



Į.



E-TR-53



DTIC FORM 70A



The Earth Technology Cor, soration

AD A11 2959

MX SITING INVESTIGATION WATER RESOURCES PROGRAM REVIEW DRAFT WATER APPROPRIATIONS HEARING PRESENTATION AND SUPPORT DOCUMENTATION

, Š

)

1

DRY LAKE VALLEY, NEVADA

VOLUME II

Prepared for:

U.S. Department of the Air Force Ballistic Missile Office Norton Air Force Base, California 92409

Prepared by:

Ertec Western, Inc. 3777 Long Beach Boulevard Long Beach, California 90807

30 September 1981

REPORT DOCUMENTATION	PAGE	READ 'NSTRUCTIO
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUM
F - tr - 53 - TT		
A TITLE (and sublide) ILENTED KESDICCO	head	5. TYPE OF REPORT & PERIOD
PEDieco Diart Mater Apar	poriotions	
HEDRING Presentation + 500	DOT	NON X
Draine station Drubake	lolley NV 1	6. PERFORMING ORG. REPORT
Vol.		$E - 7 f - 53 - \overline{H}$
7. AUTHOR(s)		8. CONTRACT OR GRANT NUMB
		CONTRACTOR C
E(tec		FC4709-801-0
PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT PROJE
Entro WENTER TOP Cloumerly	Firm National)	AREA & WORK UNIT NUMBER
Prilibex 7765		LUZIDE
Loop Beach Ca 90507		CT STAT
1. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
U.S. Department & the An	-lorce	3C Sep 81
Space and thiss ite system	US CECEDURANIC	13. NUMBER OF PAGES
Norton AFIS (092409	<u>(SAMSO)</u>	<u> </u>
14. MONITORING AGENCY NAME & ADDRESS(If different	t from Controlling Office)	15. SECURITY CLASS. (of this re
		154 DECLASSIEICATION DOWN
		SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)		······································
Metala time De	alimited.	
DISTINGIA OF		
	in Black 20 if different from	Paperti
17. DISTRIBUTION STATEMENT (of the abstract entered)	m Block 20, it atterent non	(Report)
and all a stime in	1 = $t = c0$	
DISTRIBUTION U	nnmea	
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary an	d identify by block number)	
()allogs Well OPSI	an Gravit	y surveys,
Connegs, were bes	j , s de	
for the second provide a second	,	
n - n an an Arra an an an Arra an Ar	and present of a	
20. ABSTRACT (Continue on reverse side if necessary and	lidentily by block number)	the Dara
more preserve	~ integia	" ON UK TWO W
Meers of 1 altensive A	1X Water	Pesnimes
OFFER FOR MALL HE	_ \ 	
いいい し つ ひいしん	$\rightarrow (\gamma \ N)\gamma$	-Ut sting -
.)		- (4
<u> </u>		
J		

المريشة فالمعام

ł

1

.

.

LIST OF APPENDICES

Appendix Number	
A1.0	Dry Lake Valley Section: MX Siting Investigation, Water Management Report
B1.0	Numerical Modeling Studies, Dry Lake Valley, October 1981
C1.0	Results of Aquifer Testing, Dry Lake Valley, October 1981
D1.0	Dry Lake Valley Section: MX Siting Investigation, Technical Summary Report (In Progress)
E1.0	Dry Lake/Delamar Valleys Section: MX Siting Investigation, Water Resources Program, Summary for Draft Environmental Impact Statement, FN-TR-38, revised 1 August 1980
F1.0	MX Siting Investigation, Gravity Survey - Dry Lake Valley, Nevada, FN-TR-33-DL, 17 March 1980
G1.0	Eakin, Thomas E., 1963, Ground-Water Appraisal of Dry Lake and Delamar Valleys, Lincoln County, Nevada: State of Nevada, Department of Conservation and Natural Resources, Ground-Water Resources-Reconnaissance Series Report 16, 26 p.
Н1.0	Miscellaneous Working Documents
H1.1	Well Logs and Reports to the State Engineer of Nevada
H1.2	Dry Lake Valley Well Log and Well Design (Valley-Fill)
H1.3	Dry Lake Valley Well Log and Well Design (Carbonate)

T

A1.0

DRY LAKE VALLEY SECTION: MX SITING INVESTIGATION, WATER MANAGEMENT REPORT

4.5 DRY LAKE VALLEY

4.5.1 Hydrologic Summary

Dry Lake Valley is a topographically open basin in Lincoln County, Nevada. Of the approximately 700 mi² (1813 km²) of valley area, 310 mi² (802.9 km²) are suitable for MX deployment (Table 4-10).

Dry Lake Valley is hydrologically connected with Muleshoe Valley, and the two valleys are considered as a single hydrographic unit by the Nevada State Engineer. Ground water in Dry Lake and Muleshoe valleys is essentially undeveloped, however, there are 20 acre-ft/yr ($0.02 \text{ hm}^3/\text{yr}$) of pending applications and 19 acre-ft/yr ($0.02 \text{ hm}^3/\text{yr}$) of certificated or permitted rights (Woodburn and others, 1981) for ground-water withdrawal. In addition, there is 21 acre-ft/yr ($0.02 \text{ hm}^3/\text{yr}$) of surface water use (DRI, 1980) in the valley.

The perennial yield is estimated at 3000 acre-ft/yr (3.70 hm^3/yr) for the Dry Lake-Muleshoe basin (State of Nevada, 1971). The combined peak-year MX water requirements in the two valleys, 3373 acre-ft/yr (4.16 hm^3/yr) for Dry Lake and 968 acre-ft/yr (1.19 hm^3/yr) for Muleshoe, in 1984 would exceed the Dry Lake-Muleshoe basin perennial yield by 1341 acre-feet (1.65 hm^3). However, the combined total ground water in storage within the upper 100 feet (30 m) of saturated sediments in Dry Lake and Muleshoe valleys is estimated at 2.8 million acre-feet (3452.4 hm^3) (State of Nevada, 1971). This suggests that the ground-water basin could sustain the peak MX water demand if temporary overdraft is allowed by the Nevada State Engineer.

		G	ENERAL F	PHYSIO	RAPHY				
Valley Area	Vall Leng	ley A ;th	wg. Vall Width	ley G	Guitabl Area	9	Avg. E	Valle levat	y Floor ion
700 sq	mi 38	mi	18 mi GENERAL		310 sq 3LOGY	mí		4800	ft
aquifer	Depth Water	to El	Potentic evation	netrio Rango	: e Tra	nsmiss	sivity	Sto	rativity
Valley-fil Carbonate	1 300-80 850 f	00 ft ft	4200-500	00 ft	33 13, 0	00 sq 00 sq	ft/da ft/da	ม 0 ม	. 06 -
ferennial Yield	Ground-Wai Recharge	ter (ppt)	Interbas Recharg	sin 1 je 1	Interba Dischar	sin ge	ET	Sur Dis	face charge
3000	2700		2100)	500	0	min	OT	-
WATER QUALITY									
Total Samples	Suitab: for Consumpt	le tion	Exceeds Standar	s (1) °ds	Suita fo Constr	ble r uctior	E n S	xceed tanda	s * rds
6	5		1	ن مله معر «له بنيه, جه م	5			0	
	WA	TER US	E AND AP	PROPRI	ATIONS	(2)			
Source	Current	Use	Applicat	ions	Certi Proofs/	ficate Permi	s/ Ava ts	ailab:	ility (3)
Ground Water	r 0		20		19		:	300072	2981
Surface Wate	er 21		2596 MX WAT	ER REQU	- JIREMEN	тз		-	
	1982	1983	1984	1985 :	1995 1	 987 1	1988	1989	1990
Constructi Operation	on 196	414	3373 2	2458 2	2014	225	0	0	0
 (1): Well near Bristol Silver Mine - exceeds state primary standard for nitrate (2): Dry Lake and Muleshoe valleys combined (3): Parennial Yield - Current Use / Perennial Yield - Certificated Use * : Portland Cament Association recommendations (1966). 						andard			
Note: feet p	Ali units er year ur	are in Ness o	acre- ther-				MX SIT DEPARTM	FING INV ENT OF 1 BMO/AFR	ESTIGATION THE AIR FORCE CE-MX
WISE N	uveu.			ſ			00100		
					H DR	LAKE	VALLE	UMMAN Y, NEV	ADA

 Γ

Surface water supplies are limited to ephemeral streamflow and springs. The springs are located mostly in the mountains, are generally unaccessible, and have low discharge (less than 2 gpm [0.13 1/s]).

A 10-day aquifer pump test conducted by Ertec in the southern part of the valley (3S-64E-12ca) (number 40433) indicates a generally unconfined valley-fill aquifer having an average transmissivity of 3300 ft²/day (306.6 m²/day) and a storativity of 0.06. Confined or semiconfined conditions are, however, expected in other portions of the valley due to the complex nature of the valley fill which was found to be composed of variable thicknesses of clay, silt, sand, and gravel.

The regional carbonate aquifer underlying and adjacent to the valley fill is considered to have a high potential for development. Data from an aquifer test performed by Ertec in the northern part of the valley (3N-63E-27cc) indicate a transmissivity in the carbonate aquifer of 13,000 ft²/day (1208 m²/day). The test well was pumped at a sustained rate of 106 gpm $(7 \ 1/s)$ with a drawdown of only 2 feet $(0.6 \ m)$. The hydrostratigraphic unit (Guilmette Formation and Simonson Dolomite) penetrated at the test site is considered to be a high-yield aquifer based on these investigations.

Water-chemistry tests on water samples collected by Ertec from both the valley-fill and carbonate aquifers show that all but one well, 3N-65E-21dba, meet primary and secondary drinking

water standards for the State of Nevada (Appendix D). This well, located in the northeastern part of Dry Lake Valley was found to have a nitrate concentration of 32 mg/l, which exceeds the 10 mg/l standard for nitrate. This well was, however, used for mining operations by the Bristol Silver Mine and is thought to be contaminated by mining-related activity.

4.5.2 Water-Supply Sources

Development of the valley-fill aquifer is the preferred source for the MX water supply in Dry Lake Valley (Table 4-11). Development of the valley-fill aquifer is projected to have the least potential impact on local water users and the environment, the highest physical development potential, and to be the least costly and the most timely to develop of the four water-supply options. The legal availability of ground water from the valley-fill aquifer was ranked second to importation because the estimated perennial yield of the hydrographic basin can supply only about 70 percent of the peak-year requirements. The quantity of ground water presently available for development, based on certificated and permitted water rights, is 2981 acre-ft/yr (3.68 hm³/yr). The estimated combined peak-year water requirement for Dry Lake and Muleshoe valleys is 4341 acre-feet (5.35 hm³) during 1984. However, there is essentially no ground-water use in Dry Lake Valley, and the State Engineer need not limit his decisions on the approval of ground-water applications to a comparison of approved water rights versus the perennial yield of the basin. Quantity, distribution, and type and length of

			Valle Âqu	y-řill ifer	Carbon Aquif	late er	Purch	se/ Jase	Import	ation
	Criteria	Weight	Scare	Nt. Score	Score	Wt. Score	Score	ut. Score	Score	Wt. Scor
	Legal Water Availability	10	Ч	70	r	70	0	o	ω	80
	Impacts on Man ar Environment	10	¢	0.6	œ	08	7	70	¢	60
	üevelopment Pot tial (Physical Arailability)	cen- 10	10	100	ω	C B	7	70	10	100
	i Čii t	4	10	40	n	(ປ +1	n,	50	o	0
	Timeliness	ሳ	1 Ū	φQ	CJ	1 13	~	42	1	4
	water Quality	ល	0	0	10	50	10	0 71	0	02
MX SIT	Final Weighted Score			380.4		÷ 274		525		266
ING INVESTIGATIO	* Recomendei so + First alterna	tive so	water Urce of	supply water	ųlqus					

M

current and proposed ground-water use is considered as well as the quantity of water in storage in the aquifer.

The development of the carbonate aquifer in Dry Lake Valley is considered a much more feasible alternative source of water supply than importation of water, even though it ranked only slightly higher than importation in the matrix evaluation. The results of a carbonate aquifer test conducted by Ertec near the northwest margin of the valley indicate that the carbonate aquifer has a high potential for development; however, development of the carbonate aquifer would be about three times more costly than the valley-fill aquifer and would require four times more time to construct the supply wells. The relatively high yield potential indicated by the existing carbonate test well suggests that some combination of pumping from the valley-fill and the carbonate aquifers may be viable.

Importation of water is ranked third among the four options, although it compares favorably with development of the carbonate aquifer. Importation ranked high because of the legal and physical water availability in the source valley, which would be Spring Valley. The matrix evaluation is weighted more toward legal and environmental considerations of water use and less toward MX water-supply system construction. However, importation of water from the nearest valley where it is plentiful is estimated to cost as much as 40 times development of the valley-fill aquifer and 14 times development of the carbonate aquifer.

Lease or purchase of existing water rights is presently not recommended because there are only 19 acre-ft/yr (0.02 hm^3/yr) of approved ground-water rights (Woodburn and others, 1981) and 21 acre-ft/yr (0.03 hm^3/yr) of surface-water rights (DRI, 1980). These total less than one percent of the MX peak-water requirement for Dry Lake and Muleshoe valleys combined in 1984.

4.5.3 Suitable Areas for Water-Supply Well Locations

Two large areas in Dry Lake Valley have been identified as primary areas for development of the valley-fill aquifer (Drawing 4-5). In the northern part of the valley, there is an extensive primary area in the central valley and flanking alluvial fans. In the central and southern part of the valley, a 0.25- to 3-mile (0.4- to 5-km) wide strip of primary areas occurs between the lacustrine sediments in the valley floor and the edge of the valley. In Township 3S, these strips coalesce into one and extend southward into Delamar Valley.

The primary area for development of the valley-fill aquifer in Dry Lake Valley is extensive and is capable of providing well locations for the construction and operation of the MX missile system.

Due to the extensive deposition of lacustrine deposits in central and southern Dry Lake Valley, a large area is classified as secondary. This area extends from the north-central part of Township 1N to the central part of Township 3S and is 5 to 6 miles (8 to 10 km) wide.

Additional small secondary areas have been delineated on the western flank of the valley in Township 1S and on the southwest flank of the mountains in Township 3S. These areas are classified as secondary on the basis of geophysical and water-level data which indicate that only thin saturated thicknesses of valley-fill sediments occur. There is only one Air Force water-appropriation application point of diversion in the valley, and it lies in a secondary water-supply well development area at 3S-64E-12ac (number 40433).

There is only one cultural exclusion within the valley-floor area in Dry Lake Valley which is located in Township 1S near the east side of the valley. There are, however, four waterappropriation exclusions in the northern part of the valley floor and two water-appropriation exclusions in the central portion of the valley floor. These exclusions include the area within 1 mile (1.6 km) of an existing ground-water or surfacewater appropriation. Other water-appropriation exclusions are found in the mountains adjacent to the valley. A possible regional spring occurs in Dry Lake Valley at 3N-65E-31cc.

4.5.4 Water-Supply System Alternatives

Based upon the available hydrologic data and the matrix analyses conducted as part of this investigation, there are three feasible MX water-supply alternatives for Dry Lake Valley. The alternative which can be ultimately used is largely dependent upon the decision of the State Engineer regarding temporary overdraft of the Dry Lake Valley ground-water basin. The three

alternatives, listed in order of priority from a technical standpoint, are discussed below.

4.5.4.1 Alternative I

The first alternative involves splitting the pending Air Force water-appropriation point of diversion at the existing Air Force test well at 3S-64E-12ca (number 40433) into multiple points of diversion, use of the existing test well at 3S-64E-12ca and the carbonate test well at 3N-63E-27cc, and the construction of two additional water-supply wells in the valley-fill aquifer. This approach will require the amendment of the pending application. This process should be initiated early in FY 82 to ensure that there is available water for the initial MX construction activities scheduled to begin in mid-1982.

The proposed LSC, presumed to be located in 3S-64E, will require from 230 to 1050 acre-ft/yr (0.28 to 1.29 hm³/yr) with the peak requirement in 1986. Based upon an estimated well yield of 750 gpm (47 l/s), only one water-supply well will be required to deliver the 651 gpm (41 l/s) needed for peak water use at the LSC. The existing Air Force test well at 3S-64E-12ca has been pumped at a maximum rate of 750 gpm (47 l/s) and, if a sustained yield of 651 gpm (41 l/s) is possible, no additional MX water-supply wells will be required. During the period from 1983 to 1985, and during 1987, surplus water from the existing well could be utilized for DTN and cluster construction in the southern end of the valley.

The development of MX water-supply wells for DTN and cluster construction, operation, and reclamation will require the use of the existing Air Force valley-fill well at 3S-64E-12ca, the use of the existing carbonate exploration well at 3N-63E-27cc, and the construction of two additional MX water-supply wells.

In 1982 and 1983, the entire MX water requirement in Dry Lake Valley can be met through the operation of the existing Air Force valley-fill well. In 1984, however, the existing Air Force carbonate exploration well located at 3N-63E-27cc and three additional wells will be required to deliver the 3373 acre-feet (4.16 hm³) which will be required. It is recommended that one additional valley-fill well be constructed in the primary area in the southern part of the valley and one valley-fill well be constructed in the primary area in the northern part of the valley. Assuming well yields of 650 gpm (41 1/s) or 1047 acre-ft/yr (1.29 hm³/yr) if pumped continuously, these wells should be capable of supplying more than the MX water requirement (3373 acre-feet [4.16 hm³]) during the peak-construction For the period from 1985 to 1986, the MX water requireyear. ments for nondomestic purposes decrease and a reduction in the pumping rates of the water-supply wells can occur.

4.5.4.2 Alternative II

If the State Engineer restricts MX ground-water withdrawal from the valley-fill aquifers of Dry Lake hydrographic basin (Dry Lake and Muleshoe valleys) to the perennial yield of 3000

acre-ft/yr $(3.70 \text{ hm}^3/\text{yr})$ but allows additional water to be withdrawn from the carbonate aquifer, as much as 1341 acre-feet (1.65 hm^3) may have to be withdrawn from the carbonate aquifer in 1984. This alternative would then involve splitting the pending Air Force water-appropriation point of diversion at the existing Air Force test well at 3S-64E-12ca (number 40433) into multiple points of diversion, use of the existing valley-fill aquifer test well at 3S-64E-12ca, increasing the diameter of the carbonate aquifer test well at 3N-63E-27cc, and the construction of an additional valley-fill and carbonate aquifer well.

Although the carbonate test well at 3N-63E-27cc had a sustained yield of 106 gpm (7 1/s), the drawdown in the well was only 2 feet (0.6 m). Discharge from the well was limited by the greater than 800 feet (244 m) water depth and by small well diameter. A larger capacity pump, necessitating a larger diameter well, can be expected to increase the well yield to at least 450 gpm (28 1/s) or 725 acre-ft/yr (0.89 hm³/yr) pumped continuously.

The entire MX water requirement in Dry Lake Valley can be met through the operation of the existing Air Force test well at 3S-64E-12ca in 1982, 1983, and 1987. In 1984, however, two carbonate wells, including the existing carbonate well at 3N-63E-27cc with an increased diameter, and one additional well in the valley-fill aquifer would be used to supply the required water. In 1985, most of the required water can be supplied by two wells tapping the valley-fill aquifer and only minimal water will be needed from a well in the carbonate aquifer. No water will be required from the carbonate aquifer in 1986.

4.5.4.3 General Well Characteristics

An Air Force well constructed in the valley-fill aquifer at 3S-64E-12ca (number 40433) was pumped at a constant discharge rate of 500 gpm (32 1/s), and results suggest that a higher sustained yield is possible. The valley-fill well was constructed with a 16-inch (41-cm) borehole and a 10-inch (25-cm) ID casing to a total depth of 1012 feet (308 m). Larger diameter wells may be capable of greater sustained yields if the same favorable aquifer is penetrated. Although the depth to water ranges from about 800 feet (244 m) below land surface in the northern part of the valley to over 300 feet (91 m) in the southernmost part of the valley, the depth to productive aquifer may be substantially greater. Therefore, it is recommended that MX water-supply wells be constructed to depths of at least 1200 feet (366 m). Due to the lack of hydrologic data for aquifer characteristics and well yields for much of Dry Lake Valley, it is recommended that exploratory drilling be conducted to verify the proposed locations of other MX water-supply wells.

4.5.5 Additional Investigations

Suggested possible sites for additional drilling and testing prior to operational development of the water-supply system are identified in Drawing 4-5.

An application was filed for only one point of diversion in Dry Lake Valley at 3S-64E-12ca (number 40433). The request for water at this point of diversion was sufficient to meet the peak MX water requirement for construction in the valley.

Two additional drilling sites have been identified beyond the application point of diversion in Dry Lake Valley. These sites were selected along existing roads in primary water-supply areas delineated in Drawing 4-5.

The drilling site located at 3N-64E-2ac in the northern part of the valley is the first priority. The site is located 3 miles (5 km) south of the proposed construction camp at the northern end of Dry Lake Valley. A well at this location could provide data on water quantity and quality, both of which will be necessary for planning domestic water supply at the construction camp. This site is also strategically located with respect to clusters and is approximately 1 mile (1.6 km) from the DTN in an area where little or no aquifer performance data exist.

The drilling site at 2N-64E-36cc is centrally located with respect to the DTN and the clusters. The site at 2N-64E-36cc in north-central Dry Lake Valley is approximately 12 miles (19 km) south of a proposed construction camp. Aquifer data within a 5-mile (8-km) radius are limited to one stock well. ______T

























- b <i>Pill</i>		
	EXPLANATION	
	SYMBOLS	
		- AIR FORCE OBS. WELL
PO	WERLINE(S)	AIR FORCE TEST WELL
TI	ELEPHONE/TELEGRAPH	DOMESTIC/STOCK WELL
mmmm P	IPELINE	MUNICIPAL/IRRIGATION WELL
	BAINAGE DIVIDE	UNDESIGNATED WELL
	VALLEY BOUNDARY	ABANDONED WELL
	ROCK-VALLEY FILL CONTACT	SPRING
??	PREFERRED AREA BOUNDARY:	STREAM APPROPRIATION
	QUERIED WHERE GEOPHYSICAL PART	UNDESIGNATED APPROPRIATION
	GREATER MARGIN OF ERHUN	
	- CULTURAL OR WATER APPROPRIATION	W HESSENER EVISTING WELL, UNVERIF
	AREAS OF OTHER EXCIUSIONS	WATER APPROPRIATION
41222	AIR FORCE WATER APPROPRIATION (APPLICATION NUMBER SHOWN)	
41221	AIR FORCE WATER APPROPRIATION: ADDITIONAL DRULLING/TESTING RECOMMENDED (APPLICATION NUMBER SHOWN)	,
\$	ADDITIONAL DRILLING/TESTING RECOMMENDED LOCATION	12





E

Nator rights in Nevada I the MX area, Water If Nevada System, un-

her resources, ke Valley, Nevada, kale.

ting investigation, ley, Nevada, port, 30 January 1980.

ing investigation, Lake Valley, Nevada, Cale, July 1980.

tion study, Dry **7-DL** V. I, V. II.



NORTH

SCALE 1:62,500

1 STATUTE MILES 1 n KILOMETERS

The Earth Technology Corporation

DRY LAKE VALLEY, NEVADA PREFERRED AREAS FOR MX WATER-SUPPLY WELLS

28 SEPT 81

DRAWING 4-5
B1.0

NUMERICAL MODELING STUDIES, DRY LAKE VALLEY C1.0

RESULTS OF AQUIFER TESTING, DRY LAKE VALLEY

•

-

I

D1.0

DRY LAKE VALLEY SECTION: MX SITING INVESTIGATION, TECHNICAL SUMMARY REPORT

-

2.8 DRY LAKE VALLEY

2.8.1 GENERAL PHYSIOGRAPHY AND HYDROLOGY

Dry Lake Valley is a north-trending basin in Lincoln County, Nevada. The valley is topographically open to Muleshoe Valley to the north and is separated from Delamar Valley to the south by a low alluvial divide. Dry Lake and Muleshoe valleys are considered one hydrologic basin by the Nevada State Engineer. Dry Lake Valley is 38 miles (61 km) long, 21 miles (34 km) across at its widest point, and encompasses 700 mi² (1812 km2), of which 310 mi² (803 km²) are suitable for MX deployment. The average valley floor elevation is 4800 feet (1463 m). The valley is bordered by the North Pahroc Range on the west and the Burnt Springs, Highland and Bristol ranges on the east. The mountain crests range in elevation from about 7000 feet (2134 m) to over 9000 feet(2743 m).

Perennial streamflow is absent in Dry Lake Valley there is some ephemeral surface-water inflow from Muleshoe Valley, however, total runoff from the mountains at the apex of the alluvial fans is estimated to be 9000 acre-ft/yr (ll.1 hm³/yr) (Nevada State Engineer, 1971). This estimate is for the combined Dry Lake, Muleshoe, and Delamar valleys hydrographic areas. Small springs in or near the base of the mountains surrounding Dry Lake Valley issue from the clastic rocks of Paleozic age and the volcanic and clastic rocks of Tertiary age. Four springs discharged from 0.5 to 2 gpm (0.03 to 0.1 l/s), when measured in May 1980 by Ertec personnel. Ground-water recharge is from the infiltration of precipitation in stream channels and surface runoff on the alluvial fans. The average annual recharge for Dry Lake/Muleshoe valleys is estimated to be 4800 acre-ft/yr (5.9 hm^3/yr) (Eakin, 1963). Of this amount, approximately 2100 acre-ft/yr (2.6 hm^3/yr) is derived from precipitation in the mountains around Muleshoe Valley with the remainder from sources within Dry Lake. Evapotranspiration and water discharged by wells is less than 100 acre-ft/yr (0.1 hm^3/yr). Evapotranspiration only occurs in limited areas near small springs.

The Dry Lake Valley basin is a hydrologically open system with underlfow to the south or southwest and possibly to the west through the carbonates of Paleozoic age. Total discharge by underflow is estimated to be 5000 acre-ft/yr (6.2 hm^3/yr) (Nevada State Engineer, 1971) This is considered in agreement with Eakin's (1963) estimate of 4800 acre-ft/yr (5.9 hm³/yr) recharge because the State Engineer's figure is rounded to the nearest thousand acre-foot. The hydraulic gradient in the valley fill aquifer is southward at 16 ft/mi (3 m/km) from central Dry Lake Valley to central Delamar Valley (Figure Bl.8). The potentiometric surface ranges in elevation from 5000 feet in the north to 4200 feet in the south (1524 to 1280 m) based on the regional potentiometric map. The depth to ground water in Dry Lake Valley is in excess of 300 feet (91 m), thus, there is no evapotranspiration of ground water by phreatophytes. The valley-fill aquifer in Dry Lake Valley is probably over

10,000 feet (3048 m) thick in the central part of the valley and is composed of alluvial fan, fluvial, playa, and lacustrine deposits (FN-TR-33DL, FN-TR-26E). Eakin (1963 describes the valley-fill sediments as clay, silt, sand, and gravel of Tertiary to Quaternary age deposited under subaerial and lacustrine conditions.

Carbonate rocks of Paleozoic age are exposed in the mountains and are believed to partially underlie the valley-fill sediments. The mountains bordering Dry Lake Valley to the west contain ash flow tuffs of Tertiary age with some carbonate rocks of Paleozoic age. The mountains to the east contain carbonates of Paleozoic age with minor amounts of ash flow tuffs of Tertiary age (Stewart and Carlson, 1978).

2.8.2 MX WATER REQUIREMENTS

The peak annual demand for ground water in Dry Lake Valley during the construction phase is expected to be 3411 acre-ft (4.2 hm^3) in 1984 according to preliminary figures from the U.S.Army Corps of Engineers (1981) as revised by Ertec (1981). Construction should begin in 1982 and conclude in 1987. Water demand for the operational phase of the MX project is expected to be less than 300 acre-ft/yr (0.4 hm³/yr) for the 30 year life of the project.

The Air Force has requested 3810 acre-ft/yr $(4.7 \text{ hm}^3/\text{yr})$ for appropriation in Dry Lake Valley. It should be noted that the amount of water needed in Dry Lake Valley for construction and operation is expected to be less than this because the applicat-

ions were filed before the latest cluster layouts and water requirements were determined.

2.8.3 WATER SUPPLY LIMITATIONS

2.8.3.1 <u>Perennial Yield, Use, and Appropriations</u> The combined perennial yield for Dry Lake/Muleshoe valleys is estimated to be 3000 acre-ft/yr (3.7 hm³/yr) (Nevada State Engineer, 1971). This was apparently based on Eakin's (1963) estimate of 6000 acre-ft/yr (7.4 hm³/yr) discharge for the combined Muleshoe, Dry Lake, and Delamar valleys. The discharge was divided, and a combined perennial yield of 3000 acre-ft/yr (3.7 hm³/yr) was assigned to Dry Lake/Muleshoe valleys.

Surface-water use, primarily for stock watering, is estimated to be 21 acre-ft/yr (0.03 hm^3/yr) in Dry Lake Valley. Surfacewater appropriations in the appropriation and permit phase total 2596 acre-ft/yr (3.2 hm^3/yr) (DRI, 1980). At the present time, ground-water use is minor in Dry Lake Valley. Current ground-water permits total 8 acre-ft/yr (0.01 hm^3/yr), certificates total 11 acre-ft/yr (0.01 hm^3/yr), and there are a total of 20 acre-ft/yr (0.03 hm^3/yr) of pending applications for ground-water rights in the valley (Woodburn, et al, 1981).

The quantity of ground water available for MX use is approximately 3000 acre-ft/yr $(3.7 \text{ hm}^3/\text{yr})$ when considering existing use. The water availability is 2981 acre-ft/yr $(3.7 \text{ hm}^3/\text{yr})$ when considering approved appropriations and 2961 acre-ft/yr $(3.7 \text{ hm}^3/\text{yr})$

 $hm^3/yr)$ when considering both existing and pending applications. The peak MX demand of 3411 acre-ft/yr (4.2 hm^3/yr) for ground water will exceed the reported perennial yield by 411 acre-ft/yr When considering existing appropriations, the $(0.5 \text{ hm}^{3/\text{yr}}).$ perennial yield will be exceeded by 430 acre-ft/yr (0.5 hm^3/yr). Because the State Engineer considers Muleshoe Valley as part of Dry Lake Valley for perennial yield estimates, its ground-water demand must also be considered. Peak year MX demand for Suleshoe Valley is 968 acre-ft (1.2 hm³) in 1984. Therefore, the combined peak construction water demand in 1984 and the existing appropriations will exceed the perennial yield by 1398 acre-ft/yr $(1.7 \text{ hm}^{3}/\text{yr}).$ However, if Dry Lake/Muleshoe valleys are hydrologically connected with Delamar Valley as previously discussed, and the perennial yield of Delamar Valley (3000 acre-ft/yr, 3.7 hm³/yr) and its peak MX demand (679 acre-ft/yr; 0.8 hm^3/yr) is considered, the total peak year demand for construction water in 1984 is 5058 acre-ft (6.2 hm^3/yr) compared to a combined perennial yield of 7000 acre-ft/yr (7.4 $hm^3/vr)$. The combined existing appropriations for the three valleys totals 35 acre-ft/yr (0.04 hm^3/yr), therefore sufficient water would be available from the combined basins to meet peak year MX requirements. It should also be noted that the construction period in the three valleys is from 1982 to 1987, and that the quantity of water needed for the operational phase after that period will be considerably less than that required during construction.

1.1

2.8.3.2 Source Capabilities

Surface water is limited to ephemeral steamflow and spring discharges in Dry Lake Valley. The springs in Dry Lake Valley are not believed to be a dependable source of water for the MX project because they are generally in the mountains above the valley floor, are relatively inaccessible, and have low discharge (less than 2 gpm; 0.1 1/s).

Data from an aquifer test performed by Ertec in the southern part of the valley (3S/64E-12ac) indicate a transmissivity and storativity for the valley-fill aquifer of about $3100 \text{ ft}^2/\text{day}$ $(287 \text{ m}^2/\text{day})$ and 0.04, respectively. These aquifer characteristics indicate that, in this area of the valley, the valleyfill aquifer is capble of yielding water in sufficient quantities and rates required to meet MX needs.

A carbonate aquifer test conducted by Ertec Western in the northern part of the valley (3N/63E-27ca) indicated a transmissivity in the carbonate aquifer of about 13,500 ft²/day (1250 m²/day) and a specific capacity of 50 gpm/ft.

2.8.3.3 Water Quality

Water quality data for Dry Lake Valley is shown in Appendix F1.8. Chemical analyses of water samples from the two test wells drilled by Ertec Western, one which penetrates the valley-fill aquifer and one which penetrates the carbonate aquifer, one existing well, and six springs indicate that, for the constituents analyzed, water quality are within criteria for construction water (Appendix El.1). The chemical analyses of samples from six springs and three wells indicate that all but one well, at 3N/65E-2ldba, meet Primary and Secondary Drinking Water Stand ards for the State of Nevada (Appendix El.2). This well, located in the northeastern portion of the valley was found to have a nitrate concentration of 32 mg/l, which exceeds the 10 mg/l Primary Drinking Water Standards for nitrate. This well was used when the Bristol Silver Mine was in operation and could be contaminated from surface sources. Although the valleywide water quality cannot be accurately predicted from the limited data available, it is expected that the ground water should be suitable for construction and drinking water purposes.

2.8.4 PRIMARY WATER SUPPLY ALTERNATIVES

2.8.4.1 Lease or Purchase of Existing Water Rights

It will not be possible to obtain MX water supplies through the lease or purchase of water rights in Dry Lake Valley because approved and pending ground-water appropriations total only 39 acre-ft/yr (0.05 hm^3/yr). Because of the limited current use, substantial water is available for appropriation.

2.8.4.2 Valley-Fill Aquifer

The valley-fill aquifer represents a satisfactory source of water for MX construction and operation because: a) little ground water in Dry Lake Valley has been appropriated; and b) the aquifer tests and studies performed indicate that it is

capable of supplying water at the rate necessary and insufficient quantity and quality to meet MX requirements.

2.8.4.3 Carbonate Aquifer

The aquifer test mentioned previously indicates that the carbonate aquifer has a high potential for development in Dry Lake Valley. However, it is considered only as alternative for development because the valley-fill aquifer appears adequate for MX water requirements.

2.8.4.4 Interbasin Transfer

Interbasin transfer will not be necessary in Dry Lake Valley because the valley-fill aquifer is capabable of meeting MX requirements. However, the transfer of water from Dry Lake Valley to Muleshoe and/or Delamar valleys is being considered.

2.8.5 IMPACTS OF DEVELOPMENT

2.8.5.1 Intrabasin Effects

Computer simulation of a well field in Dry Lake/Muleshoe withdrawing water for six years at rates estimated by the U.S. Army Corps of Engineers (1981) for both valleys was performed. A transmissivity of 1300 ft^2/day (120 m²/day) and storativity of 0.05 were used in the simulation. Those values were found to be representative of the average aquifer characteristics of all types of sediments in the valley. Pumping rates were varied according to annual MX needs and reached a maximum of one well pumping in Muleshoe at 600 gpm (38 l/s) and five wells in Dry Lake pumping at 420 gpm (26 l/s). Maximum drawdown effects occurred after five years and averaged about 4.1 feet (1.2 m) at a distance of one mile (2 km) from the wells in Dry Lake Valley. Because of the lack of vertical recharge on the valley floor and the absense of recharge from underlying sediments, complete recovery after cessation of pumping will occur after at least 30 years.

At the present time ground-water use in Dry Lake Valley consist of widely separated stock watering wells, so MX ground-water withdrawals should be able to avoid significant impacts to these users. The lowered water levels will have no effect on vegetation because the ground water is more than 300 feet (91 m) below the land surface and well beyond all root systems.

There should be little effect on spring discharge in Dry Lake Valley because the majority of the springs are in the hills and mountains and probably discontinuous with the valley-fill aquifer. There is a spring in Dry Lake Valley, (3N/65E-31cc) that may be considered a regional spring connected with the regional flow regime through carbonate rocks. MX wells will be located at appropriate distances from this spring to avoid any impacts.

2.8.5.2 Interbasin Effects

Water levels and spring discharge could be affected in Pahranagat and Delamar valleys because they are downgradient from Dry Lake Valley and receive underflow through the carbonate aquifer. The regional springs which could be affected include Ash, Crystal, and Hiko springs in Pahranagat Valley. However, there is not enough data available to quantify what, if any, the effects will be. Because of the great distances from the pumped wells, *however* the effects will probably be undetectable.

2.8.6 MITIGATING MEASURES

A well field design was modeled for Dry Lake Valley which consisted of two simulations, one with a single pumping well and one with five pumping wells. Results from modeling indicate that MX ground-water withdrawals will probably require five or more wells to obtain water in sufficient quantity with the least amount of drawdown. Additonal wells in Dry Lake Valley may be required to meet MX water requirements for Delamar and Muleshoe valleys.

The primary suitable for MX production wells is about 96 mi² (249 km²) along the margin of the valley. The criteria used in determining this area includes consideration of land status, environmentally sensitive areas, existing water appropriations, areas containing Tertiary sediments (which are generally fine grained), and low transmissivity zones.

Pumping schedules could be adjusted to avoid MX construction withdrawals exceeding the perennial yield of Dry Lake Valley. early storage of ground water in reservoirs prior to the construction period is a practical alternative. Another option would be to extend the construction period (reduce the rate of construction), which would reduce the peak year quantity of water required. There are an additional 71 m^2 (184 km²) that are considered secondarily suitable in the center of the valley. This area is considered secondary because of the presence of generally low transmissivity lacutrine deposits and/or less than 200 feet of thickness.

ERTEC WESTERN, INC.	DISCMARGE MEASUREMENTS, DRY LAKE VALLEY	MC/YEAR DISCHARGE LAND MEASURED (GPM) ELEV REMARKS
		STATION NAME
		SOURCE
24 SEP 81 14:03:23		ID. TOWNSHIP NJ. RANGE-SECTION

DATA SOURCE	ERTEC 79	ERTEC 80	ERTEC 80
REMARKS	607 <i>5</i> 7 30		DISCHARGE <1GPM
LAND ELEV (FT)	5100	0075	6100
DISCHARGE (GPM)	0.5	0	0.1
MC/YEAR MEASURED	8/1979 8/1979	5/1980	5/1980
STATION NAME	COYOTE SPRING	WHEATGRASS SPR. Seven dak Spr.	RED ROCK SPR.
SOURCE	8 8 8 8	4 S S	92
TOWNSHIP RANGE-SECTION	1 3N/65E-31CC 2N/63E-13CBA	\$ 25/63E-229C • 45/64E-249A	5 45164E-2500
0 N 0 N	-~	m .#	5

P.45E

25 GEP 81 14:52:36

.

EPTEC WESTERNA INC.

SELECTED WATER QUALITY DATA FOR DRY LAKE VALLEY

- -----

- 7	TOWNSHIP			STATION	TEMP	SP.		CISS.	SILICA	CALCIUM	MAGNESIUM	SCDIU™
, ,	RANGE-SECT	5 ° C E	NO AB	NAME	DEG C	COND	PH	SCLIDS	(\$102)	(CA)	(*5)	(≒≛)
1	3N/53E-27CA	¥ E	12-30	USAF TEST "ELL		550	7.3	366	24	75	30	15
2	31/635-21084	#8	-15	BRISTOL WELL		NC			49	7 6	33	37
3	3N/05E-31CC	3 P	3-79		24.0	470	6.3		43	40	10.0	21
	2N/c3E-13CBA	SP	5-79	COYOTE SPRING	20.0	550	6.3		79	32	13	4 9
5	25/635-2230	5 P	5-80	WHEATGRASS SPR.	13.0	415	7.0					
5	25/641- 2808	SP	3-75		25.3	443	5.9		44	83	10.0	53
7	35/63E- 5C2	SP	5-90	LITTLE BOULDER SPR.	13.0	250	5.5		19	2 8	7.9	12
3	35/642-1240	4 É	4-80	USAF TEST WELL		430	7.9	292	1.4	2 0	10	75
7	45/64E-243A	50	5 - E C	SEVEN DAK SPR.	8.0	£15	7.6					

a second s

PAGE 1A

....

25 ["EP 61 14:52:35

EPTEC RESTERNA INC.

SELECTED ANTER DUALITY DATA FOR DAY LAKE VALLEY

13. N	PDTASSIUM (K)	CAPEDNATE (CO3)	910495. (HCO3)	CHLORIDE (CL)	SULFATE (524)	FLUCRISE (F)	NITPATE (N)	30RON (3)	IRON MA (FE) (*	INCANESE IN) REMARKS	BFEJENCE
	5.5	0	454	5.0	20	. ć	ND				ERTEC 12
2		9	1:7	110	71		32			•5	EAKIN 63
3	2.5	3	214	17	21	. 2	. 4			+1	ERTEC 79
	7.5	J	252	25	25	.5	ND				ERTEC 79
		0	351								ERTEC 90
	7.1	0	320	30	54	. 4	1.4			+1	ERVEC TR
,	3.0	2	137	2.5	15	. 1	• 2	÷-		+1	ERTEC PC
3	5.2	1	213	21	÷		5.7			+1,4	ERTEC HD
4		3	303								EPTEC 50

NO : SAMPLES FOR WATER QUALITY ANALYSIS COLLECTID BY ERTEC EXCEPT WHERE NOTED. ALL ANALYSIS PEPORTED IN MG/L EXCEPT AS NOTED BELDW. ERTEC ANALYSES FOR DISSOLVED SOLIDS DETERMINED BY RESIDUE HONH EVAPORATION AT 180 DEGREE C METHOD. METHODS, NEVADA LOCATIONS BASED ON MT. DIABLO BASELINE, UTAH LOCATIONS BASED ON SALT LAKE BASELINE AND MERIDIAN.

THE FOLLOWING CONSTITUENTS ARE REPORTED IN MICROSPAMS/LITER: DOPON IRON MANGANESE

SQUI +1 NITRATE REPORTED AS N. NOTES:+2 NITPATE REPORTED AS NO3 +3 NITAITE + NITFATE REPORTED AS N +4 DISSOLVED SOLIDS BY SUM OF DETERMINED CONSTITUENTS +5 NA+K AS NA +6 HC03+CO3 AS HC03 ND = NOT DETECTED

.....

PAGE 18

٠

.

•

K

67 EE 99 SC 82 63 64 £5 ACTIVITY 64 DOMESTIC - LIFE ELAFORT CAMPS - INDEPENSENT WOAPERS 593 1179 200 1000 1 2 4 ۵ - PEVEGETATION :15 695 520 733 250 21 ٥J 125 10e C LANDECAR ING - DUST CONTROL A POADWAYE I WORK SITES I IN CAMPE 50 311 311 155 40 278 60 40 ----- Included Alove -----37 ------ FOAD CONSTRUCTION
RECOMPACTION
CONSTRUCTION ROADS
REGRADING 1120 17 125 34 125 E EHELTER EXCAVATION CONCRETE FOR DDA CONCRETE FOR MOBRADE. DAA .COIS 140 23 70 2 1 - CONCRETE AGGREGATE WASH 1 26 2 STOTALS (ACRE-FEET / YEAR) 196 427 3411 2533 2133 250

•

 These figures are a little higher than those in Table 4 - 13 due to difference in calculations within the COE MX water requirement document, 17 March 1981

> MX WATER USE ESTIMATES DRY LAKE VALLEY, NEVADA SEPTEMBER, 81 TABLE

. جە مە

.

PAGE 1

.

ł

WELL AND WATEP LEVEL DATA IN DRY LAKE VALLEY ERTEC WESTERN, INC.

:03	
13:53	
81	
4 i S	
54	

L

	HELL DES	CAIPTI	NO				HATER LE	VEL MEASURE	MENTS	REMARKS	DATA SO
SHIP E-SECTION	LELL DANER	1 	YEAR Drilled	WELL DEPTH (FT)	CASING ID (IN)	LAND ELEV (FT)	MOLYEAR	DEPTH-BELOW Surface (ft)	(17) (57)		
63E-27CA 64E-203AC 65E-2109A	U.S.AIR 964 0664406	FORCE	1980 1960 1962	2395 380 51	010	5390 5067 5451	2/1981 /1960 /1962	851 317 45	4539 4750 5406	CARB.TEST WELL Dev	ERTEC Eakin 63 USSS 79 Eakin 03
658- 691 645-2481	LYTLE &	ОТНЕРS	1959	515 515	19 19 19	0023	1/1959	398	4302 5650	DUG #ELL	EAKIN 63 Eakin 63
1655- 2445 1645-12451 1645-12452	U.S.AIR U.S.AIR	FORCE FORCE	1950 1980	1305	~ [4645	2/1991 2/1981	10 M 10 M 10 M	4262	OSSERVATION WELL Tést wéll	EPTEC EPTEC







Th











 $\int \nabla f$

DRY LAKE/DELAMAR VALLEYS SECTION: MX SITING INVESTIGATION, WATER RESOURCES PROGRAM, SUMMARY FOR DRAFT ENVIRONMENTAL IMPACT STATEMENT

E1.0

)]][

R

T

-

]

]

I

1

north of township 6 with total dissolved solids concentrations ranging from about 130 to about 280 mg/l. Two springs (7N/64E-33cc; 6N/63E-19da), analyzed by the BLM have moderately high bicarbonate concentrations (more than 250 mg/l). This condition is probably due to the solution of carbonate rocks by the ground water.

Cave Valley Spring located at 9N/64E-16bdb also originates from the carbonates but has low bicarbonate concentration (80 mg/l) and low total dissolved solid concentrations (127 mg/l). This is probably due to a short resident time of the ground water with the rocks which suggests that it is related to precipitation and snowmelt. Thus it is not connected to the regional carbonate aquifer. The discharge in Cave Spring ranges from a few hundred gallons per minute to less than 10 gallons per minute. Table C1-3 lists the chemical analysis of the water samples and Drawing D1-2 shows the area of good water quality. As can be seen on the Drawing, all of the valley is estimated to contain ground water of good quality.

3.3 DRY LAKE/DELAMAR VALLEYS

3.3.1 Physiography and Geology

Dry Lake and Delamar valleys are believed to be hydrologically connected through valley-fill aquifers and are treated essentially as the same ground-water basin in the ensuing discussions. The Dry Lake/Delamar drainage basin lies within central Lincoln County in east-central Nevada (Figure 1). The basin is approximately 82 miles (132 km) long and 20 miles (32 km) wide at the

Π

H

Ŋ

Ŋ

T

I

T

 $\mathbf{\Gamma}$

. .

 \mathbf{T}

31

widest point, and encompasses an area of 1300 mi² (3367 km²). Of that area, 497 mi² (1287 km²) are suitable for MX siting including 315 mi² (815 km²) in Dry Lake Valley and 182 mi² (417 km²) in Delamar Valley.

The valley-fill deposits are up to 10,000 feet (3 km) thick along the axis of the valleys and thin toward the margins. Based on detailed gravity maps constructed by Fugro National, (FN-TR-33-DL), the volume of valley-fill in Dry Lake Valley is estimated to be 635,000,000 acre-ft (732,955 hm³). The estimated volume of valley-fill in Delamar Valley is 200,000,000 acre-ft (246,600 hm³). These substantial potential aquifer volumes provide tremendous storage capacity for ground water.

Mountain crests bounding the valleys range in elevation from about 7000 feet (2134 m) to over 9000 feet (2743 m). Highland Peak, on the east side of Dry Lake Valley, has an elevation of 9395 feet (2864 m), and is the highest point in the basin. The playa, in the extreme south end of Delamar Valley, has an elevation of less than 4400 feet (1341 m) and is the lowest point in the basin. The two valleys are separated by a low, broad alluvial fan that extends across the basin just south of Dry Lake playa.

Dry Lake and Delamar valleys exhibit typical Basin and Range structure, consisting of high angle, north-south trending, normal basement faults that border the Pahroc ranges on the west and the Bristol, Highland, Chief, and Delamar ranges on the east. The area between the ranges is faulted downward. A

TUSTO NATIONAL INC.

FN-TR-38

north-south trending fault on the eastern side of the basin displaces surface alluvium and forms a prominent scarp. Additionally, Shawe (1965) shows east-west trending faults that transect the basin and displace deep valley-fill deposits. This interpretation is supported also by gravity surveys (Fugro National, FN-TR-26E).

The mountains on the western side of the valley are predominantly composed of ash flow tuffs of Tertiary age with some carbonate rocks of Paleozoic age. Conversely, the eastern mountains are composed primarily of carbonate rocks of Paleozoic age with minor amounts of ash flow tuffs of Tertiary age (Stewart and Carlson, 1978).

Coarse-grained alluvial and fine-grained lacustrine deposits make up the majority of sediments in the valleys. Although playa deposits cover only a small percentage of the valley surface, they are thought to be of great thickness and interfinger with alluvial deposits in the subsurface (Fugro National, FN-TR-27). These playa deposits are located in the southcentral portions of the valleys. From the central part of the valleys, the grain size and grading of alluvial deposits progressively increase towards the mountains.

3.3.2 General Hydrology

Dry Lake and Delamar valleys form closed surface drainage basins. There are no perennial streams in the valleys, and streamflow only occurs in the mountain ravines and alluvial fans after high-intensity rains and as snowmelt runoff.

TUGRO NATIONAL, INC.

Springs in the Dry Lake and Delamar valley area occur in volcanic rocks composed predominantly of tuffs along the basin margins. The springs are recharged by meteoric waters (precipitation and snowmelt) and are not associated with the deep regional carbonate aquifer. They generally have low yields (less than 20 gpm) and are used primarily to supply stock ponds in the area.

The ground-water table in the basin aquifer occurs at considerable depths (Drawings B1-3 and B1-4). In Dry Lake Valley, ground-water levels are about 400 feet (122 m) below ground surface, and in Delamar Valley, levels are generally greater than 800 feet (244 m) below ground surface. Some water wells in the northern and western part of Dry Lake Valley tap perched aquifers with water levels significantly higher than the underlying basin aquifer. Water use in the valleys is limited to a few isolated stock ponds fed by infrequent surface runoff and nearby springs with waters of meteoric origin.

Ground-water recharge to the basin is primarily from precipitation occurring in the mountains along the northwest and east flanks of the valleys (Eakin, 1963). From these areas, ground water moves laterally and downward toward the central part of the valleys as indicated on the ground-water level contour map (Drawing B1-3 and B1-4). Generally, the ground water moves from Dry Lake Valley toward Delamar Valley. An annual (recharge based on a percentage of average annual precipitation) of about $6000 \ acre-ft \ (7.4 \ hm^3)$ for the valleys has been estimated by

TURRO NATIONAL, INC

FN-TR-38

Eakin (1963). Discharge occurs primarily as deep underflow to the south through carbonate rocks. Alluvial ground-water gradients between Dry Lake Valley and Delamar Valley closely resemble the carbonate aquifer gradient between White River Valley and Pahranagat Valley. This suggests that the valleyfill aquifers of the basin and the regional carbonate aquifers are hydraulically connected (Eakin, 1963).

3.3.3 Aquifer Characterisitics

The considerable depth to ground water (Drawing B1-3 and B1-4) has precluded much development in these valleys and, therefore, very little has been published about specific aquifer characteristics. However, all wells in the basin tap valley-fill aquifers with little indication of confinement. Existing wells produce less than 100 acre-ft of water annually for use by livestock. During Furgo National's field investigations in 1979, none of the wells were found to be suitable for aquifer testing because of pumping limitations. In 1980, two intermediate depth test wells (3S/64E-12ca and 6S/63E-12ad) were drilled in Dry Lake/ Delamar valleys (lithologic and geophysical logs are presented in Appendices H1-3 and H1-34). At each site, observation and test wells were constructed.

Aquifer tests in Dry Lake Valley were conducted for ten days at 500 gpm (31.5 1/s) followed by an aquifer recovery test. The maximum well yield during development was approximately 750 gpm (47.3 1/s). Maximum drawdown at the pumping well during the pump test was about 50 feet (15 m). These tests indicated an

FUGRO POTIGNAL INF

I

I

T

aquifer transmissivity of about 45,000 gpd/ft (155 cm²/sec) and a storage coefficient of 3 x 10^{-4} . Because the well only partly penetrated the aquifer, the transmissivity of the total thickness of the aquifer is probably much higher. The unusually low storage coefficient in the valley-fill aquifer is probably 'due to the tremendous thickness of the aquifer.

Aquifer tests in Delamar Valley were conducted for ten days at 85 gpm (5.3 l/s) followed by an aquifer recovery test. Maximum drawdown during the test was 85 feet (26 m). Transmissivity was calculated at 5000 gpd/ft (7 cm²/sec) with a storage coefficient of 4.0 x 10^{-4} .

Potential well yields in Dry Lake Valley are expected to be high in the unconsolidated valley-fill deposits around the valley periphery. However, a significant portion of the basin is probably composed of fine-grained lacustrine deposits near the central valley areas. These areas probably have relatively low hydraulic conductivities. The extent and depth of the low yield deposits are not fully known. However, there appears to be sufficient water for development of the MX system within the basin.

Because of the great depths to water in Delamar Valley [870 ft (265 m) in test well 6S/63E-12ad], well yields are expected to be less than 100 gpm (6.3 1/s). Well yields may increase slightly away from the central valley axis, but any yield increase due to higher aquifer permeability will probably be offset by the corresponding increase in pumping lift.

3.3.4 Water Quality Limitations

Because there are very few wells in Dry Lake Valley, only four ground-water quality analyses are available. The well and spring sample locations are shown in Drawing D1-3. Four of these samples were collected by Fugro National in 1979 and 1980 and one sample was collected by Carpenter (1915) and reported by Eakin in 1963.

Based on the water quality critieria listed in Appendix Cl-1, all of the water analyzed is of good quality and is acceptable for drinking. All ground-water samples contained moderately high bicarbonate levels ranging from 187 to 320 mg/l, which result in hardness levels of about 100 mg/l. Calcium concentrations range from about 40 to 83 mg/l and were generally in the poor range. In addition, the sample collected at 3N/65E-21dbd and analyzed by Carpenter also contained relatively high chloride (110 mg/l) and nitrate (32 mg/l) concentrations.

Ground water in the northern part of Dry Lake Valley is of the calcium-magnesium/chloride-bicarbonate type. As the ground water migrates from the fans toward the central valley area, the concentrations of calcium and chloride increase slightly and sodium concentrations decrease, yielding water of the sodiumcalcium/bicarbonate type. The higher calcium and chloride concentrations in the central valley area may be related to the soil chemistry of the playa deposits.

The only ground-water samples for chemical quality testing from Delamar Valley was from the Fugro National test well. However,

TULRE NATIONAL ING.

1

M

M

211

M

31

H

the analyses were not completed at the time of publication of this report.

3.4 DUGWAY VALLEY

3.4.1 Physiography and Geology

Dugway Valley is located in Tooele and Juab counties in westcentral Utah (Figure 1) and has a total area of 890 mi² (2300 km²). Of the total area only 182 mi² (471 km²) are suitable for MX siting.

Dugway Valley trends north-south and is approximately 30 miles (48 km) long and varies in width from 1 to 8 miles (2 to 13 km). The valley is bordered on the west by the Dugway Mountains and the Thomas Range, on the south by the Drum Mountains, and on the east and northeast by Keg Mountain and Slow Elk Hills. The northern boundary of the valley is the Great Salt Lake Desert. Valley floor elevations range from 4480 feet (1365 m) at the north end to 5080 feet (1548 m) in the central-southern portion of the valley. The valley is bounded by peaks on the northwest that reach elevations of nearly 9000 feet (2700 m). Most of the area below about 4600 feet (1400 m) is nearly flat as a result of planation and deposition by ancient Lake Bonneville (Stephens and Sumsion, 1978).

Valley-fill deposits consist mainly of alluvial fan deposits along the margins of the valley which interfinger with lake and playa deposits in and near the center of the valley. These deposits consist mainly of clay, silt, sand, and minor amounts

THERD NATHINAL INC.
711-18-38			
1			
	WELL CONSTRUCTION VALLEY	ELEVATION ELEVATION E 4843	
	WELL SAETCH & LOCATION DE CROCOTNATES <u>35,7845-1</u> El cal cal ca	Zea Tap av Casing _4445'	
		PackE85	
	- 100" TETAL DEPTH BAFLED 1205		
	BELLING CONTRACTOR	PEA CRAVEL C'-720' 805'-230'	
	AIS (3) 8569 _BUCKET ADMEN 0' TO		
	- 700*	5.13"	
	E CAR IN THE AND CLUSTER AND A SACES	POLYUKA SLURAY	
	SAMPLING METHOD COLLECTED FROM DIS	CHARGE PIPE DEVELOPMENT NETHOD (S)	
	3007ACE CASING <u>0' 10 40' 27" DIA</u> COMMENTS (PROBLEMS, SHUTDOWNS, ET	c)	
]-	- 909'	TIME LOG START FINISH ELAPSED 5.0F	
1			
	MEIS DRILLER'S LOB		
	- 1000" - 1000"		
	COPIES ATTACHEDYES STEEL CASING STRING 1	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	Falls <u>0'</u> 1 <u>1220</u> 1180' Falls <u>1220'</u> 10 <u>1220'</u> 100' Falls <u>1220'</u> 10 <u>1220'</u>	PLANSDEVELOP	
1	Fatto <u>1290'</u> 79 <u>1200'</u> Fatto <u>10</u>		
	51EEL CASING 310		
	-1200" Fees T0 T0 T0T0T0T0 T0T0 T0T0 T0T0 T0T0 T0T		
	Feen T0 T0 Feen T0 T0	ULANA UISCELLANEOUS	
	- 1308" 19	PAS INSTALLED TO 40" BELOW THE SADUND SUNFACE	
	D I MENS (ONS <u>2" 1 D</u>		
	019ENS10NS <u>7⁻¹ 0</u> SLOT S125 <u>2/4 Tochiner</u> 5 <u>10</u> TS		
		F-46-3 2-21-79	
Į	<u>EXPLANATON</u>		
	D BLANK CASING	WELL POPATRIATION INC.	
	LI PERFORATED CASING	OBSERVATION WELL	
	GRAVEL PACK	DRY LAKE VALLEY, NEVADA	
	SAND PACE	WX SITING INVESTIGATION	F16#8
		DEPARTMENT OF THE AIR FORCE - DWO	111.4-

H1.4-4

DRILL CUTTINGS LOG	() L) , / PAGE _ OF _ IS FIELD LOG OF WELL NUMBER _ OW-2
PROJECT NUMBER 79-290- <u>45</u>	VALLEY NAVE Dry Lake
PROJECT NAME MX SITING INVESTIGATION	LOCATION NUMBER T3S, R64E, Sect. 12
EQUIPMENT USED <u>90-1300' Reverse Ro</u> tary	LOGGED BY JM & SC DATE <u>1-8-80</u>
CONPANY Beylik	CHECKED BY JAG DATE 4-10-80
OPERATOR Jim Clyde	TOTAL WELL DEPTH

•

נ ו

Ì

j

j

1

1

1

1

1

,

•

••

L

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
0	Silt: Tan silt with occasional gravel to $1\frac{1}{2}$ ".
10 10 10	<u>Silt</u> : Tan Silt
20 - 111 111	Silt & Sand with Gravel: Tan silt with $\frac{4}{25\%}$ med colored, fine to coarse, poorly sorted, subrounded to subangular sand, with $\frac{4}{10\%}$ med colored subrounded to angular gravel to $1\frac{1}{2}$ ".
30 20	Gravel with Cobbles - Med to dark colored, subrounded to subangular ½" gravel up to cobbles to 4".
م م	Fine Gravel with Sand: Brown color, well sorted, subrounded gravel with less than 25% coarse sand, gravel up to 3/4".
50 50	Gravel with Coarse Sand: Brown color, subangular, well sorted gravel up to 3/4" with coarse,angular sand (less than 25%).
60 61 11 11 11 11	Gravel with Sand: Brown color, well sorted, sub- rounded gravel up to 1½" with less than 25% coarse sand.
70 - 11	Gravel with Sand: Same as above (60').
80 - 11 11 11	Coarse Sand with Gravel: Dark color, well sorted, subrounded sand with less than 25% gravel up to ½".
90 90	Fine to Medium Gravel with Sand: Brown color, well sorted, subrounded gravel with less than 10% coarse sand.
100 -	Gravel with Sand: Dark color, well sorted, subangular
	graver up to 3/4" with less than 30% coarse Sand.

PROJECT NAME <u>MX SITING INVESTIGATION</u> EQUIPMENT USED <u>Reverse Circulation</u>

PROJECT NUMBER 79-290- 45____

COMPANY Beylik

OPERATOR J. Clyde

PAGE ____ OF ____3

FIELD LOG OF WELL NUMBER <u>OW-2</u> VALLEY NAWE <u>Dry Lake</u> LOCATION NUMBER <u>T35, R64E, Sect. 1264</u> LOGGED BY <u>SC & JM</u> DATE <u>1-8-80</u> CHECKED BY <u>JAG</u> DATE <u>4-10-80</u> TDTAL WELL DEPTH <u>1300 feet</u>

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
100	Gravel with Coarse Sand: Dark color, well sorted, subangular, max gravel 1" with less than 25% coarse sand.
110	Gravel with Coarse Sand: Same as above (100'-110'). Max size for gravel ½".
120	Gravel with Coarse Sand: Same as above (100'-120'). Max gravel 1½".
130	Gravel with Coarse Sand: Less than 25% sand. Max gravel 12". Most less than 1".
140-11	Gravel with Coarse Sand: Less than 10% sand. Same as above (130-140').
150 J20	Gravel with Coarse Sand: Dark, subrounded, well sorted max size 1" gravel with less than 40% very coarse, subangular sand.
160 111	Gravel with Coarse Sand: Brown, subrounded, well sorted gravel with less than 25% coarse sand. Max size 3/4".
170-11	Gravel with Coarse Sand: Brown, subangular, well sorted gravel with less than 25% coarse sand. Max size 3/4".
180	Gravel with Coarse Sand: Much coarser than 170-180', 33% of sample greater than 1" size. Brown subrounded, subangular, well sorted with less than 10% sand.
190 190	Very Coarse Gravel with Coarse Sand: Dark, well sorted subangular. Greater than 2" sized gravel. Less than 5% coarse sand.
200 - 3	

PROJECT NUMBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Circulation
COMPANY	Beylik
OPERATOR	J. Clyde

1

Ī

Ţ

1

Ì

J

Ĩ

1

1

j

J

I.

PAGE <u>3</u> OF <u>13</u>

LOCATION NU	INBER _	тзѕ,	R64E,	Sect.	12 6
LOGGED BY _	JM &	sc	DATE	1-8-	80
CHECKED BY	JA	G	_ DATE	4-10	-80
TOTAL WELL	DEPTH) feet		

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE	
200	Gravel with Coarse Sand: Brown, well sorted, subangular gravel. Max size 1" with less than 40% subangular, coarse sand.	
210 - 111	Gravel with Coarse Sand: Gray, subangular, well sorted. Max size 15". Less than 10% subangular, coarse sand.	
220	Gravel with Coarse Sand: Gray-black, subangular, well sorted. Max size 2½". Less than 10% coarse, subangular sand.	
230	Gravel with Coarse Sand: Gray-black, subangular, well sorted. Max size 1". Less than 40% subrounded, coarse sand.	
240	Gravel with Sand and Some Clay: Subangular, poorly sorted, max grave size 3/4". Less than 10% sand. Less than 20% silt and clay.	1
250 - 	Gravel with Coarse Sand: Gray-brown, subangular, well sorted, max size 1". Less than 20% coarse sand.	
260	Gravel with Coarse Sand: Gray, subangular, well sorted. Max size 2½" gravel. Less than 20% coarse, subangular sand.	
270	Gravel with Sand and Silt: Gray color, subangular, poor to medium sorted, max '2" gravel. Less than 25% fine to coarse grained sand. Less than 5% silt.	
280	<u>Gravel with Coarse Sand</u> : Gray color, subangular, well sorted. Max 3/4" gravel. Less than 20% coarse, subangular sand,	
290	Gravel with Coarse Sand: Gray, subangular, well sorted, max size gravel 1". Less than 20% subangular coarse sand.	
300		

PROJECT NUNBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Circulation
COMPANY	Beylik
OPERATOR	J. Clyde

Î

f

PAGE _4_ OF _13

FIELD LOG OF WELL NUMBER OW-2

VALLEY NAVE	D	ry Lal	ke			
LOCATION NU	WBER	тзs,	R64E,	Sect.	12	
LOGGED BY	JM &	SC	DATE	1/8/8	30	
CHECKED BY	JAG		_ DATE	4/10/	/80	
TOTAL WELL	DEPTH	130	00 feet	t		

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
300	Fine Gravel with Coarse Sand: Gray-brown, subrounded, well sorted, max size ½". Less than 40% coarse, subrounded sand.
310 310	
320	Gravel with Coarse Sand: Gray-brown, subrounded, well sorted, max size 1 gravel, less than 40% coarse, subrounded sand.
330 111 330 111	Gravel with Coarse Sand: Well sorted, brown gray, subrounded, max 'y" gravel with less than 30% coarse, subrounded sand.
340	Gravel with Sand, Silt & Clay: Poorly sorted, gray-black, subangular to subrounded, less than 40% sand. Less than 10% silt and clay, 4" gravel.
350	Gravel with Sand, Silt & Clay: Poorly sorted, brown subangular- subrounded. 40% sand, 10% silt and clay, 5" gravel.
360	<u>Gravel with Trace Sand, Silt & Clay</u> : Less than 20% sub- gravel size, gray-black, subangular, poorly sorted ½" gravel.
370	Gravel with Medium to Coarse Sand: Brown-black, subrounded- subangular well sorted less than 30% sand.
380	<u>Gravel</u> : Poorly sorted, 'gravel, subangular, less than 20% coarse sand.
380 11111111	<u>Gravel</u> : Medium sorted, gray-black-brown, subangular, less than 10% sand, 5" gravel.
400 -	

PROJECT NUMBER	79-290	45
PROJECT NAME	NX SITING	INVESTIGATION
EQUIPMENT USED	Revers	e Circulation
COMPANY	Beylik	
OPERATOR	J. Cly	de

FIELD LOG OF WELL NUMBER _ OW-2	
VALLEY NAVE Dry Lake	
LOCATION NUMBER	1200
LOGGED BY JM & SC DATE 1/14	/80
CHECKED BY JAG DATE 4/10	/80
TOTAL WELL DEPTH 1300 feet	

PAGE 5 OF 13

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
400	Gravel with Sand, Silt & Clay: Poorly sorted, gray-black, subangular-subrounded, less than 30% sand, 20% silt and clay, ½" gravel.
410-1	Gravel with Sand, Silt & Clay: Poorly sorted, subangular to subrounded, gray-black, less than 20% sand, less than 10% silt and clay.
420	Gravel with Sand, Silt & Clay: Poorly sorted, subangular, brown-gray, less than 40% sand, less than 10% silt and clay, 2½" gravel.
430	Gravel with Sand, Silt & Clay: Poorly sorted, brown-black, subangular, 3/4" gravel, less than 20% sand, less than 10% silt and clay.
440	Gravel with Sand, Silt & Clay: Poorly sorted, blue-black, subangular, 3/4" gravel, less than 15% sand, less than 10% silt and clay.
450	Gravel with Sand, Silt & Clay: Poorly sorted, subangular, gray-black, 'gravel, less than 40% sand, less than 10% silt and clay.
460	Gravel with Sand, Silt, & Clay: Poorly sorted, subangular, gray-brown, 'gravel, less than 40% sand, 10% silt and clay.
4 70	Gravel with Sand, Silt and Clay: Brown-gray poorly sorted subrounded, max 2" gravel, less than 20% sand, less than 10% silt and clay.
4 80	Gravel with Sand and Clay: Gray-black colored, poorly sorted subangular gravel with less than 30% coarse to fine-grained sand with less than 10% silty clay. Max grain size 3/4".
4 90 -	<u>Gravel with Sand</u> : White, gray-black colored moderately sorted subangular gravel with less than 20% coarse subangular sand grains. Maximum grain size 1".
E 66 -	<u> 1</u>

1.3

PROJECT NUMBER	79-290- 45
PROJECT NAME	WX SITING INVESTIGATION
EQUIPMENT USED	Reverse Circulation
COMPANY	Beylik
OPERATOR	J. Clyde

PAGE <u>6</u> OF <u>13</u>

LOCATION NUNBER _______ T3S, R64E, Sect. 1200 LOGGED BY ______ DATE ______ DATE ______ CHECKED BY ______ JAG ____ DATE ______ TOTAL WELL DEPTH ______ 1300 feet ______

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
50 0	Gravel with Sand: Gray, black colored moderately sorted subrounded to subangular gravel with less than 15% coarse subangular sand. Maximum gravel size approximately 2"
510 111 11	Gravel with Trace Coarse Sand: Brown, subangular, well sorted, gravel to 14", less than 10% sand.
520	Gravel with Trace Sand and Silt: Same as 510' with less than 10% sand and silt.
530 -	Gravel with Trace Coarse Sand: Same as 510'.
540	
5 50	Gravel with Sand and Silt: Brown-gray, subangular, moderate sorting. Less than 25% sand and silt.
5 60	Gravel with Trace Coarse Sand: Same as 510'.
5 70 -	
5 80 -	
5 90	
6 00	<u> </u>

PROJECT NUMBER	79-290- 45
PROJECT NAME	WX SITING INVESTIGATION
EQUIPMENT USED	Reverse Mud Rotary
COMPANY	Beylik
OPERATOR	J. Clyde

n Tari

| . | .

F

1

PAGE 7 OF 13

FIELD LOG OF WELL NUMBE	R2
VALLEY NAVE Dry Lake	
LOCATION NUMBER T3S, R64E	C, Sect. 12 90
LOGGED BY <u>SC & JM</u> DA	TE 1/15/80
CHECKED BY JAG DA	TE 4/10/80
TOTAL WELL DEPTH 1300 f	eet

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
60 0 / 1111	
6 10 -11	Gravel with Trace Coarse Sand: Brown, subangular,well sorted, gravel to 1½", less than 10% sand.
6 20	
630 Juni	Gravel with Trace Coarse Sand: Same as 610', but max size $\frac{1}{2}$ ".
640 1111	Gravel with Sand and Silt: Brown, subangular, poorly sorted, less than 30% sand, less than 10% silt, gravel size to $\frac{1}{2}$ ".
650 mm	
660	
6 70 -	
6 80 / 111	
88 80 1111	
	•

PAGE 8 OF 13

FIELD LOG OF WELL NUMBER ______

PROJECT NUMBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Mud Rotary
COMPANY	Beylik
OPERATOR	J. Clyde

1

 VALLEY NAVE
 Dry Lake

 LOCATION NUMBER
 T3S, R64E, Sect. 12

 LOGGED BY
 SC

 DATE
 1/17/80

 CHECKED BY
 JAG

 DATE
 4/10/80

 TOTAL WELL DEPTH
 1300 feet

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
70 0 -	Gravel with Some Coarse Sand: Brown, subangular, well sorted gravel size to 3/4", less than 20% sand.
710 - 111	Gravel with Some Coarse Sand: Same as 700' but with gravel to 2".
720-111	Gravel with Some Coarse Sand: Same as 700'.
730	Gravel with Sand, Silt, & Clay: Brown, subangular gravel to $\frac{1}{2}$ " size with 20% sand, 20% silt & clay.
740	Gravel with Some Coarse Sand: Same as 700'.
88 Brututt	Gravel with Trace Coarse Sand: Same as 700' but less than 10% sand,& gravel to 3".
760	Gravel with Trace Coarse Sand: Same as 750'.
770 - 111	Gravel with Some Coarse Sand: Same as 700'.
780	
790 -	
800	

PAGE ____ DF ____3

FIELD LOG OF WELL NUMBER_	OW2
VALLEY NAVE Dry Lake	
LOCATION NUMBER	Sect. 1254
LOGGED BY SC & JM DATE	1-18-80
CHECKED BY JAG DATE	4-10-80
TOTAL WELL DEPTH	<u>t</u>

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
800	Coarse Sand Trace Gravel & Silt: Brown subangular, well sorted, coarse sand, less than 10% gravel, less than 10% silt.
810 - 11	Gravel with Some Coarse Sand: Brown, subangular, well sorted, gravel size to 1", 20% sand.
820	
830	
8 40 - 1	
8 50 III III 1 1 1 III IIII III IIII III III III III III III I	
8 60	
8 70 -	
8 80	
8 90	
900	

 PROJECT NUMBER 79-290- 45

 PROJECT NAME NX SITING INVESTIGATION

 EQUIPMENT USED Reverse Rotary

 COMPANY Beylik

 OPERATOR J. Clyde

J

Ĵ

- total

ALCONT 2

.

j

ĺ

İ

1

1

1

5

PROJECT NUMBER 79-290- 45 PROJECT NAME MX SITING INVESTIGATION EQUIPMENT USED Reverse Rotary COMPANY Beylik OPERATOR J. Clyde

PAGE 10 OF 13

 FIELD LOG OF WELL NUMBER _____OW2

 VALLEY NAME _____Dry Lake

 LOCATION NUMBER _____T3S, R64E, Sect. 12

 LOCGED BY _____JM & SC _____DATE _____1-19-80

 CHECKED BY _____JAG _____DATE _____10-80

 TOTAL WELL DEPTH _______1300 feet

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
90 0	Sand with Some Gravel & Silt: Brown subangular, poorly sorted, sand with 10% silt & clay, 20% gravel.
910	
920	
9 30 111	
9 40 - 11 9 10 - 11	Gravel with Trace Coarse Sand: Brown subangular, well sorted, gravel to 3/4", 10% sand.
9 50 - 111	
950 950	
970	
9 80 11111	
8 8 6 111111	
1000	

Ł

h

1

Ì

1

1

1

1

PROJECT NUNBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	<u>Reverse Rotary</u>
COMPANY	Beylik
OPERATOR	J. Clyde

	PAGE 11 OF 13
FIELD LOG OF WELL	NUMBER OW2
VALLEY NAVE Dr	y Lake
LOCATION NUMBER	S, R64E, Sect. 12
LOGGED BY JM & SC	DATE 1-20-80
CHECKED BY JAG	DATE DATE
TOTAL WELL DEPTH	300 feet

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
1000 -	
	Gravel with Cobbles: Dark colored, poorly sorted subangular to angular (predominantly angular) gravel with less than 5% broken cobbles up to 3".
10 20	Gravel with Cobbles: As above (1010'),more darker rocks, medium to dark color.
10 30	<u>Gravel with Sand</u> : Medium color, poorly sorted, subangular to angular gravel up to 1", with less than 20% fine-to coarse- grained, angular to subangular sand.
10 40	Gravel: Medium color, poorly sorted, subangular to angular gravel with 20% cobbles up to 25, with 20% medium to coarse, subangular to angular sand.
1050	<u>Gravel</u> : Light to dark colored, poorly sorted, subrounded to angular gravel up to 15".
10 60	Gravel with Sand: Light to dark color, medium sorted, subangular to angular gravel up to 3/4".
1070-	<u>Gravel</u> : Medium to dark color, well sorted, angular to subangular fine-grained gravel up to $\frac{1}{2}$ ".
1080-	Gravel with Fund: Medium to dark color, poorly sorted, subangular to angular gravel up to 1" with less than 25% coarse-to medium-grained, subangular to angular sand.
90	
· •	Grivel: as above (1080'), but medium sorted.

PROJECT NUNBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Rotary
COMPANY	Beylik
OPERATOR	J. Clyde

والمحافية الأرجبان الارجبانية لرجبان ويترجب وتترير

PAGE 12 OF 13

FIELD LOG OF WELL NUMBER ______ VALLEY NAVE ______ Dry Lake Valley LOCATION NUMBER T3S, R64E, Sect. 1200 LOGGED BY ______ JM & LB _____ DATE ______ LOGGED BY ______ DATE ______ CHECKED BY ______ DATE ______ TOTAL WELL DEPTH______ 1300 feet

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
1100 -	
11 10 -1	<u>Gravel</u> : Dark colored, well sorted, angular gravel up to 3/8".
1120	Gravel: Medium color, poorly sorted, subrounded to angular gravel up to $\frac{1}{2}$ " with less than 20% sand.
11 30 - 11	<u>Gravel with Sand</u> : Light to dark color, poorly sorted, subrounded to rounded gravel up to 1" with 20% coarse to fine sand.
	Gravel with Sand: As above (1130') with occassional broken cobbles up to 4".
11 50 - 11	Gravel with Sand: Medium to dark color, medium sorted subangular to angular gravel up to 1" with less than 20% medium to coarse sand.
11 60	Gravel with Sand: Light to dark color, well sorted angular to subangular, fine gravel with 20% coarse sand.
11 70	Gravel: Medium color, poorly sorted, subangular to angular, fine to 15" gravel.
11 80	
11 90 11171	<u>Gravel</u> : Dark colored, poorly sorted, angular to subangular fine up to 2" gravel.
12 00 -	<u> </u>

PROJECT NUMBER	79-290- 45
PROJECT NAME	NX SITING INVESTIGATION
EQUIPMENT USED	Reverse Rotary
COMPANY	Beylik
OPERATOR	J. Clyde

1

PAGE 13 OF 13

Æ

FIELD LOG OF WELL NUMBER	12
VALLEY NAVE Dry Lake	
LOCATION NUMBER T35, R64E, Sec	t. 1200
LOGGED BY DATE	-22-80
CHECKED BY JAG DATE 4	-10-80
TOTAL WELL DEPTH 1300 feet	

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
1200 -	
12 10	<u>Gravel</u> : Medium to dark color, poorly sorted angular to subangular, fine up to l_{3}^{L} " gravel.
1220-	<u>Gravel</u> : Medium to dark color, medium sorted, subrounded to subangular, fine to ½" gravel.
12 30	
12 40	Sand with Gravel: Light to medium color, medium sorted, subrounded to subangular, medium to coarse sand with less than 10% gravel up to $\frac{1}{2}$ ".
12 50	Sand and Gravel: Light to dark color,well sorted,angular to subangular,fine gravel with 50% coarse sand.
12 60	Gravel with Sand: Light to medium colored medium sorted, subangular to angular gravel with less than 25% coarse sand.
1270-	<u>Gravel</u> : Light to dark colored, well sorted, angular to subangular gravel up to 3/8".
12 80 -	Sand & Gravel: Light to dark colored, well sorted, angular to subangular, fine gravel with - 50% coarse sand.
12 90 -	Gravel with Sand: Medium to dark colored, poorly sorted, angular to subangular gravel up to 3/4" with - 25% coarse sand.
1300-	

PROJECT NU	MBER	79-290-	45			Y A
PROJECT NJ	ME	MX SIT	ING INVE	ESTIGATIO	<u>N</u>	LO
EQUIPMENT	USED	Bucket	Auger	0'-40'	Reverse Rotary	LO
COMPANY	Be	ylik			40' - TD	CH
OPERATOR _	<u>J</u> .	Clyde				TO

3

tent tent

a a

J

J

2

VALLEY NAVE		Dry 1	Lake		
LOCATION NUM	BER	T65,	R63E,	Sec.	12010
LOGGED BY	JM		DATE	2-6-	80
CHECKED BY	JAG		DATE	4/10/	80
TOTAL WELL D	EPTH_	101	lO fee	t	

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
s Lind	Silt: Tan silt with occasional gravel up to 14".
5 ⊓111111	<u>Silt</u> : Tan silt.
20	Silt: Tan silt with less than 25% medium colored, fine- to coarse-grained, poorly sorted, subrounded to subangular sand with less than 10% gravel up to 1½".
30 1111111	Gravel with Cobbles: Medium to dark colored, subrounded to subangular, medium gravel with cobbles up to 4".
40 11 11 11	Gravel: Medium colored, moderately sorted, angular to subrounded, fine to coarse gravel up to 14".
; ; ; ; ; ; ;	Gravel up to 1".
	Gravel: Medium colored, moderately sorted, subangular to subrounded, fine to coarse gravel up to 15" with less than 5% coarse-grained sand.
	Gravel up to 3/4".
9000000000000000000000000000000000000	
80 1111111	Gravel up to 14".
100-3	

end National, Inc. DRILL CUTTINGS LOG

ROJECT NUNBER	79-290- 45
ROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Rotary
OMPANY	Beylik
PERATOR	J. Clyde

1

110 -

1 40 -

1 50 -

1 60

170

180

190 -

PAGE ____ OF ____ FIELD LOG OF WELL NUMBER TW-1 VALLEY NAVE Dry Lake LOCATION NUMBER T6S, R63E, Sect. 12d-LOGGED BY JFM DATE 2-6-80 CHECKED BY JAG DATE 4/10/80 TOTAL WELL DEPTH ______ 1010 feet _____

DEPTH DESCRIPTION OF CUTTINGS OR SAMPLE (FEET) 100 -Gravel: Dark brown colored, well sorted, subangular to subrounded, gravel up to $\frac{1}{2}$ ". -Very well sorted gravel up to 1/2". 120------Gravel up to 3/4". 1 30 -Gravel: Light to dark colored, very well sorted, subangular to subrounded gravel up to 4". Gravel: Light to dark colored, poorly sorted, subangular to subrounded gravel with occasional cobbles up to 2". Less than 20% medium- to coarse-grained sand. Gravel: Light to dark colored, well sorted, subangular to subrounded, fine to medium gravel, occasionally up to 1", with less than 10% coarse-grained sand. Gravel with Cobbles: Light to dark colored, poorly sorted, angular to subrounded, fine to coarse gravel, with cobbles up to 3" and less than 5% coarse-grained sand.

> Gravel: Light to dark colored, moderately sorted, subangular to subrounded, fine to coarse gravel, with occasional cobbles up to 14" and less than 5% coarse sand.

- Cobbles up to 2".

200-

PROJECT NUMBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Rotary
COMPANY	Beylik
OPERATOR	J. Clyde

U

]

PAGE _3_ OF _ 11

FIELD LOG	OF WE	LL NUM	BER_	TW-1	
VALLEY NAVI	Dry	y Lake			<u> </u>
LOCATION NU	IMBER	<u>165. R</u>	63E,	Sec.	12 đ- 12
LOGGED BY _	JFM		DATE	2-06-	-80
CHECKED BY	JAG		DATE	4-10	-80
TOTAL WELL	DEPTH	1010	feet		

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
200 -	Gravel: Light to dark colored, poorly sorted, angular to subangular, fine to coarse gravel with less than 20% cobbles up to 2½" and less than 5% coarse-grained sand.
210	Gravel: Light to dark colored, moderately sorted, angular to subangular, fine to coarse gravel, with occasional cobbles up to 4" and less than 5% medium- to coarse-grained sand.
2 30 - 	<u>Gravel</u> : Light to dark colored, well sorted, subangular to subrounded, fine to coarse gravel up to 2½", with less than 10% medium- to coarse-grained sand.
240-1	<u>Gravel</u> : Light to dark colored, moderately sorted, subangular to subrounded, fine to coarse gravel up to l", with less than 10% medium- to coarse-grained sand.
250 J	Gravel up to 2".
200	Sand: Medium colored, well sorted, fine-grained sand, with less than 25% medium-grained sand to coarse gravel up to 2".
2/1	Gravel: Medium to dark colored, medium sorted, subangular to subrounded, fine to coarse gravel up to 2½", with less than 10% coarse-grained sand.
280-1	Gravel with Sand: Medium to dark colored, poorly sorted, subrounded to angular, fine to coarse gravel up to 15", and approximately 25% medium colored, fine- to coarse- grained sand.
2 90 Juniliu	Gravel: Medium to dark colored, moderately sorted, subrounded to subangular, fine to medium gravel up to 5", with approxi- mately 10% fine- to coarse-grained sand.
300	

/:**-**4.

PROJECT NUMBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Rotary
COMPANY	Beylik
OPERATOR	J. Clyde

1

]

PAGE _4_ DF _11

1.

FIELD LOG	OF WEL	L NU	IMBER_	<u>TW-</u>]	L
VALLEY NAWE	Ľ	Dry I	ake		
LOCATION NUM	BER	r6 s ,	R63E,	Sec.	124.10
LOGGED BY	LB		DATE		-80
CHECKED BY	JAG		DATE	4-10	-80
TOTAL WELL I	DEPTH	10	10 fee	t	

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
300 111 11	Gravel: Medium to dark colored, moderately sorted, subrounded to angular, fine to medium gravel up to 1/3", with approximately 10% fine- to coarse-grained sand.
310	<u>Gravel</u> : Medium to dark colored, poorly sorted, subangular to angular, fine to 2½" gravel.
320	Gravel: Dark colored, poorly sorted, subrounded to angular, fine to 2" gravel (less than 10% sand).
3 30 11 1111	<u>Gravel</u> : Dark colored, poorly sorted, subrounded to angular, fine to 2½" gravel (less than 5% sand).
3 40 - 11	<u>Gravel with Sand</u> : Dark colored, poorly sorted, subangular to angular,fine to 2" gravel, with less than 20% medium colored, medium-to coarse-grained sand.
350	<u>Gravel</u> : Dark colored, poorly sorted, subangular to angular, fine to 3/4" gravel with less than 10% sand.
3 60 1	<u>Gravel</u> : Dark colored, moderately sorted, subangular to angular, fine to $\frac{1}{2}$ " gravel.
3 70	<u>Gravel</u> : Dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 1" gravel.
380 11111	<u>Gravel</u> : Dark colored, poorly sorted, subangular, fine to ኳ" gravel (with less than 10% sand).
390 1111111	<u>Gravel</u> : Medium to dark colored, poorly sorted, subangular to angular, 1/3"-diameter gravel with less than 15% sand.
_ nn _ =	

PROJECT NUMBER 79-290- 45 PROJECT NAME MX SITING INVESTIGATION EQUIPMENT USED Reverse Rotary

CONPANY Beylik OPERATOR J. Clyde

1

PAGE	5_	OF	_11
------	----	----	-----

FIELD LUG O	F WELL NUM	IRFK	TW-1	
VALLEY NAME _	Dry Lak	<u>.e</u>		
LOCATION NUMB	ER	R63E,	Sec.	12.120
LOGGED BY	LB , JM	DATE _	2-07-	-80
CHECKED BY	JAG	DATE	4-10	-80
TOTAL WELL DE	PTH <u>101</u>	0 feet	<u> </u>	

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
400	Gravel: Light to dark color, medium sorted, subangular to
	subrounded gravel up to $\frac{1}{2}$ " with less than 15% medium- to coarse-grained sand.
410	Gravel with Sand & Clay: Medium colored, poorly sorted, suban- gular to subrounded gravel up to 3/8", with less than 50%
420	fine- to coarse-grained sand and clay.
430	Gravel: Medium to dark colored, well sorted, subangular to subrounded gravel up to k", with less than 20% coarse-grained
440	sand.
11111	Gravel up to 1".
450	Less than 10% coarse sand.
460	
1111	Gravel with Sand: Light to dark colored, poorly sorted, subangular to subrounded, fine to coarse gravel up to 1", with less than 30% fine to coarse-grained sand.
470	<u>Gravel with Sand</u> : Medium to dark colored, poorly sorted, subrounded to subangular, fine to 1" gravel with less than 25% medium- to coarse-grained sand.
480	
490 111 1	Gravel up to 3/4".
500	<u> </u>

١.

]]

ĴĮ.

j

jį

]|

P	A	C	E		OF	_11
---	---	---	---	--	----	-----

PROJECT NUNBER	79-290- 45
PROJECT NAME	MX SITING INVESTIGATION
EQUIPMENT USED	Reverse Rotary
COMPANY	Beylik
DPERATOR	J. Clyde

FIELD LOG	OF WE	ELL NUP	MBER	TW-1	
VALLEY NAVE		Dry	Lake		
LOCATION NU	IMBER _	T65	<u>_ R63E</u> ,	Sec.	12 6 40
LOGGED BY _	LE,	JFM	DATE _	2/08,	/80
CHECKED BY	JAG		DATE _	4/10/	/80
TOTAL WELL	DEPTH_	101	LO feet		

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
500 111	Gravel with Sandy Silt: Medium to dark colored, poorly sorted, subrounded to angular, fine to 1" gravel with less than 30% tan colored, coarse-grained sand to silt.
510-11	Gravel: Medium to dark colored, moderately sorted, angular, fine to 1½" gravel.
520 - 11 - 11	5% fine- to coarse-grained sand.
530 mm	
540 - 11 1111	<u>Gravel</u> : Light to dark colored, poorly sorted, angular to subangular, fine to 2½" gravel with less than 10% sand.
550 550	<u>Gravel</u> : Medium to dark colored, poorly sorted, angular to subangular, fine to 1" gravel with less than 25% medium colored, fine- to coarse-grained sand.
560	Gravel and Sand: Medium to dark colored, poorly sorted, angular to subangular, fine to ';" gravel with less than 40% medium to dark colored sand.
570 1111 1111	Gravel: Medium to dark colored, poorly sorted, angular to subangular, fine to 1" gravel with less than 20% fine- to coarse-grained sand.
580	<u>Gravel</u> : Dark colored, moderately sorted, subrounded to subangular gravel with less than 10% sand.
590 mm	Sand content up to about 25%.

PROJECT NAME <u>NX SITING INVESTIGATION</u> EQUIPMENT USED <u>Reverse Rotary</u>

CONPANY Beylik
OPERATOR J. Clyde

PROJECT NUMBER 79-290- 45

L L

Ĵ

1

]

1

}

PAG	GE	7	0F	11
	_			

 Γ

FIELD LOG OF WE	LL NU	MBER_	TW-	1
VALLEY NAME	Dry	Lake		<u>.</u>
LOCATION NUMBER	т6S,	R63E,	Sec.	12 00
LOGGED BYLB		DATE	2-08	-80
CHECKED BY		DATE	4-10-	-80
TOTAL WELL DEPTH	101	0 feet		

 Sand and Gravel with Silt: Dark colored, moderately sorted, fine-grained to h" sand and gravel with less than 50% tan silt. Gravel: Dark colored, moderately sorted, subangular to angular fine to 1" gravel. Gravel: Dark colored, moderately sorted, subrounded to subangular, fine to 2" gravel with less than 10% sand. Gravel: Dark colored, moderately sorted, subangular to angular fine to 1" gravel with less than 5% coarse-grained sand. Gravel: Dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 2" gravel. Gravel: Medium to dark colored, well sorted, subangular to angular to angular (predominantly angular), fine to 14" gravel, with less than 10% sand. Gravel: Medium to dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 14" gravel, with less than 10% sand. Gravel: Medium to dark colored, moderately sorted, subangular to angular (predominantly angular), fine to 14" gravel, with less than 10% sand. Gravel: Medium to dark colored, moderately sorted, subangular to angular (predominantly angular), fine to 14" gravel, with less than 10% sand. Gravel: Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. Gundar dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. 	DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
 610 Gravel: Dark colored, moderately sorted, subangular to angular fine to 1" gravel. 620 Gravel: Dark colored, moderately sorted, subrounded to subangular, fine to 2" gravel with less than 10% sand. 630 Gravel: Dark colored, moderately sorted, subangular to angular fine to 1" gravel with less than 5% coarse-grained sand. 640 Gravel: Dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 2" gravel. 650 Gravel: Medium to dark colored, well sorted, subangular to angular to angular (predominantly angular), fine to 1\3" gravel. 670 Gravel: Medium to dark colored, poorly sorted, subangular to angular to angular (predominantly angular), fine to 1\3" gravel. 680 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular to angular, fine to 1/3" gravel. 680 Gravel: Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. 680 Gravel: Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. 	60 0 111 11	Sand and Gravel with Silt: Dark colored, moderately sorted, fine-grained to $\frac{1}{2}$ " sand and gravel with less than 50% tan silt.
 620 Gravel: Dark colored, moderately sorted, subrounded to sub- angular, fine to 2" gravel with less than 10% sand. 630 Gravel: Dark colored, moderately sorted, subangular to angular fine to 1" gravel with less than 5% coarse-grained sand. 640 Gravel: Dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 2" gravel. 650 Gravel: Medium to dark colored, well sorted, subangular to angular (predominantly angular), fine to 1/3" gravel. 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular (predominantly angular), fine to 1% gravel, with less than 10% sand. 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. 680 - Increasing fine-grained gravel. 690 Gravel: Medium to dark colored, well sorted, subrounded to angular, fine to ½" gravel. 	610 11 11 11	<u>Gravel</u> : Dark colored, moderately sorted, subangular to angular, fine to l" gravel.
 630 Gravel: Dark colored, moderately sorted, subangular to angular fine to 1" gravel with less than 5% coarse-grained sand. 640 Gravel: Dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 2" gravel. 650 Gravel: Medium to dark colored, well sorted, subangular to angular, fine to 1/3" gravel. 650 Gravel: Medium to dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 14" gravel, with less than 10% sand. 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular to angular, fine to 1/3" gravel. 680 - Increasing fine-grained gravel. 690 Gravel: Medium to dark colored, well sorted, subrounded to angular, fine to 4" gravel. 	620	<u>Gravel</u> : Dark colored, moderately sorted, subrounded to sub- angular, fine to 2" gravel with less than 10% sand.
 640 Gravel: Dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 2" gravel. 650 Gravel: Medium to dark colored, well sorted, subangular to angular, fine to 1/3" gravel. 660 Gravel: Medium to dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 1½" gravel, with less than 10% sand. 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular to angular, fine to 1/3" gravel. 680 Gravel: Medium to dark colored, moderately sorted, subangular to angular to angular, fine to 1/3" gravel. 680 Increasing fine-grained gravel. Gravel: Medium to dark colored, well sorted, subrounded to angular, fine to ½" gravel. 	630 1111111	<u>Gravel</u> : Dark colored, moderately sorted, subangular to angular, fine to 1" gravel with less than 5% coarse-grained sand.
 650 Gravel: Medium to dark colored, well sorted, subangular to angular, fine to 1/3" gravel. 660 Gravel: Medium to dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 14" gravel, with less than 10% sand. 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. 680 Increasing fine-grained gravel. Gravel: Medium to dark colored, well sorted, subrounded to angular, fine to 4" gravel. 	640	<u>Gravel</u> : Dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 2" gravel.
 660 Gravel: Medium to dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 14" gravel, with less than 10% sand. 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. 680 Increasing fine-grained gravel. Gravel: Medium to dark colored, well sorted, subrounded to angular, fine to 4" gravel. 	6 50 11 11 11	<u>Gravel</u> : Medium to dark colored, well sorted, subangular to angular, fine to 1/3" gravel.
 670 Gravel: Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel. 680 Increasing fine-grained gravel. Gravel: Medium to dark colored, well sorted, subrounded to angular, fine to ½" gravel. 	, 6 00 .	Gravel: Medium to dark colored, poorly sorted, subangular to angular (predominantly angular), fine to 15" gravel, with less than 10% sand.
680 Increasing fine-grained gravel. 690 Gravel: Medium to dark colored, well sorted, subrounded to angular, fine to b" gravel.	6 70 - 11	<u>Gravel</u> : Medium to dark colored, moderately sorted, subangular to angular, fine to 1/3" gravel.
690	88 80 uluulu	Increasing fine-grained gravel.
	690	<u>Gravel</u> : Medium to dark colored, well sorted, subrounded to angular, fine to ¹ / ₂ " gravel.

	PAUL UF
FIELD LOG OF WELL	NUMBER
VALLEY NAVE Dry	Lake
LOCATION NUMBER	, R63E, Sec. 120 35
LOGGED BYLB, JFM	DATE _2/09/80
CHECKED BY JAG	DATE 4/10/80

TOTAL WELL DEPTH 1010 feet

PROJECT NAME	MX SITING INVESTIGATION	
EQUIPMENT USED _	Reverse Rotary	
COMPANY	Beylik	
OPERATOR	J. Clyde	

PROJECT NUMBER 79-290- 45

DEPTH DESCRIPTION OF CUTTINGS OR SAMPLE (FEET) 700 -Gravel: Dark colored, well sorted, subangular to angular, 710 fine to 15" gravel. 720 Gravel: Dark colored, well sorted, subangular to angular (predominantly angular), fine to 1" gravel. 730 -Gravel: Dark colored, poorly sorted, subangular, fine to medium gravel up to 'z" with less than 25% fine- to coarsegrained sand. 740 -Gravel: Dark colored, poorly sorted, angular to subangular, fine to medium gravel up to 1" with less than 10% fine- to coarse-grained sand. 750 Gravel: Medium to dark colored, poorly sorted, angular to subangular, fine to medium gravel, occasionally up to 14", with less than 10% fine- to coarse-grained sand. 760 Gravel: Medium to dark colored, moderately sorted, angular 111111 to subangular, fine to medium gravel up to 3/4" (predominantly fine gravel), with less than 10% medium- to coarse-grained sand. 1111111111 770 -Gravel with Sand: Medium to dark colored, poorly sorted, angular to subangular, fine to medium gravel up to 3/4" with less than 35% fine- to coarse-grained sand. 780 -Gravel: Medium to dark colored, moderately sorted, angular to subangular, fine to medium gravel up to $\frac{1}{2}$ " with less than 10% medium- to coarse-grained sand. 790 -Gravel: Medium to dark colored, moderately sorted, angular to subangular, fine to medium gravel up to 1" (predominantly 1/8" to 1/4").

800 -

يهيينية ----- يكميناه ------ ولمسط ----- ولمستغ

TUERO NATIONAL, INC. DRILL CUTTINGS LOG

PAGE <u>9</u> OF <u>11</u>

BALL COLLINGS LOG	FIELD LOG OF WELL NUMBER
PROJECT NUMBER 79-290- 45	VALLEY NAVE Dry Lake
PROJECT NAME <u>MX SITING INVESTIGATION</u>	LOCATION NUNBER T65, R63E, Sec. 12# Ac-
EQUIPMENT USED Reverse Rotary	LOGGED BY JFM DATE 2-10-80
COMPANY Beylik	CHECKED BY JAG DATE 4-10-80
OPERATOR J. Clyde	TOTAL WELL DEPTH 1010 feet

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
80 0	<u>Gravel</u> : Light to dark colored, moderately sorted, angular to subangular, fine to medium gravel up to 1".
810	<u>Gravel</u> : Medium to dark color, poorly sorted, angular to sub- angular, fine to medium gravel (predominantly less than $\frac{1}{4}$ " and up to 3/4"), with less than 10% coarse-grained sand.
820 - 1	Gravel: Medium to dark color, well sorted, angular to subangular, fine to medium gravel (predominantly fine, occasionally up to ½"), with less than 10% coarse-grained sand.
830 - 11111	Gravel: Dark colored, moderately sorted, angular to subangular, fine to medium with occasional coarse gravel up to 2-3/4", with less than 5% coarse-grained sand.
840	<u>Gravel</u> : Medium to dark colored, poorly sorted, angular to subangular, fine to medium, occasionally up to 1".
850 111111111111111111111111111111111111	
860 n 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Gravel up to 15", with less than 5% coarse sand.
870-7	<u>Gravel</u> : Medium to dark colored, moderately sorted, angular to subangular, fine to medium gravel up to l" with less than 5% coarse-grained sand.
880	Gravel: Medium to dark colored, moderately sorted, angular, fine to medium gravel up to 14".
890	<u>Gravel</u> : Medium to dark colored, moderately to well sorted, angular to subangular, fine to medium gravel up to 3/4".
900	

COMPANY Beylik OPERATOR J. Clyde

Ę

Ī

1

1

Ĩ

PAGE _____ DF ____

PROJECT NUMBER	79-290- 45		
PROJECT NAME	MX SITING INVESTIGATION		
EQUIPMENT USED	Reverse Rotary		
COMPANYBeylik			
OPERATOR	J. Clyde		

FIELD LOG	OF WE	LL NUN	BER	TW-1	
 VALLEY NAME	<u> </u>	Dry	Lake (DL)	
 LOCATION NU	MBER	T6S,	R63E,	Sec.	124.30
 LOGGED BY _	JFM,	LB	DATE _	2/10/	/80
CHECKED BY	JAG		DATE _	4/10	/80
 TOTAL WELL	DEPTH_	101	0 feet		

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
900	Gravel: Medium to dark colored, well sorted, angular to subangular, fine gravel up to 4", with less than 5% coarse-grained sand.
910 קונוקרו קונוקרו	<u>Gravel</u> : Medium to dark colored, well sorted, angular to subangular, fine to medium gravel, occasionally up to 1", with less than 5% coarse-grained sand.
920	<u>Gravel</u> : Medium to dark colored, moderately well sorted, angular to subangular, fine to medium gravel up to 3/8", with less than 5% coarse-grained sand.
930 17111111	
940	Gravel and Sand: Dark colored, well sorted, subangular to angular, fine gravel and coarse-grained sand.
950	<u>Gravel</u> : Dark colored, poorly sorted, subangular to angular, fine to 2" gravel, with less than 10% medium- to coarse- grained sand.
960	
970	<u>Gravel</u> : Dark colored, well sorted, subrounded to subangular, fine to 1/3" gravel, with less than 20% fine- to coarse- grained sand.
980	<u>Gravel</u> : Dark colored, poorly sorted, subrounded to angular, fine to 3" gravel, with less than 10% sand.
9990	<u>Gravel</u> : Dark colored, moderately well sorted, subangular to angular, fine to 1½" gravel, with less than 5% sand.
- 10 0 0 -	

PROJECT NAME MX SITING INVESTIGATION EQUIPMENT USED Reverse Rotary

PROJECT NUMBER 79-290- 45

COMPANY Beylik

た明日

OPERATOR J. Clyde

PACE _11_ OF _11_

FIELD LOG OF WELL NUMBER <u>TW-1</u>
VALLEY NAME Dry Lake
LOCATION NUMBER
LOGGED BY JFM, LB DATE 2-10-80
CHECKED BY JAG DATE4-10-80_
TOTAL WELL DEPTH 1010 feet

DEPTH (FEET)	DESCRIPTION OF CUTTINGS OR SAMPLE
1000-	Gravel and Cobbles: Medium to dark colored, poorly sorted, subangular to angular gravel to 3". Broken cobbles to 6".
1010	
וולדדו	T.D.: 1010'
20	
30 – 111	
40 - 1	
50	
60 - 11 11	
70 - 1	
80	
90	






















F1.0

1

MX SITING INVESTIGATION, GRAVITY SURVEY-DRY LAKE VALLEY, NEVADA

MX SITING INVESTIGATION GRAVITY SURVEY - DRY LAKE VALLEY Г

NEVADA

Prepared for:

U.S. Department of the Air Force Ballistic Missile Office (BMO) Norton Air Force Base, California 92409

Prepared by:

Fugro National, Inc. 3777 Long Beach Boulevard Long Beach, California 90807

17 March 1980

FOREWORD

Methodology and Characterization Studies during fiscal years 1977 and 1978 included gravity surveys in ten valleys in Arizona (five), Nevada (two), New Mexico (two), and California (one). The gravity data were obtained for the purpose of estimating the gross structure and shape of the basins and the thickness of the valley fill. There was also the possibility of detecting shallow rock in areas between boring locations. Generalized interpretations from these surveys were included in Fugro National's Characterization Reports (FN-TR-26a through e).

During the FY 77 surveys, the measurements were made to form an approximate one-mile grid over the study areas, and contour maps showing interpreted depth to bedrock were made. In FY 79, the decision was made to concentrate the available funds on the basic Verification Program to verify and refine suitable area boundaries. This decision resulted in a reduction in the gravity program. Instead of obtaining gravity data on a grid, the reduced program consisted of obtaining gravity measurements along profiles across the valleys where Verification Studies were also performed.

The Defense Mapping Agency (DMA), St. Louis, was also requested to provide gravity data from their library to supplement the gravity profiles. For Big Smoky, Reveille, and Railroad valleys, a sufficient density of library data is available to permit construction of interpreted contour maps instead of two-dimensional cross sections.

In late summer of FY 79, supplementary funds became available to begin data reduction. At this time, inner zone terrain corrections began on the library data and the profiles from Big Smoky Valley, Nevada, and Butler and La Posa valleys, Arizona. The profile data from Whirlwind, Hamlin, Snake East, White River and Garden Coal valleys, Nevada were available from the field in early October, 1979.

A continuation of gravity interpretations has been incorporated into the FY 80 contract and the results are being summarized in a series of valley reports. The reports covering Nevada-Utah gravity studies will be numbered, "FN-TR-33-", followed by the abbreviation for the subject valley. In addition, more detailed reports of the results of FY 77 surveys in Dry Lake and Ralston valleys, Nevada are being prepared. Verification Studies are continuing in FY 80 and gravity studies are included in the program. DMA will continue to obtain the field measurements and it is planned to return to the grid pattern. The interpretation of the grid data will allow the production of contour maps which will be valuable in the deep basin structural analysis needed for computer modeling in the Water Resources Program. The gravity interpretations will also be useful in the Nuclear Hardness and Survivability (NH&S) evaluations.

The basic decisions governing the gravity program are made by BMO following consultation with TRW Inc., Fugro National and the (DMA). Conduct of the gravity studies is a joint effort between DMA and Fugro National. The field work, including planning, logistics, surveying, and meter operation is done by the Defense Mapping Agency Hydrographic/Topographic Center (DMAHTC), headquartered in Cheyenne, Wyoming. DMAHTC reduces the data to Simple Bouguer Anomaly (see Section Al.4, Appendix Al.0). The Defense Mapping Agency Aerospace Center (DMAAC), St. Louis, calculates outer zone terrain corrections.

Fugro National provides DMA with schedules showing the valleys with the highest priorities. Fugro National also recommended locations for the profiles in the FY 79 studies within the constraints that they should follow existing roads or trails. Any required inner zone terrain corrections are calculated by Fugro National prior to making geologic interpretations.

Sec. Pr

1

ì

ł

1

1

į

ł

ł

ł

1

•

.

1

}

TABLE OF CONTENTS

 Γ

			Page
FOREW	ORD		i
1.0	INTRODUCTION		1
	<pre>1.1 Objective 1.2 Location 1.3 Scope of Work</pre>	• • • • • • • • • • • • • • • • •	$\begin{array}{ccc} \cdot & \cdot & 1 \\ \cdot & \cdot & 1 \\ \cdot & \cdot & 1 \end{array}$
2.0	GRAVITY DATA REDUCTION .		•• 5
3.0	GEOLOGIC SUMMARY		7
4.0	INTERPRETATION		•• 9
	 4.1 Regional - Residual 4.2 Density Selection . 4.3 Modeling 	Separation	•••9 ••9 ••10
5.0	CONCLUSIONS		17
BIBLI	OGRAPHY		18

LIST OF APPENDICES

APPENDIX

A1.0	General	Principles of	the Gravity	Exploration	Method
A2.0	List of	Gravity Data			

LIST OF FIGURES

Figure Number

1	Location Map - Dry Lake Valley, Nevada	2
2	Topographic Setting - Dry Lake Valley,	
	Nevada	3
3	Complete Bouguer Anomaly Contours	6
4	Velocity Profile from Seismic Reflaction	
	Line DL-DS-1	1
5	Velocity Profile from Seismic Refraction	
	Line DL-DS-2	2
6	Interpreted Depth to Bedrock Map	5
7	Cross Sectional View, Profile AA' 1	6

1.0 INTRODUCTION

1.1 OBJECTIVES

Measurements of the gravitational field were made in Dry Lake Valley for the purpose of estimating the overall shape of the structural basin and the thickness of alluvial fill in the basin. These estimates are expected to be useful to the Nuclear Survivability and Hardness (NH&S) community in modeling dynamic response to nuclear detonations and to geohydrologists in evaluating ground water regimes.

1.2 LOCATION

Dry Lake Valley is located in central Lincoln County, Nevada, approximately 106 miles (170 km) NNE of Las Vegas (see Figure 1). The portion of Dry Lake Valley included in this study is approximately 40 miles (65 km) long and 13 miles (22 km) wide, comprising an area of approximately 520 square miles (1347 km²). As shown in Figure 2, Dry Lake Valley is bounded by mountain ranges on three sides and is open to Delamar Valley on the south. U.S. Highway 93, which is the only paved road in the vicinity, crosses the southern end of the valley.

1.3 SCOPE OF STUDY

The Defense Mapping Agency Hydrographic-Topographic Center/ Geodetic Survey Squadron (DMAHTC/GSS) obtained gravitational field measurements at 1069 stations in and around Dry Lake Valley during June and July, 1977. Approximately cne-half of these stations were distributed throughout the valley with about 1 mile (1.6 km) between stations. The rest of the stations were



1

ł



placed either at 1/4-mile (0.4 km) intervals along roads and trails or around the perimeter of the valley on rock outcrops. The station locations are shown on Figures 3 and 6. Station elevations were determined within a tolerance of 5 feet (1.5 m). With this elevation tolerance, the gravity precision is no smaller than 0.3 milligals. The principal facts for all stations are listed in Appendix A2.0.

In addition to the gravity data in Dry Lake Valley, information from two relatively long seismic refraction lines in the northern part of the valley was available. These seismic lines were recorded during Characterization studies by Fugro National in June, 1977 (FN-TR-26e).

2.0 GRAVITY DATA REDUCTION

DMAHTC/GSS obtained the basic observations and reduced them to simple Bouquer Anomalies (SBA) for each station as described in Appendix Al.O. Up to three levels of terrain corrections were applied to convert the SBA to the complete Bouquer Anomaly First, the Defense Mapping Agency Aerospace Center (CBA). (DMAAC), St. Louis, used its library of digitized terrain data and a computer program to calculate corrections for all stations to account for terrain to 104 miles (167 km) from the station. The second level of terrain corrections was necessary because the computer program has limitations in accounting for terrain effects near the stations. This made it necessary, for some stations, to use a ring template to calculate the effect of terrain within approximately 3000 feet of these stations. The third level of terrain corrections was applied to those stations where 10 feet or more of relief was observed within 130 feet of the station. For these stations, elevation differences were measured in the field at a distance of 130 feet along six directions from the stations. These data were used to calculate the effect of the very near relief. Figure 3 is a contour map of the CBA which also shows the locations of the gravity stations and approximate rock outcrop line at the edges of the valley.













3.0 GEOLOGIC SUMMARY

The structural geologic setting, major rock types, and depositional regime of the valley-fill material are important considerations in the interpretation of the gravitational field data. Dry Lake Valley exhibits typical basin and range structure; high angle, normal basement faults, oriented north-south, probably border the North Pahroc Range on the west, and the Bristol, Highland, and Chief ranges on the east. The area between was faulted downward. Stewart, and Carlson (1978) indicate that a north-south trending fault on the eastern side of the valley cuts through the surface alluvium. This is further substantiated by Shawe (1965) and Fugro National, Inc. (1978, FN-TR-26E). Shawe (1965) also mentions transverse faults, near the Dry Lake area, occurring at large angles to the major north-south structural trends.

The outcrops in the mountains on the western side of the valley are predominantly Tertiary ash flow tuffs with some Paleozoic carbonate rocks. Conversely, the eastern mountains are composed primarily of Paleozoic carbonates with minor amounts of Tertiary ash flow tuffs (Stewart, and Carlson, 1978). The Paleozoic carbonate rocks in Nevada are generally reported to be relatively high density, on the order of 2.8 g/cm³. The volcanic rocks in Nevada are highly variable in density. In general, their density ranges fall between 2.2 and 2.5 g/cm³.

At the surface, the total valley fill is composed of young and intermediate age alluvial fan deposits (72 percent of surface

area), fluvial and stream terrace deposits (16 percent), playa and older lacustrine deposits (six percent), and undifferentiated fluvial, alluvial, and lacustrine deposits (six percent), (Fugro National, Inc. 1978, FN-TR-26e). Except for younger stream channel and playa deposits, the valley fill is late Tertiary and early Quaternary in age. Eakin (1963) describes, the valley fill as consisting of unconsolidated to partly consolidated silt, sand, and gravel derived from adjacent highlands, and including some rocks of volcanic origin.

4.0 INTERPRETATION

The gravitational effect of the light weight material filling the Dry Lake structural basin dominates the CBA map in Figure 3. The CBA values become increasingly negative toward the center of the valley.

4.1 REGIONAL-RESIDUAL SEPARATION

A fundamental step in gravity interpretation is evaluation of the portion of the CBA which represents the geologic feature of interest, in this case, the relatively low density valley fill. The part of the gravity field which is of interest is called the "residual" anomaly. The magnitude of the residual anomaly is a product of: 1) the thickness of alluvial fill; and 2) the contrast in density between the fill and bedrock.

The residual anomaly was isolated by first estimating the way the CBA field would have appeared if there had been no valley fill present. This estimated field is called the "regional" gravity. For this study, the regional field was calculated by fitting (by least squares) a second-order polynomial surface to the CBA values at the bedrock stations around the valley. The regional field was then subtracted from the CBA. The remainder was the residual anomaly.

4.2 DENSITY SELECTION

To calculate the thickness of alluvium which caused the residual anomaly, it is necessary to know the density contrast between the alluvial fill and the bedrock. Only very generalized

information on densities is available, and, for calculation, they were treated as if they are constant throughout the valley. Upon consideration of these factors, it becomes clear that the thickness of alluvium (or depth to rock) interpretation is a coarse approximation.

Interpretations from the two seismic refraction lines in the northern end of the valley were used to constrain the selection of the density contrast. These interpretations are shown in Figures 4 and 5. The highest velocities in the profiles are on the order of 15,000 fps (4572 mps). These were interpreted to represent carbonate bedrock. By "trial and error" calculations, it was found that use of a density contrast of 0.45 g/cm³ caused the depth calculated from the gravity to approximately agree with the seismic interpretation.

The density measured for samples of alluvial fill obtained from shallow borings in Dry Lake Valley range from 2.1 g/cm³ to 2.4 g/cm³. Published values for carbonate rocks typically range between 2.6 and 2.8 g/cm³. The contrast of 0.45 g/cm³ appears to be reasonable in light of these typical values. This contrast should be considered a maximum, because the average density of the alluvial materials will become greater as the depth of burial increases.

4.3 MODELING

For computation and contouring, values for surface elevations and CBA were interpolated at the nodes of a regular 1 mile (1.6 km) grid over the valley. Portions of the grid, where







1.7





there were insufficient station data to establish reliable nodal values, were masked out.

Bedrock depths at each node were computed by iterative computer programs that considered the gravity effect from the model at the other nodes as well as beneath the node in question. Contours showing the interpreted depth to bedrock are displayed in Figure 6. The CBA contours in Figure 3 show linear gradients along both sides of the valley. These gradients range from 10 to 14 milligals per mile. These gradients are thought to be produced by large, steep bedrock faults. The second vertical derivative of the CBA field was calculated to guide the placement of the faults shown in Figure 6. Since the zero contour of the second vertical derivative marks the steepest part of the input CBA field, the faults were placed along the zero contour. This places the trace of the eastern boundary fault slightly more than 1 mile (1.6 km) west of surface cracks in the alluvium mapped as a fault along the eastern boundary of Dry Lake Valley.

The two faults interpreted to cross the valley are not so clearly defined as the boundary faults. They are positioned where changes in strike of the major gravity gradients and the axis of the valley occur. There is significant change in bedrock elevation associated with the northern transverse fault, but little, if any vertical change across the southern fault.

A cross-section view across the central part of the valley (Section AA', Figures 3 and 6) is shown in Figure 7. The top

Li

part of the figure shows the shape of the CBA profile along this section. The lower part shows the surface profile and the interpreted bedrock profile.













$\int \nabla q$

.



Π

×.

þ



5.0 CONCLUSIONS

The interpretation of the gravity survey of Dry Lake Valley indicates that there are major range bounding normal faults on both sides of the valley. The graben between the boundary faults is calculated to be on the order of 10,000 feet deep. The northern third of the valley is substantially shallower than the southern part.

There is a large, well defined negative gravity anomaly associated with Dry Lake Valley. An average density contrast of 0.45 g/cm³ between the alluvium and bedrock was used to calculate the thickness of alluvium which would create such an anomaly. If a smaller contrast had been used, the calculated thickness would have been greater. Conversely, if a larger contrast had been used, the calculated thickness would have been smaller.

Additional modeling with other density contrasts was not justified because so little is known about the actual density distribution in and around the valley.

If future studies acquire better density data or actual thicknesses of alluvium in relatively deep parts of the basin, the gravity interpretation can be refined and made more accurate.
BIBLIOGRAPHY

- Eakin, T.E., 1963, Ground Water Appraisal of Dry Lake and Delamar Valleys: U.S. Geol. Survey, Ground Water Resources - Reconnaissance Series, Report 16, 24 p.
- Fugro National, Inc. 1978, MX siting investigation geotechnical summary prime characterization sites, Great Basin Candidate Siting Province Report, 70 p., 4 appendices (FN-TR-26e).
- Shawe, D.R., 1965, Strike-slip control of basin-range structure indicated by historical faults in Western Nevada: Geological Society of America Bulletin, Vol. 76, pp. 1361-1378.

Stewart, J.H., and Carlson, J.E., 1978, Geologic Map of Nevada: U.S. Geol. Survey, 1:500,000.

.

- China and

[

5

APPENDIX A1.0

GENERAL PRINCIPLES OF THE GRAVITY EXPLORATION METHOD

۰

A1.0 <u>GENERAL PRINCIPLES OF THE GRAVITY</u> EXPLORATION METHOD

A1.1 GENERAL

A gravity survey involves measurement of differences in the gravitational field between various points on the earth's surface. The gravitational field values being measured are the same as those influencing all objects on the surface of the earth. They are generally associated with the force which causes a 1 gm mass to be accelerated at 980 cm/sec². This force is normally referred to as a 1 g force.

Even though in many applications the gravitational field at the earth's surface is assumed to be constant, small but distinguishable differences in gravity occur from point to point. In a gravity survey, the variations are measured in terms of milligals. A milligal is equal to 0.001 cm/second² or 0.00000102 g. The differences in gravity are caused by geometrical effects, such as differences in elevation and latitude, and by lateral variations in density within the earth. The lateral density variations are a result of changes in geologic For measurements at the surface of the earth, the conditions. largest factor influencing the pull of gravity is the density of all materials between the center of the earth and the point of measurement.

To detect changes produced by differing geological conditions, it is necessary to detect differences in the gravitational field as small as a few milligals. To recognize changes due to

A1-2

geological conditions, the measurements are "corrected" to account for changes due to differences in elevation and latitude.

Given this background, the basic concept of the gravitational exploration method, the anomaly, can be introduced. If, instead of being an oblate spheroid characterized by complex density variations, the earth were made up of concentric, homogeneous shells, the gravitational field would be the same at all points on the surface of the earth. The complexities in the earth's shape and material distribution are the reason that the pull of gravity is not the same from place to place. A difference in gravity between two points which is not caused by the effects of known geometrical differences, such as in elevation, latitude, and surrounding terrain, is referred to as an "anomaly."

An anomaly reflects lateral differences in material densities. The gravitational attraction is smaller at a place underlain by relatively low density material than it is at a place underlain by a relatively high density material. The term "negative gravity anomaly" describes a situation in which the pull of gravity within a prescribed area is small compared to the area surrounding it. Low-density alluvial deposits in basins such as those in the Nevada-Utah region produce negative gravity anomalies in relation to the gravity values in the surrounding mountains which are formed by more dense rocks.

The objective of gravity exploration is to deduce the variations in geologic conditions that produce the gravity anomalies identified during a gravity survey.

A1.2 INSTRUMENTS

The sensing element of a LaCoste and Romberg gravimeter is a mass suspended by a zero-length spring. Deflections of the mass from a null position are proportional to changes in gravitational attraction. These instruments are sealed and compensated for atmospheric pressure changes. They are maintained at a constant temperature by an internal heater element and thermostat. The absolute value of gravity is not measured directly by a gravimeter. It measures relative values of gravity between one point and the next. Gravitational differences as small as 0.01 milligal can be measured.

A1.3 FIELD PROCEDURES

The gravimeter readings were calibrated in terms of absolute gravity by taking readings twice daily at nearby USGS gravity base stations. Gravimeter readings fluctuate because of small time-related deviations due to the effect of earth tides and instrument drift. Field readings were corrected to account for these deviations. The magnitude of the tidal correction was calculated using an equation suggested by Goguel (1954):

 $C = P + N\cos \phi (\cos \phi + \sin \phi) + S\cos \phi (\cos \phi - \sin \phi)$ where C is the tidal correction factor, P, N, and S are timerelated variables, and ϕ is the latitude of the observation point. Tables giving the values of P, N, and S are published annually by the European Association of Exploration Geophysicists.

The meter drift correction was based on readings taken at a designated base station at the start and end of each day. Any difference between these two readings after they were corrected for tidal effects was considered to have been the result of instrumental drift. It was assumed that this drift occurred at a uniform rate between the two readings. Corrections for drift were typically only a few hundredths of a milligal. Readings corrected for tidal effects and instrumental drift represented the observed gravity at each station. The observed gravity values represent the total gravitational pull of the entire earth at the measurement stations.

A1.4 DATA REDUCTION

Several corrections or reductions are made to the observed gravity to isolate the portion of the gravitational pull which is due to the crustal and near-surface materials. The gravity remaining after these reductions is called the "Rouguer Anomaly." Bouguer Anomaly values are the basis for geologic interpretation. To obtain the Bouguer Anomaly, the observed gravity is adjusted to the value it would have had if it had been measured at the geoid, a theoretically defined surface which approximates the surface of mean sea level. The difference between the "adjusted" observed gravity and the gravity at the geoid calculated for a theoretically homogeneous earth is the Bouguer Anomaly.

Al-4

Four separate reductions, to account for four geometrical effects, are made to the observed gravity at each station to arrive at its Bouquer Anomaly value.

a. <u>Free-Air Effect</u>: Gravitational attraction varies inversely as the square of the distance from the center of the earth. Thus corrections must be applied for elevation. Observed gravity levels are corrected for elevation using the normal vertical gradient of:

FA = -0.09406 mg/ft (-0.3086 milligals/meter) where FA is the free-air effect (the rate of change of gravity with distance from the center of the earth). The free-air correction is positive in sign since the correction is opposite the effect.

b. <u>Bouquer Effect</u>: Like the free-air effect, the Bouquer effect is a function of the elevation of the station, but it considers the influence of a slab of earth materials between the observation point on the surface of the earth and the corresponding point on the geoid (sea level). Normal practice, which is to assume that the density of the slab is 2.67 grams per cubic centimeter was followed in these studies. The Bouquer correction (B_c), which is opposite in sign to the free-air correction, was defined according to the following formula.

 $B_{c} = 0.01276$ (2.67) h_{f} (milligals per foot)

 $B_{C} = 0.04185$ (2.67) h_{m} (milligals per meter) where h_{f} is the height above sea level in feet and h_{m} is the height in meters.

c. Latitude Effect: Points at different latitudes will have different "gravities" for two reasons. The earth (and the geoid) is spheroidal, or flattened at the poles. Since points at higher latitudes are closer to the center of the earth than points near the equator, the gravity at the higher latitudes is larger. As the earth spins, the centrifugal acceleration causes a slight decrease in gravity. At the higher latitudes where the earth's radii are smaller, the centrifugal acceleration diminishes. The gravity formula for the Geodetic Reference System, 1967, gives the theoretical value of gravity at the geoid as a function of latitude. It is:

 $g = 978.0381 (1 + 0.0053204 \sin^2 \phi - 0.0000058 \sin^2 2\phi)$ gals where g is the theoretical acceleration of gravity and ϕ is the latitude in degrees. The positive term accounts for the spheroidal shape of the earth. The negative term adjusts for the centrifugal acceleration.

The previous two corrections (free air and Bouguer) have adjusted the observed gravity to the value it would have had at the geoid (sea level). The theoretical value at the geoid for the latitude of the station is then subtracted from the adjusted observed gravity. The remainder is called the Simple Bouguer Anomaly (SBA). Most of this gravity represents the effect of material beneath the station, but part of it may be .e to irregularities in terrain (upper part of the Bouguer slab) away from the station.

d. <u>Terrain Effect</u>: Topographic relief around the station has a negative effect on the gravitational force at the station. A nearby hill has upward gravitational pull and a nearby valley contributes less downward attraction than a nearby material would have. Therefore, the corrections are always positive. Corrections are made to the SBA when the terrain effects were 0.1 milligal or larger. Terrain corrected Bouguer values are called the Complete Bouguer Anomaly (CBA). When the CBA is obtained, the reduction of gravity at individual measurement points (stations) is complete.

A1.5 INTERPRETATION

The first step in interpretation is to separate the portion of the CBA that might be caused by the lightweight, basin-fill material overlying the heavier bedrock material which forms the surrounding mountains and presumably the basin floor. Since the valley-fill sediments are absent at the stations read in the mountains, the CBA values at these bedrock stations are used as the basis for constructing a regional field over the valley. A regional field is an estimation of the values the CBA would have had if the light weight sediments (the anomaly) had not been there.

The difference between the CBA and the regional field is called the "residual" field or residual anomaly. The residual field is the interpreter's estimation of the gravitational effect of the geologic anomaly. The zero value of the residual anomaly is not exactly at the rock outcrop line but at some

distance on the "rock" side of the contact. The reason for this is found in the explanation of the terrain effect. There is a component of gravitational attraction from material which is not directly beneath a point.

If the "regional" is well chosen, the magnitude of the residual anomaly is a function of the thickness of the anomalous (fill) material and the density contrast. The density contrast is the difference in density between the alluvial and bedrock material. If this contrast were known, an accurate calculation of the thickness could be made. In most cases, the densities are not well known and they also vary within the study area. In these cases, it is necessary to use typical densities for materials similar to those in the study area.

If the selected average density contrast is smaller than the actual density contrast, the computed depth to bedrock will be greater than the actual depth and vice-versa. The computed depth is inversely proportional to the density contrast. A ten percent error in density contrast produces a ten percent error in computed depth. An iterative computer program is used to calculate a subsurface model which will yield a gravitational field to match (approximately) the residual gravity anomaly.

ł

i.

APPEN

APPENDIX A2.0

ľ

LISTS OF GRAVITY DATA

ŝ

1

DRY LAKE VALLEY GRAVITY STATIONS

्त	STATIO	I LAT.	LONG. 0	ELEV.	TERTO	R. NORTH	FAST	()95V	THEC	r AA	¢5A
-	IDENT.	DEG MI	N DEG HIN	+CODE	TNZL	UT UTH	UTM	GRAV	GHAV		1000
<u>i</u>		*****	-								
- 191											
	DL1	+38 75	7+1145234	5377Y	0 I	27422193	08049	148289	200331	48502	00344
: 🛎	DL 2	+38 77	1+1145117	52251	0	107422204	68620	149345	200338	98179	83465
i 📕	013	+38 79	3+1145015	515911	n i	103422249	04966	149861	200370	07963	80490
	DL4	+38 83	3+1144907	515091	0	119422323	68493	149894	800428	07943	80493
	DL5	+38 80	8+1144852	5634Y	0	194422282	69206	147022	200391	09654	00-36
- 1 -	DL6	+38 80	7+1144744	5270R	0	111422284	69364	149231	200390	58522	80020
π	DL 7	+35 79	8+11:04630	5342B	Û	11422271	69530	144085	200377	98583	87477
	DL8	+38 75	1+11/4505	5548Y	Q .	111455189	69715	141521	200300	99454	80525
1	NL 9	+38 86	1+11:44550	56051	Ŭ .	115422301	69045	146910	200469	99757	80551
1	DLIO	+38 88	0+1140672	56000	0	112422421	09465	147333	200497	99540	86552
	DL11	+38 89	2+11/4/73	5584Y	0	111422440	69317	147360	200515	49394	80465
Ş	DL12	+38 89	9+1144698	52510	0	106422449	69135	149690	200525	98584	69780
•	DL13	+38 91	4+1144999	518601	e :	133422473	04440	149923	200547	98182	00627
	DL14	+38 86	9+1145118	53044	Ó.	110422386	nAn14	148775	200480	21282	00231
ţ	0615	+38 84	0+1145139	53650	e	119422344	08097	149051	200450	09280	81050
	PL10	+38 02	9+1145195	543RY	()	1554554694	08099	146265	200569	98673	50447
	0L17	+38 95	5+1145116	53541	0	12542245	02014	148625	500905	08496	63271
	DL18	+3- 93	9+1141934	5565Y	60	1255295551	59080	147274	500284	وكروه	80423
ł	DL19	+ 38 96	n+114457/	5409Y	i)	94455222	09651	144317	500053	99105	d0~00
-	DL20	+38 94	4+1144069	50261	0	131455240	09-67	145931	200591	1(0172	50430
	DL21	+38 93	6+1144558	5934Y	n .	175422547	44454	145199	200594	100454	80390
•	5510	+38 99	1+1144572	58478	n	119422030	04507	145911	500559	166281	80457
	DL23	+38102	4+11411058	56284	0	97422688	0.8460	147027	200708	99287	20149
	nL24	+30101	3+1144/52	54494	1)	124422065	59343	148410	200691	99001	20544
	0125	+38103	4+1144876	5632Y	47	112422099	69101	146677	200725	99159	40108
	0126	+ 38100	5+114/1982	52251	6	129422038	69007	144/52	200077	96593	80557
	0127	+ 55101	1+)145178	24244	0	123422040	<u>68/94</u>	1403//	200084	98735	80555
	0120	+ 38 101	2+1115223	20001 64004	U I	157422047	- <u>56075</u>	14/012	201010	44937	00745
	1/L 30	+ 38110	4+1145069	- 13 44 49 Y	() . 	<i>ب</i> م م ۲ ۵ ۷ ۲ ۲ ۲ ۲	00076	140335	200025	6347 <u>8</u>	300
		+ 20107	0+1144957	56111	(° .	してのなくそうりじ	04/14/	147015	219092 2397	07019	70000
		* 10 107	4+1144182	110000 110000	0	しょうくさしして	- 54 36 D	1 + 0 + 0 1	200101	20112	
	101 30	- 78107	941149972	57941	0.1	1111422199	- C 7 7 7 C 	141630	2007849	1-017	9070
	DL 34	- <u>7 2 C L U /</u>	9+1144970 5+1445100	51.1	0	123422143		147510	100105	06130	64746
	DI 48	- 700 0 - 174 A	371145189 341145081	51630		1 2 4 2 4 2 4 2 2 2	- 22016 - 22016	1/9426	100207	00185	01/07 01-01
	01 39	47H 7	1411/23084	50200		113460760		1 50 7 77, J 1 50 1 800 ()	100212	04610	61270 61706
	DL 40	+ 7 9 6	3+1125833	53430	., .	21420094	58973	150501	109302	29559	31543
	DL 41	+ 211 5	5+1145000	50000	0	10420084	69113	150512	199296	03277	51334
	11-42	+38 4	6+11.1/1980	49020	c 1	LT 342 1068	09052	150000	199277	98205	61175
	DL43	+33 3	8+1190954	49220	0	108420054	F9090	151582	149205	40030	41450
	D1.44	+31 3	0+1144928	49254	0	05420846	09120	151714	129253	94-10	62117
	01.45	+38 2	1+1101402	44525	(i 1	10442 1425	69167	152012	149240	4.2446	02055
	0146	+ 38 1	3+1144870	48485	6 1	11420811	59500	151097	199628	63293	51.004
	DL.47	+ 38	4+1104650	48425	(i 1	103420795	09244	151047	199216	94040	01573
	DL4H	+3h 6	3+11/14883	HAT BY	0 1	104420403	n9193	151345	199302	92410	51593
	DL 49	+38 12	5+1144937	44450	()	98461016	59111	151245	199396	99502	H1744
	01.50	+38 13	4+1165022	51341	n	00421024	ne912	150000	199405	24400	*1540
	0651	+38 16	9+1145104	51424	0.1	13421891	NANEA	150.59	149.50	e que 5	8-1-17-
	nu 52	15 85+	1+11-5220	52570	• •	10421165	n et a et (1	147577	149510	44534	81723
	DL 53	+36 20	5+1145198	2540	1 A 1	115421155	ed126	149825	149504	99229	01010
	rus 4	+39 50	3+1105168	5203¥	ē 1	19421152	68170	150000	140500	995+6	11415
	DLSS	+38 21	5+1165141	5178-	C]	100421175	57864	150344	199523	99552	51497
	0150	+34 21	9+1145114	51476	0	121421184	n 3040	150510	199530	99419	01935
	D1.57	+34 25	5+1105-68	51220	0]	175761100	n 8 n 8 n	150000	103234	99512	41035
	N 1 1 1	1.4 1. 1.1.2		1.001	•	A	1)) ¹	the Alexand	1.00.2.07	1848 A. 198	

5

Ş.

Ł

i

FI 115.

1 7 %

Contraction of section of the sectio

DRY LAKE VALLEY GRAVITY STATIC 'S

STATION LAT. LONG. ELEV. TER-COR. MORTH EAST DRSV THE 020 204 IDENT, DEG MIN DEG MIN +CODE INJUUT UTH UTH GRAV GRAV +1103 ----------0L59 +38 237+1145034 50728 98421220 68964150581199556 98758 81556 G DLOO 243+1145007 50508 + 38 α 95421232 6900415004n199565 99607 c147c 0L61 +38 249+1144979 50260 0 96421244 69044150676109573 99403 81355 DLo2 +38 257+1144942 50024 92421260 69098150725199585 43214 61245 Û. DL63 +38 195+1145003 50508 100421143 69012150607109495 96636 01514 £. DL64 +38 214+11/4897 49574 93421182 69166151136199523 98264 61450 ι 0665 +38 166+1104857 49124 99421094 69220151595199452 98370 61715 6 DL66 +38 113+1144796 48658 99420998 09318151073149375 97070 01100 0 DLo7 + 38 23+1104790 48463 95420833 69345150793199243 97155 80723 Θ DL68 +3897420010 04504150257194223 46527 00137 9+1144672 46348 G **NL69** + 30 90+1144719 48658 97420959 69432150340199341 96783 80287 11 0670 +38 1+114/1558 48235 0 107420000 69071150326199211 96504 0111 DL.71 +38 21+1144567 48288 110420636 69057150394199240 90590 80235 0 DL72 +38 42+1144577 433-5 106423475 6964215-14149271 90000 80200 0 DL73 + 38 62+1100587 48425 103420411 09020100450149300 40721 00010 Û. 9L74 +38 83+1144597 48478 104421950 09010150405199330 90747 00319 <u>ر</u>، DL75 +38 103+1144607 48555 101420947 695951-0-22149366 96752 61297 0 DL76 +38 124+1144617 48673 107421025 09579130536149391 957-9 00250 e l DL77 +38 144+1144628 48785 0 100421662 04562156243199420 9673 02194 NL78 +38 163+11/146/13 48875 0 101461600 0954015 104149444 40708 5114. UL79 +38 181+1144657 48978 192421129 09910190110100474 90720 00127 0 0610 + 38 S00+1144672 4904S 99421164 0940015 JON1495 2 407- 00120 C DL81 +38 219+1144080 49110 0 95421196 094741501 4194530 00/41 00150 DL.82 +38 237+1144765 49225 90421231 0444015)1--194550 90914 00227 0 DL83 +38 256+1144719 49308 96421206 69424150166199564 97 01 60262 0 0L84 +38 275+1144732 49378 94421500 6940415 210179612 9700 0 51515 DLAS +38 294+1140707 49455 95421335 093821362-0192034 97157 -1300 0 DLH6 +38 51 5+ 11 44760 49575 45451370 6436612625-4144667 47243 66476 0 0187 +38 334+1144771 490ns 90421408 043401503501496640 07307 NORAD 0 DL88 +38 355+1144782 49721 91421447 69321136421199729 97440 00013 U. PL89 +38 330+1144621 4968Y 90421399 69272150528199592 975.9 66795 0 0190 +38 315+1144845 49665 91421370 0923015 195149070 4777- 60423 0 DL91 +38 20141101477 49580 1421334 04101191 - 10400 04 20 ALTA ()01.92 +38 284+1140900 49728 92421311 691501510 64199525 962.1 0.555 U 0193 30800 S201114/1922 4980C 93421284 69127150004199664 98212 81239 Ω DL94 +38 174+1144758 49615 С 94421113 09371150050199466 97317 donog DL 95 +38 251+1100814 49375 94421253 0928015-740199517 97582 60031 ŋ. DL 96 93+1140521 48448 +38 0 114420971 09721154516199345 96757 81549 0197 +38 164+1144525 48594 0 115421102 00712150452199449 96624 60333 DL9d +38 239+1144594 49004 0 104421239 09600156293199559 MODIA ACCIA DL 99 +38 308+1100057 49354 0 102421364 59513150646199666 96032 80102 DL100 +38 349+1144561 49780 0 113421443 59651119666199720 96936 80122 +38 365+1144756 49528 DL101 97021466 69365154.48149745 97368 86515 ()01102 +35 374+1141730 49718 9-421483 07403140174144768 47244 - - - Kin .1 0L103 +38 385+1144702 49671 9842150% 04444120295199/13 97308 40225 O. 0L104 +38 396+11/40A2 49705 0 101421526 69472150020199780 97013 8010K 0L105 +38 40-+1114-61 49424 100421545 69503149944199403 47026 40144 ()+38 414+1144035 49948 06106 106421570 69540149821109822 96007 00070 n DL107 +38 432+114/011 50095 104421595 69574149711199841 97010 00034 0 DL10A +38 445+1144584 56238 104421020 090131490 14199000 47110 10943 0 06109 + 30 455+1144558 50370 0 113421039 090511.9540149975 97089 01 26 DLIIO +38 407+1114532 50050 0 110421002 49080147497149692 97262 40044 CL111 +35 491+114/504 50920 1234210H9 69129149464199913 91473 00220 • 1 **UL115** +38 379+1144/02 49923 91421491 59312156485147764 97017 86706 0 DLIII +35 394+114813 49885 22421514 69281150570199786 97726 HOHOS () **DL11** +35 413+1144830 50003 9:421552 69255150009149813 97 400 80021 0

O.A.

A2-2

.

TANKS A CONTRACT OF A COMPANY AND A STREET OF

DRY LAKE VALLEY GRAVITY STATIONS

		_									
	STATION	LAT.	LONG. I	ELEV.	TFROM	OR, ADATE	FAST	UBSV	THEC	FLA	(HA
	IDENT.	DEG MIN	DEG MIN	+CODE	INA	OUT HTH	0114	GRAV	GRAV		+1000
1											
	DL116	+38 448	+1144664	50205	0	91421016	69204	150015	199865	97992	50608
	DL117	+38 468	+11/1/070	50275	0	94421652	69185	150481	199894	97896	80845
	Ditta	+ 38 // 8H	+1 (<i>и</i> //На Z	50210	, U	03421680	49175	1 1 1 1 2 1 2 1	109337	07770	40045
1		179 610	*11400A3	- 101133 - 50110		9242 (009	- 07174	1 3 V 6 M 6	199923	91129	
?	06119	+30 510	+1144043	- 20413) U	90421129	09139	150142	144422	97028	01564
	UL120	+ 58 528	+1144911	50515	0	90421762	69132	150049	199952	97502	50457
_	01151	+38 548	+1144918	20003	0	91421799	69151	149979	500011	97588	2414
	DL125	+38 568	+1144932	50038	0	95421835	69099	149920	500040	97528	80354
	DL123	+38 586	+1144947	50755	0	92421668	69077	149651	200000	97540	66329
	DL124	+38 607	+1144957	5090S	0	92421907	69061	149870	200095	97576	00407
	DL 125	+38 629	+114/1962	51010	0	94421947	69053	149922	200130	4779A	00494
	DL126	+38 700	+11/15232	53004	Ō	125422669	03055	149390	200234	99442	61091
1	DL 127	+18 676	41475174	51004	о 1	10-422028	68799	1149771	200105	981/11	RUNGA
	61136	120 675	1145134	- 51001 - 5302V		101422020			200190	00373	00040
ſ	DEIED	T 30 003	1145641	-22431	0	122451040	00040	100020	200041	97612	01314
•	01129	+ 55 601	+1145151	- 51/0Y	0	103421689	64778	150005	200088	92035	01104
1	UL130	+ 58 537	+1145160	51744	- 0	150451110	63/50	120427	194445	98948	01461
	DL131	+38 473	+1145212	527AY	C	116421050	66594	149963	1999995	99504	01779
1	DL132	+38 504	+1145112	5124Y	0	133421711	68839	150577	199947	95853	91208
i i	0L133	+36 443	+1145141	5732Y	ί ()	242421597	08199	146975	199857	101065	81757
	DL134	+36 415	+1145212	5297Y	0	120421543	03695	149921	199810	92956	62039
	DL135	+38 342	+1145223	52489	0	125421407	5356	150105	199729	99845	82072
i i	PL136	+38 263	+11/15191	51651	0	124421262	58734	150350	199594	49567	41444
	DI 137	+38 310	+1+45107	51200		125421352	68050	15:170	199663	66262	- n1954
	01139		+1+050+8	Solar		101/121 297	 	150110	10068/	776 E	- K 1 2 2 4
	01120	1 30 3C 3	-1105010	10760		101451903		151.170	197009	- 4600L	-1270
		T 30 370	+1144410	- 47070 - 6 - 9 - 9 - 9 - 9 - 9 - 9 - 9 - 9 - 9	· · · · ·	93421433	04141	1011000	199721	96631	01341
	01140	+38 420	+1144945	20081	(r	97421261	64040	151205	144852	46511	01541
	06141	+ 58 444	+1145021	50520	0	112421503	n49/4	151110	199859	98507	01555
	06142	+38 495	+1144956	50375	6	97421599	69067	150666	199934	96136	61053
	DL143	+38 531	+1145026	50705	(i	98421764	68963	150334	199986	98062	c)chn
	DL144	+38 619	+1145034	50870	0	106451956	08945	150251	200115	93010	00700
	DL145	+38 716	+1+45057	51401T	0	105422105	68910	149637	200257	97953	80527
i	DL146	+38 685	+1105003	51134	0	102422049	68990	150026	212965	97934	80597
i i	01147	+ 38 738	+1100907	51914	Ő	91/122151	69126	149720	200249	08251	60673
	DI tag	+18 575	+1144012	50545	ň	01424865		149741	200051	07261	50134
	01150	1 10 JV J	- 1 - 1 - 1 - 7 - 9 - 1 - 1 - 1 - 7 - 9	SATES		07021700	-01/1	1.0750	100027		- 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10
	DITET		1144707		U o		07241	149730	199972	41.045	760623
1		+ 30 445.	+1144720	44435	0	9/421015	69415	194661	144960	96730	79.197
	01152	+ 38 - 51 /-	+114/064	50576	C.	98421750	09495	149577	144460	97003	19:155
	DL153	+ 38 597	+1144705	50926	0	101421497	69434	149325	590683	97164	70407
1	DL154	+38 075	+11440751	51201T	C.	105455045	69470	149510	200107	91185	30197
	DL155	+ 33 735	+1104063	52424	G	104455123	09400	149172	590594	94277	1.1745
	DL156	+38 721	+1144766	51714	0	104455154	69344	149720	200264	98121	80590
	0L157	+38 058	+1100793	511511	0	9-422407	09313	149705	200172	91074	30520
	DL158	+34 692	+1144561	525291	Ð	104422078	69630	149314	200222	94541	00125
	DL159	+38 605	+1100592	51675	é	101421917	69595	149145	250096	91727	60204
	DLIDO	+ 35 526	+11/1553	51190	, ti	106421771	- 9655	1.19.652	149979	97511	
	DLIDI	+ 37/15/02	+1112002	55 175		1 7 / 1 4 1 5 0	71.10	140507	107022	101-492	1.2727
	01167	- 17/167 (c)	• 1 1 4 30 7 E.	57555		13/414014	- 1 (0 1 0 - 1		107177		
			11141720		· · · ·	160414271	- 10750 - 11. az	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1 77167	101099	- 07474
		13/401/		54771		149418273	71403	140747		1)12/4	
	01106	+ 5/46/4	+11/14074	- 74 L A Y	Ċ,	164418387	71920	14//20	197680	101404	43-144
	01167	+ 5/4077	+1123571	- <u></u>	C	125418265	71179	140 194	197277	101125	r 2 5 4 1
	DL158	+374065	+ 1 1 4 3 4 4 5	57503	C	105418370	/13nu	1-1-21-1	197250	102377	25930
	DL 1 59	+374593	+1143417	00715	C	220412232	71469	143454	12/150	103443	62401
	DL170	+ 374517	+11/17/4 30	59628	1.5	170410490	713:5	143754	147(44	102024	-2010
	CL171	+ 374740	+11/13458	57448	0	154418508	11342	145404	197369	102533	1.29.12
	DL172	+ 374745	+1103518	57224	n	141418515	7125	145725	197570	102205	
	01174	+ 374742	+11/13562	5-415	Δ	144012441	71187	1450 81	1974 40	101491	6241A
-	01176	+174786	++++++2276	5 5 1 7 5	••	176/110000	71504	147.00	197226	• • • • • • • •	12.11
	01170		- L + 4 36 7 3 - L + 4 36 7 3	- 2 10 10 - 2 6 - 3 6		- * * * * * * * * * * * * * * * * * * *	- 1000 - 11.11.	- 1 - 1 - 1 - 7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	4 7 F M 10 4 7 9 1 1 1	1 (1) (4) (4) 4 (1) (4) (4)	
_											

A2-3

/***

FN-TR-33-DL DRY LAKE VALLEY GRAVITY STATIC'S

1

1

•

ł

IN THE A

1 1 3 March 1 4 4 5

1.1 4.1 1.1 2

STATION LAT. LONG. ELEV. TER-DOR. NORTH FAST OBSV 7 HE C C++-2 1 2 4 IDENT. DEG MIN DEG MIN +CODE YN/OUT UTN HIM GRAV GRAV +1000 DL179 +374819+1143351 56578 0 193418556 71495146298197484102055 62953 0L180 +374823+1143422 57038 0 178418663 71391145024197490102370 02042 DL181 +374880+1143174 54338 184418778 71752146531197573100090 81743 0 DL182 +374901+1143356 59184 0 235418809 71484144706197604102797 82544 DL183 211418801 71308144286197601102657 02535 +374899+1143476 59474 0 DL184 134418725 71160144955197544102290 02537 +374860+1143578 5831Y (:0 284418882 71580145474197559102284 82325 DL187 +374939+1143289 57874 DL190 0 200418955 71233142848197723103728 02776 +374983+1143524 02288 DL191 +375013+1143040 60075 0 259419006 71053144002197767103336 82902 DL193 +375062+1143555 64738 346419100 71184141449197639104535 82838 34 DL199 +375099+1143712 5904Y 0 297419162 70952145118197893102792 82952 01200 +375114+11/3734 58274 n 297419189 70919145046197915102572 82995 DF505 +375214+1143616 65135 0 504419378 71087141131198001104372 02002 01205 +38 9+1144375 48305 0 127420821 69939150244199223 96477 80130 DL206 +38 48+11/14470 48305 - 0 117420390 69793150415199280 96591 80234 DL207 0 144420948 69928150545199323 96812 80435 +38 78+1100380464421 DL208 +38 123+1144454 48618 0 128421029 69610150413199389 96770 60310 DL209 137420967 70065150266199335 97423 8071: +38 86+1104286 49400 0 01210 41+1140177 5160Y 152420887 70227149986199270 98713 81470 +380 19+1143951 55024 229420855 70559146621199238 99919 81109 DL211 +38 0 433420931 70787142032199293102797 01756 0L212 + 38 57+1143794 62968 0 06213 +38 90+1123900 5758Y 275420988 70030145509199341100360 00990 0 DL214 +38 108+1144005 54454 0 207421017 70476147018199367 99495 81131 81+1104000 52494 0 177420964 70352148954199328 99025 61299 DL215 + 38 0L216 +3881+1144200 50751 155420960 70192150049199328 98482 61328 0 +38 140+1103027 01504 0L218 414421098 70734143127199426101583 61022 0 DL219 +38 150+1143918 57348 n 262421098 7000114505019942910-193 60498 005200 +38 169+1144090 53708 (1)186421127 70340148590199450 99072 01542 212421123 70187150227199450 98750 81575 155.10 +36 169+1144200 50984 0 01555 170421115 20027150010199454 97097 80519 +38 167+1144310 43014 C. 0 133421122 69912150104199461 95094 80159 DL223 +38 172+1144388488711 DL225 +38 199+1144460 49050 117421169 69506157029199501 95689 00077 0 120421284 696911 49970109506 96936 80196 **DFSS9** +38 260+1144305494591 11 119421318 09747149050199017 96805 80051 0L227 +38 279+1144408 49470 C. DF558 185421246 70078150050199550 97875 01107 +38 237+1144273 49717 U DF550 +38 218+1144127 58364 275421216 70292145598199528100995 81365 6 DL230 +38 199+11440+8550201 199421185 70452147064199501 99945 81373 0 DL231 +38 213+1143436 57568 237421214 705721456241995211 10220 40005 () DL232 +38 240+1103067 00086 0 292421267 7007114414214450010101168 30304 DL 234 0 240421380 70032144493197051101080 00945 +38 302+1143002 59701 PL235 +38 289+110000 56004 2 187421352 70475146609139532100446 81330 DL236 +38 273+1144074 57154 0 163421320 70307140575199079177754 91425 DL237 +38 276+1104181 5655Y 0 327421322 JC210146460199013103509 dtnod DL238 +38 297+110/306 5024Y 0 1-7421556 70027150370199044 9-018 81:39 DL 234 0 131421452 69082149854199725 97552 00367 +38 351+1144403502001 DL240 +38 399+1144475 50550 0 111421539 69775149537149793 47317 5014/ 01.241 +38 444+1140410510101 130031024 0966410770199659 97913 00911 0 01242 +38 416+114/307 54514 175421576 70020144366149518 49064 41452 η DL243 +3N 350+114/242 5453Y 193421456 70110140574149721 49973 41561 C. DL 244 +38 345+114/159 02164 108421450 702391433511997141 32120 01547 \cdot PL245 4 3 8 340+1142755 58260 è. 104421448 70541145920144700101 45 41508 DEPAN + 36 150421494 7043714631514974516 322 01152 360+1144023 57331 n. 01247 + 38 - 377+11040R1 - 5849Y 103421512 703521453541497611 11922 81190 0 DL24H +34 420+1144123 55040 142421540 10289141464141625 09951 01124 9 DL 249 +38 355+1142855 01144 253421480 70004143047149724101562 00462 0 01251 +34 407+1132967 58526 0 173421574 70517144972149800100272 00.01

1 / 1 1 **3 / 1** 1 / 1

Induced adamatic to the original

DRY LAKE VALLEY GRAVITY STATIOLS

STATION LAT. 822 LUNG. ELEV. TEP-COR. NORTH EAST **JPSV** Trif 0.00 IDENT, DEG MIN DEG MIN +CODE TA/OUT UTM UTM GRAV GRAV +1000 06253 +38 412+1144195 60554 0 345421573 70184144000199812101176 80869 DL254 +38 475+1144152 54650 0 14-421091 70244147024199904 99353 80859 DL255 +38 497+1144228 54544 0 122421729 70132148358149937 99751 01271 DL256 +38 491+1144335 55014 0 129421714 09978148152199927100004 81363 0 305421086 70773142023194890102775 31105 DL257 +38 465+1143790 64434 DL258 208421650 70613143952199865101028 80601 +38 448+1143900 6050Y Û. 01259 0 173421684 70503144932199894100143 00346 +38 468+1143975 5855Y 17 217421/75 70047143565199963101063 60650 DF560 +38 515+1143875 61698 538+1140004 5748Y 154421813 70457145595199996 99696 60245 DL.261 +38 0 138421777 70350146721199970 99351 80427 01265 +38 520+1144074 55894 0 DL263 0 133421745 70250147021199980 99049 80550 +38 531+1120102 54634 DL265 +38 582+1143844 03431 0 281421900 70689142445200061102087 80734 DL266 +38 575+1143929 5856Y 0 187421984 70565145167200051100231 80445 DL 269 +38 665+1143923 58924 0 174422047 70570144449200179 99723 19801 DF520 0 184422193 70/11144042200292100938 00030 +38 740+11:3524599111 17510 +38 730+1143918562811 0 150422171 70574145069200277 49642 74915 DL272 +38 692+1144026 5604Y 0 141422097 70410140050200222 98576 70003 DL273 +38 004+1113990500601 0 149422006 704721-5723200180 98666 79642 DE274 +38 627+114406255600T 0 135421975 70500146718200127 08921 00692 DL275 +38 593+1144025 56281 0 145421914 70424146315244077 99204 90154 DL276 +38 711+1144121 56221 0 121422123 70276146583200244 99614 80196 DL278 6 129421925 70204147917200096 98703 80394 +38 602+1144175540021 DF595 0 136421851 70061149553200034 99295 01395 +38 564+1144274528401 20 124421444 69941149759200031 99207 61413 DL285 +38 562+1144350 52588 +38 546+1144388 52218 DL286 153421014 699041499032000000 99110 81456 Û. 01287 +38 531+1144405 51708 0 128421785 69671150932149486 98692 01310 01238 0 122421756 69026149722199964 94329 30446 +38 510+1144435 51019 DL269 +38 504+1144458 51408 0 116421733 69795149013199947 98040 60625 +38 492+1144482 51166 0 115421710 69760149465199929 97683 80350 01290 01291 0 130421837 697971-9962200029 98599 81100 +38 560+114/455 51718 0L292 +38 613+1100291 56024 0 113421941 700341470-7200106 99666 60670 DL293 +38 628+1144381 5736Y 94 140421966 69902146579200122100435 81111 DE294 +38 623+1144491 52500 121421952 69741149622200121 95914 51129 0 DL295 +38 705+11/4433539301 124422108 040261-8545200241 44110 8034) ()DL296 +38 710+1144326552301 0 130422110 69987147485200248 99216 60504 DL297 +38 587+1144237550001 155455080 10110147556500514 98806 80110 1 01298 +373818+11104437 56938 157 269416767 69946144533196024192089 63089 DL299 +373793+1124314 58458 81 262416725 7012*143465195986122449 62696 DL 300 +373808+1144180 01475 100 355410757 7031014109414000+104740 05235 DL301 +373802+1144078 52298 252416750 70+75141-55190001104081 03087 0 DL 362 +373778+11/3971 59054 171415709 70035145122195966102732 82753 \mathbf{C} +373781+1143849 59235 DL 303 100410719 70013143241195970103057 03021 0 01 304 +373018+1143790 58745 0 164416790 70220145155196024102413 02542 PL 305 +373904+1143789 58255 0 15:41,949 700951+51141961 101756 62176 DL 304 +373449+1143900 50201 6 164414043 707311-3516196070103251 -33193 06307 + 57 3846+1143978 60728 0 199410035 71020142357195065103421 42401 DL 508 +373838+1144259 57673 0 204416010 702071446/3196053102332 43071 DL. 309 +373888+1144422 59288 0 775415897 59965142045196127102526 43163 0L310 +373069+1144343 56188 4 292416864 70082145546146694192120 B3250 +373921+1144359 31804 0L311 - ING4169NO 73-501485-7196174100923 STATE nL 312 + 57 3959+1144404 50701 0 155417928 6998214007719823,1093-3 63226 DL 313 +373482+1144512 52628 0 159417074 70122146157196263100851 5305: + 37 391++ 1144264 35948 DL 314 210416954 7019014540419010/101430 65100 1) DL 315 +373900+1144190 58905 285416427 70300143554190144102845 03.41 0 DL316 +373884+1144077 05985 0 570416902 70472138791190120104772 82834 DL 317 + 37 391 /+ 11 4401 5 59045 01031116965 70562136527461661 5337 62 21 01.31.9 チネブスロンフチナトリッズルロン いのいてい N. TO PATERARD THIT BATH DATA AND LEADED AND A STORE

and the second se

į

5

1

÷

PRY LAKE VALLEY GRAVITY STATICHS

STATICI IDENT.	N LAT, LUNG DEG MIN DEG M	. ELEV. IN +COPE	TFR-I	CR. WORTH	EAST	ORSV GRAV	T-EC GRAV	- 42	084 F1000
01 710		7 57449		1	- 70070	1	10:3641		84640
01230	- 73/390471145/	H3 37441	() (*	14141765	6 70930 E 70807	142170	1952551	0.04400	01310
06320	+ 574000+11440	40 20030		14441718		1431/5	1982901	01402	01040
01321	+379020+11459	50 29073 74 50078	11	10(41/10	6 79640 6 79671	101640	1402141	02201	05311
01.322	- + 37 399 3+11110 - + 77704 3+14 ////0	34 02010	0	28341710	5 70521 6 7017.	141308	1902001	53127 001202	92041
0L 32 3	+ 37 3962+11041	01 03(00		5441704	5 70324	140316	1902341	04305	02344
01 324	+ 3/ 3994+11441	80 53523	174	34141710	1 /0304	134407	962001	0.2445	02042
01.323	+ 374056+11003	40 24160	0	25141717	1 64440	140202	1903071		02433
01326	+ 3/4059+11442	10 5C/AY	0	17241721	ターイヤとしろ	147709	1963/51	01086	05200
01327	+ 574970+11441	50 mbolia	U	22341765	7 76346	143631	1404021	02105	-03466
04360	+379030+11440	40 01300	0	19341710	1 10402	141744	1403431	03109	02027
06329	+ 374071+11450	44 57963	0	15541727	6 /0000 • 70.070	143311	1903931	01466	01745
0530	+ 5/4102+11439	50 2001Y	0	14241721	0 70079	143467	1904301	01506	61722
01232	+ 374100+11447	55 51650	0	12941745		1 44 3 32	1402211	01002	02204
04322	+3/4150+11458	80 57765	0	15441745	6 70737	143704	1903521	01027	91404
DL 333	+ 574110+11440	73 60265	- 0	29341732	0 70468	146215	1964501	02119	652714
106.554	+ 5/4114+11442	53 32210	0	15041732	1 /0203	146162	1994551	00005	03295
06335	+374095+11443	59 33508	0	45141724	2 /0048	142241	1964201	01472	85445
UL 536	+5/4169+11444	43 4//49	0	12141741	व २५४४४४	144628	190550	98221	02002
116357	+ 574176+11444	71 48008	0	12141742	7 69286	1499992	196546	90527	Beelo
01.338	+ 5/4155+11444	47 4×40¥	0	12241740	8 644J£	149925	196530	99000	02512
01.539	+ 3/4156+11444	25 42444	6	13441759	5 04423	1444(4	19517	99487	02415
0L 340	+ 3/414/+ 1 443	07 4942Y	Ú.	15441757	6 64440	149144	196504	44750	03020
DL 341	+ 1/415/+11445	74 49651	0	1 3941 / 35	9 70024	100005	146464	99917	83034
06342	+5/4152+11445	45 50358	0	15841705	1 70007	149644	1964521	00147	0 1) [2
DL 34 3	+ 3/4181+11442	78 51385	0	1 3841744	4 70165	148012	1965531	00613	05221
NE 544	+3/4154+11441	51 5 SHAY	il	15841739	8 /032/	14/154	1965141	01548	85159
104.545	+3/4202+11441	20 55511	0	17841748	8 70585	146605	1965841	01065	n 51 1 0
01.346	+3/4180+11040	53 61038	e e	39541745	0 70494	141030	1903561	.Velel	02306
01347	+ 5/41/2+11459	99 58595	0	17241745	/ /05/4	143243	1965411	02178	02204
01 548	+ 574242+11457	98 5754Y	()	15141727	4 / 1000	144635	1966421	01885	72550
01.349	+ 574242+11455	20100	C	15241757	0 19724	144316	1966421	01614	022/1
01.330	+ 5/4256+11244	32 45925	· (·	13541757	/ 09934	128675	190003	98782	07337
116.571	+ 5/42 5/ + 1 1 44 5	76 44548	()	141754	4 70017	1 1 9 7 7 9	190032	99814	83041
012552	+ 374228+11042	17 0000	. 0	24741755	5 74251	140705	1900221	02138	0115
06303	+ 1/4203+11/462	24 01143	()	77. 41700	1 / 4629	146771	1900/01	07077	02021
06350	- 7 37 4203711441	10 00 YOU	() 5 0	73641700	4 70365	1000000	1400101	02463	- 020/7 - 47634
01.355	- + 374231+11040	n3 00010	79	- 6 5 441 / 20	1 7.1470	() 47,074	13000001	1.2030 	- 020C4
DE 1567	- + - / + 2 30 + 1 1 4 3 7	71 57085		1-441757	2 10512	1.0.1.2 A	1967261	112 JE /	- 61 2 - 61 - 61
DI 358		36 57/05	0	1/16/21750	2 70322	164566	19672 91	-91 (9e) -621 (a)	25-44 25-44
01 459	-+ 37/4 481+11/127	20 J1100 29 Se955	C C	1 2 1 / 1 7 8 2	5 70917	145-67	1966451	02114	
DL 350	+374473+11427	79 54561		126418(0	2 10583	146501	1969791	10/50	12251
DL 361	+ 374441+11 136	82 54314	0	13/141791	1 20307	Junnin	1006221	35.817	19221
DL 302	+ 374370+11439	19 56733	0	13841786	7 10-097	144991	1900291	01554	1.2 44 4
01.363	+ 37445++1++29	55 56615	0	13941740	1 10025	140050	1059571	لر 1 م لرن	53.43
DL 304	+374415+11/34	44 55055		12541788	7 71585	1401.60	1950951	01 4 A A	02024
DL 365	+ 77 1 325+110 39	72 57005	, a	13841772	1 70507	1 449 47	1967031	01819	02510
DL 30A	+374 425+11440	A1 59905	7 .	27241711	a 70476	142000	1967631	1.2494	52 479
PL 367	+ 374370+11040	54 57453	د ۲	22941750	9 70484	144502	1900351	0.22.42	0217+
DL 36H	+ \$74442+11000	10 24375		15241743	t 70015	147172	1469341	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	
DL 3ng	+37409++11941	31 99003	e	50141400	2 7 . 36 .	143191	1970051	12310	-25.0m
DL 370	+374401+11441	70 52194	r.	15041755	4 10312	140017	1900741	30640	131 14
DL 571	+ 374 57 5+ 11 11 1	65 01105		574417/1	0 70514	142200	1907601	0304	APRIN
DL 372	+ 374 324+11442	57 52183	r.	15741770	8 701/3	145451	1407001	00101	3. 90
AL 371	+ 374284+11443	14 54795	154	61441764	> 10096	141464	1957111	1.5.15	02020
01375	+374345+11404	R4 47/11	(1 12 11774	2 09.994	15044.	190142	ц. ц. Ц.н. (43-р.	~ > < ~ ~ ~
N 1 1 1					•				•

Section Section 15

EN-TR-33-DL CRY LAKE VALLEY GRAVITY STATIONS

1

STATION	S LAT.	LUNG. F	HEV.	TER-r	nR. N	MARTH	FAST	NHSV	THEC	F A A	C 34
IDENT.	DEG MIN	DEG MIN	+CODE	1.1	nut	UTN	HIS	I,DAV	GRAV		+ 010
DI 376	17/17/1CJ	1140007	26005	0	110/11	77:0	60870	150050	106792	07212	81620
	+ 374 34 34 34	1144447	40040	U	11641	11134		1 200 20	196792	61.12	
01376	· · · · · · · · · · · · · · · · · · ·	114440	- 40 210	0	10941	してつてい	70.60	12/27/0	104037	00477	- 5 - 7 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 -
01374	+ 3/44 3/4	-1144341 	-47270 - 65.000	2	12941		10037	「コリココの	100000	99366	677-1
01300	+ 5744804	1144255	55005	0	28641		70144	140404	140440	101238	07100
UL 581	+3/44014	1144254	50254	0	16801	17051	70101	149640	196074	109106	83:35
DL 384	+3737634	-1143716	5700\$	Ü	15541	16671	71009	145532	195944	101084	81/95
DL 385	+373871+	1143654	57285	G	16141	0093	71095	142004	196102	100165	61327
DL 386	+374002+	1143035	5661Y	0	13241	17134	11043	143440	196292	100011	61357
DL 387	+3740074	1143574	53558	0	15141	17148	71200	145924	19-300	100055	81414
DL 388	+3739664	1143488	52238	0	17641	7054	71335	146738	196231	9486t	95055
DL 389	+373904+	1143370	252203	0	13541	16965	71511	140291	196149	99851	8207h
DL 393	+3739844	1143357	54945	0	15641	17113	71527	145170	196266	100619	82036
DL 394	+374027+	1143428	55770	0	15541	17195	71420	144724	146359	106681	82014
DL 395	+ 37407 54	1143510	56420	0	15641	12225	11560	145390	196390	102094	83076
PL 396	+3741084	1143463	58433	. 0	18641	17339	71365	143598	195447	168143	85400
DL 397	+3740684	1143634	5500B	0	13441	17258	71115	144907	195388	100840	02010
DL 398	+3740834	1143735	57038	C	12841	1282	70965	143740	196410	101010	01057
0L 399	+3741494	1143681	56878	0	13541	7406	71612	199710	196507	10143e	H2174
DL400	+3741484	1143610	56678	n	14741	17407	71135	144575	146505	101400	9555F
DL401	+3742144	1143698	57075	0	13841	17526	71014	144746	196002	102419	02000
01.402	+3742074	1143729	57845	2	13541	7623	70456	144583	190079	102341	~2749
DL403	+374245+	1143020	56703	0	15941	17586	71127	144492	190047	103092	03256
DL404	+374230+	1143561	50555	12	19841	17572	71215	143647	190634	103402	62960
DL405	+3740954	1143373	58205	0	20441	17318	71498	143787	190428	102135	82480
DL411	+374157+	114329	58368	G	17941	17427	71205	143874	196519	102283	02557
06412	+ 3741914	1143032	58025	G	15541	7486	71112	144532	196550	112049	82435
DL413	+ 37 4 332 4	1117074	54838	Ċ	17441	7745	71937	144510	196773	163105	03214
DL414	+ 37 4 36 1 4	1143005	58535	ú	16141	17801	71144	144438	196816	102078	01050
DL415	+ 374410	+1143060	00398	Û	26441	17889	11049	143516	190880	1:3330	62997
DL416	+ 374446	11:13587	58388	0	1504	7959	71160	144437	196940	102443	025h7
01.417	+ 3744914	11/13409	58855	0	15341	18046	71294	143945	197005	102378	HEUNA
DL418	+3744024	1143521	0122S	ň	22541	17580	71265	146507	196876	1 3251	02540
01422	+ 37 3 1 2 9 4	1111435	50025	111	36641	6502	64253	14241-	195495	113014	03:19
DL 423	+373717	E1100107	58855		19541	10590	70377	145337	195877	102075	65401
DL 424	+ 37 3724	1100009	DUCHY	e	17901	6007	70521	142354	145088	103213	02-31
DL 425	+3752904	1105500	58293	c.	22741	100 X 4	00114	1:45236	198157	131934	82284
01 426	+ 3752574	11/15 405	54225	с. С.	17241	0 40 8	00009	147154	195123	100059	01730
01427	+375290	-11/2 (a)	00015	6	622/19	10468	55.095	1.2.2.15	198180	111569	41519
01/429	+ \$76 \$154	61 1 4 6 2 8 A	41139		1/13/1	10551	- 40 T -	1 10 7 25	198252	10120 / 2350 /	52292
DL 429	4 475 28/14	114-24	57128		20.01	13620	0.0010	145465	108419	101415	n2151
01.4.50			509.18		1	10065	0.0013	109955	104330	09575	
01.14	+ 175721	-114-290 -116293	58260	()	27.00	10514		147-15	106221	1-211	12.2
01.30	+ 275 443	-1113400 -1113400	- 10 200	۰۲ ۵	2. 211		na 15 2	100772	105306	1.1.21 8	
	+ 175 - 7		5000	0	11.0		- 00 2 °C	15:570	104245	0.054.00	43334
	- * 37 34 383 - * * 75 46 4 3	<u></u>	- 300 FT	.1	13491			1.197.51	100007	69.71	1.3341
01/145	+ 775 164		- 11 29 1 - 51 7 C V	4.	16194	10101	0.001.0	1.47701	1.55.4.1.7		
	+ 37 34 101 - 175 16 2		- 21/31	0	1 1 2 4 1	10703		147271	1.11.11.11.1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
01.430			- 11 - 11 - C. 15/15	0	1 4		- 55 A F	1.4.1.2.1.2		1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	- 17 - 4 C C - 14 - 14 - 14 - 14
01 11 20		T I T 45 27 U	- 36671 - 1. 36 7 4	• 1	1.1.1.1.1.1	j set:ti 4j. I rim + ⊐+	1000). 7	1911	177447	104667	- C (F 3 1 3) - M - C G (
146.9.20	+ 1 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	1145390	- 365/X - 6 300-	•)	اله، او مريد. مريد	19617	0 1 4 N N	147204	1.1.1.1.1.1.1.	1	10000
11 L 4 317 Ext. 2 - 11 A	- 7 31 747 / 1 - 1 275	* 1 * 1 * 4 ? 4 * 1 * - # - #	5744	· ·	1144	19019		1 14 17 1 19 M 1 1 1 1 1 1 1 1 1 1	1.11.11.11.11	1 (1-4/j) 1 (1-4/j)	36341
nLuun Ni sar	+ 3/ 34/6	きまちならはちらう	יייר ר	;	1404	19796	13 × 57 i	1400004	1 13444	1.001	1173 I
	- 〒 1 / つはや 19 		- 74 c 1 f	Û	1534	3634	111342	147147	197654	tud / tš.	06510
	+ 3/ 344)	* F T 15 30 5	54254	12	1441	14422	n# 509	140191	14444	1000/5	reses
11244X	* * / * 5 * / *	11/15/34-34	51424	• }	12541	19040	1,4547	150046	193505	47471	いとううち
01244 <u>4</u>	* 3/78/3.3.	1145.521	57455	Ċ	12340	CD 9 5 P	00571	لم 13 ما 14 ما 1 1 - 1 - 1 - 1	198025	100666	1.2.5.5
116 145	• • / ~ ~ ~ ~ ~ ~ ~ ~	1145411	37 (18	n.	12541	10492	n n 341	14/596	194595	1.11.14	
101 / 1 h	A 4 7 4 7 1 1 1	• • • • • • • • • • • •		<u>^</u>	1 4 1 1	N 11 1 1 1 1	A 10 A 11		***** * ****	1 1 1 1 1	• • •

ļ

Ì

STATTCH	LAT.	IUNG. E	1 F.V. T	rp=r(R. VIRTH	FAST +	nsv	1-1-1	F 4 4	- n 4
IDENT.	DEG MIN	DEG MIN	+CODE	TNZ	UT OTM	11.1.4	الأهد	GRAY	•	1 J.J.
							_ = =		* = = = _ =	****
				,		•••••	-			
DI 453	+ 375 31 2		41720	50	115/110500	n#7181		108204	100049	52611
01/15/1	+175305	* L 1 4 7 6 6 7	17951		100/00/75		5.1701.)	106170	0.00009	- CFOLL
		14 1 1 4 5 1 1 9 1 4 1 4 5 1 4 5 1 1 9	0877	0	109414475		5175	10.00176	00000	- 0 # 3 0 F.
01/154	- 7272302	11113344 1113344	- 40170	0	100414344	000411	51201	397675	0186.	6 - 4 - 4
	- T 372303	ST 1145029	47340	U A	42414443	040141	21309	190191	97636	01(20
01457	- + 37 7 50 U	1144420	4/205	0	87419583	091621	511.44	197259		01342
01450	+3/3296		40/30	0	20110420	041041	51404 S 6 6 6 7 9	195131	47534	01430
01459	+ 2/ 2 51 3	+1144030	46475		88419517	642941	30.44 5	194505	40326	70 100
01400	+3/2280	+1144065	40245	e	90419425	045471	44135	124120	95160	19459
01461	+ 37 3500	+1144000	453560		95419216	696321	44/35	108148	95166	14444
01462	+ 57 3 51 0	+1144215	46230	(+	110419525	64/641	44006	144501	45205	19513
06403	+ 575 588	+1145023	48110	Û	45419050	040171	50447	198315	97908	11594
01464	+3/5426	+1145250	50385	1	116419/12	046831	50422	158370	99404	02398
01465	+ 375419	+1145223	49938	C	116419700	667231	20410	198360	5°°5°,5	n2031
DL466	+37541	+1145197	49630	0	111419096	o67611	51190	198350	999536	#2714
DL467	+375432	+1145174	49'548	- 0	111419726	A67941	51136	14+379	09310	95265
DL468	+375447	+1145151	49398	6	103419755	084271	51217	198401	99297	42059
01469	+ 375464	+1145135	49536	()	108419787	0855U1	51239	196420	09426	02041
DL470	+375464	1+1145097	48328	0	110419788	649051	51501	148450	99151	hasha
DL471	+375455	+1145068	40005	Û	103419772	629261	51479	198413	98603	F233.
DL472	+375452	1+1145040	48368	Ú,	105419768	679891	51194	198404	98297	91901
DL473	+ 375446	+1145012	401207	e	98419757	699311	51(50	198400	97940	21025
DL474	+375445	11144986	47845	0	95419756	690691	51697	198390	97120	61444
DL475	+375441	+1144950	47585	()	92419750	691131	51225	198395	97510	01474
DL476	+ 375438	+11:44979	47425	0	90419745	691531	51290	198388	97529	01445
DL477	+375439	5+1144936	472001	G	89819781	691861	51331	198384	97442	61405
DL478	+375431	+1140076	47115	0	86419134	092201	51514	198378	9727:	61291
NL479	+375428	1+1144851	46975	C	88419730	692671	51235	198373	97064	61132
06480	+375424	+1144024	46768	n	89419723	693071	51144	198307	76781	60962
DL481	+ 375422	2+1144700	400401	0	89419720	693451	51034	198365	96562	00745
DL482	+ 375415	7+1104770	46558	()	90410710	073861	50000	198360	96307	80520
DL483	+ 375414	+1116718	464891	ė	91/119708	094031	50348	194353	95750	19904
DL484	+375409	+11/1/1090	46455	0	95419700	095641	56140	198345	95508	79760
NL485	+ 375407	+1144066	46-145	ñ	93414697	675391	49975	198343	95337	19590
DL 486	+375404	+1144034	46485	6	95410093	595811	49744	198338	951 MM	19420
DL487	+ 375 300	+11/1000	40499T	0	96419684	090251	- 4550	198331	95081	7931h
DL488	+ 375300	+1114574	46505	e	102410680	n9n751	44562	198327	04995	19237
DL480	+ 375 394	+110/1553	46495	Ω	102419677	69/0n1	49541	194523	11468	79213
DL 490	+ 315 502	+1144530	46493	0	104419574	-97241		198321	94972	79221
DL 491	+ 375 586	+1104501	404891	, j	11 1419064	1977	49577	198310	9501e	13070
DL492	+ 575 378	+1144500	anaki	0	110419649	097751	44540	198300	45174	14,45
01493	+ 175545	+1144520	40005	6	105419957	-9/251	44410	198545	- 3441m	19650
DL 494	+ 375461	+1144594	46031	(1	98/19800	696421	49.20	198422	Gueni	79081
DL 495	+ 375260	+1100702	46218		A8410433	094051	51104	198137	05512	10041
DL 496	+ 775280	+11.11755	40733	J	69419470	694141	5 614	1281-9	· • • • • • • •	74012
DL 497	+ 375 307	+1120749	Ancsis	0	82412500	094201	ر. دی. ر. دانم را دا	146147	-552	19597
01/498	+3/5/29	2 + 1 + 1 / 7 / 3	46305	. ·	80410550	09-301	مرد بر مرد م ایرون مرد م	198,24		10035
DI 490	+ 275 25(1 + 1 + 1 / 7 7 7	46333		90410580	0.01701	50 (14	198259	45065	10056
01500	- 475372	241114730	46103		9.4.1.0.0.20	- 594471	5034	108201	2571	1447
CI 501	+ 175 202		19720		94413647		56.44.	104221	46727	746 M
n 501	+ 1 75 1. Li		40.29		32/107/-		م و د و ر د ر رو د هر ژ رک	いいこうようい	1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 G n 7 h
DISAT		(*)::::::::::::::::::::::::::::::::::::			91/11/14/		· به مار · به ارز م	1980316	73043 736043	10110
0150/	- デッアントカン - よもとちょう	1 - 1 - 1 - 1 - 1	- 1. - 1. - 1 1 1 1 1 1 1.			- 0 - 0 7 2 1	9989 50109	ания 14 мл 20		15/24
01505	- + 17 547 <u>-</u>	5 * 1 1 1 1 4 4 (A 1 4 1 1 - 7 2	- 40200 - 36600	0		57311-1 	.,211 k,11.2 Kangangan	108060		10.6.
()1 4.04	- + 21 3492 - + 1744 -	271144073 24114073	40902		- 19414936 - 02410-03	5 1 1 7 C 7 1 5 C 5 2 () 1	50000000000000000000000000000000000000	190409		19079
01607	T 31 7766	シャトトルロじろう		(.		- 6423AT	ो र⊒र्थ 1342-*	10-6-2	05.00/	1.1015
NI 6.10		171709092 1414 10991	- 46190 - 46190	0	- 7444977 - 0.761044			(40565- (40565-	- 4744 	145/5
01600	**/****	*****4*41	- MET / 1933 - 1946 - 1933	U 2			4	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	· · · · · · ·	79304
								••••••		•

13

EN-TR-33-DL ORY LAKE VALLEY GRAVITY STATICHS

STATION	LAT.	LONG. E	IEV.	rra-ri	K. MORTH	FAST	HASV	THEC	i A.	COA
IDENT.	DEG MIN	DEC MIN	+0001	TNZO	UT UTM	UTH	GRAV	GHAV	+	1000
		******							· · · · · · · · · · · · · · · · · · ·	
01510	+375593	+1144620	46905	0	99420043	69599	149701	194015	95314	74417
DL511	+375612	+1144010	46498	0	98420078	09012	149704	148042	95287	19350
DL512	+375633	+1144599	47655	0	95420118	69028	149649	198573	95255	14305
DL513	+375652	+1144589	47165	0	99420153	09041	149502	198701	95187	79221
DL514	+375672	+1144579	47158	0 1	101420190	69655	149534	198730	95176	70190
DL515	+375692	+1144568	47175	0 1	103420258	69679	149259	198759	951et	79175
0L516	+375711	+1144558	47203	0 1	105420203	09074	140200	195787	95101	79146
DL517	+375731	+1144547	47325	0 1	103420501	09099	1-9-00	195010	95182	14140
DLSIA	+375752	+1144530	47425	ų l	104420340	n9715	149415	198847	95195	79125
01519	+ 375771	+1144520	47415	0 1	106420375	09/25	}	198875	95191	79127
01520	+ 5/5/41	+1144515	47455	0 1	108420413	0757	149404	196904	95420	79144
06361	+ 3/ 30 11	+1144303	41030		104420430	- 101101	147477 140402	190933	43616 05600	79170
01522	+375381	+1+44510	47033	U 4	107420037	69/2/	158.65	100124	93044 95044	11072
DI 524	+ 175966	+1144540	47703	0 1	107420200	- HOF HO.	151205	109162	06 400	86010
01525	+375901	+11.14542	47905		100020015	69699	ر دی۔ در به م ۹ رز ۱	199665	95406	79672
DL527	+375918	+11//4594	48018	0 1	100420019	69022	150157	149,990	01.249	74474
DL 528	+375910	+1104568	47953	e l	102420031	09001	150.025	199076	46073	14121
01529	+ 375927	+1143020	48045	0	100420061	0958.	15(237	199102	905.1	20:59
PL530	+375430	+1140046	48085	0	102420070	64544	152271	149110	96403	raiin
DL531	+375945	+1144672	46138	6	97420692	69507	150275	100124	46441	nulde
DL532	+375952	+1100696	48165	Ú	97420104	09471	150522	199139	90500	0:177
DL533	+375961	+1104723	48228	G	96450720	69431	150307	199152	76614	26264
DL534	+375969	+1144/48	48245	0 1	102420/34	09395	151595	199164	96758	80409
DL535	+ 375979	+11/14774	48315	0	97420751	n935n	156745	199179	97030	00050
DL536	+375987	+1144799	46393	0 I	103420765	69319	151(54	199191	97.55 n	30975
DL537	+375996	+1144826	48305	0	108420781	59219	151374	190504	9770r	61311
01538	+ 375940	+1144879	48245	6	105420076	04204	101005	199122	100000	01/55
06539	+ 5/ 34 56	+1144/70	40130	0	98420065	-0204	150347	144110	96690	- 0) 4 / 0
01540	- T2/00/0 - 47754//-	+11/1/10/5	- 49993	0 . 	102120201	- 04210 	121322	199031	97748	0/401
DL 341 DL 543	- + 37 5000 - + 37 5000	* 1 1 1 4 4 7 9 * 1 1 1 1 4 4 7 9	- 47050 - 47078	() ()	96420205	04333	120263	10001.	90304	01334 8011-
DESAR	+375620	+11/0/017	-/ 30 -///15	ι. Ο	94620467	09494	169693	196966		2467.
DESan	+375795	+11/0085	47625	•1	93429414	69496	150144	196909	56949	79961
01545	+375772	+1144767	47003	 	92420369	69375	150-34	194676	46404	45261
PL546	+375801	+1140869	41025	u .	04150410	19225	151 571	195919	9745c	11510
0L547	+375727	+1110879	47715	0	06420242	09213	151211	194816	9738r	01209
DL548	+ 375724	+11 14015	47331	()	45420294	69559	luunne	19xean	95597	1:55
DL 549	+375-81	+1144775	47328	(j	95450500	n936 m	152710	195743	994944	60452
0150	+375642	+1144571	17296	()	98420125	09224	121265	190000	47320	oters
DL551	+375030	+1144693	47115	0	03420120	からでいす。	150101	198677	45010	10443
0652	+375609	+1144209	47112	6	924208(m	00321	151993	198635	60196	00 M J 4
06557	+375586	+1144908	47115	0 1	101450650	n9177	151597	19/014	97 <u>5</u> 20	-1301
PL 554	+375531	+1144757	46870	(C	90419423	60401	1507.51	19524	96410	さいちゃく
01.555	+ 575520	+1140584	47470	6	63419916	04215	151+07	198516	+/564	mlane.
01556	+ 5/54/6	+1144/94	46755	Ð	9(4)9024	UG 204	191241	148445	5×790	06930
	+3/3502	+1145005	47585	(j)	107419861	04020	131400	148441	0745	2112
01550	- <u>* 37 - 700</u> - * 775 - 31	+1144443	. 76.40	0	1 19419775	- 10 - 1 - 2 - 10 - 1 - 2	121011	100010	0.1077	- 1 1 / / <u>6</u>
DE550	+375702	+1100000	4/355	· · · ·	1 2 7 1 2 1 2 1 2 7 2 3	- G, FOR 3- - 2, 2, 6, 6	151200	196032	24.20	
DLSAT	+375740	+1100485	4143	• • •	112420312	10157	• 51 41 2	1982 KH	45477	01-25
01562	+3/5981	+110503a	50190	6	113421/64	****	156282	149141	- 1 С. - С.И.5. Ц. С.	11111
GL503	+375400	+11/10977	49201	1	119420004	1.0 U 0 2	151194	19907-	98321	31684
DL504	+ 175818	+1141973	4411	0	119420447	04004	151516	148443	JH4GH	-1450
PLSOB	+ 575970	+1145162	53323	ę i	15 \$46 1721	n#1P4	1 लहा जे से स	149160	09459	11420
01 557	+375907	+1145090	51-10	ę	1214FOODT	NH497	15- 595	147075	به م ۲۰ به	11 7
NI 552	4 275424	+11/11 21 4	4 2 / 20	r	1		1	4 43 4 4 4 A		~ •

DRY LAKE VALLEY GRAVITY STATIONS

STATION	LAT.	LONG. F	LEV.	TFR-C	OR.	MORTH	FAST	URSV	THEC	FILA	CH4
IDENT.	DEC MIN	DEC MIN	+CODE	TN	NEU T	11 T M	(1 T M	GRAV	(n 4 V	•	F1000
							. ا <i>د و ر</i> ر				
01559	+ 375820+	F11/15097	50640	ú	1204	20446	65490	150108	198946	09008	A1788
DL57a	+ 3757754	1115189	52158	() ()	1726	20444	68757	149356	144585	00872	-91700 - n91700
DI 571	+3757604	1145088	56500	0	1160	120334	NH46.5	15(29)	168859	28050	
01572	+3757044	11030AU	54501	0	2010	20233	68968	147510	1921 12	10302	61047
DI 573	+ 3757224	L1445271	52719	0	164/	20260	- 28200	1.4196	108403	100000	42184
DI 57/	+ 3756864	-1	52515	0 A	11.34	20197	53545	144176 1490 X //	100005 100756	00765	N1969
DI 575	+ 375-504	L103136	52105	1 1	1240	120127	68675	119722	108606	166557	20100
01576	+ 375 - 2014		58120	223	5621	20677	67075	14776.2	1900-40		K212G
DI 577	+375000	611051mJ	56951	0	2871	120037	56501	145960	198625	1	5125
01579	+ 3755424	11/20204	50785	0	1300	10927	68687	150236	1925/00	09285	42295
06579	+ 3755291	+11/5195	52541	0	1080	119905	64757	148339	198521	00365	81653
01580	+3755251	+11/15076	50790	Ő	132	119901	64935	149701	198515	98985	81794
01582	+3745701	11/10778	45800	o o	851	18145	69412	149534	197121	49314	79783
DL 583	+ 37 45 7 51	+11/1/1596	46910	0	884	118166	69074	144595	197133	95762	80157
DL584	+3705101	+1144098	45825	. 0	854	118232	59521	149513	197188	95476	79903
01.505	+ 3746531	1144804	45790	0	851	RPSAL	69310	149301	197242	95151	19010
PL586	+3745004	+1140061	45808	ð	924	118013	64293	149458	197019	35555	50020
PLSH7	+374522+	+1144065	45805	0	011	112054	04285	149511	197051	95561	6)031
DL588	+3745434	11144670	45nos	0	، ج ہ	112092	69278	149541	147081	95561	60032
DL589	+ 3745634	+1104874	45418	0	9.07	12129	04211	149550	197111	95556	60022
01590	+374585+	+1144879	45008	0	896	1317e	59265	140010	197145	35574	87.42
DL591	+ 3746094	+1144CA2	45805	Ó	844	118210	69251	149057	197177	45561	60049
DL592	+374627+	+11/148A9	45805	0	904	18247	09240	149721	197204	95619	60083
06593	+3746464	+11111894	45805	ρ	891	115280	69539	149208	197234	95075	80143
01594	+ 3746694	1144898	45808	e e e e e e e e e e e e e e e e e e e	894	18324	09231	149205	197265	95723	80191
06595	+374691+	+1144902	45008	()	894	118355	69224	149289	197298	95693	80101
PL596	+3747124	+1144917	45813	()	310	112403	69505	150171	197320	05949	80.000
CL597	+ 374734+	+1144910	45015	C.	9.94	12444	09211	150163	1973nú	95914	60351
NLSOR	+3747554	+1144504	45838	0	894	118483	64514	150157	197391	95446	80.554
PL599	+ 37 4 7 7 5 4	+1104F99	45638	0	894	114250	69625	150159	197420	95469	0/1025
DLOUD	+3747979	1100095	45523	ú	- <u>88</u> (118561	09235	150147	197452	95015	E0275
ULDUI	+ 57 48154	+11/4/08/	45835	0	874	18000	07241	150170	197485	95321	80277
	+ 5/ 484 [4	1100841	45848	0	- H74	114045	69249	131205	17/510	95828	59750
	4 37 42514	F1144875	- 4 7 0 7 0 C		- N 7 G	1 8 0 3 14	61631	136220	197545	95834	1997 C
	+ 1 400 31	1144664	43083	11	 		-04600 -0340-	トラシムシウ	19/3//	- 9920A	- MC245
0100 <u>5</u>	+ 77 107 1	F[]44087	- 4 <u>3 0 6 0</u> - 3 5 2 7 8	0	841	1103103	201604	150260	1979513	05751	יכנייר בייה -
DL 607	+ 774955	-1120CR0	43673	1.	9.4	10065	64266	150150	197691	05640	00100
CL DUS	+3749764	E1127873	45073	c.	an /	11 11 12 12 12 12 12 12 12 12 12 12 12 1	69297	(197714	35592	- NO. 33
CLOUP	+3749984	1114030	45895	0 0	871	114975	09.005	15(12)	197745	95000	80199
DL 510	+3750194	+1144432	45435	C C	Ba.	118974	69313	150285	197/70	45/74	10152
DL611	+ 3750401	+11/1020	45465	0	А.ц.,	119924	0 321	150196	147010	04,32	01141
DL612	+3/50684	+1140220	45983	ti.	354	19055	69326	150094	191848	45517	79421
DL513	+3750894	+1144815	ADUIS	ť.	854	110104	09336	149455	197070	95370	7-7768
FL014	+3751114	1144809	461:35	ſ	850	10145	64343	1-4415	197916	45312	19182
01 515	+3751334	+1144002	46055	()	851	119186	69352	144926	191422	95314	10,002
PLAIA	+ 3751574	1144700	461 83	(Ant	119230	09363	149346	197977	95335	7471.4
DL517	+3751784	+1144789	46115	G.	25	110200	109364	149970	198009	95304	79725
CLOIR	+3752004	1144783	46145	٠٠	8 n 1	119510	n4371	150055	198641	5541e	14765
CL519	+315222+	1144275	16173	ŗ.	M +3 -	119351	P.0.344	153:75	198673	(, (v , f ,	19134
06430	+3752464	F1124749	14148	(,	+ 7 t	14306	40404	15/12 1	144100	95471	19515
01951	+ 375231+	+1142531	40205	t٠	1004	14370	69145	1-4447	1 adunt	459 Be	19155
L1622	+ 1752044	1144015	the fill	(·	350	110354	nunit	149717	194046	95140	19:05
01623	+ 3751704	1144000	antus.	ņ	874	119269	69520	144554	144005	91966	79314
じしかどは	+ 5/ 500 34	N 1 4 4 7 5 4	44461	()	P 34	18947	04734	1494 59	197752		77545
ግዬ ወረ ካ 	+ 5/49294	111月11日日子。	4.547	() -	H74	11424	C 4 5 4 5	14445 <u>5</u> 117	197736	3.2915	7937.
				•			* · · · ·			• • •	•

DRY LAKE VALLEY GRAVITY STATICHS

1

ļ

3

Ì

1

į

STATIC	N LAT.	ELNG. F	LEV.	TED-PI	BR. FERTH	EAST	LASV.	T≓t ()	r 1, 1	C** A
IDENT.	DEG HIN	NEG MIN	+0008	TNZ	сыт отр	51 T M	GRAV	$0 \rightarrow 0$		• • • • •
DI (25						61 F ()				
06005	+ 5/ 50 504	1145147	48175	0	102419020	000000	120220	19/621	94061	61755
06056	+ 5/51 594	1145165	48481,	Û.	108419184	046141	159729	19/452	04465	61975
11.687	+375207	1135115	4802S	0	109419312	68588	151221	198651	78302	05043
DI-688	+375245	+1145199	49105	Û	117419379	00765	150105	194106	92007	heesi
DL640	+375260	+114/454	40521	0	116419444	099220	150439	198137	45)9	o ° 157
DL691	+375250	+1184334	4741C	()	110419419	70133	150350	196113	17.157	81 599
06492	+375319	+1144407	46576	ι.	120419544	04453	150536	198214	9n1-8	60364
06693	+375385	*1124474	46470	0	113419063	09455	1-14050	106311	95077	19340
PL694	+375381	+1141445	4n#7C	()	120414057	59104	1-9-50	198305	45244	79510
DLn95	+375376	+11444494	105191	e .	125419549	24403	150497	195298	95579	70-30
DL696	+375379-	+1100387	46820	0	123419055	69950	150400	198302	4622.	8-37-
DL697	+375 540-	+1144357	47100	e	124419058	69993	150771	198303	96793	06452
DL698	+375380	+11443224	47401T	0	128419659	70045	151003	198303	97364	61304
06099	+375361-	+1144303	47720	C	126419525	70073	151042	194276	17-7-	61520
DL700	+375335	+1144293	47894	. e .	127419577	700893	151059	148230	97890	81003
DLTOI	+ 175331	+1140260	48347	()	132419571	70129	151913	198232	98274	81917
DL 702	+ 375 32 5	+1144243	48734	0	176419557	70160	159771	194220	98411	+1925
DL 703	+ 375313	+11/4/215	4921Y	с. С	140410539	10205	150441	198235	98587	343
PL 7114	+375305	+11/0198	4974Y	ò	107012526	70045	151.55	144144	QANAT	01:53
DI 705	+ 375200	م من م 1 الم من م 1 الم الم الم من م 1 الم الم 1 م	50201		151310515	70283	149.29	148185	JAGZA	n1941
01.706	475202	• • • • • • • • • • • • • • • • • • •	51.75 .	,	1. 1/1 05/17	76323	144444	108175	00173	ب فر الم
DI 707		-1:44132 -1:44132	51264		165010400	703611	4 4 7 4	104144	0051	12105
	+375070	• • • • • • • • • • • • • • • • • • •	51774		175419479	70301	1 1 9 1 1 2	14-10-2		52175 5-175
DL708	+ 37 1274	FII44V83	53104	. U .	1/34177/2	7.0.4 3.0.1	149236	100140	120200	62404
	- 1 37 2604	-1144083 -1144083	20100	••	102419314	- 700-20. - 700-541	1 12 14 14 14	105134		
01711	- T 31 28 231 - T 75 28/1	• <u>1</u> 1 21 - 1 (• 1 • 1 • 1 • 1 • 1 • 1 • 1 • 1 • 1	505030	() ()	10/41/4/04	70966	1 40 704	190161	100374	06043
	1775/17	+110390C	- 2492C	12 1	シュノリオエクセムジ	70500	()///// ()(,)/()/	140100		
01717	+775170	-11/13/13/1	60750	U i	272419352	20457	143713	140200	19177 <u>1</u> 1936/23	66916 23 02
01710	T213670	1114 <u>3</u> /80.	27121	0	287419978	70002	14447)	1.407.907	162244	67.30 83.30
01710	- 7 31 3 31 61	T]] 4 3/6/ 		()	310414005	70027	1.4.271.3 1. –	140671	103100. 103100	00024
17 L 7 L 3	+2/2201	1111440	23404	U	210414075	71370	140224	14-313		06300
01716	+ 5/ 5 501	+11030RU	20001	0 1	254419077	7.0043	140,440 140,440	1903/0		07731
	+ 3/ 3 54/	+1144444	5040¥	0	192419005	70366	1.2011.2	196202	44,351	02335
01720	+ 4/ 7404	+1144146	50054	1)	197419710	712117	130048	144336		
01721	+ 57 5 570	+11.14217	48984	<u>с</u>	153419045	70194	126025	144644	48.543	01050
	+ 575440	+1144052	53150	5 to - 1	215419780	10434	148344	194391	1002/4	22.240
PL/23	+ 57 5452	+1183939	24524	ù,	227419525	19602	147247	196425	101064	02022
01.725	+ 5/ 5498	+1143810	6616Y	e .	220419192	20781	3-4-3-6-447	195475	103078	40105
FL726	+ 37552	+ 1 1 1 2 9 1 4	517JY	(°	296419939	70630	140000	194513	105462	61013
CL 735	+ 375730	+1+03981	57294	ť i	201490353	70075	140505	198815	112004	12305
DL 736	+375732	+1143953	55000	0	522450354	71/269	1 +7 + 31	198018	106591	n1463
01739	+ 375770	+1117760	00200	(:	314420412	7.5 - 41	1 + 4 + 51	1944ARZ	102175	H:~53
DL740	+375794	+1103278	57/51	υ.	840420441	70679	172197	104404	10035	01470
01741	+375507	+1143939	54424	()	511444641	70.490	147514	194451	1-1103	A1749
01742	+ 375775	モキキャイエンモー	52294	()	191461398	11350	1 10 12 1	* ちょくしょう	0477	11903
01743	+ 475834	+1100109	5279Y	()	021460507	70346	144428	102300	1 (1) 2 3 -	2 1 5 5 S
D⊾744	+375881	+1199125	5100Y	C.	141460203	70313	144275	129935	92013	n1374
NL 745	+375894	+11aaea1	53088	(°	184420624	70435	144137	199657	01335	M1414
D1746	+375915	+11:3445	55840	C .	5544500h3	76575	140-13	149985	100682	41255
DL 747	+375874	+11039109	558591	n .	243420588	10017	1409.15	149625	100034	51251
DL 7 4 9	+ 375904	+1123541	50704		247426751	1-122	142.49	191157	1-1-575	11004
01.750	+ 375401	+ 1 1 - 12 USA	5209	• •	125460199	79409	1400 5	142196	92724	F. 031
DL751	+315940	+1+1+115	51+14	a.	154426/13	70011	149375	149130	44252	51,14
01752	+375444	41100230	49037	Ġ.	142420708	7.1120	149450	197201	974114	1 1024
PL753	+ 375954	+11_4240	49024	C	139420724	70133	149:52	149142	973%	1.1525
rt 75 a	+ 375400	+1144311	ABERY	ů.	131420030	70437	149000	149075	96404	74431
PL 755	+ 775423	+11/10370	48144	n	13142-041	n4+14	144452	129112	95131	14.
51.71	71101									

Ţ.

DRY LAKE VALLEY GRAVITY STATIC'S A2-13

1.	STATION	LAT.	LUNG. F	LEV.	FFR-COR.	NORTH	FAST	CASV	1460	- 4 4	C H A
-	IDENT.	DEG MIN	DEG MIN	+CODE	TN/CUT	UTM	Q14	GJAV	6-21		1 16.0

Š	DL757	+375891	+1144493	47775	· 0 109	420548	69771	149738	199050	95644	79400
6 7	01758	+375875	+1144470	47720	C 111	420575	640.15	149074	199031	95551	79300
	DL750	+375853	+1134481	47545	0 109	420529	59791	149559	198495	05302	10255
-	DL700	+375831	+11/1/4490	475n5	0 109	420488	64/76	149505	148963	95 501	79160
	D1.761	+ 375859	+11443604	179891	0 127	420544	-44H1	149035	199003	95792	79555
	DL762	+375864	+11/1235	49614	0 142	120558	70144	119124	199611	47397	nunth
a	DL763	+375805	+114/13394	8031T	0 132	120345	10001	144254	198926	96125	79275
1	DL7n4	+375787	+11/14422	47453	0 119	222409	- N9000	149552	194494	45319	7725
.	PL765	+375701	+11/4439	47203	0 121	120219	69654	149457	198773	951 11	79120
	DL 766	+375727	+11/103234	179201	0 1 4 7	420301	76613	150460	190010	90.500	00155
1	DL 707	+ 375789	++++	49865	0 150	420419	70170	144474	108901	97557	81601
	01768	+375727	+11/1/204	UNARY	0 170	420300	70202	150196	198810	98261	01.55
	01769	+375653	(+ 1 1 <i>n</i> /1 2 1 9	4900V	0 184	420168	76123	150730	108702	08222	- 61-60
	DL 776	- 4756/19		176415	0 140	2015-	70050	156760	108-05	0220	-0100-
		+ 175 - 14	-1:44303- .41:444303-	1160×V	0 1 2 4	120130		1.0717	100077		10
					. · · · · · · · · · · · · · · · · · · ·	42 24 32	- (-)1	197117	104661	05 07	10 502
	06772		1 - 1 - 1 - 1	4/11/		110754		1 1 4 4 2 6 4	ាល់លាល់លាល់ តែលាល់ ដែលល	- 9 7 C - 2 - 0 C - 7	10335
	51 779	- 1 275502	+1144420 +114470		10 1 K 4	414770	7 1 1 4	167280	1907805	00110	796.03
		- 1 31 3 32 0	(* 1 1 4 4 4 4 5 7 (* 1 4 5 5 7 6 7	177101	0 177	41 47 33	701070	161266	10001630		
	01774	- T 37 397 3 - 1275 501	-+ L 44270-	175501	U 177	110451	- (5 + 5 - 2 - 7 - 1 - 2 -	1916-19 1916-20	1040224	11122	-011/0 -011/0
		- + 37 3441	T11942044	ا ۲+۲. ۲) مانطقه	0 100	414007	- 1 · 1 - 2 · 1 ·	1.6	108.74 140840	9771) 0 HOL	76171
	01.779	- + 37 3478 - x 275 38 8	-11-444AL	-+0043	0 L 1 2	0128024	- 0	n in the second particular in the second particular in the second particular in the second particular in the se	120120		10020
	01770		1 T 1 1 1 1 2 3 7 4 1 T 1 1 1 1 2 3 7 4	40073 170611		41927	76571	151:55	108325	07102	- 14-20
	DL 740	- T 37 3420 - 179 753	**1199393* *********	64611 6412V	0 1 30	1232134	10071	101000	190206	00557	-91341 - 91341
		- TOO / DC	1144282	100101 10101		462613	10010	1444465	ということは つかいてつとい	9723C	- <u>nunuu</u>
		10 / 01	11111303	1777 6	0 120	402014 113337	- 7 - 9 - 9	1/20004	201323	0 0 7	2001
	DI 747	- 170 //1 - 172 015	+ 104225	5-478	- 17	127316	70050	140220	20000000	0.01	1 1 1 1 1
	DL 78/	- 1 20 011	11144279	- 1007 F	1 1 1 1	123-06		146570	200402	10020	
	01785	- 130 807 - 130 810		57	0 147	いきたからりつ		140479	200370	1972 4 6576 -	
	DL703	- 7 36 61-	(*) (<u>1</u> 1114 ()	57.74	10 100	968213		136330	262462	004.11	
		- T O O O O	14 1 1 4 4 2 7 6	17471 Gartin	0 17	127507		1.1.5.244 1.1.5.244	300407	00-11	- 12 E H / / - E M / 2 E
	01749	- T 30 - 766 - A 2 4 - 766	+1100403	57134		1002297	7:20-	1/6.54	CURDD7 746746	44633	201.101
	01740	- T 30 7 3"	171144455° 1414455°	57610	0 128	-428613 	70370	142420	21/2214		
	01700	- + 30 / - 4 - + 24 - 70 /	A 1 4 1 7 G A H	57.55	0 L30	127256 127240	10464	149200	200571	0.0172	
	01707	+ 10 / 14	1103700	56678			70.70	1.0211.2	200021	14 N 2 1 2 1 1	0.02.31
	NI 796	- T 30 - C 34 - A 7 2 - C 7 (A 14 4 4 700 1	57.11	0 202	467203	7047.	190112	201193939 2011676	1.500712 1.500712	- C + 177 C
	06743	- 1 30		(C 20-0 F	()) "S	146 6 J 74 10 3 7 11 6 5	- 73 47C	1423200	200376 200646		- 01 / 7 7 7
	OLAA:	- T 20 - 076 - E E 4 1 / 3 3		57/04	0 144	1478730 14787		1	800313 36-236		- 19 -19-1 9 - 19-19-19
	00301	- T 20 LUKK - A 26 - 307		11440	· · · · · · · · · · · · · · · · · · ·	1 C P 13 1 1	- <u></u>	140215	200100		- C (C - D C 7 3
	DL Sug	- T 30 - 7-17 - A 76 - 0 - 7				100520		4 4 4 7 7 44 4 3 2 5 7 3	6 200 0 0 0 21 0 2 4 0 0	1.0.1.∂**4. • • •	
	01865	- T 30 - 702 - 1 781005		-0111-1 	75	11:47	- C 1 7 / L - T A L L /	1 - 1 - 1 - 2	200019		
	01811	- + 30 1002 - + 10 057	171164253 1414.7700		0 1 2 1 2	402071	- 701 27 - 1673	1.1117.3	21 10 AU 77 - 10 - 01		
	01.410	- * 1 <u>0</u> - * 17 - * * - * 106 -		01311	1 1 1	422510	10740	1 44 うて近 4 1/5 2 まい	<u>, , , , , , , , , , , , , , , , , , , </u>	111465 1330 - 146	
		- T 30 1 0 0 0	+ 1 1 4 4 4 7 3			102110	0.404.5	1 1 3 7 34	6 × 0 / 7 6 37 × 5 5 33 × 5	1 (17) 3 2 2 3 1 (17) 3 2 2 4	- CO (4) - CO (4)
		- T 101149 - 17419	+ 1 1 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	01071 60770				162145		1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	- 7 H (h) -
	01920	+ 301213	1 1 1 1 1 4 2 0 -	- 20 (<u>6 1</u> - 20 (<u>6 1</u>	1 1 A A	46.500		1 4 7 7 1 4 4 4 5 7 5 7	P	1 (4 () 1 () (4) 1 () () () ()	1.11.6.11
		- T 3/ 2 3 3 4 - T 7 1 + 74		57073	0 204	114264	11000		197244		1301413
	0194	- * 37 + 1 7 -		54311	121	- (1.) 7 4 (1.) 		1 1 1 1 1 1 1	11112		
		+ 774174		- 21 / N1 - 6 1 1 1 1	0 127		PP0/7	140273	190143 1055-01	9-47-	- 1 2 St 4
	01041	- T 3/ 41/ 5 - x Z 2/4 1/ 5	171745355 	- 3 T J T Y - 6 4 6 7 4	. <u>1 ≤ 3</u> 	641739 <u>3</u> 99979	5754U	147154	1.4 L - 1 1.4 L - 1 1.4 L - 1	sana ng jin Sana ng jin	ハイムビハ
	01042	- * * * * * * * * * * * * * * * * * * *	17137753/4C	- 7 [3 <i>[</i> Y - 6 4 4 4		417275	- ****	14775	140213	4 1 9 6 5	5 6 3
	01 4 5 5 5 1 7 0 4 5	+ 2 / + 1 / /	T1145363	- 7 7 Y - 1, 7 2 7 4	9 159	917299		14/148	1 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	1 1 1 / -	5 e e e e e
	11L0-4	+ 5/ 4 20	1 1 1 4 5 59 5	27354	ν 1 ² γ	417403	64245	14//**	19556	[]). 내사용.	26.01
	06.3	+ 1/ 11/4	+1145425	57050	0.194	117406	- e e 4 e 1	147740	111111	1.1.1.1.4.1	C 1.121
	1 <u>C 7 4 6</u>	* 1/4[*]	+1145454	- 3 5 5 3 Y	0 620	417404	P. 4 + 5 5	14/210	190755	101125	n 51 to
		* 774141	(*1*4554) ****	33/71	اج ا	417-00	- e n 59 a - r	14/352	ት የስኮ ካሪ : ት / - የ	141332	1.25.1
	111.74M	-# 5741266 	11145304 14145704	54121	و مرم الم	al 7411 	- n n 554	14/120	140561	1.1.4.4/	セステレフ
				-1 11.4	· · · · ·		1 .	•• • • · · · ·			• •

14

EN-TR-33-DL ORY LAKE VALLEY GROUTTY STATICUS

Į

1

1

. |

STATION	- LAT.	LONG.	ELEV.	TFREC	DR. NORTH	FAST	CASV	THEL	F 4 m	CRA
IDENT.	DEG MIN	DEG MIN	+CODE	TNI	OUT UTM	074	G₽∆V	GFAV		+1600
									~ ~ ~ ~ ~ ~	
DL850	+374090+	1105431	55645	0	167417236	- HH73	146010	1464211	151396	62784
DL851	+374093+	1145303	5055Y	U.	145417235	orbhl	148457	196425	9900n	62509
DE855	+3739521	1125313	51201	Û	115416984	68652	147895	146220	99861	62513
DL856	+ 37 3971+	1145418	53108	0	143417016	HH497	140019	1966471	100536	02500
PL 857	+3739604	1145542	55995	ò	196416992	60315	145320	140231	111794	82893
PL 858	+3738721	11/15 128	50501	Č	118416636	00073	144235	196103	99022	82516
DL859	+3738914	11/15/439	52665	0	121416567	66464	147050	1961301	01 509	63402
DL860	+ 37 39 3	1145665	56 585	45	280418443		144746	1901901	10121	62.510
DL 861	+ 3738204	11/15273	49745	0	101416743	68716	144051	190027	GANDI	A1977
01.862	+ 3738024	1188884	50544	c.	10501-709		147.79	198921	00190	21939
DI 863	+3738574		52119	0	120014803	68497	147808	1060811	10.766	03110
DIBBU	+ 3737704	1143-44	51170	0	110012658	68387	107136	405067	00187	
01004		1145506	52528	0	1/1/12707	60307 60208	105510	100,001	101200	+2472
DI 865	+ 77 88654	1147240	52374	0	186/116517	000,40 68100	1.7.55	106105	100207	22553
DL857	+2728214	-1-1-0-3-0-3-2- -1-1-0-7-1-0-	5 1 4 C 3		1/11/11/2700	, ocyana Landara	147227	1	60717	
DISAR	- 373021 - 273880.	1147714	52104	. 0	100/1207-		147624	1061151	977122 1029444	02272
DIBAR		1103791	50700	0	17419030	- 6772L	1/17770	190112.	000	66697
01670	17760	1127228	51636	19 75	200410164	- 67700 - 57212	1.7576	190021	999400 10362-	1
DL874	+3730-01 +3730-01	11123080	51020	0	1 3 2 4 1 5 6 6 6		147224	140120	001.00	1060EV
	+ 27/10/134	1117734	00040	- 1	48 34 10 / 61 67 3/11 71 //	د مناطقات المشاطقات	1 . 2 . 75	106662	44507 103757	1088 3 3 3 8 3 5 3 6
DIAVA		- 1 /1 m 3 / / - 1 /1 m 3 / /	50100 57640	0	1 17/117-51	- 51600 - 55607	3 4 6 + 2 3 4 - 1 7 2 Z	1922221	000102	- 12000
01084		-114-343 -114-343	50100	0	15 10 1 2000	- 692977 - 2024	1.03.7	1900-C) 1900-C)	00.7	02300
DISCI	+ 77/17+7	1145675	20162	() • >	159417648		147943	199791	44414	
	* 31 4 31 31 * 7 / / / 7 / 31 31	11443/0	- 2 3 V C 3 - 4 C 2 4	12	195417050	- 60044 - 2775	141664	190740	00711	
	+ 314 31 31		602.0	()	143417754	1 1307142 1 18462	147677	196637 196230	99311	02474
	+ 7744341	1145676	- 10 14 3 - E + 2 3 6	()	152417977	07076	1.4.4.4.4.4.4	10-01-	94333	02495
	- T 7 / 4 4 7 9 7	110-234	51363	0	195411000		140044	195715	99766 10.55	02074
	+ 57 44144	11:1223	56444	9	201411035	11400	141167	1400431	1990 <u>9</u> 6.	
DLOOY	+ 3744364	1145514	20143	0	19/41/065	00331	140120	1969201	102947	03070
01040	+ 5/ 44001	1105377	26065	0	154417951	54334	1401/2	1909001		0230/
01091	+ 57 4 4 7 5 1	145467	22444	0	228417983	08405	14/200	1970121	LOILUR.	12420
06892	+ 5/ 50194	1144535	48040	1)	104/16/55	n 4 38,4	142472	190000	97064	91241
06593	+ 57 59 0 / 4	1104834	47200	ò	103416417	0.9354 0.000	144142	140154	97007	-1912
01000	+ 5/ 59 99 10	-1144035	46080	0	101417082	64373	140077	140224	00243	50703
01.095	+ 5746851	11/1/10/34	46390	() ()	9691724	n <u>1</u> () 1	140475	19n4(v	500000	80474
	+ 57 41 7 0 4	1144835	40170	0	94417404	04343	1 - 4 1 54	199530	90007	84415
01.597	4 9/4 [*/31	11446 54	46123	r) -	95417446	04240	144605	146371	95035	68499
OLA9A OLEVO	+ 5/4/14	1144833	48040	0	43417485	1 64540	149635	140002	96005	50351
DI 034	+ 3/46 304	111032	40423	0	91417524	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	144638	175532	05454	00552
01909	+ 17 2 3 4	1144631	45746	.i	94417568	1.4542	149254	19000/	45864	ち(アウセー
01901	+ 3/42444	1140828	43931	0	93417624	12620	144644	196/11	957800 	85 () et et 15
01.902	+ 1/4 5154	1144624		()	944 2078	04548	144645	195740	53142	nn 1 + 11
01969	+ 5/ 4 54 / 4	1144629	455711	0	92417751	04147	149318	196795	1915 62 81 M	79155
01000	+ + / 4 36.94	11/14/24	45053	G	93417772	0.00254	144 5-0	196027	- <u>-</u>	00176
01965	+ 574 591 +	1144839	15745	(°	93417512	6.4.5.50	1-14-5-54	1460544	929.99	639.47
01.007	+ 4/44114	1144042	45545	0	92417849	0 0 545	144741	140044	95631	8 (1) K (1
21.967	+ 1/44 5/1	1144648	43743	0	42417486	03212	144414	190940	45054	· · · · · · · · · · · · · · · · · · ·
	+ 5/445/11	1144051	45615	0	93417434	<u>n931</u> 0	149417	145452	95576	
01.014	* * * * 44 / ***	1144050	47705	()	45417464	54501	3 12 14 14 SE. 1 1 10 17 17	195954	いつう47 07 -	~ () () c')
96911	+ 5/416/4	11/4/51/	4/ 555	i, ₽	111417409	59513	144.55	190355	97003	01444
11 C 1 Z	+ 5/4169	11/14/54#	46603		109417412	n9/07	114151	190230	3/25-	-1-)-
12474	+ 5/41/04	1144570	40405	0	106417413	19120	149920	190530	47105	41 503
11.714	+ 5/ 917 91	1144605	40303	()	104417418	e trindh	149/11	19030	90/10	01622
116415	• 5741750	1144031	46155	ſ	102417411		149495	140537	36350	MG 147
06916	+ 5741704	114065	45105	0	99417410	09595	1 446 55	19555	96681	~1.157
ULY17	+ 5/41694	114/1695	46675	n	97417407	64550	144153	190335	3545 2	01.550
012919	+ 5741714	1144/25	401/14	0	95917409	- הייה	144691	1403 49	95408	04646
		にす す ゆうり それにす。		n	- 11 F F F - 4		3 1 4 4 4 14	1 / A. 14 ()		4. 18 1 14 L

jĝ

FN-TR-33-DL DRY LAKE VALLEY GRAVITY STATIUNS A2-15

STATTO	V LAT.	I CNG. E	'EEV. 1	FF₽⇒rOH.	NUSTH	FAST	CASV	THEC	r (+	011
IDENT.	DEG MIN	DEG MIN	+CODE	TNZOUT	UТы	1114	GRAV	GRAV		+1560
									•	
06950	+ 374171	+1144780	40095	0 94	417407	094501	49118	196539	95952	+632
DL 921	+374171.	+114/1807	46125	() 95	417400	693861	49134	196539	959ar	130.55
PL 922	4374172	+11/1/1/70	46285	0 05	417406	AUZHEN	39157	196541	96171	ROJA
01922	\$ 37/1171.	4 1 1 1 1 1 1 1 1 1 1	76773	5 Q /	117407			106530	06510	0057
		11144902	140440	0 94	117403	-042471		190239	- 70217 - 05479	2022
	+ 5/4175	+1144920	40000	0 95	417406	6461941	. 4 * 1 7 5	190241	04/6	0000
01-452	+574174	+1144957	40052	() 44	417407	691661	49221	190545	90/59	0000
01926	+374172	+11u49R5	47028	0 95	017402	091281	49 50 7	196541	57011	5107
01927	+374175	+110501)	47205	0 00	417401	090801	49349	146541	97313	0127
01958	+374172	+1145037	47546	0 64	417400	690401	-9340	196541	97540	6142
DF858	+314173	+1145057	47791	0 100	417402	090191	49255	196541	97539	-8109
01930	+374174	+1145083	47985	0 101	417403	084811	49232	196543	97642	0157
DL931	+ 374171	+1145110	48300	0 104	417596	689411	49125	190539	98042	6107
01932	+374170	+11/15134	48545	0 105	417405	689061	49054	190540	98190	8174
01932	237/1172	+1 = 1 = 1 = 2	18900	0 105	11:7396	nAr.651	JRAHP	1965/11	06301	A179
	+ 374177	*1145100	00.00	0 100	917298 9177030			106504	03.70	
06734	- T 214111 - 774777		00501	- 0 112	417404			190390	- 40070 - 00030	0140
00935	+3/41//	*1145251	44543	(1 <u>1</u> 1)	417405	001031		190540	10774	0204
UL 936	43/3814	+1144050	20.320	0 147	43.6764	04//11	48214	140026	99517	8620
DL937	+373825	+11440/13	44273	0 124	416772	690431	44254	196034	98295	6161
DF336	+373819	+1144722	485.00	0 117	416758	nº5271	38570	196020	ORTHR	6170
06939	+373805	+1144009	48635	0 155	116903	n96901	48730	196137	0-1359	8109
DL940	+373907	+1144205	49800	0 162	414929	698461	146080	190154	44163	3247
DL941	+373907-	+1164724	47540	0 109	1416921	695201	46691	190154	07477	6137
01945	+373939	+1144588	482711	0 120	416985	697141	43092	196201	99.512	8197
NL943	+373994	+1144502	48920	0 127	417090	698431	49349	146280	99107	6254
01.944	+ 37 3994-	+liagota	47521	0 112	417086	696/01	49147	196280	97587	5149
111.945	+ 37 3995	+114/24	467 11:	u i Gr	417084	045101		190290	26720	RESAR
DI 946	+374081	+11/1518	47125	0 114	117250	-90151	49/94	196408	08-95	1.213
DL947		+ 1 1 a // co 7 5	46689	0 105	117218		49.600	10-409	OFUST	- 10 C () - 2 - 45 T () - 1
DIQUE	274002	F11440255 F1440255	-160/ G	0 10 3	14 E 7 2 4 5 14 E 7 2 4 5	- 0 - 0 - 0 - 1		10407	00063	- 01 00 - 1 00
	+ 314003	*1144773		0 100	1417 <u>4</u> 47	.010140		196410	90631	
DL 944	774211	T 1 1 4 4 5 5 5	40133	0 195	417440	01/0/1	39236	1.402.01	111021	01/7
01.450	+514252	+11/100 (7	47000	0 190	417225	690241	49440	190046	95471	8045
06421	+ 314259	+1144/21	0.28.31	0 94	1417572	092091	49179	190067	6,26,25	C111
01.925	+374278	+1102561	45985	C 104	1417513		2030A	1900.92	90802	8139
DL954	+ 474346	+1144007	45506	à 97	417737	696731	49475	196794	95754	9650
01.955	+374346	+1104717	45600	0 95	417733	095111	49217	196794	95565	7099
DL956	+374405	+1144025	45791	0 94	417846	695441	49433	140480	95035	8011
DL957	+374436	+1144521	45955	0 102	417895	597951	50154	195910	46484	8091
01.458	+374432	+1101/31	45805	1 29	417592	024871	49245	196920	15421	70.10
01.959	+ 374495	+1104785	45005	6 8 9	418904	604051	49599	197012	45394	7900
DL960	+374445	+1104588	45575	(1. 92	412.12	090901	49021	197012	45717	فسم مدينا دخ
DEPAT	+ 374.190.	+1105212	69125	0 124	117900	nH77/1	4975	197012	08071	- H 2 4 3
DIGES	AZ70057	-1-4-5-18 -1-5-5-18	16600F	6 100	417000	- 0.0 / F + 1	4.03.72	1.0.5.1.5.		<u>C</u> . 3 - 4 - G. 4. 2 - 2
DE GAR	× 37/// 2.3.	• • • • • • • • • • • • • • • • • • •	44406	0 100				10-630	11202	
06903	- T 7744361		4010a	0 76	417085	0.00161		1111420		C. 1 1 1
	+ 314436	+1145462	4/314	0 105	017280	-9400T	26404	1.16420	41555	- 1 - 1 - 4 - 3
01465	+ 5/44 52	+1145142	48545	0.113	447477	nn/15/11	44305	14040	-3-442 m	5140
01966	+ 374346	+1+44949	46.58.1	0 96	417729	691831	+ 4 2 4 1	190797	48 548	ols/
DL967	+374363	+11/150150	12201	0 101	417750	n90131	49710	146814	47225	4133
ቦኒዓ6ጸ	+374348	+1145105	47760	0 111	417724	n84411	49007	196797	23012	r135
NL 969	+ 374 540	+1145161	48354	0 118	417722	111541	44000	140797	23374	そん さつ
01.970	+374289	+11/15025-	111111	0 100	417017	n91011	44744	14-711	77417	Atua
01971	+ 374252	+11:1920	46515	1. 9.	417571	602001	44404	120012	36592	1000
r1912	+374214	+11/15120	48135	6 111	317526		4951-	196651	10110	
01977	+ 37/1214	+11/12277	494011		1417470		44754	160002	36751	ر بن د د ۱۰ م
n 01/1	JINGLO	- L: 47677 414 - 80-414	111201	U 1014		-007071		1 700.07	3163.	
01075	- 727411/3 - 17/1/137	* 1 1 6 1 4 1 4 1 4 * 1 4 5 6 7 7	1. 1. 1.	 	(4 L / 2)(() 		(4 7 6 7 8) (, 6 4 4	140402	1/3/4	
06975	43/40/47	T 1 1 4 4 4 50	45125	1 I I I I I I I I I I I I I I I I I I I	417647	04601	· • · · ·]]	140410	10205	- <u>r</u> v / c
111.11/1	+ • / 4 (1 (1 (1 (1	+ I + 4494S	18003	0 100	417087	641941	44 14 22 24 44	195291	46430	1097
	******	••• • • • • • • • • • • • • • • • • • •	1 7 1. 1 1 1	0 10	COLUMN CLAS	- C (111) - 1		· O + I - i	10 / S. N. S.	•• • ·

EN-TR-33-DL DRY LAKE VALLEY GRAVITY STATINGS

ł

STATION LAT. LONG. ELEV. TE	R=rOR.	монтн	FAST	PASV	THEC	F 4 A	CBA
IDENT. DEG MIN DEG MIN +CODE	TNZOUT	HTM	11TM	GPAV	GRAZ		1000
						-	
NI 978 +378087+1145179 88089	6 11AA	17200	489021	187/11	0-010	381 77	51 040
	0 1004	17270	28/101	1855-1	0.4.10		5.21
$D_{1}^{1}Q_{1}Q_{1} + 37410341904222 + 3043$	0 1264	17110			04719	97030	41.07
	0 1004	12073			198218	17202 0740 1	- 01 0777 1 - 1 1
	0 1024	10765	091091	496191	0.0101	47402	01433 61620
	0 1304	16787	094241	440443	90213	41024	01234
NL965 - +373780, +1445162 - 49690	0 1154	10700	(000/0) (0000)	-40017) 	110154 107154	48344 46034	C1/42
		16084	08/901	401041	90130	48478	n2400
	0 1024	10026	0.0041	102041	98080	97711	01428
0L000 +373000+114490 4755	0 1944	16/51	441541	407251	95027	9/44/	01335
DL968 + 37 3520+1165(58 48620)	0 1014	16/45	040621	488151	96027	95130	01500
01909 + 57 57 76 + 1145085401001	0 1014	16066	649931	140301	95963	97553	81029
01000 +373674+1145225466241	0 1004	16473	68/951	4/4651	95814	97300	80843
01.991 +373692+1145089460901	0 1 1 4 4	16511	684451	476491	95841	97066	80776
06002 +373644+1145014484611	0 1054	15526	040451	4/50/1	92021	97522	66593
11443 +373706+1144918490711	. 0 1084	16543	642431	4 (2 (5)	95061	97545	80955
01994 +373722+1144814494591	0 1174	16576	093901	+/4071	95884	98070	6151 <i>i</i>
02995 +373726+1144696 49954	0 1394	16587	095691	420451	95896	99106	02500
01996 +373755+1144600511911	0 1594	15009	69/101	-1/871	920921	00659	02759
01997 + 37 37 14 + 11 45 95 5 497 11	1) 994	16523	n7/171	4/9501	95673	98860	42005
01998 +373732+1145822 50900	1094	16561	679121	4/19/1	452444	34501	h1044
DL999 +373687+114564049961T	954	1-1484	501421	1.76.271	95034	21540	61172
DL1000 +373728+1145602 50528	1014	16561	672361	404621	95093	78014	r 1 36 3
DL1001 +373670+1145494 49928	954	10457	083971	471001	95219	48271	91542
DL1002 + 373661+1145371 49428	() 994	15444	045791	411271	95795	47641	01004
DL1003 +373672+1145259 48810	0 994	16468	08/451	474151	95012	47534	N6440
DL1004 + 575729+1144273 49204	0 974	1-573	547201	414141	95695	47822	61134
DL1000 +38 775+1145748 5537Y	0 1024	55103	678901	487475	100345	98714	79431
DL1007 +38 864+1145749 56/PY	0 1144	22550	0/0931	465087	200473	99553	80361
061000 +38 952+1145749 58154	4 وہ ² م 1	62218	675891	402002	0000021	00525	nente
DL1009 +381023+1145715 63/14	0 2654	22651	679361	450972	0070e1	02354	66684
0L1010 +38 928+1145055 5891Y	0 1394	22477	222999	450962	<u>20056/1</u>	69773	80619
0L1011 + 38 853+1145693 5788Y	0 1144	22537	679751	406546	004511	00520	n1n45
041013 + 48 874+1145574 59031	6 1384	22380	681481	458162	004801	0.0242	80,580
DL1014 +36 803+1145520 57224	0 1254	22220	64d101	404/46	2003841	0.0445	51 51
DL1015 + 381001+1145578 6144Y	0 1734	22015	ph1371	446792	000741	01431	81649
0L1016 + 38 902+1105520 6150Y	0 1524	22207	062241	444122	2005881	01707	61003
01.1020 +38 805+1145289 54874	0 1324	2252	065671	480512	200387	90300	80755
DL1021 +35 864+1144319 5500Y	0 1634	22371	n+5341	چ در ک ے دی کر ہے۔ ا	00473	994H2	9,041
6-1022 +3A 900+1125362 5852Y	0 13-4	22444	04-15/1	46.05¢¢	1005351	19200	n() / 7 n
DL1023 +38 951+1145308 36598	0 1604	22531	685331	400742	200601	99231	80144
PL1024 +38 998+11/15408 60394	0 1754	22015	5551	447352	200 67 41	90965	311244
DL1027 + 321,48+1145307 58231	0 1794	22/10	042311	120215	2007431	29/17	r 1 v 3 n
DL1024 +38 30+1145359 50164	0 1300	20537	nn4971	443961	992621	00519	81504
NL1030 +38 87+1105260 54134	6 1254	<)434	nr.02n1	485951	99327	けいかけい	e1557
DL1031 +38 128+1105400 5583Y	0 1354	61900	of4341	473091	993971	11:456	01547
DL1035 +38 173+1145297 53541	0 1374	51005	249451	40/001	49405	999941	*1569
DL10*4 +38 217+1145256 5290C	0 1234	c1175	1100401	495991	99527	29557	01054
DL1035 +38 224+1145283 53426	6 1244	21127	580011	488441	97537	29727	H1n31
DL1030 +38 230+1145311 5395H	e 1174	21197	085541	400 591	99540	94001	~1545
101037 +38 234+114537 54768	a 16aa	21206	n#5201	481771	995521	00152	c151+
06163N + 3H 244+1145364 5576H	6 14 n 4	1221	044811	415431	445661	0.0222	cinnis
DE1042 + 36 402+1145201 5304Y	0 1284	21210	045611	-95451	977901	025477	01050
TL1943 + 3H 439+1145373 5440Y	5 0au	61583	645191	44/001	196261	0.1163	21233
061040 +30 563+1146335635001	1 1114	91215	685101	461325	00033	99331	71244
DL1047 + 30 50 3+1145437540591	5 931	51208	n#3611	1952245	00035	99473	01125
DL1043 + 58 614+1145 594 55134	0 001	21965	634151	44.1247	0.010c	34450	61125
わとすらにす ふえん いりするすく とくかり ちんようか	- e - 1 /i e u	230104		14 B 14 B 1	N 67 2 N 6	たびさせん	14 T 4 1 1 4

1

1

.

1

.

.....

1 FN-TR-33-DL DRY LAKE VALLEY GRAVITY STATIONS A2-17

STATION LAT. LONG. ELEV. Ident, deg min deg min +code	TFR-0 TN/	OR. MORTH	E A S T U T M	URSV GRAV	THEC GRAV	¥ да 4	C 156 1666
		~~~~~~				*****	
DI 1052 +38 743+1105457 55060	0	130/221/11	AR 325	47955	200296	138644	61194
DL1053 +38 715+11/55/0 55-20	0	101422987	662341	117772	200255	99862	82493
0L1054 +374509+1143837 53934	ġ	120418006	707961	40/03	197032	100492	82215
DL1055 +374504+1143989 58154	0	509418051	70573	44000	197024	102312	62738
DL1055 +374540+1144286 4935Y	0	148418107	701301	150419	197077	99785	83101
DL1057 +374515+1144401 46764	Ú.	112418057	n9965	151361	197041	98546	85203
DL1058 +374527+1144491 46400	6	97418076	090351	15(108)	197058	9671c	60987
= 01.1059 + 374586 + 1100489 + 46500	0	94418185	698351	44410	197144	96513	80757
DI 1060 + 574540+1144414 46474	e	102414145	- 099995 - 700821	51400	197150	97719	-01441 2024
DI 1062 +374501+1144320 4/014 DI 1062 +374563+1400159 56219		252018150	703211	146090 146090	197100	101882	02960
DL1063 +374576+1144077 54414	ν ά	128418181	704411	47012	1971361	101090	82001
DL1064 +374592+1143963 5466Y	0	129418215	706071	47055	197153	101345	62831
DL1065 +374568+1143698 5301Y	n N	125418173	707191	47447	19711e	100218	62203
DL1066 +374576+1143792 5421Y	. ()	118418192	708591	48593	1971301	100482	e2111
DL1067 +374619+1143053 52581	i)	132418269	707681	47/10	197192	100008	45501
0L1068 +374696+1143763 5416Y	0	142418415	708961	47649	197305	101310	05490
DL1069 +374713+1143880 52739	0	167418442	701241	48141	147530	00437	シアウビリ
	0	123418403	- 795761 - <b>7</b> 54461	140120	1972591	100320	88052) 88052
DETUTE + 374603+1144073 57211	0	244418276	763471	46474	1972011	101767	22315
DL1073 + 374620 + 1144230 + 9288	Ó	140418257	102051	56541	197194	99724	+3155
DL1074 +374637+1144279 48370	Ğ	122418287	701411	51196	197219	99210	62943
DL1075 +374042+1144318 47950	0	109418295	700841	51088	055761	94988	82743
DL1076 +374646+1144345 47730	()	105418301	700441	151058	197232	98745	12571
DL1077 +374648+1144372 47440	0	107418304	100041	156420	197234	04337	25503
DL1078 +374652+1144304 47230	0	98418310	e9960'	150700	197241	97913	-1405
DL1079 +374660+1144424 46949	0	98418324	69928	[50457	197252	97360	01400
011080 + 574660+1144458 40710 011081 + 774661+146 44985 40710	. 0	93419323	- 04575 0830	150111	197256	90017	80979
	. ()	92418324	- 04030 - 70297	1447733	10/204	90449	-04070
	· 0	-137418458 -513418458	78193	146902	197353	130596	02014
DL1084 + 374735 + 1144354 + 47440	0 0	101418465	70027	150954	197362	94238	82158
DL1085 +374745+1144439 46704	n n	93412421	60902	150123	197370	96640	1000
DL1085 +374749+1, 10079 5031Y	0	118418501	70430	49886	147342	99851	02810
DL1087 +374789+1104156 4964Y	<u>(</u>	107418572	70315	150020	197491	99236	8247 <i>2</i>
DL1088 +374782+1143764 54901	0	174418574	7:091	47392	197430	101632	93041
DL1089 +374798+1113828 63694	0	862419601	707961	141998	197453	103590	62729
011090 +274861+1144755 38704 011001 x 27/1971x1407405 50005	ר ביות ביו ביות ביו	195413720	70905	143196	1975-05	してないし、	5.14/5
DL1092 +3747789+11, 2957 5130	C2C	-220414735	100071	149275	197300	199114	N2115
0L1093 +374859+11/13945 51964	· · · ·	155418704	700101	44974	1475421	100114	12704
DL1094 +374810+1144076 4987Y	0	119418614	704311	150022	147471	99484	-2574
061095 +374583+1100071 4967Y	n.	122418749	714351	40196	197571	99150	02250
DL1096 +374931+1143751 56424	38	254418850	7 3 9 0 3 1	+0005	147nun	102457	131 m
DL1097 +374950+1107852 54171	a	212412481	707541	147047	97575	101190	15000
DL1100 +375120+1144760 57721	Ú.	500110100	708811	145949	147923	102310	45013
011101 + 5/5126+1107/85 5724Y	4	255414234	7 1**/44	46125	1979321	しいど 1 11月 -	P2P31
		275419636	1 1 7 7 7 7	1403/5	1 2015-01	NUTION NUTICE	20115
011104 +3751654114		231212220	10/211	147:22	147424	121514	ションシュ
PU1105 +375191+1142892 54944	(	218419507	TINAL	41450	1486131	1011344	-2011
0L1100 +375195+1103921 5444Y	()	204419532	7 1041	147042	1980331	17144	22AAU
061107 +375200+1143944 51674	់ ត	210414255	700071	14+47E	198052	100913	-2-41
DL1108 +375224+11 13465 53/34	õ	197419384	105751	144314	148076	100871	H0115
061109 +3/5234+1143902 52211	0	191417401	105151	hat this	14में में में	100055	1.71.24
(1) まちをかった 生きに 3 ほうしょう しんかうしょう	•	4.1. EXPERIMENT	<b>7</b> (1) (1) (1) (1)	i chi 7 ann	e a e su s	1 A. A. 1 A. 7	

FN-TR-33-DL BRY LAKE VALLEY GRAVITY STATIONS

1

ŧ

į

1

÷

A2-18

STATION LAT. LONG. ELEV. T	FR-rin.	LORTH	FAST 0	ASV	THE	r 14	CAA
IDENT, DEG MIN DEG MIN +CODE	TNADUT	UTM	HIM G	QAV.	GRAN	•	1.00
						-	•
DE1111 +375131+1103870 55274	0 222	419215	7071914	72 431	979401	01310	82-81
PL1112 + 375120 + 1103951 - 53339	0 186	419192	70-0114	102491	974241	00610	82571
DI 1113 + 375167+11/2989 52804	0 181	110278	7054314	8/9-11	470421	16490	82.502
DL1114 +375195+1100088 51064	0 150	419326	7039014	92531	48677	29272	2000
DI 1115 +375138+1100059 5136V	0 107	1419221	703314	96251	97951	00101	52720
011116 + 375083 + 1100050 - 51007	0 1/1/1	410120	7045110	92221	9747 -	0941-2	A213A
D11117 + 375012 + 1104033 5072	0 144	/114980	7048516	911341	97160	99004	RISHO
DE1115 +374010+1+44032 50964	0 130	418802	7053514	90321	97612	00175	221622
n 1119 + 37/081+11/2002 5257V	0 1.37	11997-	7065014		07700	00976	02120
DE1120 +375052+11/3951 52597	0 181	119066	7060414	82811	97024	19950	N2194
DE1121 +375229+1140257 49196	0 127	41938	7019115	05161	GRORX	UH720	52174
$\frac{1}{1134} + 275000 + 11000000 + 46385$	6 113	110327	6969715	090/1		04511	52310 56360
DI 1124 437519/41144420 40200	0 112	110315	7008715	09141	90041	90311	61514
DI 1135 +375103+1100215 /6678	0 133	110236	7021215	1.4 H K I	07057	04617	43477
$\hat{D}$	0 122	414223	7027115	( <b>3</b> ) ( • )	07648	09507	42000
DE 1137 - 4770664414577 - 47711	0 172	1412800	7020515	00010 <u>1</u> 000504	77090 07605		81.50
DI1128 + 374874+1484178 - 40271	0 463	110720	7027515	62671	97560	000000	82 (63
	0 100	469167	7029115	002071	17671	0256.	83155
B(1170 + 775) = 0.000 + 1000 + 7500 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 + 0.0000 +	0 113	418968	7018515	07891	07789	08370	66130
DI1131 +375041+1144237 40211	0 120	110110	7019315	ati74	97866	98788 38788	62006
$\frac{1}{1} = \frac{1}{1} = \frac{1}$	0 104	112157	7106615	01076	97900 9790n	40100 47678	41642
$\frac{1}{1133} + \frac{1}{375137} + \frac{1}{1100} + \frac{1}{100} +$	0 L00	ULOZNA		11521	97900 97905	97070	11 J J 12
$n_{1132} + 275147 + 1144271 - 40067$	0 100	110200	- 177777 - 6960315	111111	07963	97115 95560	80247
$\frac{1}{11115} + \frac{1}{15} + \frac{1}{1$	0 101	/101/17	6995715	10201	97821	071HQ	HIZUN
DE1135 +375059+1104502 46250	0 401	419047	6950815	(12271	97536	Un117	85041
DI 1137 +374975+118/44415 446527	0 90	412906	- 5978115 - 5978115	0 - 261	47712	96596	N0921
D(1133 + 370995 + 1100373 + 47277)		418947	2004515	09469	97741	97660	alaat
D[1139 + 374952 + 1 + a/325 + 47369]	0 100	418067	70.)4515	64751	97578	97764	81716
D(1)40 + 374875 + 1144280 4866Y	21 100	413727	7012915	012241	97560	-9884N	52368
DL1141 + 374875 + 1144391 + 46967	1 96	419724	-097ee15	0.57.51	9756b	97503	01056
DE1142 +374824+1100403 46964	0 95	418028	6995115	07591	97491	37471	81550
DL1145 +374917+1144447 46480	6 95	419799	0938215	66401	37627	96760	81402
DL1144 +374805+1100201 4854Y	0 10	412597	7011015	645.11	97464	03979	02397
PL1145 + 374508+1145335 51111	0 167	418012	6-59-514	69521	976301	المرشم ما 0 0	82757
DL1140 +374575+1145427 5305Y	0 218	418133	0845914	76401	971261	00645	3,27 - 3
DL1147 +374587+1145287 50715	0 135	418160	0806414	92401	97145	99018	02050
DL1148 +374030+1145347 51583	0 169	412248	6857414	89251	972171	99249	62625
DL1149 +374662+1145403 55013	0 184	418694	0249014	65431	012551	01000	82451
DL1150 +374044+1105463 58105	0 631	114259	6840314	39131	912241	ation	N1750
DL1151 +374091+1145277 51285	0 1 10	418352	0407414	80741	91290	99841	NAHI
DL1152 +374741+1:45368 50483	0 207	418444	n402014	40251	47376	497-2	1215-
061153 +374745+1145427 59155	0 330	418447	5845214	47221	973701	13000	1417A
DL1154 +374706+1105524 62865	0 395	418372	n# 51114	10551	473211	18294	N2455
DL1155 +374771+1105539 67085	0 844	41HUN2	n-chats	1.1.1.1.1	472161	Core	rloni
DL1150 + 3748 31+1145480 57355	0 211	418504	0030114	5-24-61	4750.1	otorr	12518
061157 +374819+1145368 53458	0 150	412546	0053114	1-2-51	474441	10345	2011
DL1158 +3/4871+1105317 50108	0 145	418684	bondel +	4-9-41	97500	49447	.2545
0L1159 +374904+1145 126 52143	1) 171	418741	A#44014	A43+1	976301	104.2	1.27 G (L
DL1160 +374930+1145521 53005	n 160	418777	118 34014	0-151	110551	1454	*2425
FL1161 +374075+1105001 56023	6 242	414082	+ - 1911 +	N 341 1	+75551	1122	Sec.4.
DL1163 +375000+11 15952 59618	61 183	J18915	nershia	t thnt	477481	1:5:5	-2017
RL1164 +374971+1165425 51900	0 154	412765	n844514	917-11	77776.1	.4314	reinn
061165 + \$75023+1145307 51714	0 134	118425	6148414	44+41	11742	4124 24	112 4-4-4
DL1100 +375038+1105328 50764	6 121	a12492	005851-	9-4-4-21	97504	9944	~225e
DL1167 +3/5055+1195259 49523	0 115	41902n	0008515	03301	47824	22347	02314
DI 1160 + 375053+1145485 57 413	0 1 7 7	110015	- H 3571 -	55514	47-201	21041	12222
わしますんね えきちんかんたい とたみ シスタイカン		, 1 e	• • • • •	$C_{1,2}(C_{1,2}, \varepsilon, \varepsilon, \varepsilon)$	e. 1	· · ·	

7.

FN-TR-33-DL DRY LAKE VALLEY GRAVITY STATICINS

A2-19

STATION LAT LENC FL		118 SHOTH	EAST (055)	THER' FAS	~ + 5
TRENT DEC MIN DEC MIN		цока сонско. ОППТ ПТТИ	LITH COAV	ten Sterrer a	
IDEN, DED BIN GED MIN 4			UTH DRAV	13° 47 1	1001
			0.000 B		
UL1170 +375109+1145457	547AS 0	149410119	585921414041	97906101112	62577
DL1171 +375104+1145322	54045 0	201419115	685911471461	97900100107	610/0
DL1172 +375160+1145371 5	54225 0	144419210	645101474401	97982100495	02:40
DL1173 +375169+1145262	5069S 0	117419237	000701501201	97995 99836	05004
011174 +375220+1145342	51895 0	153419328	CR5551469971	98070 99767	65555
DL1175 +375199+1195444 5	56178 0	162419286	6H +0H1465771	98039101403	67467
DL1176 +375212+1145522	5622S 0	55941930H	082931455421	94024102274	02047
DL1177 +375147+1145521 5	5668S 0	200419187	n#2971455751	97965100957	81825
DL1178 +375217+1145597	5917S 01	207419314	081831364611	48665103501	01115
DL1179 +375119+1145627 (	5028 236	554410132	081431390241	97922103099	01712
DL1180 +375033+1145042	5448S (	691414973	081241398271	97797103190	5171d
DL1181 +374949+1145312	50295 1	121418828	686121497871	97674 99443	62413
061913 +38 505+1145000 5	51416 0	111421713	680711509491	99945 99363	01459
DL1914 +38 640+11448925	0951T 0	92021970	091551499372	00145 97741	P6455
DL1918 +375417+1144743	46528 0	90419/13	69426150r 521	98357 96054	80277
DL1919 + 374203+11450374	7520T 0	03417458	690471493991	96565 97535	61425
061961 +374525+1144084	45300 0	87418065	095521495221	97055 95568	006.54
PL2000 + 574595+1144984 4	464400 0	94418185	h*1001303621	9/15/ 96909	01103
DL2001 + 574598+1145011 4	HACKY O	474141A9	0-30(60-33)	91152 91245	01420
	400341 () 0774129 0	101418190	093291300031	97355 97521	-01040 
	47151 U	100410177	009901300211	97100 97027	- C ( D 4 C -
		100410177	- 801-110-20011 - 807-2012-2011	91155 903:4	- 202121 - 2021
DI 2000 - 17705031100178 -		1124131/3	F # # 3 4 4 4 6 # 7 6 4 6 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1/100 90100 9/100 90103	22412
	⇒⊂/51 U 901-9V .	141919178	- 000241430031 	9/100 90000	-02010 
	4~101 U	136413165	667031470261	971/0 98762	22222
- DE2009 +374307+1185636 -		120413102	6674414744721	97100 99030	588228 52472
	50100 (C	177/18157	6870324743221	9714/ 494 13	82710
012010 + 374585414ac438		1/0/1015/	685891456851	97143100132	62770
- Dt 2012 +37458341446345 (	5211V C	170/19150	685491483761	97140100266	22.56
$= \frac{1}{1} \frac{1}{2} $	52665 0	175/14152	684951479891	9714310059/	82746
012060 + 373975 + 1105809	5200V 0	283417008	677891470531	96253100304	02545
012060 + 374060 + 1145930 + 1	55528 a	347/17164	677411453731	962321642 5	12559
DI 2062 +374127+1+//5951 5	56836 0	2/18/117286	677511407021	96475101/13	82578
DL2063 + 374190+11/15916	5496 0	240417405	077531450251	90560101499	52313
DL2064 +374360+1105506	5545Y 0	230417732	663441462291	96614101661	82916
0L2065 +374272+1145324	50670 a	158417570	645221465911	90000 9407r	02085
DL2060 + 375864+11/4450	47545 0	115420550	698751496481	90211 95472	19337
NL2067 +375852+1144427	170n5 0	117420529	59-741440141	GA443 95474	79335
DL2068 +375839+1144402	47735 0	121420506	6440/1446:31	48974 45547	79359
DL2069 +375427+1144381 4	47755 0	120426484	044301490021	44440 14021	79483
DL2070 +375813+1144357 :	17401 1	127420459	099741497011	92430 45910	10-04
DL2071 +375730+1144310	48320 0	130420418	70.351499021	48908 48533	01104
062072 +375779+1100200	1406C 0	130400308	700001444021	AAAAA AEC75	MG214
062073 +375760+1144272 -	+900C 0	141420575	7-110-1444711	ANNA 47217	46 4,60
0L2074 +375754+1144250 4	49320 1	140420354	7-13515-01/1	94650 97577	2002
0L2075 +375742+1144224 -	19620 0	154420332	701551500001	96632 27411	51:41
PL2070 +375716+1144182 5	50200 4	144420285	102351566721	98795 98721	A1284
0L2077 + 575704+1144150 7	5073C ···	6114-0265	7-26/1500001	4×77/ 44648	11441
DL2078 +375691+1141137 5	5164C E	021460241	1-58-1490101	4475- 4945H	02172
DL2222 +36 741+1113770 4	534AY 0	c2+422197	1419-141-1978	00294192022	Man7
PL3001 +373951+1143210 5	3013 1	153417058	717331465631	462111 10754	10004
01 3002 + 374 31 d+ 114 3457 +	97248 1rt	471417/16	713041340751	44745135214	02420
DL3003 +374715+1143314 /	51375 251	234318467	715541430271	97338153154	-5-12
DL 3004 +374990+1143344 /	57785 /	581415974	714971396201	477341050M2	12555
NL 4000 + 375587+1123934 /	5444Y <b>5</b>	544420656	70-56-14112-1	95635133171	n1 : 62
へい ていのブ ショブメビルブイルイト・ウェッシー		a second same	17 19 1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Care State Students	

1/m

FN-TR-33-DL DRY LAKE VALLEY GRAVITY DATA 

....

**N** 

The second se

1

1

• • • •

STATIO	N LAT.	LUNG. F	LEV.	TF 10 + (	TOR. DARTH	FAST URS	V THEC	FAA	254
IDENT.	DEG MIN	DEG MIN	+CODE	T (4)	VOUT UTM	UTM - GRA	V		+ : + + + + + + + + + + + + + + + + + +
				40 AV 74 -		~~~~~~			
DL 30 0 8	+38 277+	11/13657	77785	2	971421343	707715329	571996151	105850	81301
DL 30 19	+38 691+	11/3650	01555	, i	201422109	709671444	39200220	11144	80 (53
013010	+38 7/1+	1107706	50485	0	15/1/20100	705831464	522452071	1 1 1 1 2 1	00107
	- 734 7914	1 44 5160	- 87 TV	0	134468174	704741301			40150 <b>1</b>
	+ 30 10/04	1144005	17777	~	445462715	- 70* 301 3710	77780711	03174	00104
013014	+ 58 704+	1145740	53111	0	46422058	0/02114//	11209234	48147	741.99
DL 3015	+38 409+	1145464	5// 54	8	129421523	5852514620	414480E	100815	61262
DL 3016	+375996+	1145497	00595	115	318420758	6829714419	261992041	101980	81747
nl 3017	+375701+	1145334	57028	16	174420218	085451463	711987731	101263	82005
DL 3018	+375612+	1145657	52828	1	159450043	680791486	94198642	99574	81755
DL 3019	+375350+	1145561	06005	313	709419562	542301387	47198259	103172	01479
OL3021	+374846+	1145751	58088	7	164418023	079721445	151975231	101755	01155
DL3022	+374434+	1145661	05905	413	579417864	661211383	181969231	103422	01737
DL 3025	+374011+	1145712	69555	2821	130417080	6606313502	291963051	04187	61877
DL 3024	+374260+	11/15915	55335	249	169417534	677531450	201960691	101272	82601
DL 3025	+ 37 38 33+	115 25	4988Y	0	122416741	670101405	14196046	99207	82410
DI 3500	+ 375522+	1100277	4707N		178/11092/	701041513	80162511	47100	81291
DL 3501	17765331	1144611			170419724	701041515		77100	41201
003301	- T 31 - 5777	1144511	47075	G o	110414-54	- 74110419194		071115	61301
013306	+5/0022+	1144277	47073	9	1/8014454	701041313	99195311	97169	01311
963503	+512522+	1144270	47088	Q	118410450	701061514	12148511	97201	01201
0_3504	+375522+	1140276	47098	n N	178419924	701061514	00198511	97269	81367
DL 3505	+375522+	1144275	47098	0	179419924	701071514	11198511	91220	5133
0L 3506	+375522+	1144275	4710H	Ģ	179419924	701071514	15198511	61535	61345
DL 3507	+375521+	1144275	47116	0	179419922	701071514	17198509	97242	81353
DL3508	+375521+	110/270	47128	n	180419922	701091514	22193509	97255	61355
DL 3509	+375521+	11/1/274	47138	Ú)	180419955	701091514	22198509	07204	61570
0L3510	+375521+	1144273	47133	()	180419922	701101514	20196509	97274	F1374
DL 3511	+375521+	1144273	47144	ę	179419922	701101514	20104500	07283	01304
DL 3512	+375521+	1144273	47158	Ó	179414922	701101514	31198509	97293	51546
DL 3513	+ 375521+	1144272	47158	0	181419922	761121514	37198509	47502	81401
DL 3514	+375521+	11 1/272	4716B	0	181419922	701121514	39193509	47 51	51.465
01 4515	+375521+	11/1/271	47179	 م	180010922	701131514	3-144504	97320	01-1-
DL 3516	+ 375521+	11/1/1271	47198	0	185010422	701131514	41198509	97332	ntude
013517	+ 475520+	1100271	47100	0	170/110920	701141510	46198508	01302	A 1
DI 45 ( A	-+3723294 -+7756474	1 4 4 4 25 7	47040	()	190419720	7.16.151515		17607	
01.3510	- 7 37 33177	11/10277	- 4707JC	0	10.4414.11	- 701241213	33404-000 20130303	71012	- <b></b>
	+ 3/ 7 7 1 4 4	11/14/44	41424	()	1*2419410	701001012	1130433	91019	
11L 3029	+ 1 / 2 2 1 1 +	11442 51	48214	Q	188419905	7.1721511	33190493	48134	01042
01.3521	+ 5/5508+	1144218	48878	0	190413900	701411517	55144441	98343	r1445
PL 3522	+3/55-15+	1141205	49651	0	215419095	762111505	12190486	04,224	r 2 , 4 L
DE 3523	+375502+	1140102	4455	ų	532419496	/0c301505	59193451	Santo	05144
PL 3524	+375522+	1144270	470nt	0	177419624	101031513	56193511	97121	M1275
01.3525	+375522+	1144873	47060	0	125410451	701031513	73196511	971 19	P1275
PL 3524	+375522+	1111279	47050	- ú	171419424	701011513	0*198511	471 Sr	01200
01.3527	+375522+	110/279	47056	0	177419924	701011515	NC198511	07120	e1:56
PL 3528	+315523+	1142779	471 an	`	178410925	701011515	53194513	47113	elete
PL 3529	+ 375523+	1104680	47644	ζ,	176419925	7010(1515	44148513	67115	71231
063530	+ 375523+	1144286	47. 315	٥	176419925	701(01513	30148513	11089	olees
DL 35 71	+ 375523+	1111241			175419925	704951515	51198515	47679	01215
DL 3572	+ 274427+	1100281	17.24		175110125	7.10901515	22104516	774++	41 P 11 P
11 35 22	+ 275% > 2+	11/2201	u7:58	2	175410435	700961516	17198516	27 15-	
01 55 70	4 2/51.34	11.00000	47.24		175010926	70.471610	1727-012 3569-014-61-6	· · · · · · · ·	1173
11 26 96	・ ディンスペンプ ・ A 7 7 6 1. 3 4 +	1.14626			- 4 イカイ 4 イイクラー - 4 カビバイム・3 カビー	- 7 · · · 7 / 1 2 · 1 · - 7 / 10 / 1 · · ·	()) ()) ()) ()) () () () () () () () () () () () ()	1. 7 . 3 P	
PE 25 * 3	- デスト ひつくろく			۱	1 1 1 1 1 1 1 1 7 <b>7</b> 5	- 712 ( <b>7</b> 771016) - 276 (01 - 71016)	78179213 311779117	· · · · · · · ·	
1 6 37 50	* * * * * * *	114645			114414425	100001012	21222212	47919	01159
01 11 - 1	* 5/ 7 7 7 5 *	1114685	47104	n	174419925	1009515160	-414/515	4/11/	<b>D115</b> 6
1.5574	+ 575524+	1146283	47964	1P	174419727	744951512	11-98513	49.944	n 1 1 5 4
01.5539	+ 375524+	1144584	44344	( i	174412427	700941512	(1194515	0 <b>0</b> 984	21120
01 3540	+ 675524+	1143284	46991	C.	174114427	7-16941516	56198513	4.475	01121
P ( 7 ) (		1 1 1 1 m 1	1994 - A 🕈 A -	100	17.001/01/20	1993 11 1 L I .	at the constraint	1. 1. 1. 1. 1.	• • • • *

FN-TR-33-DL ORY LARE VALLEY GRAVITY DATA

Î

STATION LAT. LONG.	ELEV. TER	-COK . WORTH	FAST URSV	THEC	FAA	CB4
IDENT, DEG MIN DEG MI	A +CULE I:	WILL UTM	UIM GRAV	is the d		+1000
		*********	~~~~			
DL3542 +375530+114421	) 46768 (	346419941	70202150881	193523	95363	80766
DL3543 +375533+114432	46726 (	195919945	705 50644	198527	46681	80310
DL 3544 +375536+114433	7 46715 (	152419947	70.11.50417	198531	95042	84604
DL3545 +375539+114435	J 46728 (	) 145419953	69997150220	198530	45051	7986c
RL3546 +375542+110436	3 4673P (	1/12419958	09977150003	198540	95502	79705
DL3547 +375530+114427	6 4707B (	170419939	70105151377	198523	97153	01277
DL3548 +375530+114/127	5 4708B (	179419939	70105151581	198523	97107	51287
DL3549 +375529+110027	5 47098 (	180419937	70107151334	198521	97151	11299
DL3550 +375529+114427	5 47108 (	180419937	70107151337	198521	97191	81300
DL3551 +375529+114427	5 47118 (	180419937	70107151391	198521	97203	01310
DL3552 +375529+114427	47113 (	182419937	70108151397	198521	97214	81327
PL3553 +375529+114427	47128 (	181419937	70108151400	198521	67225	81334
DL3554 +375529+114427	3 47128 (	181419937	70110151409	198521	97232	81342
0L3555 +375529+11/427	3 47138 (	) 18/410937	70110151409	198521	97244	81344
DL3556 +375529+114427	3 47148 . (	181419937	70110151414	198521	97256	61359
DL3557 +375529+114427	2 47158 (	182419937	70111151416	198521	97000	01307
DL3558 +375530+114427	7 47078 (	1 170419939	70104151372	198523	97142	81258
DL3559 +375530+114427	7 47065	180419939	70104151369	198523	97133	61262
DL 3560 +375530+114427	7 47058 (	180419939	70104151363	198523	97121	81253
DL3561 +375530+114427	8 47054 (	178419938	70102151256	194523	9711c	81241
DL3562 +375530+114427	47048 C	178419938	70102151347	198523	97098	61230
DL 3563 +375530+114427	9 47446 (	179419934	70101151341	198523	97085	61221
DL 3564 +375530+114427	3 47638 (	179419938	70101151336	198525	97473	01211
DL3565 +375530+114427	9 4702H C	179419938	70101151529	198523	97061	81202
DL3566 + 375530+114428	) 4702A C	177419938	70039151521	198523	97051	61140
DI 7547 17755711110020	1 17:22	170,1109,10	7603315131	104520	07077	61170

G1.0

× ...

.

STREET, JUL

GROUND-WATER APPRAISAL OF DRY LAKE AND DELAMAR VALLEYS, LINCOLN COUNTY, NEVADA **K**1

### GROUND-WATER RESOURCES - RECONNAISSANCE SERIES

Report 16

# GROUND-WATER APPRAISAL OF DRY LAKE AND DELAMAR VALLEYS,

Lincoln County, Nevada

Ъу

Thomas E. Eakin

Prepared cooperatively by the

Geological Survey

U. S. Department of the Interior

May 1963

### FOREWORD

This is the 16th report in the series of reconnaissance ground-water studies which were initiated by action of the Legislature in 1960. In these sixteen reports, the ground-water resources of some nineteen valleys have been appraised and described.

The present appraisal of the ground-water resources of Dry Lake and Delamar Valleys in Lincoln County, Nevada, was made by Thomas E. Eakin, geologist, U. S. Geological Survey.

These reconnaissance ground-water resources studies make available pertinent information of great value to many State and Federal agencies. As development takes place in any area, demands for more detailed information will arise and studies to supply such information will be undertaken. In the meantime these reconnaissance type studies are timely and adequately meet the immediate needs for information on the ground-water resources of the areas on which reports are prepared.

Hugh A. Shamberger Director Department of Conservation and Natural Resources

May, 1963

### CONTENTS

Page

Summary	1
Introduction	1
Location and general features	2 <-́
Climate	3
Physiography and drainage	8 <
General geology	9 <
Water-bearing properties of the rocks	0 \
Ground-water appraisal	1
Occurrence of ground water	1 🗧
Estimated average annual recharge	5
Estimated average annual discharge	8
Perennial yield	8
Ground water in storage	0
Chemical quality	0
Development	1
Designation of wells	2
References cited • • • • • • • • • • • • • • • • • • •	4
List of previously published reports	6
# **ILLUSTRATIONS**

a characteristics

7 -

Page

Figure	1.	Map of Nevada showing areas described in previous reports of the Ground-Water Reconnaissance Series and in this report	following p. 2
	2.	Sketch map showing relation of Dry Lake and Delamar Valleys to adjacent areas	following p. 3
Plate	1.	Map of Dry Lake and Delamar Valleys, Lincoln County, Nevada showing areas of bedrock, valley fill, and location of wells	pock <b>et</b>
Photo	1.	View of stock wells 3N/65-21d32 and 21d4 in Dry Lake Valley	cover
	2.	View of stock pond in Delamar playa	insid <b>e</b> c'over
	3.	View of stone cabin at Bristol Wells	following p. 12
	4.	View of Delamar	- 11

# TABLES

Table	1.	Summary of precipitation at Alamo, Caliente, and Pioche, Nevada
	2.	Average monthly and annual temperature, in degrees Fahrenheit, at Alamo, Caliente, and Pioche, Nev. for the period 1931-60 5
	3.	Total evaporation at Caliente, Nev. (1956-61) 7
	4.	Estimated average annual ground-water recharge from precipitation in Dry Lake and Delamar Valleys, Nev
	5.	Records of selected wells in Dry Lake and Delamar Valleys, Lincoln County, Nev 23

# GROUND-WATER APPRAISAL OF DRY LAKE AND DELAMAR VALLEYS,

## LINCOLN COUNTY, NEVADA

by Thomas E. Eakin

****

## SUMMARY

The results of this reconnaissance of Dry Lake and Delamar Valleys suggest that average annual ground-water recharge from precipitation may be on the order of 6,000 acre-feet. Ground water is discharged largely by undernow through bedrock from the valleys, most probably to the southwest or south oward Pahranagat Valley.

The substantial depth to water, in excess of 300 feet in the topographically ower parts of the valleys, precludes low-cost development of substantial supplies of ground water. However, this apparently adverse feature for usual watersupply purposes may be desirable from the standpoint of possible special testing purposes required in modern technology.

The area roughly including Tps. 1 S. to 2 N., R. 64 E. may be most favorable for eventual interception of most of the recharge which is principally supplied from the mountains to the east and north. Here, perennial yield might closely approach the average annual recharge. It should be pointed out, however, that the depth to water, ranging from about 400 feet to 700 feet or more, probably precludes development of substantial water supplies for most purposes because of the high cost of pumping.

## INTRODUCTION

Ground-water development in Nevada has shown a substantial increase in recent years. Part of the increased development is due to the effort to bring new land into cultivation, part is due to the effort to supplement surface-water supplies, and part is due to the general increased demands for water. In any case, as efforts to develop ground water increase, there is a corresponding increase in demand for information on the ground-water resources throughout the State.

Recognizing this need, the State Legislature enacted special legislation (Chapt. 181, Stats. 1960) for beginning a series of reconnaissance studies of the ^{round}-water resources of Nevada. As provided in the legislation, these studies are being made by the U. S. Geological Survey in cooperation with the Nevada Department of Conservation and Natural Resources.

Interest in ground-water resources currently includes many areas and s extending to additional areas almost continuously. Thus, the emphasis of the econnaissance studies is to provide as quickly as possible a general appraisal f the ground-water resources in particular valleys or areas where information s urgently needed. Ultimately, ground-water information will be available for ractically all valleys of the State, at least at a reconnaissance level. For this eason each study is limited severely in time, field work for each area generally veraging about two weeks.

The Department of Conservation and Natural Resources has established special report series to expedite publication of the results of the reconnaisance studies. Figure 1 shows the areas for which reports have been published In this series. A list of the titles of previous reports published in the series s given at the end of this report. This report is the sixteenth in the Reconnaisance Series.

The purpose of the Reconnaissance Series is to provide a general appraisal of the ground-water resources of virtually all valleys of the State for public information, and to provide a preliminary estimate of the amount of round-water development that the areas might sustain on a perennial basis as in initial guide to possible requirements for administration of the areas under he State ground-water law.

The scope of this report is limited to a general description of the physical conditions of Dry Lake and Delamar Valleys, including observations of the interrelation of climate, geology, and hydrology as they affect ground-water resources; and possible movement of ground water between valleys is discussed. The report also includes a preliminary estimate of the average annual recharge o and discharge from the ground-water reservoir.

## Location and General Features:

h

Dry Lake and Delamar Valleys are in central Lincoln County and lie within an area bounded by lat 37° 15' and 38° 28' N., and long 114° 33' and 115° W. The two valleys occupy a north-trending trough which is about 82 miles long and a maximum of about 20 miles wide between drainage divides. The combined area of the two valleys is nearly 1,300 square miles.

U. S. Highway 93 crosses the area in an eastward alinement about at the divide between Dry Lake Valley on the north and Delamar Valley on the south (fig. 2). Caliente lies along the highway about 20 miles east of the area.

A gravel road extends southward from U.S. Highway 93 to the former mining town of Delamar. State Highway 83 and improved roads connect formerly active mines on the western side of the Bristol Range with U.S. Highway 93 to the cast in the vicinity of Pioche. Trails provide limited access to the lower parts of the valleys during fair weather.

The valleys are used principally for livestock range, although full use of " area may be somewhat limited by inade uate distribution of permanent forting points.



SERIES AND IN THIS REPORT.

## Climate:

The climate of Dry Lake and Delamar Valleys is semi-arid. Precipitation and humidity generally are low, and summer temperatures and evaporation rates are high. Precipitation is irregularly distributed but generally is least on the valley floor and greatest in the mountains. Snow is common during the winter months and localized thundershowers provide much of the summer precipitation. The daily and seasonal temperature range is relatively large.

Records of precipitation are not available for Dry Lake and Delamar Valleys. However, the magnitude and distribution of precipitation in parts of the valleys probably are reasonably represented by the records for Alamo in Pahranagat Valley west of Delamar, and for Caliente and Pioche to the east (fig. 2). Table 1 lists the annual and the average monthly and average annual precipitation at Alamo, Caliente, and Pioche.

Maximum annual precipitation, in inches, during the period 1931-60 for Alamo, Caliente, and Fioche was 14.91 (1941), 18.73 (1941) and 22.38 (1941), respectively. Maximum monthly precipitation, in inches, for the same period was 6.15 (August 1945), 4.29 (October 1946), and 5.01 (August 1945), respectively. Minimum annual precipitation, in inches, for the respective stations was 1.23 (1956), 2.92 (1950), and 3.81 (1956). Minimum monthly precipitation has been zero a number of times at each of the stations.

Table 2 lists average monthly and annual temperature for the period 1931-60 at Alamo and Caliente and for the period 1939-60 at Pioche. Maximum and minimum temperatures recorded are: at Alamo,  $115^{\circ}$  F. on August 11, 1940, and  $-9^{\circ}$ F. on January 21, 1937; at Caliente, 109°F. on June 22, 1948, and  $-31^{\circ}$ F. on January 9, 1937; and at Pioche,  $102^{\circ}$ F. on June 22, 1954 and  $-5^{\circ}$ F. on January 4, 1949.



••.

	<b>9</b>													
	A Tabl	e 1	- <u>Summ</u> (fi	ary of rom pu	precip Iblishe	d reco	n at A ords c	lamo, of the	Cali U.S.	ente, a Weathe	r Bur	oche, 2 eau)	Nev.	
	-	AVC	i age n	1011111			proci	Preder	<u>, , , , , , , , , , , , , , , , , , , </u>			1		
		Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Ala	no	.70	.68	.68	. 57	.45	.15	.73	.77	. 32	. 43	.43	.60	6.60
Cal	ente	.83	.79	.85	.70	. 56	.39	.76	• 92	.49	. 89	.75	. 86	8.79
Pic Pic		1.55	1.26	1.46	1.19	.83	.33	.87	1.12	.69	1.18	.96	1.36	12.80

Average for 1939-60.

And the state of the

# Annual precipitation, in inches, (1931-61)

jé or	Alamo	Caliente	Pioche	Year	Alamo	Caliente	Pioche
221	9.60	9.49		1947		7.47	10.70
17:2	9.68	11.61		1948	2.75	5.23	8.39
	7.29	8.16		1949	6.09	10.03	15.36
1934	3.01	7.14		1950	5.32	2.92	7.14
1735	5.58	9.43		1951	4.89	10,15	13.98
فر شقو	8.97	11.60		1952	6.88	11.52	16.32
1037	6.30	6.84		1953	1.98	4.66	7.26
1937	11.15			1954	5.96	9.31	13.28
132	7.42	9.41	10.05	1955	5.65	7.13	14.09
(04)	6.16	7.49	13.48	1956	1.23	4.78	3.81
1941	14.91	18.73	22.38	1957	7.43	10.88	17.14
?==	2.94	6.63	7.18	1958	6.47	8.13	15.51
1043		11.70	16.08	1959	4.42	4.83	10.41
،، بې ې		7.96	11.59	1960	6.02	9.77	12.85
214	10.65	11.60	20.60	1961	3.63	8.80	9.62
+>47		12.36	14.04				

4.

able 2. -- Average monthly and annual temperature, in degrees Fahrenheit,

t		Jan.	Feb.	Mar.	Apr.	May	June	July	Aug	Sept.	Oct.	Nov.	Dec.	Year
Эзо		36.6	41.1	47.2	56.1	62.9	71.9	79.2	76.9	69.7	58.6	46.8	39.3	57.1
3 nt	e	30.4	36.0	43.7	52.2	60.2	68,5	75.9	73.9	65.9	54.1	41.5	33.5	52.9
-cae	1/	29.5	33.6	39.3	48.6	57.0	66.3	73.9	71.7	64.8	52.8	40.3	34.0	51.0

(from published records of the U.S. Weather Bureau)

at Alamo, Caliente, and Pioche, Nev. for the period 1931-60

Average for 1939-60.

Low humidity and high temperatures are favorable for high rates of vaporation. Pan evaporation recorded at Caliente since 1956 is listed in able 3. Evaporation from May through September accounts for most of the annual total and averages about 50 inches for the 6-year period of record.

The average growing season in Dry Lake and Delamar Valleys has not een determined. An approximation of the probable growing season may be stained by reference to the nearby Upper Meadow Valley Wash, which is 20 iles east of this area. Houston (1950, p. 19) lists an average growing season (157 days (May 2 to October 6), based on records af Caliente. Killing temperaires vary according to type of crop. In recent years Weather Bureau records ist freeze data rather than killing frosts; the dates are listed for the occurrence (the last spring minimum and the first fall minimum for temperatures of 32°F. rbelow, 28°F. or below, and 16°F. or below. From these data the number of sys between the last spring minimum and the first fall minimum occurrence for e respective temperature groups are given. The following tabulation lists the mber of days for the three temperature groups recorded for the period 1952-61 (Alamo, Caliente, and Pioche.

		(f	rom publ	ished re	ecords of the U.S. Weather Bureau)						
		320	F or belo	w	28 ⁰ F	or below	r	24 ⁰ ]	F or belo	w	
1	ear	Alamo	Caliente	Pioche	Alamo	Caliente	Pioche	Alamo	Caliente	Pioche	
1	652	177	183	173	212	208	210	22 <b>7</b>	227	232	
:1	53	117	122	143	150	144	161	208	191	166	
	54	219	151	136	230	206	176	257	210	177	
ļ ā	55	141	137	143	178	178	170	208	186	197	
•	56	134	151	152	183		163	202	204	204	
•	57	163	138	134	169	162	190	238	227	227	
	<u>5</u> 8	173	134	178	176	152	179	222	191	224	
	羽	151	135	131	184	150	178	228	200	209	
	Ko L	144	141	144	164	189	164	198	205	204	
, . <b>)</b>	61	129	136	148	156	179	165	188	183	188	
۰.	i.	154	142	148	180	174	175	217	202	180	

Number of days between temperatures of:

6.

AL

Ta	ble	3.	Total	evaporation	at	Caliente,	Nev.	(1956-61)
						-		

(from published records of the U.S. Weather Bureau)

	r	March	April	May	June	July	August	September	October	November
195	6			7.42	^b 12.55	11.10	10.86	8.07	b4.65	2.05
195	7	3.97	6.76	6.33	10.66	11.45	^b 11.60	7.54		
135	8		^ь 6.39	9.35	11.99	12.39	11.73	7.56	5.00	
17:	9		7.56	9.59	11.89	11.71	10.10	7.18		
<u>, 7</u>	0			9.78	10.94	11.16	10.87	7.34	4.06	
196	1		7.19	9.40	12.07	11.06	7.90	6.68	Ъ4.07	
Þ,	ra	.ge		8.64	11.67	11.48	10.51	7.39		

b/ Adjusted to full month by Weather Bureau.

## Physiography and Drainage:

Dry Lake and Delamar Valleys occupy a surficially closed trough in the reat Basin section of the Basin and Range physiographic province of Fenneman 931, p. 328). The north-trending trough is bounded on the east successively om the north by the Ely, Bristol, Highland Peak, and Delamar Ranges. A suthwest-trending spur of the Ely Range forms the northwest boundary of Dry Lake Valley. The Pahroc (also Pahrock) Range bounds the central part of the ough on the west. On the southwest unnamed ranges, commonly with poorly defined drainage divides, comprise the boundary. The south end of Delamar delay is separated from Pahranagat Valley by a low alluvial divide.

The highest point in the mountains enclosing Dry Lake and Delamar valleys is Highland Peak with an altitude of about 9,500 feet. The crest of the *U*ristol and Highland Peak Ranges is more than 8,000 feet above sea level for a stance of about 12 miles. The crest of the mountains along the northwest and ast sides has an altitude of more than 7,000 feet for a combined distance of bout 42 miles. Elsewhere the crests are less than 6,000 feet above sea level, weept for short segments whose altitudes are somewhat above 7,000 feet.

The lowest part of the trough of Dry Lake and Delamar Valleys is the aya or dry lake, in the southern part of Delamar Valley (see inside cover hotograph) which has an altitude of slightly less than 4,400 feet. The altitude the playa in Dry Lake Valley is somewhat less than 4,600 feet. Dry Lake and clamar Valleys are separated by an alluvial divide whose saddle altitude is about 4875 feet.

The trough of Dry Lake and Delamar Valleys is higher than those of White River and Pahranagat Valleys on the west and Meadow Valley Wash on e east, which are tributary to the Colorado River (fig. 2). In Dry Lake and Lelamar Valleys the altitude decreases irregularly from about 5,400 feet at the titude of Fairview Peak in the north to about 4, 400 feet at the north end of the Lelamar playa in a distance of about 55 miles, or an average decrease of 18 feet er mile. In the White River and Pahranagat Valleys to the west the altitude of the floor of the channel decreases from about 5, 100 feet to 3, 600 feet in the same ⁻istance, giving an average gradient of about 27 feet per mile. Similarily, in Meadow Valley Wash and in Lake Valley to the cast, the altitude decreases from 5,900 feet to 3,900 feet in the same distance, giving an average gradient of about 3 [6 feet per mile. Thus, the steeper gradients in the adjacent valleys result in e land surface altitude of the channels being substantially lower than the land urface altitude in the southern part of the trough of Dry Lake and Delamar alleys. In fact, the playa in Delamar Valley is nearly 1, 200 feet higher than e floor of Pahranagat Valley in the vicinity of Maynard Lake. The topographic positions and geology of these valleys largely control the occurrence and moverent of ground water in the region. There are no perennial streams in Dry Lake nd Delamar Valleys, and the gross physiographic features of most of the stream hannels and washes probably were formed during periods of greater precipitaon--probably in Pleistocene time. Present-day streamflow occurs for short eriods only after high-intensity rains and from snowmelt runoff. Only runoff

(rom high-intensity rains can provide large volumes of flow to cause local erosion and substantial transport of sediments in sufficient quantity to modify scream channels and washes.

The main channel along the axis of the northern part of Dry Lake Valley is contained between relatively steep banks about 25 feet below the general level of the valley. The floor of the channel is covered with white sage, and the soil is fine-grained as it is in adjacent parts of the valley floor. This feature suggests that flash-flood erosion in this channel is most uncommon. Farther south, channels draining the Highland Peak and Delamar ranges have somewhat steeper gradients. In this area flood flows occasionally transport relatively coarse gravel to the lower part of the alluvial apron. One example of this was noted along a wash crossing the trail about in sec. 22, T. 1 N., R. 65 E.

During Pleistocene time, lakes occupied the playa areas of Delamar and Dry Lake Valleys. Tschanz and Pampeyan (1961) mapped about 16 miles of beach or strand line along the west, south, and southeast sides of the Dry Lake playa, and about 14 miles along the equivalent segments of the Delamar playa. These represent the highest shore lines identified in these valleys.

Maximum depths of the Pleistocene lakes were on the order of 75 feet in Dry Lake Valley and perhaps 50 feet in Delamar Valley, according to Carpenter (1915, p. 65, 66). The surface areas of the lakes in Dry Lake and Delamar Valleys were about 30 and 16 square miles, respectively.

## GENERAL GEOLOGY

The following discussion of geology is based largely on the reconnaissance geologic maps of Tschanz and Pampeyan (1961) and Tschanz (1960). Other reports that relate to the geology in and adjacent to Dry Lake and Delamar Valleys include those prepared by Westgate and Knopf (1932), Callaghan (1936, 1937), Reso and Croneis (1959), and Kellog (1960).

For the purposes of this report the rocks of Dry Lake and Delamar Valleys are divided into two general groups and further subdivided int four najor units. The distribution of these four units is shown on plate 1. One group primarily represents bedrock in the mountains. It is divided into a Paleozoic carbonate unit and a Paleozoic clastic and Tertiary volcanic and clastic rock unit.

Tschanz (1960, p. 198) indicates that the total thickness of Paleozoic ocks exposed in northern Lincoln County is between 30,000 and 33,000 feet. As described, one may infer that carbonate rocks (limestone and dolomite) probably constitute about 60 percent of the total section. This is somewhat less han the 80 percent of carbonate rocks in a total section of about 30,000 feet noted by Kellog (1960, p. 189) in his study of the southern Egan Range, which is 10 to 15 miles northwest of the area. The second unit of the bedrock group ncludes Paleozoic shale, sandstone or quartzite, and conglomerate and Tertiary 'olcanic rocks, chiefly tuff and intravolcanic sedimentary rocks. Because of their importance to the ground-water hydrology of the region, the Paleozoic carbonate rocks are distinguished from Paleozoic clastic and Tertiary volcanic rocks on plate 1 as discussed subsequently in this report.

The second group is designated the valley fill and is divided into older and younger valley fill. The older deposit consists of unconsolidated to partly consolidated silt, sand, and gravel derived from adjacent highland areas, but also includes some rocks of volcanic origin. This unit was deposited largely under subaerial and lacustrine environments. Although data are not available, the maximum thickness of this unit probably is at least several hundred feet.

The younger valley fill includes clay, silt, sand, and gravel of Quaternary age and is largely restricted to stream channels and playa areas. As defined, this unit is relatively thin and probably is no more than a few tens of feet thick. The valley fill is underlain by bedrock, presumably similar in character to that exposed in the mountains.

## Water-Bearing Properties of the Rocks:

The rocks of Paleozoic age generally have had their primary permeability, that is, permeability at the time of deposition, considerably reduced by consolidation, cementation, or other alteration. However, because they subsequently have been fractured repeatedly by folding and faulting, secondary openings have developed through which some ground water is transmitted. Further, fractures or joints in Paleozoic carbonate rocks locally have been enlarged by solution as water moves through them. Solution openings develop near sources of recharge where carbon dioxide carried by rain water penetrates the ground, where organic acids derived from decaying vegetation, or where otherwise derived acids may be carried by the water into contact with the carbonate rocks. Solution openings need not be restricted to the vicinity of present day recharge areas and outcrops of these rocks. Rather, they may occur wherever the requisite conditions have occurred anytime since the deposition of the carbonate rocks. The principal significance of solution openings is that they further facilitate movement of ground water through carbonate rocks.

Whether existing fractures or solution openings have extensive hydraulic connection or not is related to the overall geologic history of the rocks. In the absence of detailed information, ground-water movement through carbonate rocks in this region is assumed to occur both through fractures and solution openings. Certainly, the large quantity of ground water issuing from fractures and solution openings, such as those at Crystal and Ash Springs in Pahranagat Valley, is a dramatic demonstration that ground-water movement through Paleozoic carbonate rocks occurs in this region of Nevada.

E1

The Paleozoic classic rocks and the Tertiary volcanic and classic rocks exposed in the mountains generally have little primary permeability. Secondary fractures probably are the principal means by which limited amounts of ground water are transmitted through them. Favorably disposed fractures in these rocks probably provide the network of openings through which water

noves and is discharged at small springs in the mountains and which yield a few allons per minute to wells penetrating these rocks. Under extremely favorable onditions the distribution of fracture openings in welded tuff, lava flows, or paleozoic clastic rocks may permit the development of moderate yields of water from wells. However, these occurrences are likely to be so localized that the odds of a well encountering them are very small indeed.

The unconsolidated sand and gravel of the valley fill in Dry Lake and elamar Valleys is capable of transmitting ground water freely. However, most if the valley fill probably is composed of deposits of fine sand and silt. Grains if this size generally have relatively low permeability and, where saturated, ransmit water much more slowly than coarse sand and gravel. Deposits of ilty clay and clay may transmit water so slowly to wells that they will not yield upplies adequate for stockwatering purposes. Various parts of the valley fill probably are moderately consolidated or cemented and this further reduces the apacity of these deposits to transmit useful supplies of water to wells.

### GROUND-WATER APPRAISAL

## Occurrence of Ground Water:

Ground-water recharge in <del>Dry Lake and</del> Delamar Valleys is derived principally from precipitation within the surficial drainage area of the valleys. In a general way, ground water moves from recharge areas in and bordering the nountains toward the central parts of the valleys, thence southward or southvestward to discharge through drock formations. This is in contrast with hydrologically closed valleys commonly found in the Basin and Range province. Carpenter (1915, p. 67) indicated that ground water in Bristol (Dry Lake) and Delamar Valleys probably finds an outlet in Pahranagat Valley. Snyder (1963, 4.400) refers to Dry Lake Valley as being a drained valley; that is, ground water noves out of the valley to discharge elsewhere.

In typical hydrologically closed valleys in the Great Easin, ground water s recharged from precipitation largely in the mountains enclosing the valley. Ground water moves from areas of recharge toward the ground-water reservoir in the valley fill underlying the central part of the valley. In or adjacent to the lopographically lowest part of the valley, the water table, or upper surface of the zone of saturation, is within a few feet of land surface. Where the water table is close to land surface, ground water is discharged naturally by evaporation from the soil or from free-water surfaces and is transpired by plants (phreatophytes) which obtain most of their water from the zone of saturation or overlying capillary fringe.

Under long-term conditions in a hydrologically closed ground-water ⁵ystem, average annual recharge to the ground-water reservoir equals the average annual natural discharge. However, if a ground-water system in a topographically closed valley is hydrologically open, recharge from precipitation in the valley may be greater or less than the discharge within the valley. Where ^{recharge} from precipitation within the valley is greater than discharge in the Valley, ground water must be discharging by underflow from the valley to an area

11.

Ŷ.

recass of lower hydraulic head. Where the recharge from precipitation within the valley is less than discharge in the valley, recharge in part must be entering the valley from an area or areas beyond the topographic divide having a higher draulic head.

In addition to hydraulic controls, the water-bearing character of the rocks and their structure are important factors in the movement, or impedance to povement, of ground water. Where bedrock formations in the enclosing mounins are relatively impermeable, ground water normally is part of a closed drologic system in a topographically closed valley. Where the bedrock formaons are at least locally permeable, the ground-water system may be hydrobgically open. Winograd (1962, p. 110) has referred to this relationship in the cinity of Yucca Flat in southern Nevada.

The chemical quality of the ground water is another factor that may be an aid in evaluating the nature of a ground-water system. Ordinarily, the concentration of chemical constituents shows considerable variation in different arts of a ground-water system. Generally, the concentration is least in areas crecharge and tends to be greatest in areas of natural discharge. Despite the ormal variations that may be expected in the chemical constitutents in ground water in a given system, the character and concentration of one or more constiments may aid in identifying whether or not a given system is closed.

In summary, closed or open ground-water systems may be identified by  $\dot{\tau}_i$  e relationship of recharge to discharge within the valley, by potential hydraulic gradients between the reference valley and adjacent valleys, by the water-bearing aracter of geologic formations, including modifications by structural deforma-  $\dot{\tau}_i$  on, and by the chemical quality of the ground water with respect to that in adjacent areas.

In Dry Lake and Delamar Valleys, the principal areas of recharge are intered in the mountains along the northwest, northeast, and east sides of Dry ake Valley. From the areas of recharge, ground water moves toward the intral part of the valley. Along at least some of the stream canyons or washes yound water is not far below land surface, such as at Bristol wells (3)N/65-21d3) (See cover photograph and photograph 3) and well 1N/65-2al where the depth to water is about 45 feet and 10 feet, respectively. Near the centers of the valleys the depths to water generally are substantial. For example, well (4)N/64-14al is dry at a depth of about 240 feet, an altitude of roughly 5, 385 feet: the depth to water in well 3N/64-20bl is about 318 feet, altitude of about 4, 820 thet; the depth to water in well 2N/64-3bl is about 564 feet, altitude about 4, 350 thet; and the depth to water in well 1N/64-24al is about 398 feet, altitude on the of the depth to water in well 1N/64-24al is about 398 feet, altitude on the of the of 4, 300 feet.

In Delamar Valley, water for the mines and town of Delamar (photograph 4) sobtained from small springs and wells in the volcanic rocks in a nearby wash cording to Callaghan (1937, p. 35). Callaghan further states that this supply inadequate and that a well was drilled 900 feet deep in the alluvium of clamar Valley which was dry throughout. The approximate well site is shown



	A112 959 LASSIFIE	D ERT MX SEP D E-T	EC WES SITING 81 R-53-2	TERN IN INVEST	C LONG	BEACH	CA R RESOU	RCES PR	OGRAM. F	VOLUME 04704-81	F/6 II. RE -C-000 NL	13/2 ETC (U 6	1)	
	3 of 3 40 4 12 96 9													
														1
										END DATE FILMED 105-821 DTIC				
1														
						_	_							



als 65/63-12al on plate 1. However, the details of drilling are not known. If the well literally did not encounter water throughout the full 900 feet, the water-level attitude in this area may be below about 3,700 feet, subject of course to the accuracy of land-surface altitude and the location of the well site.

The great depth to water below the playa areas of Dry Lake and Delamar Valleys precludes evapotranspiration losses from the ground-water reservoir in these valleys, except for extremely small amounts adjacent to scattered springs in the mountains. Inasmuch as the average annual ground-water recharge to Dry Lake and Delamar Valleys is estimated to be several thousand acre-feet per year

, 34-37), and as no equivalent ground-water discharge by evapotranspiration occurs in the valleys, virtually all the ground water is discharged from the valleys by underflow through bedrock.

That ground water is discharged outside these valleys is further confirmed by the hydraulic gradients between Dry Lake and Delamar Valleys and adjacent belleys. As noted previously the altitude of the ground-water levels in Dry Lake and Delamar Valleys decreases southward along the axial part of the valleys. available control points do not precisely define the altitude of the ground-water fevels in the valleys. However, an apparent gradient is indicated by the watervel altitudes at the several drilling sites; that is, less than about 5, 385 feet in cec. 14, T. 5 N., R. 64 E., about 4,820 feet at well 3N/64-20b1, about 4,350 feet at well 2N/64-3a1, and somewhat below about 3,700 feet at well 6S/63-12a1 belamar Valley. Thus, the hydraulic gradient is southward at more than 35 feet per mile in the northern part of Dry Lake Valley, and southward at somewhat theore than 18 feet per mile from the north-central part of Dry Lake Valley to the central part of Delamar Valley.

Valleys to the east and west of Dry Lake and Delamar Valleys surficially rain to the Colorado River. Along the White River channel in Pahranagat Valley, Hiko Spring issues from about the alluvial-carbonate bedrock contact at an altitude of about 3,890 feet. About 5 miles south of Hiko Spring, Crystal Springs issue from limestone and alluvium at an altitude of about 3,815 feet. About 5 miles frther south in Pahranagat Valley, Ash Springs issue from limestone at the olluvial-bedrock contact at an altitude of about 3,610 feet. About 30 miles farther South in the vicinity of Lower Pahranagat and Maynard Lakes, at the south end of Pahranagat Valley, ground water in the alluvium is near land surface and is at an altitude of about 3, 150 feet. Additionally, the depth to water in well 4S/61-15al, Jout 6 miles east of Hiko Spring, is about 678 feet or an altitude of about 3,700 eet. Land surface along the White River channel and known water-level altitudes outh of Maynard Lake along the White River channel are lower still. Maynard ake is only about 10 miles southwest of the playa in Delamar Valley. Thus, round water from Dry Lake and Delamar Valleys could discharge to Pahranagat alley by underflow to the west, south, or southwest, based in terms of the ^{potential} hydraulic gradient.

Along Meadow Valley Wash to the east, land-surface altitude in the wash ^a above: 4,000 feet northward from a point about 10 miles south of Caliente. The ^epth to water in the wash is generally within a few tens of feet below land surface;

therefore, the water-level altitude in Meadow Valley Wash probably is equal to or higher than that in Dry Lake and Delamar Valleys at equivalent latitudes throughout most of their lengths. For most of the same distance, the mountain area probably provides sufficient recharge to maintain a hydraulic divide between the two areas. Thus, a major transfer of ground water between the two areas does not seem likely.

In further considering ground-water discharge by underflow from Dry Lake and Delamar Valleys, the Paleozoic carbonate rocks appear to be the most favorable rocks to transmit ground water. The springs in Pahranagat Valley demonstrate that ground water moves through solution openings and fracture systems in some quantity, at least locally. Ground-water movement through similar Paleozoic rocks in Cave Valley, northwest of Dry Lake Valley, has been described in a previous report (Eakin, 1962). Drilling at the Nevada Test Site, about 75 miles southwest of this area, has shown that the Paleozoic carbonate rocks transmit ground water more readily than do the Paleozoic clastic rocks and Tertiary tuff (Winograd, 1962, p. 110). Thus, the Paleozoic carbonate rocks probably afford the best opportunity for ground-water movement between valleys in this area.

Plate 1 shows the surficial distribution of Paleozoic carbonate rocks in Dry Lake and Delamar Valleys. They are exposed most extensively along the east and northwest sides of Dry Lake Valley. Along the west and south sides of Delamar Valley, younger volcanic rocks crop out. However, Paleozoic carbonate rocks undoubtedly underlie the volcanic rocks in this area and, further, are exposed along White River channel in Pahranagat Valley and southward (Tschanz and Pampeyan 1961, and Bowyer, Pampeyan, and Longwell, 1958). Accordingly, the distribution of Paleozoic carbonate rocks in this area in favorable to the movement of ground water southward or southwestward from Dry Lake and Delamar Valleys to Pahranagat Valley.

If the Paleozoic carbonate rocks are capable of transmitting ground water by underflow from Dry Lake and Delamar, the converse may be true; that is, ground water may move into Dry Lake and Delamar Valleys from the north through carbonate rocks from valleys upgradient from Dry Lake and Delamar Valleys. This may be evaluated roughly as follows: In the northern part of Dry Lake Valley the lowest known water-level altitude is about 4,820 feet at well 3N/64-20b1. Higher water-level altitudes occur in White River Valley to the west and northwest; in Cave Valley to the northwest, and in Lake Valley to the north and east. However, the mountains enclosing the northern part of Dry Lake Valley are areas favorable to recharge from precipitation. Because they are areas of recharge, the water levels, in these mountain blocks also must be assumed to be areas of relatively high water levels. Thus, although actual water levels are not available in these areas, it is strongly inferred that ground-water divides occur beneath the mountains and thus provide hydraulic barriers to ground-water movement from adjacent valleys into the northern part of Dry Lake Valley. Similarly, it is inferred that a hydraulic divide exists in the Bristol and Highland Peak Ranges on the east side of Dry

Lake Valley and provides a hydraulic barrier to ground-water movement between Dry Lake Valley and Meadow Valley Wash. The same condition probably occurs in the Delamar Range on the east and southcast sides of Delamar Valley, although this range probably receives less recharge from precipitation than do the ranges to the north.

The mountains bordering the west side of Dry Lake and Delamar Valleys apparently provide only meager recharge from precipitation. The amount probably is not sufficient in magnitude or time to maintain a hydraulic barrier between Dry Lake and Delamar Valleys and White River and Pahranagat Valleys.

In summary most, if not all, of the ground-water recharged to Dry Lake and Delamar Valleys is believed to be derived from precipitation within their surficial drainage areas. Ground water moves from the areas of recharge toward the central part of the valleys, thence generally southward or southwestward. Ground water is discharged from the trough of Dry Lake and Delamar Valleys by underflow through Paleozoic carbonate rocks to areas downgradient from the trough; that is, most probably into Pahranagat Valley, southwest of Delamar.

The depth to water in the central part of the trough of Dry Lake and Delamar Valleys is deep--probably too deep for economic recovery of ground water for the usual uses in this region, except possibly for stock purposes. Depths to water in the lower parts of the valleys decrease from somewhat more than 300 feet in T. 3 N., R.  $64 E_{\bullet}$ , to about 400 feet in the south part of T. 1 N., R.  $64 E_{\bullet}$ , to possibly more than 1,000 feet beneath the playa area of Delamar Valley. Perched or semiperched ground water in the mountains and upper parts of the alluvial apron locally supply water to small springs and locally is at a sufficiently shallow depth to permit the development of small water supplies by wells, such as at Bristol wells and well 1N/65-2al.

#### Estimated Average Annual Recharge:

:1

1

. 3

. 3

đ

.3

9. . .0

Ì

The average annual recharge to the ground-water reservoir may be estimated as a percentage of the average annual precipitation within the valley (Eakin and others, 1951, p. 79-81). A brief description of the method follows: Zones in which the average precipitation ranges between specified limits are delineated on a map, and a percentage of the precipitation is assigned to each zone which represents the probable average recharge from the average precipitation for that zone. The degree of reliability of the estimate so obtained, of course, depends on the degree to which the values approximate * • :tual precipitation in the several zones, and the degree to which the avd percentages represent the actual proportion of recharge to ground wate. Neither of these factors is know precisely enough to assume a high degree of reliability of the recharge estimate for any one valley. However, the method has proved useful for reconnaissance estimates and experience suggests that in many areas the estimates probably are relatively close to the actual long-term average annual recharge.

The precipitation map of Nevada (Hardman and Mason, 1949, p. 10) has been adjusted (Hardman, oral communication, 1962) to the improved toposaphic base maps (scale 1:250,000) now available for the whole State. The base map for plate 1 of this report was prepared from the same series of toposraphic maps. The several zones of precipitation applicable to Dry Lake and Delamar Valleys are as follows: the boundary between the zones of less than & inches and 8 to 12 inches of precipitation was delineated at the 6,000-foot contour; between 8 to 12 inches and 12 to 15 inches, at the 7,000-foot contour; between 12 to 15 inches and 15 to 20 inches, at the 8,000-foot contour; between 15 to 20 inches and more than 20 inches at the 9,000-foot contour.

્યક્ર ds

ാർ

រខ្លាំ

103 1.7

051

1. 72 1

. . 11

The average precipitation used for the respective zones, beginning with 1.6 the zone of 8 to 12 inches of precipitation, is 10 inches (0.83 foot), 13.5 inches (1.12 feet), 17.5 inches (1.46 feet), and 21 inches (1.75 feet).

The percentages of the average precipitation assumed to represent recharge for each zone are: less than 8 inches, 0; 8 to 12 inches, 3 percent; 12 to 15 inches, 7 percent; 15 to 20 inches, 15 percent; and more than 20 inches, coal 25 percent.

Table 4 summarizes the computation of recharge for Dry Lake and Delamar Valleys. The recharge (column 5) for each zone is obtained by multiplying the figures in columns 2, 3, and 4. Thus, for the zone of 12 to 15 inches of precipitation in Dry Lake Valley the computed recharge is 16,000 (acres) times 1.12 (feet) times .25 (25 percent) = about 1,300 acre-feet. The estimated total average annual recharge to ground water in Dry Lake and Delamar Valleys is about 6,000 acre-feet.

Table 4. --Estimated average annual ground-water recharge from precipitation in Dry Lake and Delamar Valleys, Nev.

•

I

3

	(5)	Estimated	recharge	(acft)	(2x3x4)		1	300	006	1 2	1,000
Vallev	(4)	, ,	Percent	recharged	)	E	3 3	7	٣	0	average scharge ed)
Delamar	(3)	Average	annual	precipitaion	(feet)	1	J E	1.12	. 83	1	Estimated annual re (round
	(2)	Approximate	area of	zone	(feet)	درد در 0	0	4,000	35,000	208,000	247,000 about 385 sq. mi.
	(2)	Estimated	recharge (	(acre-feet)	(2x3x4)	100	200	1, 300	2,700	1	5,000
	(4)		Percent	recharged		25	15	2	ю	0	d average recharge led)
y Lake Valley)	(3)	Average	annual	precipitation	(feet)	1.75	1.46	1.12	. 83	1	Estimate annual (round
Dr	(2)	Approximate	area of zone	(acres)		200	3, 200	16,000	114,000	442, 300	575,400 about 900 sq. mi.
	(1)	Precipitation	zone	(in inches)		20+	15-20	12-15	8-12	<b>+</b> 80	

π

#### Estimated Average Annual Discharge:

Only a very small amount of ground water is discharged from Dry Lake and Delamar Valleys by evaporation and transpiration. Areas where ground water evaporates from soil or from free-water surfaces or is transpired by vegetation are restricted to isolated areas adjacent to the few small springs. The largest of these occurs near the spring at the Meloy Ranch in the southern part of T. 5 N., R. 65 E. Discharge was estimated to be about 20 gpm in March 1963. The few wells in the valley are used largely to provide water for stock, and the total withdrawals are very small. In the past, Bristol wells have been used in part to supply water requirements for mine camps and travelers. Similarly, wells and springs in Cedar Wash were used for water supply at Delamar. However, neither of these supplies were adequate.

Because of the great depth to water, no large areas of evapotranspiration from ground water occur in the lower parts of Dry Lake and Delamar Valley. Most of the ground water apparently is discharged by underflow through bedrock from Dry Lake and Delamar Valleys, but the amount cannot be directly determined. However, to the extent that the estimate of ground-water recharge is correct, and because over a long period of time recharge equals discharge, ground-water discharge by underflow is about 6,000 acre-feet per year minus the small amount, probably less than a few hundred acre-feet discharged by wells and by evapotranspiration adjacent to spring areas.

#### Perennial Yield:

The perennial yield of a ground-water system is the amount of natural discharge that can be salvaged for beneficial use from the ground-water system. It is the upper limit of the amount of water that can be withdrawn economically from the system for an indefinite period of time without causing a permanent and continuing depletion of ground water in storage and without causing a deterioration of the quality of water. The average recharge from precipitation and streams, discharge by evapotranspiration, discharge to streams, and underflow from a valley are measures of the natural inflow and outflow from the ground-water system.

In an estimate of perennial yield, consideration should be given to the effects that ground-water development of wells may have on the natural circulation in the ground-water system. Development by wells may or may not induce recharge in addition to that received under natural conditions. Part of the water discharged by wells may re-enter the ground-water reservoir by downward percolation, especially if the water is used for irrigation. Ground water discharged from wells theoretically is offset eventually by a reduction of the natural discharge. In practice, however, it is difficult to offset fully the discharge from wells by a decrease in the natural discharge, except when the water table has been lowered to a level that eliminates both underflow and evapotranspiration in the area of natural discharge. The numerous pertinent factors are so complex that, in effect, specific determination of perennial yield of a valley requires a very extensive investigation, based in part on data that can be obtained economically only after there has been substantial development of ground water for several years.

The ground-water system in Dry Lake and Delamar Valleys, as presently understood, is such that economics probably is the controlling factor in the determination of perennial yield. The great depth to water in most of the valley more or less precludes large-scale withdrawals for most uses. Hydrologically, the saturated zone, or reservoir, underlying the floor of the valleys is the most likely area in which to develop substantial water supplies. At the depth of water indicated, the ground-water reservoir probably occurs largely in Tertiary rocks or in underlying Paleozoic carbonate rocks beneath the floor of the valleys.

Whether development occurs in the Tertiary or younger rocks of the valley fill or in the Paleozoic carbonate rocks, withdrawals for a long time would have to come largely from ground water in storage. The amount of stored ground water to be removed is many times the average annual recharge and undoubtedly would require many years of pumping. Pumping from storage would result in a lowering of water levels extending outward from the area of pumping farther and farther until the area of influence eventually would divert virtually all the water from areas of recharge to the area of pumping. After this was accomplished, pumping levels would tend to stabilize, providing that the average annual net withdrawals from pumping were equal to the recharge to the pumped area. The net withdrawals at that time would be equal to perennial yield. Thus, the perennial yield would be limited to the amount of inflow that could be diverted from the areas of recharge to the area of pumping influence.

Whether the magnitude of perennial yield ultimately equals total recharge to the valley depends upon the relative location of the area of pumping with respect to the several areas of recharge to the valley, the relation of the area of pumping with respect to the principal area of ground-water discharge or underflow from the valley, and the altitude of economic pumping levels with respect to altitude of natural discharge or underflow. In Dry Lake and Delamar Valleys, the costs of pumping relatively large quantities of ground water to modify appreciably the natural ground-water regimen to salvage all the natural discharge undoubtedly would be prohibitive for all but the most exceptional water requirements. However, to the extent that such development might occur, the area in and adjacent to Tps. 1 S. and 1 N., R. 64 E., is located favorably with respect to ground-water storage, and sufficient development might result ultimately in salvaging much of the discharge from Dry Lake Valley. However, it is conceivable that to salvage a large part of the estimated 6,000 acrefeet of average annual discharge from the valley, water levels might have to be drawn down as much as 1,500 feet below land surface.

#### Ground-Water in Storage:

The amount of ground water stored in the valley fill and underlying bedrock in Dry Lake and Delamar Valleys is substantial. It is many times the average annual recharge to and discharge from the ground-water reservoir in these valleys. To the extent that ground water may be developed, the volume of ground water in storage provides a reserve for maintaining an adequate supply for pumping during protracted periods of drought or for temporary periods of high demand under emergency conditions. This reserve, in effect, increases the reliability of ground water as a dependable source of supply and is an important asset in semiarid regions where surface-water supplies vary widely from year to year.

## **Chemical Quality:**

The chemical quality of the water in most ground-water systems in Nevada varies considerably from place to place. In the areas of recharge the chemical concentration of the water normally is very low. However, as the ground water moves through the system to the areas of discharge, it is in contact with rock materials which have different solubilities. The extent to which the water dissolved chemical constituents from the rock materials is governed in large part by the solubility, volume, and distribution of the rock materials, by the time the water is in contact with the rocks, and by the temperature and pressure in the ground-water system.

The following analysis of water from Bristol well was reported by Carpenter (1915, p. 30). Constituents are listed in parts per million.

Silica	(Si02)	49	Carbonate	(C03)	0.0
Iron	(Fe)	.7	Bicarbonate	(HC03)	187
Calcium	(Ca)	76	Sulfate	(S0 ₄ )	71
Magnesium	(Mg)	33	Nitrate	(N03)	32
Sodium plus			Chloride	(C1)	110
Potassium (Na	+ K)	37			
То	tal hardnes	ss as CaCO	3 325		
То	tal solids		509		

The analysis probably does not represent the typical chemical quality of ground water in Dry Lake Valley. However, it is somewhat suggestive of a mixed-water type found in the region. In some areas, ground water in Paleozoic carbonate rocks will contain a relatively high proportion of calcium magnesium, and bicarbonate due to solution of the carbonate rocks. As that water moves into Tertiary volcanic rocks or deposits derived from such rocks the proportion of sodium will increase partly by base exchange and partly by addition to the dissolved solids in the water until the water becomes a sodiumbicarbonate type. The relatively high chloride and nitrate in the analysis suggests local contamination, a condition that might well be expected from the local concentration of people and stock of the watering point when Bristol wells supplied water to the nearby mines and was the site of a small settlement and a smelter.

If it can be assumed that the analysis may be more or less representative of ground water in the lower part of Dry Lake Valley, with the exception of the high concentration of chloride and nitrate, the water would be suitable for domestic and stock purposes.

#### Development:

Small amounts of ground water from springs and wells are used to water livestock feeding on the range in Dry Lake Valley. Carpenter (1915, p. 66) reported that Bristol well (3N/65-21d1) formerly furnished the water supply for a smelter. He reported too, that several wells were dug in the vicinity and a small town sprung up around them. However, when Carpenter visited the area in 1912, only one well remained. This well had been in use to supply water to the traveling public and for miners at the Bristol mine a few miles east. The well could be pumped dry at that time during the filling of water tanks used to supply water at the mine. In October 1912 the well was 51 feet deep and water level was 43 feet below land surface. Seemingly the well has since been destroyed. There are three drilled wells in that area that are used to water stock. Reportedly, however, all three do not provide a sufficient supply to meet the needs.

Near Delamar, Carpenter (1915, p. 67) noted that water was piped from several springs, reported to be small seepages in the limestone and granite. Callaghan (1937, p. 35) also refers to the water supply of Delamar but refers to the earlier used springs and wells in a nearby wash as being developed in volcanic rocks. Carpenter also reported that well 65/63-12a1, drilled 900 feet deep at the foot of the alluvial slope below Delamar, was dry. He further states that when the mine at Delamar was active, water supply was obtained from Meadow Valley Wash, which was pumped over the Meadow Valley Range (Delamar Range) through two 3 1/2-inch pipe lines.

Presently, ground water from wells and springs probably supplies less than 100 acre-feet per year and is used principally for watering stock in Dry Lake and Delamar Valleys. Development of ground water for irrigation probably would be prohibitive because of high pumping costs. Limited amounts of

ground water could be developed, if the need were great enough.

The very substantial depths to water in the central parts of Dry Lake and Delamar Valleys, which makes the cost of development of ground water too high for usual purposes, may make the area attractive for some types of special testing or operation required in modern day technology. In turn, ground water probably could be developed to meet limited water requirements of such activitics.

## DESIGNATION OF WELLS

In this report the number assigned to a well is both an identification number and a location number. It is referenced to the Mount Diablo base line and meridian established by the General Land Office.

A typical number consists of three units. The first unit designates the township; "N" after the number identifies the township as north of the Mount Diablo base line; "S" after the number identifies the township as south of the Mount Diablo base line. The second unit, a number separated by a slant line from the first, is the range east of the Mount Diablo meridian. The third unit, separated from the second by a dash, is the number of the section in the township. The section number is followed by a lower case letter, which designates the quarter section, and finally, a number designating the order in which the well was recorded in the quarter section. The letters a, b, c, and d, designate, respectively, the northeast, northwest, southwest, and southeast quarters of the section.

Thus, well number 3N/64-20b1 indicates that this well was the first well recorded in the northwest quarter of sec. 20, T. 3 N., R. 64 E.

Wells on plate 1 are identified only by the section number, quarter section letter, and serial number. The township in which the well is located can be ascertained by the township and range numbers shown on the margin of plate 1. For example, well 3N/64-20bl is shown on plate 1 as 20bl and is within the rectangle designated as T. 3 N., R. 64 E.

## Table 5. --Records of selected wells in Dry Lake and Delamar Valleys, Lincoln County, Nev.

<u>1N/64-24a1</u>. Owners R. Lytle, S. A. Hollinger, and A. Delmue. Drilled stock well; depth 515 feet, casing diameter 5 inches. Reported depth to water below land surface 398 feet, January 17, 1959. This well caved between 428 feet and 515 feet. Driller's log:

Material	Thickness (feet)	Depth (feet)	
Clay	3	3	
Gravel, sandy	12	15	
Clay	45	60	
Sand and gravel. stratified	29-	350	
Sand, fine	70	420	
Lime, cemented	8	428	
Clay	87	515	
Total	depth	515	

1N/65-2a1. Owner not determined. Dug well; depth 12 feet, diameter 48 inches. Reported depth to water 10 feet.

2N/64-3b1. Coyote well. Owner, Bureau of Land Management. Drilled stock well; depth 742 feet; diameter, 6 inches; casing perforated 702 to 742 feet with torch-cut 1/4- x 8-inch slots, 6 to the round. Equipped with pump jack and gasoline pump. Reported depth to water, 664 feet, March, 1963.

2N/65-6bl. Owner not determined. Abandoned drilled well; depth 376 feet. Dry.

<u>3N/64-20b1</u>. Owner Bureau of Land Management. Unused, drilled stock well; depth 380 feet, casing diameter 6 inches. Depth to water below land surf- 2 304 feet, when drilled; measured depth to water 316.54 feet, Mar. 11, 196

<u>3N/65-21d1.</u> Bristol well. Destroyed dug stock and domestic well. Reported depth, 51 feet. Reported depth to water 43 feet.

<u>3N/65-21dp</u>. Bristol well. Drilled stock well; casing diameter, 8 inches. Equipped with pump jack. Reported depth to water about 45 feet.

<u>3N/65-21d3.</u> Bristol well. Drilled stock well; casing diameter, 6 inches. Equipped with windmill and cylinder pump:. Reported depth to water, 45 feet.

3N/65-21d4. Bristol well. Drilled stock well; casing diameter, 5 inches. Equipped with pump jack and engine. Reported depth to water, 45 feet.

5N/64-14al. Owner not determined. Drilled well; depth 239.5 feet. Dry.

#### REFERENCES CITED

Bowyer, Ben, Pampeyan, E. H., and Longwell, C. R., 1958, Geologic map of Clark County, Nevada: U.S. Geol. Survey Mineral Inv. Field Studies Map MF-138.

Callaghan, Eugene, 1936, Geology of the Chief District, Lincoln County, Nevada: Univ. Nevada Bull., Geol. Mining Ser. 26, 32 p.

- Callaghan, Eugene, 1937, Geology of the Delamar District, Lincoln County, Nevada: Univ. Nevada Bull., Geol. Mining Ser. 30A, 72 p.
- Carpenter, Everett, 1915, Ground water in southeastern Nevada: U.S. Geol. Survey Water-Supply Paper 365, 86 p.
- Eakin, Thomas E. and others, 1951, Contributions to the hydrology of eastern Nevada: Nevada State Engineer, Water Resources Bull. 12, 171 p.
- Eakin, Thomas E., 1962, Ground-water appraisal of Cave Valley, Nevada: Nevada Dept. Conserv. Nat. Resources, Ground-Water Resources -Reconnaissance Ser. Rept. 13, 18 p.
- Fenneman, N. M., 1931, Physiography of western United States: New York, McGraw - Hill, 534 p.
- Hardman, George, and Mason, Howard G., 1949, Irrigated lands in Nevada: Univ. Nevada Agr. Expt. Sta. Bull. 183, 57 p.
- Houston, Clyde E., 1950, Consumptive use of irrigation water by crops in Nevada: Nevada Univ. Agr. Expt. Sta. and Div. Irrigation and Water Conserv., Soil Conserv. Service, U.S.Dept. Agriculture Bull. 185, 27 p.
- Kellog, Harold E., 1960, Geology of the southern Egan Range, Nevada: Intermountain Assoc. of Petroleum Geologists, Guidebook to the geology of east central Nevada, p. 189-97.
- Reso, Anthony, and Croneis, Carey, 1959, Devonian system in the Pahranagat Range, southeastern Nevada: Geol. Soc. America Bull., v. 70, no. 9, p. 1249-1252.
- Snyder, C. T., 1963, Hydrology of stock-water development in the Ely Grazing District, Nevada: U.S. Geol. Survey Water-Supply Paper 1475-L.
- Tschanz, Charles M., 1960, Geology of northern Lincoln County, Nevada: Intermountain Assoc. of Petroleum Geologists, Guidebook to the geology of east central Nevada, p. 198-208.

Tschanz, C. M., and Fampeyan, E. H., 1961, Preliminary geologic map of Lincoln County, Nevada: U.S. Geol. Survey mineral Inv. Field Studies Map MF-206.

Westgate, Lewis G., and Unopf, Adolph, 1932, Geology and ore deposits of the Pioche District, Nevada: U.S. Geol. Survey Prof. Paper 171, 79 p., 8 pls., 13 figs.

Winograd, Isaac J., 1952, Interbasin movement of ground water at the Nevada Test Site, Nevada: U.S. Geol. Survey Prof. Paper 450-C, p. 108-111.

## PREVIOUSLY PUBLISHED REPORTS OF THE GROUND-WATER RESOURCES RECONNAISSANCE SERIES

## Rep. No. 1 Ground-Water Appraisal of Newark Valley, White Pine County, Nevada. Dec. 1960, by Thomas E. Eakin. 2 Ground-Water Appraisal of Pine Valley, Eureka and Elko Counties, Nevada, Jan. 1961, by Thomas E. Eakin. 3 Ground-Water Appraisal of Long Valley, White Pine and Elko Counties, Nevada, June 1961, by Thomas E. Eakin. 4 Ground-Water Resources of Pine Forest Valley, Humboldt County, Nevada, Jan. 1962, by William C. Sinclair. 5 Ground-Water Appraisal of the Imlay Area, Humboldt River Basin, Pershing County, Nevada, Feb. 1962, by Thomas E. Eakin 6. Ground-Water Appraisal of Diamond Valley, Eureka and Elko Counties, Nevada, Feb. 1962, by Thomas E. Eakin. 7 Ground-Water Resources of Desert Valley, Humboldt County, Nevada, April 1962, by William C. Sinclair, 8 Ground-Water Appraisal of Independence Valley, Western Elko County, Nevada, May 1962, by Thomas E. Eakin. 9 Ground-Water Appraisal of Gabbs Valley, Mineral and Nye Counties, Nevada, June 1962, by Thomas E. Eakin. 10 Ground-Water Appraisal of Sarcobatus Flat and Oasis Valley, Nye County, Nevada, Oct. 1962, by Glenn T. Malmberg and Thomas E. Eakin. 11 Ground-Water Resources of Hualapai Flat, Washoe, Pershing, and Humboldt Counties, Nevada, Oct. 1962, by William C. Sinclair. 12 Ground-Water Appraisal of Ralston and Stonecabin Valleys, Nye County, Nevada, Oct. 1962, by Thomas E. Eakin. 13 Ground-Water Appraisal of Cave Valley in Lincoln and White Pine Counties, Nevada, Dec. 1962, by Thomas E. Eakin. 14 Ground-Water Resources of Amargosa Desert, Nevada - California, March 1963, by George E. Walker and Thomas E. Eakin. 15 Ground-Water Appraisal of the Long Valley-Massacre Lake Region, Washoe County, Nevada, by William C. Sinclair; also including a section on The Soils of Long Valley by Richard L. Malchow.











н1.0

MISCELLANEOUS WORKING DOCUMENTS
H1.1

والمنافقة والمنافقة والمنافقة والمتعادية والمنافقة والمنافية والمنافية والمسترين والمنافقة والمنافعة والمراجع

WELL LOGS AND REPORTS TO THE STATE ENGINEER OF NEVADA

W	ÉIL LO	DG ANI	D REPORT TO THE STATE	Rec. DCG. 4. 196.2-
'Æ	-)	ENGIN	EER OF NEVADA	Well No
0	PLE	ASE COMPL	ETE THIS FORM IN ITS ENTIRETY	Do not fill in
ner7.4.'.	<u> </u>	foait	Diller 10 cm	( free
ressZ.	RoyL	<u>t[                                    </u>	Adress In Address	Lic. No. 3.
tion of	f well:		Sec. 21., T. 3. N/8; R.G.S.E., in	County
	<u>zi stel</u>	21'. Î.	P	
er will	be used for	Steel	Total dept	ll of well <u>12</u> c
of dril	led hole			linear foot
e i. kness o	of casing	10 30	ا المعنى Temp. of water	
neler a	nd length of	casing5	<u>sc'</u>	·
		(Casin	g 12" in diameter and under give inside diameter; c	nsing 12" in diameter give outside diameter.)
owing w	well give flo	w in c.f.s. or	g.p.m. and pressure	
~ ·	ng well give	depth of sta	nding water from surface 17	·
orflow:				
owing 1	weli describe	e control wo	the second size of a	
owing 1	well describe	e control wo	Type and size of the second size of the second size of the second s	valve, elc.)
owing to owing t	weli describe	e control wo of well.744	tks (Type and size of the state	valve, etc.) of well <u>Line 222-ities 1, 1962</u>
owing to owing the of core of wa	well describe	e control wo of well. 7/1 frances ()	Type and size of a completion of the completion	valve, etc.) of well <u>kining and its in 1962</u>
owing the of core of we	well describe	e control wo of well.74 francess	Type and size of a completion of the second size of a completion of the second	Water-bearing Formation, Casing Perforations. Ste.
owing to of conternations of we trem	well describe mmencement ell rig	control wo of well.74 francess LOG Thickness feet	Type and size of a (Type and size of a Constraint of completion of Constraint of completion of Constraint of the completion of the com	Water-bearing Formation, Casing Performations, Stc.
of cor of cor of we rem reet	mmencement ell rig <u>f</u>	control wo of well 7/4 francess LOG Thickness feet	Type and size of a (Type and size of a State of completion of State of comp	Water-bearing Formation, Casing Performations, Etc.
of con of con to of we teet	mmencement ell rig	control wo of well 7/1 france 10 LOG Thickness feet 6-0	Type and size of n Type and size of n Summer of the second seco	Water-bearing Formation, Casing Perforations, Stc. Chief aquifer (water-bearing formation) from 17' to 77 ft
of cor of cor of we cof we rem feet	mmencement ell rig Cz To feet CO J 2 C	control wo of well 7/1 france 1 1 LOG Thickness feet LOG LOG LOG	Type and size of a Constraint 28, 19,67. Date of completion of S-11. OF FORMATIONS Type of materiai wand - gravel - boulder: Committed gravel.	Water-bearing Formation, Casing Perforations, Stc. Chief aquifer (water-bearing formation) from 17' to 77 ft. Other aquifers
of cor of cor cof we rem rem	mmencement ell rig <u>f</u>	control wo of well <u>-</u> ]. <u>LOG</u> Thickness feet <u>LO</u> <u>LOG</u> CO <u>C</u> O	Type and size of r Constraint 25, 1962 Date of completion of N_1[ OF FORMATIONS Type of materiai wand - gravel - concoline Constitut gravel.	Water-bearing Formation, Casing Performations, Etc. Chief aquifer (water-bearing formatica) trom 17' to 77 ft. Other aquifers
of cor of cor of war cof war rem rem	mmencement ell rig (2 To feet (CO ) 2 C	e control wo of well <u>51</u> <u>LOG</u> Thickness feet <u>60</u> <u>60</u>	iks (Type and size of r	Water-bearing Formation, Casing Water-bearing Formation, Casing Perforations, Etc. Chief aquifer (water-bearing formatica) from 17' to 77 ft. Other aquifers
of cor of cor of war of war of war rem rem	well describe mmencement ell rig_C_ feet 60 120	e control wo of well. <u>7</u> <u>LOG</u> Thickness feet <u>LO</u> <u>LO</u> <u>LOG</u>	iks (Type and size of r winning 25, 19,67. Date of completion of N_[[. OF FORMATIONS Type of materiai wand - gravel - boulding Committed gravel.	Water-bearing Formation, Casing Water-bearing Formation, Casing Perforations, Etc. Chief aquifer (water-bearing formatica) from 17' to 77 ft. Other aquifers
of cor of wing to of cor of we cof we rem rem	mencement mencement ell rig <u>f</u>	e control wo of well. 74 free	its (Type and size of r Type and size of r Sull OF FORMATIONS Type of materiai ward - guard - boulder: Commited gravel.	valve, etc.)         of well kinescaring Formation, Casing Perforations, Etc.         Water-bearing Formation, Casing Perforations, Etc.         Chief aquifer (water-bearing formatica)         trom       17'         to       77         Other aquifers
of cor of wing to of cor of we rem rem	mencement minencement ell rig <u>f</u> feet <i>L</i> 0 <i>j</i> 2 C	e control wo of well. 74 free control LOG Thickness feet LOO LOO LOO	its (Type and size of r in indian 28, 19,67. Date of completion of N_[[. OF FORMATIONS Type of materiai ward - guive f - boulder: Committed gravel.	valve, etc.)         of well kine and intervention, interventinterventinterventintervention, intervention, interventinterventin
of con of con to of we teet	mmencement ell rig <u>f</u>	e control wo of well. 74 free control LOG Thickness feet CO CO CO	its (Type and size of r in 1962) Life of completion of Sulf OF FORMATIONS Type of materiai wand - guard - boulder: Committed grand.	valve, etc.)         of well kinic and intervention, Casing Performation, Casing Performation, Casing Performation, Etc.         Chief aquifer (water-bearing forwation)         trom       17'         to       77         to       77         there aquifers         First water at       17         casing performance
of cor of wing to of cor cof we rem rem	mencement mencement ell rig <u>f</u>	e control wo of well. 34. france ,	its (Type and size of r winschen LE, 19.6.2. Date of completion of N_[[. OF FORMATIONS Type of materiai wand - gravel - boulder: Cernintial gravel.	valve, etc.)         of well kincharting Formation, Casing Perforations, Etc.         Water-bearing Formation, Casing Performation)         Cbief aquifer (water-bearing formation)         from 17' to 77 ft.         Other aquifers
or flows owing to of cor of we rem rem rem	mmencement ell rig <u>f</u>	e control wo of well. 74 free control LOG Thickness feet CO CO CO	iks (Type and size of r winning 25, 19,62. Date of completion of N_1[ OF FORMATIONS Type of material wand - gravel - & ouldine Cernintial gravel.	value, etc.)         of well \$\overlinestyle=2.2222\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$
or Howa owing to of cor of we rem leet	mencement ell rig <u>f</u>	e control wo of well. 74 free LOG Thickness feet LOG LO LO CO	its(Type and size of r <u>viscological</u> A&, 1962 Date of completion of <u>vill</u> OF FORMATIONS Type of materiai wand - guessil - Eouldini Committed granel.	Valve, etc.) of well <u>A. z 222</u> <u>is 1, 19, 62</u> Water-bearing Formation, Casing Perforations, Etc. Chief aquifer (water-bearing formation) trom <u>17'</u> to <u>77</u> ft. Other aquifers First water at <u>17</u> feet. Casing perforated from <u>2.0'</u> to <u>5.6'</u> ft. Size of perforations <u>15'</u> <u>5'</u> <u>5'</u> <u>5'</u>

Los Nul to Said WELL LOG A D REPORT TO THE ST Dro. 6. 10 62 Rec. Well No. ENGINEER OF NEVADA Permit No. RLEAST COMPLETE THIS FORM IN ITS ENTIREDY The net fill in Owner I La tre the Terrangeo way Deilles Miles Address & Provide Lie Lie Address Prince Contraction Lie No. Bit fel 10.16 aspelan inter at al Cl Water will be used for ..... fine for Size of drilled hole Diameter and length of casing 12" in diameter and under give inside diameter; casing 12" in diameter give outside diamet If flowing well give flow in c.f.s. or g.p.m. and pressure If nonflowing well give depth of standing water from surface. 1.4-If flowing well describe control works a und size of valve, etc., Date of commencement of well 7/11 Correction Rds Rd 196 States Completion of well 7/00 mentions 26.196 Type of well rig To free how I roll LOG OF FORMATIONS Water-bearing Formation, Casing Perforations, Etc. From fect To fæt Thickness Type of a aterial feet Chief aquifer (water-bearing sand-gravel - bouldie formation) 45 ٥ 45 15 to 50 . 50 5 samply clay from ..... 45 80 50 30 Gear-el Other aquifers_____ montul First water at 16 feet Casing perforated 20 10 60 from Size of perforntions 1/2 × 12 

	,	ginada Shediyi (cy. Jina Indoniye			Log No.
17-	WE	ELL LO	G ANE	REPORT TO THE STATE	Rec. 125 4 1963
			ENG	EER OF NEVADA 30,65	-2/ Well No.
		PLFA	TE COMPT	ETE THIS FORM IN ITS ENVIRENT 4	Do not All in
ľ.	Owner?	<u>t</u> ie	Coatt	2. Cistany in many Driller The	<u>(                                    </u>
l .	Address Z.	Car of	tt: Co	Address Address	Lic. No. 3
5	Location of	well:	······································	Sec. 21., T.J. N/S, R. 55 E, in	Co.
	or	<u>i : È ç-(</u>	2016	·	······································
	Water will	be used for.	. P.E F	Total dept	b of weil <u>120</u>
	Size of drill	led hole E		Weight of casing per	linear foot
n alter och	Thickness of	f casing	10 30.5	Temp. of water	
	Diameter an	d length of	casing	501	
			(Casing	z 12" in diameter and under give inside diameter; ca	ising 12" in diameter give outside dlamer
	i li Howing w	vel! give flov	v in c.t.s. or	g.p.m. end pressure	· · · · · · · · · · · · · · · · · · ·
	- if nonflowir	ig well give	depth of stat	nding water from surface	· · · · · · · · · · · · · · · · · · ·
· ·	If flowing w	ell describe	control was	ks(Type and size of v	alve, etc.)
	Date of con	mencement	of well.742	warding 25, 19.19. Date of completion of	of well 13 1 2 2 2 2 2 1 1 9 10 7
1	Type of we	11 riz : (= (	<u>}</u>	<u>Self</u>	
1. E	<u></u>		LOG		
	Frem	To feet	Thickness feet	Type of materiai	Perforations, Ste.
					Chief anuifor (warns-bearing
	C,	60	60	ward - quest - coulder	formation)
	60	120	60	Commented grand	from tot
	• • •			•	Other aquifers
	·-	1	•		
	•				
					First water at 17 feet.
			l		
					Casing perforated
					from <u>20</u> to 50
		 			Size of perforations
<u>.</u>		ļ			1/4 X 10
			1		
		· ·			
		ļ			\$19 <b></b>
		:	•	1 (04/2)	N Sector

1					
	· . Wa	IL LC	G AND	(REPORT TO THE STATE	Roc_Dac_11_12-22
 	•		ENGIN	EER OF NEVADA 30/65-2	Well No.
					dcb Do not Bit to
-	Orm Ql	best	Defm	Drillor Daris	l. Free
	Address	Proch	e nu	Aldres Carot	he Menada In No30
1	Location of	well:		500, TN/S, RE, in	rid alm
	07	nesto	2 . 90	3.	<b>~</b> ~ /
	Water will !	be used for.	ato:	Total depi	a ei well
	Size of drill	led 'solel	5		lizer foot
	Thickness of	f casing	<u>o gan</u>	Trop. of veloc	aga antarinan kaya na minangan kanangan kanangan kanan na ana di sabah kanan kaya ka
	Unazhlet az	n incin ci	Cash	g 12" in diameter and under give imide diameter; c	any 12" is diameter sive ostulde diameter.)
	If Bowley n	rell give flo:	# ia c.f.s. or	apine and pressime	,
	If nonflowin	ng well give	depth of sta	nding weine from conficer and a	·····
	If flowing u	roll describe	e ountral wa	ria. (Type and she of 1	ralve, stc.)
	Date of con	mencement	of well 10.	remain 3, 1959 Date of completion	of well 10 seembra 9, 1939
Ĵ	Type of the	Il rig. <u> </u>	fran: Sas	baill	
		,	LOG	Water-bearing Formation, Caulog	
	FT049	To fust	Thickness fast	Type of material	Perforationa, Etc.
	° C	12	12	gravel	Catal agailer (water-bearing
	18	29		Concourse and anough	ston 10 2.9 12
	10		a.	very brand + stight	Other agailters
					********
					First water at 4 6 - con
					Caldne perforated
					mar tet w 80 a
ŕ					
					1/4- X 12
,					
		r		1	4
•	· · · · •	1			310

-----

3N/63-12. Log No. 1010~X WELL LOG AND REPORT TO THE STATE Rcc. 19 ; Well No. :-- ENGINEER OF NEVADA Dry Lake Permit No. 2397% PLEASE COMPLETE THIS FORM IN ITS ENTIRETY Do ict fil! inPASIN Driller Y 10 K 197 - Conta 1. splan Owner. Address P = Star 21 2 Jul Lic. Ngil Address..... Location of well 1/2 1/2 Sec. 7. N/S, R. J. E, in 1 12/2/2/ .. or... _____ Water will be used for IRRADATION Total depth of weil Total Size of drilled hole 14 Thickness of casing...... 2 If flowing well give flow in c.f.s. or g.p.m. and pressur-If nonflowing well give depth of standing water from surface Date of commencement of well ______Date of completion of well ______ 220 Type of well rig. LOG OF FORMATIONS Wath-pearing Formation, Casing Perforations, Etc. Thickness From To fect Type of material feet feet  $\zeta'$ 5 54126 Chief aquifer (water-bearing formation) 1 AV21 SAND 5 ร from a Conto to to to 62010 1 711 うち Other agulfers..... 59 ズ W/SAN) 11 Ŀ 5 3ANd 11 5 03 IJ 3 5 2 З ر کم 3 Grado Ļ Casing perforated 11 IJ 1.[ from a from to ..... L Ç ٠<u>'</u> Size of perforations c3

To feet	Thickness			Type of material	
		h	. •		
					•
· . ·			•		•
			•		
		. •			
				• • •	
•					
•				•	
		· ·	CASI	ING RECORD	
From	To	Length	·.	"Remarks"—Seals, Grouting, Etc.	-
1001			•		
					•
-· •					
					•
	<u> </u>		<u>-17 </u>		
	GE	NERAL INFO	RMATION-	-Pumping Test, Quality of Water, Etc.	- ,
				· · · · · · · · · · · · · · · · · · ·	:
				· · · · · · · · · · · · · · · · · · ·	•
		•			
	<u> </u>	•		· · · · · · · · · · · · · · · · · · ·	
WELL DRI	LLER'S ST	ATEMENT		(Not to be filled in by Driller)	•
was drille	d under m	• v jurisdictior	and the		
ormation is	true to my	best inform	ation and		
•			,	~	
igned	We	ll Driller		• • • • • • • • • • • • • • • • • • •	
·			• · · • • • • • • • • • • • • • • • • •		
	T :	No			
	Phoenes	110	••••••		
	•••••••••••••••••	, 19	······································	11 01 12 21 914 000	•
		•			

list on some 21 .1 Ca The state of the second states W BR JJ Well LOG AND REPORT TO THE STATE ، کندر ا ñs. Wed Ib. ENGINEER OF NEVADA IN/64E-39 #5 1177:58 Provin 14 20 und ca in the second Delmon Dille 7a Burga 122 and The 1-3-21 K. -Bry1-Eache Meinin 130 Alianna NT X 34. FL/M. 2 8645 12 A Landos of mal: and will be ١ Compily an ß 515 set or ીખની તેમપુરત ની જ્યો Wese will be used for. 714 She of Cottled Lake __Visight of centry par Conse look 3 loo i see Thinks a sosier 5 5" 515' actions at 193 Elementar and bength of only a والمراجعة المحجو وجلى المحجول فا الله والعدة : المحمولة والحد دما: حذها عده المحمولة الم الا وحدار . . . 1 2-2 -l'anning well give fire in alla or gran and pressen 398' TO WATER. If performing well give depth of strong water from oralism. If faming well describe seeised works. (in and the est the other Date of occurrences of and Plan. 15, 1958 Die d'anginin a millon 1959 17. Type of will sig The Same Will EGH CH LICHDLANSTON the second second Water-Dearing Dimension, Cashar 29 Sout Chieferta Porsian Line .. Jona Bont Corps of mediated Sent. - -. .. .. CHAR ADNIFOR WATCH BELANT З 3 ila. υ Con senter ( senter-carely Ling stratuna) 3 15 12 grave sand 515 428 5. 60 15 45 (J CUPH DURDED 60 350 290 ind sand & gravel ..... 350 find. aand 1120 70 temented lime 420 428 8 515 87 428 محنك 15 1.15 м - ++tak k ord stalleset og af som år genegendet som k FIRST WATER AT 428 Fact INFO CHANGE IN 41 7 9 Post Casing perforted . - 515 System - 152 -ા ્રે . Like at substitutes .... Ko * 10" scot size. • • 1/2 X 10

WELL

(32-) **35/63-224b** LT TO THE STATE ENGL Log No. 10 6164 Rec. 11-26-69 19 Well No. . NEVADA Permit No. 22147.7. Do not f.!! in. 1 THIS FORM IN LIS ENTIRETY ORROW Driller VICK Machun NEVADA Address BEAVER Lic. No. 7381 3. T. 3. 3 //S, R / 3. E, in UN COLH Cou 51 22477 Total depth of weil 130 (Casing 12" in diameter and under give inside diameter; casirg 12" in diameter sive outside diameter.) . p.m. and pressure 3' 4" diag water from surface. (Type and size c? volve, ctc.) :/3/66 Date of completion of well 3/2/66 J FORMATIONS Water-bearing Formation, Casing Perforations, etc. Type of material GREY CLAY BLUE CLAY Chief aquifer (water-bearing formation GREY CLAY from 125 to 23:0 GRAVEL Other aquifers..... CLA GRAVIC : INV GARVEL CLAY First water at 8 SANDYCLAY GRAVEL * Casing perforated SAuch from 60 to 230 Stud + Shavel CLAY Size of perforations 3. M . 240

"ANARY-CLIENT'S PINK-WILL PRILL	COPY ER'S COPY	(	DIV	1510N - 2 a C	OF WAT	ER RESOUR S Leg No
F Observ	ation )+-	35/6	e	ELL T Please con	DRILLI nptete (lii) E	RS REPORT Basin
I. OWNER Ba	5. DEPT OF T	۲- HE Al! ssile (	x FORC	E	Λ	DDRLSS Norton AFB, Calif. 92409
					••••	······································
2. LOCATION PERMIT NO. DOI	NE 14 Su ne req. Exg	/ 14 plorate	sec 12 ory we	т. 11	3	ж/s _R 64 <u>E</u> Nye Co
3.	TYPE OF WOR	₹K.		4.		PROPOSED USE 5. TYPE WELL Reven
Deepen		her			unicipal []	Infigation [] Test [] Cable [] Rotar Industrial [] Stock [] Other []
6.	LITHOLO	GIC LO	G			8. WELL CONSTRUCTION
Mate	rial	Water Strata	From	To	Thick ness	Casing record
fine sand, so	<u>me small ro</u>	<u>ck</u>	0	50	£t	Weight per foot
sand and grav	vet	<u>.</u>	<u>50</u>	185	÷	Diameter * From To
gravel corse	se sand some	 •	240	275	+	2 inches 6 feet 1300
clay		F			†	inches feet
gravel, sand	some silt		275	340		in hes fort
coarse sand.	gravel, tra	aces	340	370	+	inches feet
of silt and of	lay	+	-770-	+ ******		inches
and 1/2" tor			570	112.07		Surface seal Yes 🕅 No Li - Type - GLOUE
sand. gravel	trace of s	silt	420	510	+	Depth of scal 40 ft.
& clay, rock	from 1/2" 1	to 3"			+i	Gravel packed: Yes XX No []
gravel and co	barse sand		510	610		Graves packed from
gravel, sand	, small rock	K		11010	$\downarrow$ – –	Perforations:
1/2" to 2" al	nd silt		010	11010	+	Type perforation. mill slot
sand, gravel	SULEARS WI	Lii 	1010	1300	+	Size perforation
200.05 up 00		<u> </u>	<u></u>	+	+	From 768 for 788
						From feet to
						From
·		<b> </b>			•	From
		} <b></b>	+	+	• • • • • • • •	
			t		· · · · · · · · ·	7. WALLK LEVEL
· · · · · · · · · · · · · · · · · · ·						Flow
				·		Water temperature. COld * F. Quality
		L		<u></u>		
Date started	Decemb	er 20			19 79	10 DRILLERS CERTIFICATION
Date completed	J.	anuary	26	······································	03.01	This well was drilled under my supervision and the report is tri- the best of my knowledge.
7.	WELL TE	ST DAT	٨			Name BEYLIK DRHLING, INC. (James L. Cly
Pump RPM	G.P.M.	Draw Do	wn I	After Hour	s Pump	Address 591 S.Walnut Street-Ia Habra. Ca.9
air lift	<u>15 ±</u>			4	·····	Nevada contractor's license number
		+				
المحدد بحدد والمراجع		!	<u> </u>			Presidea armer's access manager
not applical	ble BAILE	R TEST	n., r	'r er t	bours	Signed Jerris A. Corport
G.P.M.		Draw dow	n í	ice:	hours	Date Seb. 12, 1980
G.P.M		Draw dow	n	iet -	hora	
				na na ini ia un	v 2 2	and the second and the second structure and the second second second second second second second second second

);- i	CANARY-CLIENT'S C PINK-WELL DRULER 	OPY US COPY	( (	DIV ∕₩	ST. ISION ( ELL F	DF WAT	NEVADA FER RESOUKS ERS REPORT	Log No. Permit No. Basin	OFFICE USE ONLY
·(_			•		lease com	plete this	form in its entirety	Dasili	
-m	Germanie 11 9-	-15 8 1 (-	1 niping	q_123		5			
•	I. OWNER U. S.	DEPT. OF	INE AIR	REORC:	F	A	DDRESS Norton AFE,	Calif.	92409 ·
	Balli	stic Missi	le Dept						
	(Well	is: Dry 1	Lake Va	illey	Test W	lell No	. TW-1)	••••	
2	2. LOCATION	E 1/4 SW	1/4 S	ec 12	T.	3.5	N/S R 64E F · II	n Lincol	n Cou
	PERMIT NO. NO.	ne require	ed – Ex	plora	itory h	ole			
. =									
	3 1	TYPE OF WOR	K		4.		PROPOSED USE		5. TYPE WELL
	' New Well 🏌	] Re	econdition		Do	mestic [	Irrigation 🗇 Tes	1 <b>1</b> 9	Cable 🗆 Rotary
	Deepen	] <b>O</b>	ther		Mu	nicipal [	Industrial 🗂 Stoo	ak 🗖	Other M Reverse
		-							Circuiation
́ (	6.	LITHOLO	GIC LOG	ì			8. WELL C	CONSTRUC	TION
=			Water		1	Thick	Diameter hole. 18-1/2	inches Tot	al depth 1,000
	Materia	1	Strata	From	To	Dess	Casing record		
	gravel, clay,	small rock	ĸ	0	140		Weight per foot		Thickness 5/16
Ċ	ravel, small	rock		140	150		Diameter *	From	••••••••••••••••••••••••••••••••••••••
j	large rocks, 2"	dia. grav	el	150	190		22" x 1/4" wall	0	40
ā	and fine sand					[	10 x 5/16"	+ 2	1000
j	large rocks, 2"	dia.grave	1	190	260		inches	·······	
ġ	ravel & small	l" dia.ro	cks	260	370	1	inches	••••••	
Ť	fine sand & fe	w small roo	cks	370	400		inches	•••••••••••	
Ċ	ravel & small	rocks/cla	y I	400	440		inches		
Ĕ	prown clay, smal	11 amt. or	avel	440	520	t	inches		foet] f
o	ravel and small	11 rocks	· · · · ·	520	600		Surface scal: Yes (X No	[] Туре ⊢	grout
1	ravel, verv li	ttle clav		600	630		Depth of seal. 4.1 I	L.	
b	nown clay sma	11 rocks		630	710		Gravel packed: Yes 🔯 🖪	lo D	1000
	mavel			710	760		Gravel packed from	LU fe	1 to 1000
. b	rown clay and	gravel	┝╌╾──┣	760	780-	<u> </u>	D for the		
ā	mavel and fin	e sand		790	000		Johnse Johnse	an a co	
ž Ž	ravel very li	ttle clav		200	000		Type perforation	W1rg	screen
. v	mavel & small	rocks		000	950	<u> </u>	Size perforation	.050	
7	mavel some s	mall rocks		0.50	000		From	feet to	<u>. </u> <u> <u> <u> </u> <u></u></u></u>
77 0	mall 1" dia	mocks grat		000	000		From	feet to	
	mks & gravel	Locias, gra		000	1000		From	fect to	750
- -				3000	1000		From	feet to	··· <del>7</del> 60·· ····· 1
9 1	Laver		<b></b> }	1000	1005		From	feet to	
1	aru tuuk ano	Some grave	<u>+</u>	1002	TOTO				
-					<u> </u>	┣	9. WA	TER LEVE	•
-						<u> </u>	Static water level .422	Feet be	low land surface
-					{···	<u> </u>	Fiow	G.P.M.	
					<u>+</u> –	+	Water temperature. 82.5.	F. Quality	slightly cloudy
:	nn:	lans a state d	ur a and		<u></u>	+=			
1	Dub started Fel	b. 6th				. 80	10. DRILLERS	S CERTIFIC	ATION
	Dita complete AD	ril 20th	•••••	••••••••••••••	<b>.</b>	80	This well was diffled under n	ny supervisio	n and the report is true
-	Date completed				·····	19	the best of my knowledge.		
	,		C.E. 1. 1. 40 1				INTVIJIK	DRILLIN	G. INC.
	· · · · · · · · · · · · · · · · · · ·	WELL IE	SI DATA	`	_		Name.	······································	
-	Pump RPM	GPM i	Draw Duw	n	After Hours	Punp	591 S. I	Walnut S	treet
•	1800	500	41	70			Address La Faor	a, Calif	. 9LOJ_
•							4		
							Nevada contractor's licen e i	number	C07055A
•									
. •		·······				•••••	Nevada drillet's ticonse num	ber 11	68 and 1169
	- : Lauren er <del>en</del> earen -		L <u>2.99</u> - 2.27			· · ·			110000 01-
	lione lione	BATI L'I	k TEST				Signed James Lift	de la	Judies Cly
						•			···· vritter
	G.P.M		raw down.		CL	nours	· · ·		
	G.P.M G.P.M		raw down. raw down	10 fe	ct	hours	Dat April 21	, 1980	

4 ľ

£ •	WEL	L LOG	ANE a	. ORT TO THE STATE ENG.	Log No.
I	•			OF NEVADA	L Well No.
	••••••	PLE	 NSE COMPL	ETE THIS FORM IN IT'S ENTIRETY	Permit No. 2.2.5.55 Do not Ell in.
	Owner E.	<u></u>	11 tin	Driller Macill	÷.
ŀ	Address3.	50 Jtac	Roct 1	Hantow Trib France Address Presses	
	Location of	well: S.E.	4 SE 1/1 Se	c 23, T. 4 N/S, R 6 E, in	Frince-la-
	Permit No		Dimit	6	
	Water will	be used for	<u>. 19. r.c.</u>	antre Total dept	1 of well
	Size of drill	led hole	12	U	r linear foot
	Thickness o	casing	L. Cru	Temp. of water	
	Diameter ai	nd length o	f casing	(Casing 12" in diameter and under size inside diameter	rasing 17° in diameter nive cutting diameter )
	If flowing v	vell give flor	w in c.f.s. o	r g.p.m. and pressure	
	If nonflowin	ng well give	depth of st	anding water from surface	
1	If flowing v	vell describe	e control w	orks	-
	Data of cor	mmencomer	t of well 7	(Type and size	of wall 01 and 19 486
-	Tune of wel		l Joch		or wenting and the second s
_			LOG	OF FORMATIONS	
	From feet	To feet	Thickness feet	Type of material	Water-bearing Formation, Casi Perforations, etc.
	Ċ	5	5	wort	Chief aquifer (water-bearing form.
	5	12	7	when	fromto
	12	51	39	Committed grani	Other aquifers
	57	61	10	grande in would ic	
			• •		
				· · ·	
					furst water at1
					Casing perforated
					fromto
(					Size of perforations
<b>N</b> . /					
	1				
		······································			

40165 Log No. 96 36 (34) WELL LUG AND EPORT TO TE STATE Rec Aug E Well No. OF NEVADA Permit No. 2.2.8 > 5 105 PLEASE COMPLETE THIS FORM IN IT'S ENTIRETY Do not fill in. Owner and the C. Marin - Driller 10 - 10 Fr 5. Ila Low OFISh March Address Presence 7/ 1000 la Lic. No. 30 Address 350 Stars Location of well 5 E 1/ 5 121/ Sec 24, T. 4 M/S, R 6 3 E, in Stranger David Ent Permit No. Water will be used for tot full Total depth of well 360 Diameter and length of casing..... (Casing 12" in diameter and under give inside diameter, casing 12" in diameter give outside diameter.) If flowing well give flow in c.f.s. or g.p.m. and pressure..... WATER 410 If nonflowing well give depth of standing water from surface If flowing well describe control works..... (Type and size of valve, etc.) Date of commencement of well 52. 6. 24, 1.7. Date of completion of well 52. 6. 29, 1967 Type of well rig Coble . Too LOG OF FORMATIONS Water-Jearing Formation, Casi To feat From Thickness Perforations, etc. Type of material feet fcet 125 5 Chief aquilir (water-bearing form: 65 226 161 Cerninted second from fo 228 226 2 ilay Other aquifes 8 228 236 materil alerel cfa-f 2 238 236 Conventint desmal 238 240 Э. 240 250 10 class sunthe large of signal 250 250 2 S. til -296 252 44 conjunt of Commander & second First water at _____fer - - *I*a ~ 297 296 326 29 297 y Commenteri Casing perforated 327 326 from 360 .327 .33 ر من از. Size of perforations ( )

H1.2

1

DRY LAKE VALLEY WELL LOG AND WELL DESIGN (VALLEY-FILL) DRY LAKE VALLEY ORSERVATION WELL (DL-1-0-1) 3S/64E-12da

_										1
	sign	[		22	00000	0.000	0 <b>0</b> 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	· · · · · · · · · · · · · · · · · · ·	0	
	ell De	[								
	3	à	01			9				
	Log	Res.								
	ysical	S.P.								
	Geoph *	Gamma								
		Symbol								0000
	Lithologic Log	Description	Sar - 10' - 30'), tan (d); silt 90%, sand 10%.							
	Penetra - tion	1 <b>°=</b> 100 Min.						<u>.</u>		,
	Depth	Ŀ.		+++++ %	<u>+++</u> 	+++++ § L	<u>1</u> 35 	-+++++++++++++++++++++++++++++++++++++	+- <b> </b> + + + + <del>  + + + +  </del> 2 1	

 $\sum$ 





								والمراجع المحجب والمراد
0.000,000,000		00.2000						
		<u>~ 0 ~ 0 ~ 0 ~ 0</u>			0.000 ()00		<u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>	
						6		
						t (900)		
		ب				1 And Sil Bravel 20		
						me Gravu Ind 70%,		
						J With So vn (w), 18		
						Sanı Drov		
┍╺┎┟╻╼╼╼┼┥╸╸╸╸	<del>++++++++++</del> +	<del>· • • • • • • • • • • • • • • • • • • •</del>	+++++++++++++++++++++++++++++++++++++++	┊╶╪╾╋╴╋╴╋╸╋╸╋╸╋╸╋	<del>╞╺╸╸╺╶╸╡╺╶╶╺┈╡╸</del>	┝┼┼┽┽╃╉	<del>* * * * <b> </b> * * * *</del>	<del>╡╡╡╺╶╸┥┨╺</del> ╋┥
89	ę20	8	- 750	800	958 1		 86	1000
				<b>b</b> ia				
	,							





22 1.D Centre Well Design • .... ;; 00.° • 0 • DRY LAKE VALLEY TEST WELL (DL-I-T-1) 3S/64E-12da \$ Res. **Geophysical Log** S.P. Gamma # Symbol (0' - 30'); tan (w); silt 100%, trace gravel. Lithologic Log Description Silt 1**°=** 100 Min. Penetra -tion * Ľ. Depth <u>8</u> 1 31-- 200 - 250 3







1.

H1.3

DRY LAKE VALLEY WELL LOG AND WELL DESIGN (CARBONATE)

Well Design Res. DRY LAKE VALLEY TEST WELL 3N/63E-27cg **Geophysical Log** S.Р. Gamma 0 0 0 0000 200 000 0.0.0 Symbol • . 2 Tuff (196) 3.351) yellow (Y2.5YH7/6) 80%, mixed volcanics 20%, (Meeozoic-Tertiary) Alluvium (0° 196°) duskyred (R 10R 3/3) mixed volcanics. Lithologic Log Description 1*****= 100 Min. Penetra-(206' - 240') no time (0' - 25') no time (30' - 40') no time Rate tion Ľ. Depth - 200 - 150 81-- 250 3

7

F		· ·								7
				3 /	10" I D turut taing grout					B C C L L L L L L L L L L L L L L L L L
				347						
om	human	h	h							
		Tuff (196 3351) yailow (Y2.5YH7/b) 80%, mixed volkanius 20%. (Meaozok: Tariwy)		Sandstone And Limestone - (335' - 360') weak rwd (R 10R5/4), intigrbedded,	Liniescone - (360° - 410'), week zed (A10R4/3), tuff and calcite present. (Guilmette Formation (?), Devoryan)	-		Dulumite (41c' 680') reddich grav (R5YH5/2), 95%.	calcite present. 5% (Guilmette Formation(7), (Pevonard).	
k	no time * 240')		I							
<b></b> ∎ ₩++++	ᠬᢆ᠒ᡔᠬᡗᢩ	┎┎┎┍╼┰┠ _╍ ┎ ┼┼┼┼┼┼┼┼┼	┶╍╾┓┎┚ ┼┼┽┽┼┼┽┽	└ <u>╮</u> ┨╻┍╺ ┝┼┼┼┼	<mark>Ъ┎╍╍</mark> ┺ ┿┿┿┿┿┿	<b></b>	ᡗᢇᡄ_ᡗᡐᠧ ᡰ᠇᠋ᢩᡰ᠇᠇	┍┛┓╸╴╸╸	<b>╶╶╻┚┖┚╹┶╻╶┎</b>	
	500	790	001	- 350	Q Q Q	ł	0\$* -	805	099 -	600



-











,

