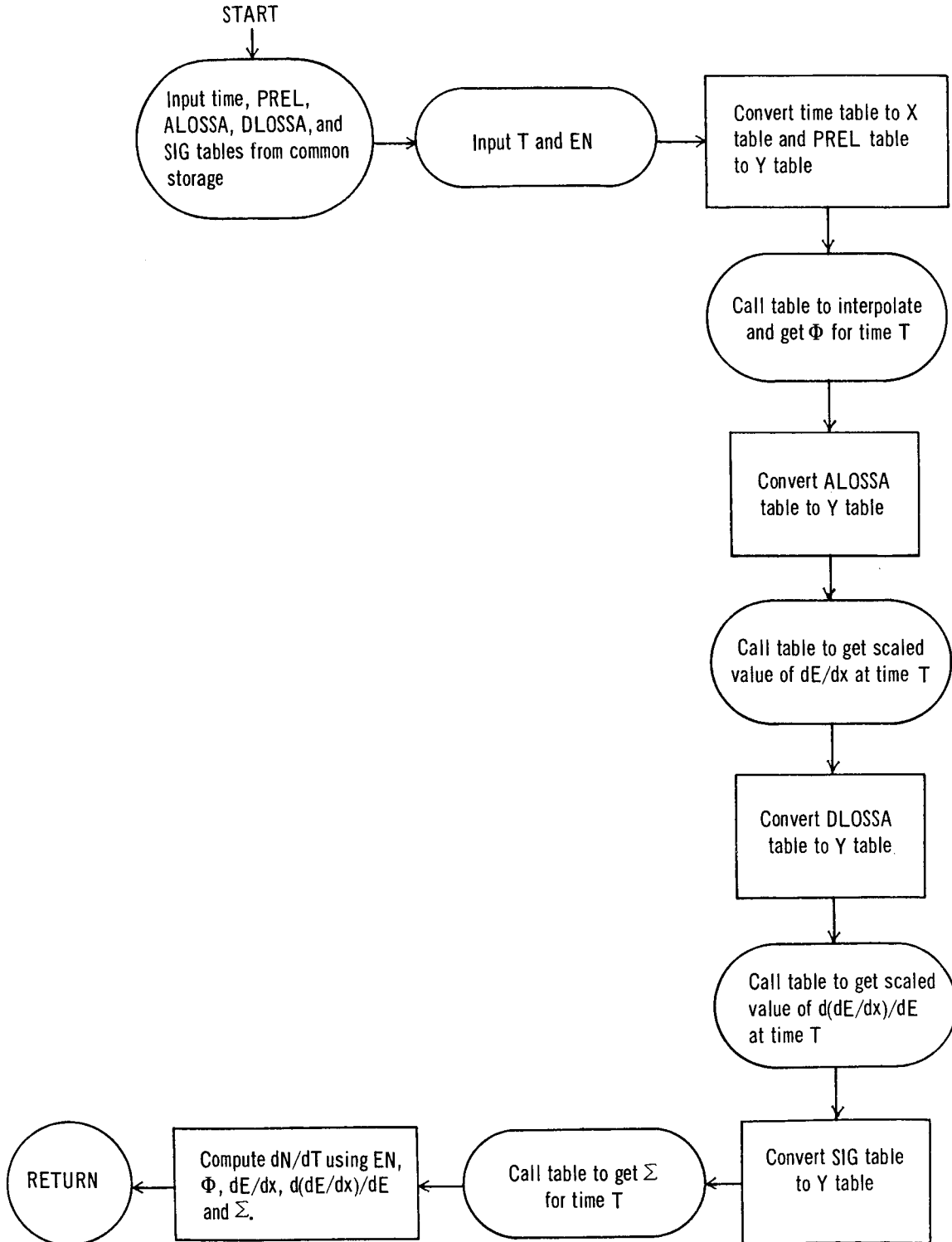
### 1. Main Program



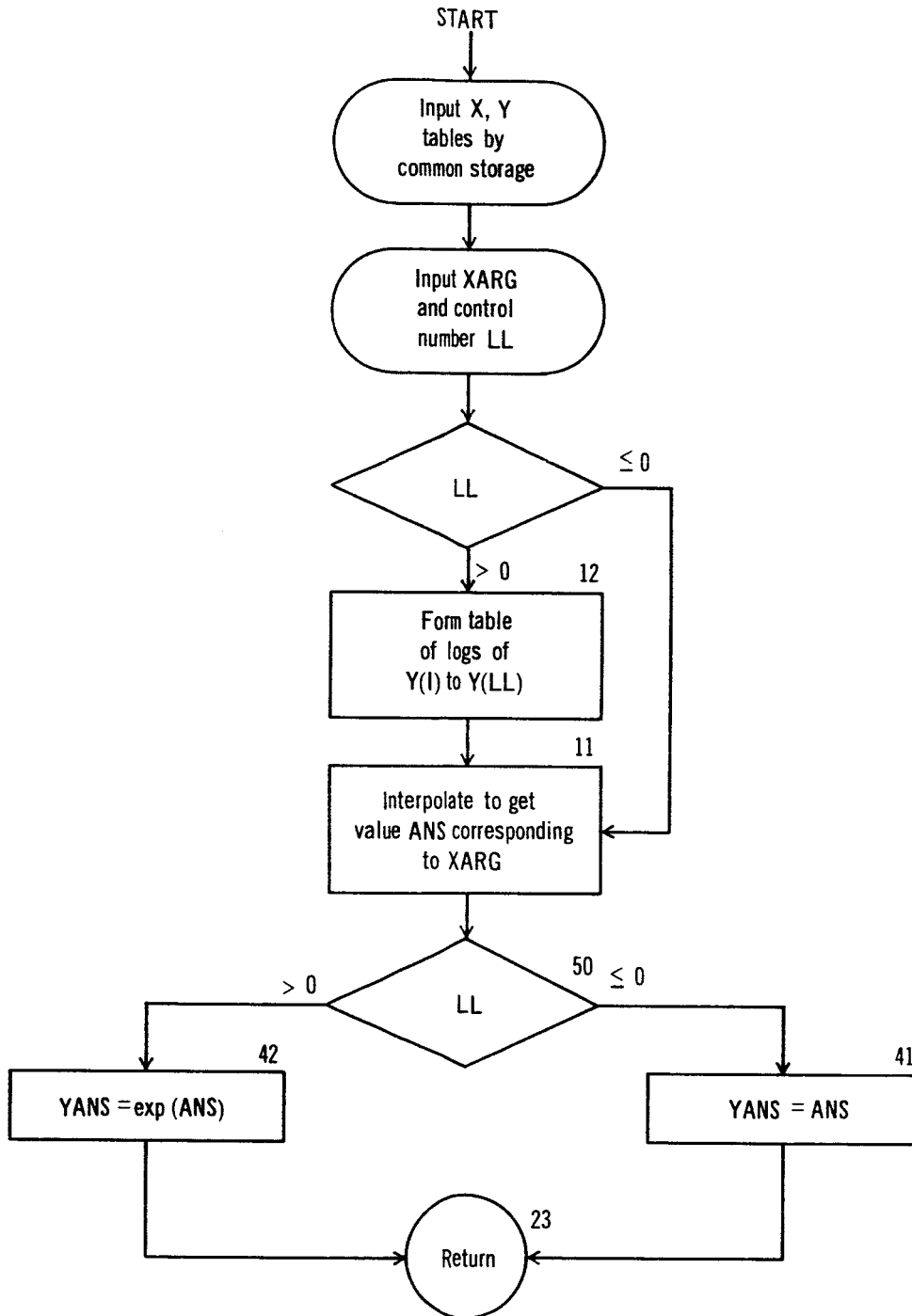
## 2. Subroutine RUNGE



### 3. Subroutine DERIV



4. Subroutine TABLE







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```

C      80-E-700 MEV
      AHO=CCNVM*3.4792E-13
      AH1=CCNVM*4.617E+8
      AH2=CUNVM*1.343E+5
      BHO=2.549
      BH1=.656
      BH2=.344
      CC(1)=10.
      DE(2)=10.*5
      DE(3)=16.*5
      DE(4)=27.*5
      DE(5)=52.*5
      DE(6)=72.*5
      DE(7)=92.*5
      DE(8)=137.*5
      DE(9)=212.*5
      DE(10)=262.*5
      DE(11)=312.*5
      DE(12)=412.*5
      DE(13)=525.*5
      DE(14)=625.*5
      DE(15)=700.
      DLOSS(1)=-.40E-2
      DLOSS(2)=-.3985E-2
      DLOSS(3)=-.1770E-2
      DLOSS(4)=-.7051E-3
      DLOSS(5)=-.2173E-3
      DLOSS(6)=-.1172E-3
      DLOSS(7)=-.743E-4
      DLOSS(8)=-.354E-4
      DLOSS(9)=-.153E-4
      DLOSS(10)=-.101E-4
      DLOSS(11)=-.713E-5
      DLOSS(12)=-.410E-5
      DLOSS(13)=-.244E-5
      DLOSS(14)=-.166E-5
      DLOSS(15)=-.131E-5
      PREL(1)=1.25
      PREL(2)=1.245
      PREL(3)=1.22
      PREL(4)=1.13
      PREL(5)=1.0
      PREL(6)=1.02
      PREL(7)=1.05
      PREL(8)=1.04
      PREL(9)=1.15
      PREL(10)=1.16
      PREL(11)=1.20
      PREL(12)=1.25
      AVPRL=1.14625
5C0    RLAD INPUT TAPE 2,1,ALAT,LL,B
      CUNVR=C.17453292E-1
      ALATO=ALAT*GUNVR
      CSLAT4=CUSP(ALATO)**4
      EREL=EL*REL
      READ INPUT TAPE 2,2,((RI(I),I=1,12),(SIG(I),J=1,12))

```

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```

400 READ INPUT TAPE 2,72C,ENC,TSUBO,DT1,DT2,TEND,TEST,IEDEL,ILEND,
  IIEP4,VPRENT,ICSUBC
C INPUT PRINTOUT
  WRITE OUTPUT TAPE 3,70C
700 FORMAT(2uF1) ***** PROGRAM INPUT *****(/)
  WRITE OUTPUT TAPE 3,701,ALAT,EL,B,ENG,TSUBO,DT1,DT2,
  IEND,TEST,ICFL,IFEND,IFPR,ICSUBO,NPRINT
701 FORMAT(13H) L ATO *** =F8.4/13H B ***** =
  IF8.4/13H NP SUB C =E12.4/13H T SUB C =E12.4/
  113H DELTA T1 =F8.4/13H DELTA T2 =F8.4
  2 /13H T END ** =
2F8.17/23H ENERGY LEVEL START =13/23H DELTA ENERGY LEVEL =13/
323H ENERGY LEVEL END =13/30H ENERGY LEVEL TIME HISTORY =13,
47X,92H INDICATES ENERGY LEVEL AT WHICH TIME HISTORY CF DENSITY AND
5FLUX WILL BE PRINTED ON TAPE 5. /40X,43HZERU INDICATES NU TIME HI
6STORY ON TAPE 5. //30H CYCLE AT T SUB ZERU ***** =15//35H PRI
7NITIG ON TAPE 5. AFTER EVERY 16.5H DELTA T.//)
  WRITE OUTPUT TAPE 3,702,(R(1),SIG(1),I,1,12)
702 FORMAT(2X,4HR(1),10X,6HSIG(1)/(2E14,4))
C HEADING AND R,SIG,PREL, AVERAGED FOR TIME AVERAGE ST. ST. SOLUTION
C IF(DTL) GO TO 1006,1098
1000 WRITE OUTPUT TAPE 3,1001,ALAT,EL,B
1001 FORMAT(48H1 TIME AVERAGE STEADY STATE SOLUTION FOR L ATO =F8.4,
  16H , L =F7.4/6H , B =F7.4/7H// PROTON- PHI BAR SIG BAR
  288H ENERGY PROTON- PROTON- PHIBAR SIGBAR
  3 (DE/DX) D(DE/DX)/DE/ DENSITY//
  434H (MEV) FLUX
  SUMR=0.0
DC 1002 NV=1,12
1002 SUMR=SUMR+R(IN)
  AVR=SUMR/12.0
DC 1003 NV=1,12
1003 R(NN)=AVR
  SUMSIG=0.0
DC 1005 NV=1,12
1005 SUMSIG=SUMSIG+SIG(NN)
  AVSIG=SUMSIG/12.0
DC 1006 NV=1,12
1006 SIG(NN)=AVSIG
DC 1008 NV=1,12
1008 PREL(NN)=AVPREL
  GO TO 1055
1098 WRITE OUTPUT TAPE 3,705,ALAT,EL,B
705 FORMAT(49H1 TRANSIENT STEADY STATE SOLUTION FOR L ATO =F8.4,
  16H , L =F7.4/6H , B =F7.4/7H//
  240H ENERGY CYCLE I MINIMUM - PROTON-6X,22HPRCTON- I MAX
  31PMU -5X, 7HPRCTON-6X,7HPRCTON-,3X,13H1 FLUX RATIO/
  4X,33H (MEV) NO. I TIME (MC)
  3 4 FLUX,9X,31FDENSITY I TIME (MC)
  4 53X,13H1 (MAX/MIN)/
  510X,1F1,37X,1F1,35X,1H1
  T=TSUBC
  TMAX=132.
  TCK=0.0
C IEEND MUST BE LESS THAN OR EQUAL TO 15 , BUT GREATER THAN 0

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10/01/64

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```

1009 DU 300 M=IEST,IEEND,IEDEL
      DT=DTI
      ICYCLE=ICSUBC
      EMAX(I)=LNC
      EMIN(I)=LNG
      EMIN(1)=0.0
      EMIN(2)=0.0
      ENER=E(N)
C   TIME HISTORY HEADING ON TAPE 5
      ITESTJ=N-ILPR
      IF(ITESTJ) 310,301,310
301 WRITE OUTPUT TAPE 5,302,ENER,ALAT,EL,B
302 FORMAT(6HI TIME HISTORY OF DENSITY AND FLUX FOR ENERGY =F6.1, FLUX
1 9H , L A10 =F8.4, 6H , L =F7.4/24X, 95HTIME FLUX
2 DENSITY 1 TIME FLUX DENSITY 1 TIME FL
3UX DENSITY)
      WRITE OUTPUT TAPE 5,900,ICYCLE
900 FORMAT(14H CYCLE NO. =I4,35X,1H1,33X,1H1)
      IF(I32.0/(FLCAT(INPRINT)*CTI)-5000.0) 310,310,901
901 WRITE OUTPUT TAPE 3,902
902 FORMAT(61HONPRINT WILL CAUSE T5,ED,AND FL5 TO EXCEED DIMENSION OF
15000.)
      GO TO 500
310 ALOSS=ALOSS(M)
      DO 201 K=1,15
      X(K)=CL(K)
201 Y(K)=DELOSS(K)
      CALL TABLE(ENER,EANS,15)
      DO 20 J=1,12
      ALOSSA(J)=R(J)*ALCSS
      DLOSSA(J)=R(J)*EANS
C   NOW HAVE (DE/DX)ATMOS AND (DE/DX)/(DE)ATMOS AS FUNCTIONS
C   OF TIME FOR A GIVEN ENERGY AND L
710 IF(ENER=80.) 21,21,22
      A1=ALC
      A2=AL2
      B0=BLC
      B1=BL1
      B2=BL2
      GO TO 23
22 A0=AH0
      A1=AH1
      A2=AH2
      B0=BH0
      B1=BH1
      B2=BH2
23 CU=AG/(LELE*ENER**BC*CSLAT4)
      CL=A1/(ENER**B1)
      C2=A2*LN(R**B2)
C   COMPUTE TIME AVERAGE STEADY STATE SOLUTION
      IF(DTI) 500,1100,1959
1100 DEDX=ALOSSA(1)
      DEDX=ALOSSA(1)
      DENS=A0*AVPRL/((AC/CO)*(CL*DEDX+C2*(CDECDX+AVS(G))))
      FLUX=?*O*DENS*C2/CCNVN

```

CONSER

```

WRITE LUPUT TAPE 3,1101,ENER,FLUX,DENS,AVPRL,AVSIG,
IDEDX,CUEDX
1101 FORMAT(I10,F8.2,1P6E13.4)
GU TO 300
C BEGIN RUNGE KUTTA TECHNIQUE
1599 NP=0
N5=0
EN=ENO
30 CALL RUNGE(T,EN,DT,DEN,T1,EN1)
IF(T1-TMAX) 31,100,100
31 EN=EN1
T=T1
C TEST/STORE TIME HISTORY
IF(ITEST1) 759,910,799
910 NP=NP+1
IF(NP-NPRINT) 759,911,911
911 N5=N5+1
NP=0
T5(N5)=T1
E5(N5)=EN1
FL5(N5)=EN1*2.0*C2/CCAVM
C TEST AND STOR MIN-MAX
759 IF(EMAX(ICYCLE)-EN1) 800, 30,801
800 EMAX(ICYCLE)=EN1
ETMAX(ICYCLE)=T1
GU TO 30
801 IF(EMIN(ICYCLE)-EN1) 30,30,802
802 EMIN(ICYCLE)=EN1
ETMIN(ICYCLE)=T1
GU TO 30
C ADJUST END OF 11 YEAR CYCLE
100 EN1=EN+((TMAX-T)/DT)*DEN
IF(ITEST1) 101,915,101
C PRINT TIME HISTORY ON 5
915 N5=N5+1
T5(N5)=TMAX
E5(N5)=EN1
FL5(N5)=EN1*2.0*C2/CCAVM
WRITE OUTPUT TAPE 5,916,(T5(1),FL5(1),E5(1),I=1,N5)
916 FORMAT(I2X,0PF9.3,0PF11.4,1PE12.4,2H 1,0PF9.3,0PF11.4,1PE12.4,
12H 1,0PF9.3,0PF11.4,1PE12.4)
ICYS=ICYCLE+1
WRITE LUPUT TAPE 5,900,ICYS
N5=0
NP=0
C CHECK END POINT FOR MIN-MAX
101 IF(EMAX(ICYCLE)-EN1) 810,815,811
810 EMAX(ICYCLE)=EN1
ETMAX(ICYCLE)=TMAX
GU TO 815
811 IF(EMIN(ICYCLE)-EN1) 815,815,812
812 EMIN(ICYCLE)=EN1
ETMIN(ICYCLE)=TMIN
C TEST STEADY STATE SOLUTION
815 TCK=TCK+132.0
IF(ICYCLE-ICSUBC) 819,849,820

```

CUNSER

```

819 SIOP 77777
820 ICM1=ICYLE-1
TEST1=EMAX(ICYLE)/EMAX(ICYM1 )-1.0
TEST2=EMIN(ICYLE)/EMIN(ICYM1 )-1.0
IF(AHSH(1,ST1))-1.0E-4) 821,821,849
821 IF(AHSH(1,ST2))-1.0E-4) 822,822,849
822 TPRI=EMIN(ICYM1)
EPR1=EMIN(ICYM1)
FLPR1=FLPR1*2.0*G2/CONVM
TPR2=EMAX(ICYM1)
EPR2=EMAX(ICYM1)
FLPR2=FLPR2*2.0*G2/CONVM
RATIO=FLPR2/FLPR1
WRITE OUTPUT TAPE 3,823,ENER,ICYM1 ,TPR1,FLPR1,EPR1,TPR2,FLPR2,
1,EPR2,RATIO
823 FORMAT(10P5,2,3X,I3,4H I,OPF9.4,CPFI3.4,IPEI3.4,3F I,OPFIC.4,
10PE14.4,IPEI3.4,3F I,OPFIC.4)
IF(AHSH(FLPR1)-50000.) 866,831,831
866 IF(RATIO-1.050) 861,861,830
861 WRITE OUTPUT TAPE 3,862
862 FORMAT(///196H ALL HIGHER ENERGY LEVELS ARE BEING NEGLECTED SINCE
LE THE FLUX RATIO HAS BECOME LESS THAN 1.050.)
GO TO 300
831 WRITE OUTPUT TAPE 3,822
832 FORMAT(/// 52H I BLEW UP. KERON THIS CASE WITH SMALLER DELTA I
1.)
GO TO 300
830 WRITE OUTPUT TAPE 3,824
824 FORMAT(18X,1F,37X,1H1,39X,1H1)
GO TO 856
849 IF(TCK-1.0) 850,855,855
850 I=0.0
EM=ENI
DT=DT2
ICYLE=ICYLE+1
EMAX(ICYLE)=EM1
EMIN(ICYLE)=EM1
EMAX(ICYLE)=0.0
EMIN(ICYLE)=0.0
GO TO 30
C NO TRANSLIENT STEADY STATE SOLUTION AS YET
855 TPRI=EMIN(ICYLE)
EPR1=EMIN(ICYLE)
FLPR1=FLPR1*2.0*G2/CONVM
TPR2=EMAX(ICYLE)
EPR2=EMAX(ICYLE)
FLPR2=FLPR2*2.0*G2/CONVM
RATIO=FLPR2/FLPR1
WRITE OUTPUT TAPE 3,857,ENER,ICYLE,TPR1,FLPR1,EPR1,TPR2,FLPR2,
1,EPR2,RATIO
857 FORMAT(10P5,2,3X,I3,4H I,OPF9.4,CPFI3.4,IPEI3.4,3F I,OPFIC.4,
10PE14.4,IPEI3.4,3F I,OPFIC.4,
122H 1.5.S. SOLN. AS YET)
WRITE OUTPUT TAPE 3,824
856 T=TSUNG
TCK=0.0

```







STORAGE NOT USED BY PROGRAM

DEC GCT  
17467 42073  
DEC GCT  
32468 77324

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC GCT DEC GCT DEC GCT DEC GCT DEC GCT  
ALCOSA 32504 77370 C0 32561 77461 C1 32560 77460 C2 32559 77457 OLCSSA 32492 77354  
PREL 32516 77404 SIG 32480 77340 TIME 32528 77420 X 32558 77456 Y 32543 77437

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC GCT DEC GCT DEC GCT DEC GCT DEC GCT  
CELLSS 17424 42020 DE 17405 42001 E3 11594 28512 ELCSS 17451 42053 EMAX 17394 41162  
EMIN 16994 41142 E 17466 42072 EIMAX 17194 41452 ETMIN 16794 40632 FL5 6594 14702  
R 17436 42034 T5 16554 40322

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC GCT DEC GCT DEC GCT DEC GCT DEC GCT  
A0 1594 03072 A1 1553 03071 A2 1592 03070 AHO 1591 03067 AH1 1590 03066  
AH2 1589 03065 ALO 1588 03064 AL1 1587 03063 AL2 1586 03062 ALATC 1585 03061  
ALAT 1584 03060 ALCSS 1583 03057 AVPR1 1582 03056 AVPR2 1581 03055 AVSIG 1580 03054  
B0 1579 03053 B1 1578 03052 B2 1577 03051 BHO 1576 03050 B1 1575 03047  
B2 1574 03046 BLC 1573 03045 BLC 1572 03044 BL2 1571 03043 B 1570 03042  
CONVM 1569 03041 CONVR 1568 03040 CSLAT4 1567 03037 DCEEX 1566 03036 DEEX 1565 03035  
JEN 1564 03034 DENMS 1563 03033 DT1 1562 03032 DT2 1561 03031 CI 1560 03030  
EANS 1559 03027 EELL 1558 03026 EL 1557 03025 ENG 1556 03024 EN1 1555 03023  
ENER 1554 03022 EN 1553 03021 EPR1 1552 03020 EPR2 1551 03017 FLPR1 1550 03016  
FLPR2 1549 03015 FLUX 1548 03014 ICSUP0 1547 03013 ICY5 1546 03012 ICYCLE 1545 03011  
ICYMI 1544 03010 IEDEL 1543 03007 IEEND 1542 03006 IEPR 1541 03005 IEST 1540 03004  
IEST3 1535 03003 M 1534 02776 SUMR 1533 02775 SUMSIG 1532 02774 NPRINT 1536 03000 NP 1535 02777  
RATIC 1534 02776 TEST1 1528 02770 TEST2 1527 02767 T1 1531 02773 TCK 1530 02772  
TEND 1529 02771 T 1523 02763 TSUB0 1522 02762 TPRI 1525 02765

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN LCC EFN LCC EFN LCC EFN LCC EFN LCC  
811 1 02750 812 2 02746 813 3 02744 819E 302 02344 81LS 700 02734  
81LT 701 02726 81LU 702 02554 81M1 705 02464 81MG 720 02740 81PN 823 02234  
81PO 824 02160 81Q 832 02173 81CP 857 02153 81CU 862 02215 81SA 500 02301  
81S6 902 02272 81SK 516 02253 81V9 1001 02546 81J2C 1101 02257

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC GCT DEC GCT DEC GCT DEC GCT DEC GCT  
1) 1513 02751 2) 1000 01750 3) 1007 01757 4) 32767 77777 6) 1100 02114  
C1G4 1518 02756 C1G6 1519 02757 C1G7 1520 02760 C1G8 1521 02761 D1203 201 00311  
C121T 909 01615 D1220 588 01734 D1603 260 00310 E1L 400 00620 E1C 451 00703  
E110 541 01035 E112 591 01117 E113 642 01202 E115 664 01230 E116 779 01413  
E1503 203 00313

10/01/64

RUNGE

```
C SUBROUTINE FOR RUNGE KUTTA TECHNIQUE
SUBROUTINE RUNGE(TO,YO,H,DELY,TA,YA)
COMMON CO,C1,C2,X,Y,TIME,PREL,ALOSSA,DLCSSA,SIG
CALL DERIV(TO,YO,CER)
CONT1= DER*H
TI = TO+H/2.
Y1 = YO+CONT1/2.
CALL DERIV(TI,Y1,CER)
CONT2=DER*H
Y1 = YO+CONT2/2.
CALL DERIV(TI,Y1,CER)
CONT3=DER*H
TI=TO+H
Y1=YO+CONT3
CALL DERIV(TI,Y1,CER)
CONT4=DER*H
DELY=(CONT1+2.*CONT2+2.*CONT3+CONT4)/6.
TA= TO+H
YA= YO+DELY
RETURN
END(TI,1,0,0,C,0,0,1,0,C,0,C,0,0)
```

STORAGE NOT USED BY PROGRAM

DEC OCT  
129 00175  
32551 77447

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC OCT	DEC OCT	DEC OCT	DEC OCT	DEC OCT
32554 77452	CC 32561 77461	C1 32560 77460	C2 32559 77457	DLCSSA 32553 77451
PAFL 32555 77453	516 32552 77450	TIME 32556 77454	X 32558 77456	Y 32557 77455

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC OCT	DEC OCT	DEC OCT	DEC OCT	DEC OCT
CC11 124 00174	CC1T2 123 00173	CUNT3 122 00172	CCNT4 121 00171	DER 120 00170
Y1 115 00167	Y1 118 00166			

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC OCT	DEC OCT	DEC OCT
1) 115 00164	3) 108 00154	6) 110 00156

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC OCT	DEC OCT	DEC OCT
DERIV 0 00000		

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

DERIV

10/01/64

DERIV

```
C SUBROUTINE TO EVALUATE (DN/DT) FOR A GIVEN T AND EN
SUBROUTINE DERIV(1,CA,DER)
DIMENSION TIME(12),PREL(12),ALOSSA(12),DLCSSA(12),X(15),Y(15),SIG(
112)
COMMON C,C1,C2,X,Y,TIME,PREL,ALOSSA,DLCSSA,SIG
DO 1 K=1,12
X(K)=TIME(K)
1 CONTINUE
DO 2 K=1,12
Y(K)=PREL(K)
2 CONTINUE
CALL TABLE(1,TANS,0)
P=TANS
DO 3 K=1,12
Y(K)=ALOSSA(K)
3 CONTINUE
CALL TABLE(T,ANS,12)
EX=ANS
DO 4 K=1,12
Y(K)=DLCSSA(K)
4 CONTINUE
CALL TABLE(T,ANS,12)
EXX=ANS
DO 5 K=1,12
Y(K)=SIG(K)
5 CONTINUE
CALL TABLE(T,ANS,12)
SIGMA=ANS
EVALUATE(DN/DT)C
DER =C0*P-C1*EX-C2*EN*EXX-SIGMA*EN*CZ
RETURN
END(1,1,0,0,0,0,0,0,0,0,0,0,0,0,0)
```



10/01/64

TABLE

```
C SUBROUTINE TO INTERPOLATE A GIVEN TABLE
SUBROUTINE TABLE(XARG,YANS,LL)
DIMENSION X(15),Y(15)
COMMON CO,C1,C2,X,Y,TIME,PREL,ALOSSA,BLESSA,SIG
IF(LL)11,11,12
12 DO 10 K=1,LL
A=Y(K)
Y(K)=LUGH(A)
10 CONTINUE
11 DO 20 J=1,15
IF(X(J)-XARG)20,21,22
21 ANS=Y(J)
22 GO TO 30
F1=X(J)
Y1=Y(J)
HG=X(J-1)
YG=Y(J-1)
ANS=Y1-(Y1-YG)*(F1-XARG)/(F1-HG)
GO TO 30
20 CONTINUE
50 IF(LL)41,41,42
41 YANS=ANS
GO TO 23
42 YANS=FAPE(ANS)
23 RETURN
END(1,1,0,0,C,0,C,1,0,C,C,C,C,0,0)
```



## F. Restrictions

- (1)  $132/(\text{NPRINT} \times \text{DT1})$  must be less than 5000 in order that T5, E5 and FL5 subscripts do not exceed their dimension specifications.
- (2) IEEND cannot exceed 15 since the table of energy levels contains only 15 values (see energy level table below)

## G. Input

Input to this program consists of five data cards and four control cards for every B-L line considered. The data cards are those output by the preceding program. The control cards are those that handle the selection of the many available calculations in this program. The first control card contains the initial density (END) and the initial time (TSUBO) for integration. The second card contains the integration interval for the first cycle (DT1), the integration interval for all other cycles (DT2) and the end limit of integration (TEND). Setting DT1 equal to zero will give a time averaged steady state solution of the equation. The next control card defines the energy level(s) to be used. It gives the initial energy level subscript (IEST), the increment in energy level subscripts (IEDEL) and the final energy level subscript (IEEND). Energy levels are as follows:

E(1) = 10 Mev	E(6) = 125 Mev	E(11) = 350 Mev.
E(2) = 25 Mev	E(8) = 150 Mev	E(12) = 400 Mev.
E(3) = 50 Mev	E(8) = 200 Mev	E(13) = 500 Mev.
E(4) = 75 Mev	E(9) = 250 Mev	E(14) = 600 Mev.
E(5) = 100 Mev	E(10) = 300 Mev	E(15) = 700 Mev.

Note that IEST, IEEND and IEDEL must be greater than zero and that IEND cannot be greater than 15. The fourth control card contains three numbers (1) IEPR is the subscript of that energy level whose time history is to be printed on tape 5. If IEPR = 0 then no time history will be printed. (2) NPRINT tells the computer how often to print density, flux and time values on tape 5 if IEPR  $\neq$  0. Values will be given for every NPRINT increments in time. However, if  $132/(\text{NPRINT} \times \text{DT1})$  is greater than 5000 the computer will print an error message and go on to the next case. This is done in order to prevent time, energy and flux subscripts from exceeding their dimension statement capacities. (3) ICSUBO is the cycle number at initial density (ENO) and initial time (TSUBO). ICSUBO is always greater than or equal to 1. All input occurs on tape 2.



## 1. Input Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
<u>Card 1</u>	1-8	F	ALAT	degrees	latitude
	9-16	F	EL	earth radii	magnetic field line
	17-24	F	B	gauss	magnetic induction
<u>Card 2</u>	1-10	E	R(1)	-	scale factor R for TIME(1)
	11-20	E	R(2)	-	scale factor R for TIME(2)
	21-30	E	R(3)	-	scale factor R for TIME(3)
	31-40	E	R(4)	-	scale factor R for TIME(4)
	41-50	E	R(5)	-	scale factor R for TIME(5)
	51-60	E	R(6)	-	scale factor R for TIME(6)
<u>Card 3</u>	1-10	E	R(7)	-	scale factor R for TIME(7)
	11-20	E	R(8)	-	scale factor R for TIME(8)
	21-30	E	R(9)	-	scale factor R for TIME(9)
	31-40	E	R(10)	-	scale factor R for TIME(10)
	41-50	E	R(11)	-	scale factor R for TIME(11)
	51-60	E	R(12)	-	scale factor R for TIME(12)
<u>Card 4</u>	1-10	E	SIG(1)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(1)
	11-20	E	SIG(2)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(2)
	21-30	E	SIG(3)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(3)
	31-40	E	SIG(4)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(4)
	41-50	E	SIG(5)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(5)
	51-60	E	SIG(6)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(6)

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
<u>Card 5</u>	1-10	E	SIG(7)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(7)
	11-20	E	SIG(8)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(8)
	21-30	E	SIG(9)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(9)
	31-40	E	SIG(10)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(10)
	41-50	E	SIG(11)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(11)
	51-60	E	SIG(12)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(12)
<u>Card 6</u>	1-10	E	ENO	# protons/ cm <sup>3</sup>	initial proton density
	11-20	E	TSUBO	months	initial time
<u>Card 7</u>	1-8	F	DT1	months	first cycle integration interval
	9-16	F	DT2	months	remaining cycle integration interval
	17-24	F	TEND	months	limit of integration
<u>Card 8</u>	1-3	I	IEST	-	initial energy level subscript*
	4-6	I	IEDEL	-	energy level subscript incre- ment*
	7-9	I	IEEND	-	final energy level subscript*
<u>Card 9</u>	1-5	I	IEPR	-	subscript of energy level to be printed on tape 5
	6-10	I	NPRINT	-	print on tape 5 after so many increments in time
	11-15	I	ICSUBO		cycle corresponding to ENO and TSUBO

\* see table of energy levels in INPUT.

## 2. Sample GENERAL PURPOSE DATA SHEET

Problem	INPUT - CONSERVATION EQUATION CALCULATION										Date	SAMPLE	Page	of		
Sponsor	TAPE 2															
1																
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## H. Output

Output from this program exists in several forms. First of all there is the output from the transient steady-state solution. In this solution there are two pages of printout for each case (each B-L line considered). The first page merely lists the input with explanatory headings. The second page lists each energy level and the cycle number at which steady-state was reached for that energy level. It also gives the maximum and minimum density and flux for that cycle with the times at which they appear within the cycle. Finally it lists the ratio of the maximum to the minimum flux. If, for any energy level, the absolute value of the minimum flux becomes greater than 50,000 protons/cm<sup>2</sup> sec. mev. then the program will ask that a smaller integration interval be used and go on to the next case. On the other hand, if the ratio of the maximum to the minimum flux becomes less than 1.09 for any energy level the program will neglect all higher energy levels and pass on to the next case since there will be no solar cycle variations in higher energy levels. This output occurs on tape 3.

The time-averaged steady-state solution has the same output with the exception that on the second page for a given B-L line  $\bar{\phi}$ ,  $\bar{\Sigma}$ ,  $dE/dx$  and  $d/dE$  ( $dE/dx$ ) are printed along with the flux and density for each energy level.

Time histories for energy levels are printed on tape 5 if requested during the steady-state solution. Here time, flux and density are printed for each cycle at the intervals indicated by NPRINT. See figure 13 for an idea of the results to be expected from the transient steady-state solution. Figure 15 shows output from several time history runs.

1. Transient Steady-State Sample

```

***** PROGRAM INPUT *****
LATO *** = 15.9450
L ***** = 1.2500
R ***** = 0.2240
NP SUB 0 = 0.
T SUB 0 = 0.
DELTA T1 = 0.1000
DELTA T2 = 0.1000
T ENC ** = 13200.C

ENERGY LEVEL START = 2
DELTA ENERGY LEVEL = 2
ENERGY LEVEL END = 14
ENERGY LEVEL TIME HISTORY = 0
INDICATES ENERGY LEVEL AT WHICH TIME HISTORY OF DENSITY AND FLUX WILL BE PRINTED ON TAPE A5.
ZERO INDICATES NO TIME HISTORY ON TAPE A-5.

CYCLE AT T SUB ZERO ***** = 1
PRINTING ON TAPE A-5 AFTER EVERY 10 DELTA T.

R(I)          SIG(I)
C.3529E-12    C.4902E-18
C.3880E-12    C.5401E-18
C.9239E-12    C.1311E-17
C.2289E-11    C.3259E-17
C.2617E-11    C.3780E-17
C.2141E-11    C.3082E-17
C.1639E-11    C.2350E-17
C.1054E-11    C.1499E-17
C.6659E-12    C.9377E-18
C.5155E-12    C.7224E-18
C.3880E-12    C.5401E-18
C.3529E-12    C.4902E-18

```

TIME AVERAGE STEADY STATE SOLUTION FOR LATG = 15.9450 , L = 1.2500 , B = 0.2240

ENERGY (MEV)	PROTON- FLUX	PROTON- DENSITY	PHI BAR	SIG BAR	(DE/DX)	D(IDE/DX)/DE
25.00	1.0457E-01	1.5521E-11	1.1462E 00	1.5868E-18	2.8576E-14	9.6523E-16
75.00	5.0094E-02	4.4027E-12	1.1462E 00	1.5868E-18	1.1943E-14	1.2295E-16
125.00	3.7291E-02	2.6373E-12	1.1462E 00	1.5868E-18	8.1699E-15	4.8304E-17
200.00	2.5994E-02	1.5639E-12	1.1462E 00	1.5868E-18	5.9342E-15	1.9541E-17
300.00	1.8619E-02	9.7436E-13	1.1462E 00	1.5868E-18	4.6547E-15	8.6384E-18
400.00	1.4035E-02	6.6527E-13	1.1462E 00	1.5868E-18	4.0121E-15	4.8793E-18
600.00	8.9035E-03	3.6709E-13	1.1462E 00	1.5868E-18	3.3845E-15	2.0338E-18

2. Tape 5 Time History Sample

\*\*\*\*\* PROGRAM INPUT \*\*\*\*\*

LATC \*\*\* = 29.7350  
 L \*\*\*\*\* = 1.5500  
 B \*\*\*\*\* = 0.2208  
 NP SUB C = 0.  
 DELTA T1 = 0.1000  
 DELTA T2 = 0.3000  
 T END \*\* = 13233.0

ENERGY LEVEL START = 2  
 DELTA ENERGY LEVEL = 2  
 ENERGY LEVEL END = 14

ENERGY LEVEL TIME HISTORY = 0

INDICATES ENERGY LEVEL AT WHICH TIME HISTORY OF DENSITY AND FLUX WILL BE PRINTED ON TAPE A5.  
 ZERO INDICATES NO TIME HISTORY ON TAPE A-5.

PRINTING ON TAPE A-5 AFTER EVERY

J DELTA T.

R(I)	SI(I)
0.1679E-15	0.7208E-21
0.2078E-15	0.8339E-21
0.1628E-14	0.3571E-20
0.1674E-13	0.2518E-19
0.2370E-13	0.3479E-19
0.1437E-13	0.2142E-19
0.7066E-14	0.1159E-19
0.2267E-14	0.4501E-20
0.7115E-15	0.1915E-20
0.3938E-15	0.1273E-20
0.2078E-15	0.8339E-21
0.1679E-15	0.7208E-21

TRANSIENT STEADY STATE SOLUTION FOR LATD = 28.9050 , L = 1.6500 , H = 0.2228

ENERGY (MEV)	CYCLE NO.	MINIMUM - TIME (40)	PROTON- FLUX	PROTON- DENSITY	MAXIMUM - TIME (40)	PROTON- FLUX	PROTON- DENSITY	FLUX RATIO (MAX/MIN)
25.00	2	54.000	4.9453	7.3402E-10	22.5000	87.7865	1.3030E-09	17.7515
75.00	6	68.500	5.2627	4.6253E-10	28.0000	15.0626	1.3238E-09	2.8621
125.00	11	72.500	5.0683	3.5847E-10	29.5000	8.3303	5.8914E-10	1.5435
200.00	19	74.000	3.9392	2.3700E-10	30.0000	5.0901	3.0624E-10	1.2922
300.00	31	74.500	2.9495	1.5436E-10	30.0000	3.4172	1.7883E-10	1.1595
400.00	41	74.500	2.2517	1.0673E-10	30.0000	2.4980	1.1841E-10	1.1094
600.00	59	75.000	1.4299	5.8954E-11	30.0000	1.5293	6.3054E-11	1.3595



### 3. Time Averaged Steady State Sample

```

***** PROGRAM INPUT *****
LA10 *** = 28.7050
L ***** = 1.6000
B ***** = 0.2208
NP SUB 0 = 0.
T SUB 0 = 0.
DELTA T1 = 0.1000
DELTA T2 = 0.1000
T END ** = 13200.0

ENERGY LEVEL START = 8
DELTA ENERGY LEVEL = 8
ENERGY LEVEL END = 8

ENERGY LEVEL TIME HISTORY = 8      INDICATES ENERGY LEVEL AT WHICH TIME HISTORY OF DENSITY AND FLUX WILL BE PRINTED ON TAPE A5.
ZERO INDICATES NO TIME HISTORY ON TAPE A-5.

CYCLE AT T SUB ZERO ***** = 1
PRINTING ON TAPE A-5 AFTER EVERY 50 DELTA T.

R(I)          SIG(I)
0.1679E-15    0.7208E-21
0.2078E-15    0.8309E-21
0.1628E-14    0.3571E-20
0.1674E-13    0.2518E-19
0.2370E-13    0.3479E-19
0.1407E-13    0.2142E-19
0.7046E-14    0.1159E-19
0.2267E-14    0.4581E-20
0.7116E-15    0.1915E-20
0.3938E-15    0.1273E-20
0.2078E-15    0.8309E-21
0.1679E-15    0.7208E-21

```

TIME HISTORY OF DENSITY AND FLUX FOR ENERGY = 200.G, LATO = 28.9030, L = 1.6000, B = 0.2208

CYCLE NO. =	TIME	FLUX	DENSITY	TIME	FLUX	DENSITY	TIME	FLUX	DENSITY	
1	5.000	0.0849	5.1058E-12	10.000	0.1695	1.0200E-11	15.000	0.2539	1.5273E-11	
	20.000	0.3372	2.0286E-11	25.000	0.4187	2.5191E-11	30.000	0.4951	2.9784E-11	
	35.000	0.5592	3.3645E-11	40.000	0.6042	3.6354E-11	45.000	0.6379	3.8381E-11	
	50.000	0.6617	3.9811E-11	55.000	0.6901	4.1517E-11	60.000	0.7253	4.3635E-11	
	65.000	0.7672	4.6161E-11	70.000	0.8157	4.9078E-11	75.000	0.8700	5.2344E-11	
	80.000	0.9306	5.5930E-11	85.000	0.9963	5.9921E-11	90.000	1.0655	6.4106E-11	
	95.000	1.1388	6.8516E-11	100.000	1.2145	7.3072E-11	105.000	1.2910	7.672E-11	
	110.000	1.3681	8.2313E-11	115.000	1.4466	8.7032E-11	120.000	1.5264	9.1335E-11	
	125.000	1.6076	9.6723E-11	130.000	1.6903	1.0170E-10	132.000	1.7238	1.0371E-10	
	2	5.000	1.8077	1.0876E-10	10.000	1.8912	1.1379E-10	15.000	1.9742	1.1878E-10
		20.000	2.0545	1.2361E-10	25.000	2.1290	1.2809E-10	30.000	2.1678	1.3163E-10
		35.000	2.2068	1.3277E-10	40.000	2.1675	1.3041E-10	45.000	2.1079	1.2682E-10
50.000		2.0335	1.2234E-10	55.000	1.9827	1.1929E-10	60.000	1.9574	1.1777E-10	
65.000		1.9543	1.1758E-10	70.000	1.9700	1.1854E-10	75.000	2.0010	1.2039E-10	
80.000		2.0469	1.2315E-10	85.000	2.1032	1.2544E-10	90.000	2.1071	1.2303E-10	
95.000		2.2369	1.3458E-10	100.000	2.3103	1.3900E-10	105.000	2.3950	1.4349E-10	
110.000		2.4667	1.4809E-10	115.000	2.5380	1.5270E-10	120.000	2.6170	1.5745E-10	
125.000		2.6975	1.6229E-10	130.000	2.7799	1.6723E-10	132.000	2.8128	1.6923E-10	
3		5.000	2.8960	1.7424E-10	10.000	2.9789	1.7922E-10	15.000	3.0609	1.8416E-10
		20.000	3.1393	1.8887E-10	25.000	3.2094	1.9309E-10	30.000	3.2571	1.9596E-10
		35.000	3.2476	1.9539E-10	40.000	3.1551	1.8982E-10	45.000	3.0364	1.8268E-10
	50.000	2.9001	1.7488E-10	55.000	2.7992	1.6842E-10	60.000	2.7358	1.6460E-10	
	65.000	2.7042	1.6270E-10	70.000	2.6992	1.6240E-10	75.000	2.7154	1.6337E-10	
	80.000	2.7521	1.6588E-10	85.000	2.8027	1.6862E-10	90.000	2.8030	1.7225E-10	
	95.000	2.9306	1.7632E-10	100.000	3.0026	1.8065E-10	105.000	3.0761	1.8507E-10	
	110.000	3.1509	1.8957E-10	115.000	3.2275	1.9418E-10	120.000	3.3059	1.9890E-10	
	125.000	3.3860	2.0372E-10	130.000	3.4676	2.0863E-10	132.000	3.5007	2.1062E-10	
	4	5.000	3.5835	2.1560E-10	10.000	3.6659	2.2050E-10	15.000	3.7475	2.2546E-10
		20.000	3.8456	2.3011E-10	25.000	3.8919	2.3416E-10	30.000	3.9326	2.3660E-10
		35.000	3.9051	2.3695E-10	40.000	3.7789	2.2738E-10	45.000	3.6230	2.1798E-10
50.000		3.4476	2.0742E-10	55.000	3.3151	1.9943E-10	60.000	3.2276	1.9418E-10	
65.000		3.1779	1.9120E-10	70.000	3.1598	1.9011E-10	75.000	3.1667	1.9352E-10	
80.000		3.1976	1.9238E-10	85.000	3.2445	1.9521E-10	90.000	3.3027	1.9870E-10	
95.000		3.3689	2.0269E-10	100.000	3.4399	2.0696E-10	105.000	3.5126	2.1134E-10	
110.000		3.5869	2.1580E-10	115.000	3.6631	2.2039E-10	120.000	3.7412	2.2509E-10	
125.000		3.8209	2.2788E-10	130.000	3.9023	2.3478E-10	132.000	3.9353	2.3576E-10	
5		5.000	4.0178	2.4173E-10	10.000	4.1000	2.4667E-10	15.000	4.1811	2.5156E-10
		20.000	4.2575	2.5619E-10	25.000	4.3231	2.6010E-10	30.000	4.3593	2.6227E-10
		35.000	4.3204	2.5994E-10	40.000	4.1730	2.5107E-10	45.000	3.9936	2.4627E-10
	50.000	3.7934	2.2823E-10	55.000	3.6410	2.1906E-10	60.000	3.5382	2.1287E-10	
	65.000	3.4772	2.0200E-10	70.000	3.4508	2.0762E-10	75.000	3.4518	2.0768E-10	
	80.000	3.4790	2.0431E-10	85.000	3.5237	2.1200E-10	90.000	3.5804	2.1541E-10	
	95.000	3.6457	2.1936E-10	100.000	3.7161	2.2359E-10	105.000	3.7884	2.2793E-10	
	110.000	3.8623	2.3237E-10	115.000	3.9382	2.3694E-10	120.000	4.0161	2.4163E-10	
	125.000	4.0957	2.4604E-10	130.000	4.1769	2.5130E-10	132.000	4.2098	2.5328E-10	
	6	5.000	4.2922	2.5624E-10	10.000	4.3742	2.6317E-10	15.000	4.4451	2.6804E-10
		20.000	4.5310	2.7261E-10	25.000	4.5954	2.7648E-10	30.000	4.6289	2.7349E-10
		35.000	4.5828	2.7572E-10	40.000	4.4220	2.6605E-10	45.000	4.2277	2.5336E-10
50.000		4.0118	2.4137E-10	55.000	3.8668	2.3146E-10	60.000	3.7364	2.2468E-10	
65.000		3.6662	2.2058E-10	70.000	3.6346	2.1866E-10	75.000	3.6319	2.1851E-10	
80.000		3.6568	2.2001E-10	85.000	3.7000	2.2261E-10	90.000	3.7598	2.2597E-10	
95.000		3.8206	2.2986E-10	100.000	3.8906	2.3406E-10	105.000	3.9626	2.3641E-10	
110.000		4.0363	2.4284E-10	115.000	4.1120	2.4740E-10	120.000	4.1898	2.5208E-10	
125.000		4.2693	2.5686E-10	130.000	4.3503	2.6173E-10	132.000	4.3832	2.6371E-10	

## I. Running Time

Transient steady-state solutions where  $DT1 = .5$  and  $DT2 = 1.0$  will cover eleven cycles per minute. See figure 14 for an idea of how many cycles are necessary to reach steady-state for various B's at an L of 1.25 earth radii.

Runs requesting a time history print on tape 5 take about twice as long.

Time averaged steady state solutions take about a quarter of a minute for each B-L line.

## VIII. STEADY-STATE CALCULATION

### A. Introduction

This program evaluates the solar maximum and solar minimum steady state conditions of the conservation equation. That is, with  $dN_p/dt$  set equal to zero, the flux and density are studied at solar minimum (time = 0.0 years, see Figure 1) and solar maximum (time = 4.0 years). The mean lifetimes of the protons are also calculated as well as  $dE/dx$ ,  $d/dE(dE/dx)$ , the three coefficients of the conservation equation  $C_0$ ,  $C_1$  and  $C_2$  and the source and loss terms. This is all printed together with the appropriate  $\Sigma$  for a given  $B$ ,  $L$ ,  $\lambda$  and energy level. All 15 energy levels of the preceding program are evaluated for each  $B$  and  $L$ .

### B. Equations

The equations used in this program are listed below:

$$\text{SOURCE} = \text{XX} = A_0 \phi / L^2 E^{B_0} \cos^4 \lambda_0$$

$$\text{LOSS} = \text{YY} = \frac{A_1 N_p}{E^{B_1}} \left( \frac{dE}{dX} \right) + A_2 N_p E^{B_2} \frac{d}{dE} \left( \frac{dE}{dX} \right) + A_2 N_p E^{B_2} \Sigma$$

$$\text{MEAN LIFETIME} = \text{TAU} = N_p / \text{XX}$$

$$\text{FLUX} = \text{FLUXP} = N_p (\text{EXT}) E^{B_2} C = N_p \beta C = N_p v$$

$$\text{DENSITY} = \text{EN1} = \frac{A_0 \phi}{L^2 E^{B_0} \cos^4 \lambda_0 \left[ \frac{A_1}{E^{B_1}} \left( \frac{dE}{dX} \right) + A_2 E^{B_2} \left( \frac{d}{dE} \left( \frac{dE}{dX} \right) + \Sigma \right) \right]}$$

where  $C$  = speed of light

$\phi$  = PREL = relative neutron source strength

$\Sigma$  = SIG = atmospheric loss parameter

$A_0, \dots, A_2$  = high or low energy conservation equation coefficients depending upon whether  $E > 80$  Mev. or  $E \leq 80$  Mev respectively

$B_0, \dots, B_2$  = high or low energy conservation equation coefficients depending upon whether  $E > 80$  Mev. or  $E \leq 80$  Mev. respectively

$\lambda_0$  = Mirror latitude

$N_p$  = proton number density

$v$  = neutron velocity

$\beta = v/C$

$EXT = \beta/E^{B_2}$

### C. Mnemonics

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
TIME(J)	abscissa of time in increments of years for 12 years	years
ELOSS(J)	dE/dX corresponding to E(J) (see Figure 11)	Mev./cm.
E(J)	energy corresponding to ELOSS(J) (see Figure 11)	Mev
ALO	$A_0$ for $E \leq 80$ Mev. (see preceding page)	$\frac{\# \text{ protons}}{\text{cm. sec. Mev.}}$
AL1	$A_1$ " " "	cm/sec
AL2	$A_2$ " " "	cm./Mev <sup>2</sup> sec.
AH0	$A_0$ for $E > 80$ Mev. (see preceding page)	$\frac{\# \text{ protons}}{\text{cm. sec. Mev.}}$
AH1	$A_1$ " " "	cm. sec.
AH2	$A_2$ " " "	cm/Mev <sup>2</sup> sec.

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
BL0	$B_0$ for $E \leq 80$ Mev. (see preceding page)	-
BL1	$B_1$ " " "	-
BL2	$B_2$ " " "	-
BH0	$B_0$ for $E > 80$ Mev. (see preceding page)	-
BH1	$B_1$ " " "	-
BH2	$B_2$ " " "	-
DELOSS(J)	$d(dE/dX)/dE$ corresponding to DE(J) (see Figure 12)	$\text{cm.}^{-1}$
DE(J)	energy corresponding to DELOSS(J) (see Figure 12)	Mev.
PREL(J)	$\Phi$ for TIME(J) (see Figure 11 and page 167)	-
CONVR	conversion factor - degrees to radians	-
ALAT	mirror latitude $\lambda_0$	degrees
EL	magnetic field line L	earth radii
B	magnetic induction B	gauss
R(J)	atmospheric scale factor R for TIME(J)	-
SIG(J)	atmospheric loss parameter $\Sigma$ for TIME(J)	atoms/cm
ALATO	ALAT in radians	radians
SVPR	temporary storage of PREL(1)	-
SVSG	temporary storage of SIG(1)	atoms/cm
t	time	years

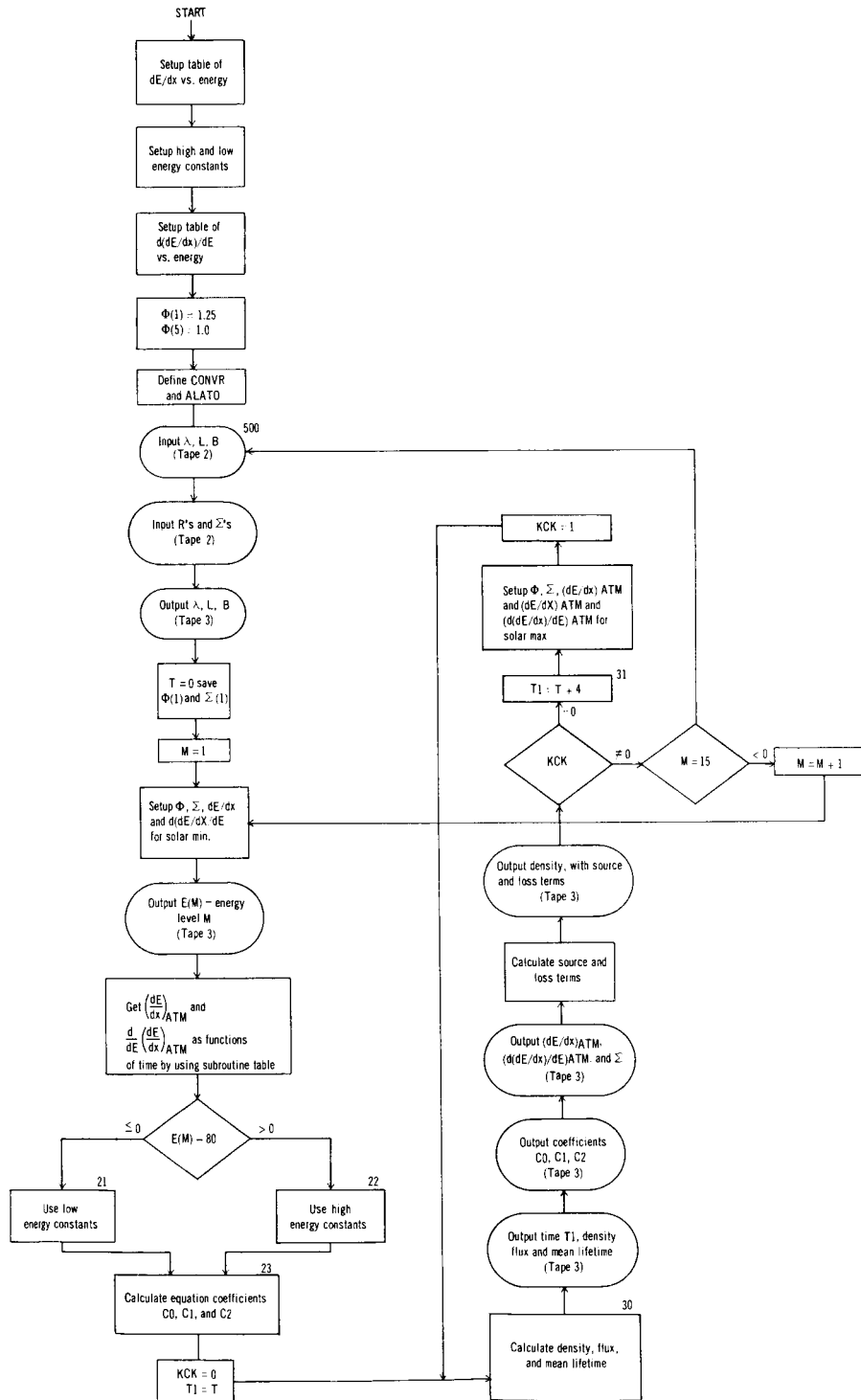
<u>Quantity</u>	<u>Description</u>	<u>Units</u>
M	energy level subscript	-
ENER	energy level E(M)	Mev.
ALOSS	dE/dX for E(M)	Mev/cm
X(k)	temporary storage of DE(k)	Mev.
Y(k)	temporary storage of DELOSS(k)	cm <sup>-1</sup>
EANS	d(dE/dX)/dE for E(M)	cm <sup>-1</sup>
ALOSSA(J)	(dE/dX) X R(J) for E(M)	Mev/cm
DLOSSA(J)	(d(dE/dX)/dE) X R(J) for E(M)	cm <sup>-1</sup>
A0	temporary storage of AL0 or AH0	$\frac{\# \text{ protons}}{\text{cm. sec. Mev.}}$
A1	temporary storage of AL1 or AH1	cm./sec.
A2	temporary storage of AL2 or AH2	cm/Mev <sup>2</sup> sec.
B0	temporary storage of BL0 or BH0	-
B1	temporary storage of BL1 or BH1	-
B2	temporary storage of BL2 or BH2	-
EXT	(see page 168)	-
C0	conservation equation coefficient $c_0$ where $C_0 = A_0 / L^2 E^{B_0} \cos^4 \lambda_0$	$\frac{\# \text{ protons}}{\text{cm}^2 \text{ sec. Mev.}}$
C1	conservation equation coefficient $C_1$ where $C_1 = A_1 / E^{B_1}$	cm/sec. Mev.
C2	conservation equation coefficient $C_2$ where $C_2 = A_2 E^{B_2}$	cm/sec. Mev.

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
KCK	counter to determine if solar maximum or solar minimum is being evaluated	-
T1	particular time under consideration	years
EN1	proton density	$\frac{\# \text{ protons}}{\text{Mev. cm}}$
FLUXP	proton flux	$\frac{\# \text{ protons}}{\text{cm}^2 \text{ sec. Mev.}}$
TAU	mean proton lifetime	sec
XX	conservation equation source term (see page 167)	$\frac{\# \text{ protons}}{\text{cm}^2 \text{ sec.}}$
YY	conservation equation loss term (see page 167)	$\frac{\# \text{ protons}}{\text{cm}^2 \text{ sec.}}$

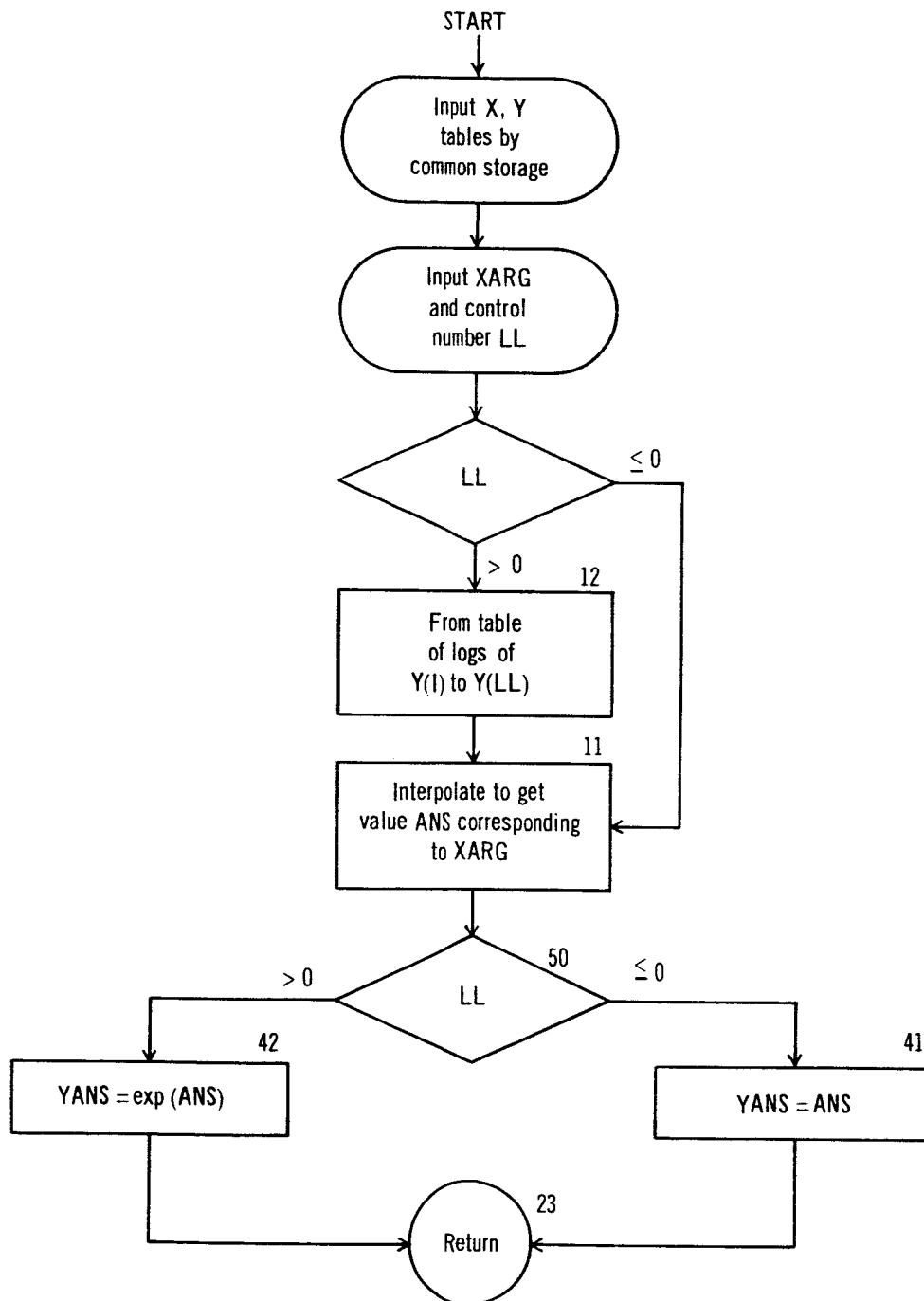


## D. Flow Charts

### 1. Main Program



## 2. Subroutine Table



E. Fortran Listing

10/01/64

ST-LADY

```

C      STEADY STATE
      DIMENSION L(15),ELC(15),ELCSS(15),TIME(12),R(12),R(12),DEL(15),PREL(5)
      1,ALUSSA(12),DLOSSA(12),X(15),Y(15),SIG(12)
      COMMON X,Y
      1 FORMAT(3F8.4)
      2 FORMAT(6E10.4)
      3 FORMAT(1F15.3,1E20.4,1F20.5,1E20.5)
      4 FORMAT(1H1,2X,5HLATQ=1F8.3,2X,2HL=1F6.3,3X,2Hh=F7.4)
      5 FORMAT(10X,7FENERGY=1F8.2,3HREV)
      6 FORMAT(9X,4HTIME,15X,4HN(E),17X,4HFLUX,10X,13HMEAN LIFETIME)
      7 FORMAT(15X,3HC0=E12.5,5X,3HC1=E12.5,5X,3HC2=E12.5)
      8 FORMAT(11X,7HALUSSA=E12.5,1X,7HALDSSA=E12.5,4X,4HSIG=E12.5)
      9 FORMAT(3X,5HN(E)=E12.5,1X,7HSOURCE=E12.5,3X,5HLCSS=E12.5)

```

```

      TIME(1)=0.0
      DO 11 J=1,11
      TIME(J+1)=TIME(J)+12.0
11 CONTINUE

```

```

      ELOSS(1)=5.3585E-2
      ELOSS(2)=2.5732E-2
      ELOSS(3)=1.4755E-2
      ELOSS(4)=1.0754E-2
      ELOSS(5)=8.6553E-3
      ELOSS(6)=7.3567E-3
      ELOSS(7)=6.4720E-3
      ELOSS(8)=5.3435E-3
      ELOSS(9)=4.6543E-3
      ELOSS(10)=4.1514E-3
      ELOSS(11)=3.8607E-3
      ELOSS(12)=3.6127E-3
      ELOSS(13)=3.2701E-3
      ELOSS(14)=3.0476E-3
      ELOSS(15)=2.8542E-3

```

```

      E(1)=10.
      E(2)=25.
      E(3)=50.
      E(4)=75.
      E(5)=100.
      E(6)=125.
      E(7)=150.
      E(8)=200.
      E(9)=250.
      E(10)=300.
      E(11)=350.
      E(12)=400.
      E(13)=500.
      E(14)=600.
      E(15)=700.

```

```

C      10-C-80 MEV      2.5664E-13
      AL0=      3.463E+8
      AL1=      7.255E+E
      BL0=2.309
      BL1=.523
      BL2=.477
      80-E-700 MEV

```

STEADY

```

AH0= 3.4792E-13
AH1= 4.6172E+8
AH2= 1.343E+9
RH0=2.549
RH1=.656
RH2=.344
DL(1)=10.
DL(2)=10.5
DL(3)=16.5
DL(4)=27.5
DL(5)=52.5
DL(6)=72.5
DL(7)=92.5
DL(8)=137.5
DL(9)=212.5
DL(10)=262.5
DL(11)=312.5
DL(12)=412.5
DL(13)=525.5
DL(14)=625.5
DL(15)=700.
DELOSS(1)=-.40E-2
DELOSS(2)=-.3585E-2
DELOSS(3)=-.1770E-2
DELOSS(4)=-.7051E-3
DELOSS(5)=-.2173E-3
DELOSS(6)=-.1172E-3
DELOSS(7)=-.743E-4
DELOSS(8)=-.354E-4
DELOSS(9)=-.193E-4
DELOSS(10)=-.101E-4
DELOSS(11)=-.713E-5
DELOSS(12)=-.410E-5
DELOSS(13)=-.244E-5
DELOSS(14)=-.166E-5
DELOSS(15)=-.131E-5
PREL(1)=1.25
PREL(2)=1.0
CUNVR=1.797.29577
READ INPUT TAPE 2,1,ALAT,EL,E
READ INPUT TAPE 2,2,R(1),R(2),R(3),R(4),R(5),R(6)
READ INPUT TAPE 2,2,R(7),R(8),R(9),R(10),R(11),R(12)
READ INPUT TAPE 2,2,SIG(1),SIG(2),SIG(3),SIG(4),SIG(5),SIG(6)
READ INPUT TAPE 2,2,SIG(7),SIG(8),SIG(9),SIG(10),SIG(11),SIG(12)
WRITE OUTPUT TAPE 3,4,ALAT,EL,H
ALAT0=ALAT,CUNVR
SVPR=PREL(1)
SVSG=SIG(1)
T=0.0
DU 300 M=1,15
ENERGE(M)
WRITE OUTPUT TAPE 3,5,ENER
WRITE OUTPUT TAPE 3,6
ALOSS=ELUSS(M)
DU 201 K=1,15
X(K)=UL(K)

```

500

```

STADY
      Y(K)=E(L)S(K)
201 CONTINUE
      CALL TABLE(ENL,R,ENAS,15)
      DO 20 J=1,12
      ALOSSA(J)=R(J)*ALCSS
      BLOSSA(J)=R(J)*EAS
20 CONTINUE
      NEW PAVE (DE/EXIATPUS AND (DICE/DAI)/DEIATPUS AS FUACTIONS
      C OF TIE FOR A GIVEN ENERGY AND L
      IF(ENER=00.) 21,21,22
21 AG=ALC
      A1=AL1
      A2=AL2
      R0=RLC
      B1=BL1
      B2=BL2
      EXT=.0494
      GO TO 23
22 AG=AH0
      A1=AH1
      A2=AH2
      R0=RH0
      B1=BH1
      B2=BH2
      EXT=.0696
23 CO=AOZ/(EL**2.*ENER**R0*CCSF(ALAT0)**4)
      C1=A1Z/(ENER**B1)
      C2=A2Z/(ENER**B2)
      KCK=0
      TI=T
20 ENI=C0*PREL(1)/(C1*ALCOSA(1)+C2*DLCOSSA(1)+C2*SIG(1))
      FLUX=ENI*C1*ENER**R2*.9795E1C
      TAU=ENI/ICG*PREL(1)*2.592E6
      WRITE OUTPUT TAPE 3,3,11,ENI,FLUXP,TAU
      WRITE OUTPUT TAPE 3,7,CG,C1,C2
      WRITE OUTPUT TAPE 3,8,ALCOSA(1),DLCOSSA(1),SIG(1)
      XX=CO*PREL(1)
      YY=C1*ALCOSA(1)+C2*DLCOSSA(1)+C2*SIG(1)
      WRITE OUTPUT TAPE 3,5,ENI,XX,YY
      IF(KCK) 301,31,301
31 TI=**4.
      ALOSSA(1)=ALCOSA(5)
      DLOSSA(1)=DLCOSSA(5)
      PREL(1)=PREL(5)
      SIG(1)=SIG(5)
      KCK=1
      WRITE OUTPUT TAPE 3,6
      GO TO 30
301 PREL(1)=SWPR
      SIG(1)=SVSG
300 CONTINUE
      GO TO 500
      FND(1,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0)

```



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```
TABLE
C  SUBROUTINE IC INTERPOLATE A GIVEN TABLE
  SUBROUTINE TABLE(XARG,YANS,LL)
  DIMENSION X(15),Y(15)
  COMMON X,Y
  IF(LL)11,11,12
  12 DO 10 K=1,LL
    A=Y(K)
    Y(K)=LQGF(A)
  10 CONTINUE
  11 DO 20 J=1,15
    IF(X(J)-XARG)20,21,22
  21 ANS=Y(J)
  22 H1=X(J)
    Y1=Y(J)
    H0=X(J-1)
    Y0=Y(J-1)
    ANS=Y1-(Y1-Y0)*(H1-XARG)/(H1-H0)
  20 CONTINUE
  50 IF(LL) 41,41,42
  41 YANS=ANS
  42 YANS=EXP(ANS)
  23 RETURN
  END(1,0,0,0,0,0,0,0,0,0,0,0,0,0,0)
```

TABLE

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STORAGE NOT USED BY PROGRAM

DEC CCT  
110 00156  
32531 77423

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC CCT  
X 32561 77461  
Y 32546 77452  
DEC CCT DEC CCT DEC CCT

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENT

DEC CCT  
ANS 109 00155  
Y0 104 00150  
A 108 00154  
Y1 103 00147  
F0 107 00153  
H1 106 00152  
DEC CCT DEC CCT DEC CCT  
J 105 00151

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC CCT  
11 99 00143  
E17 43 00060  
2) 92 00134  
E1C 82 00122  
DEC CCT DEC CCT DEC CCT  
C1C 102 00146  
D140A 75 00113

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC CCT  
EXP 1 00601  
LOG 0 00000  
DEC CCT DEC CCT DEC CCT

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

EXP LCC  
EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS  
EFN IFN LCC EFN IFN LCC EFN IFN LCC EFN IFN LCC  
12 6 00031 10 5 00043 11 10 00045 21 12 00053 22 14 00061  
20 20 00111 50 21 00114 41 22 00117 42 24 00123 23 25 00130



## F. Input

Input to this program occurs on logical tape 2 and consists of B, L,  $\lambda$ , R(1), ..., R(12)  $\Sigma$  (1), ...,  $\Sigma$  (12) for each case under consideration. As with the conservation equation calculation the B-L- $\lambda$  card is followed by two R cards which are followed in turn by two  $\Sigma$  cards. The control cards are left out of this program since there is only one method of computation available here.

### 1. Input Card Description

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
B-L- $\lambda$ Card	1-8	F	ALAT	degrees	latitude
	9-16	F	EL	earth radii	magnetic field line
	17-24	F	B	gauss	magnetic induction
First					
R Card	1-10	E	R(1)	-	scale factor R for TIME(1)
	11-20	E	R(2)	-	scale factor R for TIME(2)
	21-30	E	R(3)	-	scale factor R for TIME(3)
	31-40	E	R(4)	-	scale factor R for TIME(4)
	41-50	E	R(5)	-	scale factor R for TIME(5)
	51-60	E	R(6)	-	scale factor R for TIME(6)
Second					
R Card	1-10	E	R(7)	-	scale factor R for TIME(7)
	11-20	E	R(8)	-	scale factor R for TIME(8)
	21-30	E	R(9)	-	scale factor R for TIME(9)
	31-40	E	R(10)	-	scale factor R for TIME(10)
	41-50	E	R(11)	-	scale factor R for TIME(11)
	51-60	E	R(12)	-	scale factor R for TIME(12)
First					
$\Sigma$ Card	1-10	E	SIG(1)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(1)
	11-20	E	SIG(2)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(2)
	21-30	E	SIG(3)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(3)
	31-40	E	SIG(4)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(4)

	<u>Columns</u>	<u>Mode</u>	<u>Quantity</u>	<u>Units</u>	<u>Description</u>
	41-50	E	SIG(5)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(5)
	51-60	E	SIG(6)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(6)
<b>Second</b>					
$\Sigma$ Card	1-10	E	SIG(7)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(7)
	11-20	E	SIG(8)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(8)
	21-30	E	SIG(9)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(9)
	31-40	E	SIG(10)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(10)
	41-50	E	SIG(11)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(11)
	51-60	E	SIG(12)	atoms/cm	atmospheric loss parameter $\Sigma$ for TIME(12)

## 2. Sample

# GENERAL PURPOSE DATA SHEET

Problem	INPUT - STEADY STATE	Date	SAMPLE	Page	of
Sponsor	TAPE 2				
1					
2					
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5					
6	9730	1.1420	0.2239		
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## G. Output

Output for this program occurs on tape 3. Time, density, flux, mean lifetime,  $dE/dX$ ,  $d(dE/dX)/dE$ ,  $\Sigma$ , source and loss are all printed for each energy level at a given B, L and latitude. The headings are listed below with explanations and dimensions:

TIME - time - years

N(E) - density - # protons/cm<sup>3</sup> Mev.

FLUX - flux - # protons/cm<sup>2</sup> sec. Mev.

MEAN LIFETIME - proton mean lifetime - sec.

C0 - C<sub>0</sub> (see MNEMONICS) - # protons/cm<sup>3</sup> sec. Mev.

C1 - C<sub>1</sub> (see MNEMONICS) - cm/sec. Mev.

C2 - C<sub>2</sub> (see MNEMONICS) - cm/sec. Mev.

ALOSSA -  $(dE/dX)$  ATMOS - Mev./cm.

DLOSSA -  $(d(dE/dX)/dE)$  ATMOS - cm<sup>-1</sup>

SIG -  $\Sigma$  - atoms/cm

SOURCE - conservation equation source term - # protons/cm<sup>3</sup> Mev.

LOSS - conservation equation loss term - # protons/cm<sup>3</sup> Mev.

ENERGY - energy - Mev.

LATO - latitude - degrees

L - magnetic field line - earth radii

B - magnetic induction - gauss

LATO=	12.954	L=	1.188	B=	0.2331			
ENERGY=	10.00MEV							
TIME	N(E)		FLUX		MEAN LIFETIME			
0.	0.7172E-13		0.00031		0.30695E-04			
CO=	0.72115E-15	C1=	0.10386E 09	C2=	0.21759E 10			
ALOSSA=	0.47404E-10	DLOSSA=	0.35124E-11	SIG=	0.13080E-14			
N(E)=	0.71720E-13	SOURCE=	0.90144E-15	LOSS=	0.12569E-01			
TIME	N(E)		FLUX		MEAN LIFETIME			
4.000	0.7083E-13		0.00031		0.37893E-04			
CO=	0.72115E-15	C1=	0.10386E 09	C2=	0.21759E 10			
ALOSSA=	0.38400E-10	DLOSSA=	0.28452E-11	SIG=	0.10610E-14			
N(E)=	0.70831E-13	SOURCE=	0.72115E-15	LOSS=	0.10131E-01			
ENERGY=	25.00MEV							
TIME	N(E)		FLUX		MEAN LIFETIME			
0.	0.2246E-13		0.00015		0.95765E-04			
CO=	0.72376E-16	C1=	0.64318E 08	C2=	0.33586E 10			
ALOSSA=	0.22595E-10	DLOSSA=	0.76320E-12	SIG=	0.13080E-14			
N(E)=	0.22457E-13	SOURCE=	0.90470E-16	LOSS=	0.40286E-02			
TIME	N(E)		FLUX		MEAN LIFETIME			
4.000	0.2218E-13		0.00015		0.11822E-03			
CO=	0.72376E-16	C1=	0.64318E 08	C2=	0.33586E 10			
ALOSSA=	0.18303E-10	DLOSSA=	0.61823E-12	SIG=	0.10610E-14			
N(E)=	0.22178E-13	SOURCE=	0.72376E-16	LOSS=	0.32634E-02			
ENERGY=	50.00MEV							
TIME	N(E)		FLUX		MEAN LIFETIME			
0.	0.9981E-14		0.00009		0.24227E-03			
CO=	0.12715E-16	C1=	0.44760E 08	C2=	0.46886E 10			
ALOSSA=	0.12956E-10	DLOSSA=	0.21465E-12	SIG=	0.13080E-14			
N(E)=	0.99806E-14	SOURCE=	0.15894E-16	LOSS=	0.15925E-02			
TIME	N(E)		FLUX		MEAN LIFETIME			
4.000	0.9857E-14		0.00009		0.29908E-03			
CO=	0.12715E-16	C1=	0.44760E 08	C2=	0.46886E 10			
ALOSSA=	0.10495E-10	DLOSSA=	0.17387E-12	SIG=	0.10610E-14			
N(E)=	0.98567E-14	SOURCE=	0.12715E-16	LOSS=	0.12900E-02			
ENERGY=	75.00MEV							
TIME	N(E)		FLUX		MEAN LIFETIME			
0.	0.6368E-14		0.00007		0.42753E-03			
CO=	0.45973E-17	C1=	0.36207E 08	C2=	0.56891E 10			
ALOSSA=	0.94431E-11	DLOSSA=	0.97214E-13	SIG=	0.13080E-14			
N(E)=	0.63681E-14	SOURCE=	0.57466E-17	LOSS=	0.90241E-03			
TIME	N(E)		FLUX		MEAN LIFETIME			
4.000	0.6289E-14		0.00007		0.52777E-03			
CO=	0.45973E-17	C1=	0.36207E 08	C2=	0.56891E 10			
ALOSSA=	0.76493E-11	DLOSSA=	0.78748E-13	SIG=	0.10610E-14			
N(E)=	0.62890E-14	SOURCE=	0.45973E-17	LOSS=	0.73100E-03			
ENERGY=	100.00MEV							
TIME	N(E)		FLUX		MEAN LIFETIME			
0.	0.4893E-14		0.00006		0.69244E-03			
CO=	0.21809E-17	C1=	0.22509E 08	C2=	0.65475E 10			
ALOSSA=	0.76002E-11	DLOSSA=	0.57659E-13	SIG=	0.13080E-14			
N(E)=	0.48928E-14	SOURCE=	0.27261E-17	LOSS=	0.55716E-03			
TIME	N(E)		FLUX		MEAN LIFETIME			
4.000	0.4832E-14		0.00006		0.85460E-03			
CO=	0.21509E-17	C1=	0.22509E 08	C2=	0.65475E 10			
ALOSSA=	0.61565E-11	DLOSSA=	0.46707E-13	SIG=	0.10610E-14			
N(E)=	0.48320E-14	SOURCE=	0.21309E-17	LOSS=	0.45134E-03			
ENERGY=	125.00MEV							
TIME	N(E)		FLUX		MEAN LIFETIME			
0.	0.3812E-14		0.00005		0.95289E-03			
CO=	0.12348E-17	C1=	0.19444E 08	C2=	0.76899E 10			
ALOSSA=	0.64599E-11	DLOSSA=	0.38193E-13	SIG=	0.13080E-14			
N(E)=	0.38123E-14	SOURCE=	0.15435E-17	LOSS=	0.40488E-03			
TIME	N(E)		FLUX		MEAN LIFETIME			
4.000	0.3765E-14		0.00005		0.11763E-02			

CO= 0.12348E-17	C1= 0.19444E 08	C2= 0.70699E 10	
ALOSSA= 0.52328E-11	DLOSSA= 0.30938E-13	SIG= 0.10610E-14	
N(E)= 0.37650E-14	SOURCE= 0.12348E-17	LOSS= 0.32798E-03	
ENERGY= 150.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.3115E-14	0.00005	0.12391E-02
CO= 0.77584E-18	C1= 0.17252E 08	C2= 0.75275E 10	
ALOSSA= 0.56631E-11	DLOSSA= 0.27029E-13	SIG= 0.13080E-14	
N(E)= 0.31148E-14	SOURCE= 0.96980E-18	LOSS= 0.31135E-03	
ENERGY= 200.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.3076E-14	0.00005	0.15296E-02
CO= 0.77584E-18	C1= 0.17252E 08	C2= 0.75275E 10	
ALOSSA= 0.46035E-11	DLOSSA= 0.21895E-13	SIG= 0.10610E-14	
N(E)= 0.30761E-14	SOURCE= 0.77584E-18	LOSS= 0.25222E-03	
ENERGY= 200.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.2258E-14	0.00004	0.18701E-02
CO= 0.37265E-18	C1= 0.14285E 08	C2= 0.83106E 10	
ALOSSA= 0.46921E-11	DLOSSA= 0.15451E-13	SIG= 0.13080E-14	
N(E)= 0.22579E-14	SOURCE= 0.46582E-18	LOSS= 0.20630E-03	
ENERGY= 250.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.2230E-14	0.00004	0.23084E-02
CO= 0.37265E-18	C1= 0.14285E 08	C2= 0.83106E 10	
ALOSSA= 0.38008E-11	DLOSSA= 0.12516E-13	SIG= 0.10610E-14	
N(E)= 0.22298E-14	SOURCE= 0.37265E-18	LOSS= 0.16713E-03	
ENERGY= 250.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.1753E-14	0.00003	0.25641E-02
CO= 0.21100E-18	C1= 0.12340E 08	C2= 0.89736E 10	
ALOSSA= 0.40869E-11	DLOSSA= 0.98392E-14	SIG= 0.13080E-14	
N(E)= 0.17529E-14	SOURCE= 0.26375E-18	LOSS= 0.15046E-03	
ENERGY= 300.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.1731E-14	0.00003	0.31651E-02
CO= 0.21100E-18	C1= 0.12340E 08	C2= 0.89736E 10	
ALOSSA= 0.33106E-11	DLOSSA= 0.79702E-14	SIG= 0.10610E-14	
N(E)= 0.17310E-14	SOURCE= 0.21100E-18	LOSS= 0.12189E-03	
ENERGY= 300.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.1404E-14	0.00003	0.32680E-02
CO= 0.13257E-18	C1= 0.10949E 08	C2= 0.95545E 10	
ALOSSA= 0.36805E-11	DLOSSA= 0.68303E-14	SIG= 0.13080E-14	
N(E)= 0.14037E-14	SOURCE= 0.16571E-18	LOSS= 0.11805E-03	
ENERGY= 350.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.1386E-14	0.00003	0.40338E-02
CO= 0.13257E-18	C1= 0.10949E 08	C2= 0.95545E 10	
ALOSSA= 0.29813E-11	DLOSSA= 0.55329E-14	SIG= 0.10610E-14	
N(E)= 0.13861E-14	SOURCE= 0.13257E-18	LOSS= 0.95643E-04	
ENERGY= 350.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.1142E-14	0.00002	0.39376E-02
CO= 0.89495E-19	C1= 0.98958E 07	C2= 0.10075E 11	
ALOSSA= 0.33896E-11	DLOSSA= 0.50877E-14	SIG= 0.13080E-14	
N(E)= 0.11418E-14	SOURCE= 0.11187E-18	LOSS= 0.97978E-04	
ENERGY= 400.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.1127E-14	0.00002	0.48601E-02
CO= 0.89495E-19	C1= 0.98958E 07	C2= 0.10075E 11	
ALOSSA= 0.27458E-11	DLOSSA= 0.41212E-14	SIG= 0.10610E-14	
N(E)= 0.11274E-14	SOURCE= 0.89495E-19	LOSS= 0.79381E-04	
ENERGY= 400.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.9561E-15	0.00002	0.46341E-02
CO= 0.63676E-19	C1= 0.90659E 07	C2= 0.10548E 11	
ALOSSA= 0.31723E-11	DLOSSA= 0.38580E-14	SIG= 0.13080E-14	
N(E)= 0.95607E-15	SOURCE= 0.79596E-19	LOSS= 0.83253E-04	
ENERGY= 400.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.9440E-15	0.00002	0.57195E-02

CO= 0.63676E-19	C1= 0.90659E 07	C2= 0.10548E 11	
ALOSSA= 0.25697E-11	DLOSSA= 0.31252E-14	SIG= 0.10610E-14	
N(E)= 0.94400E-15	SOURCE= 0.63676E-19	LOSS= 0.67454E-04	
ENERGY= 500.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.6953E-15	0.00002	0.59518E-02
CO= 0.36054E-19	C1= 0.78313E 07	C2= 0.11390E 11	
SSA= 0.28715E-11	DLOSSA= 0.24088E-14	SIG= 0.13080E-14	
N(E)= 0.69526E-15	SOURCE= 0.45068E-19	LOSS= 0.64821E-04	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.6864E-15	0.00002	0.73491E-02
CO= 0.36054E-19	C1= 0.78313E 07	C2= 0.11390E 11	
ALOSSA= 0.23260E-11	DLOSSA= 0.19512E-14	SIG= 0.10610E-14	
N(E)= 0.68642E-15	SOURCE= 0.36054E-19	LOSS= 0.52525E-04	
ENERGY= 600.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.5248E-15	0.00001	0.71499E-02
CO= 0.22653E-19	C1= 0.69485E 07	C2= 0.12127E 11	
ALOSSA= 0.26761E-11	DLOSSA= 0.16081E-14	SIG= 0.13080E-14	
N(E)= 0.52477E-15	SOURCE= 0.28316E-19	LOSS= 0.53959E-04	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.5181E-15	0.00001	0.88230E-02
CO= 0.22653E-19	C1= 0.69485E 07	C2= 0.12127E 11	
ALOSSA= 0.21678E-11	DLOSSA= 0.13026E-14	SIG= 0.10610E-14	
N(E)= 0.51805E-15	SOURCE= 0.22653E-19	LOSS= 0.43727E-04	
ENERGY= 700.00MEV			
TIME	N(E)	FLUX	MEAN LIFETIME
0.	0.4033E-15	0.00001	0.81399E-02
CO= 0.15292E-19	C1= 0.62302E 07	C2= 0.12788E 11	
ALOSSA= 0.25414E-11	DLOSSA= 0.11503E-14	SIG= 0.13080E-14	
N(E)= 0.40331E-15	SOURCE= 0.19115E-19	LOSS= 0.47397E-04	
TIME	N(E)	FLUX	MEAN LIFETIME
4.000	0.3981E-15	0.00001	0.10044E-01
CO= 0.15292E-19	C1= 0.62302E 07	C2= 0.12788E 11	
ALOSSA= 0.20586E-11	DLOSSA= 0.93180E-15	SIG= 0.10610E-14	
N(E)= 0.39811E-15	SOURCE= 0.15292E-19	LOSS= 0.38412E-04	

#### H. Running Time

This program will do eleven cases in a minute and a half.



## IX. REFERENCES

1. Blanchard, R.C., Hess, W.N., "Solar Cycle Effects in Inner Zone Protons," NASA, GSFC Publ. X-640-64-50, March, 1964.
2. Harris, I., and Priester, W., "Theoretical Models for the Solar-Cycle Variation of the Upper Atmosphere," NASA, GSFC publ. X-640-62-70, June 1962.
3. McIlwain, C.E., "Coordinates for Mapping the Distribution of Magnetically Trapped Particles," Journal of Geophysical Research, vol. 66, (1961), pp. 3681-3691.
4. Jensen, D.C., and Cain, J.C., unpublished, presented at April, 1962, meeting of the American Geophysical Union, Washington, D.C.
5. Ray, Ernest, C., "On the Theory of Protons Trapped in the Earth's Magnetic Field," Journal of Geophysical Research, vol. 65, no. 4, April, 1960, pp. 1125-1133.
6. Scarborough, J.B., Numerical Mathematical Analysis, 3rd Edition, Oxford University Press, copyright, 1955.
7. Aron, W.A., Hoffman, B.C., Williams, F.C., "Range-Energy Curves" (2nd Rev. 1949) U.S.A.E.C., Univ. of Calif. Rad. Lab.

# X. ILLUSTRATIONS

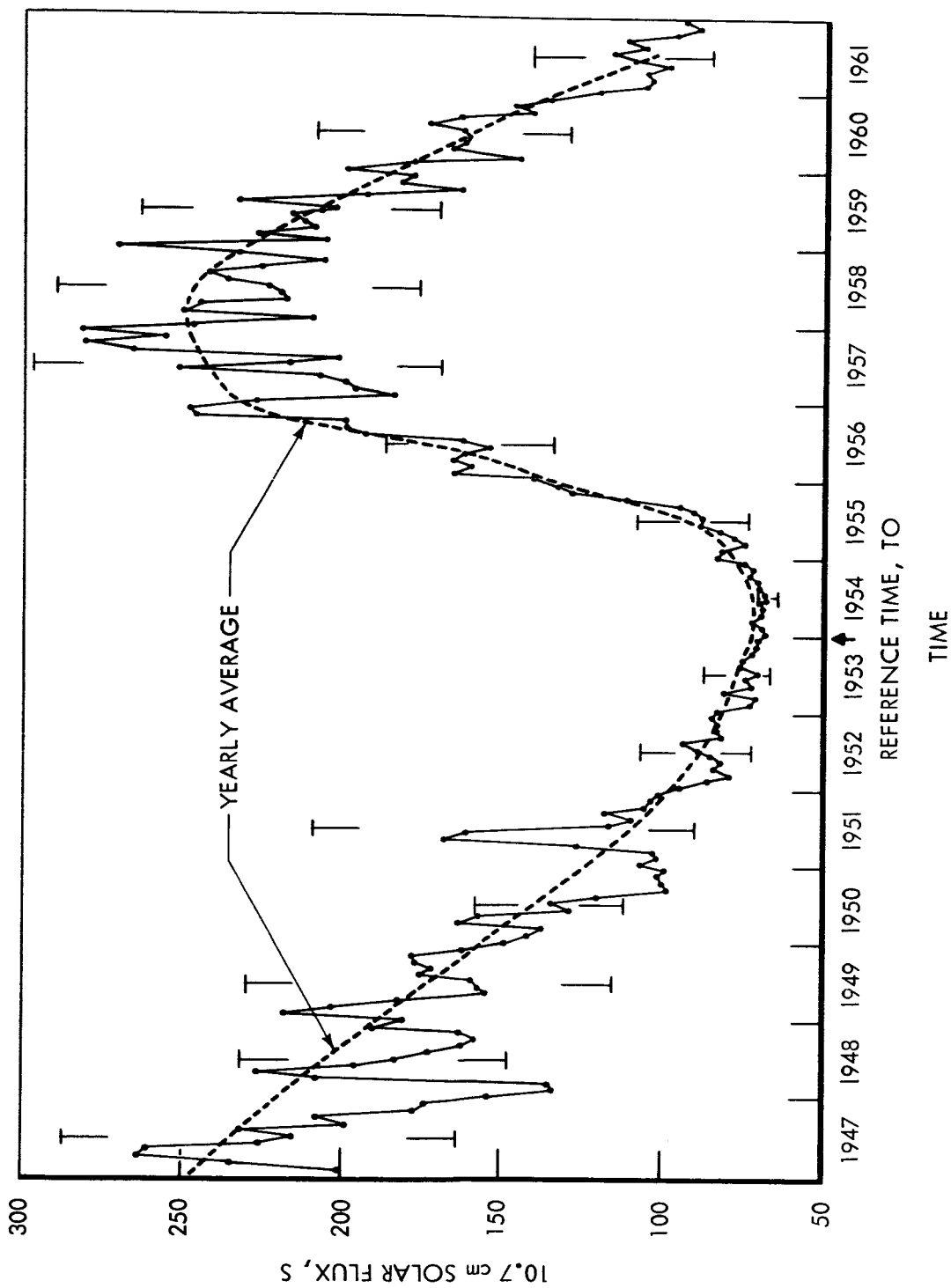


Figure 1-A time history of the 10.7 cm solar flux according to the measurements of the National Research Council of Canada for the recent past. The heavy dotted line indicates the approximate yearly average.

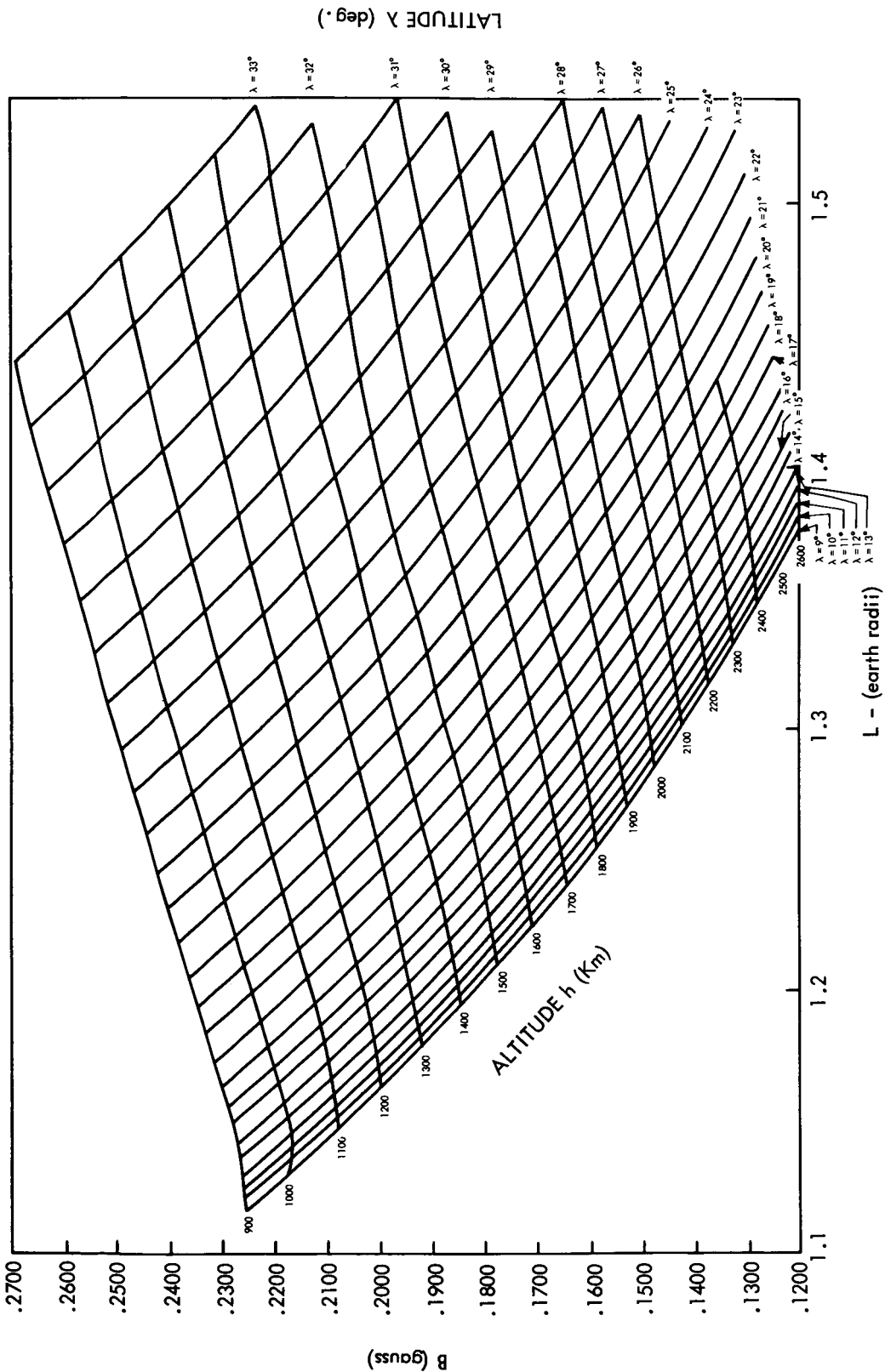


Figure 2-A mapping of the polar coordinates  $R$  and  $\lambda$  onto the B-L plane  
 where  $R = (h + 6378.2)$

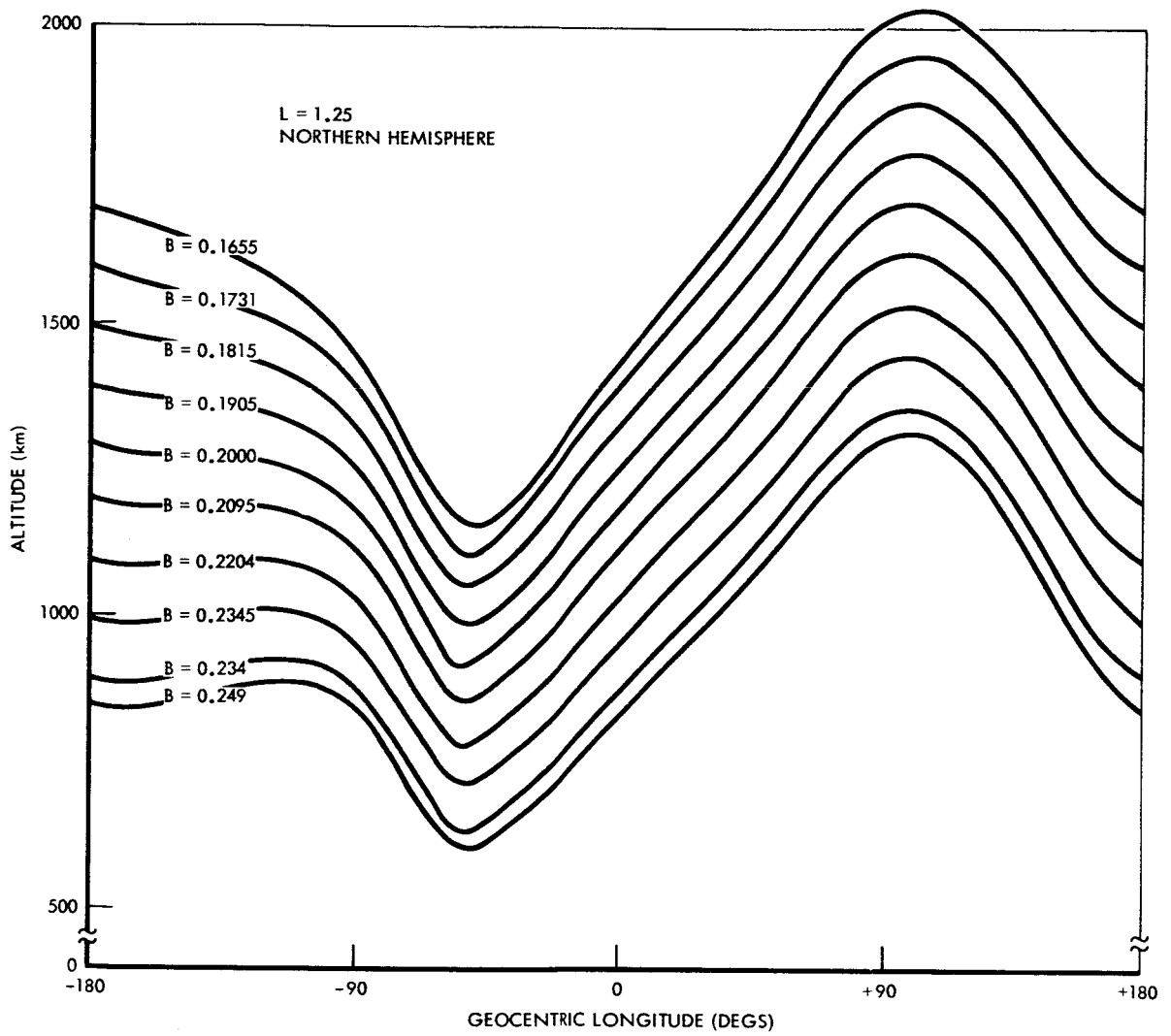


Figure 3-B-L contours for the northern hemisphere at an  
L of 1.25 earth radii

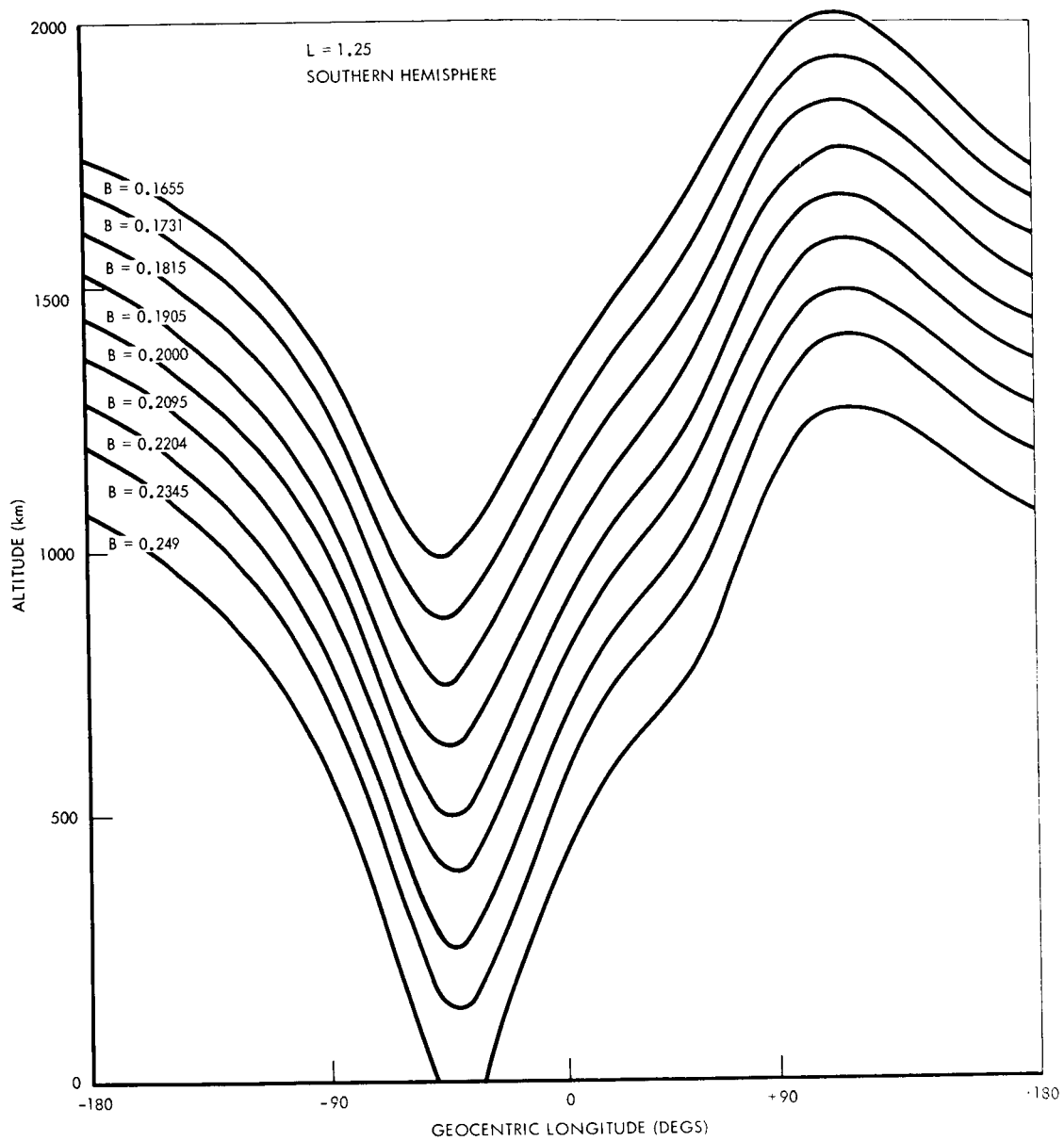
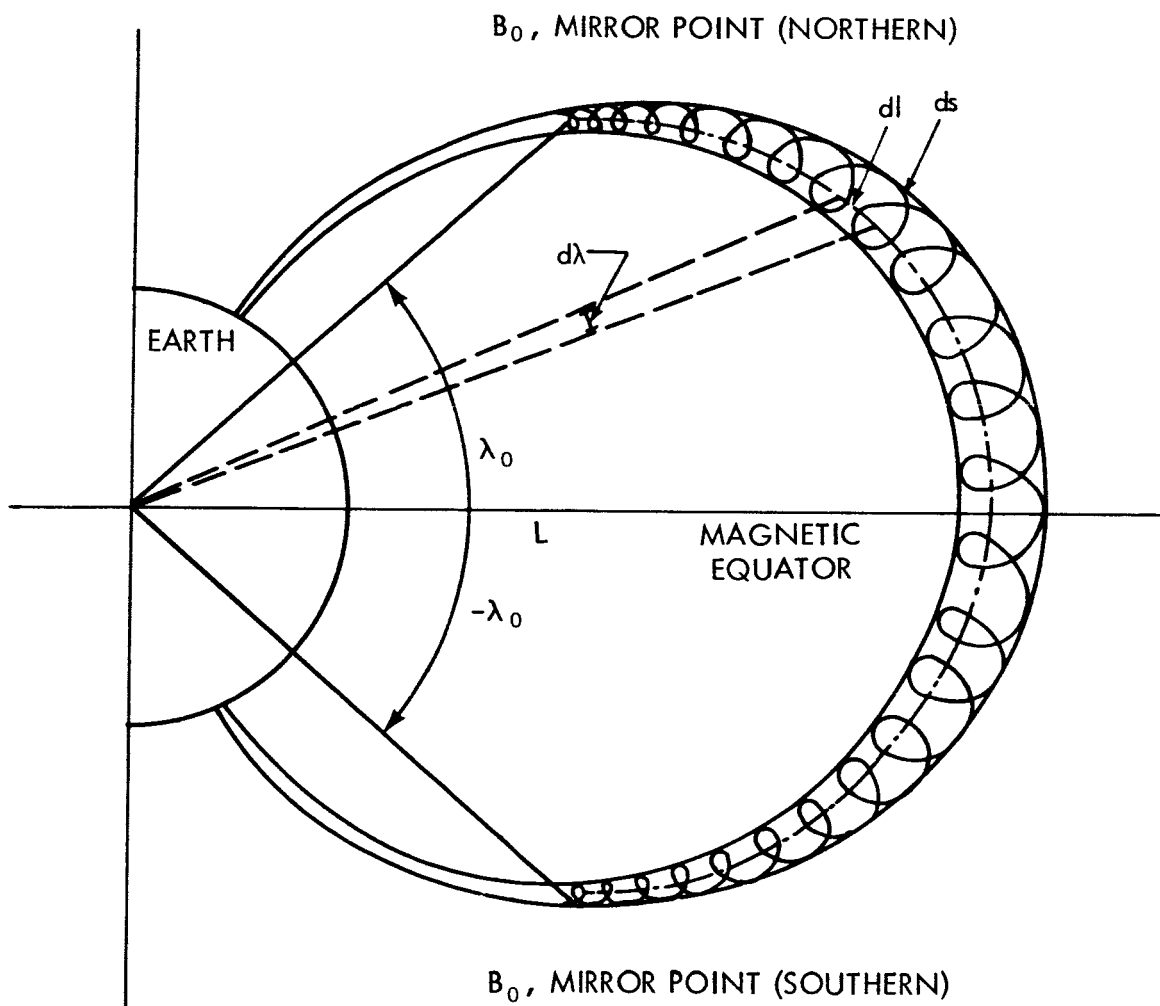


Figure 4-B-L contours for the southern hemisphere at an L of 1.25 earth radii



WHERE:

$ds$  - Element of Arc along the particle's helical trajectory

$dl$  - Element of Arc along the field line

Figure 5-Schematic of a trapped particle's north-south motion

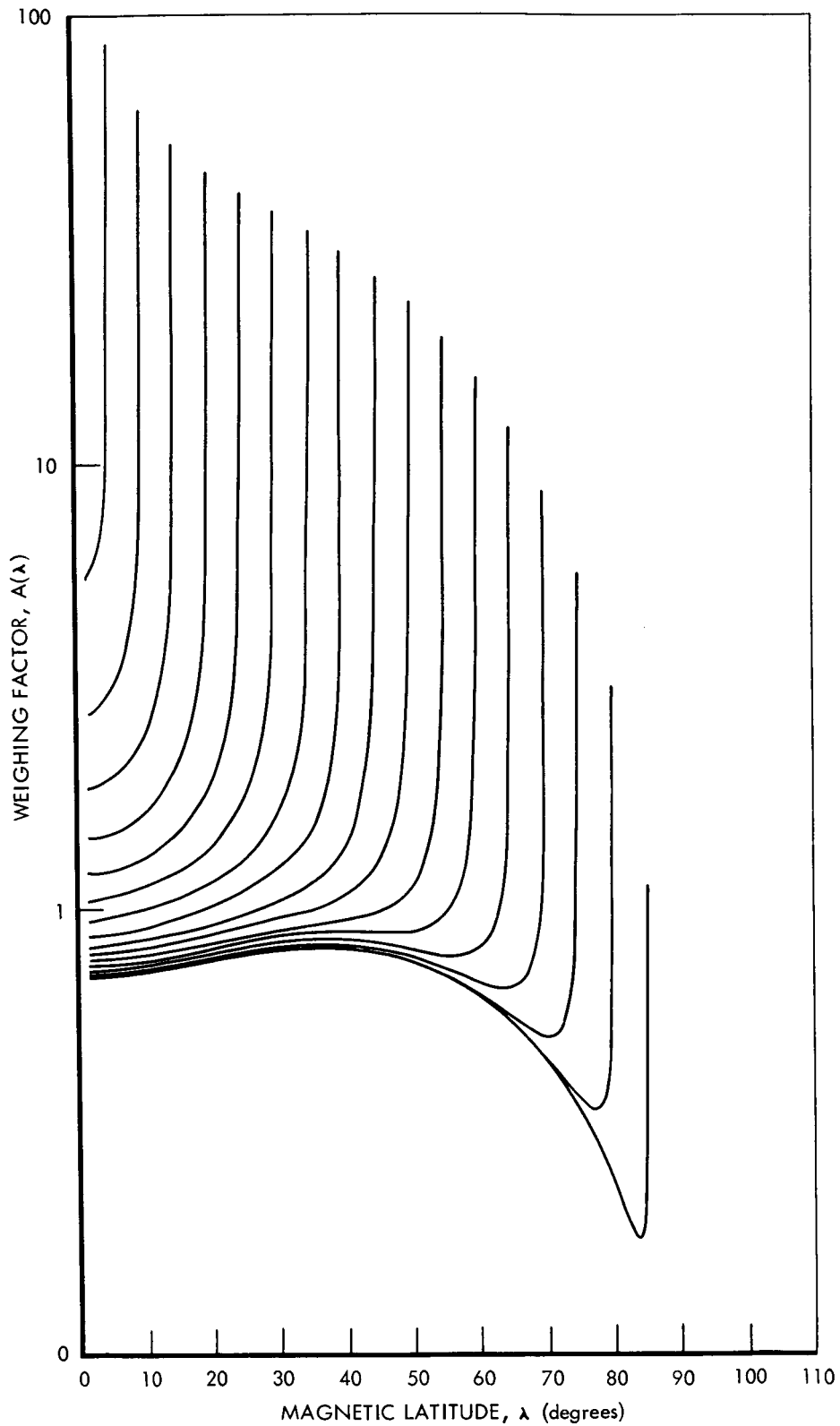


Figure 6-The weighing factor,  $A(\lambda)$ , versus latitude for various mirror latitudes,  $\lambda_0$ , where  $\lambda_0$  are the asymptotes of each curve

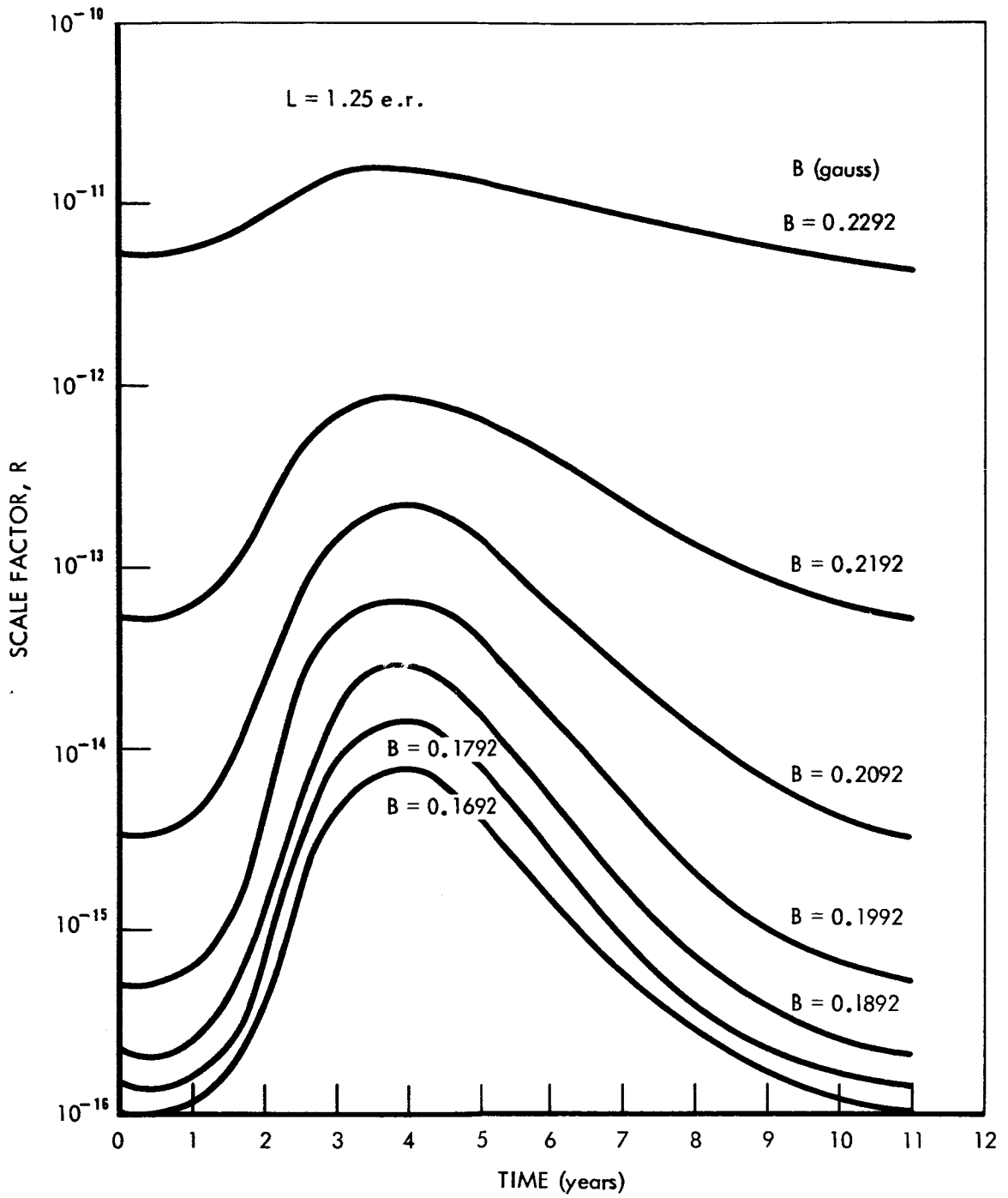


Figure 7-A time history of the atmosphere scale factor, R, as a function of B at L = 1.25 e.r.



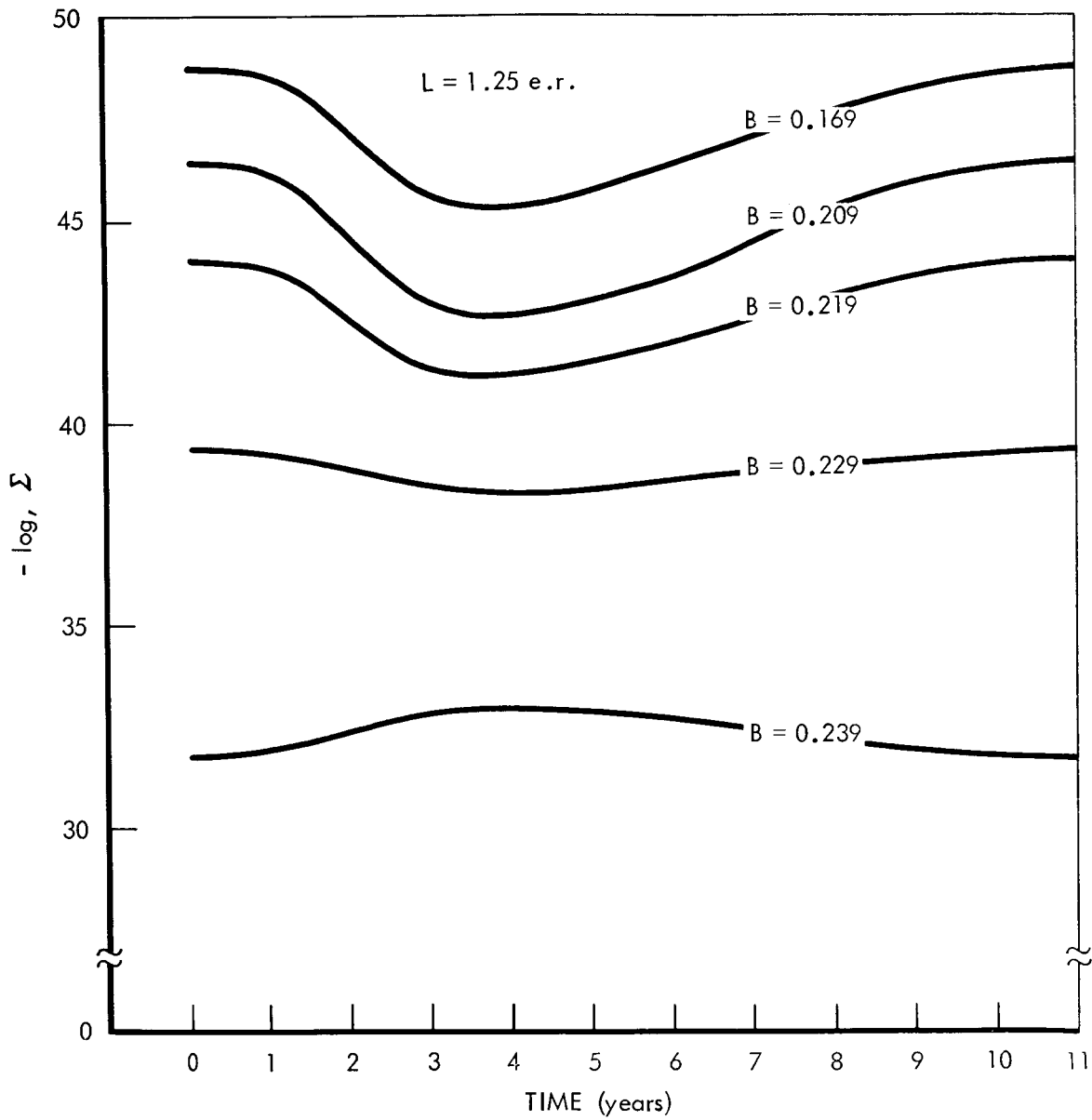


Figure 8-A time history of the atmospheric loss parameter  $\Sigma$ , as a function of  $B$  at  $L = 1.25 \text{ e.r.}$

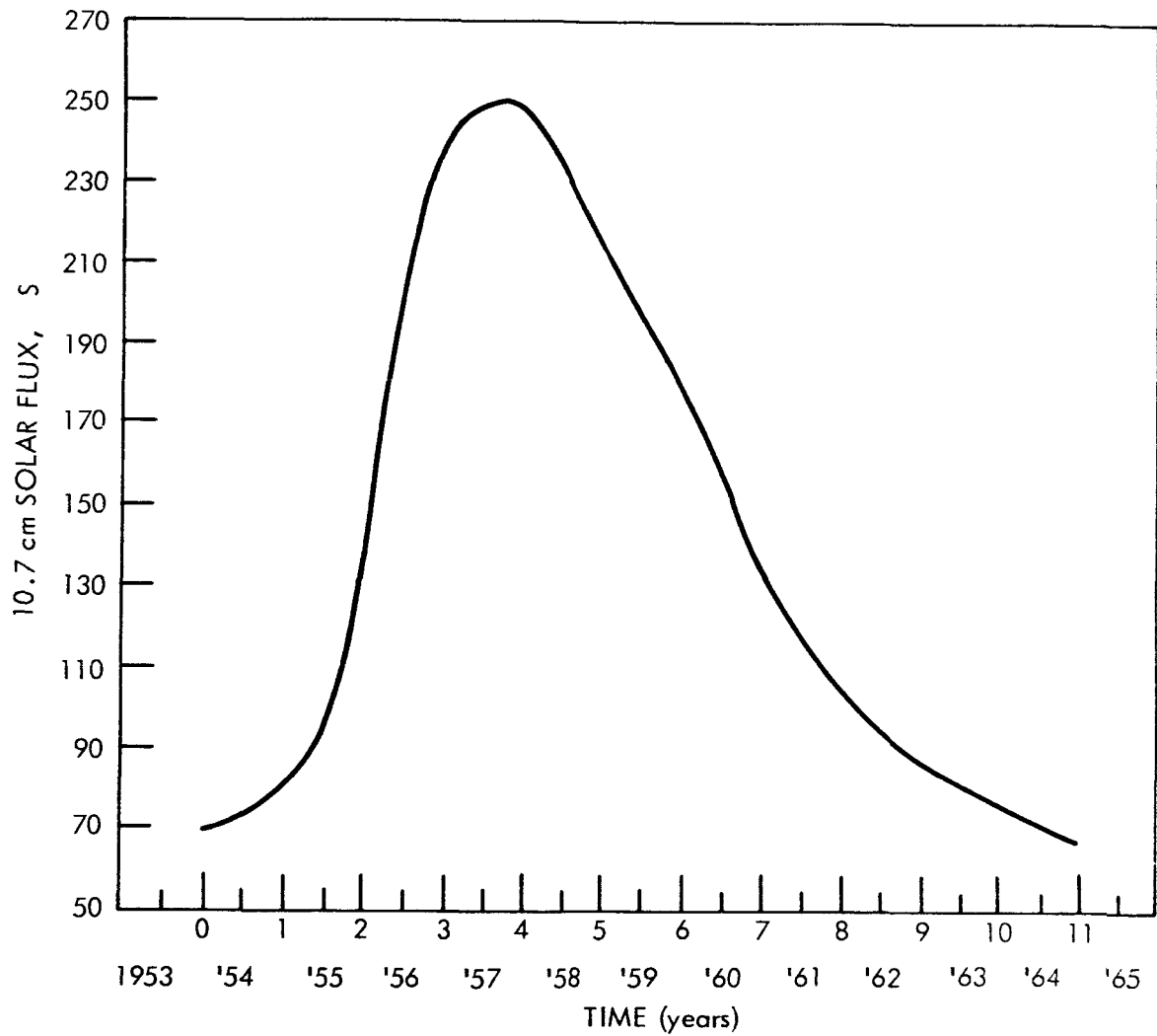


Figure 9-A time history of the constructed mean solar cycle variation of the 10.7 cm. solar flux with reference time  $t_0$  of Jan., 1954

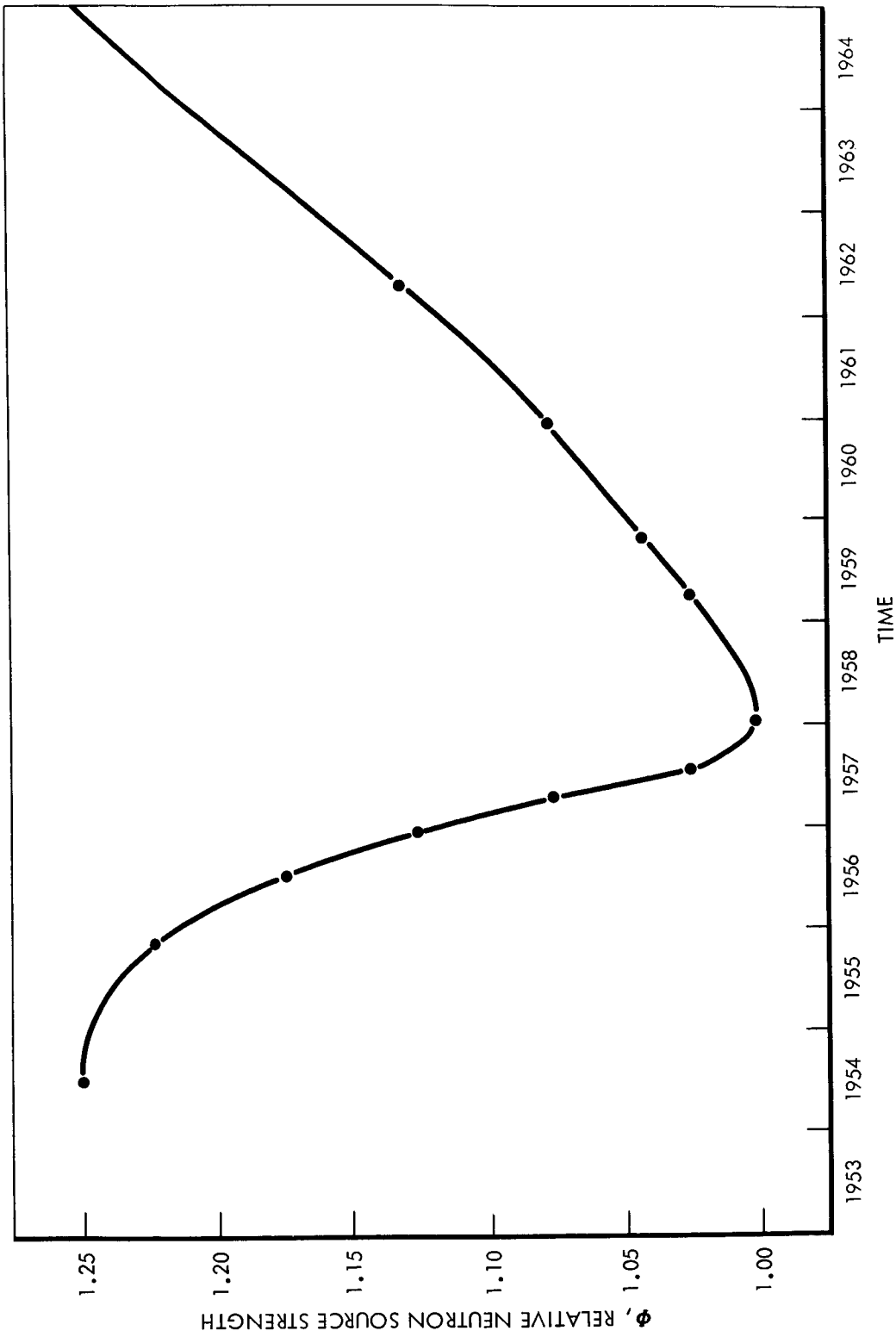


Figure 10-A time history of the relative inner belt source strength

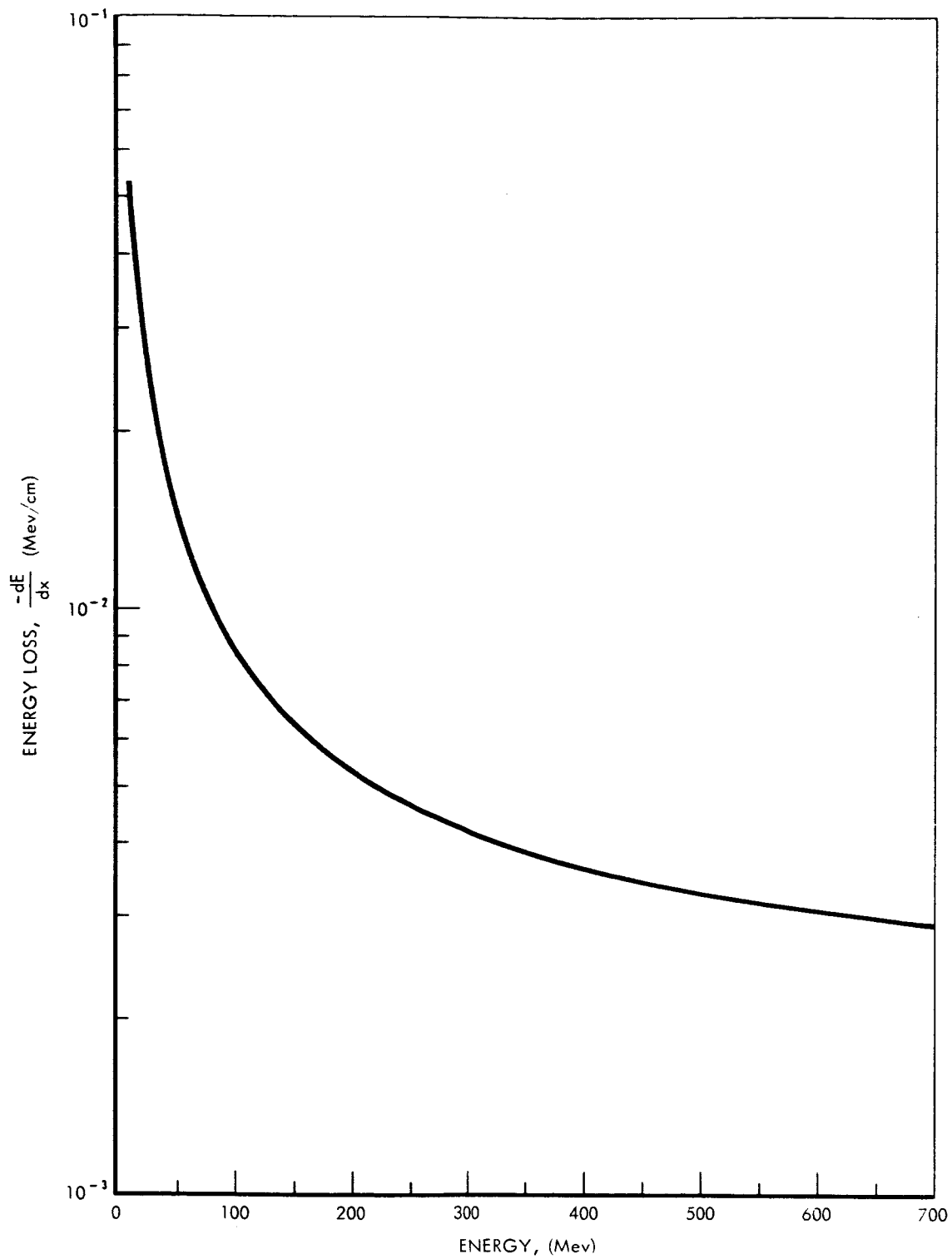


Figure 11-The proton energy loss spectrum for an oxygen target

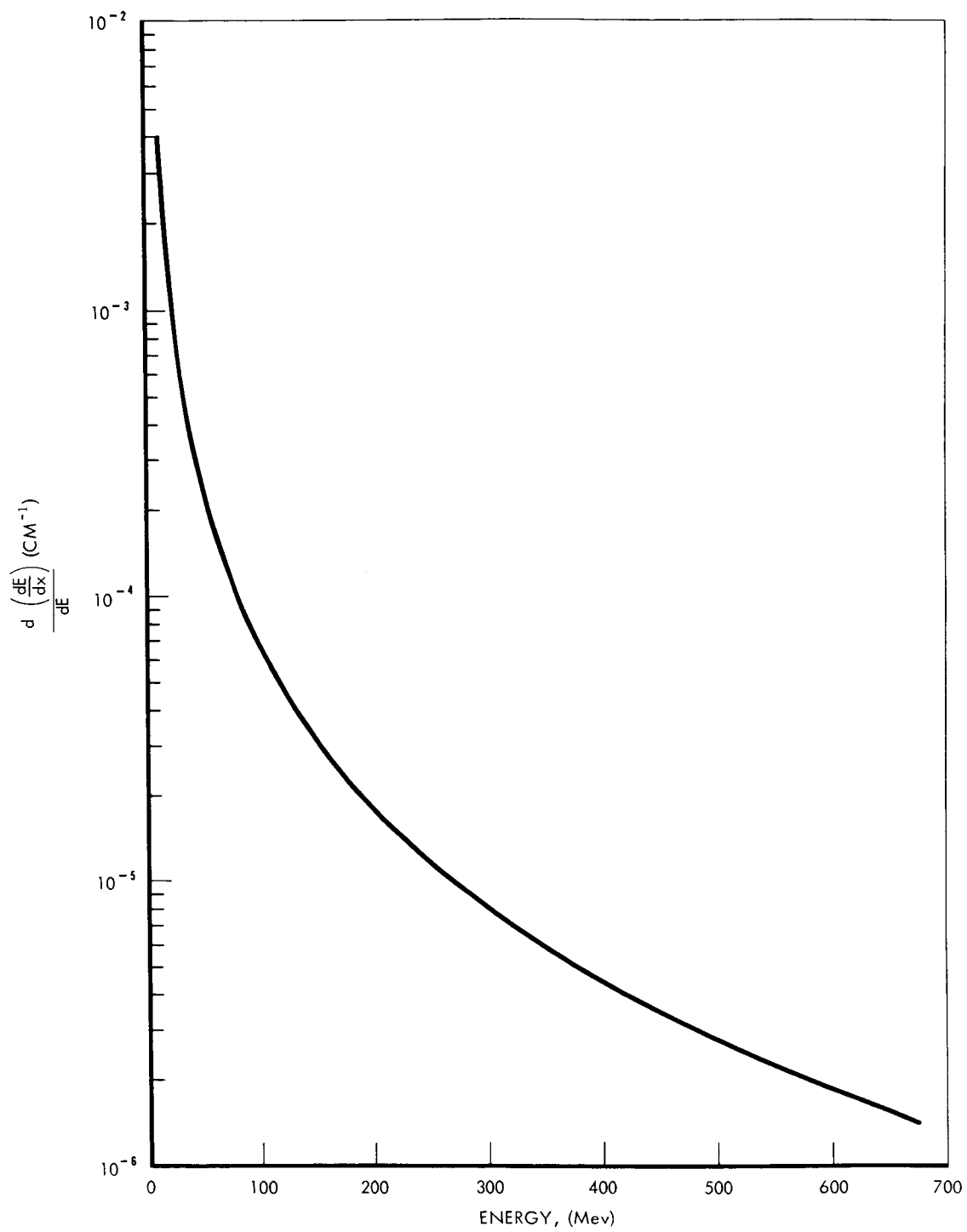


Figure 12-The slope of proton energy loss versus energy for an oxygen target

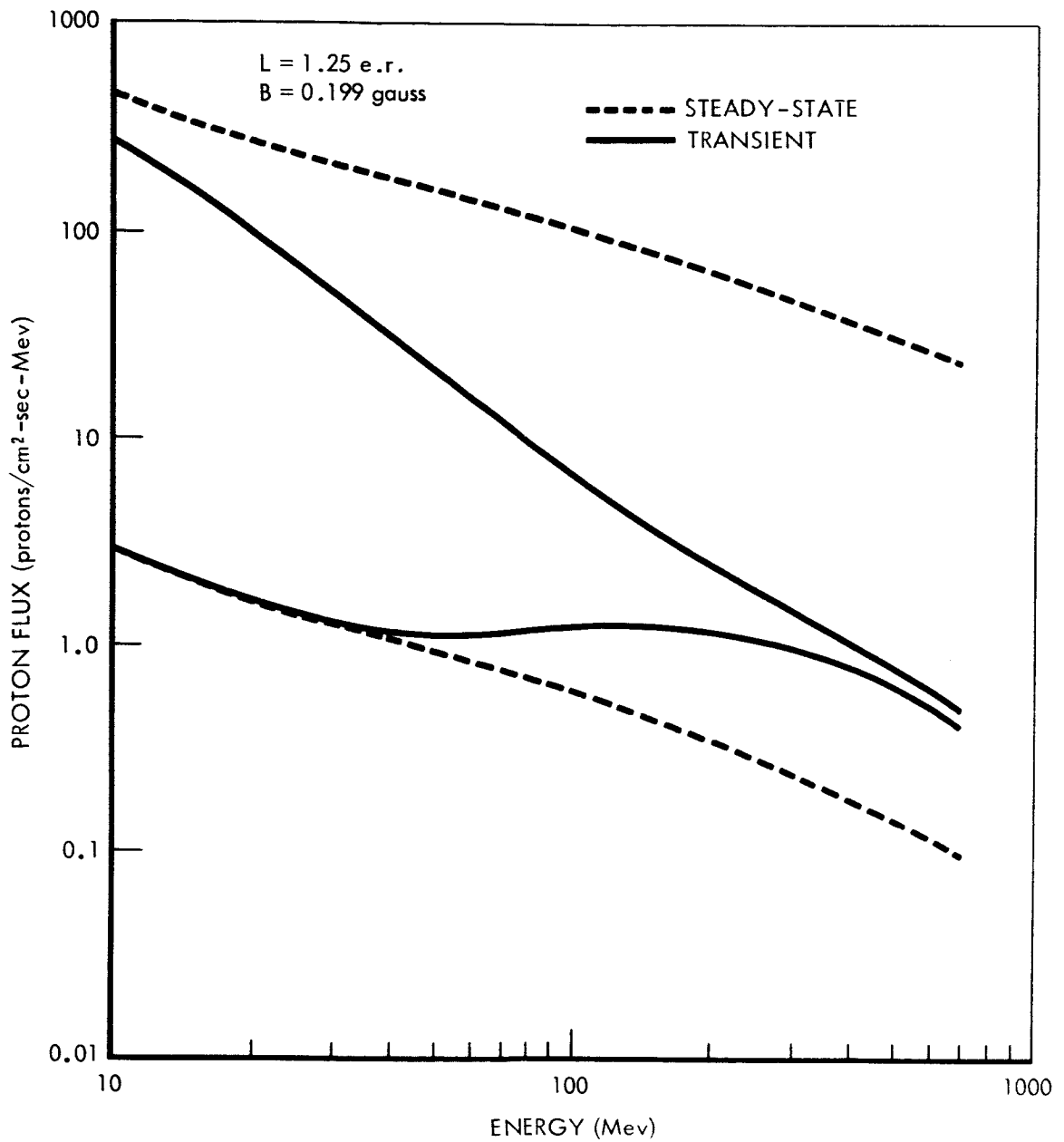


Figure 13-A comparison of the steady-state and transient proton flux energy spectrums for  $L = 1.25$ ,  $B^* = .199$  at solar minimum and solar maximum

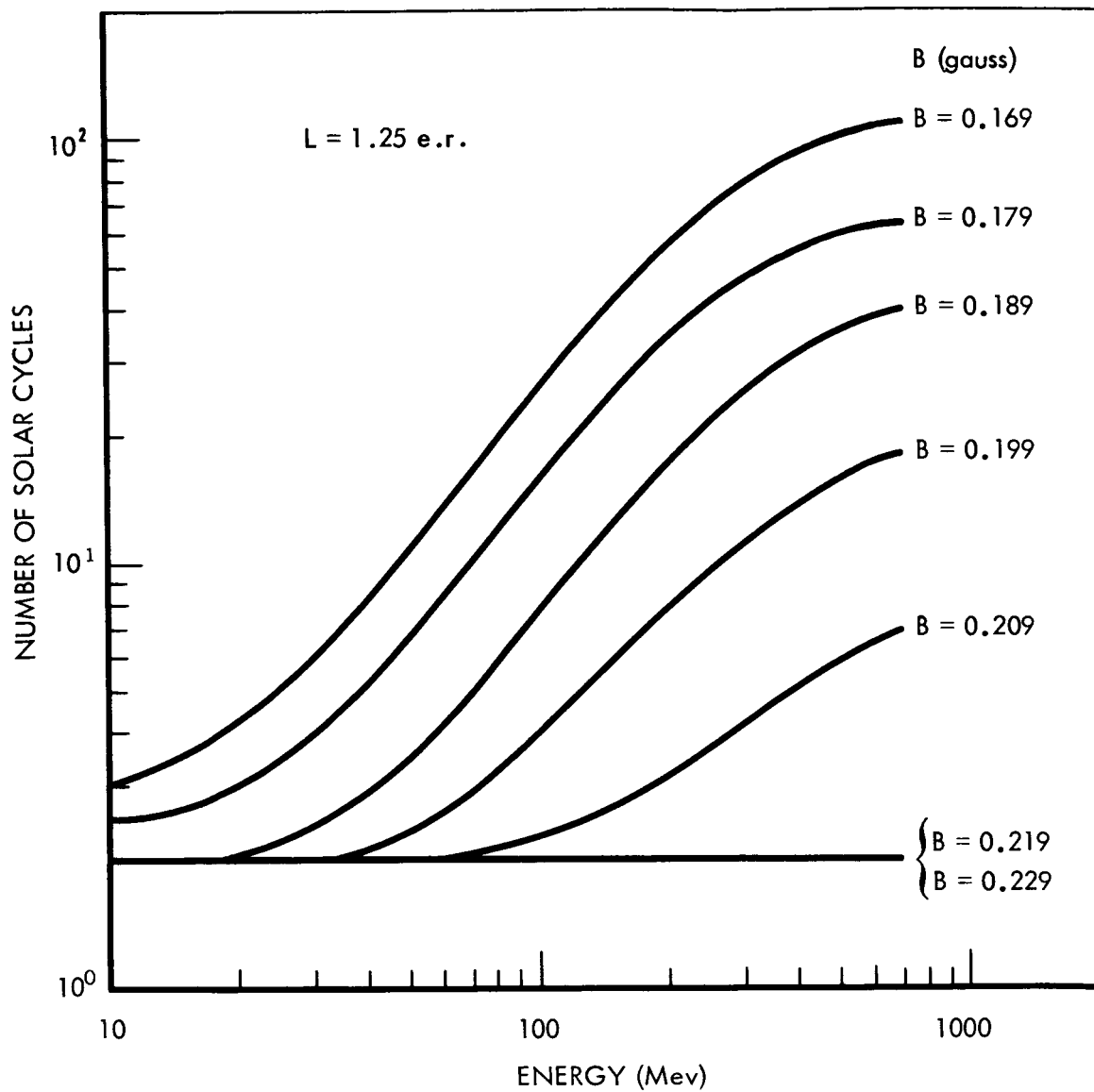


Figure 14-The time required in terms of solar cycles to build steady state conditions versus energy as a function of B

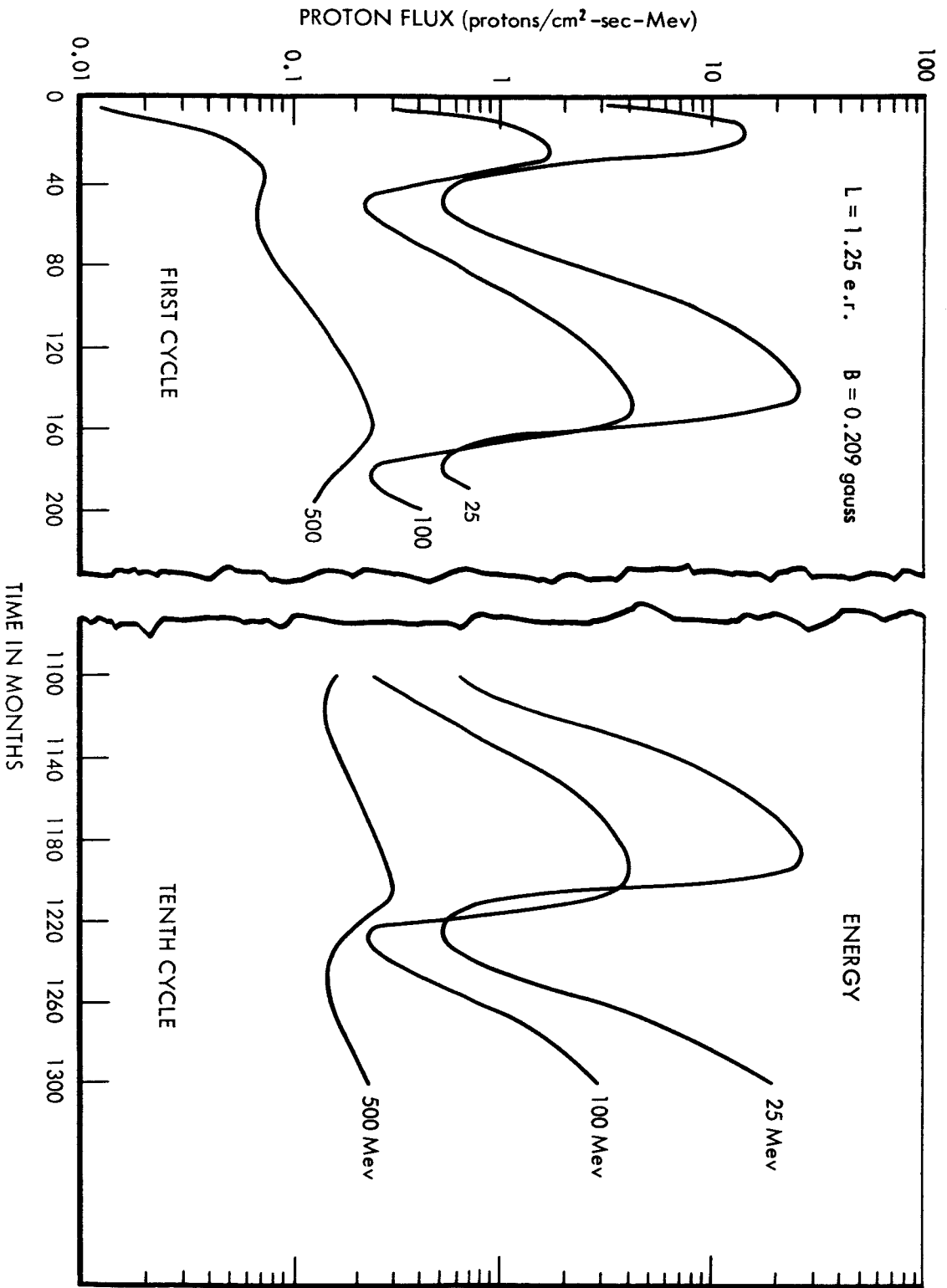


Figure 15-A time history of proton flux as a function of energy at L = 1.25, B = .209 for the first and tenth solar cycles