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Technical Report 591

AIRBORNE FIBER OPTICS MANUFACTURING TECHNOLOGY

Aircraft Installation Processes

G Kosmos **RA Greenwell**

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19 August 1980

Final Report: May 1978 - June 1980

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Prepared for **Naval Air Systems Command** Washington, DC 20361

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NAVAL OCEAN SYSTEMS CENTER SAN DIEGO, CALIFORNIA 92152

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NAVAL OCEAN SYSTEMS CENTER, SAN DIEGO, CA 92152

AN ACTIVITY OF THE NAVAL MATERIAL COMMAND

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ADMINISTRATIVE INFORMATION

Work was conducted under contract N00123-78-C-0193 to <u>Boeing</u> Aerospace Corporation, <u>Seattle</u>, <u>WA</u> as part of the Airborne Fiber Optic Manufacturing Technology Program of the Naval Air Systems Command (NAVAIR 520) under Program Element APN, work unit ET15. This final report covers work from May 1978 to June 1980, and was approved for publication on 19 August 1980.

Released by CL Ward, Head Design Engineering Division Under authority of CD Pierson, Jr, Head Electronics Engineering and Sciences Department

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LF Buldhaupt	Program Manager
OR Mulkey	Project Engineer
SP Suave	Program Planning
P Thain	Cost Analysis
C Hand	Installation Process and Procedures

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OBJECTIVE

The objective of this manufacturing technology program was to develop and demonstrate the procedures/documents for fabricating and installing fiber optic harnesses and a fiber optic stand-alone link in a military airframe. The procedures/documents are developed based upon the current state-of-the-art fiber optics technology and then updated by prototyping, production fabrication, and airframe installation (mock-up) of fiber optic harnesses. The output of this program is a complete set of documents for the successful fabrication and installation of a fiber optic interconnect system into a military type aircraft.

RESULTS

1. The two fiber optic harnesses designed and fabricated during the initial two phases of the program were successfully installed in the E-3A Class III mock-up, using the installation procedures documented in Phase I. The harnesses were tested optically before and after installation and evidenced no changes during the installation processes except for one section of the stand-alone link which was damaged (broken fibers) during an observed gross mishandling incident. The cable in this case was pulled 90° to the cable tie in an effort to adjust its position. Precautionary notes have been added to the installation document to emphasize the dangers of violating the minimum bend radius restriction specified. Phases I, II, and III documentation were reviewed and revised as required to incorporate knowledge gained during the production fabrication phases of the twenty bundle-fiber harnesses and the one prototype single-fiber harness.

2. The twenty-one fiber optic harnesses were successfully fabricated during Phase IV. The grinding and polishing of fiber ends was found to be the most time consuming and costly operation in the manufacturing flow. No major problems were experienced during this production activity. Five harnesses were installed aboard the E-3A mock-up, per the developed procedures, with no damage.

3. Full documentation for the successful fabrication and installation of a fiber optic harness/cable has been developed. This documentation has been verified by the fabrication of twenty-one harnesses in a production type environment, using production wire/cable assembly technicians for the actual fabrication. In addition, four of the production harnesses and the single-fiber prototype harness were successfully installed in the E-3A mock-up.

4. A routing analysis was developed to provide a basis for future applications of fiber optics in military aircraft.

5. A life-cycle cost analysis of the optical cable was completed. It is apparent that weight and size reductions of fiber optics offer economic advantages. It is possible to increase the E-3A sortie time by 2.5 percent, which can be equated to a reduction of fleet size by 1.5 aircraft. The reliability of fiber optic interconnect systems appears to be equivalent to wire interconnect systems. It appears easier to install, remove, and/or replace optical fibers. Optical fiber interconnect systems are also simpler to test. Spares, repair parts, materials, and special support/test equipment add to initial costs, as does almost any new technology, but the impact is minor. With simpler equipment and techniques there may be a long-term savings potential. Overall costs and benefits of fiber optics appear to surpass the Bp E-3A wire interconnect configurations. Districtico,

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RECOMMENDATIONS

- Initiate a manufacturing technology program to address the entire spectrum of the termination operation, including automated grind/polish operations, mass polishing techniques, tooling, ultimate producibility, and cost.
- Initiate a program whose objective would be elimination of epoxy in connector designs.
- Initiate a manufacturing technology program on fiber optic transmitter/receiver subsystems so that the entire cost of manufacturing a fiber optic system (transmitterinterconnect-receiver) can be determined.
- Develop and optimize volume production processes for the fabrication of fiber optic harnesses using large core single fiber technology.
- The above program should be a joint effort involving not only the system integrator but both cable and connector suppliers.
- Use the present set of harnesses in a test program to determine the capabilities of the current technology in the area of environmental/mechanical and application stress.
- Expand the technology to include that necessary for the use of fiber optics in shipboard applications.

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INTRODUCTION

The objective of this work is to establish manufacturing methods in industry to assure the ability to install, on a production basis, fiber optic interconnect systems aboard military aircraft. This report contains the information gained through a four-phase contract (N00123-78-C-0193) with Boeing Aerospace Corporation, Seattle, Washington.

BACKGROUND

It has been demonstrated in the A-7 Airborne Light Optical Fiber Technology (ALOFT) program that fiber optics can be successfully used on military aircraft. The many advantages of a multiplexed, fiber optic data interface – such as immunity to electromagnetic interference (EMI), electromagnetic pulse (EMP), and lightning strikes; reduced systems weight; and reduced complexity in external harnesses and connectors, resulting in improved reliability and maintainability – have also been demonstrated. Before fiber optics can be used on a production aircraft, installation practices and procedures must be established for high volume, low cost. Ther optic interconnects. By the development or improvement of installation processes, techniques, and equipment by the contractor (Boeing Aerospace), this work is intended to develop an industry source for the timely, reliable, and economical assembly of the required fiber optic interconnects.

SCOPE

As fiber optics has progressed from research and development to feasibility demonstrations, it has become apparent that planning for high volume production of fiber optic components is necessary. Questions of production compatibility, applicability, and cost are addressed under this contract in order to identify and correct problems associated with the installation of fiber optics aboard military aircraft. Two major requirements have been undertaken in this contract: (1) the fabrication and installation of fiber optic harnesses; and (2) the fabrication and installation of "stand-alone links." Present electrical harnesses conduct both electrical signal and electrical power. Fiber optic harnesses developed under this contract conduct optical signals and electrical power and are a one-for-one replacement of the electrical harness counterpart. The stand-alone link accounts for retrofit applications for which no fiber optic harness is required - just stand-alone links. Associated with the two major requirements is the development of assembly methods and installation specifications for the incorporation of the harnesses and stand-alone links aboard a Boeing military-type surveillance aircraft. The assembly methods installation specifications, as well as the identification of routing techniques, support test equipment, field repair techniques and procedures, and a detailed cost analysis between the fiber optic cost and the original wire interconnect cost were verified on a full-scale production mock-up.

PROGRAM OVERVIEW

This final report covers a 25-month four-phase program entitled "Fiber Optic Interconnect System: Manufacturing Processes For" (NOSC Contract N00123-78-C-0193). This report covers the activity of all four phases of the contract, with particular emphasis on the final phase. The fourth phase verified all documentation/procedures by the fabrication of 21 production-type harnesses and subsequent mock-up of 5 harnesses aboard an E-3A Class III mock-up. Documentation developed during the fourth phase of this program includes:

Final Installation Process Specification Final Production/Acceptance Test Procedure Engineering Drawings Final Field Repair & Technique Procedure Final Cost Analysis Final Description of Harness Assembly and Tooling

The interim procedures developed earlier in the program were updated to generate the above final procedures. These procedures are attached to this report in the appendices and they form, in conjunction with the other reports, procedures, and specifications developed during Phases I, II, and III, a complete set of documentation for the fabrication and installation of complex fiber optic cables and harnesses.

The program plan, as shown in figure 1, was to develop all required documentation for the fabrication and installation of fiber optic harnesses in military aircraft by conducting four distinct phases. The first phase was primarily a design stage where the aircraft type was selected, harnesses for that aircraft were defined or chosen, and the necessary process specifications were developed for fabrication and installation. In this stage, materials were selected and a preliminary cost analysis was then developed based upon the selected materials and processes.

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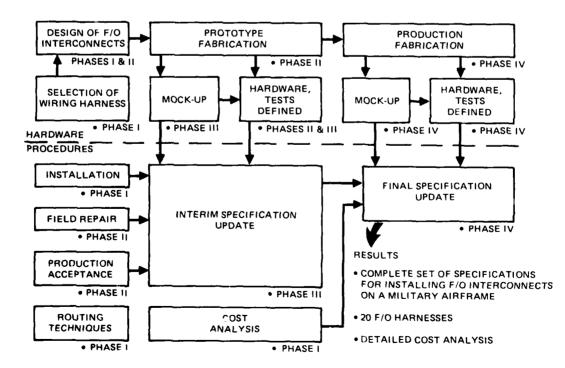


Figure 1. General program flow diagram.

Appendix	Document Title	Document Number
A	Final Installation Process Specification (General)	D180-24693-20
В	Final Installation Process Specification (Specific)	D180-24693-21
С	Final Production/Acceptance Plan	D180-24693-22
D	Final Field Maintenance and Repair	D180-24693-23
Е	Manufacturing Technology Cost Analysis	
F	Final Harness Assembly Description and Tooling	D180-24693-25
	Fiber Optic Rack Integration Harness	D180-59004
G	Fiber Optic Assembly Procedure, General	D180-24693-26
н	Fiber Optic Assembly Procedure, Hughes	D180-24693-26.1
1	Fiber Optic Connector Assembly Procedure, Amphenol	D180-24693-26.2
j	Fiber Optic Termination Procedure, General	D180-24693-27
К	Fiber Optic Termination Procedure, Hughes Connectors	D180-24693-27.1
L	Fiber Optic Termination Procedure, Amphenol, Connectors	D180-24693-27.2
М	Fiber Optic Shop Aids Requirements, General	D180-24693-29
N	Routing Techniques	D180-24693-5

Table 1 lists documents developed for this program. Copies of the documents are appendices to this report.

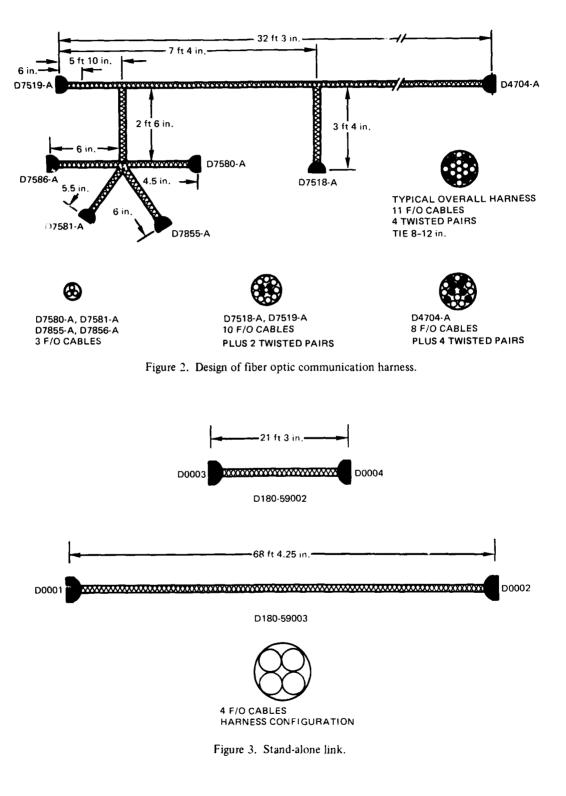
Table 1. Documentation for fiber optic interconnect systems.

The aircraft selected for this program was the E-3A, a military surveillance aircraft. A communication harness within the E-3A was selected for replacement with fiber optics. The basic design of the harness is shown in figure 2. All signal lines were replaced with fiber optic cables; the electrical power requirements were satisfied by conventional twisted-pair wire. The harness design, therefore, was hybrid in nature – consisting of bundle fibers, single fibers and twisted-pair wire. The harness was all point-to-point, with no couplers.

The stand-alone link (SAL) was designed using fiber optic cables only. The purpose of this link is for retrofit applications in which no fiber optic harnesses are required; just stand-alone cables. The configuration of this link is shown in figure 3.

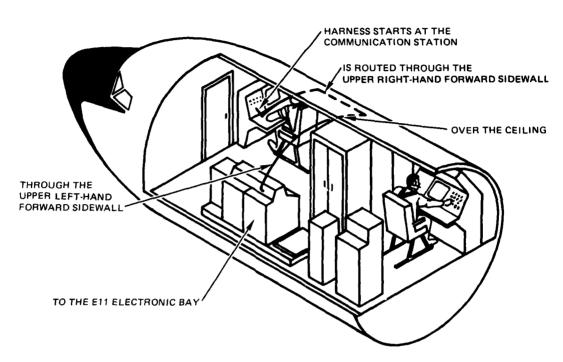
The routing of the harness is shown in figure 4. Figure 5 shows the relationship of both the harness and SAL to the E-3A aircraft. Originally, the SAL was intended to be designed for retrofit to the harness. However, it was decided to design a configuration that would go through a pressurized bulkhead into the wheel-well area. This configuration would provide additional information on routing and handling problems.

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Figure 4. Simplified details of the harness routing.

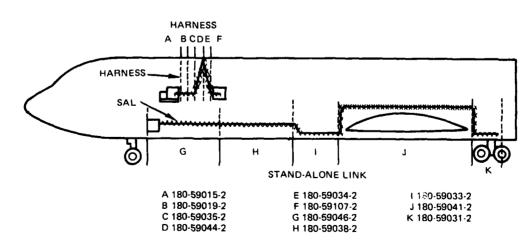


Figure 5. Routing of fiber optic harness and stand-alone link in E-3A aircraft.

SUMMARY OF TECHNICAL WORK

INTRODUCTION

A summary of technical work is presented on a phase-by-phase basis to provide continuity and to present program accomplishments in serial form over the two-year period. Further details of each phase may be found in references 1, 2, and 3.

PHASE I ACTIVITY

The Phase I activity initiated the development of the preliminary procedures/documentation and component selection for the cable configurations. Details of this activity are given below.

CONFIGURATION MANAGEMENT PLAN

A Configuration Management Plan was developed which set down the policies by which all drawings, documents, and deliverable hardware configurations were controlled and modified. The system program contained in D180-24693-7 designates the program manager as chairman and designates representatives from each of the line and staff functions for that board and the change board. The full plan is contained in appendix $\frac{1}{2}$ of that document.

COMPONENT SELECTION

Major components selected for the Phase I Link Designs (stand-alone link and harness) included four 4-terminal connectors, the fiber optics cable for the link, and seven (three 20-terminal and four 4-terminal) connectors plus fiber bundle cable, single fiber cable, and conventional wire for the harness. Relatively minor items including outer braid, tie materials, clamps, etc, are common shop stock and were selected as required on the program.

Connectors were chosen from three different vendors so that a broad base of connector types could be evaluated as to cost, availability, termination ease, suitability for manufacturing and assembly processes, optical properties, and environmental capability. The connector chosen for the stand-alone link was the Amphenol 4-terminal unit which is compatible with the heavy duty fiber optics 46-mil bundle cable required by the RFQ for this application. The connectors chosen for the harness include three 20-terminal Hughes C-21 rectangular jackscrew units capable of mating single fiber, 46-mil fiber bundle (medium duty) and conventional wire. The four 4-terminal connectors chosen for the harness were the ITT Cannon MIL-C-83723(PV) type, of which three were suitable for fiber bundle use and one was suitable for single fiber applications. All connectors for both links were supplied

^{1.} OR Mulkey, SP Suave, Final Technical Report – Phase I: Fiber Optic Interconnect System: Manufacturing Processes For (MTP), Boeing Document D180-24693-7, September, 1978.

LF Buldhaupt, SP Suave, OR Mulkey, Final Technical Report – Phase II: Fiber Optic Interconnect System: Manufacturing Processes For (MTP), Boeing Document D180-24693-14, February, 1979.

^{3.} LF Buldhaupt, SP Suave, OR Mulkey, Final Technical Report - Phase III: Fiber Optic Interconnect System: Manufacturing Processes For (MTP), Boeing Document D180-24693-15, December, 1979.

with suitable inserts and backshells. All connector assembly was done at Boeing, using standard polishing and terminating equipment plus special crimping and assembly tools peculiar to each of the connectors and cables. All connectors chosen met the contract requirements for aircraft environments.

The cables chosen for the links were of four types: single fiber, heavy duty fiber bundle, medium duty fiber bundle, and standard 22-gage twisted pair. The heavy duty and medium duty 46-mil fiber bundle cable was quoted by three manufacturers and was purchased from Valtec (based upon final pricing) during the next phase of the contract. The single fiber cable chosen (to be used in the harness) was of the large core type (8-10 mil core diameter) and was Galileo Type 3000 LC. This particular cable provided much better optical properties with respect to coupling losses and could be terminated with reasonable ease using any of the connector types chosen for the contract. The conventional wire vas drawn from stock.

SELECTION OF MILITARY TYPE AIRCRAFT AND CONVENTIONAL HARNESS

A contractual requirement was the selection of a suitable airframe or mock-up for the fiber optic interconnect installation. The airframe or mock-up was limited to one of the following:

- a. High performance fighter type aircraft
- b. Military surveillance aircraft
- c. Other aircraft which must perform in the military environment.

For this program, the aircraft selected was the E-3A, for which a full-scale, Class III mock-up was available.

A complex communication system cable harness was selected from the E-3A to be the conventional harness replaced by the fiber optic interconnect system. (See figure 4.)

PRELIMINARY INSTALLATION PLAN

The installation plan developed for use on this program was based upon the harness/ link designs discussed below, as well as the detailed installation procedure developed to provide the detailed information on each of the process steps involved in the assembly and installation process. (This updated installation plan is included as D180-24693-20, -21 (appendices A and B)). The installation plan details the routing of the cable through each of the sections of the airplane and is supported by production illustration drawings which illustrate all support points for each of the cables plus information on the pressure hull penetration and the conduit necessary for protection from the landing gear environment (for the case of the stand-alone link).

The installation methods were based primarily upon present methods used for conventional cable, utilizing special handling procedures developed for small-diameter coax cable and modified for fiber optics cable.

Particular problems during installation included:

- 1. Adequate protection of terminations during the pull.
- 2. Protection against shock.

- 3. Protection against strain.
- 4. Observance of minimum bend radius criteria.

Problems during the harness assembly operation included:

1. Proper termination and polishing.

2. Second end assembly (should this be done at the form board or back at the primary polishing/termination station?)

3. Protection of terminations during the assembly sequence.

4. Lower cost marking and identification methods compatible with the Tefzel cable covering.

FIBER OPTICS HARNESS/LINK DESIGNS

The two fiber optics designs are the stand-alone link and the seven-connector communications harness. The harness design was based upon the E-3A W1870 communication harness. This harness originally contained 114 terminations of wires, jumpers, shields, and grounds which was reduced to 56 terminations of fiber optics cables, wires, and grounds in the fiber optics/conventional wire hybrid version, while still meeting the EMI and TEMPEST requirements of the original harness. The connectors and cables chosen for this harness and the link are as described in the component selection section and appendix C. The link design was based upon discussions held with the customer and the contractual requirements of a straight point-to-point link for an add-on system containing 4 fiber bundle cables of the heavy duty type. The routing of this cable was intentionally chosen to include passage through a pressure seal, a midpoint disconnect, and exposure to the environmental extremes (such as weather, flying rocks, and hydraulic fluid) found in the landing gear area. This routing demanded that the routing procedures and the cable construction and protection (conduit) include not just the minimum needed to install a cable but also a full measure of procedures designed to provide maximum fiber optics cable utilization. It is believed that this goal has been met.

ROUTING TECHNIQUES

An analysis of the routing techniques for fiber optic interconnects was made using the routing criteria of conventional wire as a starting point. An assessment was made of hazardous/sensitive areas on the aircraft and the ability of fiber optics to be routed through these areas. Coupled with this analysis are the environmental constraints placed on the fiber optic system (per MIL-E-5400P requirements) and the ability of the fiber optic components to withstand this environment.

With proper attention to the cladding material, fiber optics can be routed through any hazardous or sensitive area within a military-type airframe. However, some areas exist which will prohibit either the detection or sourcing of fiber optic information. This is due to current limitation on the lifetime of sources/detectors as a function of temperature. Similarly, sources/detectors, and to some degree fibers themselves, are sensitive to radiation effects, although to varying degrees. Technology trends, however, show a gradual improvement in component parameters; it will become feasible (in the mid-1980's) to route fiber optics into, out of, and through all areas of the aircraft. The complete routing technique section is presented in D180-24693-5 (appendix N).

COST ANALYSIS

Acquisition cost estimates by models and by analysis of processes and techniques reflect potential cost savings for fiber optic interconnect systems as compared to wire harnesses. Since most models rely upon historical data and "conventional methods of business," it is implied that savings are realizable with technology maturity and with methods and techniques commonly employed.

Many options exist for production set-up and related costs. The most desirable option will depend on factors such as levels of business forecasts, advancement of the technology. demands on existing harness/cable production equipment and facilities, facility space available for expansion or relocation, economic posture of the company, etc.

The potential for cost improvement in the manufacturing/fabrication process is promising. The development of automated equipment and expedient techniques is needed to exploit this potential, however:

- Cost elements related to operations and support aspects appear to have offsetting effects.
- Cost savings are realized through weight and size advantages, while losses occur through added inventories, training, and special equipment requirements.
- Reliability considerations have a similar neutralizing effect.

The updated cost analysis is given in D180-24693-25 (appendix E).

PHASE II ACTIVITY

PRODUCTION/ACCEPTANCE PROCEDURE

This procedure detailed the inspection steps and equipment required for the fabrication phase of fiber optic cables and harnesses. Test points were detailed as far as the general requirements are concerned, but test limits were left to be included in assembly drawings and documents. This was necessary because limits for parameters such as cable loss are length dependent. The test hardware needed to perform the in-process tests was developed in prototype form. Level II drawings were prepared which detail all information necessary to reproduce the test equipment.

HARNESS ASSEMBLY DESCRIPTION

A description of the harness assembly procedures was developed which used as its basis the manufacturing plan for the particular harness. All cable drawings, form board drawings, cable lists, plug maps, termination procedures, connector assembly procedures, and details of the manufacturing processes are considered part of the manufacturing plan and are referenced by it.

HARNESS AND LINK ASSEMBLY

Based upon the harness and link designs developed in Phase I, a prototype harness and link were fabricated. No unusual problems were uncovered during this manufacturing cycle. The harness/link designs were then finalized in preparation of the actual production run. The final designs are shown in figures 2 and 3.

PRELIMINARY FIELD REPAIR TECHNIQUES

A field repair and maintenance specification was prepared which details the types of damage to cables, harnesses, and connectors. For each type of damage or contamination, the proper procedures for repair, cleaning, etc, are detailed, as well as the material requirements. In addition, before and after test requirements are detailed to assure the quality of the maintenance or repair and the integrity of the assembly.

PHASE III ACTIVITY

HARNESS AND STAND-ALONE LINK INSTALLATION

The prototype harness and the stand-alone link were successfully installed in the E-3A Class III mock-up using production personnel. The hardware was optically tested and photographed at a single contact level before and after installation to assure that no damage occurred. One section of cable was damaged by mishandling, but the optical link remained intact. The damage occurred when the installation personnel pulled on the fiber optic cable to gain more slack. This pulling was done without loosening the cable ties and the pulling motion was 90° to the cable tie.

INTERIM INSTALLATION PROCESS SPECIFICATION

The preliminary installation process specification (D180-24693-2) developed during Phase I of the program was used as the installation procedure for the two harness assemblies. All problems in this documentation were noted, and this information was used to revise the preliminary document to its present form as the interim installation process specification. This document was updated and used in Phase IV for the installation of the five production seven-connector harnesses.

The interim installation process specification was assigned document number D180-24693-16. This document covered the installation of the specific harnesses developed under this program. A general installation specification for all harnesses also developed during Phase I (D180-24693-3) was revised to reflect observations/problems during the mock-up activity. This document was numbered D180-24693-17.

INTERIM TEST REPORT (PRODUCTION/ACCEPTANCE PROCEDURE)

The Phase II production/acceptance procedure (D180-24693-8) was reviewed and modified for use in Phase IV cable fabrication and installation based upon this mock-up activity. No major problems were uncovered in this area. The interim production/accept-ance procedure was documented in D180-24693-18.

INTERIM FIELD REPAIR TECHNIQUES

The preliminary field repair techniques document (D180-24693-9) developed and issued during Phase II of the program was reviewed and modified as required to reflect technology and material changes. The interim document was D180-24693-19.

PROBLEM IDENTIFICATION

MATERIALS AND COMPONENTS. The primary problems relating to the materials and components selected for use during this phase of the contract were identification of viable sources and subsequent procurement. The only connector source willing to commit to development of a connector/backshell/terminus combination suitable for use was Hughes. Other vendors either did not have sufficient engineering personnel available or were not structured to provide the support required. Two cable manufacturers had the necessary background and production experience to bid on the bundle cable requirements, and the lower cost type was selected. Only one company bid on the single fiber cable but did not deliver. To provide a suitable cable in time to support connector development, an alternate source (Siecor) was selected.

INSTALLATION EQUIPMENT, PRACTICES, AND PROCEDURES. Installation of the harnesses was a relatively smooth operation marred by the one incident of cable harness damage during positioning of the stand-alone link. In this incident, the harness bend radius restrictions were violated. The installation specification was modified to reiterate in stronger terms the requirements on bend radius and the warnings and instructions on radius limits.

TESTING AND TEST EQUIPMENT. Test methods and equipment documentation were modified to remove optical power measurement tolerance limitations on detectors used for continuity tests, as it was not felt necessary or cost effective to impose an accuracy limit on this test.

HARNESS ASSEMBLY, TESTING, AND DESIGN. No significant problems were encountered in this area.

ENGINEERING DRAWINGS

The engineering drawings developed for installation of the harness during Phase III were revised to reflect the changes in materials and processes required for the cables and connectors used in the revised harness.

PHASE IV ACTIVITY

SUMMARY OF LINK DESIGNS

All design documentation for the 20 fiber bundle/single fiber/wire hybrid harnesses Part No, F0-0004 and the one single fiber/wire hybrid harness is contained in D180-24693-25 (appendix F) and the supporting documentation listed in that document. As described earlier in this report, these 7 connector harnesses were designed as a direct replacement for the W1870 harness used in the E-3A aircraft. The harness configuration, parts list and interconnection list, and assembly method are illustrated in Drawings 180-59004 and 180-59005, part of the -25 document.

COST ANALYSIS

Life cycle cost comparisons for fiber optics and wire interconnect systems are assembled under the three major cost categories of design, development, test, and evaluation (DDT&E), production, and operation and support (O&S). (See appendix E.)

Cost comparisons for a small quantity of interconnect systems typical of a DDT&E portion of a program revealed that fiber optics interconnect systems offer a potential cost savings. Some key considerations in the cost comparison include:

1. The estimated reduction in engineering, primarily through the reduced complexity of the fiber optic system

2. An estimated equality in manufacturing when baselined to a small scale manual assembly process for each type of interconnect system

3. An estimated reduction in fiber optics parts and material costs consistent with present cost projections for large quantity purchases

4. The manufacture of fiber optics systems with pre-established specifications, standards, and processes

Analysis of cost data for production set-up and manufacture of a large quantity of wire and fiber optics interconnect systems revealed that new procedures and processes required for fiber optics systems are dominant cost factors. Consequently, cost effective large scale production depends upon development of tools, equipment, and techniques.

Analysis of cost data for operation and support revealed that advantages of savings in size, weight, and complexity would yield cost benefits in operations and maintenance to offset initial investment costs for special tools, equipment, training, parts, repair materials, and added inventory.

SUMMARY OF FINAL INSTALLATION PLAN

The installation plan is contained in two document sections: D180-24693-20 (appendix A), a general installation procedure for all fiber optic cables and harnesses, and D180-24693-21 (appendix B), an installation procedure specifically for the 180-59004 and 180-59005 (F0-0004 and F0-0005) harnesses. The general procedure covers all phases of the fabrication and installation of harnesses and includes separate appendices which cover harness identification, fabrication, detailed installation procedures, and harness marking.

No revisions other than typographic were required in the "general" document. The "specific" document was revised to include the single fiber cable installation and to delete references to the "stand-alone link" installation which had been completed earlier in the program (Phases II and III). No technical changes to the process were necessary.

SUMMARY OF FINAL PRODUCTION/ACCEPTANCE PROCEDURE

This procedure is contained in D180-24693-22 (appendix C) and lists the procedures for the in-process and final tests of all fiber optic cables and harnesses. Test methods covered include continuity, insertion loss; and visual inspection details of the tests and test limits are included in the Assembly Drawing 180-59004 and -59005. No changes were necessary in the -22 document.

SUMMARY OF FIELD REPAIR AND MAINTENANCE PROCEDURE

This procedure is contained in D180-24693-23 (appendix D) which lists facilities and maintenance methods for all types of fiber optic cables and harnesses. Specific maintenance methods include avoidance of:

Contamination Abrasion Cuts/Breakage Connector Damage

No revisions were required in this document during the fourth phase of this contract.

PROBLEMS ENCOUNTERED DURING THE PROGRAM

CABLE PROCUREMENT. Procurement attempts for the single fiber and fiber bundle cable indicated only one viable source (Galite) for the single fiber cable and several sources for the bundle cable. Galite was chosen as the sole source for the single fiber cable and as lowest bidder for the bundle cable. Orders were placed early in the program (July, 1979) and the bundle cable was received in September, well within schedule. As the single fiber was not received shortly afterwards, checks were made to determine progress. Initial checks indicated delivery, but further investigation revealed that the order had been misplaced and that no cable was available or in process and that no delivery could be promised for 4 months. As this would not support the intended contract schedule, new sources were sought and an order was placed with Siecor for 600 m of their type 155 cable which was in stock. This cable was received and samples were shipped to Hughes, the connector supplier. for their use in designing the connector accessories for the contract. In December, Boeing was informed by Siecor that the furnished cable "had problems" and should not be used. No immediate reasons were given but answers were expected early in January. At this time Hughes was put on hold and another supplier was sought for backup. Galite promised quick delivery and when at the end of January Siecor could not replace the fiber an order was placed to Galite. Delivery of the cable, mid-February, was not per schedule, however, so that connector development was slowed until mid-March when production of the harnesses was started.

CONNECTOR PROCUREMENT. Of the three connector manufacturers identified as being capable of providing connectors of the type required (Amphenol, Cannon, and Hughes), only Hughes responded positively with designs providing adequate strain relief, termination ease, and hermeticity. Hughes was, therefore, selected to provide all connectors for the harness assembly. Two connector types were used, the C21 series 20 contact connector with a larger backshell and a new circular 4-contact connector with integral backshell and positive strain relief. Termination methods for both connectors and both cable types were provided by Hughes and refined by Boeing to meet the production environment to the extent possible. Connector and related hardware deliveries were slower than scheduled but hardware was available to meet production schedule.

PRODUCTION. This phase of the contract was completed using personnel from Boeing Aerospace Company production wire and cable shops. All personnel, including quality assurance, had to be trained in all phases of the production processes different from conventional wire technology. A flow diagram of the manufacturing cycle is shown in figure 6.

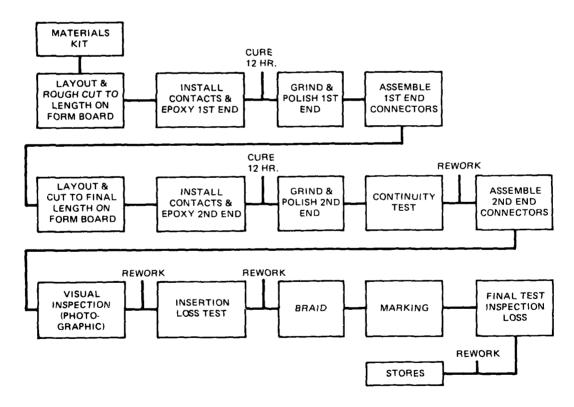


Figure 6. Assembly flowchart, fiber optic harnesses.

All assembly and process steps were optimized and tooling was modified or developed to meet assembly requirements. The grinding and polishing operation was slower than expected and required 3 to 4 minutes for the grind operation and the same for the polish step. The special contact holding fixtures developed by Hughes for these operations tended to clog up and had to be disassembled and cleaned at least once a day, slowing the grind/polish operations.

Wear on some of the inner surfaces of the contact made insertion both difficult and hazardous to the contact. Hughes provided new tooling and repaired the old tools with updated internal parts, which helped the situation later in the program. Hughes in all cases proved to be responsive and helpful in all connector related problems during the program.

The epoxy used in the termination process (BI Pax 2143D) was a viscous material deliberately chosen so to prevent wicking in the termination of the bundle contacts. The high viscosity slowed the application process considerably but the results made it worthwhile. This epoxy also was a room cure (12-hour) type so that the curing type affected flow rates through the production cycle.

The termination of the bundle fiber contacts involves the use of added shrink tubing to protect the fibers at the contact end. Use of the tubing fitted over the end of the contact prevents use of a conventional insertion tool so that special tooling and techniques were required to accomplish the contact insertion and to prevent damage to the cable, fibers, or heat shrink tubing. The single fiber cables, because of the buffer coating and small internal jacket which fit inside the contact barrel, did not require additional sleeving and could be terminated with the standard tooling at a much faster rate.

Harness handling and contact protection during the production sequence was a constant problem throughout the program in that additional time was required to prevent damage to the harness. Use of a multiple contact polishing jig for mass termination finishing would do much to speed the process and to cut down on potential damage.

Inspection of the harness during the production sequence consisted of standard monitoring of strip lengths, crimps, and workmanship items as well as the fiber optic peculiar tests, which were continuity, insertion loss, and visual inspection. The visual inspection operation for terminated bundle cables was the only difficult operation as it required a photograph be taken of each contact. Use of the camera microscope developed by Boeing QC during the second phase of the program speeded the photographic steps, but the time spent in the operation and the counting time was significant in the total cable construction time. Again, as this step is not required with the single fiber cable, the cost advantage of single fiber cable is increased.

ENGINEFRING DRAWINGS

All drawings (top. form board, and production illustration) for the seven-connector harness and its installation were revised to reflect process changes and materials changes from the previous stages of the contract. The revised drawings are included as a part of the contract deliverables (CDRL Item D0004).

CONCLUSIONS

Successful completion of the final phase of this program has demonstrated that fiber optic cables and harnesses can be fabricated in a production mode and installed in military aircraft using techniques quite similar to those used in conventional wire harness technology. Fabrication of the harnesses can be accomplished in a production environment using shop personnel trained and skilled primarily in conventional wire technology. Tooling and equipment necessary for the fabrication in a very high production mode have not yet been developed, as no requirement has yet been forthcoming, but these items have been identified and costed. Further development still needs to be accomplished in the tooling and equipment for lower volume production, if fabrication costs are to be minimized.

Hardware (connectors and cables) available today is adequate for military aircraft installation but is not yet optimized. Right-angle connectors are not yet available, but will be required. Strain relief methods are adequate but tend to increase assembly time and are costly, complex, and larger than desired. Terminations are still the most driving cost item. Cabling available today will meet requirements but can still be further optimized for aircraft use. Large core $(100\mu-200\mu \text{ dia.})$ fibers now coming on the market appear to be ideal for this use, and if jacketing materials are chosen properly then high performance cables can be manufactured. The further use of bundle fibers is not recommended as their cost is high, performance is low, and termination/inspection cost is higher in multicontact connectors when compared to state-of-the-art single-fiber cables.

Test equipment now on the market (such as portable power meters and optical time domain reflectometers) can be utilized for harness test and checkout in the shop and in the field. Optical equipment for visual inspection purposes is not yet commercially available. Boeing-designed test equipment (Phase II) will accomplish the task, as proved on this program, but the inspection task would be reduced considerably with the use of single-fiber technology by the elimination of broken fiber count and packing fraction related inspection. Field repair techniques currently available work and are acceptable. Hand termination, using a kit of selected grinding and polishing materials. is not much slower than mechanical finishing. Epoxy cure time can be in the 5-minute range with selected materials, but these materials need to be evaluated for suitability over the expected environmental range of the system.

RECOMMENDATIONS

- Initiate a manufacturing technology program to address the entire spectrum of the termination operation, including automated grind/polish operations, mass polishing techniques, tooling, ultimate producibility, and cost.
- Initiate a program whose objective would be elimination of epoxy in connector designs.
- Initiate a manufacturing technology program on fiber optic transmitter/receiver subsystems so that the entire cost of manufacturing a fiber optic system (transmitterinterconnect-receiver) can be determined.
- Develop and optimize volume production processes for the fabrication of fiber optic harnesses using large core single fiber technology.
- The above program should be a joint effort involving not only the system integrator but both cable and connector suppliers.
- Use the present set of harnesses in a test program to determine the capabilities of the current technology in the area of environmental/mechanical and application stress.
- Expand the technology to include that necessary for the use of fiber optics in shipboard applications.

REFERENCES

- OR Mulkey, SP Suave, Final Technical Report Phase I: Fiber Optic Interconnect System: Manufacturing Processes For (MTP), Boeing Document D180-24693-7, September, 1978.
- LF Buldhaupt, SP Suave, OR Mulkey, Final Technical Report Phase II: Fiber Optic Interconnect System: Manufacturing Processes For (MTP), Boeing Document D180-24693-14, February, 1979.
- LF Buldhaupt, SP Suave, OR Mulkey, Final Technical Report Phase III: Fiber Optic Interconnect System: Manufacturing Processes For (MTP), Boeing Document D180-24693-15, December, 1979.

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APPENDIX A

FINAL INSTALLATION PROCESS SPECIFICATION (General)

D180-24693-20

FINAL INSTALLATION PROCEDURE (GENERAL)

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O. R. Mulkey

Boeing Aerospace Company P.O. Box 3999 Seattle, Washington 98124

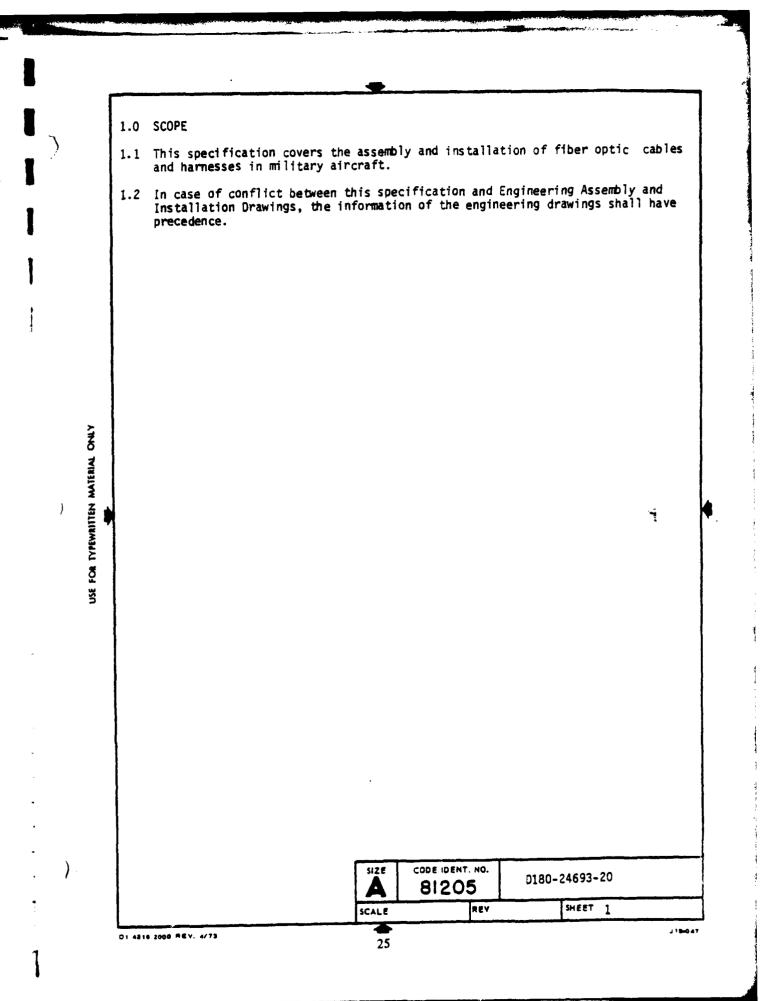
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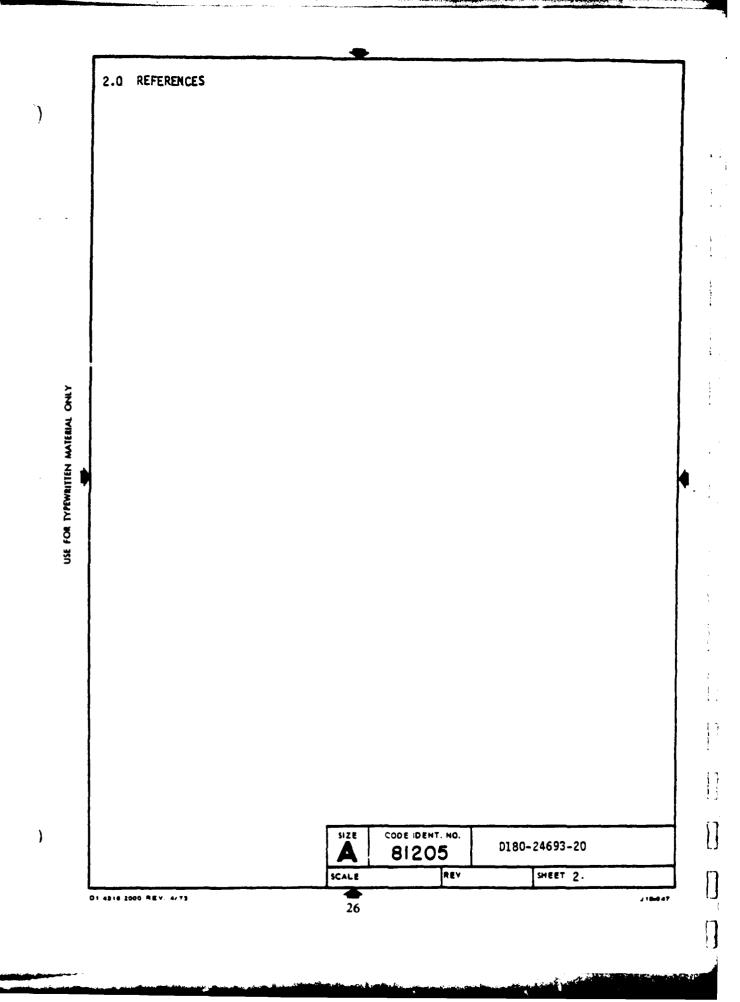
Final Report for Period 16 December 1979 Through 4 June 1980 Phase IV of NOSC Contract N00123-78-C-0193

Prepared For:

NAVAL OCEAN SYSTEMS CENTER Code 9313 San Diego, California 92152

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4.0	ASSEMBLY OF FIBER OPTIC CABLES AND HARNESSES
4.1	CABLE IDENTIFICATION (Marking)
4.1.1	Physically identify cable as follows:
	 Include in each identification all the information specified by the Bundle Assembly Drawing.
	 Where the Bundle Assembly Drawing specifies identification of the bundle number and cable number, use only the hot embossing on sleeve or tape methods of Appendix A.
4.1.2	Cable Identification Sleeves and Tape
4.1.2.1	a. Identification of cables by means of sleeves or tape is required wit 6 inches of the terminating points and within twelve inches of each side of a pressure bulkhead.
	b. Identification of unmarkable cables by means of sleeves or tape is required only at terminating noints and may be staggered up to twelv inches from termination points to reduce bulk and within twelve inch of each side of a pressure bulkhead.
	c. For cable bundles using protective "Expando" sleeving over the cable or harness, the cable identification sleeves or tape may be staggere up to a maximum of twelve inches from termination points to reduce bulk.
4.1.2.2	Include color coding as indicated by the Bundle Assembly Drawing on identification sleeve or tape when these are installed around a multi- conductor cable. No color coding is required when the identification sleeve or tape is used on individual cables of a bundle.
4.1.2.3	Add identification sleeves to unidentified cables on vendor furnished components when numbers are required by the Bundle Assembly Drawing.
	 Imprint the cable numbers assigned by the Bundle Assembly Drawing on the identification sleeves.
	Locate an appropriate sleeve on each cable within three inches of th component.
4.1.2.4	Where heat shrinkable sleeving is used for cable identification, the act shrinking operation is required only where necessary to prevent the slee from sliding out of position on the cable during normal service.
4.1.2.5	When marking RT 876 heat shrinkable sleeving, use a type temperature of $500 \pm 25^{\circ}$ F. Regulate the machine pressure and dwell time to provide the maximum pigment transfer from foil to sleeve.
4.1.2.6	Quality Control shall determine, on a surveillance basis, that the impressions are clear and legible.
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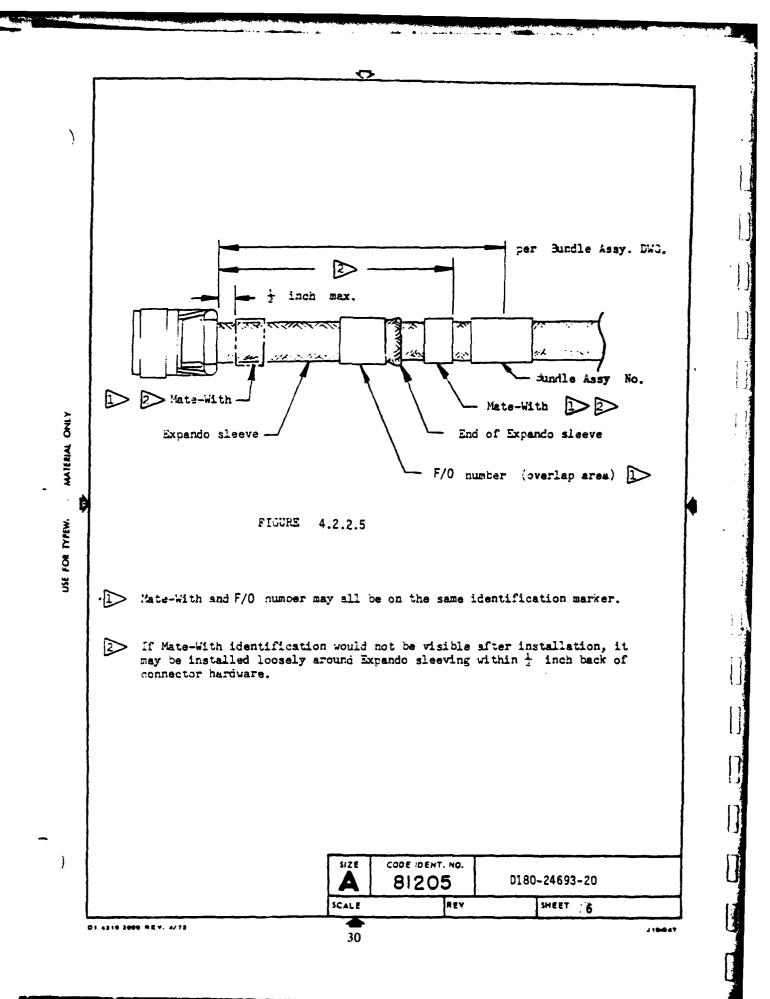
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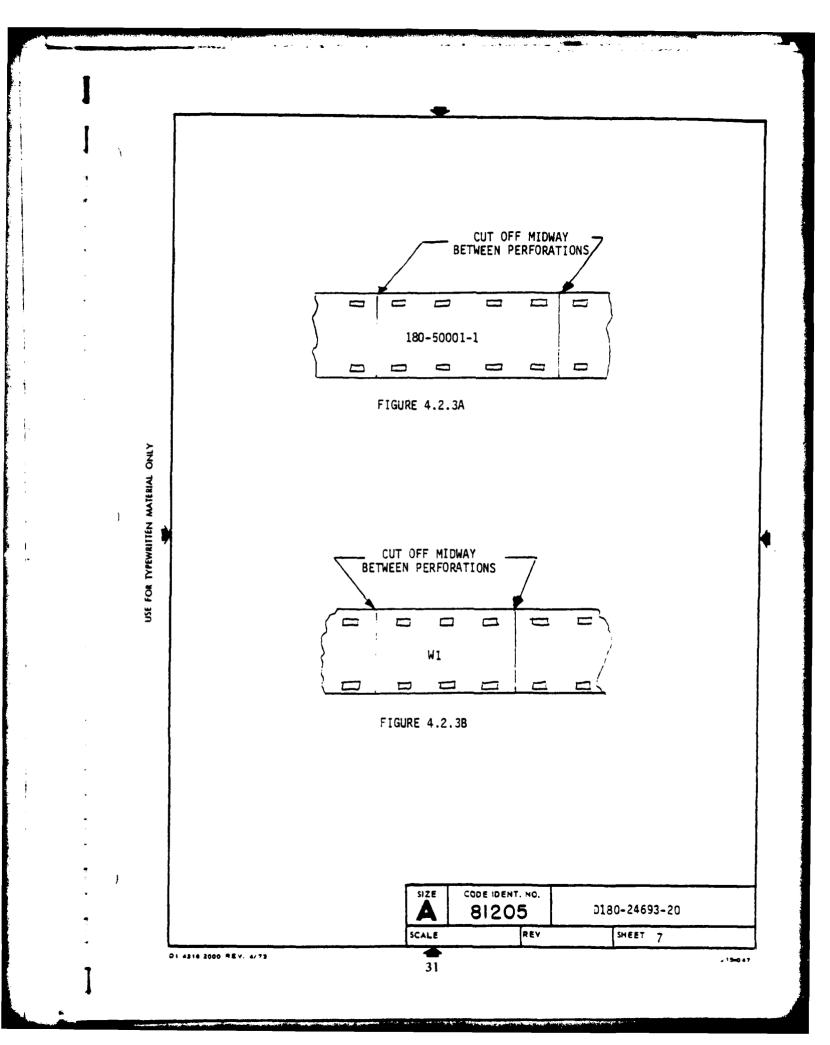
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CAUTION -	- SLEEVE MATERIAL USAGE IS DETERMINED BY TEMPERATURE TYPE I OR TEMPERATURE TYPE II, AND HYDRAULIC FLUID OR NON-HYDRAULIC FLUID AREAS.			
4.2.3.1	'T&B' 650-51983 nylon perforated tape (or equivalent) imprinted with the information along the length of the tape and centered with respect to th tape perforations shall be optional material. See Fig. 4.2.3A and 4.2.3			
4.2.3	Materials for Cable Bundle Identification Markers.			
	NOTE: Mate with and F/O No. may all be on the same identification marke			
4.2.2.5	For cable bundles with protective "Expando" sleeving, the F/O number (yellow wire bundle ID) shall be installed in the overlap area per Figure 4.2.2.5.			
4.2.2.4	Sundle F/O number markers shall not be used on cable bundles that contai any cable that can be marked by direct imprinting.			
4.2.2.3	Bundle F/O number markers may be placed from six to twelve inches from the bundle terminations and at six foot intervals throughout the length of the cable bundles that contain only cables that cannot be marked by direct imprinting.			
	EXAMPLE: $180-50001 = F/01$ 180-51121 = F/01121			
7,6,6,6	four digits of the Bundle Assembly Drawing number with the leading zeros omitted.			
4.2.2.1	Cable bundle F/O numbers shall be placed on cable bundles per Appendix A Bundle F/O numbers shall consist of the letter F/O followed by the last			
4.2.2	Cable bundle F/O number.			
	Bundle Assembly Drawing. Markers shall be located at one end of the bundles if locations are not given by the Bundle Assembly Drawing.			
4.2.1.3	numbers and dash numbers. Example: 180-50101-1			
4.2.1.2	Bundle assembly part numbers shall consist of Bundle Assembly Drawing			
4.2.1.1	Bundles shall be part numbered per 4.2.3.			
4.2.1	Bundle Assembly Part Number			

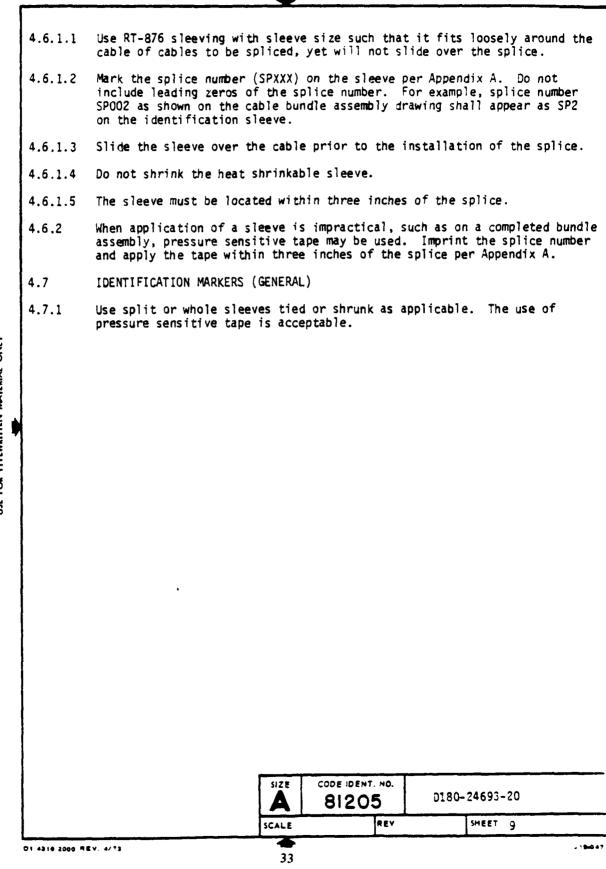
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4.3.1	Production illustration (PI) reference points shall be identified per Appendix A.		
4.4	SPECIAL INFORMATION MARKERS		
4.4.1	Install special information markers on individual cables or on entire bundles as specified by the Bundle Assembly Drawing.		
4.4.2	Locate the markers as near the end of the cable or bundle as possible - unless otherwise noted in the Bundle Assembly Drawing.		
4.4.3	Use the materials and installation methods as specified for connector information by Appendix A.		
4.4.4	Imprint on the marking media that information which is specified by the Bundle Assembly Drawing.		
4.5	CONNECTOR IDENTIFICATION		
4.5.1	a) A "Mate With" tape is required for all plugs and receptacles that are not identified with a "P" or "J" suffix. The "Mate With" information on the tape shall match the equipment item numbers shown in the parts list of sheet 1 of the Bundle Assembly Drawing.		
	b) Mate-With tape is not required on seal fittings.		
4.5.2	Identification of equipment mating connectors will be per Appendix A.		
4.5.3	In-line connectors will be identified per Appendix A, normally the "Mate-With Dxxxx" notation will be omitted.		
4.5.4	Use of nylon tags, per Para. 4.2.3, for connector identification in Type I and Type II temperature areas and in either hydraulic fluid or non- hydraulic fluid area is permitted.		
4.5.5	For bundles with protective Expando sleeving, the Mate-With tape or sleeving shall be installed per Figure 4.2.2.5. When the PI markers are located in the Expando area 18 inches back of the connector or on a short cable bundle with Expando on the entire bundle, the PI marker shall be installed tight and secured with a bundle tie, making the flag marker stationary at the location specified by the Bundle Assembly Drawing.		
4.5.6	Connector identification markers are not required when connectors are attached permanently to support plate with connector identification marked thereon. "Mate-With" information is not required.		
4.6	SPLICE IDENTIFICATION		
4.6.1	Where physical identification of a cable splice is specified by bungle assembly or bundle installation drawings, identify the splice as follows:		
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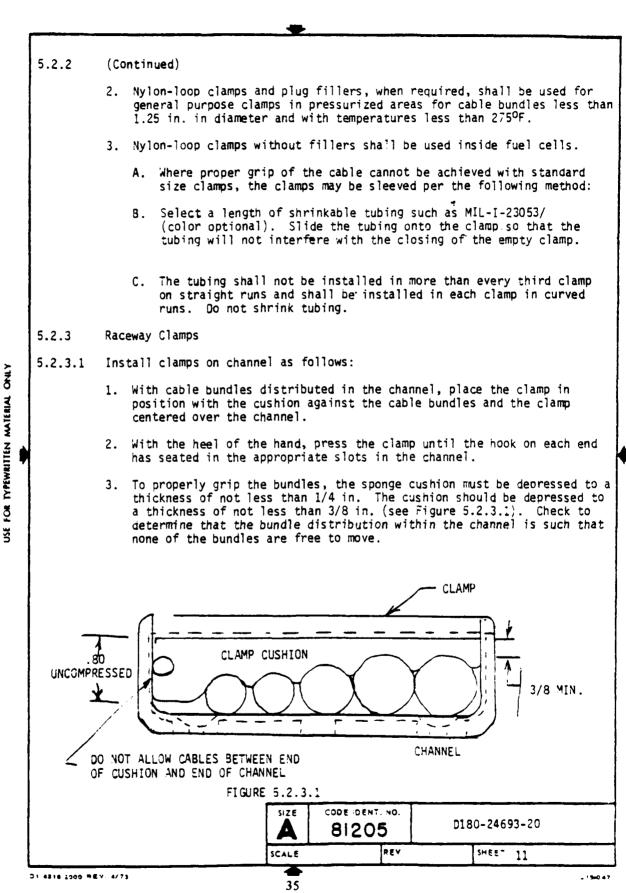
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5.0	INSTALLATION OF FIBER OPTICS CABLES AND HARNESSES					
	NOTE: Mixed electric and fiber optic cables must be installed using applicable practices for electrical cables plus these extra installation notes applicable to fiber optics.					
5.1	ROUTING OF CABLE BUNDLES					
5.1.1	Install all cables per Appendix C except as noted.					
5.1.2	Install cables with sufficient clearance to prevent chafing of the installed bundles against sharp edges of structures, equipment, etc. (1/8 in. clearance minimum unless secondary protection is provided by engineering drawing). Normal bundle slack may require 3/4 in. separation to account for vibration and bundle movement.					
5.1.2.1	When not specifically controlled by engineering drawings, slack portion of bundles may contact smooth flat surfaces and smooth radii 1/8 in. or larger of either metal or plastic. This does not apply to the engine area.					
5.1.2.2	Fiber optic cables may be scuffed on the surface without degradation of performance. Scratches deep enough to damage reinforcing braid are rejectable.					
5.1.3	Bundles shall not be tied together unless required to provide support for small bundles. When structure for clamping is not available, bundles per above shall be tied to adjacent cable bundles to achieve support.					
5.1.4	Reference Point Indicators (PI Markers) for Production Facility.					
5.1.4.1	When reference point indicators are specifically called out on the installation drawing, (not all bundle assemblies through a reference location are considered critical at that point) locate the reference point indicators on the side of the support device indicated by the cable bundle installation drawing. The gap between the support device and the near edge of a green indicator will be $1/2$ in. $\pm 1/2$ inch. Do not use green indicators in fuel tanks.					
5.1.4.2	Allow Reference Point Indicators under the Protective Sleeving.					
5.2	CABLE SUPPORTS					
5.2.1	Cable bundles shall be supported by channel raceway clamps or loop clamps as specified on the wire provisions installation drawings. Bolt and nut installation shall be per standard practice.					
5.2.2	Loop Clamps shall be installed as follows:					
	 Cushion-loop clamps (such as ADEL part number 5095_) shall be used for general purpose clamps in nonpressurized areas and for the following special applications in pressurized areas: 					
	A. Bundles in high temperature areas (275 ⁰ F or greater) B. Bundles 1.25 in. in diameter or larger					
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Where a short channel is not available, allow trimming of a longer part to 5.2.3.2 the dimensions of the required shorter part. Break sharp edges of reworked area. 5.2.4 Nylon Clamps 5.^.4.1 Where nylon clamps are specified use only Olympic Plastics Co. or Peco Manufacturing Co. clamps as required throughout the airplane. 5.2.4.2 When a nylon clamp is used with a NAS 42 spacer or a metal stand-off, install washers as shown in Figure 5.2.4.2. CAUTION: Do not use washers within a fuel tank. WASHER (REFERENCE) -NYLON CLAMP NAS 42 SPACER OR ZIZ METAL STAND-OFF MATERIAL FIGURE 5.2.4.2 TYPEWAIFIEN 5.2.5 Flip Type Grommet (NAS 1368N) õ 5.2.5.1 Install flip grommets with Western Sky Industries tools WSI-T-3 or WSI-T-32 or WSI-HT-3 through WSI-HT-32 or equivalent. ŝ 5.2.5.2 To replace a damaged flip grommet, carefully cut the damaged part out of the hole in structure and install a new grommet with the tool specified in Paragraph 5.2.5.1. 5.2.5.3 If cables are installed through the damaged grommet, cut the grommet as required to remove it from the cables. Install the replacement grommet as follows: 1. Flip the grommet with tool specified in Paragraph 5.2.5.1. 2. Split the grommet as shown in Figure 5.2.5.3 using a sharp knife or razor blade. 3. Apply adhesive to the grommet. 4. Install the grommet around the cable and in the hole of the structure. CODE IDENT. NO. SIZE 0180-24693-20 Д 81205 SCALE REV SHEET 12 Ŧ 01 4316 2000 REV. 4/73 . 1940 47 36

	CUT IN SLANT DIRECTION NAS 1368N					
	FIGURE 5.2.5.3					
5.2.6	Use NAS 603-() screws for installation of all single lobe wire bundle support clamps.					
5.2.7	Dakota Cab-L-Tite Clamps shall be installed as follows:					
	 Select a Cab-L-Tite clamp size which will provide a minimum of one notch above both ends of the keeper when installed. 					
	Select countersink screw or hex head bolt as applicable. Insure that the head of the fastener does not protrude above the base of the clamp into the cable gripping area.					
	 Mount Cab-L-Tite clamp as specified by installation drawing, lay cable bundle in clamp and install keeper, insuring bundle is securely held. 					
5.3	REPAIR OF FIBER OPTIC BUNDLE					
	 If the outer jacket has minor scuffing such that the inner strength member braid is not exposed, apply a coating of Vyna-Kote No. 6 (Spectra-Strip Wire and Cable Corporation, Garden Grove, California). 					
	 If the outer jacket is scuffed such that the strength member braid is exposed but is not damaged, apply one coat of Vyna-Kote No. 6 and allow to dry for 3-5 minutes. Wrap area with .033007 fiberglass tape, tie ends with nylon or dacron cord and cover with another coat of Vyna-Kote No. 6. 					
5.4	RACEWAYS AND CONDUIT					
5.4.1	Position cable bundles within raceways as specified in cross-section views on the Wire Bundle Installation Drawings.					
5.4.2	Mark and install pull-cord as follows when specified on engineering drawings.					
	 Imprint the words "Pull-Cord" on one side of the pull-cord at not more than 15 in. intervals throughout its length using hot embossing machine with D11-51 black foil. Use Bently-Harris Mfg. Co. TG. 40 cord. Optional: Dodge Fibers Corporation TB303. 					
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5.4.2	(Continued)					
	 Install the pull-cord in the conduit or raceway with the excess length divided approximately equal and coiled at each end of the inaccessible area. Tie the two coils to the bundle with which it is routed. Do no include the pull-cord under any bundle ties or clamps. 					
	Replace the pull-cord per 1 and 2 above if for any reason it is used prior to delivery of the airplane.					
5.4.3	Cetyl Alcohol may be used as a lubricant for installations in conduit.					
5.5	BEND RADIUS					
5.5.1	Use the bend radii specified in Appendix C. Where the stiffness of a cabl bundle will not allow bending to the minimum, it is permissible to remove the bundle ties locally. After the bend is formed, retie the bundle per Appendix B. The bundle need not resume a round, cross-section in the bend area.					
5.6	FUEL TANK BUNDLES					
5.6.1	Do not use cable bundle ties within any fuel tank area.					
5.6.2	Do not use tapes or tied-on markers on cable bundles within any fuel tank area.					
5.6.3	Wire bundle clamps within fuel tanks shall be procured from the Olympic Plastics Co or the Peco Manufacturing Co.					
5.7	CONNECTOR INSTALLATION					
5.7.1	Install connectors with the major keyway in the "UP" or "FORNARD" position unless otherwise noted on drawing.					
5.7.2	Torque all firewall connector coupling rings per supplier's specification prior to lockwiring.					
5.7.3	Where the drawing specifies application of a "red dot", the coupling nut of threaded coupling connectors shall be safety wired.					
	NOTE: Safety wiring or otherwise mechanically locking is required to prevent loosening under vibration when installed in engine nacelles in other areas of severe vibration (excluding those on shock-mounte equipment), and in areas which are normally inaccessible for periodic maintenance inspection of the aircraft.					
5.7.3.1	The "red dot" shall be 1/2 inch diameter painted or affixed on the structure adjacent to each connector. The material of the painted "red dot" shall be protective enamel. Color shall be "red" #11136 per federal standard 595, or equivalent.					
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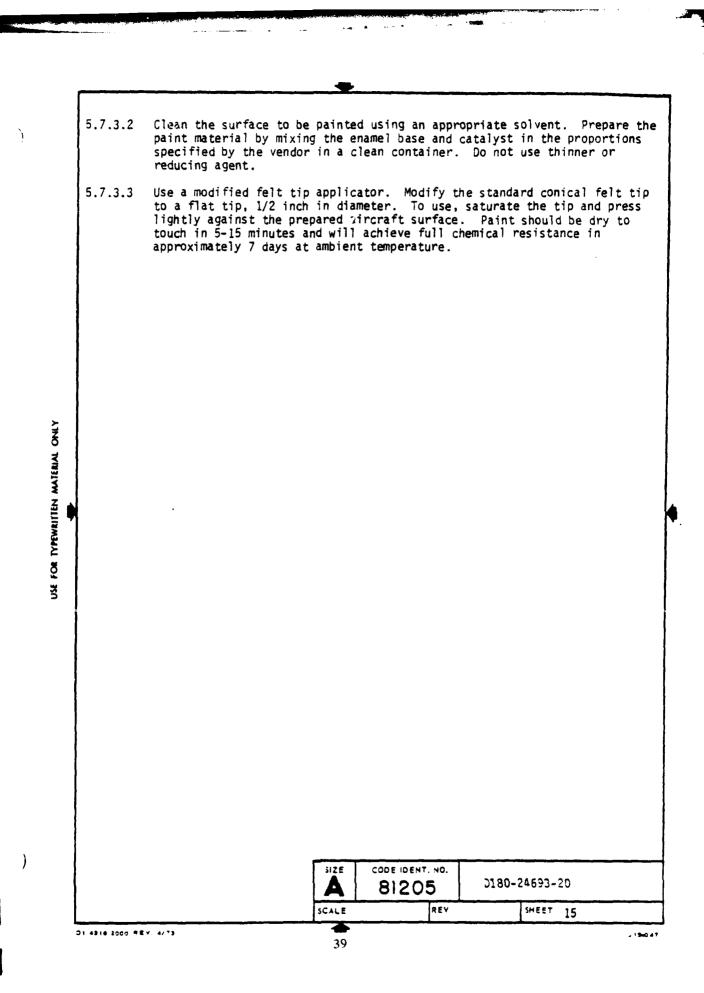
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	SCALE REV SHEET 16
	SIZE CODE IDENT. NO. D180-24693-20
	a. To prevent fluids or contaminants from entering junction boxes, connecto or other enclosed items, use drip loops unless potting is used in such a way as to accomplish the moisture barrier.
6.2	Orip Loops
6.1.8	Make sure that there is sufficient separation from adjacent suffaces so that bundles with normal slack will not make contact.
6.1.8	effect is least obvious to the inspector. Make sure that there is sufficient separation from adjacent surfaces so that
6.1.7	Normal expansion and contraction of the airplane should not exert strain on the bundle. This is especially critical in long straight runs where the
6.1.6	On shock mounted equipment, the bundle slack should provide for full travers of the equipment without transmitted strain to the bundle.
6.1.5	Slack for normal coupling and uncoupling of connectors should be provided.
6.1.4	Where equipment may be removed with the bundle installed, sufficient slack should be available to provide operating clearance during rework.
6.1.3	The bundle shall be free about hinge joints with sufficient slack to prevent binding when the hinge is fully opened.
6.1.2	The bundle slack shall be evenly distributed between P.I. location markers. The additional slack for retermination should be included in the slack of th first 6 feet at each end of the bundle.
6.1.1	Sufficient length of individual conductor lengths shall be available for 3 reterminations. This results in additional bundle slack.
6.1	SLACK
	When the installation of the cable is complete per the Wire Bundle Assembly, the installation procedure and this document, the quality control department shall inspect the finished installation to assure the bundle has been installed in a workmanlike manner. The installation shall be specifically examined for the following:

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USE FOR INPEWRITTEN MATERIAL ONLY

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 6.3 Bend Radius The bend radius shall be no less than 6 times the finished cable diameter 1.5 inches (3 inch bend diameter), whichever is greater. 6.4 Bundle and Cable Support Cable clamps must be compatible with the area where the cable is install and the smallest which will hold the bundle without crushing or pinching cable, but will not permit abrasive movement. 6.5 Coupling of Connectors a. Make certain that the plugs and receptacles are properly mated and for coupled. Check for tightness by hand and <u>only</u> in the direction of coupling. On bayonet types the locking pin should be visible. b. Check that safety wiring is installed properly. c. Make certain that the connector number and mate-with information are drawing. 6.6 Bundle Identification Check that cable and bundle marker tapes or sleeves, and marks on cable per drawing and do not penetrate the cable jacket. 6.7 Optical/Electrical Tests Prior to closure of the connectors, check continuity and insertion loss	6.2	(Continued)
 The bend radius shall be no less than 6 times the finished cable diameter 1.5 inches (3 inch bend diameter), whichever is greater. 6.4 Bundle and Cable Support Cable clamps must be compatible with the area where the cable is install and the smallest which will hold the bundle without crushing or pinching cable, but will not permit abrasive movement. 6.5 Coupling of Connectors a. Make certain that the plugs and receptacles are properly mated and f coupled. Check for tightness by hand and <u>only</u> in the direction of coupling. On bayonet types the locking pin should be visible. b. Check that safety wiring is installed properly. c. Make certain that the connector number and mate-with information are drawing. 6.6 Bundle Identification Check that cable and bundle marker tapes or sleeves, and marks on cable per drawing and do not penetrate the cable jacket. 6.7 Optical/Electrical Tests Prior to closure of the connectors, check continuity and insertion loss the cables and visually inspect the interface per D180-24693-18. Electrine 		b. Locate drip loops so that fluid will not drip on electrical equipmen
 1.5 inches (3 inch bend diameter), whichever is greater. 6.4 Bundle and Cable Support Cable clamps must be compatible with the area where the cable is install and the smallest which will hold the bundle without crushing or pinching cable, but will not permit abrasive movement. 6.5 Coupling of Connectors a. Make certain that the plugs and receptacles are properly mated and f coupled. Check for tightness by hand and <u>only</u> in the direction of coupling. On bayonet types the locking pin should be visible. b. Check that safety wiring is installed properly. c. Make certain that the connector number and mate-with information are drawing. 6.6 Bundle Identification Check that cable and bundle marker tapes or sleeves, and marks on cable per drawing and do not penetrate the cable jacket. 6.7 Optical/Electrical Tests Prior to closure of the connectors, check continuity and insertion loss the cables and visually inspect the interface per D180-24693-18. Electri 	6.3	Bend Radius
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Prior to closure of the connectors, check continuity and insertion loss the cables and visually inspect the interface per D180-24693-18. Electri		
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	6.7	per drawing and do not penetrate the cable jacket.
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SIZE CODE IDENT. NO. 81205 0180-24693-20	6.7	per drawing and do not penetrate the cable jacket. Optical/Electrical Tests Prior to closure of the connectors, check continuity and insertion loss of the cables and visually inspect the interface per D180-24693-18. Electric cables are tested per a separate specification. SIZE CODE DENT. NO.

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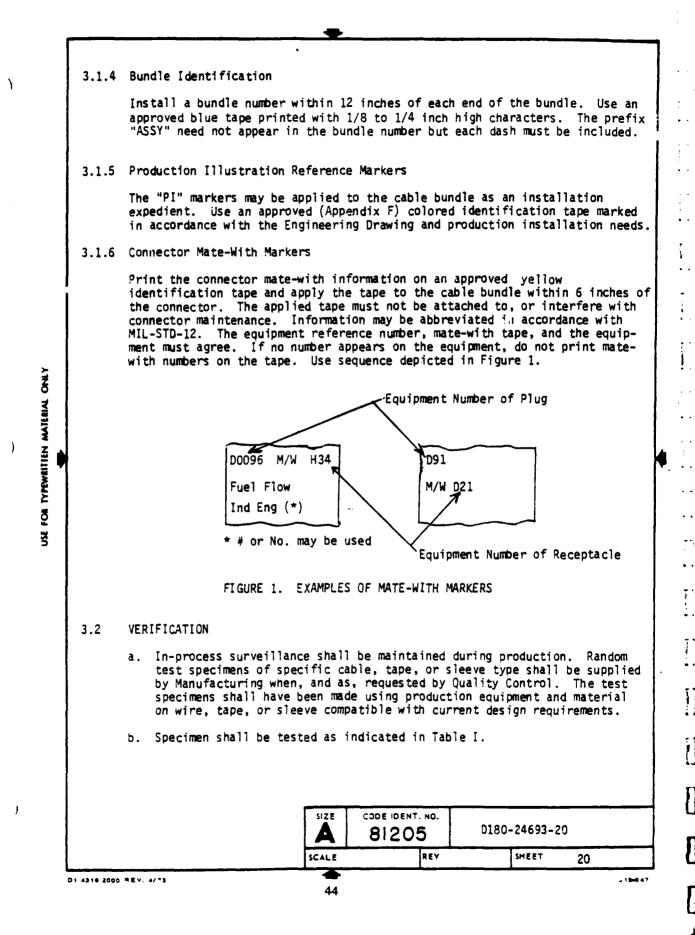
I	DENTIFICAT	ION OF FIBER OPTICS CABLE, CABLE BUNDLES, AND HARNESSES					
1.0	SCOPE						
	This specification contains engineering requirements for the identification of production cabling.						
2.0	CONTENTS						
	Section	Title	. <u>Page</u>				
	3.0	Requirements and Verification	18				
	3.1	Requirements	18				
	3.1.1	General	18				
	3.1.2	Identification of Cable Covering Suitable for Direct Printing	19				
-	3.1.3	Identification of Cable Covering not Suitable for Direct Printing	19				
	3.1.4	Bundle Identification	20				
	3.1.5	Production I11	20				
	3.1.6	Connector Mate-With Markers	20				
	3.2	Verification	20				
	3.2.1	Fluid Test	21				
	3.2.2	Abrasion Test	22				
	3.2.3	Longevity Test	23				
3.0 3.1 3.1.1	REQUIREMEN	NTS AND VERIFICATION					
	REQUIREMEN	VTS					
	General						
		ification is not required on cable less than 3 inches long aled runs.	or withi				
1	b. Identi	ification is not required on module bundles or connectors w	when:				
	(1) 1	No form board is required.					
	(2)	The bundle is formed on the module.					
	(3)	The module is not a panel module.					
	sleeve	able identification information code printed on the cable, e must resist environmental characteristics to the class a s noted on the engineering drawing or data processing (EDP	nd grace				
		SIZE CODE IDENT. NO	0				
		SCALE REY SMEET	18				

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3.1.2	I de	entification of Cable Covering Suitable for Direct Printing				
	a.	Print identification directly on outer surface. The printed identific tion shall not puncture or damage the cable. After printing, bending and/or flexing of the cable shall not cause cracks or splits in the co				
	Þ.	A complete identification code shall be legible within 12 inches of th cable termination points, excluding splices, and at 15 inch maximum intervals throughout cable length.				
3.1.3	Ide	entification of Cable Covering Not Suitable for Direct Printing				
	a.	Apply a yellow heat shrinkable sleeve or identification tape, printed as indicated below.				
	Ъ.	Use cable number and color code specified by Engineering Drawing. Spathe color code characters so they do not appear as an integral part of the wire number.				
		Example: IN260H18 GR L24D18 Y IN261H18 R L24D18 BR				
	c.	Identify spare cable stubs with the connector contact letter or number. When a contact is identified by a lower case letter, the corresponding cable will be identified by an upper case letter followed by a dash.				
	d.	Where two or more unterminated cables, bearing the same identification are routed together in a single group or bundle, include the code numbe of the plug in which they terminate on the corresponding cable.				
	e.	If Engineering Drawing requires that the cable(s) or the bundle be pro- tected with sleeving, cable identification may be printed directly on t sleeving.				
	f.	Install printed sleeves or tapes:				
		(1) Within 3 inches of entrance/exit points of concealed cable runs.				
		(2) Within 3 inches of connector cable clamos and terminating points, excluding splices, and at 6 foot intervals throughout cable length				
		(3) Within 12 inches of each side of bulkhead seal fittings.				
		(4) So they are outside the connector grommet, potting area, or adapte clamps.				
(5) By tieing or shrinking all sleeves unless their movement is restricted to not more than 3 inches by a bundle tie, clamp, shi etc. Do not shrink the sleeve over a bundle tie. If the sleeve split and tied in place, it must overlap itself 1/4 inch minimum						
		SIZE CODE DENT. NO. 81205 D180-24693-20				
		SCALE REV SHEET 19				



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TABLE I

Marking Application Test Required on Specimen Method Class Per Fluid Abrasion Longevity 3.2.2 3.2.3 Appendix F 3.2.1 Hot Stamp X 1 0 Ž X Ink Ribbon 0 1 X X 2 X X 0 = Specimens must be tested consecutively with previous test. X = Specimens may be tested concurrently. 3.2.1 Fluid Test Characters printed on cable, tape, or sleeve shall withstand a 24-hour minimum soak in an approved hydraulic fluid at $70 \pm 2^{\circ}C$, followed by a 24-hour air dry at room temperature and remain legible after being subjected to conditions of 3.2.2. ≻īvo 3.2.2 Abrasion Test Characters printed on cable, tape, or sleeve must remain legible to the unaided eye at a minimum distance of 15 inches in minimum daylight of 30 foot candles after 20 rubs with an abrasive felt (Federal Specification C-F-206b, Type III, Class 7A1) using 2 pounds of weight pressure (including the weight of the fixture) and a speed of 30 to 60 rubs per minute. The felt surface shall be 3/16 to 1/4 inch wide and completely contact the printed characters. 3.2.3 Longevity Test õ ŝ Characters printed on cable, tape, or sleeve shall remain legible after a 24-hour minimum exposure in a weatherometer chamber to alternating cycles of ultra-violet light and typical tap water spray. The cycle periods shall be $102 \pm .25$ minutes of ultra-violet light and $18 \pm .25$ minutes of ultra-violet light plus typical tap water spray. SIZE CODE IDENT. NO. 0180-24693-20 Δ 81205 REV SCALE SHEET 21 31 4316 2000 REV. 4/73 . 19-0 47 45

TYPEWRITTEN MATERIAL

		APPENDIX B	
	FA	BRICATION OF FIBER OPTIC CABLE BUNDLES	S/HARNESSES
1.0	SCOPE		
	This sp of fibe	ecification describes methods and fabri r optic bundles/harnesses.	ication materials for assembly
2.0	CONTENT	S	
	Section	Title	Page
	3.0	Materials Control	22
	4.0	Definitions	28
	5.0	Manufacturing Control	28
	5.1	Wire Groups and Bundles	28
	5.2	Protection of Bundles	31
3.0	MATERIA	LS CONTROL	
	only ma	ture listed below. Where drawing speci terials of that classification shall be I is not available, a higher temperatur	used, except, where a specific
	When th no subs	a specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shal	calls out a specific material, ure "type" or material is not
	When th no subs	e specification or Engineering drawing titution shall be made. Where temperat	calls out a specific material, ure "type" or material is not
	When th no subs specifi	e specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shal Type I - to 200 ⁰ F Type II - to 275 ⁰ F Type III - to 350 ⁰ F	calls out a specific material, ure "type" or material is not 1 be generally used.
	When th no subs specifi	e specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shal Type I - to 200°F Type II - to 275°F Type III - to 350°F Type IV - to 500°F	calls out a specific material, ure "type" or material is not 1 be generally used.
3.1	When th no subs specifi This 2 Exc	e specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shal Type I - to 200°F Type II - to 275°F Type III - to 350°F Type IV - to 500°F ; material is resistant to Skydrol 500.	calls out a specific material, ure "type" or material is not 1 be generally used.
	When th no subs specifi This EXCO	e specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shal Type I - to 200°F Type II - to 275°F Type III - to 350°F Type IV - to 500°F a material is resistant to Skydrol 500. Ept for the adhesive, this material is	calls out a specific material, ure "type" or material is not 1 be generally used.
	When th no subs specifi This 2 Exco TYPE I Sleeving a. Sleeving	e specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shal Type I - to 200°F Type II - to 275°F Type III - to 350°F Type IV - to 500°F c material is resistant to Skydrol 500. Ept for the adhesive, this material is	calls out a specific material, ure "type" or material is not 1 be generally used. resistant to Skydrol 500.
	When th no subs specifi This 2 Exco TYPE I Sleeving a. Sleeving	a specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shall Type I - to 200°F Type II - to 275°F Type III - to 350°F Type IV - to 500°F c material is resistant to Skydrol 500. Ept for the adhesive, this material is MATERIALS I, Insulating eving; insulating, flexible, transparen	<pre>calls out a specific material, ure "type" or material is not 1 be generally used. resistant to Skydrol 500. t, extruded viny!, per ired in the following ranges: .)</pre>
	When th no subs specifi This 2 Exco TYPE I Sleeving a. Sleeving	a specification or Engineering drawing titution shall be made. Where temperat cally designated, Type I materials shall Type I - to 200°F Type II - to 275°F Type III - to 350°F Type IV - to 500°F a material is resistant to Skydrol 500. Ept for the adhesive, this material is MATERIALS I, Insulating Eving; insulating, flexible, transparen E1-7444, Type I, standard sizes as requ Range I (20 AWG to 1/2 I.D. Incl.) Range II (5/8 inch to 1-1/2 I.D. Incl.)	<pre>calls out a specific material, ure "type" or material is not 1 be generally used. resistant to Skydrol 500. t, extruded viny!, per ired in the following ranges: .) Incl.)</pre>

3.1.1	a. (Con	itinued)				
	(1)	The Borden Co., Chemical Division, Resinite Department, Santa Barbara, Calif. "EP-93C" For All Ranges				
	(2)	The Wm. Brand and Co., Inc.; Williamantic, Conn. "Turbo 625" For Range I and II				
	(3)	3M Co., Irvington Division, Freehold, New Jersey "Irvington 3022" For All Ranges				
3.1.2	Strip, I	insulating				
	per MIL-	plastic, vinyl, transparent, flexible (material $1-7444$, Type I), .020 or .040 inch \pm .0015 thic dth as required (tolerance \pm 5%) in 1/4 inch in	ck and .060 inch \pm .00			
		The Borden Company, Chemical Division, Resinite Department, Santa Barbara, California "CT-93C" for .020 inch "EP-93C" for .040 and .060 inch	3			
3.1.3	Tape, In	sulating				
	opaq	e; electrical, vinyl, pressure sensitive, black que, per MIL-I-7798, .007 + .001 inch thick, wic erance <u>+</u> 1/16) in 1/4 inch increments.				
	(1)	Permacel, New Brunswick, New Jersey "P-29, Black"				
	(2)	3M Co., St. Paul, Minn. "Scotch #33"				
	(3)	Technical Tape Corp., New Rochelle, New York "Tuck No. 330, Black"				
3.1.4	Tape, Cushioning (Cable Clamp)					
	Tape, pressure sensitive, rubber and cork composition, per MIL-T-6841A, $1/32$, or $1/16$ inch thick, width as required in $1/4$ inch increments.					
	Armstrong Cork Co.; Lancaster, Pa. "DK-153"					
3.1.5	Tying Material					
	wide	d, flat woven, $.0125 \pm .0030$ inch thick and app e, color white or tan, unwaxed, mildew resistance T-713, and 48 pound minimum breaking strength.	proximately 3/32 inch ce effectiveness per			
		SIZE CODE DENT. 40.	180-24693-20			
		SCALE REV	SHEET 23			

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 (1) Western Filament Corp.; Glendale, Calif. Image: No. 17-D" (Dacron) (2) Hemingway & Bartlett Mfg. Co.; New York, N.Y. Image: Image: Image: The state of the state	3.1.5	a.	(Continued)				
 (2) Hemingway & Bartlett Mfg. Co.; New York, N.Y. D "Dacron Flat Braided Lacing Tape G.E. Finish" (3) Eon Corporation; Los Angeles, Calif. (a) Airtex #417X (Dacron) (b) Airtex #217 (Dacron) (4) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. D Dacron Stur-D-Lace H "18DH" b. Braid, flat woven, "Dacron", .0125 + .003 inch thick and approximately 3/32 inch wide, vinyl coated, color black, end-fray resistant; includir mildew proofing effectiveness and 50 pound average breaking strength ir accordance with MIL-T-713A. (1) Eon Corporation; Los Angeles, Calif. "Airtex 217, Class 2, Black" (2) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. "Fyr-Lace R, Style 18DR, Black" 3.1.6 Talcum Powder a. Talcum Powder No. 325 Van Waters & Rogers; Seattle, Washington 3.2 TYPE II MATERIALS 3.2.1 Sleeving, Insulating, Heat-Shrinkable a. Sleeving (heat-shrinkable), insulating, irradiated polyolefin, opaque colors as required, sizes per applicable standard (MIL-I-23053). (1) Material may be obtained from: Raycnem Inc.; Redwood City, California 			 Western Filament Corp.; Glendale, Calif. 				
 D "Dacron Flat Braided Lacing Tape G.E. Finish" (3) Eon Corporation; Los Angeles, Calif. (a) D Airtex #417X (Dacron) (b) D Airtex #217 (Dacron) (4) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. D Dacron Stur-D-Lace H "18DH" b. Braid, flat woven, "Dacron", .0125 ± .003 inch thick and approximately 3/32 inch wide, vinyl coated, color black, end-fray resistant; includir mildew proofing effectiveness and 50 pound average breaking strength ir accordance with ML-T-713A. (1) Eon Corporation; Los Angeles, Calif. "Airtex 217, Class 2, Black" (2) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. "Fyr-Lace R, Style 18DR, Black" 3.1.6 Talcum Powder a. Talcum Powder No. 325 Van Waters & Rogers; Seattle, Washington 3.2 TYPE II MATERIALS 3.2.1 Sleeving, Insulating, Heat-Shrinkable D a. Sleeving (heat-shrinkable), insulating, irradiated polyolefin, opaque colors as required, sizes per applicable standard (MIL-I-23053). (1) Material may be obtained from: Raychem Inc.; Redwood City, California 			<pre>"No. 17-D" (Dacron)</pre>				
 (3) Eon Corporation; Los Angeles, Calif. (a) Airtex #417X (Dacron) (b) Airtex #217 (Dacron) (4) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. D Dacron Stur-D-Lace H "18DH" b. Braid, flat woven, "Dacron", .0125 + .003 inch thick and approximately 3/32 inch wide, vinyl coated, color black, end-fray resistant; includir mildew proofing effectiveness and 50 pound average breaking strength ir accordance with ML-T-713A. (1) Eon Corporation; Los Angeles, Calif. "Airtex 217, Class 2, Black" (2) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. "Fyr-Lace R, Style 18DR, Black" 3.1.6 Talcum Powder a. Talcum Powder No. 325 Van Waters & Rogers; Seattle, Washington 3.2 TYPE II MATERIALS 3.2.1 Sleeving, Insulating, Heat-Shrinkable a. Sleeving (heat-shrinkable), insulating, irradiated polyolefin, opaque colors as required, sizes per applicable standard (MIL-I-23053). (1) Material may be obtained from: Raychem Inc.; Redwood City, California 			(2) Hemingway & Bartlett Mfg. Co.; New York, N.Y.				
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 (b) Airtex #217 (Dacron) (4) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. Dacron Stur-D-Lace H "18DH" b. Braid, flat woven, "Dacron", .0125 ± .003 inch thick and approximately 3/32 inch wide, vinyl coated, color black, end-fray resistant; includin mildew proofing effectiveness and 50 pound average breaking strength in accordance with MIL-T-713A. (1) Eon Corporation; Los Angeles, Calif. "Airtex 217, Class 2, Black" (2) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. "Fyr-Lace R, Style 18DR, Black" 3.1.6 Talcum Powder a. Talcum Powder No. 325 Van Waters & Rogers; Seattle, Washington 3.2 TYPE II MATERIALS 3.2.1 Sleeving, Insulating, Heat-Shrinkable D a. Sleeving (heat-shrinkable), insulating, irradiated polyolefin, opaque colors as required, sizes per applicable standard (MIL-1-23053). (1) Material may be obtained from: Raychem Inc.; Redwood City, California 			(3) Eon Corporation; Los Angeles, Calif.				
 (4) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. D Dacron Stur-D-Lace H "18DH" b. Braid, flat woven, "Dacron", .0125 ± .003 inch thick and approximately 3/32 inch wide, vinyl coated, color black, end-fray resistant; includir mildew proofing effectiveness and 50 pound average breaking strength ir accordance with MIL-T-713A. (1) Eon Corporation; Los Angeles, Calif. "Airtex 217, Class 2, Black" (2) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. "Fyr-Lace R, Style 18DR, Black" 3.1.6 Talcum Powder a. Talcum Powder No. 325 Van Waters & Rogers; Seattle, Washington 3.2 TYPE II MATERIALS 3.2.1 Sleeving, Insulating, Heat-Shrinkable a. Sleeving (heat-shrinkable), insulating, irradiated polyolefin, opaque colors as required, sizes per applicable standard (MIL-I-23053). (1) Material may be obtained from: Raychem Inc.; Redwood City, California 			(a) 1 Airtex #417X (Dacron)				
 Dacron Stur-D-Lace H "18DH" Braid, flat woven, "Dacron", .0125 ± .003 inch thick and approximately 3/32 inch wide, vinyl coated, color black, end-fray resistant; includin mildew proofing effectiveness and 50 pound average breaking strength in accordance with MIL-T-713A. (1) Eon Corporation; Los Angeles, Calif. "Airtex 217, Class 2, Black" (2) Gudebrod Bros. Silk Co. Inc.; Philadelphia, Pa. "Fyr-Lace R, Style 18DR, Black" 3.1.6 Talcum Powder a. Talcum Powder No. 325 Van Waters & Rogers; Seattle, Washington 3.2. TYPE II MATERIALS 3.2.1 Sleeving, Insulating, Heat-Shrinkable a. Sleeving (heat-shrinkable), insulating, irradiated polyolefin, opaque colors as required, sizes per applicable standard (MIL-I-23053). (1) Material may be obtained from: Raychem Inc.; Redwood City, California 			(b) 1 Airtex #217 (Dacron)				
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Raychem Inc.; Redwood City, California	Ð	a.	Sleeving (heat-shrinkable), insulating, irradiated polyolefin, opaque colors as required, sizes per applicable standard (MIL-I-23053).				
Raychem Inc.; Redwood City, California "Thermofit CRN"			 Material may be obtained from: 				
			Raycnem Inc.; Redwood City, California "Thermofit CRN"				
			SIZE CODE IDENT. NO. 81205 D180-24693-20				
			SCALE REY SHEET 24				

3.3 TYPE IV MATERIALS

3.3.1 Sleeving, Insulating, Heat-Shrinkable

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Sleeving, heat-shrinkable, Polytetrafluoroethylene, (TFE "Teflon") natural color, sizes as listed below:

Raychem, Inc.; Redwood City, California "Thermofit TFE"

Size	Max. I.D. as Supplied (In.)	Recovered I.D., (In.)	Size	Max. I.D. as Supplied (In.)	Recovered I.D. (In.)
30	.030	.022	14	. 121	.078
28	.035	.025	12	.153	.096
28 26	.040	.028	10	. 191	.116
24	.050	.032	8	.240	.144
22	.055	.037	6	. 302	.178
22 20	.060	.044	4	.370	.224
18	.076	.052	2	.430	.278
16	.093	.063	0	.470	. 347

Note: Use on high temperature wire and parts only.

3.3.2 Sleeving, Insulating

a. Sleeving; insulating, fiberglass, silicone rubber covered, fungus resistant treated, white color, per specification MIL-I-18057, (200°C, 8000V minimum average dielectric strength), ASG sizes 24 to 1/0, and 3/8, 7/16, 1/2, and 5/8 inch ID.

- Bentley Harris Mfg. Co.; Conshohocken, Pa. "Ben-Har 1151"
- (2) 3M Co., Irvington Division; Freehold, N.J.

<u>Note</u>: This material limited to procurement only when material per a(1) is unavailable.

"Irvington 411"

b. Tubing, insulating, Polytetrafluoroethylene (TFE "Teflon"), nonrigid per MIL-I-22129, tubing I.D. sizes AGW 0 thru 30, and additional sizes as follows:

<u>Note</u>: This material may be used only when specified on Engineering drawings.

	size	CODE DENT. NO. 81205	D180-24693-20	
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3.3.2	Ь.	(Continued)						
		Nominal ID (In.)) Wall	l Thickn (In.)	ess			
		3/8 7/16 1/2 9/16 5/8 3/4 7/8 1).).).).).	$\begin{array}{c} 0.25 + .0\\ 0.25 + .0\\ 0.25 + .0\\ 0.25 + .0\\ 0.25 + .0\\ 0.30 + .0\\ 0.35$	06 06 06 06 06 08 08			
	с.	Tubing; nonrigid, constr ethylene (TFE "Teflon") strength 5000 volts r.m. 0, and 3/8, 1/2 inch ID.	tape, pe s., wall	er AMS 3	553, r	ed, min	imum br	eakdown
{		Hitemp Wires, Inc.; Mine	ola, N.Y	′ .				
ł		1 "Nonrigid Temprene	Teflon T	ubing"				
		Note: This material may drawings.	be used	ionly w	ien sp	ecified	on Eng	ineering
3.3.3	Str	ip, Protective						
	a.	Strip (or film); Polytet skived, virgin or reproc or .020 thick and width	essed, r	natural	or blu	e color	, .005,	.010, .015,
		(1) Continental Diamond	Fiber C	Co.; Newa	urk, De	21.		
		I "Unsupported	'Teflor	n'; Skive	ed Str	ip"		
		(2) W. S. Shamban & Co.	; Culver	· City, (Calif.			
		 "Kelon-T; Sk 	ived Str	·ip"				
		(3) Raybestos-Manhattan	, Inc.;	Mannheir	n, Pa.			
		I "R/M 829; Sk	ived Str	'ip"				
3.3.4	Tap	e, Insulating						
	a.	Tape, Polytetrafluoroeth setting adhesive, per MI increments, nominal over	L-T-2359)4, widtl	n as re	equired	in 1/4	inch
		(1) 3M Co.; St. Paul, 1	Minn.					
		2 "Scotch #61"	I					
		Г		CODE IDENT			20-2455	
		Ļ		8120			30-2469 Танеет	26

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3.3.4		ontinued)
	(2)	Permacel; New Brunswick, New Jersey
		2 "P-421"
	(3)	Connecticut Hard Rubber Co.; New Haven, Conn.
		Z Temp-R-Tape Type "TV"
3.3.5	Tape, P	rotective
	sen	e, Polytetrafluoroethylene (TFE "Teflon"), glass supported, pressu sitive thermosetting adhesive, width as required in 1/4 inch increment nominal overall thickness aslisted.
	(1)	3M Co.; St. Paul, Minn.
		2 "Scotch #64" (.0065 thick)
	(2)	Permacel; New Brunswick, N.J.
		2 "ET3758" (.005 thick)
	(3)	Connecticut Hard Rubber Co.; New Haven, Conn.
		2 "CHR-A-2005" (.005 thick)
3.3.6	Tying M	aterial
		id; flat woven, fiberglass, "Teflon" coated, approximately 1/8 inch e x 1/64 inch thick, and minimum breaking strength 90 pounds.
	(1)	Bentley Harris Mfg. Co.; Conshohocken, Pa.
		T "TG40"
	(2)	Dodge Fibers Corp.; Hoosick Falls, N.Y.
		1 "E775-303" (Formerly TB-303)
	b. Bra wid	id, flat woven, fiberglass, "Teflon" coated, approximately 5/64 inc le x 1/64 inch thick and minimum breaking strength 45 pounds.
	(1)	Bentley Harris Mfg. Co.; Conshohocken, Pa.
		1 "TG25"
	(2)	•
		1 "E775-476" (Formerly TB-476)
		SIZE CODE DENT. NO. D180-24693-20
		SCALE REV SHEET 27

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	c Group	-			les tied toget	ther and rou
	b. Bundl		bundle" is bundle tie	a number of cal	oles routed to	ogether and
	c. Group	- A cable "	group" is	a number of cab		ther and rou
	c. aroup			set of equipment		
	d, Junct	entering to a flan Connector	an electri ge mountin	e support fixtu cal junction bo; g connector end mping requiremen ping.	c. The fixtur cell with a ca	re is simila ible clamp.
5.0	MANUFACTURING CONTROL					
5.0			105 cn 20	to minimize stru	ess on cables	and connect
	due t	o cable b <mark>ends</mark> a	nel clampin	g during instal ble harnesses of	lation. Formi	ng may be
	to pri conne	vent stresses	or strains	g of cable asset from being plac ench clamps or c	ced on termina	itions or
5.1	CABLE GRO	JPS AND BUNDLES				
5.1.1	Binding C	ables Into Grou	ps and Bun	dles		
J	-			with Appendix	4	

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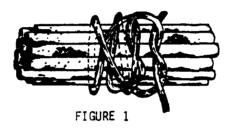


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- b. Untangle cables as much as practicable before tying them into groups. Lay cable groups as parallel as practicable before tying into bundles. Crossed cables under bundle clamps are <u>not</u> acceptable.
- c. Tie cable groups and bundles with tying material (3.1.5, 3.3.6) using a clove hitch and square knot as shown in Figure 1. Tying cord may be doubled when cable groups or bundles exceed 1-1/2 inches in diameter.
 - (1) Before tying the square knot, cinch the clove hitch firmly in place by pulling the free ends of string in opposite directions while rotating them 90° to 180° about the hitch so they twist beneath it and are held in place. Do not stress or deform wire or cable insulation by overtightening the clove hitch.
 - (2) The square knot tightly over the clove hitch and cut off free ends to a length of 1/4 to 1/2 inch.

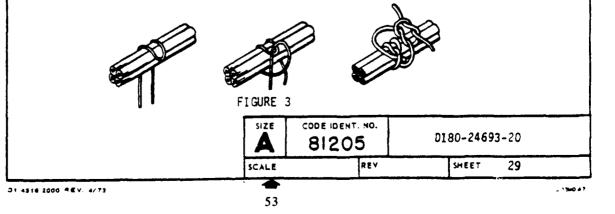


(3) For cabling on which ties tend to slip, an optional tie may be made by passing an initial loop through the bundle prior to making clove hitch as shown in Figure 2. Tighten clove hitch on opposite side of bundle from the initial loop. Tie a square knot over the clove hitch (see Figure 1).



FIGURE 2

d. In restricted areas, the modified clove hitch and square knot shown in Figure 3 may be used as an optional tie for tying cable groups. Follow the procedure in c(1) and (2) above to secure the tie.



5.1.1	(Co	ntinued)
	e.	Minimize fraying of fiberglass tying braids (3.3.6) by cutting tied ends using very sharp cutting tools. A small amount of nylon varnish (3.4.2) may also be applied on braid ends and knots if necessary to prevent fraying or loosening.
5.1.2	Spa	cing Ties for Bundle Support
	a.	Except as provided in 5.1.3, space ties on cable groups and bundles a minimum of 8 inches and a maximum of 12 inches apart except as follows:
		 Tie as necessary to provide adequate support at bends, breakouts, a locations where cable groups or bundles are adjacent to moving parts
		(2) Tie cables together in junction or terminal boxes only as required for support to facilitate removal of cabling and equipment.
		(3) Tie groups and bundles such that support is not derived from terminals.
		(4) When cable groups are tied within a bundle, the ties on the individual groups may be spaced a maximum of 30 inches.
		(5) Space ties a maximum of 30 inches on groups and bundles installed i raceways.
		(6) Use the minimum number of ties necessary to adequately support the groups or bundles as specified herein.
	b.	Assemble cables in conduit or insulating tubing such that they are untangled and parallel as much as practicable. Cables in conduit or insulating tubing shall not be tied together. Talcum (3.1.7) may be use as a lubricant on cables and tubing.
	с.	All temporary ties placed on cable bundles to facilitate handling or storage must be removed during or prior to bundle installations.
5.1.3	Tyi	ng of Equipment Internal Wiring
	a.	Stationary groups and bundles contained within ground support equipment consoles, cabinets, and components may be bound together by continuous lacing as an optional method to spot tying per 5.1.1.
		(1) Using tying braid (3.1.5b), start the lacing by making a tie per Figure 1. Cut off only the short end after making the knot.
		(2) Make a continuous lacing using a series of locking stitches as show in Figure 4.
	-	
		FIGURE 4.
		SIZE CODE IDENT. NO. 81205 D180-24693-20
		SCALE REV SHEET 30

5.1.3	•	ntinued)				
	(3)	Apply continuo stitches per F adjacent to ea	igure 5, ex	cept that a st	itch may	erval between also be provided
		<u>D</u> (Inches)	<u>L_</u>	(Inches)		
		Less than 1/2 to 1 More than	1-	4 + 3/16 1/2 + 3/8 + 7/16		
	Not	e: Two successi 20% of the 1			shall no	t differ by more t
			FIGURE 5			
		ipment, space ti				of ground support imum of 6 inches
5.2	PROTECT	ION OF BUNDLES				
	otherwis		protect grou			be possible but i afing or abrasion
	(3.		e non-shrin	kable sleeving		shrinkable sleevin with bundle ties
	b. Ins	tall shrinkable :	sleeving as	follows:		
	(1)	When practical sleeves.	, remove gra	oup or bundle [.]	ties prion	r to installing
	(2)	Use a sleeve s Ties may be om	ize that will	ll fit permaner ght fitting sle	ntly in pl eeves.	lace after shrinki
	(3)	Shrink sleeving	g using good	d standard prac	ctice.	
	(4)					cing a minimum of ght inches in lend
			512	CODE IDENT. NO.		
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			SCALE	REY		SHEET 31

5.2 (Continued)

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c.	Provide drain holes in protective sleeves where more than 12 inches long.
	A pair of drain holes may be spaced diametrically opposite at 2 inch
•	intervals with alternate pairs rotated 90°, or they may be provided in
	groups of 4 holes evenly spaced around the sleeve circumference at 4 inch
	intervals. Make 1/8 inch holes in AWG 4 (nominal ID .208 inch) or larger
	sleeves and 1/16 inch holes in smaller sleeves.

Note: Drain holes are not required in close fitting shrinkable sleeves.

- d. An alternate method to a, above, is to wrap the cable(s) with vinyl or teflon strip (3.1.2, 3.3.3). Completely cover starting end of strip on the first lap, then proceed with a one-half width spiral overlap. Secure wrapping with bundle ties at each end and at intervals of 8 inches maximum.
- e. Protect cables and bundles from abrasion in uncushioned metal clamps by wrapping the cables with a minimum of two concentric wraps (.03 inch minimum buildup) of insulating or protective strip or tape (3.1.2, 3.1.3, 3.1.4, 3.3.3, 3.3.4, 3.3.5). Wrap the cables and tighten the clamp in such a manner that the jacket is not crushed or damaged and does not slip. Tightly wrap and hold the strip while tightening the clamp to prevent unwrapping.
- f. Protect cables against abrasion at bundle supports and clamps by covering with sleeving or tape (3.1.1, 3.1.3, 3.2.1, 3.3.1, 3.3.2, 3.3.4, 3.3.5). Extend this protection 1 inch $\pm 1/8$ on each side of the support. Install sleeving per a or b, above. Spirally wrap tape with a one-half width overlap, covering the starting end before lapping is begun, and spiral by wrapping the finishing end back under the support clamp or tie.

A 81205 DIE		
SCALE REY	SHEET 32	

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		A DETAILED INS	APPENDI: STALLATI		URES			
					•			
1.0	SCOPE							
	This sect and harme	ion covers detail sses.	ed step	s in the	instal]	ation c	f fiber optic	cab l
2.0	CONTENTS							
	<u>Section</u>	Title						Pag
	3.0	Requirements an	d Verif	ication				33
	3.1	Requirements						33
	3.1.1	General						33
	3.1.2	Cable Slack						34
	3.1.3	Orip Loops						35
	3.1.4	Bend Radius						35
	3.1.5	Bundle and Cabl						35 37
	3.1.6	Coupling of Con						37
	3.1.7 3.1.8	Modification of Test of Cabling		ses				38
	3.1.8	Protection of T		ions				38
	3.2	Verification	erannaç	10113				39
	3.2.1	In-Process Surv	eillanc	e				39
3.0	REQUIREME	NTS AND VERIFICAT	ION					
3.1	REQUIREME	NTS						
3.1.1	General							
		ct unattached end undles and stow t			. Neat	ly coil	the free ends	of
	untan	ble cables in con gled and parallel g must not be tie	to eac	h other.				ting
	c. All t handl	emporary ties or ing or storage mu	straps st be r	placed on emoved du	cable t ring or	bundles prior	to facilitate to installation	۱.
	NOTE:	Exercise care t straps and to p aircraft compon	revent	cut straps	s or ti			; or
			SIZE	CODE IDENT	r. NO.	<u> </u>		.
			A	8120	5	0180	-24693-20	
			SCALE		REV		SHEET 33	

3.1.1 (Continued)

- d. Smoothing and filling compound may be applied over projecting ri/ets, bolts, nuts, or other protrusions which present an abrading surface to adjacent cables.
- e. Cabling shall not be encased with tape or sleeve unless specified on the bundle assembly or installation drawings. When shrinkable sleeving is specified to be shrunk, shrink from one end heating evenly until the other end of the tube is reached. Move the heat gun evenly without overheating the cable.
- f. At shock mounted equipment, all cables from each connector may be tied together, but the cables from one connector shall not be tied to the cables from another connector between the unit and the first clamp.

3.1.2 Cable Slack

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a. Distribute slack evenly throughout the length of the bundle. Install cable bundles as shown in Figure 1.

Where installation location markers are used, distribute slack evenly between the markers.

- b. In applicable areas make certain that there is adequate slack to meet the following requirements:
 - (1) Replacement of terminations at least three times.
 - NOTE: Where space permits, include the excess cable length for retermination of connectors in the form of a drip loop. Otherwise include the length in the first six feet leading to the connector or other terminations.
 - (2) Movement of hinged joints.
 - (3) Removal of face-mounted equipment, where other means of access is not provided.
 - (4) Coupling and uncoupling of connectors.
 - (5) Special maintenance and service applications specified on the engineering drawing (e.g., to permit ample shifting of equipment while still in the aircraft, for the purpose of realignment, removal of dust covers, servicing, tuning and changing components or assemblies).

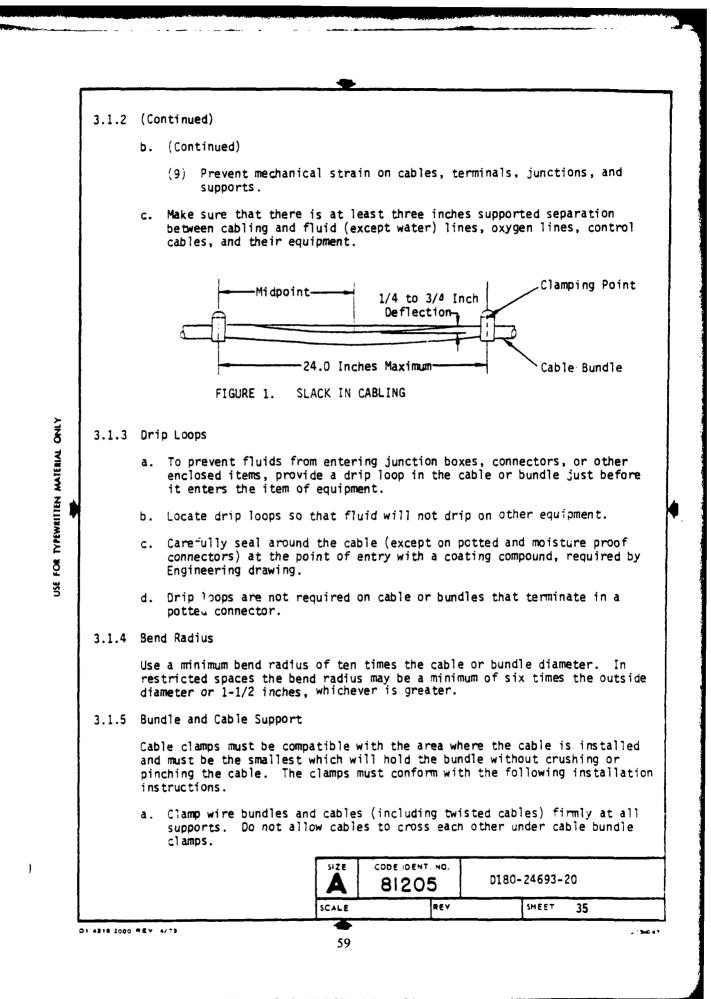
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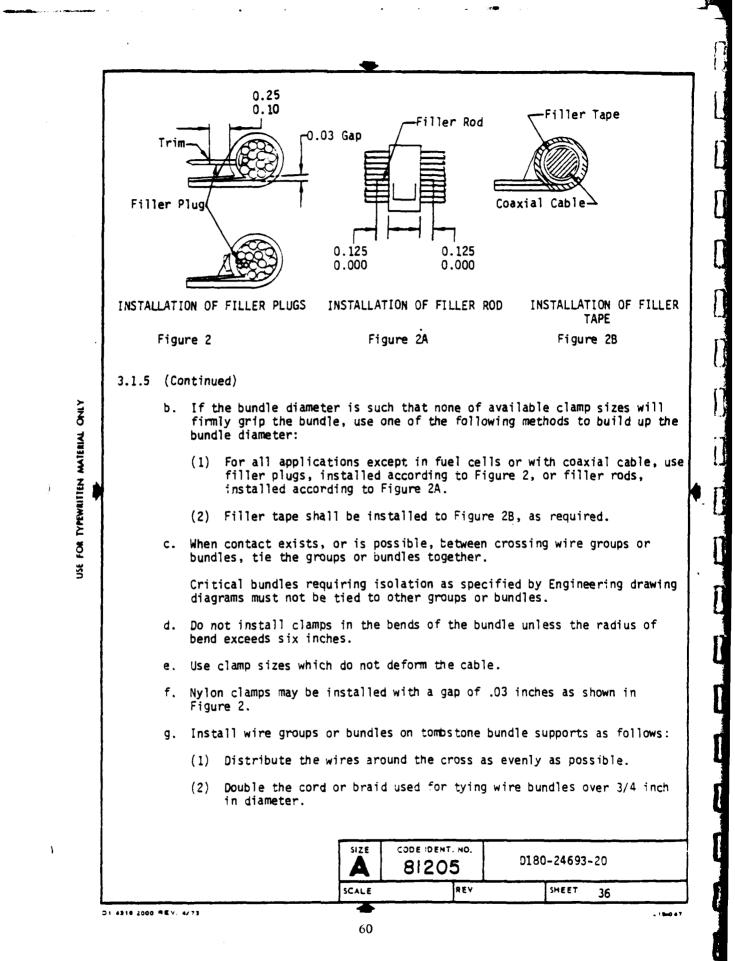
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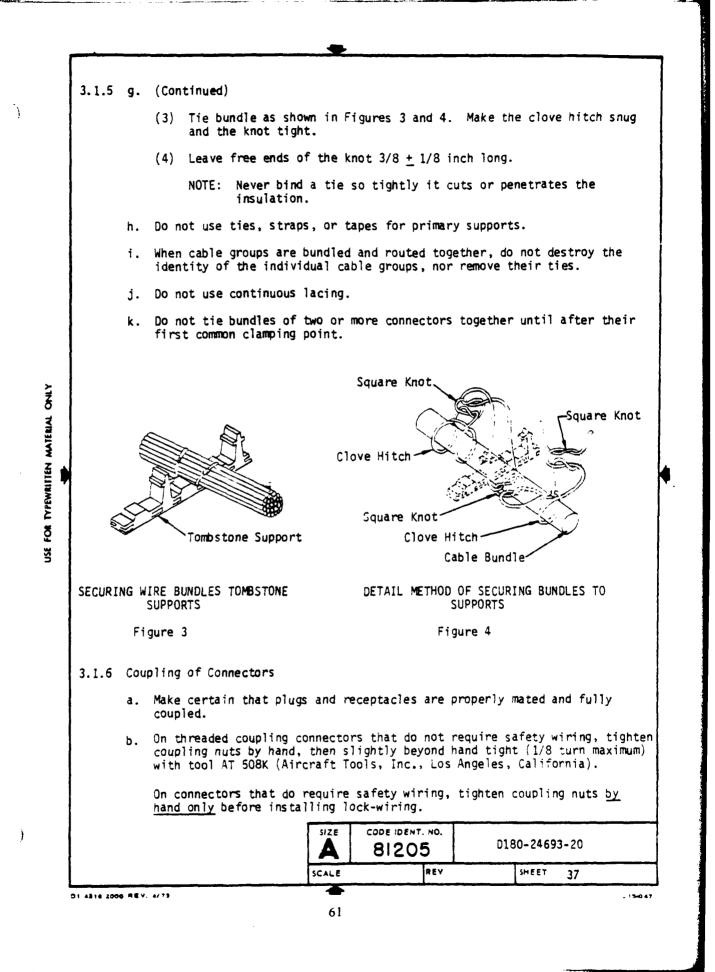
- (6) Prevention of strain on cables to shock-mounted equipment.
- (7) Provision of drip loops.
- (8) Adequate cabling movement at bulkheads and on long straight cable runs to compensate for the expansion and contraction of the aircraft structure induced by climate extremes.

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3.1.6	(Conti	nued)			
					only by hand. Make certa mpletely locked position.
	C0				irection of coupling. On for tightness <u>only prior</u>
	e. En	gage connectors w	ith jackscrew-	type couplin	g as follows:
	(1) Before threading tightly against		ews into the	jacksockets, seat them
	(2				rn at a time alternately f er the socket contacts.
	(3) Continue tighte the connectors			two turns alternately uni
3.1.7	Modifi	cation of Harnesse	es.		
	result		Materials Rev		to a completed bundle as a tion, accomplish the
	a. Id	entify cable or ca	bles by appro	priate marki	ngs.
	pu		through the		ed by either threading and and support clamps or by t
	(1)	accordance with	Appendix B.	If the bund	f the bundle with ties in le is installed, ties are eximately one foot interva
	(2)		in the parent	bundle. Howe	existing ties, tapes, ever, they must be install bundle.
3.1.8	Test o	f Cabling			
					bility of the Manufacturi Engineering drawing.
3.1.9	Protec	tion of Terminatio	ns		
		ling is to remain t the unconnected			red product installation,
	a. In	sulate unattached	cable ends wi	th tape or sh	nrink sleeving.
	b. Pro	otect installed ur	coupled conne	ctors with du	ist caps.
				DE IDENT. NO. 81205	D180-24693-20
			SCALE	REV	SHEET 38

3.1.9	(Continued)
	c. Stow the cabling so that contaminants cannot fall or drain into the protective covers.
3.2	VERIFICATION
3.2.1	In-Process Surveillance
	a. Assure that only approved materials are used to satisfy the requirement: of this specification.
	b. Assure that temperature, fluid, and vibration restrictions are observed
	c. Assure that terminals, splices, connectors, and wires are properly installed, supported, and protected.
	d. Assure that circuits are properly tested as specified on the Eng nee lay drawing before application of aircraft power.
	A 81205 0180-24693-20

		APPENDIX D	
		MARKING OF FIBER OPTIC CABLING	
1.0	SCOPE		
	The purp marking	ose of this document is to provide the methods and requirements fiber optic cables and bundles.	for
2.0	CONTENTS		
	Section	Title	Page
	3.0	Materials Control	41
ł	4.0	Facilities Control	44
	5.0	Manufacturing Control	44
	5.1	General Requirements	44
	5.2	Individual Cable Marking	45
	5.2.1	Selection of Marking Method	45
	5.2.2	Location of Marking	46
	5.2.3	Marking Application	47
	5.3	Bundle Marking	49
	5.3.1	Selection of Harness Marking Method	4 9
	5.3.2	Location of Harness Marking	49
	5.3.3	Marking Application	50
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	5.5.1	Attachment to Polyurethane Molded Parts	57
	5.5.2	Heat-Shrinkable Tubing	57
	5.5.3	Tied-On Sleeving	57
	5.5.4	Adhesive Tape	57
	5.6	Test Methods	58
	6.0	Quality Control	58
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3.0	MATERIALS CONTROL								
	NOT	E: These are suggested sources. Where competing equal suppliers are available, use is permissible.							
	a.	ent, Parting, Silicone Grease, 400 ⁰ F minimum decomposition temperature							
		Dow Corning "High Vacuum Grease" Dow Corning Corporation							
	b.	Adhesive							
		(1) Gaco N-29 Cold Bond and N-39 Accelerator (BAC 5010, Type 53) Gates Engineering Company							
		(2) PR1527M with PR1523M, Primer (BMS 8-81) Products Research Corporatio							
	c.	Braid, flat woven, synthetic fiber, 0.0125 ± 0.0030 inch thick and 0.070 to 0.100 inch wide, color white or tan, unwaxed. Mildew resistance effectiveness in accordance with MIL-T-43435 and 48 pounds minimum breaking strength.							
		(1) Airtex 417X (Dacron), Associated Suppliers Co.							
		(2) No. 17D (Dacron), Western Fishing Line Company							
		(3) Dacron Flat Braided Lacing Tape, G.E. Finish Heminway and Bartlett Manufacturing Company							
	d.	Braid, flat woven, fiberglass, Teflon coated, approximately 5/64 inch wid by 1/64 inch thick, minimum breaking strength 45 pounds.							
		 ≠TG-30, Bentley Harris Manufacturing Co. 							
		(2) ≠TG-476, Dodge Fibers Corporation							
	e.	Coating, Spray, Protective, Removable, Spraylat #SC1071, Spraylat Corporation							
	f. Coating, Spray, Protective, Nonremoveable								
		(1) Acrylic Aerosol Spray							
		Tartan #91-1, Rudd Paint and Varnish Company Krylon #1303, Krylon Incorporated							
		(2) Varnish, Moisture, and Fungus Proof, IAW MIL-V-173 Sprayon ≠608, Sprayon Products, Incorporated							
		SIZE CODE DENT. NO. 5130-24693-20							
		SCALE REV SHEET 41							

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3.0	(Co	ntinu	ed)							
	g.	Foil	, Pri	nting 1-1/2 and	d 3 inch	width	5			
		(1)	King	sley Stamping M	Machine C	ο.				
			(a)	K-36	Gener	al Pu	rpose			
			(b)	K-46	Nylon					
			(c)	KFP-16 Black	Surfa	ce Tre	eated Te	flon		
			(d)	K-289 White	Polye	thyler	le			
		(2)	M. S	wift and Sons,	Incorpor	ated				
			(a)	C20114 Black	Surfa	ce Tre	eated Te	flon & G	eneral	Purpose
			(b)	C20118 Black	Surfa	ce Tre	eated Te	flon & G	eneral	Purpose
			(c)	C2O2O6 White	Gener	al Pur	pose			
			(d)	C20110 Black	Nylon					
		(3)	Номш	et Corporation,	, Roll Le	af Div	vis ion			
			(a)	5821 Black	Gener	al Pur	pose			
			(b)	WW99 Black	Surfa	ce Tre	ated Te	flon		
	h.	Ink,	Mark	ing						
		(1)	#73X	-NW, Black, Inc	lependent	Ink,	Incorpo	rated		
		(2)	W. E	. 42 Paste Ink,	, White,	Genera	1 Print	ing Ink,	Incorp	orated
	i.	Paper, Liner, Creped-Kraft, width as required								
		(1)	No.	RP360, 3M Compa	iny					
		(2)	Perm	acel E13734, Pe	ermacel D	ivisio	on, John	son and	Johnsor	, Inc.
	j.	Ribbon, Printing								
		(1)	IBM	143341 (for IBM	1 407 Pri	nter)				
		(2) IBM 1403-OCR No. 424325 Black (for IBM 1403 Printer)								
		(3) IBM Cartridge ≠1136108 (for IBM Selectric typewriter)								
		(4) H&M Gold Star =37 (heavy black) (for IBM Selectric Typewriter)								
		(5)	Sing	er (Friden) 440	003030 (f	or Sir	nger (Fr	iden) Fl	exowrit	en typewrit:
				Γ	SIZE C	ODE DE	NT. NO.			
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k.	Sleeving, insulating, f	iberglass,	, silico ne r	ubber covered,	fungus resis-	•
	tant treated, color whit	te, Class	H-B-1 meeti	ing performance	requirements	of
	MIL-I-3190, in standard	sizes as	required.			

- (1) Turbo 117, Brand-Rex Division, American Enka Corp.
- (2) Class H-B-1 Type SR-9, Varflex Corp.
- m. Sleeving, identification, fiberglass, Kel-F suspensoid treated, in standard sizes as required, Gencote 125C, General Plastics Corp.
- n. Sleeving, insulation, electrical, flexible in accordance with MIL-I-7444, Type III, Class 2, color yellow
- o. Strip, polyvinyl alcohol film, perforated, 17/64 or 3/4 inch spacing on diagonal, 3 mil thick x 3/4 or 1 inch width. Reynolds Metals, Plastic Division
- p. Strip, plastic vinyl (PVC), transparent, flexible (material same as for sleeving in accordance with MIL-I-7444), 0.020 <u>+</u> 0.0015 inch thick, 3/4 or 1 inch widths. Strip-Plastic No. CT93, Borden Co., Chemical Division, Resinita Department
- q. Strip, plastic, polyvinyl chloride, black opaque, nonrigid, Type F, form Ts, Class, Category I, in accordance with MIL-I-631, 0.020 ± 0.0015 inch thick, width as required (tolerance ± 5 percent) in 1/4 inch increments. Plymouth Rubber Company
- r. Strip, silicone rubber, self bonding, 0.020 inch thick x 1 inch width. Permacel 2650 Permacel Division, Johnson & Johnson, Incorporated
- s. Tape, Electrical Polyvinylchloride, pressure sensitive, yellow or black, opaque, 0.007 <u>+</u> 0.001 inch thick, width as required (tolerance 0.06 inch) in 1/4 inch increments.
 - Permacel No. 29 (specify yellow or black) Permacel Division, Johnson & Johnson, Incorporated
 - (2) X-1235, Prebacked (specify yellow not available in black)- 3M CO.
- t. Tape electrical, glass cloth-backed, white, pressure sensitive, according to MIL-I-19166 widths as required in 1/4 inch increments. Mystic Brand #7000, Mystic Tape, Inc.
- u. Tape Masking, creped, various widths Purchased from any available source.
- v. Tape, paper backed cloth, vinyl impregnated
 B-500 + specify color, width, and type of backing, N. -. Brady Company

	SIZE	CODE DENT. NO. 81205	0130-24693-20	
	SCALE	REV	энеет 43	
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3.0	(Co	ntinued)							
	w.	Tape, polyvinylchloride, pressure sensitive, red, opaque, width as required in 1/4 inch increments, Parmacel No. P-32, Permacel Division, Johnson & Johnson, Inc.							
	x.	T.bing, shrinkaula, heat reactive plastic							
	у.	Tubing, shrinkable, heat reactive plastic according to BMS 1-41, Type 5, sizes according to BACT63B							
4.0	FAC	ILITIES CONTROL							
	The printing devices listed below are suggested. Equivalent models or devices may be used provided all marking requirements are met.								
	a.	a. Embossing Machines							
		(1) Kingsley Wire Marking Machine Model KW-7 for sleeve and tube marking							
		(2) Kingsley Wire Marking Machine Model AW3.							
		(3) Kingsley Wire Marking Machine Model AWIV.							
		(4) Kingsley Wire Marking Machine Model AWIVC.							
		(5) TAB Wire Marking Machine Model MA-200.							
	Ъ.	Cold Imprinting Machi.es							
		(1) Singer (Friden) Automatic Typewriter, Model 2201 Flexowriter							
		(2) IBM Selectric							
		(3) IBM 407 and 1403							
5.0	MAN	UFACTURING CONTROL							
5.1	GEN	ERAL REQUIREMENTS							
	a.	All marking shall be of sufficient size and definition to be legible and of a permanent nature.							
	5.	The characterisitcs of the wire or cable shall not be impaired by the use of any marking device or by the removal of marking when required.							
	с.	Metallic markers or bands shall not be used for identification.							
	4.	The information for identification, mate-with, and P.I. markers shall be obtained from the Engineering drawings.							
	e.	Identification of wiring in furnished equipment shall not be altered unless authorized by the procuring activity.							
		312E CODE DENT. NO. D180-24693-20							
		SCALE REV SHEET 44							

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5.1	(Con	tinued	1)							
	ו 1	recept he ma	acles st	nall be nall be	applied	outsi	ie potting	, materia	connector plugs al or adapter c g under the cab	lamp
	- i	lires Ind ex Irawin	it point	nently s of t	conceal he run a	ed run: nd at a	s shall be iny additi	e identii ional poi	fied at the ent ints specified l	ranc by t
			space pe markers.		marking	s on ca	bles and	harnesse	es shall not co	ncea
			dnance M NCE".	arking	s shall	be red	, and mark	ked in wh	lite with the wo	ork
	ר ו ר ע	lamps remove fermin vire o	, support d, or th ating po r beneat	ting d le cabl pint id ch a ti	evices, e twiste entifica e are ac	shield d in ou tion wh ceptab	ing, and t der to re lich falls	erminals ad the i on the can be	fication so the do not have to dentification. underside of th easily read by	o be ne
							and size	e selecti	on shall be per	rfor
5.2	INDI	/I DUAL	CABLE M	ARKING						
5.2.1	Selec	tion	of Marki	ng Met	hod					
5.2.1	1 Ide	entifi	cation N	larkers	(Direct	Imprir	ting)			
	a.	cont or,	rast wit if ink :	h the et mar	most sui	table n vailabl	marking fo e, the mo	il from	which provide the materials l ble ink identif	list
5.2.1	.2 Ide	ntifi	cation #	larkers	(Imprin	ted Tub	ing or S1	eeves)		
	a.	cabl	es which	will.	not acce	ot or i	; when imp retain a c ed as foll	lear mac	ith marking foi hine imprinted	1,
		(1)	Use yel contair directl	ed in	areas wi	kable f th temp	ubing (3. Deratures	0x) to i below 20	dentify wiring O ^O F which is no	ot
		(2)	tubing	for wi	re ident	ificati	option in on. The Aill fit o	sleeve s	heat-snrinkabl nall nave the s wire.	le ;mal
					SIZE	1	DENT. NO.		0180-24693-20	
					SCALE	<u>.</u>	REV	A	SHEET 45	

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	(3) When specified on the Engineering drawing, for use in high temper ature areas (above 200 ^o F), markers shall be made from sleeving.
	 b. Identification (number and color code) for individual cables contained in jacketed bundles shall be installed on the cable outer covering usi
	heat-shrinkable tubing or imprinted sleeves. The color coding as show below shall be spaced so that it does not appear as an integral part o the cable number.
	Blu - Blue Yel - Yellow Grn - Green Brn - Brown Řed - Red Orn - Orange Blk - Black Whi - White Gra - Gray Vio - Violet
	When a multiconductor cable is broken out into individual branches which are 12 inches or shorter the cable marking shall be sufficient. Indiv dual branches longer than 12 inches shall be marked in addition to the normal cable marking.
	c. Split identification sleeves may be used to replace defective sleeves. Split sleeves may also be used to identify wires at terminating points
5.2.1.3	Identification Markers (Imprinted Adhesive Tape)
	When specified on the Engineering drawing, paper-backed vinyl impregnated cloth tape shall be used to identify cabling.
5.2.1.4	Ordnance Markers
	Ordnance markers shall be made from red heat-shrinkable tubing marked in white with the word "ORDNANCE".
5.2.2	Location of Marking
5.2.2.1	Identification Markers
	a. These markings shall be located at intervals not greater than three inches except as noted in b. and c. below.
	5. When specified on the Engineering drawing, for electronic equipment and interconnects in aircraft or missiles, the markings shall be within three inches of each end and at intervals not greater than 15 inches between end marks.
	c. Lengths less than three inches long shall not require marking.
	SIZE CODE DENT. NO. 0150-24693-20
	SCALE REV SHEET 46

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5.2.2.2 Ordnance Markers

Ordnance markers shall be located as near as possible to the wire ends and at intervals no greater than 15 inches throughout the cable length.

5.2.3 Marking Application

5.2.3.1 Direct Imprinting

a. Select the size of type which is appropriate for the cable to be marked. The curvature of the type face should approximate the surface curvature (See Figure 1).

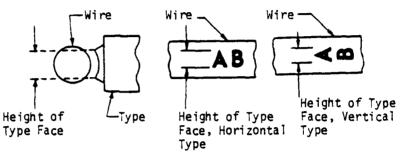


FIGURE 1

b. Table I gives the ranges of type face heights for corresponding diameters which will produce the optimum mark with the least penetration of the type into the outer surface.

T	AB	LE	I
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WIRE SI	ZE	AND	TYPE	FACE	HEIGHT
---------	----	-----	------	------	--------

	Kingsley Type	Wire	C.D.	Tro.	jan Type
Type Height	Identification Number	Minimum	Maximum	Type Height	Identification Number
0.025	VC-24	0.035	0.025	0.025	Vertical Type AP204 1
0.025	VC-24	0.040	0.061	0.040	AP104
0.050	DS	0.052	0.076	0.050	AP 105
1/16	RS	0.068	0.096	0.050	AP105
1/16	RS	0.075	0.106	0.070	AP106 2
5/64	S	0.095	0.165	0.080	AP108 3
7/64	Ĺ	0.162	And Larger	0.109	AP110 1
2 AP 3 AP 4 AP	104 (Optional) 105 (Optional) 105 or AP106 (Opt 105, AP106, or AP otional)		CODE DE 8120		D180-24693-20
		SCAL		REV	SHEET 47
2000 4EV	4/*3	-		····	
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- c. To prevent uneven depth marking, make sure that type faces are clean and that all characters are set in the same plane. Plated and unplated type may be of different lengths and should not be used together.
- d. Select a marking foil as specified in the materials list for the jacket type being marked.
- e. Adjust machine pressure, temperature, and dwell time to provide markings for best legibility. Markings shall be considered permanent if legible after being subjected to the test specified in the test methods.

5.2.3.2 Imprinting Tubing and Sleeving

a. Printing on heat shrinkable tubing and sleeving shall be accomplished by hot embossing as on wire insulation. Printing shall be along the length of the tubing or sleeving. Heat shrinkable tubing on bandolier or with similar type backing in tubing may also be printed with a Friden automatic typewriter, modified as necessary, and using printing ribbon.

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- CAUTION: Exercise care not to smear markings on tubing immediately after printing with Friden typewriter. Printing is not permanent for up to 1/2 hour after typing.
- b. In most cases flat-faced type will be used with a flat anvil. Very small size tubing or sleeving may be marked with curved face type and a wire guide if the marking requirement can be met.
- c. For hot embossing, the imprinting type temperature shall be 400°F minimum (indicated temperature). Use printing foil specified in Table II.

Tubing or Sleeving Type	Foil Type
3.0x.	3.0g.
3.On.	3.0g.
3.Om.	3.0g.(1)(a) 3.0g.(2)(a) 3.0g.(2)(b)
3.0y.	3.0g.
3.0x. (Ordnance)	3.0g.(1)(d) 3.0g.(2)(c)

TABLE II

HOT EMBOSSING FOIL

	size	CODE IDENT. NO. 81205	D180-24693-20	
	SCALE	REV	SHEET 48	<u> </u>
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inese markers shall be to	SIZE					
			nce wi+	h Engine	erina draw	inas
3 inches of the rear face cause misalignment of con	e of the itacts o	e connecto iue to pre	r gromm	et, but	not close	
Mate-With Markers						
Identification Markers						
Location of Harness Marki	ng					
						inkable
Ordnance Markers						
P.I. markers shall be mad	le of ta	pe (3.s.,	yellow) unless	otherwise	specif
Production Illustration ((P.I.) M	larkers				
a. Use tape (3.0s., yell (3.0x., yellow).	ow), sī	eeves (3.	On.), o	r heat-s	hrinkable	tubing
Mate-With Markers						
b. When specified on Eng (above 200 ^o F), marker (3.0k. or 3.0m.).	jineerir 's shall	ng drawing i be made	, for u from ta	se in h [.] pe (3.01	igh tempera t.) or slee	iture ar ving
a. Use tape (3.0s., yell	ow) or	h ea t-shri	nkable	tubing ((3.0x., yel	low).
Identification (part numb	er) mar	kers shal	l be as	follows	5:	
Identification Markers						
Selection of Harness Mark	ing Met	thod				
HARNESS MARKING						
Print identification on t	the tape	e in accor	dance w	ith 5.3	.3.2.	
	HARNESS MARKING Selection of Harness Mark Identification Markers Identification (part numb a. Use tape (3.0s., yell b. When specified on Eng (above 200°F), marker (3.0k. or 3.0m.). Mate-With Markers Connector mate-with market a. Use tape (3.0s., yell (3.0x., yellow). b. When specified on Eng (above 2000F), marker Production Illustration (P.I. markers shall be mad Ordnance Markers Ordnance markers shall be tubing (3.0x., red) market Location of Harness Marki Identification Markers These markers shall be lo harness, and at intervals the harness. Mate-With Markers These markers shall be pl 3 inches of the rear face cause misalignment of con Production Illustration (Print identification on the tape HARNESS MARKING Selection of Harness Marking Met Identification Markers Identification (part number) mar a. Use tape (3.0s., yellow) or b. When specified on Engineerir (above 200 ^{OF}), markers shall (3.0k. or 3.0m.). Mate-With Markers Connector mate-with markers shall a. Use tape (3.0s., yellow), si (3.0x., yellow). b. When specified on Engineerir (above 2000F), markers shall Production Illustration (P.I.) M P.I. markers shall be made of ta Ordnance Markers Ordnance Markers Ordnance markers shall be made f tubing (3.0x., red) marked in wh Location of Harness Marking Identification Markers These markers shall be located a harness, and at intervals no gre the harness. Mate-With Markers These markers shall be placed or 3 inches of the rear face of the cause misalignment of contacts of Production Illustration (P.I. Ma These markers shall be located i	Print identification on the tape in accor HARNESS MARKING Selection of Harness Marking Method Identification (part number) markers shal a. Use tape (3.0s., yellow) or heat-shri b. When specified on Engineering drawing (above 200°F), markers shall be made (3.0k. or 3.0m.). Mate-With Markers Connector mate-with markers shall be as fr a. Use tape (3.0s., yellow), sleeves (3.1 (3.0x., yellow). b. When specified on Engineering drawing (above 200°F), markers shall be made in Production Illustration (P.I.) Markers P.I. markers shall be made of tape (3.s., Ordnance Markers Ordnance markers shall be made from tape tubing (3.0x., red) marked in white with Location of Harness Marking Identification Markers These markers shall be located as near as harness, and at intervals no greater than the harness. Mate-With Markers These markers shall be placed on the connector cause misalignment of contacts due to pre: Production Illustration (P.I. Markers) These markers shall be located in accordated Size Contacts and to present and the harness These markers shall be placed on the connector Cause misalignment of contacts due to present Production Illustration (P.I. Markers) These markers shall be located in accordated Size Contacts and to present and the present and the harnest and the present	Print identification on the tape in accordance w HARNESS MARKING Selection of Harness Marking Method Identification (part number) markers shall be as a. Use tape (3.0s., yellow) or heat-shrinkable b. When specified on Engineering drawing, for u (above 200°F), markers shall be made from ta (3.0k. or 3.0m.). Mate-With Markers Connector mate-with markers shall be as follows: a. Use tape (3.0s., yellow), sleeves (3.0n.), o (3.0x., yellow). b. When specified on Engineering drawing, for u (above 2000F), markers shall be made of tape Production Illustration (P.I.) Markers P.I. markers shall be made of tape (3.s., yellow Ordnance Markers Ordnance markers shall be made from tape (3.0w., tubing (3.0x., red) marked in white with the wor Location of Harness Marking Identification Markers These markers shall be located as near as possib harness, and at intervals no greater than 6 feet the harness. Mate-With Markers These markers shall be placed on the connector o 3 inches of the rear face of the connector o 3 inches of the rear face of the connector grown cause misalignment of contacts due to pressure o Production Illustration (P.I. Markers) These markers shall be located in accordance wit SIZE CODE-DENT. NO. B12O5	Print identification on the tape in accordance with 5.3 HARNESS MARKING Selection of Harness Marking Method Identification (part number) markers shall be as follows a. Use tape (3.0s., yellow) or heat-shrinkable tubing (b. When specified on Engineering drawing, for use in hr (above 200 ^{OF}), markers shall be made from tape (3.01 (3.0k, or 3.0m.). Mate-With Markers Connector mate-with markers shall be as follows: a. Use tape (3.0s., yellow), sleeves (3.0n.), or heat-s (3.0x., yellow). b. When specified on Engineering drawing, for use in hi (above 2000F), markers shall be made of tape (3.0t.) Production Illustration (P.I.) Markers P.I. markers shall be made of tape (3.0t., red), or tubing (3.0x., red) marked in white with the word "ORDAR Location of Harness Marking Identification Markers These markers shall be located as near as possible to ea harness, and at intervals no greater than 6 feet, throug the harness. Mate-With Markers These markers shall be placed on the connector or on the 3 inches of the rear face of the connector grommet, but cause misalignment of contacts due to pressure on wires. Production Illustration (P.I. Markers) These markers shall be located in accordance with Engine Size Code OFT, NO. BI205 DIS	Print identification on the tape in accordance with 5.3.3.2. HARNESS MARKING Selection of Harness Marking Method Identification Markers Identification (part number) markers shall be as follows: a. Use tape (3.0s., yellow) or heat-shrinkable tubing (3.0x., yellow) b. When specified on Engineering drawing, for use in high tempera (above 2000F), markers shall be made from tape (3.0t.) or slee (3.0k. or 3.0m.). Mate-With Markers Connector mate-with markers shall be as follows: a. Use tape (3.0s., yellow), sleeves (3.0n.), or heat-shrinkable (3.0x., yellow). b. When specified on Engineering drawing, for use in high tempera (above 2000F), markers shall be made of tape (3.0t.) or sleevi Production Illustration (P.I.) Markers P.I. markers shall be made of tape (3.0w., red), or heat-shr tubing (3.0x., red) marked in white with the word "ORDNANCE". Location of Harness Marking Identification Markers These markers shall be located as near as possible to each end of harness, and at intervals no greater than 6 feet, throughout the 1 the harness. Mate-With Markers These markers shall be placed on the connector or on the wire harn 3 inches of the rear face of the connector grommet, but not close cause misalignment of contacts due to pressure on wires. Production Illustration (P.I. Markers) These markers shall be located in accordance with Engineering draw

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These markers shall be located as near as possible to the ends of the harness and at intervals no greater than 15 inches throughout the length of the harness.

5.3.3 Marking Application

5.3.3.1 Imprinting Heat-Shrinkable Tubing and Sleeves

Imprinting heat-shrinkable tubing and sleeving shall be accomplished as specified in 5.2.3.2.

5.3.3.2 Imprinting Adhesive Tape

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- a. Tape which is not prebacked shall have the adhesive protected with backing paper (3.0i.) during this operation. Tape shall be marked by direct embossing or printed with an automatic typewriter (4.0b.) as follows:
 - (1) Direct Embossing Apply marking using a hot stamping machine (4.0b.) with 1/8 inch high printing type and with type regulator set at approximately 450° F. Use printing foil in accordance with Table III.

Таре	Ribbor
3.0s. (Yellow)	3.0g.(1)(a) 3.0g.(2)(b) 3.0g.(3)(a)
3.0s. (Black)	3.0g.(1)(d) 3.0g.(2)(c)
3.0w. (Red)	3.0g.(1)(d) 3.0g.(2)(c)

TABLE III HOT EMBOSSING TAPE & FOIL

(2) Automatic Typewriter - Apply marking with an automatic typewriter using tape and ribbon in accordance with Table IV.

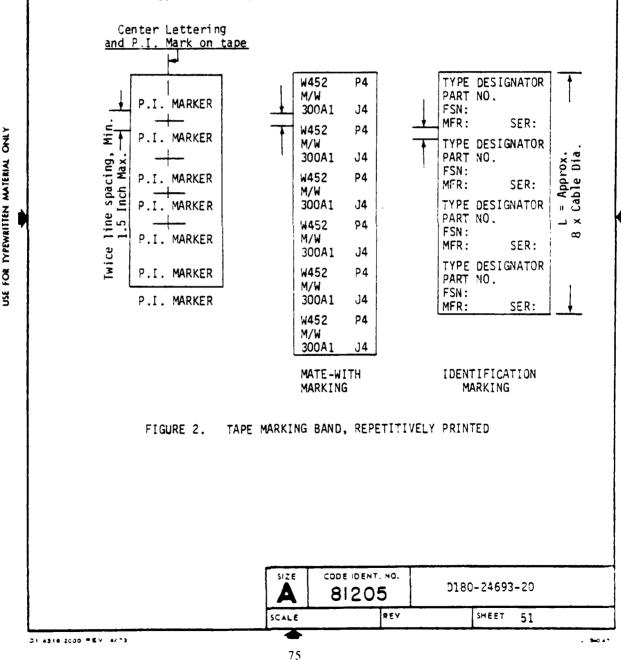
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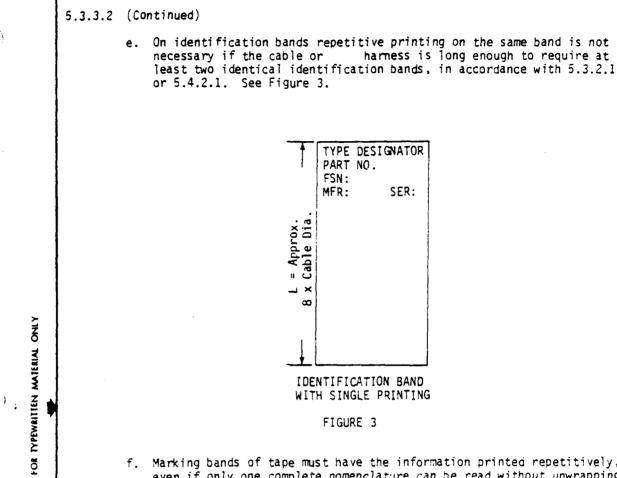
AUTOMATIC TYPEWRITER TAPE & RIBBON

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size	CODE DENT. NO. 81205	0180-24693-20
3.0s. (Yellow)	3.0j.(3) 3.0j.(4) 3.0j.(5)	
3.0t.	3.0j.(3) 3.0j.(4)	
Tape	Ribbon	

5.3.3.2 (Continued)

- b. Print across the width of the tape. The printing shall be wholly contained on the tape.
- c. The P.I. mark and the lettering on the marker must be printed symmetrically to the centerline of the tape in accordance with Figure 2.
- d. Print the marking repetitively (except according to 5.3.3.2e.) on a continuous tape. Space between each marking shall be at least twice the line spacing but not to exceed 1-1/2 inches, however tape length shall be such as to accommodate at least two complete markings. See Figure 2 for typical Marking Bands.





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f. Marking bands of tape must have the information printed repetitively, even if only one complete nomenclature can be read without unwrapping the tape. This assures at least two sources from which to reconstruct information from worn, one-of-a-kind cable bands. Mate-With Marking bands and P.I. Marker bands appear once only on each cable or wire harness regardless of length. Therefore, they must always be printed repetitively if marking tape is used, because the printing on tape is less permanent than hot stamped printing.

SER:

- g. Cure markings on tapes printed with an automatic typewriter by one of the following methods.
 - (1) Process marked tape through an infrared heating unit.
 - (2) Apply heat from a 500⁰F rated air gun. Exposure shall be from one minute to five minutes maximum. Distance from the tape shall be 6 to 7 inches.
 - (3) Apply a light coating of Acrylic Aerosol Spray (3.0f.(1)).

size	CODE DENT. NO. 81205	0180-24693-20
SCALE	REY	SHEET 52

5.3.3.2	g. (3) (Continued)					
	con	tainer.	The sprag	s instructi y may not b bly areas.	uns printed e used in e	on the lectric
	h. Marking shall be c subjected to the t	onsidered est spect	d permanen ified in S	nt if it is 5.6.1.	legible af	ter being
5.4	CABLE MARKING					
5.4.1	Selection of Cable Mar	king				
5.4.1.1	Jacketed Cables					
	Cables shall be marked	using th	ne applica	ible method	indicated	in Table V.
	CARLE .	TABLE	E V ARKING GUI	DE		
	Marking Method Jacket Material	Shr S1e	vinkable eve 0x.)	Tied-On Sleeve (3.0k.)	Adhesive Tape	Direct Embossing
	Neoprene	} [2	Do Not Use	4	Do Not Use
	Polyurethane	[2	Do Not Use	4	Do Not Use
	Polyvinylchloride (PVC)		2		3	Do Not Use
	Polyethylene	[1)	2	3	2
	Teflon	[1	2	3	Do Not Use
	Nylon	[1)	2	3	Do Not Use
	 Use this method un Use this method on Use this method (t marking sleeves. Use this method (t Engineering drawing) 	ape 3.0s ape 3.0s aps.	ecified o ., yellow ., black) code de	n Engineer) for rewor only when	ing drawings rk on cables specified o	with damaged n the
		A	8120)5 REV	0180-24693-	20

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5.4.1.3	Polyurethane Connector Moldings
	a. When specified on the Engineering drawing, polyurethane connector moldings shall be marked with white ink stamping with a clear acrylic overcoat.
	b. When specified by Engineering drawing, adhesive patches per 5.4.3 may be applied to connector moldings.
5.4.1.4	Polyolefin Heat-Shrinkable Boots
	When specified on the Engineering drawing, marking shall be applied to po olefin heat-shrinkable boots by white ink stamping with overcoats of clea acrylic and abrasion resistant varnish.
5.4.1.5	Cadmium-Plated Connector Backshells and Fittings
	When specified on the Engineering drawing, marking shall be applied to cadmium-plated connector rear hardware by black ink stamping with an acry overcoat.
5.4.2	Location of Bundle Marking
5.4.2.1	Identification Markers
	a. On cables over six feet long, these markers shall be located as near possible to each end of the cable jacket.
	b. Cables six feet long, or shorter, shall be identified at the approximic center.
	c. Breakouts of individual cables shall be marked as required in 5.2.1.2
5.4.2.2	Mate-With Markers
	Mate-with markers shall be located on the connector or on the cable adjace to the connector. When specified on the Engineering drawing, they shall b placed on the molding, boot, or backshell.
5.4.2.3	Production Illustration (P.I.) Markers
	P.I. markers shall be located in accordance with Engineering drawings.
5.4.2.4	Ordnance Markers
	Ordnance markers shall be located as near as possible to each end of the cable jacket and at intervals no greater than 15 inches throughout the length of the cable.
	SIZE CODE IDENT. NO. A 81205 D180-24693-20
	SCALE REY SHEET 54

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5.4.3 Marking Application

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5.4.3.1 Printing on Adhesive Patches

This procedure describes the color transition marking of the green surface Hypalon laminate. Heated areas of the patch change from green to yellow producing a contrasting legible marking which is inherently permanent.

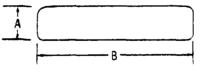
Preparation of Patch for Printing:

a. Spray or brush a thin layer of "spraylat" (3.0e.) on the rear (black side) of the laminate stock. Allow a minimum of 90 minutes drying time at normal room temperature before trimming the patch to size.

CAUTION: Do not spray in electric wiring or part assembly area.

b. Cut the patch, after drying, to the dimensions shown in Figure 4, taking care not to delaminate the patch nor separate the "spraylat" coating from the patch. For patches requiring more than three lines of type or more than 20 characters and spaces per line, dimensions A and B may be increased proportionately. Minimum edge margin requirements of 5.4.3.1c must be maintained. Patch size tolerance is $\pm 1/4$ inch.

Patch Type	Dim. "A" (Inches)	Dim. "B" (Inches)
Identification	3/4	3
	3/4	3/4
Mate-With	1/2	1 1/4
	3/4	1 1/4 or 3
P.I. Marker	3/4	1 1/4
Reference Designator	1/2	1/2



3/32 <u>+</u> 1/32 Radius (Typical)

FIGURE 4. PATCH SIZES

SCALE	REV	SHEET 55	
SIZE	CODE DENT. NO. 81205	D130-24693-20	

5.4.3.2	Printin	g on Polyurethane Connector Moldings
		lyurethane connector moldings using method specified on Engineering (adhesive patches or ink stamping).
	a. Adh	esive Patches
	Arp	Ly marking to adhesive patches as specified in 5.4.3.1.
	b. In'	ce ping
	(1)	Use rubber stamps with a character height of 1/8 to 1/2 inch. On small components, where size is a limiting factor, 1/16 inch character height may be used.
	(2)	Abrade the area to be marked with an aluminum oxide grit drum, disk, or rotary file.
	(3)	Clean surface to be printed with aliphatic naphtha. Wipe dry with clean material and then allow surface to air dry for ten minutes.
	(4)	Use white paste ink (3.0h.(2)) without thinning. Apply a small amount to a clean sheet of glass or metal and roll out to a smooth layer. Apply ink to the prepared area using rubber stamp.
	(5)	Air dry until tack-free and for an additional ten minutes.
	(6)	Overcoat marking with a light coat of acrylic spray, 3.0f.(1). When tack-free, apply an additional coat to achieve a glossy, continuous coating. Air dry for ten minutes.
		CAUTION: Do not spray in electric wiring or part assembly area.
5.4.3.3	Printin	g on Polyolefin Heat-Shrinkable Boots
		lyolefin heat-shrinkable boots by ink stamping as follows when ed on Engineering drawings.
	com	rubber stamps with a character height of 1/8 to 1/2 inch. On small ponents, where size is a limiting factor, 1/16 inch character height be used.
	b. Abr	ade the area to be marked with 400 grit abrasive paper.
		an surface, apply markings, air dry, and overcoat with clean acrylic specified in 5.4.3.3b.(3) through b.(6).
	d. Ove	rcoat clear acrylic with abrasion resistant varnich (3.0f.(2)).
		SIZE CODE DENT. NO.
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		SCALE REY SHEET 56

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5.4.3.4	Printing on Cadmium Plated Connectors Backshells and Fittings
	Mark cadmium plated connector hardware by ink stamping as follows when specified on Engineering drawings.
	a. Use rubber stamps with a character height of 1/8 to 1/2 inch. On small components, where size is a limiting factor, 1/16 inch character neight may be used.
	b. Clean surface to be printed with aliphatic naphtha. Wipe dry with clea material and then allow surface to air dry for ten minutes.
	c. Apply black ink (3.0h.(1)) to the prepared area using rubber stamp.
	d. Air dry and overcoat with clear acrylic as specified in 5.4.3.3b.(6).
	e. Overcoat clear acrylic with abrasion resistant varnish (3.0f.(2)).
5.5	INSTALLATION OF MARKERS
5.5.1	Attachment to Polyurethane Molded Parts
	Bond patches to molded parts using procedure specified, except roughening of the molded part prior to cleaning is not required.
5.5.2	Heat-Shrinkable Tubing
	Shrink in place in accordance with good standard practice.
5.5.3	Tied-On Sleeving
	a. Tie all sleeves at both ends with braid (3.0c. or 3.0d.) using square knots unless the axial movement is restricted to one inch or less by obstructions such as bundle ties, clamps, or shielding.
	b. On teflon insulated wire, two wraps of 1/2 inch tape (3.0t.) shall be applied, centered under the sleeve, before tying.
5.5.4	Adhesive Tape
	a. After printing, wrap $2-1/2 \pm 1/2$ turns of the tape around the cable, cable harness, or cable jacket, so that at least one complete nomenclature appears on the outermost layer.
	b. Where a complete nomenclature would not appear on the outermost wrap, apply tape around the circumference for one turn and pinch excess and lengths together to form flag. Fold flag back around and tie at both ends of tape with braid (3.0c.), using a square knot, as necessary to preclude flag damage during handling and installation.
	c. P.I. marker tape flags, and flags inside equipment, are not required to be folded back and tied with braid unless the cables or wire bundles are to be pulled through conduit or other restricted openings which may result in damage to the flag.
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- d. When printed adhesive markers are to be installed over <u>vinyl sleeving</u>, do not use pressure sensitive tape directly applied. The use of adhesive tape is acceptable provided the adhesive does not come in contact with the vinyl sleeving. This may be accomplished by folding the tape back on itself and wrapping around the sleeving. If there is a possibility of the tape sliding on the cable, fasten securely by tying both ends of the tape with braid (3.0c.) using a square knot.
- 5.6 TEST METHODS
- 5.6.1 Permanent Marking Test

Marking shall be considered permanent if it is legible after being subjected to 20 strokes from a wire mark abrasion tester using a 1/16 inch gray felt abrasive in accordance with Federal Specification C-F-206, Type I, Class 9R4 Operate the tester either manually or under power on 3 or more imprints no sooner than 2 minutes after the coding operation if the mark is applied with a hot stamping machine, or no sooner than 4 hours after marking and curing if the mark is applied with a cold stamping machine (automatic typewriter).

6.0 OUALITY CONTROL

- Quality Control shall perform surveillance of marked cables and harnesses to ensure conformance with the requirements of this specification. Particular attention should be paid to the following:
 - (1) Correct markings placed on cables and harnesses.
 - (2) Correct placement of markings on cables and harnesses.
 - (3) Legibility of markings.
 - (4) Use of proper type marking for cable jacket material and wires.
 - (5) Verification of tests specified in 5.6.
- b. Quality Control shall ensure that the operation of any device used for the marking processes mentioned in this specification conforms to the requirements.

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APPENDIX B

FINAL INSTALLATION PROCESS SPECIFICATION (Specific)

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FINAL REPORT FABRICATION AND INSTALLATION PROCEDURES, FIBER OPTICS RACK INTEGRATION HARNESS, AND STAND-ALONE LINK

> O. R. Mulkey Boeing Aerospace Company P.O. Box 3999 Seattle, Washington 98124

> > 4 June 1980

Final Report for Period 16 December 1979 Through 4 June 1980

Phase IV of NOSC Contract N00123-78-C-0193

Prepared For:

NAVAL OCEAN SYSTEMS CENTER Code 9313 San Diego, California 92152

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1.0 INTRODUCTION

1.1 SCOPE

This document will cover the physical installation of harnesses 180-59004 and 180-59005. Also included are the installation sequence and cautions to be observed during installation, inspection standards, and remove and replace notes. The purpose of the installation is to demonstrate production installation methods for F/O cables.

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1.2 KEY WORDS

Fiber Optic Cables E-3A AWACS Flight Instrumentation Aircraft Installation

1.3 FOREWORD

The installation of the fiber optics harnesses into the AWACS (E-3A) airplane will use standard cabling procedures as a baseline. The intention of this effort is to demonstrate that fiber optics harnesses can be installed and tested in a production environment as opposed to special lab conditions. Except as noted, standard tools and normal handling procedures may be used in installing fiber optics cables. Fiber optics cables are a different technology from standard electrical cables and a few precautions must be taken initially, especially to protect ends and connectors during installation. Sharp impacts could be disastrous to fiber optic cables. This is a result of the fracture properties exhibited by glasses under impulse shear stresses. Copper is malleable under the same conditions, even when the critical yield point is exceeded. Stress concentrations occur at connector joints, at clamps and accessory hardware fastening points, and at the point of impact.

This document will describe the steps taken in installing the fiber optics cables into the airplane, including site preparation, installation sequence, and procedures and quality control inspection, and general removal and reinstallation procedures.

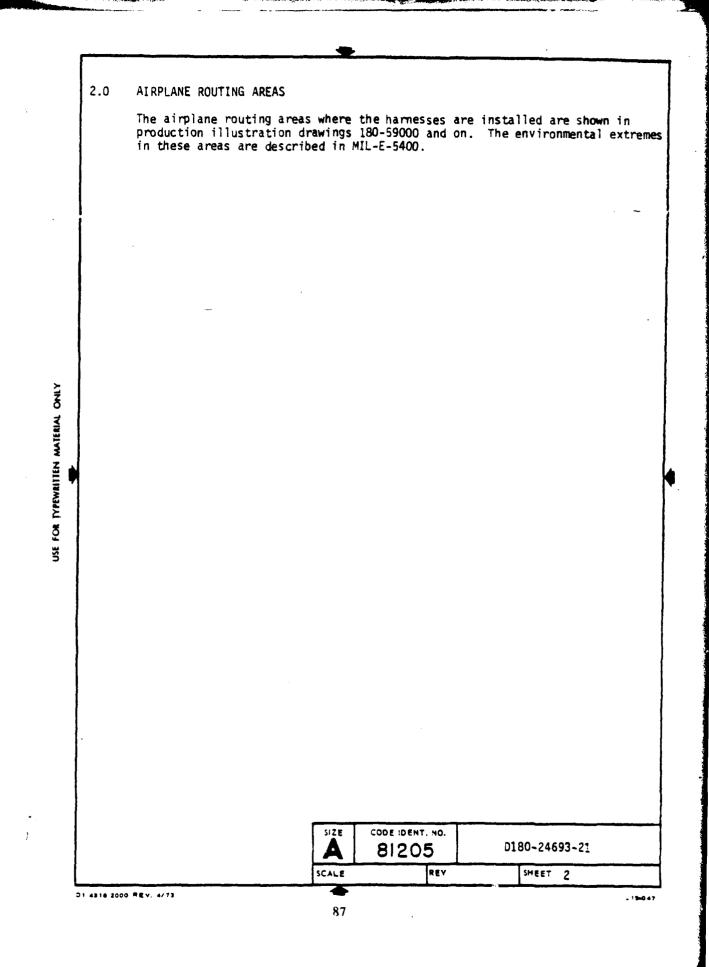
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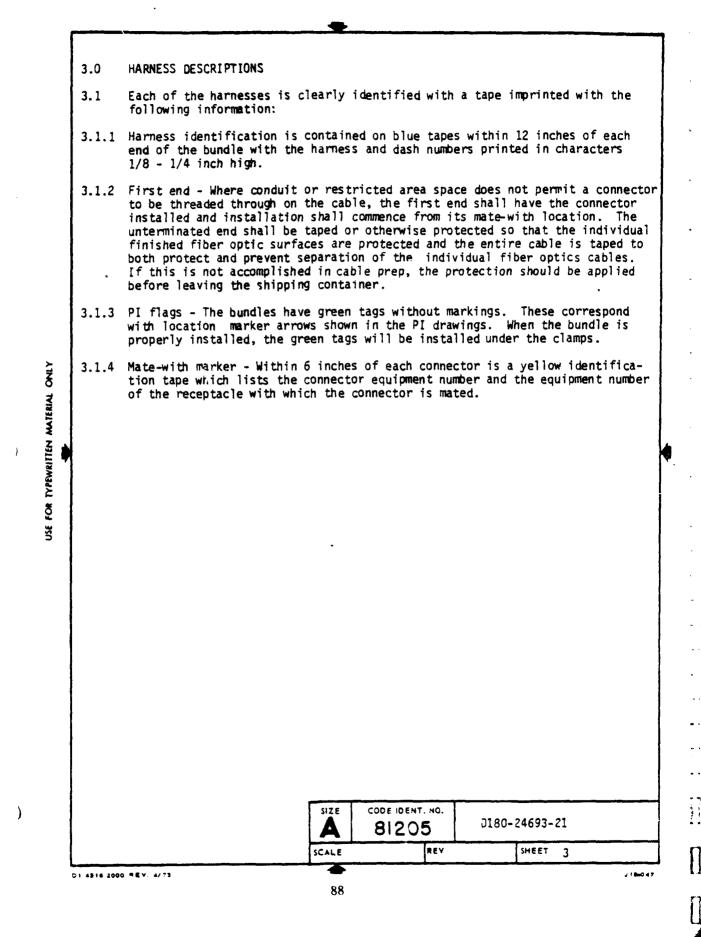
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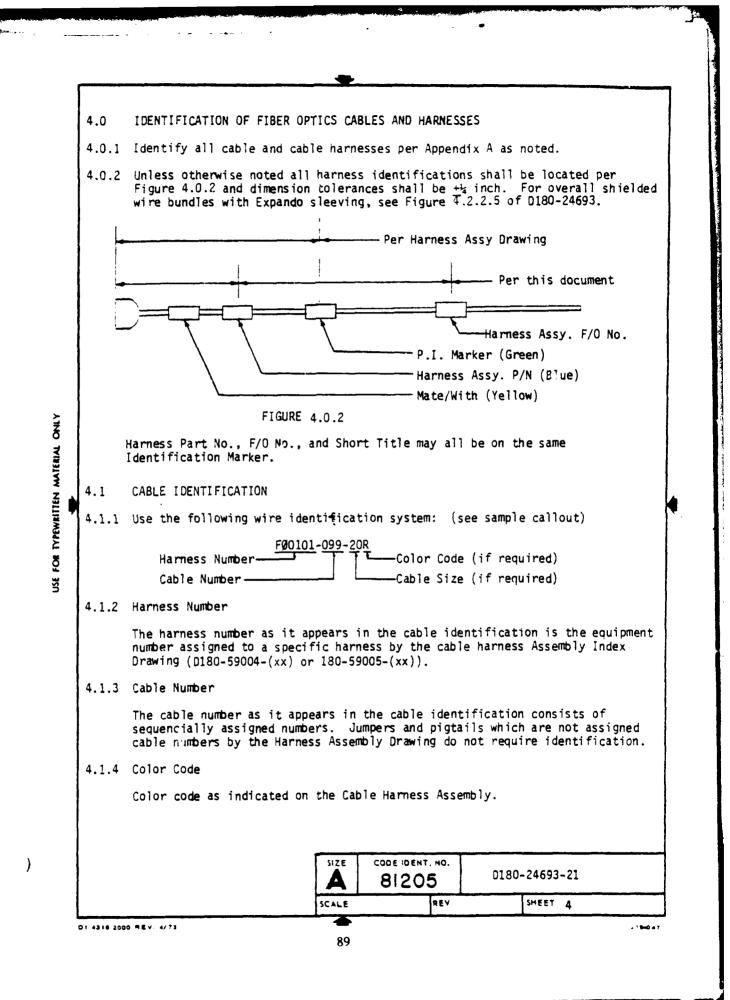
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5.0	INSTALLATION
5.1	SPECIAL HANDLING CAUTIONS
5.1.1	Glass has low impact and compressive strength. Never drop or hit the cable
5.1.2	Glass has high tensile strength but low tolerance to elongation and shear. Microfractures otherwise unnoticeable may cause stress risers. Whipping, jerking, or flexing which exceed the installation limits, even momentarily, should be avoided.
5.1.3	The contact surfaces are precision finished and can be damaged by dust, oil from your fingers, or by scratching.
	Leave the protective covers in place until closing the connector.
	Check alignment of the connector shells when closing so that they're as straight as possible.
5.1.4	Shocks over 100 g's can occur inside a connector by seemingly minor roughnes to the bundle near the connector. Be careful handling connectors.
5.2	SEQUENCE PLANNING
	The sequence planning for the two harnesses is:
	180-59004: Interrack Harness 180-59005: Interrack Harness (single fiber)
5.2.1	Bundle tie table with excess length allowed at both ends.
5 .2. 2.	Form board fabrication with excess length trimmed to with sufficient slack allowed for 3 subsequent reterminations at each end allowed. At this step, the ends must be capped off with tape or shrink sleeving and the end taped so no subsequent damage may occur.
5.2.3	Solder one 1st end termination where both ends have terminations, connector halves, and backshell hardware installed.
	NOTE: Protective end caps are necessary for subsequent shipping.
	NOTE: Check continuity and proper pins.
5.2.4	Final assembly for installation of cable but not end closure.
5.3	INSTALLATION STEPS
	Harness 180-59004: Rack Integration Bundle Harness 180-59005
5.3.1	The 180-59004 and -59005 harnesses will be installed in the same routing clamps as the 204-51870-5 harness which they replace. The first end is installed at the floor joint shown in the production illustration.
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Leave the connector protective caps in place until inspection is conducted. Measure, without connecting, the distance between the mate-with connector and the first run clamp and allow sufficient length so that, when the cable connector is mated, the cable directly behind the connector backshell is not stressed. The harness must not be installed with a flex point at the backshell; any flex distribution must run evenly from the backshell to the first cable clamp. See Figure 5.3.1.

- 6.0 FIBER OPTIC HARNESS CONFIGURATION
- 6.0.1 Harness configurations consist of fiber optic lines and pairs of standard wire that are twisted together. Various configurations are shown in Figure 6.0.1.



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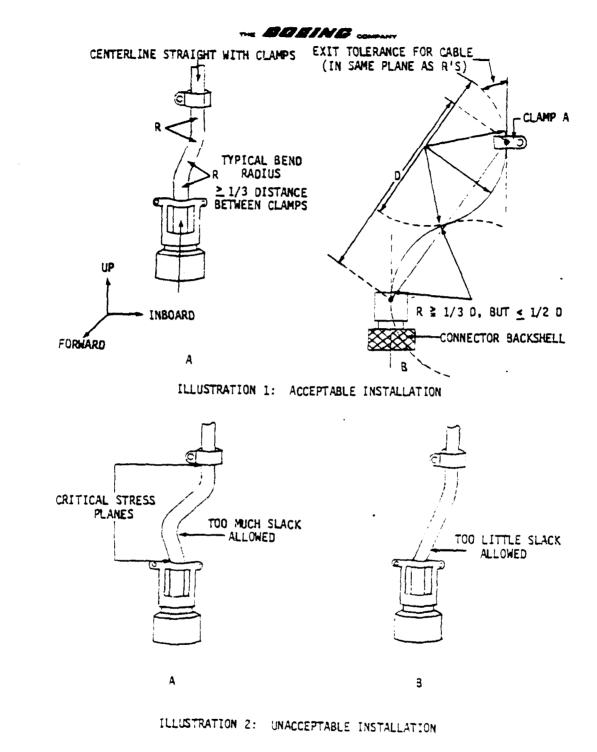


FIGURE 5.3.1: EXAMPLE INSTALLATIONS

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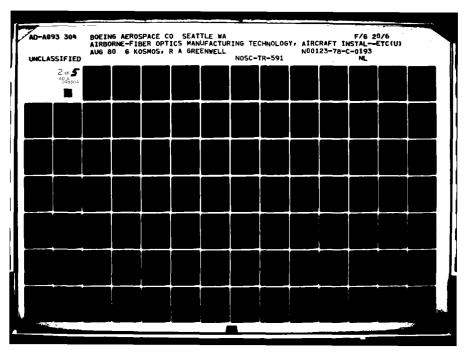
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The second phase of the contract was a "proof" stage for the Phase I design and consisted of the fabrication of a harness and "stand-alone link" to the designs and documents developed during Phase I. In addition, all processes were reviewed and additional ones were written to provide complete documentation.

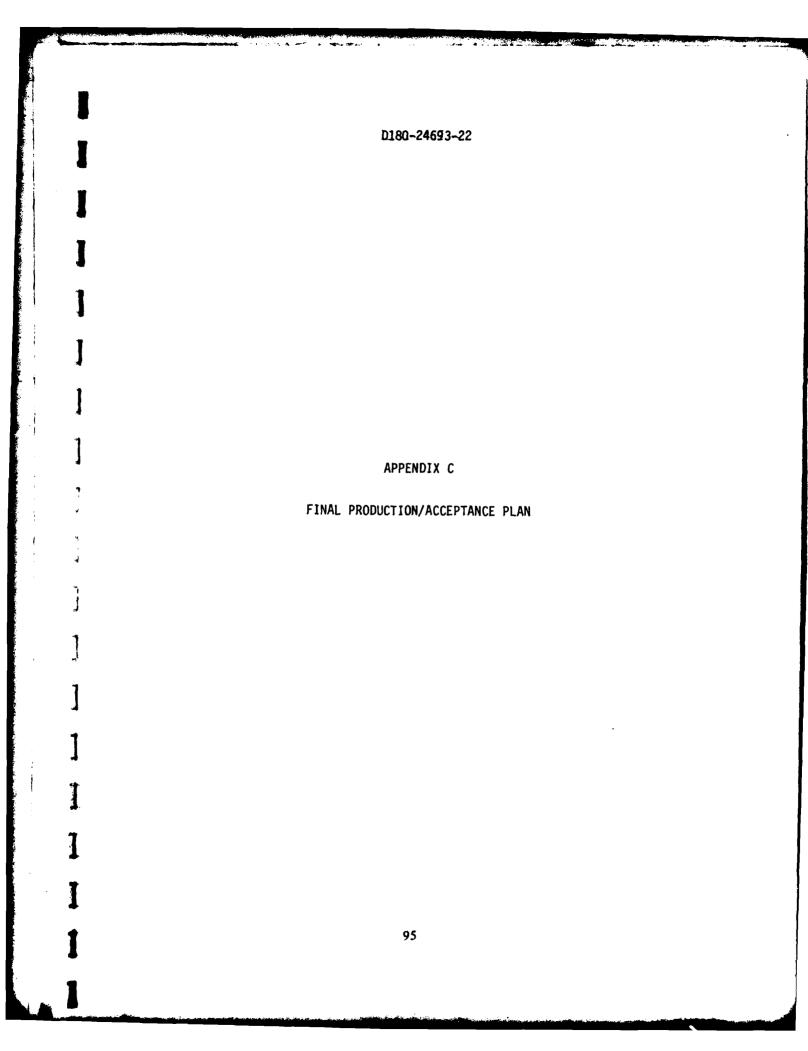
Phase III of the program consisted of the installation of the prototype harness and stand-alone link in the Class III (Full Scale) E-3A mock-up and then the complete review and modification of all program documentation to upgrade it based upon knowledge gained thru the prototype fabrication and installation. Design of a production cable to be built in Phase IV was initiated so that materials could be ordered to meet schedule requirements.

Phase IV of the program consisted of the fabrication of 21 harness (20 hybrid fiber bundle, single fiber, and conventional wire types and 1 single fiber, conventional wire type). All harnesses were built in a production mode using the revised documentation to test validity of the design and the process specifications. After the fabrication sequence, four of the twenty harnesses and the one single fiber harness were installed in the mock-up and checked for installation damage. Process specifications were again reviewed to verify correctness and utility. This final installation was part of the contract demonstration.



-21 FT 3 IN D0003 D0004 D180-59002 USE FOR DRAWINGS AND HEND PRINTED MATERIAL ONLY - NO TYPEWRITTEN MATERIAL -68 FT 4.25 IN-00001 00002 D180-59003 4 F/O CABLES HARNESS CONFIGURATION FIGURE 6.0.1B 180-59002 and 180-59003 STAND-ALONE LINK) CODE DENT NO. SIZE 0180-24693-21 A 81205 REV SCALE SHEET 9 T 01 4816 2001 REV. 1/74 -----94

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FINAL REPORT

IN-PROCESS TESTING OF FIBER OPTIC CABLES AND HARNESSES

O. R. Mulkey

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Boeing Aerospace Company P.O. Box 3999 Seattle, Washington 98124

4 JUNE 1980

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FINAL REPORT FOR PERIOD 16 DECEMBER 1979 THROUGH 4 JUNE 1980

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Phase IV of NOSC Contract N00123-78-C-0193

Prepared For:

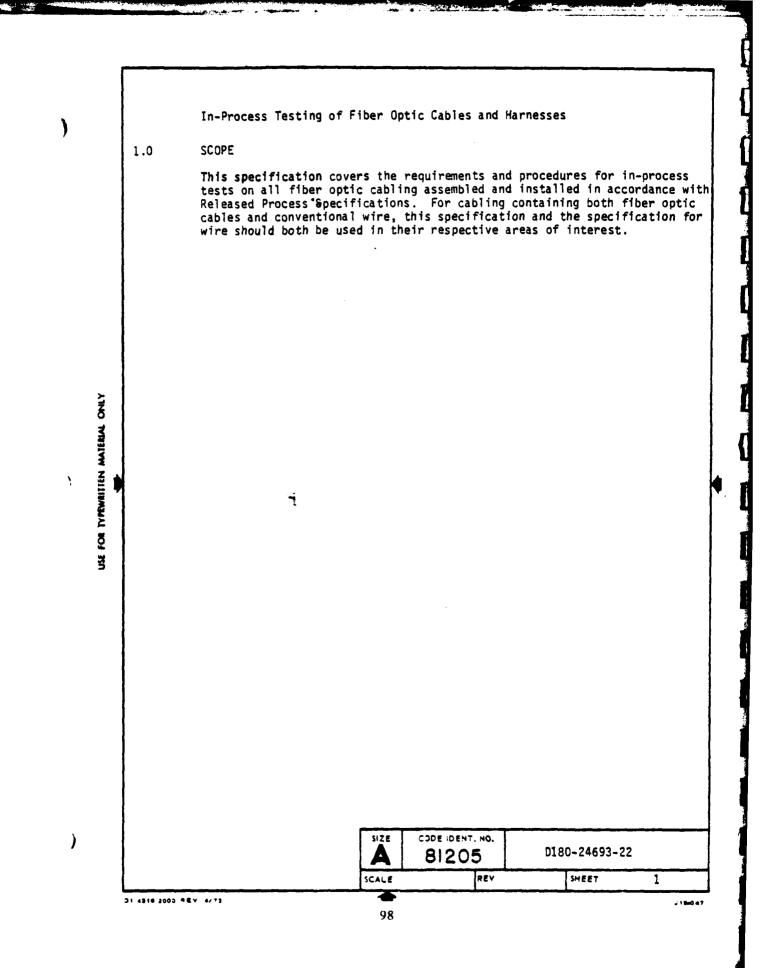
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		- CONTRACT OF GRANT NUMBER(4)
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Seattle, WA 98124		
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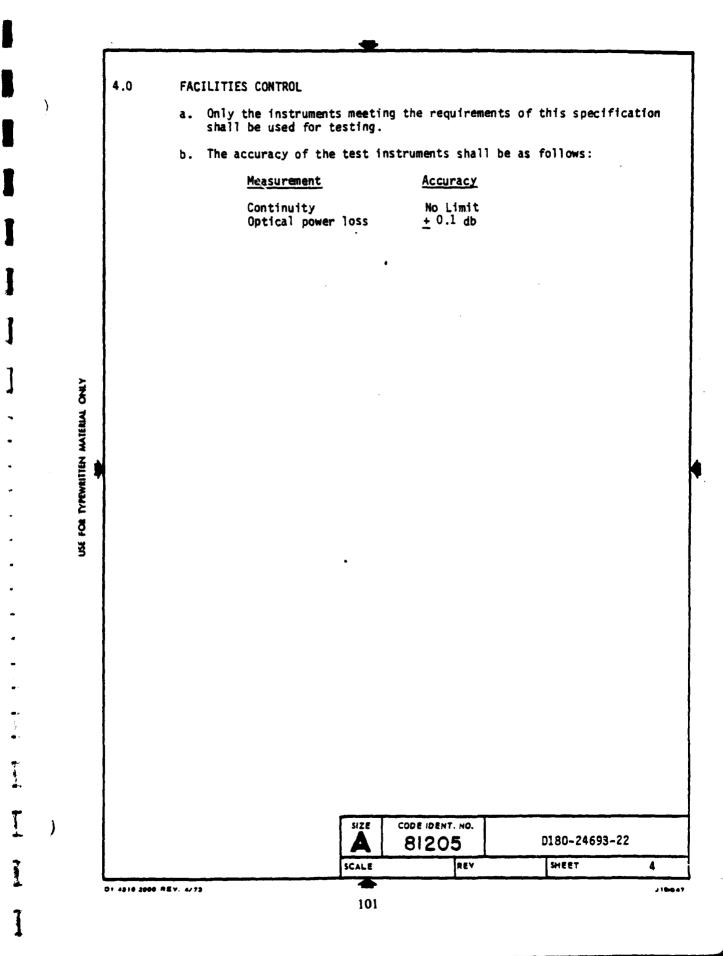
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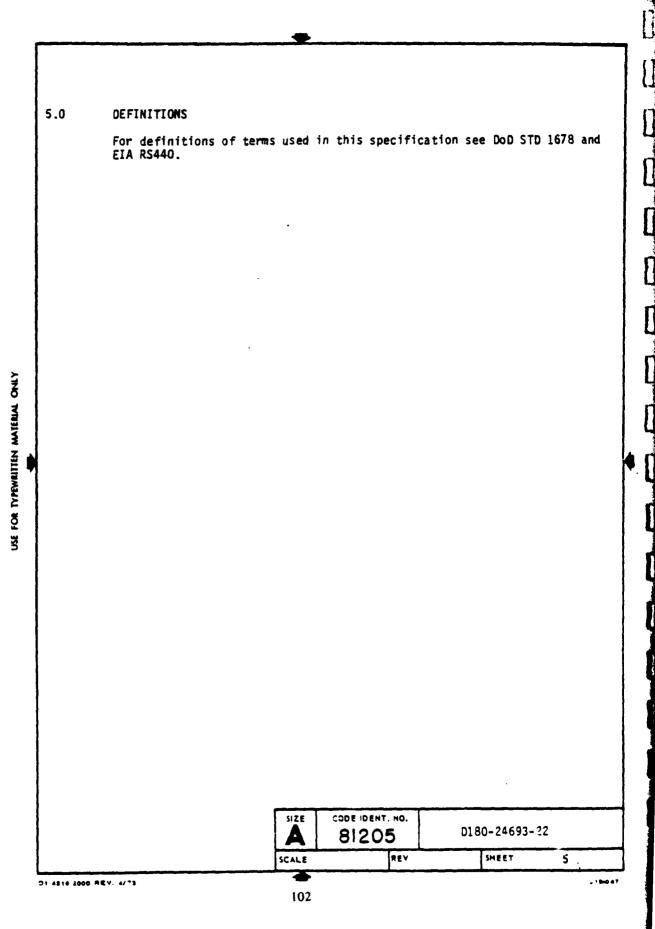


2.0	REFERENCES								
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6.0	MANUFACTURING CONTROL								
	All personnel involved in the testing of fiber optic cabling shall be properly instructed to operate the test equipment and adequately trained to carry out the test procedure.								
	WARNING:	hazardous areas explosive materi	which e al of t in the t	ither containe he ordinance,	be not made in a d, or have conta dust, or flammab formed with an e:	ined, le vapor			
	CAUTION:	Uncoupled plugs cables which mat with dust caps.			oduction cables, les, are to be p				
6.1	Testing to Basic Requirements								
	This level of testing shall be used unless otherwise specified on Engineering drawing.								
6.1.1	Terminated Cabling Without Connectors (Assembled cabling terminating in any hardware except connectors).								
	The following tests shall be performed on all assembled cabling not having connectors.								
6.1.1.1	Continuity								
		the continuity of t source. Measur							
6.1.2	Cabling With Connectors								
	The follo connector	wing tests shall s.	be perf	formed on all a	ssembled cabling	having			
6.1.2.1	Continuity								
	a. Test for the continuity of all cables.								
	b. For cabling having potted connectors, the continuity of all cables may be tested before potting and must be tested after potting								
6.1.2.2	Insertion Loss								
	Cables shall be tested to the insertion loss limits detailed on the assembly drawing.								
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 6.1.2.3 Visual Inspection a. Surface finish shall be inspected to the limits detailed in the assembly drawing. Microscope power to be used shall be such that, for fiber bundles, the bundle end shall fill from ½ to all of the field of view. For a 45 mil bundle, the range will generally be from 50X to 100X. Single fiber ends shall be examined at no less than 100 Oblique reflected light shall be used. b. Active fiber count shall be determined photographically for all bundle containing greater than 19 fibers. The quantity or percentage of unl fibers shall be detailed in the assembly drawing. 6.1.3 Installed Cabling The following tests shall be performed on all installed cabling. 6.1.3.1 Continuity a. Test for the continuity of all cables. b. For cabling having potted connectors, the continuity of all cables may be tested before potting and must be tested after potting data wing. 6.1.3.3 Visual Inspection a. Surface finish shall be inspected to the limits detailed in the assembly drawing. 6.1.3.3 Visual Inspection a. Surface finish shall be inspected to the limits detailed in the assembly drawing. 6.1.3.3 Visual Inspection a. Surface finish shall be inspected to the limits detailed in the assembly drawing. Microscope power to be used shall be such that, for fiber bundles, the bundle end shall fill from ½ to all of the field of view. For a 45 mil bundle, the range will generally be from 50X to 100X. Single fiber ends shall be used. b. Active fiber count shall be determined photographically for all bundle containing greater than 19 fibers. The quantity or percentage of unl? fibers and the allowable area of voids shall be detailed in the assembly drawing. 		
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- a. Quality Control shall verify the successful completion of in-process testing in accordance with the requirements of this specification.
- b. Quality Control shall ensure that both test connectors and terminated connectors and their contacts are clean and have contacts straight, smooth, and aligned before and after tests.
- c. Quality Control shall ensure that test leads are not placed so that they can be jarred or stumbled over, thus exerting damaging forces on contacts.
- d. Quality Control shall ensure that uncoupled ends of plugs and receptacles of production cables and test cables which mate with production cables are protected with dust caps except when necessary to work directly upon them.
- e. Quality Control shall ensure proper selection and utilization of equipment to meet the requirements of this specification.
- f. Quality Control shall ensure that test equipment is certified in accordance with the applicable test equipment certification requirements.

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USE FOR TYPEWRITTEN MATERIAL ONLY

APPENDIX D

FINAL FIELD MAINTENANCE AND REPAIR

D180-24693-23

FINAL REPORT FIELD MAINTENANCE AND REPAIR OF FIBER OPTIC CABLES AND HARNESSES

O. R. Mulkey Boeing Aerospace Company P.O. Box 3999 Seattle, Washington 98124

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4 June 1980

Interim Report for Period 16 December 1979 Through 4 June 1980 Phase IV of NOSC Contract N00123-78-C-0193

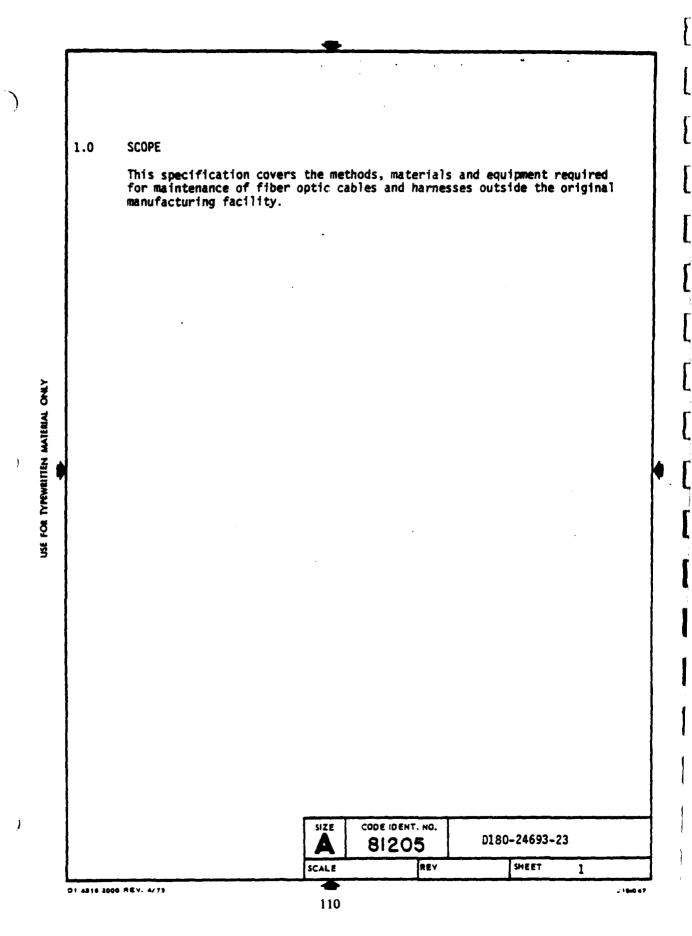
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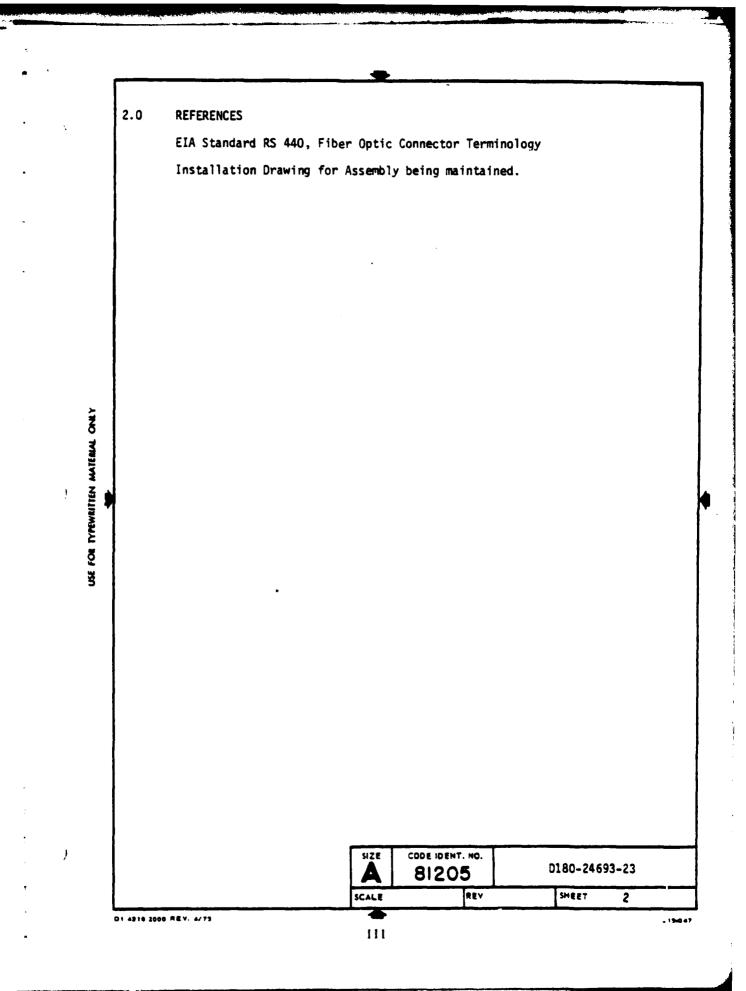
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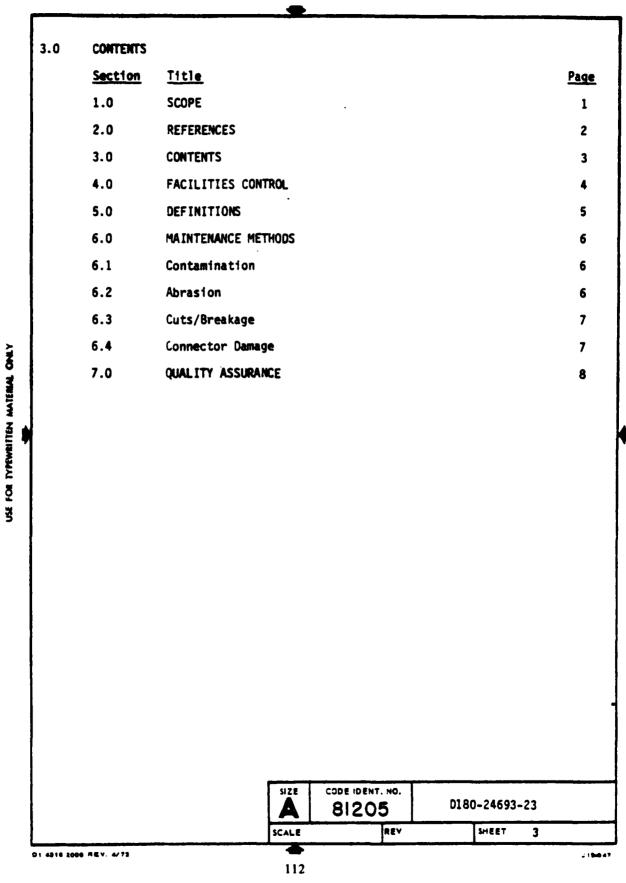
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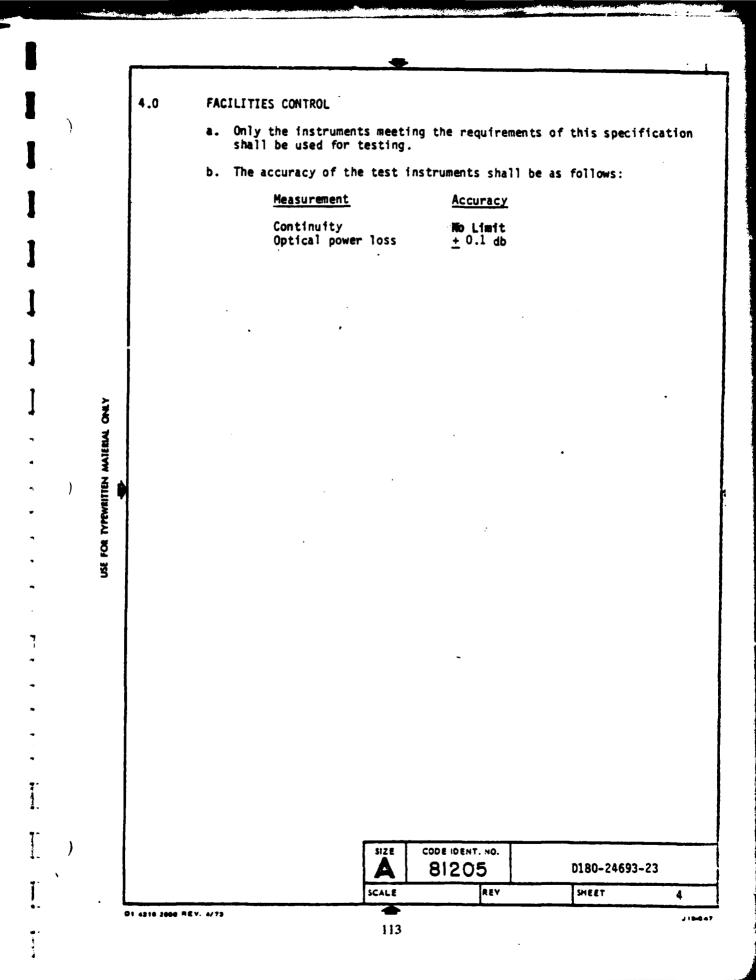
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) 5.0 DEFINITIONS For definitions of terms used in this specification see DoD STD 1678 and EIA RS440. USE FOR TYPEWRITTEN MATERIAL ONLY \$) SIZE CODE IDENT. NO. D180-24693-23 81205 SCALE REV SHEET 5 11 T D1 4818 2008 REV. 4/73 134847 114

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Service of

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	SIZE	CODE IDENT. NO. 81205	D180-24693-23
	Superficial damage may be repair applicable pressure sensitive ta overlap. The wrap should extend area. An alternate method is co shrinkable tubing extending one	pe using a spiral one inch on each vering the affecte inch on each side	wrap with 1/2 lap side of the damaged ed area with a heat
	Cable Exterior		
	Check for surface contamination If either is present follow the		
	Optical Surface Abrasion		
5.2	Abrasion		
	Remove any soft contaminant by w residue may be removed by rewipi assembly drawing.		
	Protect optical surfaces of the near the connector.	connector during a	any cleaning operation
6.1.2	Cable/Connector Exterior Contami	nation	
	If the resurfacing procedure is per Assembly drawing.	not satisfactory,	replace or reterminate
	If repeated cleaning of the surf if excessive surface damage is e acceptable limits) the connector tools and materials called out o be as noted.	vident (see Insta may be resurface	llation drawing for d using the polishing
	Gently clean surface of termina A "Q tip" or similar cotton tip removal of the termination from removal is required use only the for the connector type. Inspect made for complete removal of res pitting. The optical power loss detailed on the installation dra	bed applicator may the connector may e removal and inse tion of the cleane idue and for abse s should be retest wing or maintenan	be used. In some cases be necessary. If rtion tools recommended d termination should be nce of scratching or ed using test equipment ce procedure.
6.1.1.2	Maintenance Procedures		
	Indications of optical contamination in signal strength and visual e	tion include loss	of signal, variation
6.1.1.1	Indications		
6.1.1	Optical Contamination		
6.1	Contamination		
6.0	MAINTENANCE METHODS		

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 6.3.1 Optical Fiber 6.3.1.1 Fiber Bundles Cables A limited number of individual fibers may be broken in a fiber bundle cable. The quantity is listed on the assembly drawing for that cable. A count may be made either visually or photographically. An excessive number of broken fibers in a cable is cause for rejection and replacement unless spare cables are included in a harness. Removal and replacement onless compare cables are included in a harness. Removal and replacement of cable terminations from the connector must be accomplished usit tooling described on the assembly drawing or in an established maintem procedure. 6.3.1.2 Single Fiber Cables A broken fiber in a single fiber cable which is part of a harness may lipelaced with a new fiber if sufficient sheath material is left to provide an area for termination. The broken fiber should be removed and the new one fished through the sheath using a length of "piano wire as a tool. A spare cable of course may be used if available. Terminations should be removed and replaced from the connector per the instructions of the assembly drawing or maintenance procedure. 6.3.2 Sheath/Jacket Cuts or breakage of the sheath or jacket which penetrate to the optical fiber of fibers may be repaired using the method of 6.2.2. 6.4 Connector Damage Superficial damage to connector shells or backshells, i.e., nicks, gouges, scrapes, are not cause for replacement. Any rough edges should be dressed with a file or deburing tool to prevent damage to personnel or other equipment. 	6.3	Cuts/Breakage	•			
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7.0	QUALITY ASSURANCE
7.1	General Seneral
	Any cable repair involving the removal of the cable or disconnection of the connectors will require that protective end caps be placed on all matings surfaces of affected connectors.
	Care should be taken in handling cables and harness so as not to exceed minimum bend radius limits detailed in the cable assembly drawing or maintenance procedure.
	Cables should not be subjected to severe shock, i.e., dropping, etc., If in doubt as to the handling history of the cable/harness during repair a full visual examination and optical power loss test should be performed
7.2	Optical Surfaces
	Any repair technique to the optical surfaces of a cable or termination/ contact other than "gentle" cleaning with an approved solvent will requir the visual examination of the repaired resurface and retest for optical power loss which is detailed in the cable assembly drawing or maintenance procedure.
7.3	Cable
	Repairs to the cable should be examined for neatness and workmanship. Materials used should be those detailed on the assembly drawing or maintenance procedure.
7.4	Connector
	Repairs involving disassembly of the connector terminations will require visual examination and optical power loss test per cable assembly drawing or maintenance procedure.
	Superficial damage repair requires examination for workmanship and proper operation of the connector only.
	SIZE CODE DENT. NO. 81205 D180-24693-23

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APPENDIX E

MANUFACTURING TECHNOLOGY COST ANALYSIS

APPENDIX E MANUFACTURING TECHNOLOGY COST ANALYSIS

In a contract awarded to the Boeing Aerospace Corporation, Seattle, Washington, the objective of the task was to develop installation processes and procedures for the incorporation of fiber optic interconnect systems aboard military aircraft. As a portion of this task, a life-cycle cost analysis of the optical cable was performed. It was apparent that weight and size reductions of fiber optics offered economic advantages. With the E-3A as the baseline military aircraft, it was possible to increase the E-3A sortie time by 2.5 percent, which can be equated to a reduction of fleet squadron size by 1.5 aircraft.

The reliability of fiber optic interconnect systems appears to be equivalent to wire interconnect systems. It appears easier to install, remove and/or replace optical fibers. Optical fiber interconnect systems are also simpler to test. Spares, repair parts, materials, and special support/test equipment add to initial costs, as does almost any new technology, but the impact is minor. With simpler equipment and techniques there may be a long-term savings potential. Overall costs and benefits of fiber optics appear to surpass the E-3A wire interconnect configurations.

An important assumption has been made that must be recognized as a basis for the results of this life-cycle cost analysis. Material costs are based on current vendor estimates but production set-up cost and other engineering/manufacturing costs are based on a futuristic analysis and prediction of a large production of fiber optic harnesses fabricated at a rate typical of wire harnesses. This report will not attempt to predict with accuracy the cost variations of the current fiber optic technology nor the inflationary impacts of the future of fiber optics versus wire materials.

The overall results from Boeing's parametric cost model (PCM) indicate a per system cost for this project's twenty-one systems at \$7893 for technology developments. Projecting these initial costs and manufacturing technology concepts to a planning production cost base, the fiber optic harness cost will be about \$3620, which is a reduction of more than half of the initial technology development costs. Wire harness costs per system are about \$4900, which is a nine-percent increase over the optical fiber harness. Engineering costs are reduced by 38 percent for the fiber optic harness and manufacturing costs are reduced by 16 percent. Initially, because of the high cost of the connectors, fiber optic material costs had increased above wire material costs by nearly 300 percent. After one year, the increased use of fiber optic materials has driven costs down, while the cost of metals was rising. Thus, this results in a cost savings in using fiber optics.

This cost analysis includes acquisition cost elements involved in producing fiber optic harnesses in a modern production and manufacturing facility. It also includes ownership cost elements derived from applicable historical data and from reliability and maintainability analysis.

Production set-up costs, the nonrecurring costs, are based on the concept of a production facility which is of minimal scale for yielding economical benefits from advanced automated equipment and methods. Equipment costs are based on quotes or estimates of purchase prices or upon engineering estimates.

Manufacturing costs, the recurring costs, relate primarily to the flow of tasks and processes which generally dictate the greatest share of the cost of a harness assembly.

Production and manufacturing cost estimates are based on a survey and analysis of company experience in producing various quantities of wire harness assemblies for both military and commercial programs. Three separate and distinctly different company production/manufacturing facilities provide the primary base of experience. The approach used was to correlate this experience with similar tasks related to production/manufacture of a fiber optic harness assembly and then to provide engineering estimates of unique equipment, tasks or processes. These results are supported by harness assembly cost model estimates and by generic level cost factors established from direct experience or past and ongoing company programs.

In manufacturing, process flow manhours is the dominant factor related to manufacturing costs. The tasks, steps, and related timelines for the baseline wire harness assembly have been estimated by financial and by mechanical and industrial engineering specialists. Similar estimates have then been applied to a planned fiber optics harness assembly process, with the addition of unique steps and processes. The epoxy/dry/cure/grind/polish task is the dominant cost factor. Cost effectiveness therefore hinges to a large degree upon development of automated equipment and improved techniques.

Wire harness and cable production costs incurred on past programs, SRAM, Minuteman, E-3A, etc., have been factored into a manhour-per-wire ratio. This factor has also been tracked along improvement curves as program and production experience is accrued. This history applied to the baseline wire cable yields a first unit DDT&E cost of approximately 24 menhours. The historical data for the Short Range Attack Missile, SRAM, reflects an approximate 28% higher cost for carrier aircraft harnesses than the average harness on the program. With

this adjustment, costs of 47 and 31 manhours are obtained for the DDT&E and production units, respectively. Using this history along with a range of improvement curve histories, the following high and low estimates are obtained for the average cost of 20 production units:

1. High estimate, assuming a 90% improvement curve slope and 47 manhours for the first unit, is 35 manhours.

2. Low estimate, assuming a 90% improvement curve slope and 24 manhours for the first unit, is 16.5 manhours.

These estimates frame the range of costs for typical DDT&E and production units.

Estimates of fabrication costs of the fiber optic harnesses utilized in the YC-14 were made based on the assumption of a cost breakdown similar to this contract. This assumes that the company which fabricated the eight YC-14 optic harnesses/cables did so as part of a DDT&E effort which allocated 12 percent of the total cable cost to fabrication. In this case \$167 of the 1393.00 purchase price would be allocated to fabrication. Further, assuming that technology advancements and labor rates act to balance cost effects of fabrication, then this would equate to approximately 5 manhours at a \$34 per manhour manufacturing WRAP rate.

The DTLCC cable assembly computer model estimated an average cost of approximately 8 manhours for each of eight equivalent wire harnesses produced on an improvement curve with a 90% slope.

The above results suggest that fiber optics manufacturing and fabrication experience of the past offers economies at least comparable to wire harness

assemblies. It should be observed that three assemblies were utilized on two YC-14 aircraft (six harnesses) with no failures in over 600 flight hours. Each of the harnesses included four fiber cables and two connectors.

Operation and support costs analyses are based on historical data on the E-3A aircraft along with an extensive history on four Navy aircraft, the S-3A, E-2C, P-3C and EC130G and Q.

A reliability analysis of both the baseline wire harness assembly and the fiber optics assembly provides the added information base appropriate for prediction of fiber optic harness field reliability maintenance factors. Policies of the using agency relative to inventory, spares, and repair parts appear to be the dominant factor affecting the supply and support costs. Since the baseline harness assembly is for an E-3A aircraft, the policy for this aircraft was selected as a baseline in conjunction with policies formulated in the A-7 ALOFT Project Technical Reports NELC TR 2024, 1998, 1982 and 1968. Some cost elements are also derived based on operational efficiencies that could be realized for a fiber optic harness configured E-3A.

A historical base for estimating installation, operation, and support costs and data for MTBF and MTTR estimates for fiber optics harnesses is extremely limited. The experience record of six fiber optic harnesses (four fiber bundles per harness) utilized in the YC-14 aircraft avionics system reflects zero failures in over 600 flight hours. A history base for wire harnesses in military and commercial aircraft is also relatively limited. Wire harness failures and maintenance actions are most generally recorded in a category associated with the system or subsystem of which they are a part. A

search of service history records on military aircraft uncovered some data on five aircraft which are included in Appendix H. The lack of data indicates a proper area to be investigated by the services in the interest of minimizing life-cycle costs. This conclusion is based on costs attributed to failure and maintenance of harnesses and cables as compared to costs of maintaining detailed records.

For comparison and estimation purposes assume that fiber optics harnesses/ cables are used for all applications except power distribution. Further, assume that a weight savings of 50% is achieved by replacing baseline wire harness with the fiber optics harness. This results in a total weight savings of 1,378 pounds per aircraft. When this weight savings is replaced by jet fuel it increases the sortie length by a factor of 1.167×10^{-4} hours/lb. The sortie length increases by 0.16 hours (9.65 minutes) or a 2.5% increase. Under the assumption that this increased sortie length can be utilized effectively over the fleet of E-3As (a reasonable assumption) then an increase in effectiveness equivalent to 1.5 aircraft is achieved. This equates to an acquisition cost savings for at least one aircraft at a cost in excess of \$100,000,000.

An institute for defense analysis paper (IDA paper P-1244 May 1977) concluded that a decrease of one pound in avionics weight will result in a decrease of six to eight pounds in 'dry' weight due to system overhead effects within the total aircraft system. It concluded that since fly away cost per pound of a modern fighter is approximately \$500 per pound the savings in cost per pound would average in the range of \$3500 per pound of avionics weight reduction in 1975 dollars.

Applying this factor to the E-3A example yields an acquisition cost savings of \$4,823,000.

Estimate for the installation of a group of harness assemblies which include the baseline wire harness assembly during aircraft production is approximately six hours. Since, during cable installation a group of cables are installed at one time, the exact time line for a single cable is not traced. However, installation of the baseline harness by itself would approach one half to one hour.

Installation or removal and replacement estimates are dependent upon the size and weight of the harness assembly. Hence, if the fiber optics harness is smaller and lighter, then a potential savings exists but it is judged to be of minimal significance.

Appendices A through H provide the necessary cost elements, cost data, and cost equations to support the findings reported in this analysis.

In summary, acquisition cost estimates by models and by analysis of processes and techniques reflect potential cost savings for fiber optic interconnect systems as compared to wire harnesses. Since most models rely upon historical data and "conventional methods of business," it is implied that savings are realizable with technology maturity and with methods and techniques commonly employed.

Many options exist for production set-up and related costs. The most desirable option will depend on many factors such as level of business forecasts, advancement of the technology, demands on existing harness/cable production

equipment and facilities, facility space available for expansion or relocation, economic posture of the company, etc.

The potential for cost improvement in the manufacturing/fabrication process is promising. The development of automated equipment and expedient techniques is needed to exploit this potential; however,

a. cost elements related to operations and support aspects appear to have offsetting effects.

b. cost savings are realized through weight and size advantages, while losses occur through added inventories, training, and special equipment requirements.

c. reliability considerations have a similar neutralizing effect.

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- 5. Greenwell, R.A. & G. Kosmas, <u>Airborne Fiber Optics Manufacturing Technol-</u> ogy, NOSC TR 340 24 Oct 1978.

APPENDIX A COST BREAKDOWN STRUCTURE

- A. Research and Development Cost Elements
 - 1. Program Management

Contracts

Cost/Schedules

Logistics Support

Configuration Baselines, Changes and Records

2. Engineering

Design Engineering and Design Support

Direct Labor

Materials

Overhead

3. Fabrication

Full scale model development

Direct labor

Materials and overhead for material procurement

Tooling and test equipment for manufacture, fabrication, assembly and test

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4. Development Tests

Demonstrate that design specifications are met.

Performance

Maintenance/Reliability

Direct labor, materials, overhead

5. Test Support

Support of government tests.

6. Producibility Engineering and Planning

Technical data packages

Special purpose equipment/tool design

Computer modeling/simulation

Engineering drawings/diagrams

Material, inspection, test, etc. information

7. Engineering Data

Drawings or lists

Specifications

Plans and procedures

Reports and documents

Technical orders and manuals

8. Peculiar Support and Test Equipment

Equipment

Tools

9. General and Administration

General Officers and staff

Fringe benefits

10. Fee or Profit

8. Production (Non-Recurring)

1. Program Management

Configuration

Cost/schedules

2. Production Facilities

Engineering

Tooling and tooling modifications

Property acquisition/modification

Manufacture support equipment

3. Technical Support

Acceptance tests or operational acceptance/evaluation test

- 4. Spares and Repair Parts
- 5. Training

Instructor and maintenance training of Navy personnel.

6. Engineering Data

Drawings, lists, specifications

Plans, procedures, reports, documents

7. Support Data

Maintenance data

Provisioning data and lists

Logistics support plans and progress reports

8. Management Data

Configuration management

Cost, schedule, contract data

Labor, materials and overhead

9. Peculiar Support and Test Equipment

Equipment, tools

develop under other cost element

(PMS checks and routine maintenance)

10. General Administrative

General and executive offices

Staff services, etc.

- 11. Production Acceptance Test and Evaluation
- 12. Profit/Fee

- C. Production (Recurring)
 - 1. Manufacturing

Fabrication, assembly, processing, etc.

Labor, overhead and direct charges

2. Production Material

Off-the-shelf hardware

Subcontract items

Raw material/semi-fabricated material

3. Sustaining Engineering

Redesign and evaluation

Maintainability/reliability

Manufacture/production

4. Quality Control and Inspection

5. Packaging and Transportation

Packing for shipment

Transportation to point of contract

- 6. Assembly, Installation and Checkout
- 7. General and Administrative

8. Fee or Profit

- D. Operations and Support
 - 1. Operations

Cost of readiness

Im proved efficiencies

- 2. Maintenance Personnel
- 3. Maintenance Facilities
- 4. Support Equipment Maintenance
- 5. Supply Personnel

6. Supply Facilities

7. Spare Parts and Repair Materials

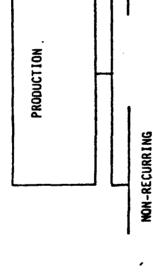
8. Inventory Management/Administration

9. Packaging, Handling and Transportation

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DEVELOPMENT TEST AND EVALUATION

DESIGN

ECULIAR SUPPORT AND TEST EQUIPMENT

GENERAL AND ADMIN.

FE

GENERAL AND ADMIN. **FRAINING**

PECULIAR SUPPORT AND TEST EQUIPMENT

MANAGEMENT DATA SUPPORT DATA

EE/PROFIT

GOVERNMENT SUPPORT

PRODUCTION ACCEPTANCE TEST & EVALUATION

FIBER OPTICS IN _RCONNECT SYSTEM

LIFE-CYCLE-COST CONSIDERATIONS

MANUFACTURE RECURRING

PRODUCTION FACILITIES

TECHNICAL SUPPORT

PROGRAM MANAGEMENT

SUSTAINING ENGINEERING PRODUCTION MATERIAL GENERAL AND ADMIN. INSTALL & CHECKOUT QC AND INSPECTION PACKAGING AND TRANSPORTATION FEE/PROFIT

SPARES AND REPAIR PARTS

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ENGINEERING DATA

MANUFACTURING SUPPORT EQUIPMENT

OPERATION AND SUPPORT

FACILITIES SUPPORT EQUIP. INVENTORY MGMT. AND SPARE PARTS AND REPAIR MATERIALS FACILITIES PERSONNEL PERSONNEL MAINTENANCE **OPERATIONS** ADMIN. SUPPLY

PACKAGING, HANDLING, AND TRANSPORTATION **FRAINING**

TECHNICAL DATA

Interconnect Harness Cost Breakdown Table B-1 Interconnect Harness Cost Comparisons for DDT&E

Fiber Optics (Projected Design and Build with Established Processes and Standards)	Dollars	1,100	1,449	520(3)	1	\$3,069
Fiber Optics (Projected Design and Build with Es Processes and Standards)	Hours	20(4)	41.9(5)	ı	·	
Wire (Baseline Harness)	Dollars	1,199	1,490	552	,	\$3,241
W (Baseli	Hours	21.8	43.1(5)	1	I	
Fiber Optics (Current Contract)	Dollars	4,335	2,153	1,356	49	\$7,893
Fibe (Curren	Hours	130	63			
Function		Engineering (1)	Manufacturing (2)	Production Material	Other	Totals(6)

The engineering WRAP rate for the current contract is \$33.30 as compared to a WRAP rate of \$55 used for the baseline harness and the fiber optics projection. The \$55 WRAP rate is typical for large programs. Ξ Notes:

- (2) The manufacturing WRAP rate is approximately \$34 for all comparisons.
- (3) Material costs are adjusted based on projected quantity purchases.
- Engineering is projected to be less than wire due to reduced size, weight and complexity of design. Refer to pages 24 and 25 for a summary of engineering tasks and considerations. (4)
- Manufacturing estimates are based on experience data for small quantity design and build. Refer to 5.0.A and Appendix G for manhour estimates based on experience data. (2)
- (6) Values are expressed in 1978 Dollars.

APPENDIX B

A few important and vital factors relative to the above comparisons must be recognized. First, fiber optics is a new technology while wire harness production is a matured industry. Second, for the current contract effort some fiber optic components are comparatively expensive and additional parts and materials are required for developmental contingencies. Production costs of fiber optic components in quantity lots can decrease costs considerably. Thirdly, even establish technologies offer opportunity for dramatic cost improvement. Initial harness assemblies have experienced improvement along an improvement curve with 70% slope. Follow-on production quantities also commonly experience improvement along improvement curves with slopes in the average range of 90%. A greater rate of improvement is anticipated for fiber optics harnesses.

Included below are program financial estimates broken down to a single harness assembly for both fiber optic and baseline wire harness assemblies. The fiber optic estimate is based on the revised firm price fixed proposal dated 24 April 1978. The wire harness estimate is based on financial accounting and cost estimates.

Cost Element	Cost Goal
Direct Labor Engineering Developmental Elec. Mil. Quality Assurance Program Finance Controls Total Direct Labor	\$ 1,465 508 34 <u>210</u> \$ 2,217
Labor Overhead Engineering Manufacturing Elec. Mil. Quality Assurance Program Contracts Total Labor Overhead	453 441 25 <u>567</u> \$ 1,486
Travel	36
Other Direct Costs Fringe Benefits Freight-In Product Liability Insurance Sub Total (All of above)	995 28 <u>2</u> \$ 4,728
General and Admin. Expense Products New Business Puget Sound Total G&A	811 136 \$ 947
Direct Materials Production Materials	\$ 1,217
Washington State Taxes	\$ 89
BCS	\$6
Total Estimated Cost	\$ 6,987
Profit	849
Total Price	7,836
CAS 414 Cost	57
Total Grand Price	\$ 7,893

Fiber Optic Interconnect System Cost Estimates

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Table B-2

Note: The above estimates were derived from proposal estimates by extracting the stand-alone link engineering costs and then by factoring other costs by 22 (the total number of harnesses to be produced under the current contract).

<u>Lost Element</u>	Cost Es	
	Dollars	Mannours
Engineering (3 manmonths)	\$1,198	21.7
Fabrication Production Labor Tool and Planning Tool Labor Inspection Labor Finge @ 43%	254 22 22 45 147	32.7 2.55 2.55 5.3
Manufacture Overhead	777	-
Production Material	493	-
Distributed Material	19	-
Jol Material	4	-
Direct Chaliges	15	-
State and Local Taxes	5	-
CAS 414 Costs	21	-
Total Cost (excluding Engineering)	\$1,824	-
Profit/Fee (excluding Engineering) @ 12%	<u>\$ 219</u>	-
Grand Total (including Engineering)	\$3,241	

Table B-3							
Baseline	Wire	Harness	Assembly	Cost	Estimates		

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A CONTRACT OF A

		Cost		Fixed or Tradable*	
		<u>Qty</u> .		Mire	F/o
1.	Cut and code equipment options				
	a. Ink jet marker b. Conrac C. Trojamatic	1 1 1	100,000 150,000 20,000	A A 0(2)	A(1) A(1)
2.	Stripper equipment options				
	 a. Ewbanks (or equivalent) automatic b. Ideal (or equivalent) manual c. Carpenter (or equivalent) manual, power d. Work station - tables, lighting, storage 	2 100 2 3	8,000 5,000 1,200 4,200	R R O R	R R O R
3.	Crimper equipment options				
	a. Amp (or equivalent) automatic/power b. Vip (automatic/power) c. Manual, hand operated @ 250 ea.	3 1 250	60/mo.ea. 4,550 62,500	R 0(3) R	0(4) 0(4) 0(4)
4.	Tie tables and form boards				
	a. Tie tables @ \$1000 ea. b. Form board support tables @ \$500 ea. c. Form boards @ \$25 ea.	3 50 100	3,000 25,000 2,500	R R R	R R R
5.	Processor/Printer equipment				
	 a. Word processor Xerox, 850 or equiv. b. Convertor or communicator c. Frieden 	1 1 1	18,000 3,600 12,000	0(5) 0(5) 0(5)	0(5) 0(5) 0(5)
6.	Braiding equipment				
	a. Braid machine b. Braided shield termination equipment c. Wire wrap (Wraps tape) d. Braid spool machine	1 1 1 1	18,000 8,000 4,000 3,000	R R R R	R O R R
7.	Tie wrap equipment				
	a. Panduit (or equivalent) plastic tie, power b. Thomas & Betz (or equivalent) manual c. Ultrasonic (or equivalent) cloth tie	2 4 2	1,800 250 3,000	R R R	R R R

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APPENDIX C PRODUCTION SET-UP EQUIPMENT COST OPTIONS

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*R-required, A-alternates, O-optional

		0 - 1	Fixed or Tradable*	
	<u>Qty</u> .	Goal	Wire	<u>F/0</u>
Testing Equipment		٠		
 a. DITMACO (or equivalent) b. Cable, scan (or equivalent) continuity tester c. Test cables d. Cable management system 	1	110,000	R	R
	2 100 1	20,000 50,000 200,000	R O	A R O
Miscellaneous equipment				
 a. Heat guns @ \$80.00 b. Hand cutters @ \$25.00 c. Solder irons @ \$80.00 d. Burn tools @ \$100.00 e. Exhaust fans @ \$190.00 f. Pin insertion/removal tools 	20 50 15 10 15 20	1,600 1,250 1,200 1,000 2,850 1,000	R R R R R R	R R R R R
Potting and Epoxy Equipment (silicon and non-silicon)				
 a. Oven (hot air) b. Vacuum table (mixing, etc.) c. Vacuum impregnator d. Electronic balance (scales) e. Mechanical balance (scales) f. Marble tables g. Deep freeze (80° below zero) h. Refrigerators i. Ovens j. Paint shakers k. Test benches 	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	8,000 4,000 40,000 2,500 8,000 1,500 1,400	R R R R R R R R R R R R	R R R R R R R R R R R R R R R R R R R
	٤	300	K	· ·
 a. Conveyor 200 ft. @ \$50/ft. b. Shelving c. Bulk parts d. Small carts \$360.00 	3 10	10,000 10,000 6,000 3,600	R R R R	R R R R
Epoxy/dry/cure equipment				
a. Oven (hot air) b. Tables and fixtures	2 2	16,000 2,000	-	R R
Grind and polish equipment				
a. First end connector machine b. Holding fixtures and supplies, i.e.,	2	9,000	-	R
abrasion wheels, solverts, swabs		2,000	-	R
	 a. DITMACO (or equivalent) b. Cable, scan (or equivalent) continuity tester c. Test cables d. Cable management system Miscellaneous equipment a. Heat guns @ \$80.00 b. Hand cutters @ \$25.00 c. Solder irons @ \$280.00 d. Burn tools @ \$100.00 e. Exhaust fans @ \$190.00 f. Pin insertion/removal tools Potting and Epoxy Equipment (silicon and non-silicon) a. Oven (hot air) b. Vacuum table (mixing, etc.) c. Vacuum table (mixing, etc.) c. Vacuum tables g. Deep freeze (80° below zero) h. Refrigerators j. Paint shakers k. Test benches l. Eye bath Materials and Parts Handling and Storage a. Oven (hot air) b. Shelving c. Bulk parts d. Small carts \$360.00 Epoxy/dry/cure equipment a. Oven (hot air) b. Tables and fixtures Grind and polish equipment a. First end connector machine b. Holding fixtures and supplies, i.e., 	Testing Equipmenta. DITMACO (or equivalent)1b. Cable, scan (or equivalent) continuity tester2c. Test cables100d. Cable management system1Miscellaneous equipment1a. Heat guns @ \$80.0020b. Hand cutters @ \$25.0050c. Solder irons @ \$80.0015d. Burn tools @ \$100.0010e. Exhaust fans @ \$190.0015f. Pin insertion/removal tools20Potting and Epoxy Equipment (silicon and non-silicon)1a. Oven (hot air)1b. Vacuum impregnator2c. Vacuum impregnator2f. Marble tables2g. Deep freeze (80° below zero)1h. Refrigerators2i. Ovens2j. Paint shakers2k. Test benches2l. Eye bath2Materials and Parts Handling and Storagea. Conveyor 200 ft. @ \$50/ft.3d. Small carts \$360.0010Epoxy/dry/cure equipment2a. Oven (hot air)2b. Tables and fixtures2Grind and polish equipment2a. First end connector machine b. Holding fixtures and supplies, i.e.,2	Testing EquipmentImage: Constraint of the systema. DITMACO (or equivalent) continuity tester1110,000b. Cable, scan (or equivalent) continuity tester220,000c. Test cables10050,000d. Cable management system1200,000Miscellaneous equipment31200,000a. Heat guns @ \$80.00201,600b. Hand cutters @ \$25.00501,250c. Solder irons @ \$80.00151,200d. Burn tools @ \$100.00101,000e. Exhaust fans @ \$190.00152,850f. Pin insertion/removal tools201,000Potting and Epoxy Equipment (silicon and non-silicon)18,000a. Oven (hot air)18,000b. Vacuum impregnator240,000c. Vacuum impregnator240,000d. Electronic balance (scales)2f. Marble tables2g. Deep freeze (80° below zero)1h. Refrigerators2f. Ovens4g. Deep freeze (80° below zero)1h. Refrigerators2f. Ovens2g. Tots backers2k. Test benches2l. Eye bath2solo10d. Small carts \$360.0010d. Small carts \$360.00	Cost Qty. Goal Goal Trai Wire a. DITMACO (or equivalent) cable, scan (or equivalent) continuity tester 1 110,000 R b. Cable, scan (or equivalent) continuity tester 1 100 50,000 R c. Test cables 100 50,000 R 1 200,000 O Miscellaneous equipment 1 200,000 0 R 1 200,000 0 Miscellaneous equipment 1 200,000 0 15 1,200 R c. Solder irons © \$80.00 15 1,200 R 1 1,000 R c. Solder irons © \$80.00 15 2,850 R 1,000 R e. Exhaust fans © \$190.00 15 2,850 R R 1,000 R d. Vacuum table (mixing, etc.) 2 4,000 R

		<u>Qty</u> .	Cost Goal	Fixed or Tradable Wire F/O
14.	Optical test and inspection			
	 a. Microscope b. Attenuation test set 	2 2	2,000	- R - R
15.	Cut and splice equipment			
	a. Cleaving b. Splicing	2 2	3,000 2,400	- R - R

Notes:

(1) The Ink Jet Marker is required for fiber optics cables if marking is required. If marking is not required the Trojamatic or equivalent may be used. - • }

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(2) A Trojamatic or similar machine is needed if a Conrac is used.

- (3) This unit is efficient for small wires.
- (4) These are required with fiber optics harness production due to possible mix of wire and fiber in a harness.
- (5) This equipment produces tapes, patches, work orders, etc. Computer services can be purchased as an alternate.

APPENDIX D

EQUIPMENT DDT&E COST OPTIONS

Equipment Description		QUANTITY	COST GOAL
1.	Ewbanks (or equivalent) automatic stripper	1	50 ,000
	evaluation and modification		
2.	Epoxy application and dry/cure equipment		
	a. Fixtures, tools, etc.	1	2,000
	b. Oven (modified)	2	3,000
3.	Grind and Polish Equipment engineering,	2	175,000
	factory and materials		
4.	Optional automatic cut, strip, epoxy, grind,		500 ,000
	polish		

APPENDIX E

Production Set-up Facilities Options

Pro	duction set-up racifities options	
1.	Expansion of an existing producti	on facility into adjacent unused areas
`	of 3000 sq. ft.	
	a. Refurbish cost with air condi	tioning = \$180,000
	b. Special electrical	≈ 9,000
	c. Air Hook-ups	= 36,000
	d. Exhaust Hook-up	= 4,000
	e. Equipment Installation	
	f. Miscellaneous	
2.	Approx. Build on to existing facilities t	
	a. New expansion (90 + 15)	= 315,000
	b. Special electrical	≈ 9,000
	c. Air Hook-ups	= 36,000
	d. Exhaust Hook-up	= 4,000
	e. Equipment Installation	•
	f. Miscellaneous	=
	Approx. Tota	1 = 365,000

 Locate complete production set-up into a refurbished facility, assume 30,000 sq. ft. and assume that parts and materials and tool storage is available in separate support area.

a. Refurbishment costs

	27,000 without air conditioning	= 1,215,000
	3,000 with air conditioning	= 180,000
b.	Special electrical	= 9,000
c.	Air Hook-ups	= 36,000
d.	Exhaust Hook-ups	= 4,000
e.	Equipment Installation	•
f.	Miscellaneous Approx. Total (142	= = 1,450,000

4.	Cons	struct new facility, assume 30,00	00 sq. ft. plus required support are	28
	of a	approximately 20,000 sq. ft.		
	a.	New facility cost	= 5,000,000	
	b.	Special Electrical	= 9,000	
	c.	Air Hook-ups	= 36,000	
	d.	Exhaust Hook-ups	= 4,000	
	e.	Equipment Installation	•	
	f.	Miscellaneous	•	
		Approx. Total	= 5,050,000	

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APPENDIX F TRAINING COSTS AND OPTIONS

A. Contractor Training

A projection of training requirements for the size of production facility and for the two proposed courses is tabulated below:

	Cou	rses
Personnel	24 Hour	16 Hour
Manufacturing (hourly)	100	10
Quality Control	10	10
Engineering	-	25
Supervision	12	15
	122	60

The above personnel and course requirements yield the following:

1.	Approximate number of 24 hour classes	-	12	classes
2.	Approximate number of 16 hour classes	-	6	classes
3.	Total classroom hours	-	384	bours
4.	Total student hours	-	3888	hours
5.	Course development hours			
	a. Eight hours per course hour for 16 hour course &x16	-	128	hours
	 Four hours per course hour for 24 hour course 4x24 	-	96	hours
	c. Instructor preparation 8x16	-	128	hours
	d. Illustrations 26x6	-	156	hours
6.	Course maintenance			
	Course length x 2 24x2 16x2	-		hours hours
	Course development manhour cost goal		588	hours
	Course development dollar cost goal 144	\$24	4,431	

APPENDIX G

MANUFACTURING PROCESS FLOW

A. Baseline Wire Harness Assembly

			COST ESTIMAT	ES (MANHOURS)
		Method #1	Method #2	Method #3	Method #4
1.	Wire Cut and Code	1.0	0.53		1.8
2.	Wire Shields - Strip and terminate	6.9	2.54	12 wires at	1.1
3.	Wire Ends - Strip and Crimp	2.8	1.33	.20 is 2.40	
4.	First End Connectors - Install pins	1.0		44 wires	.8
5.	Form Board - Layout and tie	3.0	6.46	at .50 is	6.0
6.	Wire Shield - Braid or install	3.5		22.00	2.1
7.	Jacket - braid or ' install	2.5	2.15	17 Shields at	2.1
8.	Wire Ends - strip and crimp	2.8	1.33	.20 is 3.40	
9.	Second End Connectors - Install pins	1.0	1.69		1.1
10.	Labels/Patches/Tape	.8	.32		.8
11.	Test	.5	.5		.5
12.	Pack and Ship		.3	0.3	3_
+ F.	TOTALS	26.1	17.15* to 41**	28.1	16.6*

* Estimate based on high rate/large quantity production/manufacturing set-up and 100% production efficiency.

**Estimate based on reduced rate of production and a lower level of production efficiency. Production efficiency levels based on past experience May vary over a 2.5 to 1 range.

APPENDIX G (Continued)

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B. FIBER OPTICS HARNESS ASSEMBLY

			Manhour	Estimate
			Single Fiber	Multi- Fiber
1.	Cut and Code		1.0	-
2.	Fiber Ends			
	Termination (20x.5)		10.0*	15.0*
	Grind and Polish (20x.25)		5.0*	6.7*
3.	Wire Enas - Strip and Crimp (12x.06)		0.7	-
4.	First End Connector - Install Pins		0.7	-
5.	Form Board Layout and Tie		2.2	-
6.	Fiber Ends			
	Termination (20x.5)		10.0*	15.0*
	Grind and Polish (20x.25)		5.0*	6.7*
7.	Wire Ends - Strip and Crimp		0.7	-
8.	Second End Connect - Install Pins		0.7	-
9.	Test - Photographic and Insertion Loss		2.3	-
10.	Jacket - Braid or Install		2.5	-
11.	Labels/Patches/Tape		0.8	-
12.	Pack and Ship		0.3	-
		TOTALS	41.9	55.3

*The manhour cost driver is associated with new processes. A potential exists for significant improvements.

APPENDIX H

1.0 MAINTENANCE AND RELIABILITY DATA ON AIRCRAFT WIRING

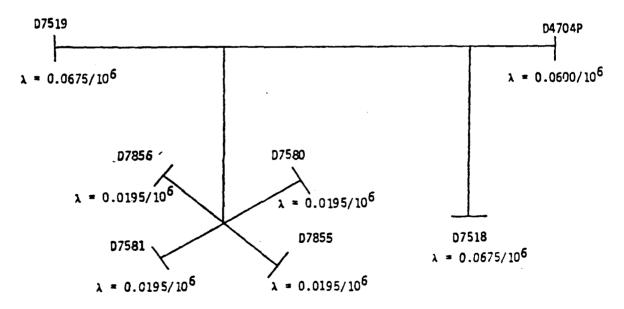
The following data base (Table H.1) was used as source for aircraft wiring maintenance and reliability history. The data is formatted in Table H.2.

TABLE Aircraft	H.1 HISTORY DATA B	ASE Flight Hours	Average Inventory	Average Sortie Length	Utilization/ Month/ Aircraft
E-2C	Jul '76 - Jun '77	13,181	23	2.79	47.76
5-3A	Mar '76 - Jun '77	56,831	81	2.75	53.97
EC-130G,Q	Mar '75 - Nov '77	38,514	10	6.78	128.4
P-3C	Jan '74 - Dec '74	71,321	93	4.85	63 .9
E-3A	May '77 - Mar '78	1,635	3	6.36	49.54

2.0 BASELINE WIRE HARNESS ASSEMBLY RELIABILITY CALCULATIONS

Failure Rate of 204-51870-5 Wire Harness Assembly

 $\lambda = 0.273$ failures/10⁶ hours, distributed as shown.



Back-up information and calculations attached.

TABLE H.2 MAINTENANCE AND DEL

AIRCRAFT WIRING MAINTENANCE AND RELIABILITY

WORK U CODE A (NUMBE OF WIR HARNES	WORK UNIT CODE AND (NUMBER OF WIRE HARNESS TYPES)	FLIGHT LINE REMOVE AND REPLACE	FLIGHT LINE FAILURES	SHOP FAILURES	REMOVE AND REPLACE PER 1000 FLIGHT HOURS	MANHOURS/ REMOVE AND REPLACE TASK	FAILURES PER 1000 FLIGHT HOURS	MMH/ 1000 FL I GHT HOURS
(101)		0	2	0	0	2.2	8	\$ 9 9 9 9
428 (172)		12	562	~	016	4.90	42.789	061.
428		38	1006	16	.669	12.974	17.983	.185
428 (206)		66	896	22	1.013	6.651	23.835	.162
428 (203)		72	1017	64	1.009	5.004	15.157	.081
TOTALS		161	3481	104	Average .9003	Average 7.276	Average 24.941	Average .1545

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2.0 (Continued)

Basic Information and Calculations for Failure Rate of 204-51870-5 Wire Harness Assembly

- Cable Construction cable is made of AWG #20 and #22 wire, with seven

 MS27467 type connectors.
- 2. Connectors used -

1 ea. MS27467T23B53P. 24 active pins, including 4 shields 2 ea. MS27467T15B35SA. 27 active pins, including 3 shields 4 ea. MS27467T11B35S. 6 active pins, including 1 shield Insert Material - dially1 phthalate

3. Operating Conditions -

Temperature - 25°C ambient with no appreciable rise due to current Environmental Service Condition - airborne, inhabited transport (A_{IT}) Connector Mating/Unmating - assume 1-5 cycles (both connect and disconnect) per 1000 hours

4. Connections - crimp, manual, standard quality factor

Calculation of failure rate due to connectors:

From MIL-HDBK-217C, Table 2.11.1-1, "Prediction Procedure for Connectors", the failure rate model for a mated pair of connectors is:

 $\lambda_p = \lambda_b (\pi_F x \pi_p x \pi_K)$ failures/10⁶ hours, where

 λ_{b} = base failure rate for the part

 π_F = factor for environmental service condition

 π_{D}^{L} = factor for the number of active pins

 $\pi K = factor for connector mating/unmating cycles$

From MIL-HDBK-217C, Table 2.11.1-5, the value for λ_b at 25°C is (by extrapolation) 0.00050 failures per million hours. The π factors in the model have the following values in this instance:

Then, $\lambda_{p1} \approx 0.0005(5x4.62x2)x1$ for the first connector type listed. $\lambda_{p1} \approx 0.023/10^6$ hours

 $\lambda_{p2} \approx 0.0005(5x5.11x2)x2$ for the two connectors of the second type. $\lambda_{p2} \approx 0.051/10^6$ hours

 $\lambda_{p3} = 0.0005(5x2.02x2)x4$ for the four connectors of the third type. $\lambda_{p3} = 0.040/10^6$ hours

 $\lambda_p = \lambda_{p1} + \lambda_{p2} + \lambda_{p3} = 0.114 \text{ failures}/10^6 \text{ hours}$

2.0 (Continued)

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Calculation of failure rate due to lead connections:

From MIL-HDBK-217C, Page 2.13-1, the failure rate model for an individual connection is:

 $\lambda_p = \pi_b(\pi_E \times \pi_T \times \pi_0)$ failures/10⁶ hours, where

 λ_b = base failure rate for type of connection π_E = factor for environmental service condition π_T = factor for tool type (manual or automated) π_Q = factor for quality grade employed

From Table 2.13-1, λ_b for the crimp connector is 0.00026 failures/10⁶ hours. Values for the π factors are:

 $\pi E = 3.0$ (Table 2.13-2, for A_{IT}) $\pi T = 2.0$ (Table 2.13-3, for manual) $\pi O = 1.0$ (Table 2.13-4, for manual tools, standard)

Substituting, $\lambda_p = 0.00026(3.0x2.0x1.0) = 0.00156/10^6$

In this cable, there are 102 active pins, so $102 \times 0.00156 = 0.159$ failures/ 10⁶ hours is the rate due to lead connections. Added to the failure rate due to the seven connectors, the predicted failure rate of the cable is:

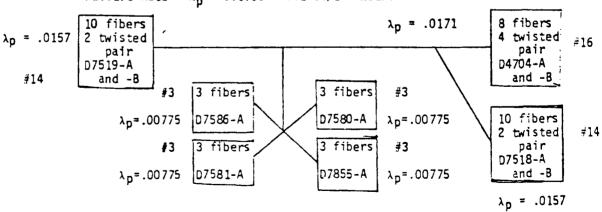
 $^{\lambda}P(\text{connectors}) + ^{\lambda}p(\text{crimps}) = (0.114 + 0.159)/10^{6} \text{ hours}$

= 0.273 failures/10⁶ hours

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Failure rate of the lead wires (approximately 0.003/10⁹ hours) is considered negligible.

3.0 FIBER OPTICS INTERCONNECT SYSTEM RELIABILITY CALCULATIONS



a. Connectors - λ_p = failures/10⁶ hours Failure Rate = λ_p = 0.0795 failures/10⁶ hours 3.0 a. (Continued)

 $\lambda_{p} = \lambda_{b} (\pi_{E} \times \pi_{p} \times \pi_{K}) \text{ failures/10}^{6} \text{ hours}$ $\lambda_{b} = A_{e}^{X}$ where $x = \frac{N_{T}}{T+273} + (\frac{\dot{T}+273}{T_{0}})^{p}$ T = operating temperature

= ambient + temperature rise

Insert material B is chosen, which fixes λ_b as a function of operating temperature. In this case with milliamp current, operating temperature equals ambient (temp rise = 0).

Assuming ambient temperature = $25^{\circ}C$

 $\lambda_b = .00050$

#F (environmental service condition)

Assuming A_{IT} (airborne inhabited transport) πE (Mil-Spec) = 5.0

 π_p = multiplier for number of active pins in a connector

Calculations here are based on the assumption that fiber optic connections behave like regular connections.

Number of Contacts	<u>π</u> ρ	# of Times
3	1.55	4
14	3.14	2
16	3.42	1

(from Table 2.11.1-7.)

 π_{K} = mating/unmating factor

= 2.0 from Table 2.11.1-8.

$$\lambda_{p} = .00050[5.0(2.0 (4x1.55)+(2x3.14)+3.42)]$$

$$\frac{4 \text{ connectors}}{D7580-A} \frac{2 \text{ connectors}}{D7519-A \text{ and } -B} \frac{1 \text{ connector}}{D4704-A \text{ and } -B}$$

$$D7581-A$$

$$D7585-A$$

$$D7586-A$$

$$\lambda_{\rm D} = .0795$$
 total failures/10^b hours

3.0 (Continued)

b. Opto-Electronic Devices $\lambda p = \lambda b = C = E = 0$ failures/10⁵ hours $\lambda_b \approx base failure rate in failures/10^6 hours$ $<math>\pi_C \approx complexity factor (from tables)$ $\pi_E \approx environmental factor (from table)$ $\pi_0 =$ quality factor (from table) #E = selected environment = 2.8 $\pi_0 = 1$ (JANTXV Quality) $\pi_{\rm C}$ = 1.5 for a simple single isolator $\lambda_{\rm h}$ = .0028 for hermetic Assuming S = .5, $T_s = 25^{\circ}C$ T_{max} = 125°C hermetic $\lambda_p = (0.0028)(1.5)(2.8)(1) = .01176$ failures/10⁶ hours c. Lead Connections $\lambda_p = \lambda_b(\pi_E \times \pi_T \times \pi_Q)$ failures/10⁶ hours λ_b = .00026 for crimped wires = .0013 for fiber optic welds $\pi E = environmental factor = 3.0$ Table 2.13-2 πT = tool type factor = 1 for fibers = 2 for wires π_0 = quality factor = 1 for fibers = 1 for wires Total fiber ends = 40Total wire terminations = 16 $\lambda_{\rm p} = 16(.00026)(3)(2)(1) + 40(.0013)(3)(1)(1)$ wires fibers = .02496 + .15600 = .18096 failures/10⁶ d. System Failures = (Lead)+(Connector)+(Opto-Electronic) Failures **a** .18096 + .0795 + .01176 **a** .26046 + .01176

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* 0.27222 failures/10⁶ hours

D180-24693-25

APPENDIX F

FINAL HARNESS ASSEMBLY DESCRIPTION AND TOOLING

D180-24693-25

HARNESS ASSEMBLY DESCRIPTION & TOOLING

O. R. Mulkey

Boeing Aerospace Company P.O. Box 3999 Seattle, WA 98124

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4 June 1980

Final Report for the Period of 16 December 1979 Through 4 June 1980

Phase IV of NOSC Contract NO0123-78-C-0193

Prepared For: Naval Ocean Systems Center Code 9313 San Diego, CA 92152

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS
	BEFORE COMPLETING FORM
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	Final Report
Harness Assembly Description & Tooling	16 Dec 79 - 4 June 80
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1.0 SCOPE

This report covers the details of the assembly procedures, parts, and tooling used in the fabrication of the FO-0004 fiber optics harness as well as those used for the FO-0005 "Single Fiber Harness". The technology for both single fiber and fiber bundle harness is covered for all phases of the assembly. Because the termination and fabrication of conventional wire harnesses is well documented by both the military and industry, details of the processes used in the fabrication of that part of the harnesses not covered.

2.0 REFERENCES

2.1 Introduction

To provide the most flexibility in the use and extraction of the information contained in this report, the technical information and instructions for the various processes are formatted as stand-alone specifications, engineering drawings, and production illustrations. This documentation is then referenced by the "Harness Manufacturing Plan" which details the harness assembly and test. The following documentation therefore forms a part of this report as referenced by the "Harness Manufacturing Plan".

2.2 Data List

CALY

MATERIAL

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	Document No.	<u>"Title"/{Inform</u>	mation Containe	<u>d)</u>		
	180-59000 180-59004	(The top drawi (Harness drawi shop aids pack	ng, form board	drawing, a	also includes	
	180-59004 D180-24693-20 Appendix A Appendix B Appendix C Appendix D	(Single fiber "Preliminary I	harness drawing nstallation Pro identification fabrication) procedures)	cedure, Ha	board drawing) arness General"	
5)	D180-24693-21				es, Fiber Optics and installation	
7)	D180-24693-22 D180-24693-23 D180-24693-26 D180-24693-27	(Maintenance pr (Connector ass		tion)	es and Harnesses"	
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3.0	CONTENTS			
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	2.1 2.2	Introduction Data List		1
	3.0	CONTENTS		2
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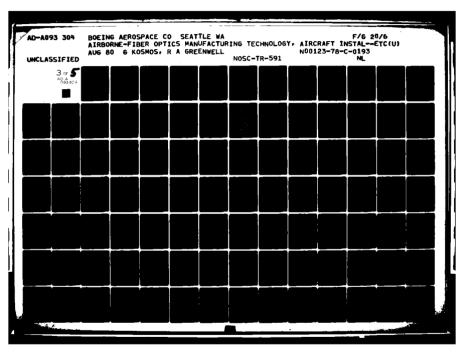
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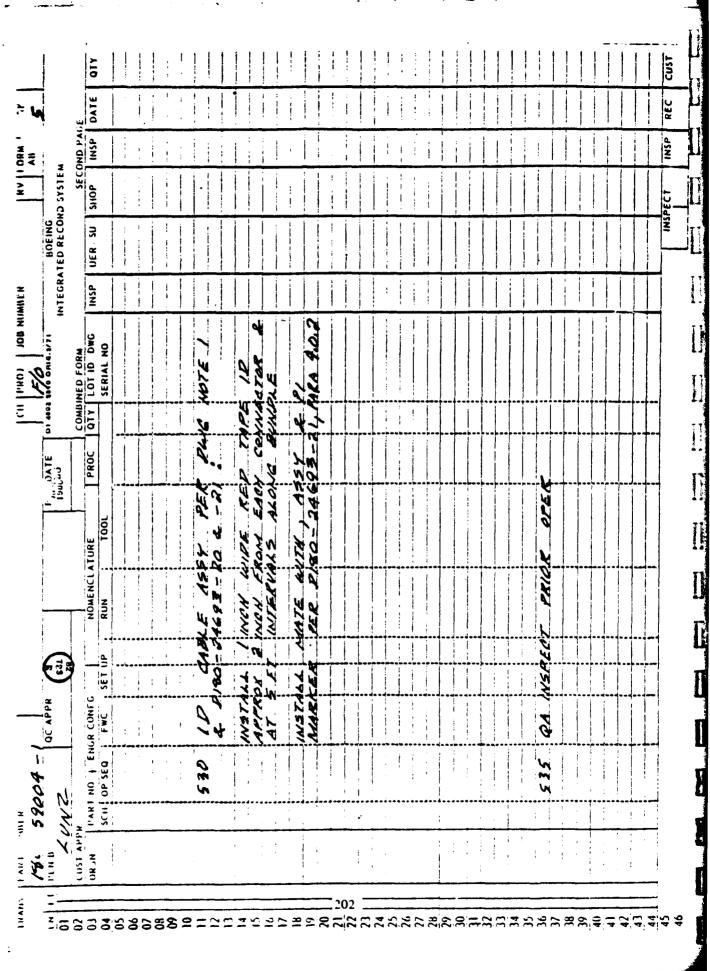
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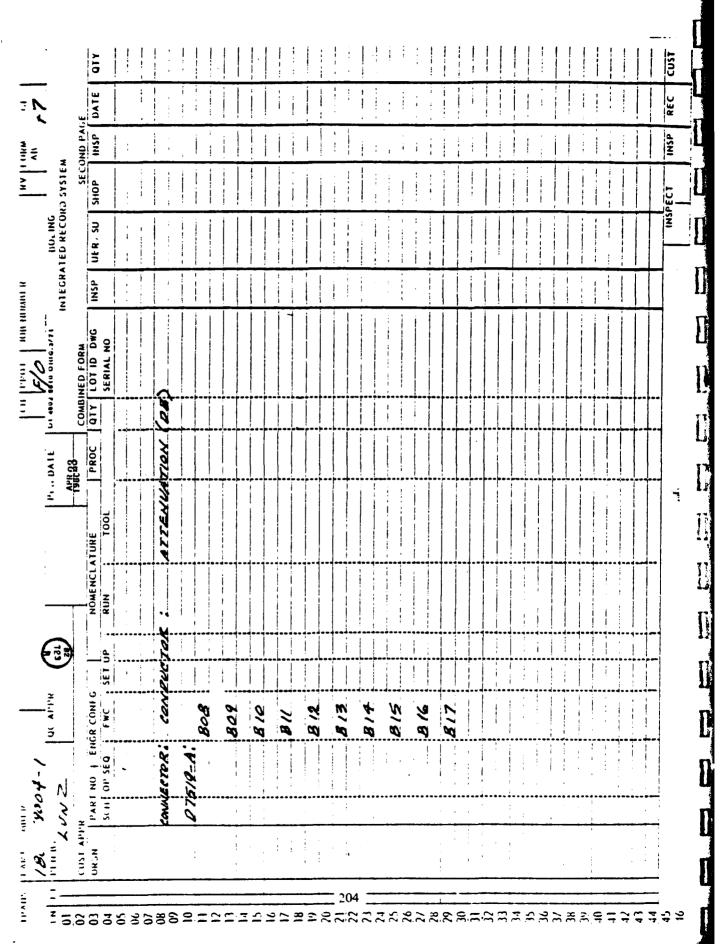
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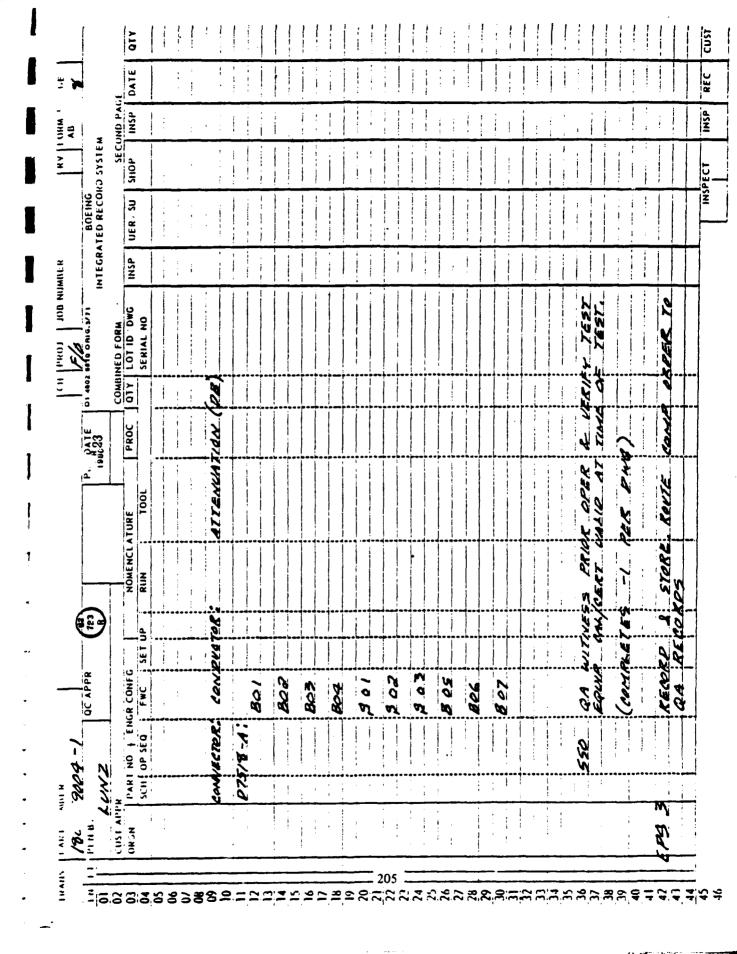
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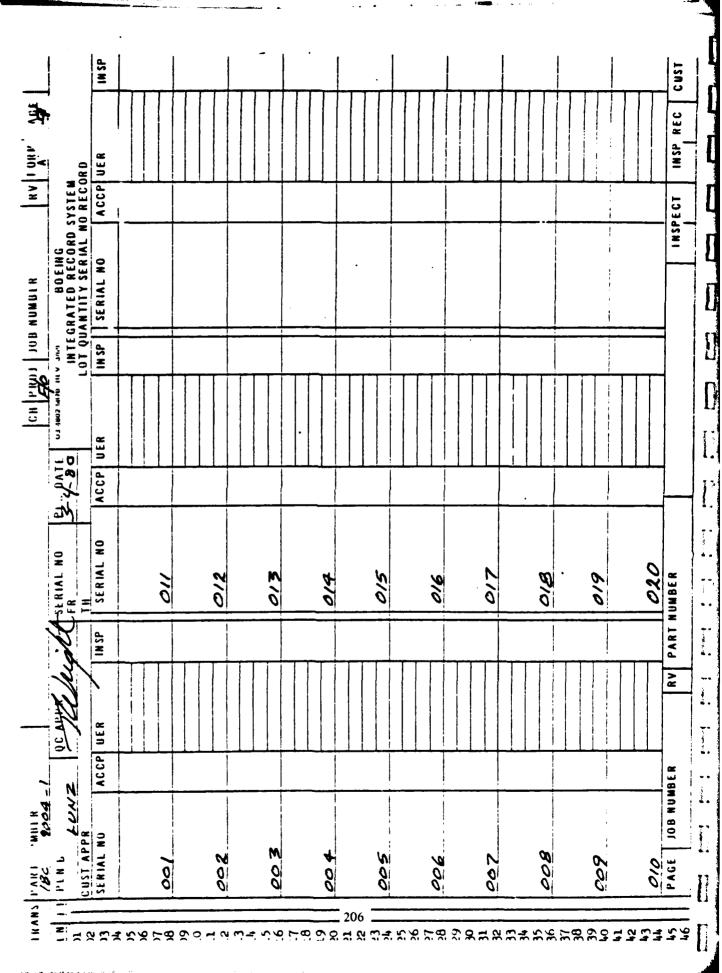
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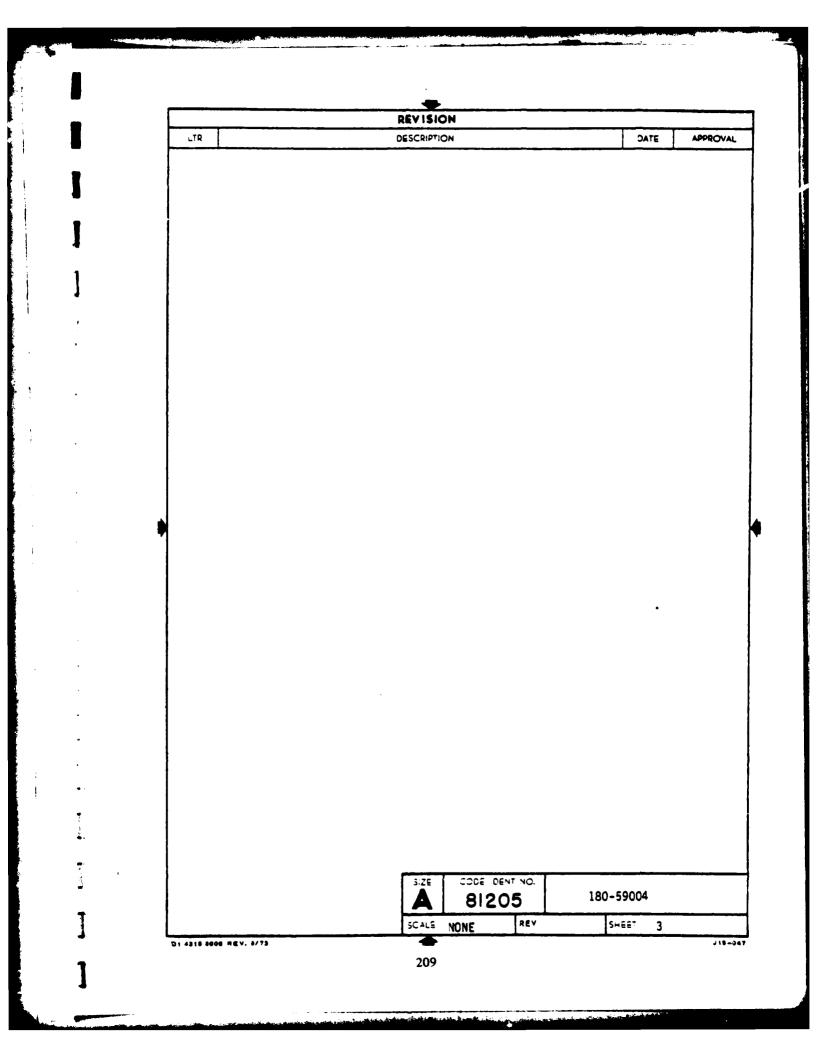
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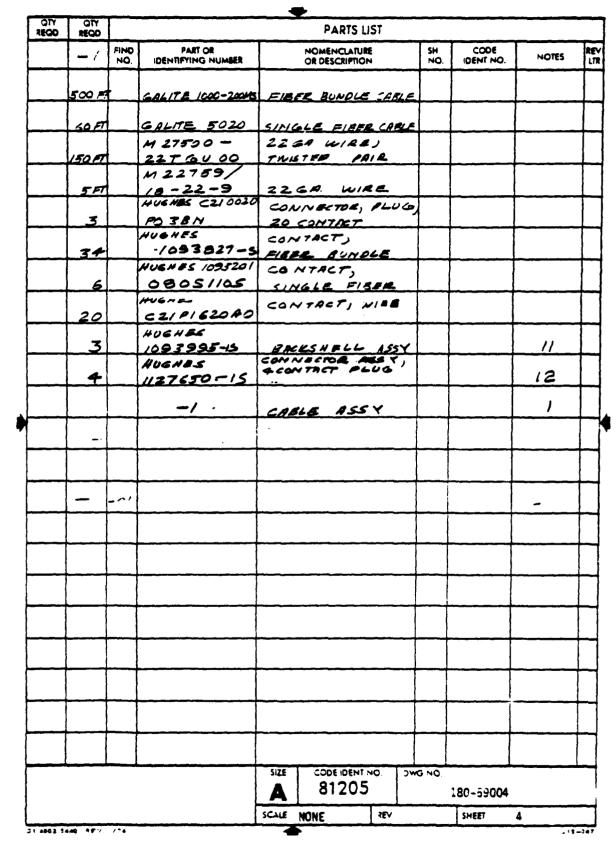
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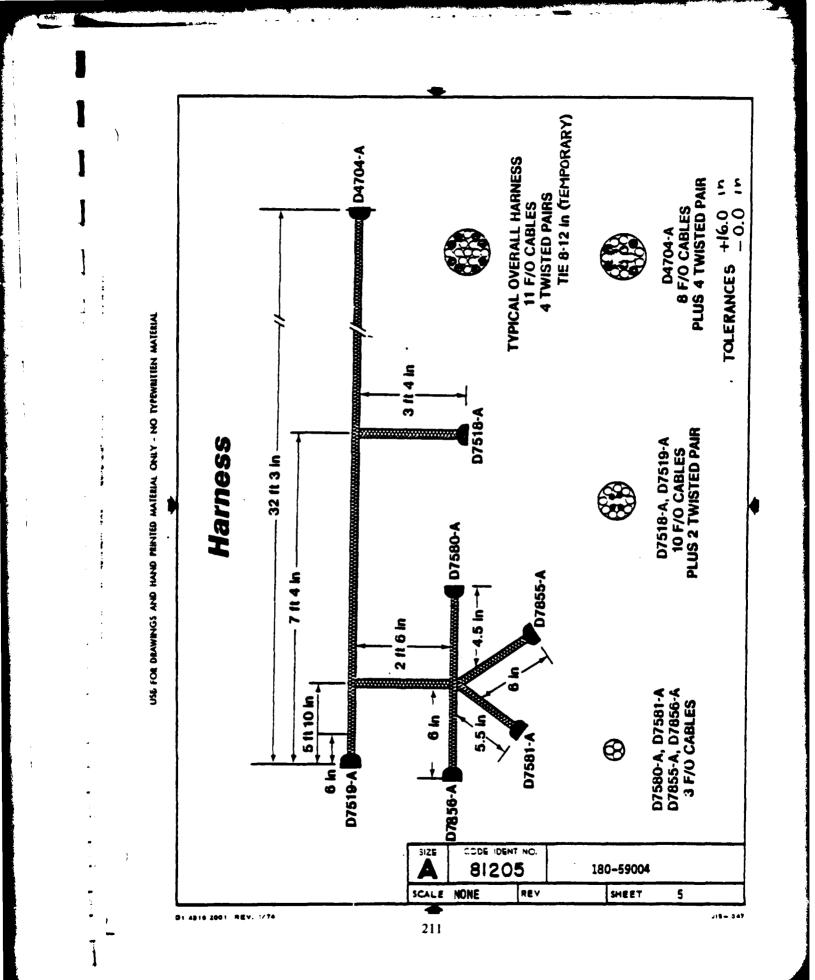
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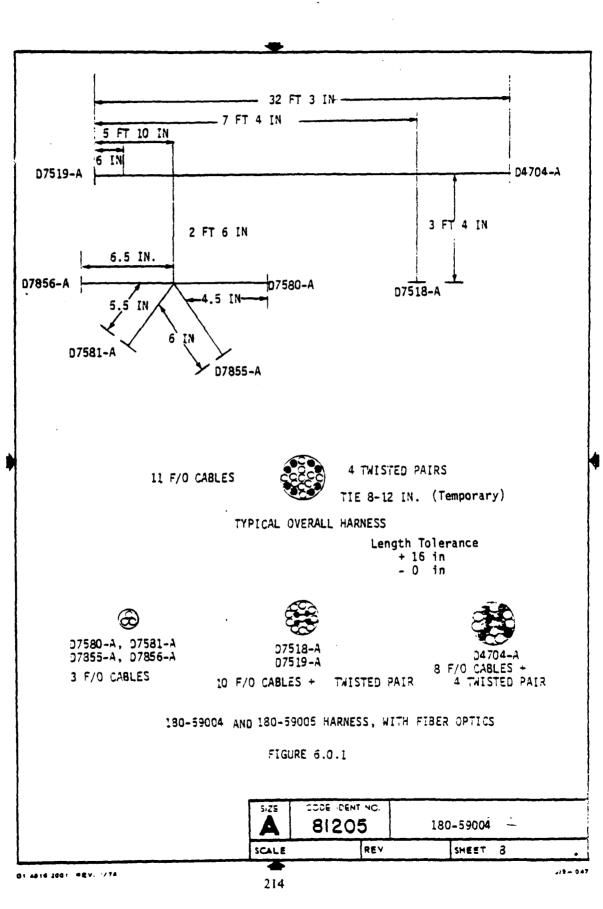
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REVISION LTR DESCRIPTION DATE APPROVAL RECP-OPER HOST-MIC RECP-OPER HDST-MIC RECP-OBSV HOST-MIC RECP-OBSV HDST-MIC PLUG - B169 J1 PLUG - B171 J1 PLUG - E11 MATES WITH MATE WITH DATA 1 CONNECTOR D7518A D7519A D4704PA D7855A D7856A D7856A D7681A 2005 DENT NO. 81205 SIZE 180-59004 SHEET 8 A NONE 21 4315 6006 ORIG. 3/71 215

	HARNESS ASSEMBLY NOTES						
1)	Install one-inch-wide red tape on bundle near each connector and at $5' \pm 3'$ intervals along bundle and identify per D180-24693-20 and -21.						
2)	Terminate cables per D180-24693-27.						
3)	Assemble connectors per D180-24693-26.						
4)	Repair harness per D180-24693-23.						
5)	Test per 0180-24693-22. Tool BCX 230969 may be used for photographs. See 0180-25451-2 TEST LIMITS						
	Single Fiber Channel 3dB (50%) maximum below single fiber reference cable 10 meters long. Terminated using identical contacts and cable.						
	Fiber Bundle Channel 3dB (50%) maximum below fiber bundle reference cable 10 meters long terminated using identical contacts and cable plus .01dB/inch allowance or decrease for length difference (Note 10M = 394 in.). Broken fiber limit - 15% or 35 fibers maximum (170 good fibers are acceptable).						
6)	Braid outer jacket (white nomex) per 204-10900~1.						
7)	Lay out harness using form board drawing FB180-59004-1 and -2.						
	VISUAL INSPECTION CRITERIA						
	Surface Finish Fiber ends shall appear smooth and flat and free of major scratches, chips or epoxy smears. Small imperfections that do not degrade the insertion loss below test limits are acceptable (Insertion loss test may be done out of sequence for this verification) for crimped terminations inspect per DI80-24693-27 Par. 6.3.						
8)	Crimp 22 6A wire using tool called in D180-24693-27.1 strip wire .25 to .30 inch using 22 ga Stripmaster tool.						
9)	All cable ends may be cut and terminated 6 inches longer than the drawing dimensions so that if broken they may be reused in another harness.						
10)	No Cal Cert is required on crimp, insertion and removal tools.						
11)	Hughes 1093995-15, 25, 35 and 45 are identical and may be used interchangeably.						
12)	Hughes 1127650 1S-4S are identical and may be used interchangeably.						
13)	Anodization scrapes or slight deformation of the crimp on the crimp sleeves and ferrules is acceptable.						
14)	Seal plugs not required on connectors on the 1st 21 units.						
	SIZE CODE IDENT. NO.						
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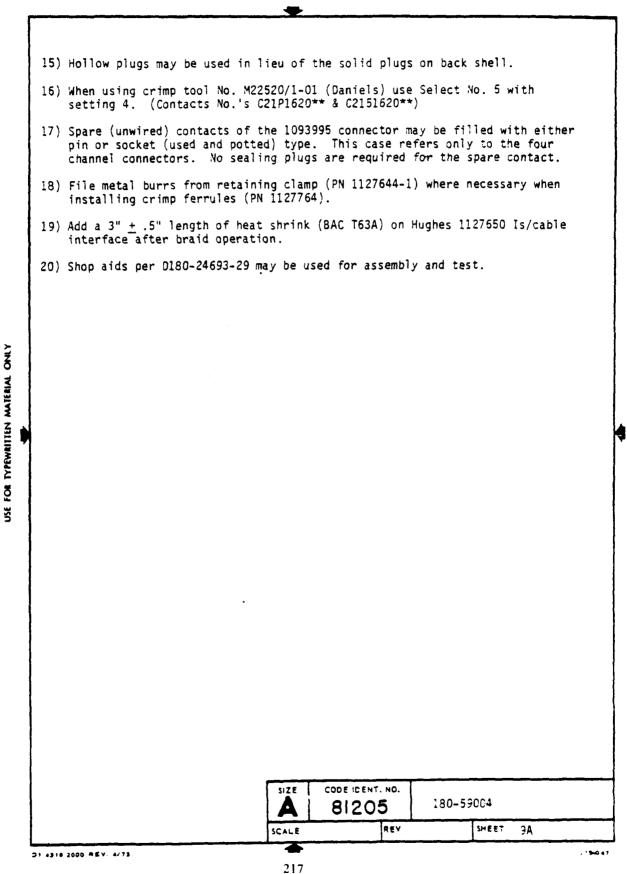
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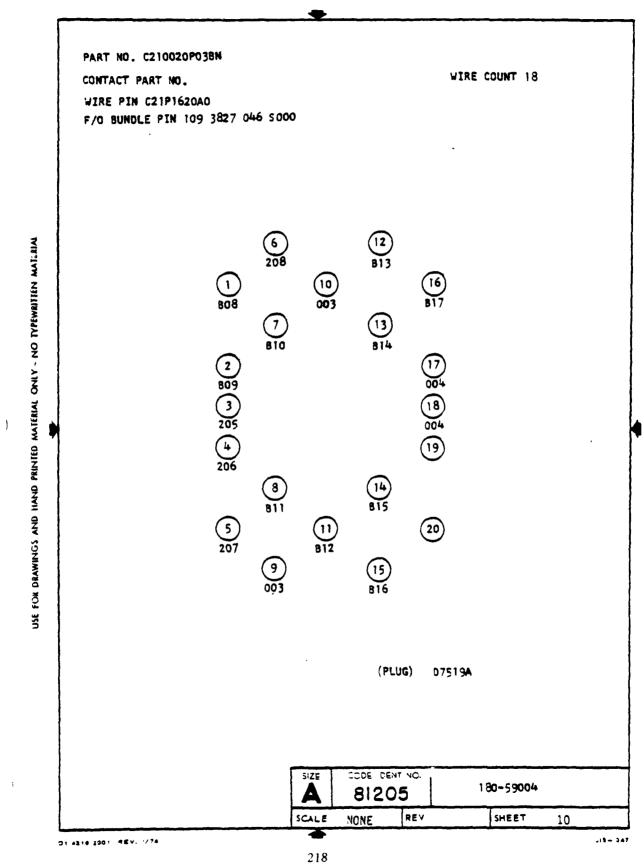
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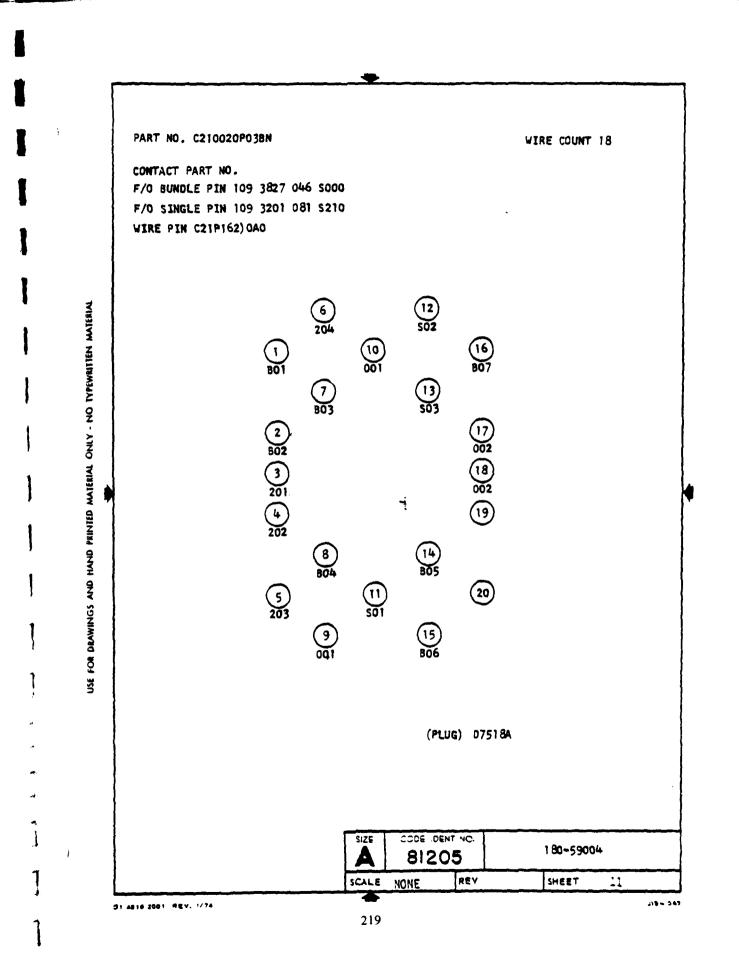




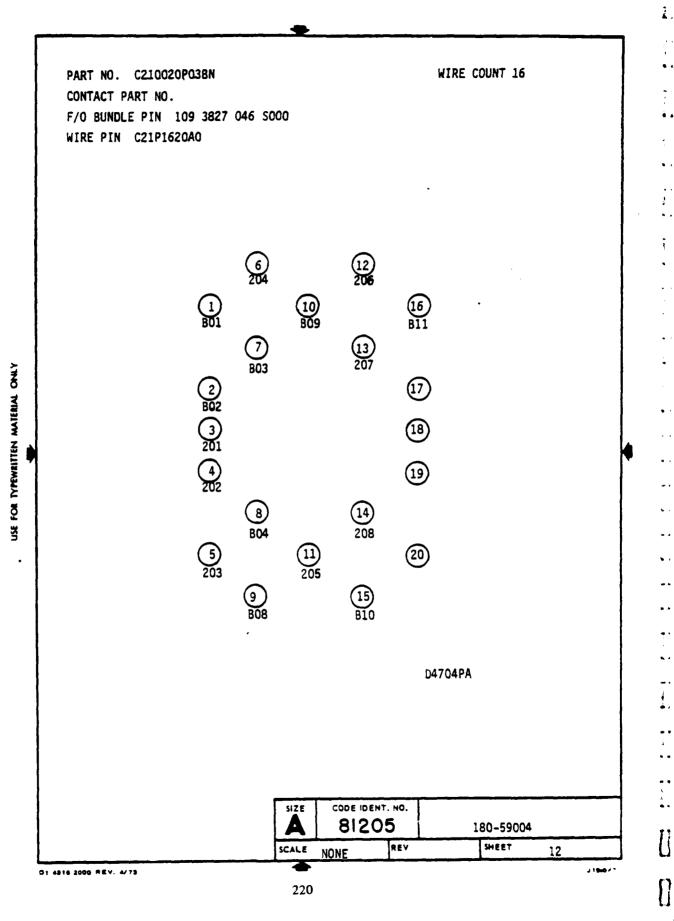
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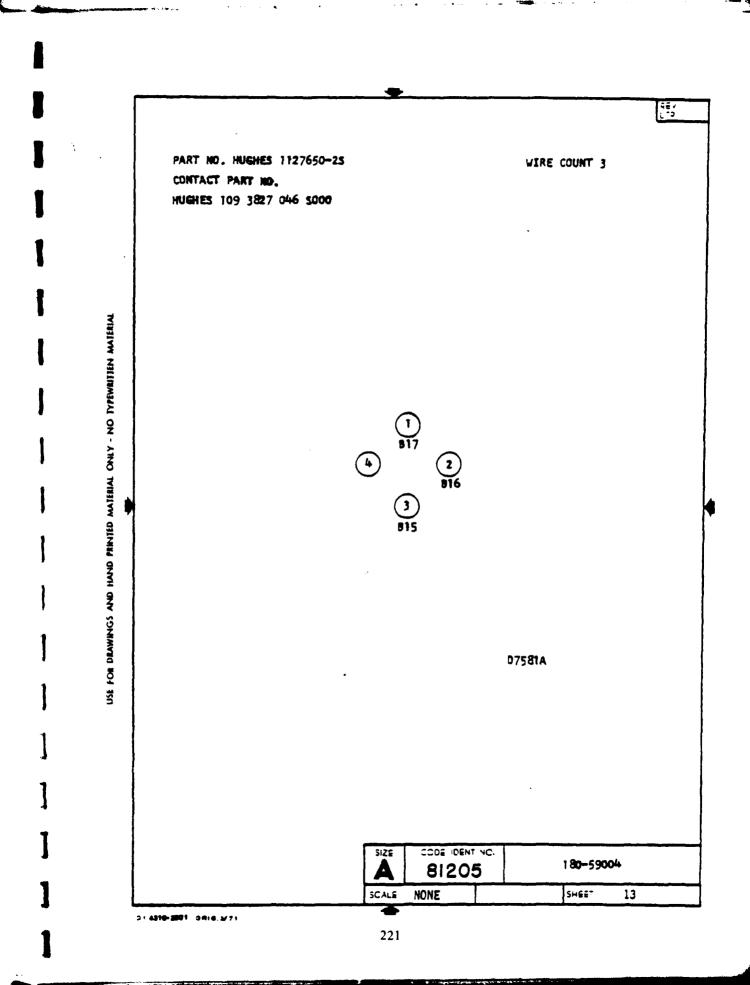
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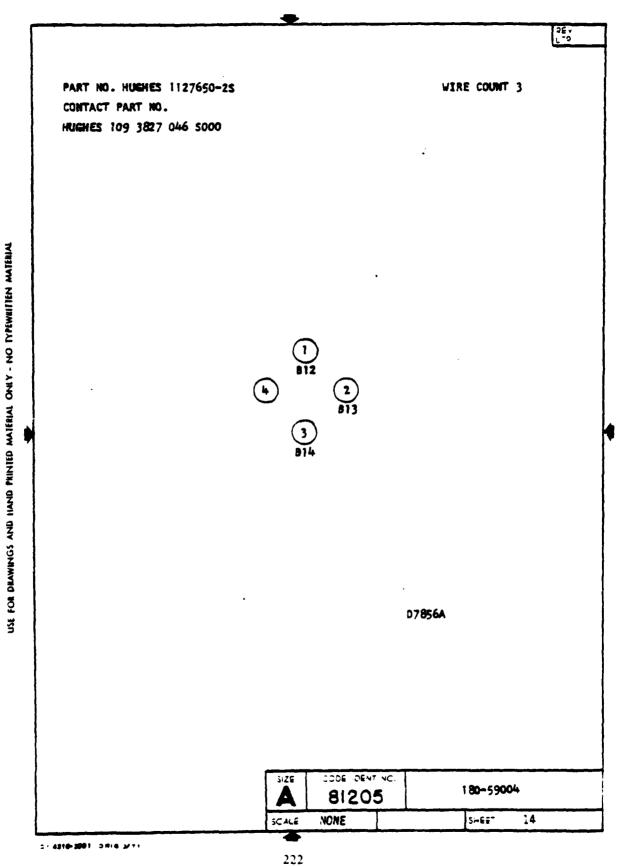


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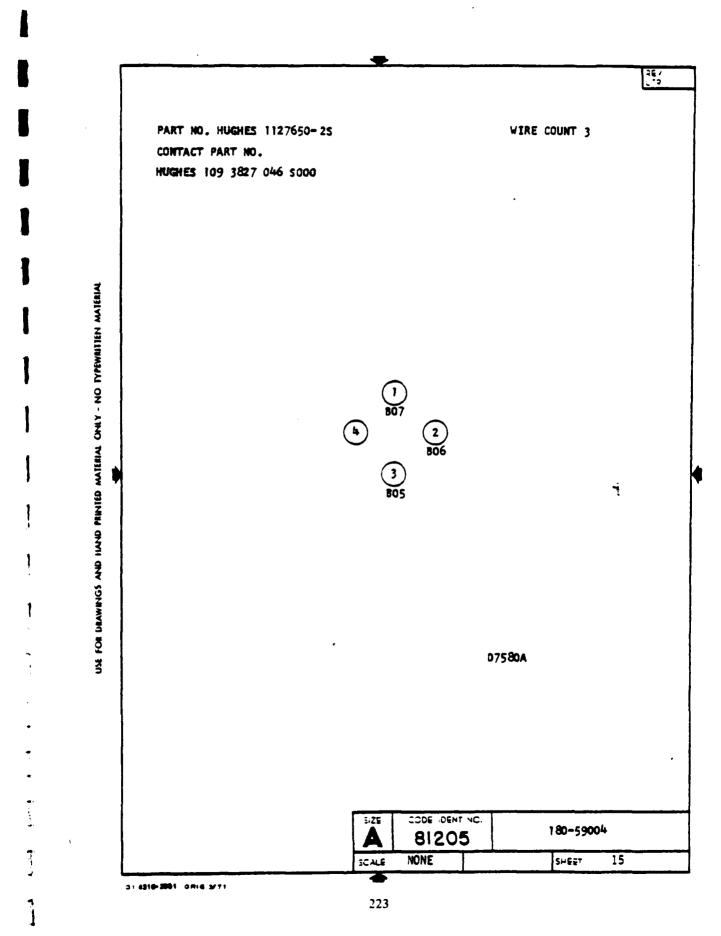
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D180-24693-26

APPENDIX G

FIBER OPTIC ASSEMBLY PROCEDURE, GENERAL

D180-24693-26

FIBER OPTIC CONNECTOR ASSEMBLY PROCEDURE, GENERAL

0. R. Mulkey

Boeing Aerospace Company P.J. Box 3999 Seattle, Washington 98124

4 June 1980

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Final Report for Period 15 December 1979 through 4 June 1980 Phase IV of NOSC Contract N00123-78-C-0193

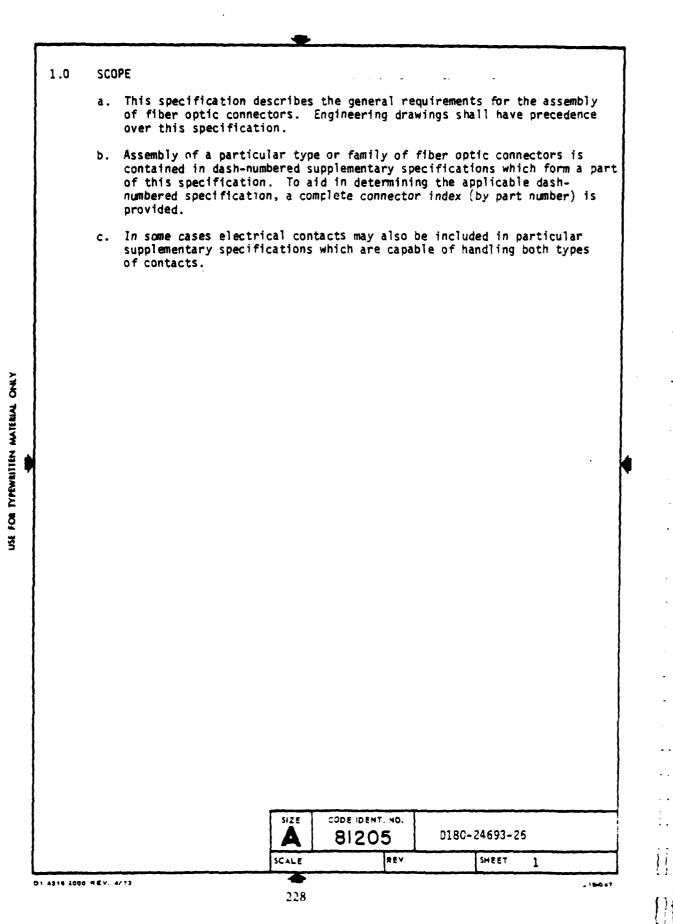
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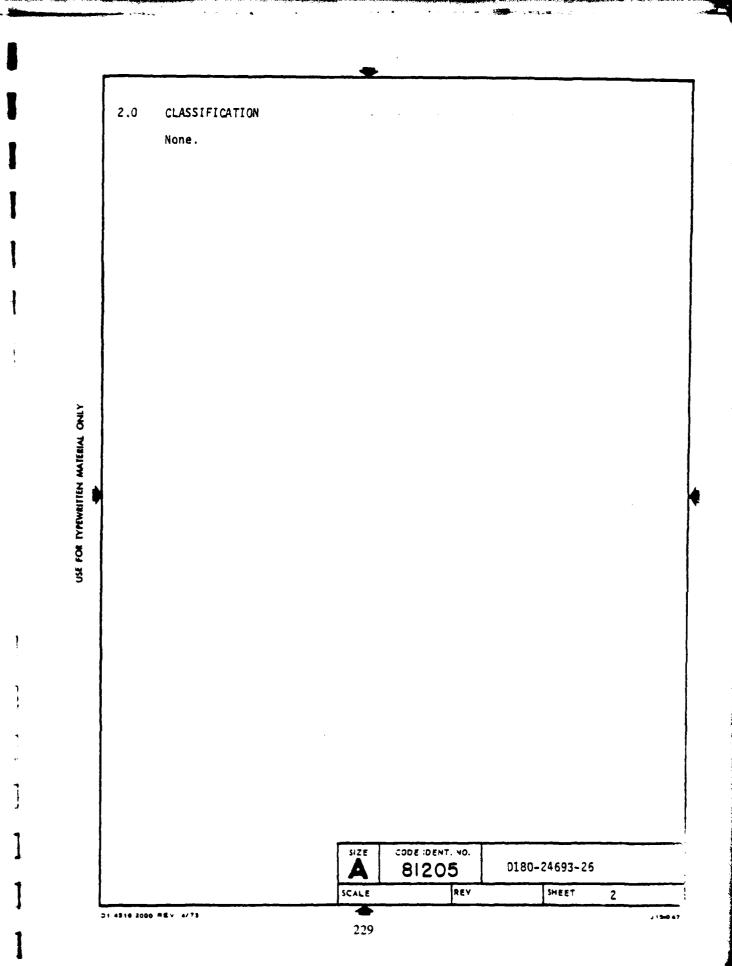
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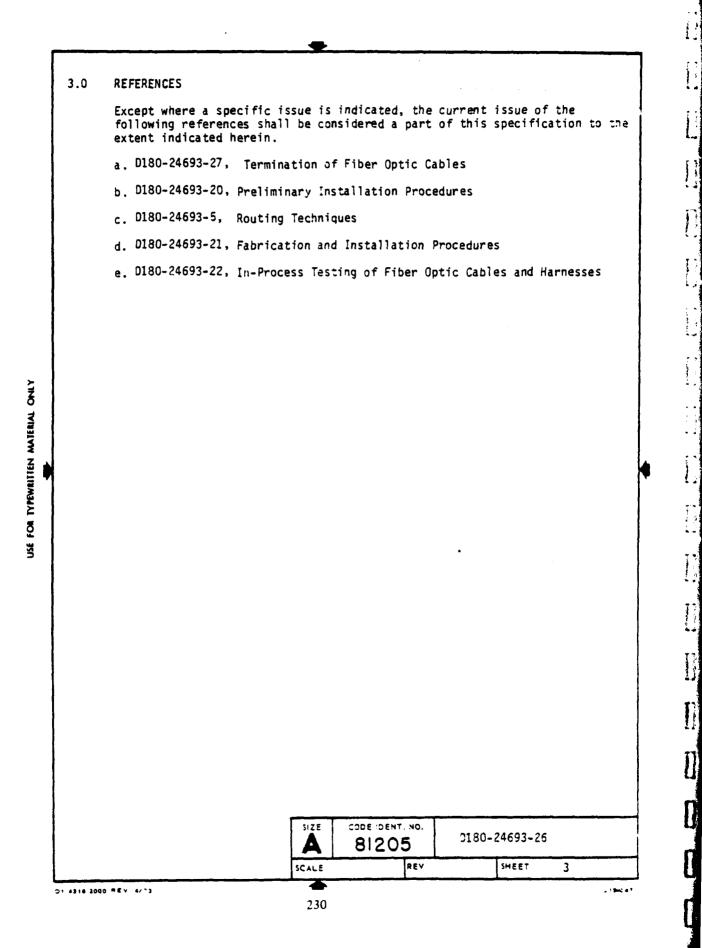
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	5.0	MATERIALS CONTROL						
	6.0	DEFINITIONS						
	7.0	MANUFACTURING CONTROL						
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			(b)	E-775-303 Dodge Indus	tries,	Inc.				
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- (1) Alcohol isopropyl
- (2) Cleaning, naphtha, aliphatic in accordance with Specification TT-N-95
- g. Strip

Plastic, vinyl, transparent, flexible (material same as for sleeving in accordance with MIL-I-7444), 0.020 ± 0.0015 inch thick, width as required (tolerance + 5 percent) in 1/4 inch increments.

CT-93 The Borden Chemical Div., Borden, Inc.

h. Tape

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- (1) Insulation, electrical pressure sensitive, black, plastic for low temperature applications in accordance with HH-I-595.
- (2) Electrical, nonpressure sensitive, Mylar, MIL-I-631, Type G, Form T, Grade A, Class I, Category 1, one inch width.
 - E. I. duPont deNemours and Co., Inc.
- i. Insulation Sleeving
 - (1) Electrical, flexible, Type I in accordance with MIL-I-7444
 - (2) Fiber glass, silicone rubber-covered, fungus resistant treated, color brown or white, Class H-B-1 (200C, 4000V minimum average dielectric strength) meeting performance requirements of MIL-I-3190 in standard sizes as required.
 - (a) "Turbo 117" Brand-Rex Division, American Enka Corp.
 - (b) Class H-B-1, Type SR-9 Varflex Corp.
- j. Rod, grommet sealing Polytetrafluoroethylene in accordance with AMS 3651, sizes as required.
- k. Strip

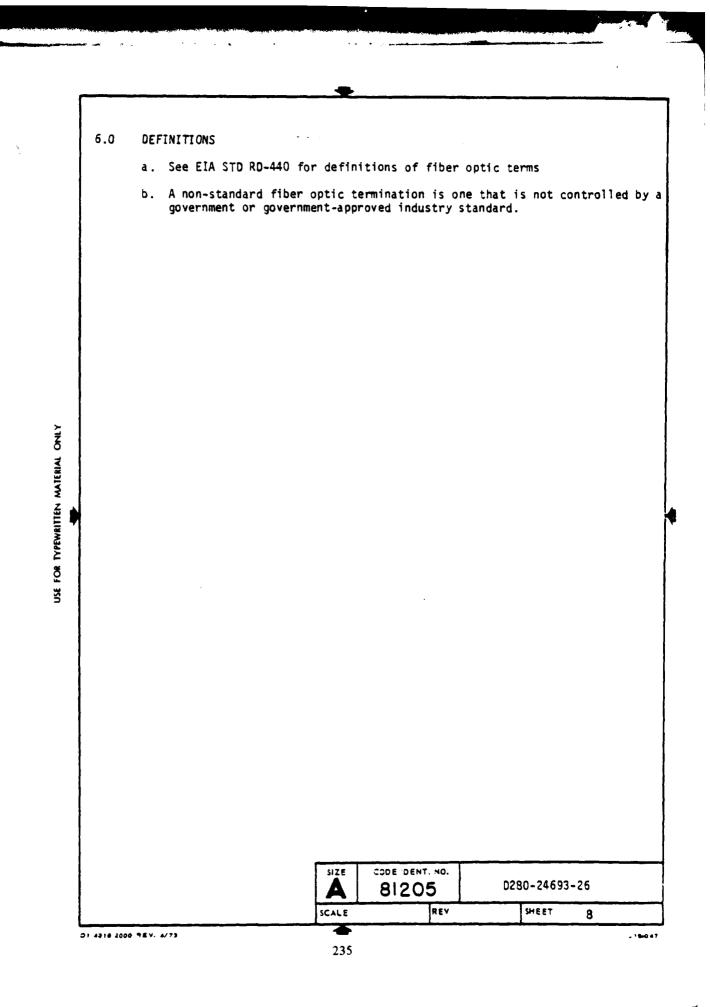
Plastic, polyvinyl chloride, black opaque, non-rigid, Type F, Form T, Grade a, Class 1, Category 1, in accordance with MIL-I-631, 0.020 inch + 0.0015 inch thick, width as required (tolerance \pm 5 percent) in 1/4 inch increments.

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7.0	MAN	UFACTURING CONTROL
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7.1		IRONMENTAL CONTROL
	a.	Processes described herein shall be performed in an area meeting the requirements of Fed STD 209.
	b.	Activity restrictions - the following operating practices shall be observed.
		(1) No paint spraying shall be performed in the area.
		(2) All personnel assembling, inspecting handling, or otherwise touching those surfaces of cable assembly parts to be potted, molded, or encapsulated shall wear gloves to prevent contamination of the surfaces after they are cleaned. Cable assembly parts include bare conductors, connector contacts, terminals, splices, connectors, and primed or etched surfaces.
		The gloves shall be made of rubber or a synthetic fiber of a quality which sheds a minimum amount of lint. Cotton gloves shall not be used. Finger cots may be used in lieu of gloves when handling small parts which will not contact the bare palm or uncovered parts of the fingers. The gloves or cots shall be replaced sufficiently often (at least once per shift) to ensure cleanliness and no transfer of perspiration, grease, oil, or other contaminants to the parts.
		CAUTION: The presence of silicone in hair preparations, cosmetics, and other products presents a serious source of contamina- tion. Gloves must be replaced at any time they come in contact with such contamination.
	с.	Remote Sites - When assembly drawings require the assembly of electric connectors to cable after the cable has been pulled through conduit at remote sites, environmental requirements as stated above, with the exception of 7.1b(3), may be waived. Precautions shall be taken to protect the assemblies from dust, rain, internal-combustion engine exhaust, or other environmental contaminants which may affect the serviceability of the completed assembly.
		SIZE CODE DENT. NO. D180-24693-26
		A 81205 0180-24693-26

7.2	Operator Qualification						
	Personnel involved in the assembly of connectors to cables shall satisfy following minimum requirements:						
	a. Be familiar with the general requirements of this specification.						
	b. Be capable of identifying tools required for stripping cables and assembling connectors.						
	c. Be trained in the use of tools and processes described in this specification.						
7.3	Tool Requirements						
	a. The following tools must be certified in accordance for use in the processes of this specification.						
	(1) Mechanical stripping tools.						
	(2) Crimp tools.						
	(3) Metal contact insertion tools.						
	(4) Metal contact removal tools.						
	b. No certification is required for the following tools:						
	(1) Expander barrel tools.						
	(2) Tapered lead tools.						
	(3) Plastic contact insertion tools.						
	(4) Plastic contact removal tools.						
7.4	Cable Stripping and Cable Jacket Removal						
	Perform stripping and cable jacket removal in accordance with D180-24693- termination.						
7.5	Crimping						
	Perform crimping operations in accordance with D180-24693-27 termination.						

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7.6	Spa	re Cable Stubs	~ -	· · ·	• • • • • • • • •		
	a.	Protect the ends of secure them within c			ng with heat shrink and le bundle.		
	b.	tors to be potted si	all be fill ch predomina	ed with spare ca ates in the bund	y contacts in all connec ble stubs. Make the stu les and of the sizes that		
	c.		essive stub		or at least seven inches nector 1_{2}^{3} inches longer		
	d.	Identify each spare cable size as shown			or contact letter and th		
		Identification		Explan	ation		
		A-16 SMALL A-10			Cable Size 16 Cable Size 10		
	e.		and running	g through a comm	which are attached to on group or bundle, shou de a part of their		
]		Cable	Connector	Identi	fication Marking		
		A-8 A-8	P72 J8		A-8-P72 A-8-J8		
f. Spare cable stubs which will eventually be used in a circuit identified with a sleeve. The sleeve shall be marked with th number of the cable to which it will be spliced and applied a D180-24693-20 Appendix A.							
	g.		gable with	an identificati	ut the cable according t on sleeve in accordance in place.		
	h.		two ties be		of the spare cable stub tor and the end of the		
7.7	Connector and Cable Protection						
7.7.1	Handling						
	a.	minimum to reduce th	e possibili	ty of connector	carefully and held to a or cable damage. Partic contain both connector a		
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7.7.1 (Continued)

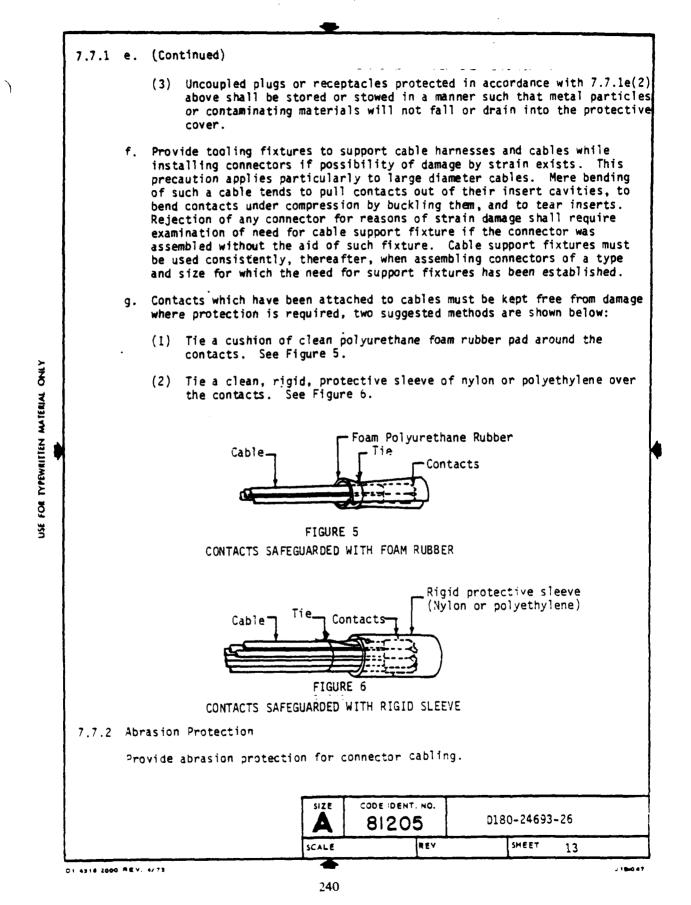
- b. Unassembled connectors and contacts shall be handled as follows:
 - Except as necessary, do not open connector and contact containers until the time of assembly.
 - (2) They shall be guarded against contamination and must be returned to the original container as soon as practicable.
- c. Uncoupled plugs and receptacles of production cables, and test cables which mate with production cables, are to be protected with metal or plastic dust caps. Metallic dust caps shall mate with the connector coupling devices. Plastic dust caps shall fit snugly over the coupling ring of plug connectors and over the mating end of receptacle connectors. Plastic bags may be used to protect connectors which standard type metallic or plastic dust caps do not fit. The open end of the plastic bag shall be closed and secured in place.
- d. Polyethylene (or equivalent) bags shall be used to individually cover unpotted plugs and receptacles against contamination. These bags shall be secured in place by closing and fastening the open ends with tying cord, elastic bands, or tape. Do not allow tape adhesive to contact cable or contacts.
- e. The protective requirements are as follows:
 - (1) Dust caps according to 7.7.1c above shall be provided on all uncoupled ends of plugs and receptacles except when necessary to work directly upon them. Where this is not feasible during potting or molding operations, connector ends may be protected by masking with tape, Permacel 2650 or Permacel 29. Tape adhesive shall not touch connector contacts, insert face or contact surfaces. Replace tape with plastic cap after potting and molding operations are complete.
 - (2) In addition, a protective cover in accordance with 7.7.1d above shall be provided on all unsealed plugs and receptacles (unpotted or without sealing grommet), whether coupled or uncoupled, under the following conditions.
 - (a) When located in an area where the plug and receptacles may be exposed to falling or flying metal particles from operations such as drilling, filing, chipping, soldering, cleaning, etc.
 - (b) When located in an area where the plug and receptacle may be contaminated by foreign matter such as water, dirt, oil, grease, carbon, etc.
 - (c) When transported through an area where the plug and receptacle may be exposed to metal particles or contamination as described in e(2)(a) and (b).

NOTE: For the purposes of this specification, the use of bags shall be held to a minimum consistent with the protective require-

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7.	.7	.3	Stra	iin	Rel	ief

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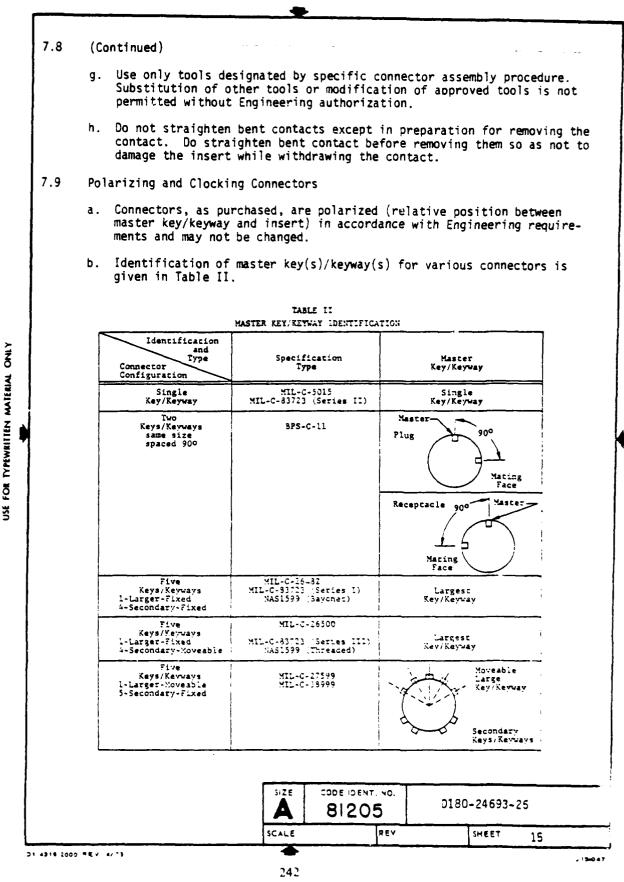
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- a. Provide all connectors with adapter clamps when specified on the Engineering drawings.
- b. Form individual cables to provide natural strain relief for the connector terminations when the adapter clamp is tightened.
- c. Use caution in dressing cables so that contact float is not destroyed. Exercise special care in providing strain relief for contact where resilient inserts are used to prevent the contacts from being pulled out of alignment.
- d. Where necessary to build up jacketed cable diameter to fit connector adapter clamp, wrap the jacket with plastic strip (4 n.) or tape (4 o.). For cables in areas specified on the Engineering drawing as being high temperature use only tape (4 o.). Use the narrowest practicable strip or tape centered under the adapter clamp extending a minimum of 1/16 inch on both sides of the clamp.

The plastic strip may be held in place by heat sealing to itself. When the adapter clamp is tightened, the cable insulation shall not be cut or crushed and the cable(s) to connector shall show no apparent stress. The adapter clamp shall be bottomed only when gripping ground braid terminals and only on the side containing pigtail terminations.

- 7.8 Insertion and Removal of Contacts
 - a. Carefully insert the contact into the appropriate insert cavity required by the Engineering drawing and push on the tool handle until the contact is seated. Refer to connector and insert arrangement standards or drawings for correct cavity identification.
 - b. If an unterminated contact cannot be removed from the grommet by hand, a pair of pliers may be used to extract it. Any contact removed with the pliers must be discarded if dented or marred to the extent that the base metal is exposed.
 - CAUTION: Pins and sockets must be driven straight to avoid bending them or damaging the insert.
 - c. Do not use contact insertion and removal tools for any function other than inserting and removing contacts.
 - d. Protect tool tips with suitable guards when they are not being used.
 - e. Do not use tools which show visible defects to the extent that grommets, inserts, contacts, or taper pins may be damaged.
 - f. Align the contact and tool with the contact cavity and do not rotate the contact or tool during insertion or removal to avoid the possibility of bending the contact or damaging the insert.

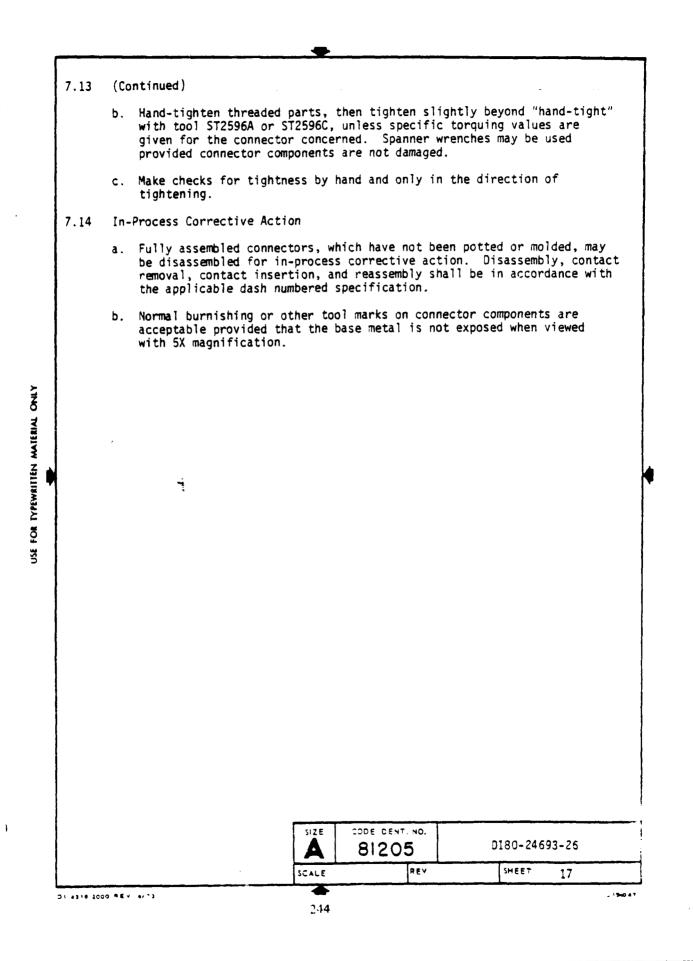
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7.9	(Co	ontinued)			-
	c.	Clock angle accessor otherwise specified, (30 degrees). See Fi	the allo	rding to the Engine owable clocking tol	ering drawings. Unles: erance is <u>+</u> 1 hour
		11, 10, 9,		Master Key of	
		8 7		4 with refer numerals.	ke-off" downward rence to clock
			FIGURE	clocked at	ngle type receptacle t l'oclock.
7.10	Con		ICAL CLC W OF ANG	OCKING BLE TYPE CONNECTOR)	
	Per	form tests on cabling	with con	nectors in accorda	nce with D180-24693-8.
7.11	Con	nector Potting			
	a.	Abrade all Teflon-ins paper before terminat			grit aluminum oxide
	Ь.	Apply primer to cable contacts.	es and co	nnectors after term	minating cables to
	c.	Pot the connector and Engineering drawings.		using potting comp	oound called out on
	d.	Do not use insulating	sleeves	on potted connecto	or terminations.
	e.	Sleeves, or wrapping potting material unle			ct into or from the
7.12	Ins	tallation of Connector	S		
	See	D180-24693-20.			
7.13	Thr	eaded Components			
	a.	Avoid excessive tight parts.	ening wh	ich might damage th	nreads or connector
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use	lity Control shall ensure that only the materials specified nerein are ad and that the procedures covered are observed with particular note to e following points:
a.	Damaged cable jacketing which will not meet specification requirements and connectors with contaminated inserts (paint, adhesives, grease, carbon, metal chips, etc.) or with bent or corroded contacts are unacceptable.
b.	Prior to attachment of the backshells or potting of connectors, visual inspection shall be made for the following:
	(1) Damage to inserts, contacts.
	(2) Quality of crimped terminations.
	(3) Proper seating of removable-type contacts.
	(4) Proper application of sleeves when required.
	(5) Clean inserts and contacts.
c.	Check the tightness of connector fittings only in the direction of tightening.
d.	Quality Control shall ensure compliance with the environmental control requirements of this specification.
e.	Quality Control shall verify that only properly certified employees are performing or operating operations such as terminating, potting or other processes which are designated as "critical" by Operating Procedures.
f.	Quality Control shall verify that all cable assemblies are tested in accordance with D180-24693-22.
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APPENDIX H

FIBER OPTIC CONNECTOR ASSEMBLY PROCEDURE, HUGHES

D180-24693-26.1

FIBER OPTIC CONNECTOR ASSEMBLY PROCEDURE

- HUGHES CONNECTORS -

O. R. Mulkey

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Boeing Aerospace Company P.O. Box 3999 Seattle, WA 98124

15 June 1980

Final Report for the Period of 16 December 1979 Through 15 June 1980 Phase IV of NOSC Contract N00123-78-C-0193

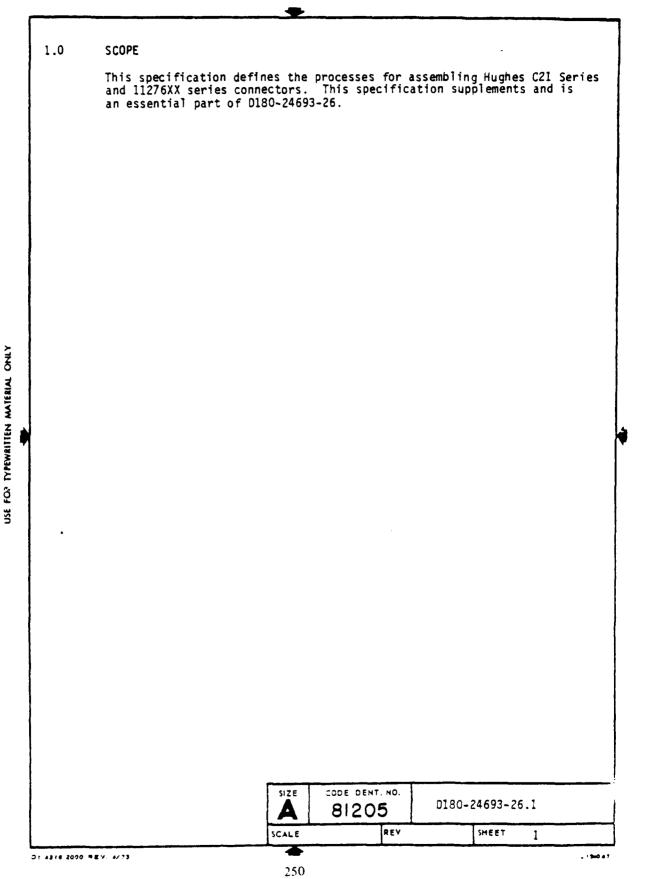
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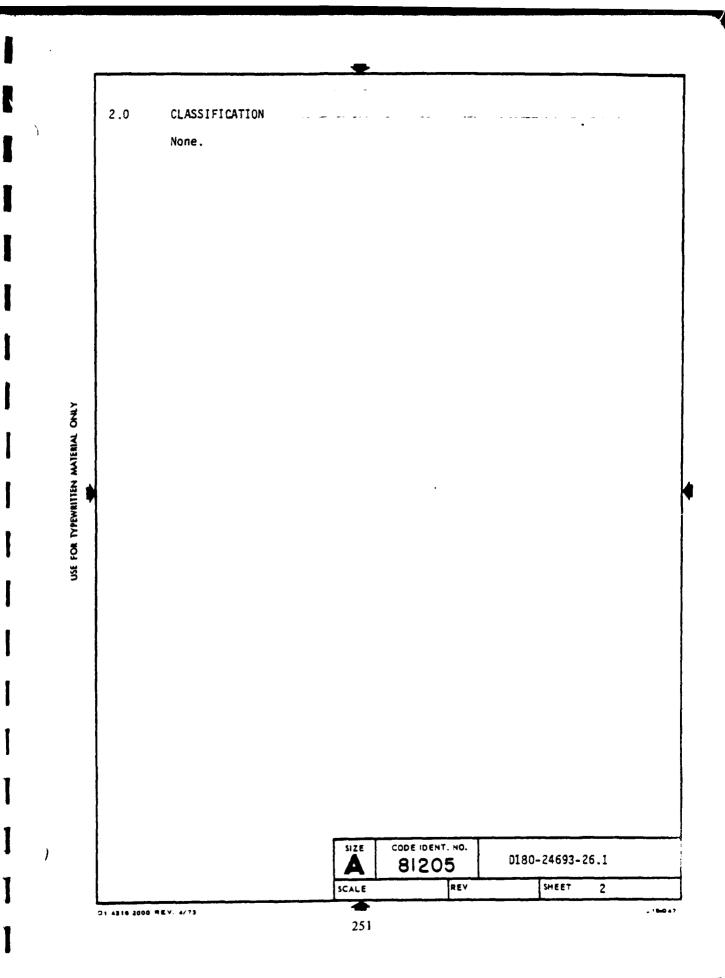
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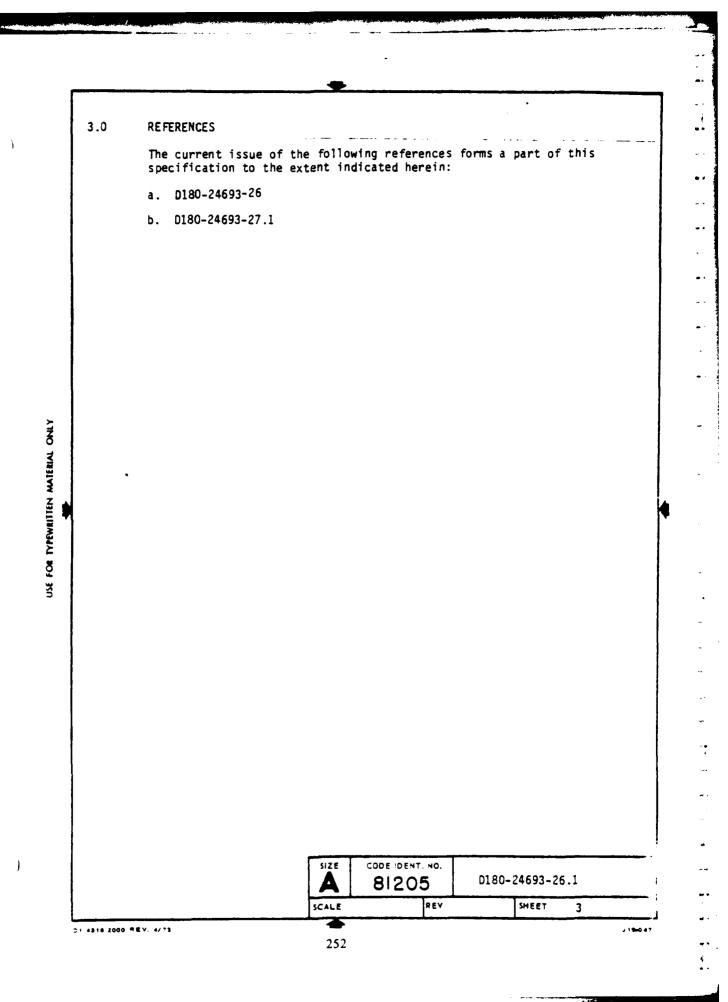
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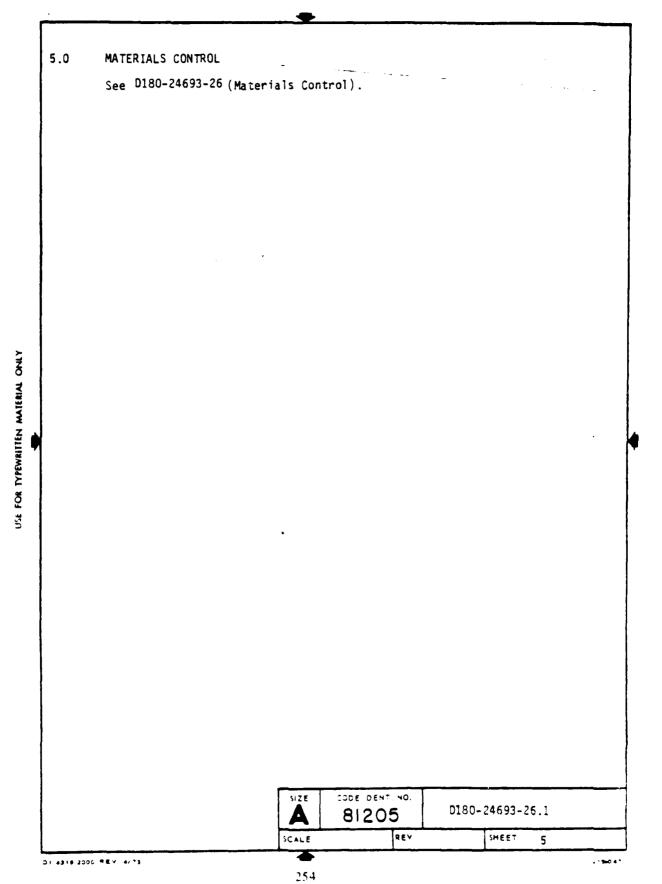
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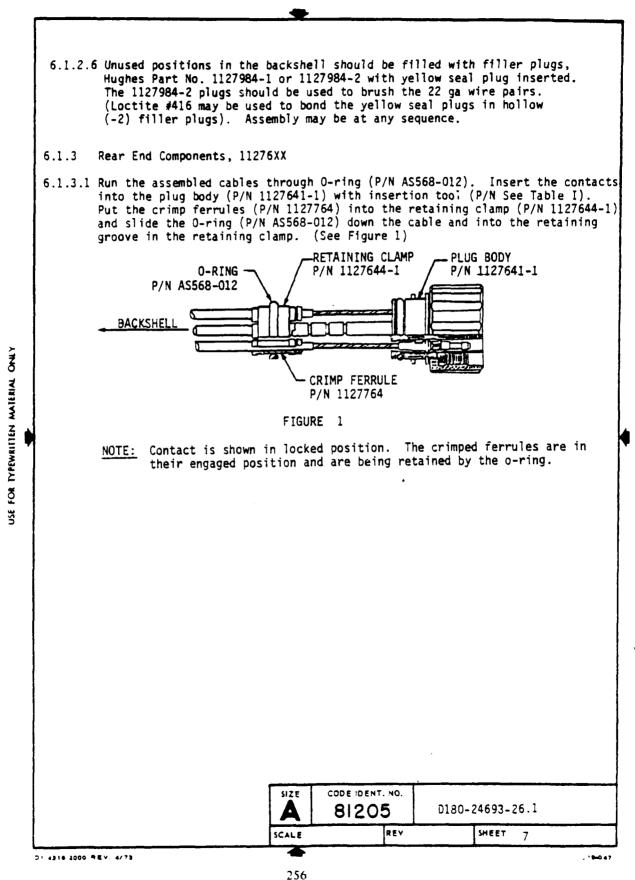
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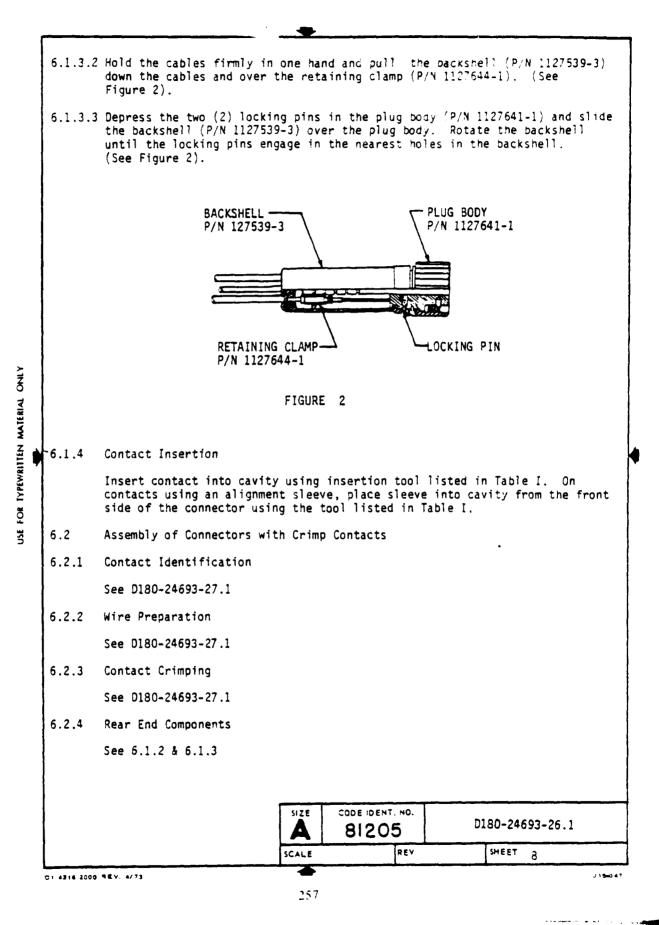
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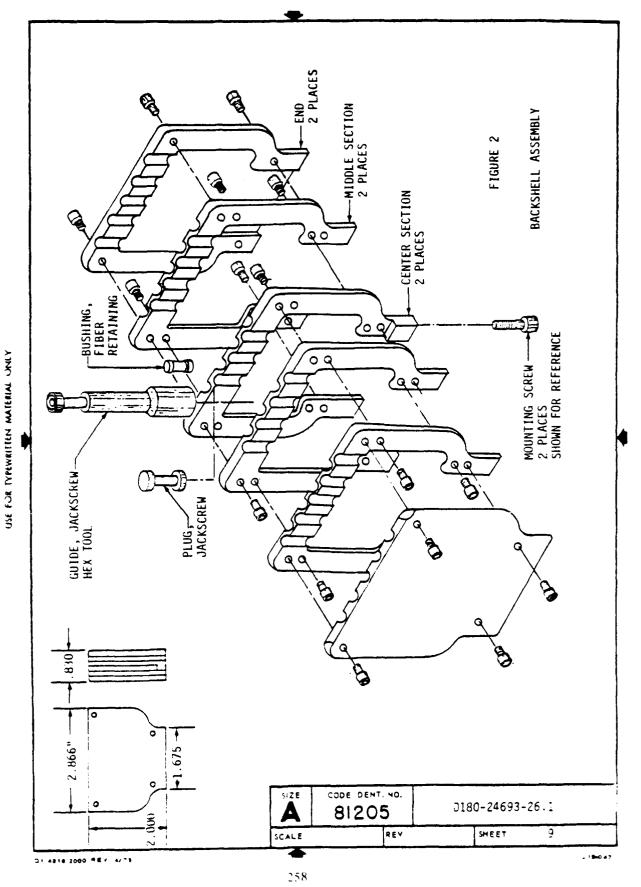
	care is exercised to avoid overtightening, or damage to connector or finish. Unless otherwise specified, threaded parts of connectors herein shall be tighted by hand, and then slightly beyond hand tight with tool ST2596C or equivalent (avoid damage to connector
	or finish). c. The sequence of operations presented herein is intended only as a guid and may be modified to facilitate connector assembly.
6.1	Assembly of Connectors with Fiber Optic Contacts
	See D180-24693-27.1.
	Assure that backshell sleeve is crimped at end of outer jacket.
6.1.2	Rear End Components, C-21
	The backshell assembly is assembled as illustrated in Figure 3 from the center section out. The jackscrew guide is used on the plug half of the connector pair, the jackscrew plug on the receptacle half.
6.1.2.1	Fasten a Backshell Center Section (P/N 1127188) to a C-21 Pin Body (P/N 1093827) or to a C-21 Socket Body (P/N 1035904) with Fillister Head Machine Screws.
6.1.2.2	Insert two pin or socket assemblies as appropriate into the applicable connector cavity with the right angle contact (P/N 114304S) provided.
6.1.2.3	The Hex Tool Guide (P/N 1127270) or the Plug (P/N 1127271) is positioned on the center section, depending upon which connector half is being assembled. The second Backshell Center Section (P/N 1127188) is placed to retain the ferrules and the Hex Tool Guide or plug and fastened into position with a Fillister Head Machine Screw and four Socket Head Capscrews.
6.1.2.4	Four pin or socket assemblies as applicable are inserted into each side of the Backshell Center Section, one side at a time, and a Backshell Middle Section (P/N 1127005) is attached to the sides with four Socket Head Capscrews, respectively.
6.1.2.5	Five pin or socket assemblies, as applicable, are now inserted into each side adjacent to the middle sections, one side at a time, and retained with a Backshell End Section (P/N 1127000) and four Socket Head Capscrews.

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COMMECTORS, CONTACTS, AND INSERTION AND REMOVAL TOOLS COMMECTORS, CONTACTS, AND INSERTION AND REMOVAL TOOLS Connector Part Assembly Pragmaph Contact Contact Fart Number Tool 61 10337043-2 Tool 63 10337043-2 Current Receptache 6.1 16 Collact Gontact Part Number Tool 64 111 Tool 64 101 Tool 64 101 Tool 64 101 Tool 64 10337043-2 Tool 64 103370						TABLE I			
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1143046 (Crimp Sleeve) Special TM16RT006 (Silver) TM16RT006 (Silver) TM16RT006 (Green) TM16RT006 (Green) TM]6RT006 (Green) TM16RT006 (Silver) Tools Removal CONNECTORS, CONTACTS, AND INSERTION AND REMOVAL TOOLS Insertion TK0161PP01 **TK0161PS01** 10937845 1093784S 1093784S 10937845 (Continued) 10932010815210 F.O. Single Fiber (Pin) Part No.'s 127539-3, 1127641-1, 1127644-1, A5568-012, 1127764 are part of the connector assy. 10938280465000 F.O. Bundle (Socket) Contact Part Number 10938270465000 F.O. Bundle (Pin) TABLE I 10932020815210 C21S1620A0 Wire (Socket) C21P1620A0 Wire (Pin) Contact Size 16 16 16 16 Assembly Paragraph 6.1 N/A 6.1 6.1 6.1 Connector Part (Plug Assy.) 1127650-35 1 1127668S (Receptacle) Number CODE DENT. NO. 81205 size A D180-24693-26.1 SCALE REY SHEET 101 -----01 4314 2000 REV. 4/73

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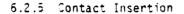
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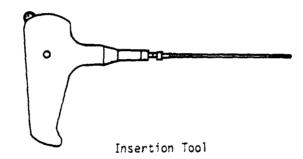
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a. Insert the Hugnes Pull-Thru Insertion Tool into the contact cavity at the mating face of the connector until the tip protrudes from the rear of the connector, free of the wire bundle. Next, insert the contact 'into the tip of the tool. Pull the locking lever on the tool back with the thumb to lock the contact into the tool. Carefully draw the tool back through the connector block until the contact retention clip locks into place with a click. Then push the contact forward to insure that contact is locked in the connector. When locked, release the contact from the tool by pushing the thumb locking lever forward. Withdraw the tool carefully and repeat the operation until all contacts are seated.



- 5. Check for the proper seating of each contact by grasping one wire between the thumb and forefinger of one hand and pulling slowly, in line with the contact, without jerking, until the thumb and forefinger slip on the wire.
- c. Fill all unused contact cavities with spare (unwired) contacts, in accordance with 6.2.5a and 6.2.5b, followed by seal plugs selected from Table II. Insert seal plugs (small end first) until plug butts against back of contact, or shoulder on seal plug bottoms on seal plug bottoms on rear grommet face.

		SEAL PLU	GS		
	Contact		Seal Plug		
	Size	Color	Eau	ivalent Part No.	
	20 15 12	Red Blue Yellow		NAS1668-1 NAS1668-2 NAS1668-3	
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TABLE II

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6.3	In-Process Corrective Action
	Should it become necessary to remove contacts from connectors which have no been potted or molded, disassemble rear end components, slide them back on cable, and proceed as follows:
	CAUTION: Maintain axial alignment of tool with contact cavity and avoid rotating removal tool any time tool is within contact cavity.
6.3.1	Wired Contact Removal
	a. Insert removal tool selected from Table I into the contact cavity.
	NOTE: Remove alignment sleeve first, if present.
	b. Push until contact releases.
	c. Remove contact from rear of connector.
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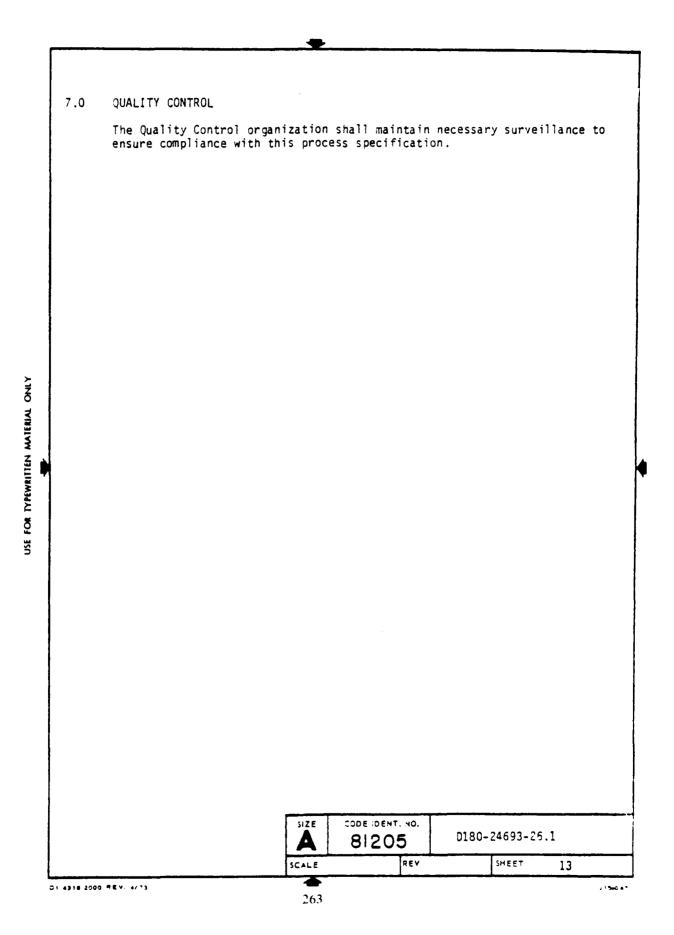
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APPENDIX I

FIBER OPTIC CONNECTOR ASSEMBLY PROCEDURE, AMPHENOL

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FIBER OPTIC CONNECTOR ASSEMBLY PROCEDURE

- AMPHENOL CONNECTORS -

O. R. Mulkey

Boeing Aerospace Company P.Q. Box 3999 Seattle, WA 98124

15 June 1980

Final Report for the Period of 16 December 1979 Through 15 June 1980 Phase II of NOSC Contract N00123-78-C-0193

> Prepared For: Naval Ocean Systems Center Code 9313 San Diego, CA 92152

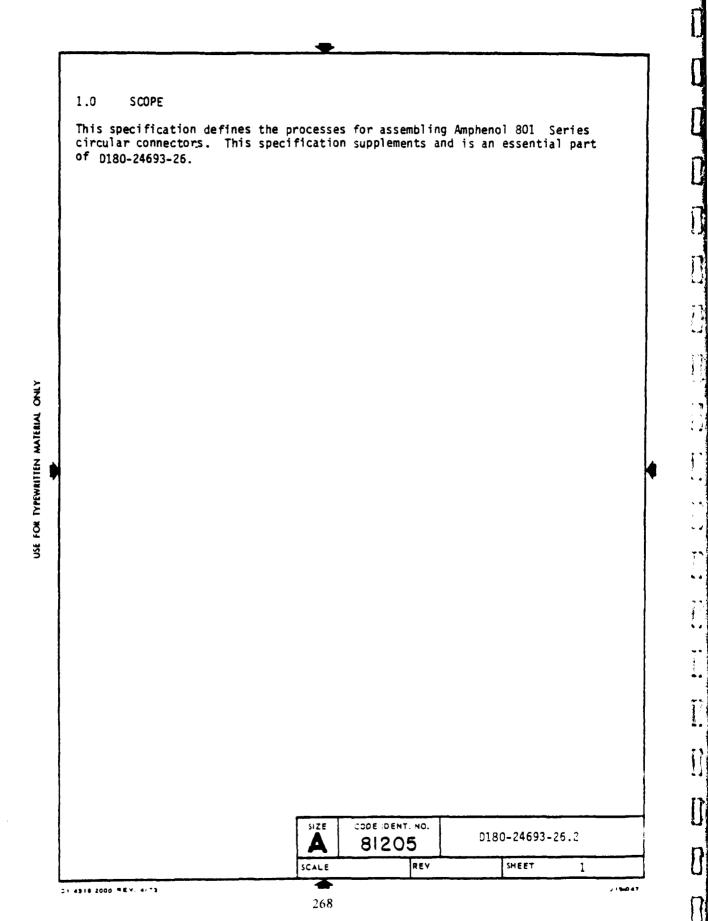
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Fiber optic harnesses	
Fiber optic cables	
Fiber optic connectors	
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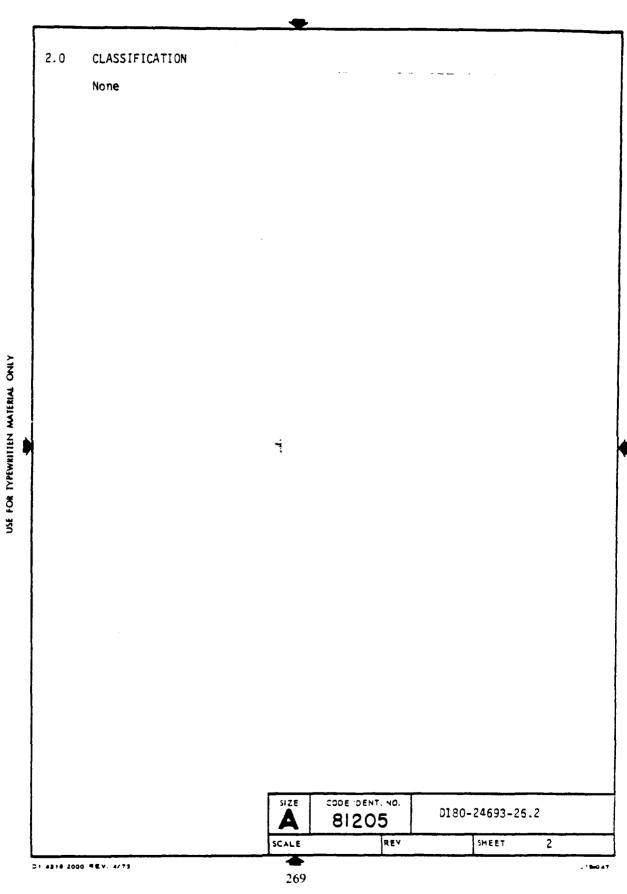
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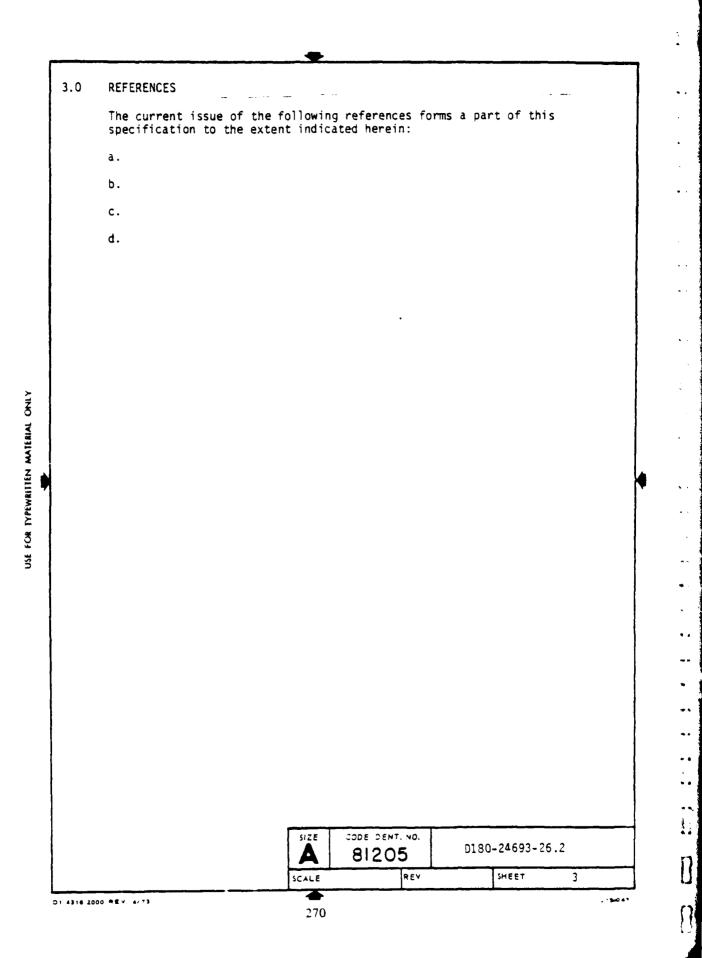


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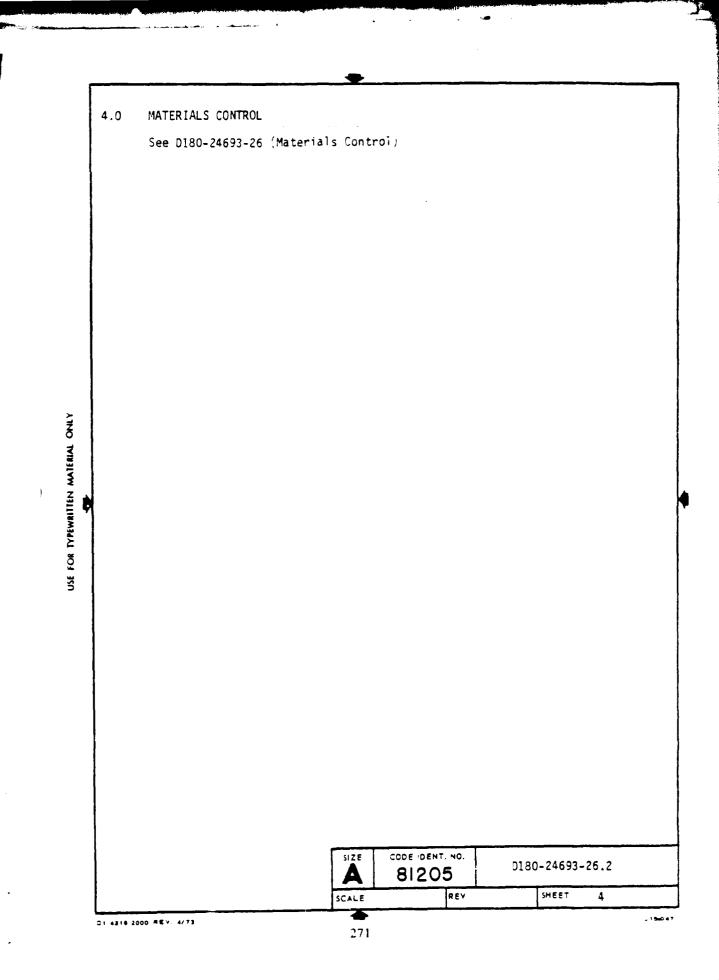
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	CONNECTOR	RS CONTAC	TABLE : TS AND INS		REMOVAL	. TOOLS		
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801-104-5208 Receptacle	6.2	12	M39029/4 Pin (Wi		227-90 Yellow end	9-2018 White end		
801-104-5004 Receptacle	6.1	12	801-999- Pin (F.		fellow end	White end		
801-105-5208 Plug	6.2	12	M39029/5 Socket	-12-12 (Wire)	227-90 (ellow end			
01-105-5004 Receptacle	6.1	12	801-999- Socket		ellow end	White end		
801-5030 Backshell							<u> </u>	
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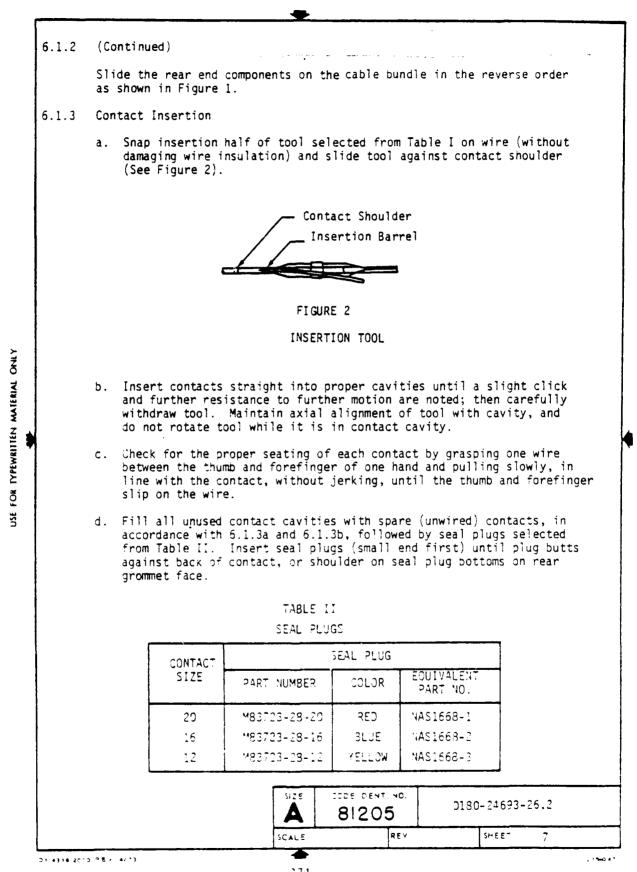
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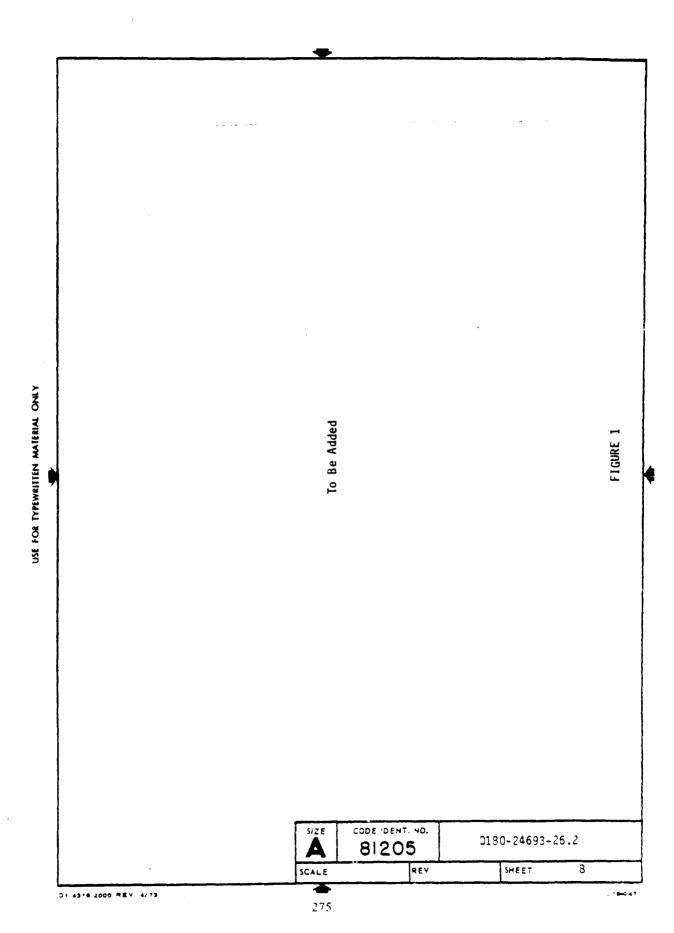
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6.1.4	Backshell (Rear End Components) Assembly
	Assemble backshell components.
6.2	Assembly of Connectors With Crimp Contacts
6.2.1	Contact Identification
	Crimp contacts for the various connectors covered herein are shown in Table I.
6.2.2	Wire Preparation
	Remove cable jacket as required for backshell assembly. Strip wire insulation in accordance with standard procedure.
6.2.3	Contact Crimping
	Crimp contacts on wire in accordance with standard procedure.
6.2.4	Rear End Components
	Rear end components (backshells) are supplied as part of the connectors herein.
	Slide the rear end components on the wire bundle in the reverse order as shown in the appropriate table.
ó.2.5	Contact Insertion
	a. Snap insertion half of tool selected from Table I on wire (without damaging wire insulation), and slide tool against contact shoulder (see Figure 2).
	b. Insert contacts straight into proper cavities until a slight click and further resistance to further motion are noted; then carefully withdraw tool. Maintain axial alignment of tool with cavity, and do not rotate tool while it is in contact cavity.
	c. Check for the proper seating of each contact by grasping one cable between the thumb and forefinger of one hand and pulling slowly, in line with the contact, without jerking, until the thumb and forefinger slip on the cable.
	d. Fill all unused contact cavities with spare (unterminated) contacts, accordance with 6.2.5a and 6.2.5b., followed by seal plugs selected from Table II. Insert seal plugs (small end first) until plug butts against back of contact, or shoulder on seal plug bottoms on rear grommet face.
5.2.5	Backshell (Rear End Components' Assembly
	Assemble backshell components.
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6.3	.n-	-Process Corrective Action
	not	build it become necessary to remove contacts from connectors which have t been potted or molded, disassemble rear end components, slide them ck on cable, and proceed as follows:
	CAL	JTION: Maintain axial alignment of tool with contact cavity and avoid rotating removal tool any time tool is within contact cavity.
6.3.1	Ter	minated Contact Removal
	a.	Sn ap remov al half of tool selected from Table I on cable (without damaging jacket).
	ь.	Carefully slide tool straight into rear of contact cavity and over rear of contact until tool bottoms.
	c.	Hold cable against serrations on tool and pull both tool and terminat contact straight out of contact cavity.
6.3.2	Unt	erminated Contact Removal
	a.	Manually remove seal plug.
	b.	Carefully push unterminated contact removal tool (selected from Table straight into rear of contact cavity, and over rear of contact until bottomed. Apply no pressure to plunger of tool.
	c.	Pull both tool and unterminated contact out of contact cavity.
	d.	Depress plunger to free unterminated contact from tool.
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7.0	QUALITY CONTROL
	The Quality Control organization shall maintain necessary surveillance to ensure compliance with this process specification.
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APPENDIX J

FIBER OPTIC TERMINATION PROCEDURE, GENERAL

D180-24693-27

FIBER OPTIC TERMINATION PROCEDURE

- GENERAL -

O. R. Mulkey

Boeing Aerospace Company P.O. Box 3999 Seattle, WA 98124

4 June 1980

Final Report For the Period of 16 December 1979 Through 4 June 1980 Phase IV of NOSC Contract NC0123-78-C-0193

> Prepared For: Naval Ocean Systems Center Code 9312 San Diego, CA 92152

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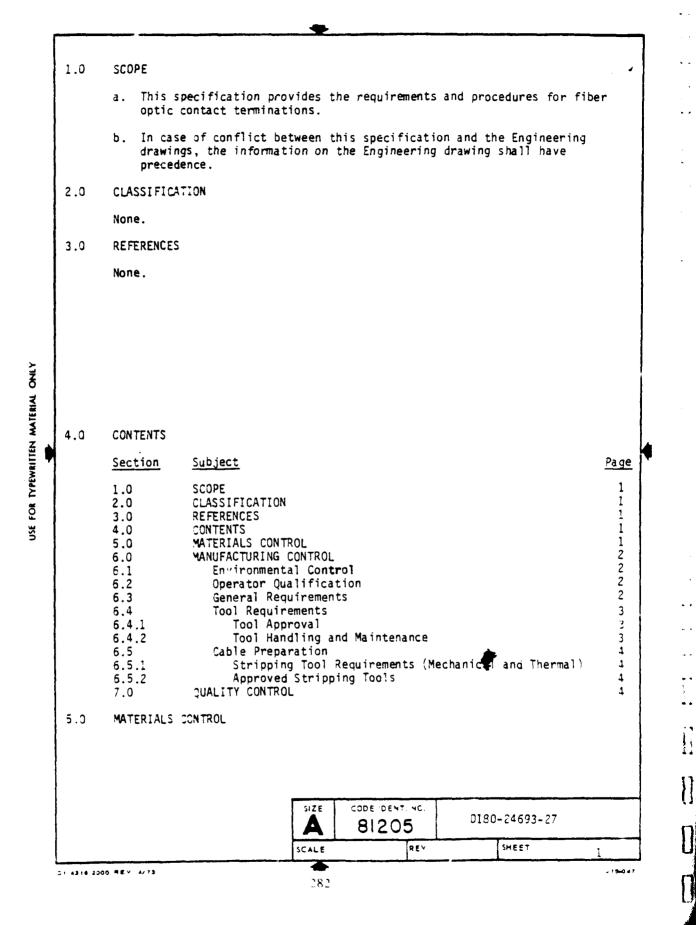
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6.0	MANUFACTURING CONTROL
6.1	Environmental Control
	a. Processes described herein shall be performed in an area meeting the requirements of FED-STD-209 1,500,000.
	 Activity Restrictions - The following operating practices shall be observed:
	No paint spraying shall be performed in the area.
	c. All personnel assembling, inspecting, handling, or otherwise touching those surfaces of cable assembly parts to be potted, molded, or encapsulated shall wear gloves to prevent contamination of the surfaces after they are cleaned. Cable assembly parts include bare conductors, connect contacts, terminals, connectors, and primed or etched surfaces. The gloves shall be made of rubber or a synthetic fiber of a quality which sheds a minimum amount of lint. Cotton gloves shall not be used. Find cots may be used in lieu of gloves when handling small parts which will not contact the bare palm or uncovered parts of the fingers. The glove or cots shall be replaced sufficiently often (at least once per shift) ensure cleanliness and no transfer of perspiration, grease, oil, or oth contaminants to the parts.
	CAUTION: The presence of silicone in hair preparations, cosmetics, and other products presents a serious source of contamination. Gloves must be replaced at any time they come in contact with such contamination.
6.2	Operator Qualification
	Personnel involved in terminating operations shall:
	 Be familiar with the requirements of this specification and associated dash-numbered specifications.
	b. Receive instructions explaining the process requirements pertaining to stripping and polishing operations.
	c. Receive training in the operation of tools employed in the specific process phase.
	d. Be skilled in the identification and use of tools required for the particular termination hardware.
6.3	General Requirements
	 All terminating devices shall be examined for conformance with the Engineering drawing parts requirements.
	b. Crimping shall not cause terminals, connector contacts, or any other terminating device to exhibit fractures, cracks, or base metal when viewed under five power magnification.
	SIZE CODE DENT. NO. D180-24693-27

	6.3 6.4 6.4.1	<pre>(Continued) c. If damage occurs to a contact or terminal, while crimping and it is not readily apparent that this damage was caused by operator, contact, terminal, or splices, the crimp tool must be recertified before further use. Tool Requirements Tool Approval a. New types of tools, including power units, modifications to existing tools and new applications for tools shall be approved by Components, Processes, and Standards Group of Engineering.</pre>					
		 readily apparent that this damage was caused by operator, contact, terminal, or splices, the crimp tool must be recertified before further use. Tool Requirements Tool Approval a. New types of tools, including power units, modifications to existing tools and new applications for tools shall be approved by Components, Processes, 					
		Tool Approval a. New types of tools, including power units, modifications to existing tools and new applications for tools shall be approved by Components, Processes,					
	6.4.1	a. New types of tools, including power units, modifications to existing tools and new applications for tools shall be approved by Components, Processes,					
		and new applications for tools shall be approved by Components, Processes,					
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		b. Suitability of Engineering approved stripping and crimping tools to pro- duction requirements shall be determined by the responsible Manufacturing organization. Any tool listed herein for the intended application may be selected, or Manufacturing may submit a request to Engineering for approval of new or modified tools.					
	6.4.2	c. Mechanical stripping tools and crimping tools shall be periodically certified. A sticker or dab of sealing putty with inspection symbol shall be attached to each tool indicating that the tool has been certified. The lack of a certification sticker or symbol on a tool indicates it has not been certified for production work and is not approved for use under this specification.					
	6.4.2	2 Tool Handling and Maintenance					
		a. Manufacturing may perform the following subject to Quality Control verification:					
		(1) Interchange crimping dies or contact locators in tool heads or frames when they are furnished with the tool or as a tool kit.					
-		(2) Interchange locators of infinite die closure adjustment crimping tools.					
		(3) Change die closure selector position number on crimping tools having this feature.					
		(4) Adjust blades of adjustable wire stripping tools.					
		b. Protect all tools as provided below:					
		(1) During transportation and storage keep each tool in a clean separate compartment or container which will protect the tool from mechanical damage.					
		(2) While in use the tools may be deposited on benches or other working surfaces but not on hardware.					
、		(3) Tools accidentally dropped or hit with other objects shall be recertified prior					
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6.5.1	Stripping Tool Requirements (Mechanical and Thermal)				
	à.		nical stripping tools shall satisfy the following rements:		
		(1) F	Fibers shall not be nicked, gouged, or cut.		
		r f r	The end of the jacket shall be cut as squarely and cleanly as required to meet subsequent operation requirements. Excess fibrous strands or extruded plastic protuberances may be removed provided that the minimum bend radius requirement of the cable is not violated.		
	b.		al stripping shall satisfy the mechanical stripping tool rements in addition to the following:		
			Fiber strands shall be clean with no evidence of plastic film deposit resulting from the stripping operation.		
			The cable jacket shall not be blistered, but a slight discoloration or deformation is acceptable.		
6.5.2	Appr	roved St	tripping Tools		
	a.	Approv	ved manual mechanical stripping tools are listed in Table I.		
	b.	cable limita	rp edged instrument may be used to remove insulations from sizes not covered by mechanical strippers, or when space ations will not permit use of mechanical strippers, subject e requirements of 6.5.1a.		
6.6	Visu	al Insp	pection Guidelines		
6.6.1	Scope				
fiber a	nd fi other	ber bun	des general guidelines for the visual inspection of single ndle cable terminations and may be used as inspection criteri ndicated on the detail termination procedure or assembly		
6.6.2	Fibe	er Bundl	le Cable Termination		
under m The sum (ratio than 50 viewed 15% of	agnif face of ar)%. 1 with the t	fication should rea of f The numb transmi total nu	nation should have a smooth (specular) surface when viewed n. A few (less than 5) surface scratches may be tolerated. be free from epoxy smears and voids. The packing fraction fibers to the total usable area of contact) should be greater ber of chipped lit fibers should be less than 10% when itted light. The number of unlit fibers shall be less than umber of fibers present in the cable. The total number of shall be greater than 85% of the nominal number of fibers		
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6.6.2 Fiber Bundle Cable Termination - Continued

for the cable type (45 mil bundle cable nominally contains 210 fibers); partially lit fibers may be counted as 1/2 of a lit fiber.

The termination should be viewed with a magnification such that the f ser containing portion of the termination covers at least 1/2 but less than the total viewing diameter.

6.6.3 Single Fiber Cable Termination

The finished termination shall have a smooth specular finish, when viewed under magnification. One scratch may be present on the fiber end surface. No epoxy smears or edge chips greater than 20% of the end area are allowed.

7.0 QUALITY CONTROL

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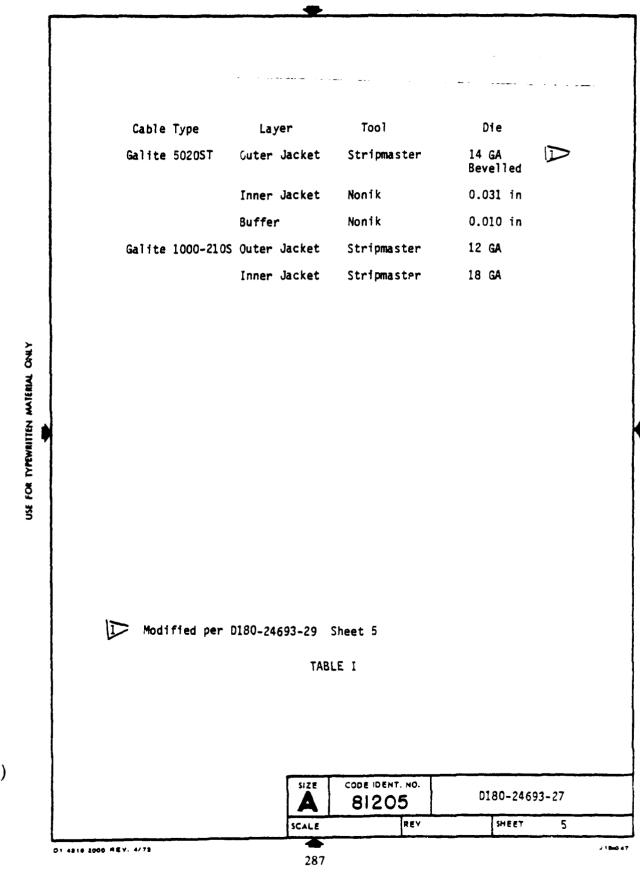
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- a. The Quality Control Department shall maintain the necessary surveillance to ensure the following:
 - Complete compliance with the requirements of this specification and associated dash-numbered specifications except operator qualification.
 - (2) Verification that only approved tools are used and that the tools have been certified to the applicable requirements of Document D2-6438.
 - (3) Label each machine setup by size and type.
- b. Quality Control shall ensure compliance with the environmental control requirements of this specification.

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APPENDIX K

FIBER OPTIC TERMINATION PROCEDURE, HUGHES CONNECTORS

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FIBER OPTIC TERMINATION PROCEDURE

- HUGHES CONNECTORS -

O. R. Mulkey

Boeing Aerospace Company P.O. Box 3999 Seattle, WA 98124

15 June 1980

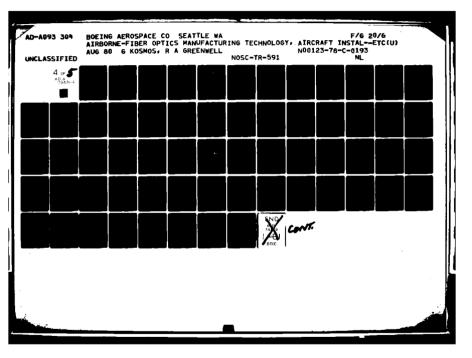
Final Report for the Period of 16 December 1979 Through 15 June 1980 Phase IV of NOSC Contract N00123-78-C-0193

> Prepared For: Naval Ocean Systems Center Code 9313 San Diego, CA 92152

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1.0	SCOPE	
	a. This specification establishes requirements for termination of fibe cables using Hughes C21 series connector contacts. This specificat complements D180-24693-27and is an essential part of that specifica	tion
	b. In the event of conflicting requirements, this specification shall precedence over D180-24693-27, and the Engineering drawing shall to precedence over both specifications.	
2.0	CLASSIFICATION	
	None.	
3.0	REFERENCES	
	None.	
4.0	CONTENTS	
	Section Subject	Page
	<pre>1.0 SCOPE 2.0 CLASSIFICATION 3.0 REFERENCES 4.0 CONTENTS 5.0 MATERIALS CONTROL 6.0 MANUFACTURING CONTROL 6.1 Tools 6.2 Cable Preparation 6.3 Polishing Procedure 6.4 Crimp Requirements 7.0 QUALITY ASSURANCE</pre>	1 1 1 1 2 3 3
5.0	MATERIALS CONTROL	
	Epoxy, Bi Pax 2143 D Alcohol, isopropyl Acetone	
6.0	MANUFACTURING CONTROL	
6.1	Tools - Also See Table I and Figure 1	
	Polishing tool Hughes 10939925 Hand fixture	
	Heat Gun, Ideal 4603A with Nozzle No. 46-922, No Certification Required	J
	SIZE CODE IDENT. NO. D180-24693-27.1	

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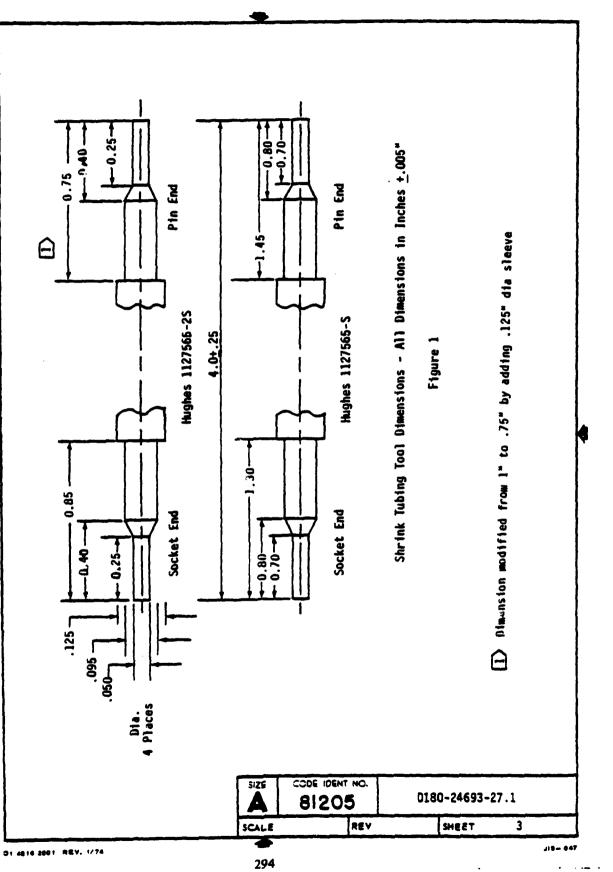
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	Shrink Tubing		HCX-3/32 Black				HCX-3/32 Black		outside)	
	Shrink Tubing Tool		11275655-S Pin End				11275655-S Socket End		og the small (
	EPOXY	B1 Pax 2143 D	I	2		1	3	2	red us in	
	Terminus (Type)	Ptn F.O. Single 1093201- 08051105	Ptn F.O. Bundle 10938275	Pin 22 GA C21P1620A0		Socket F.O. Single 1093202 080S110S	Socket F.O. Bundle 10938285	Socket 22 GA C2151620A0	ctor. An extra crimp on the Ferrule is required using the small (outside)	
TABLE I TERMINATION TOOLS	Crimp Tool (Wire Contact)			Danfels M22520/101	With TP4-303 Head			Daniels M22520/101 With TP4303 Head	tor. n extra crimp on	
F	Crimp Tool (Ferrule)	1143046S Middle	1143046S Middle	1143046S Middle		11430465 Middle	1143046S Middle	1143046S Middle	e e	
	Crimo Ríng	1127765				1127765			ared back: contact co ition.	
	Crimp Ferrule	1127773 1 1127764	112773 1127764	1127964-2		1127773 1127764	1127773 1127764		3 Used on flared backshell con 4 Used on 3 contact connector. crimp position.	
	Cable	Galite 5020ST	Galite 1000-2105	M27500- 22TGU 00		Galite 50205T	Galite 1000-2105	M27500- 22TGU00	1 1127773 1127764	
					SIZE		DENT. NO. 205	D180-	-24693-27 .1	
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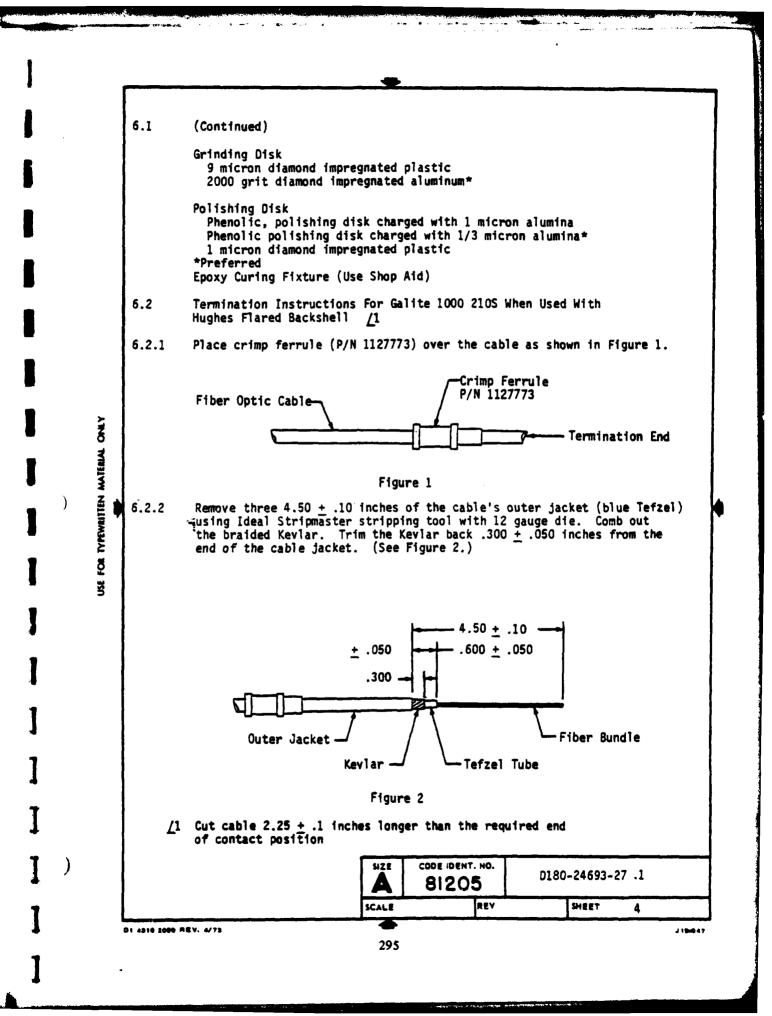
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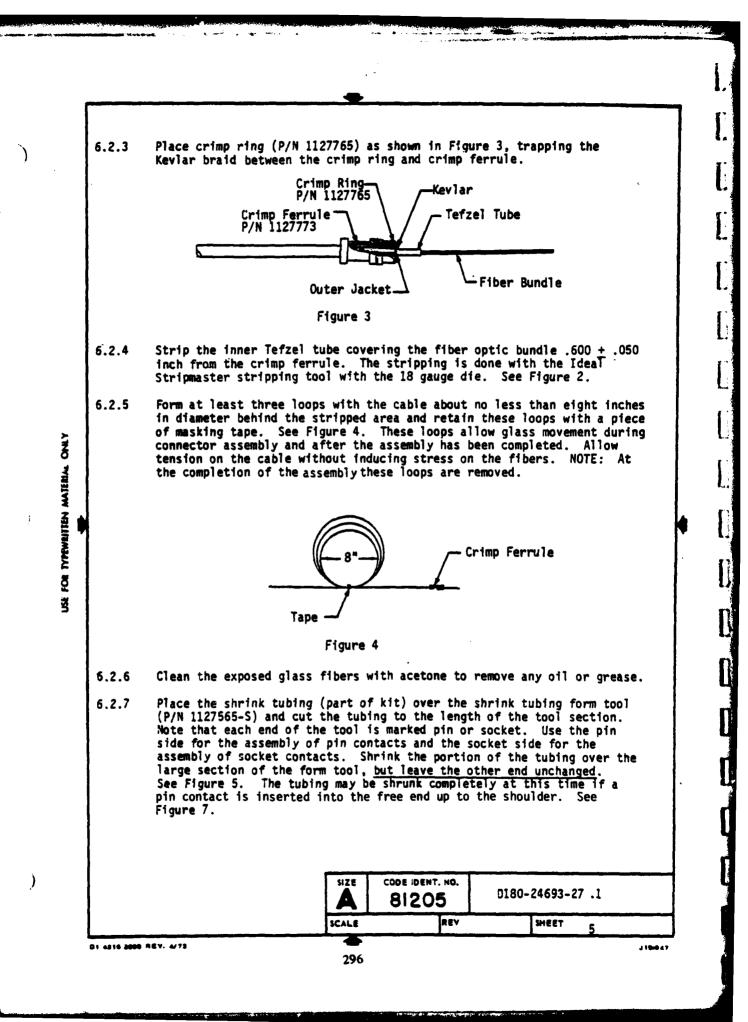
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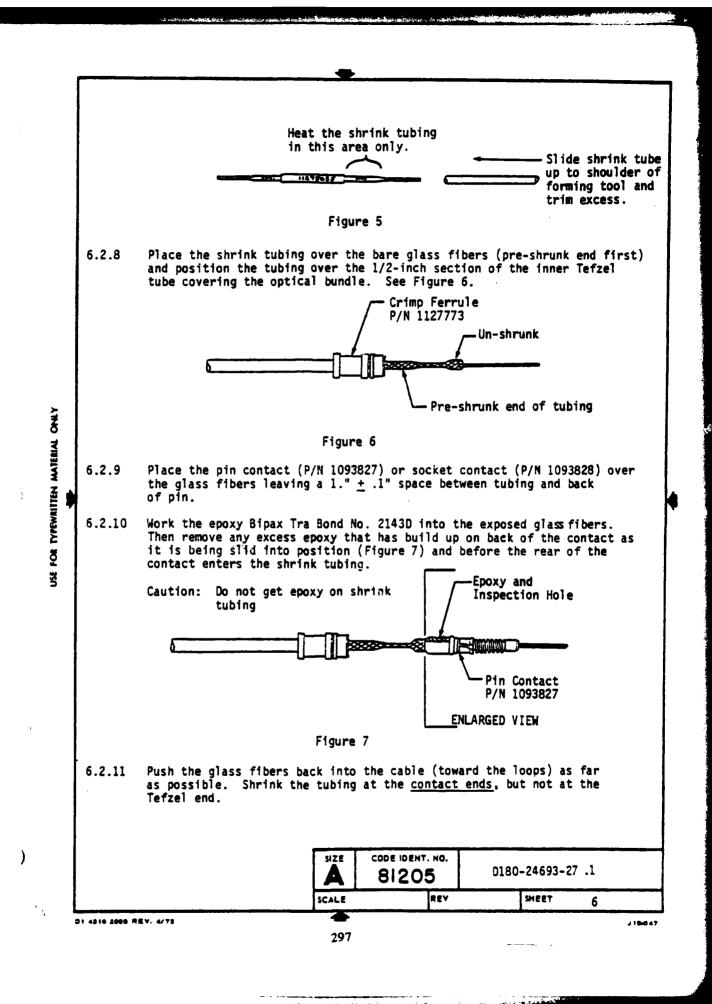
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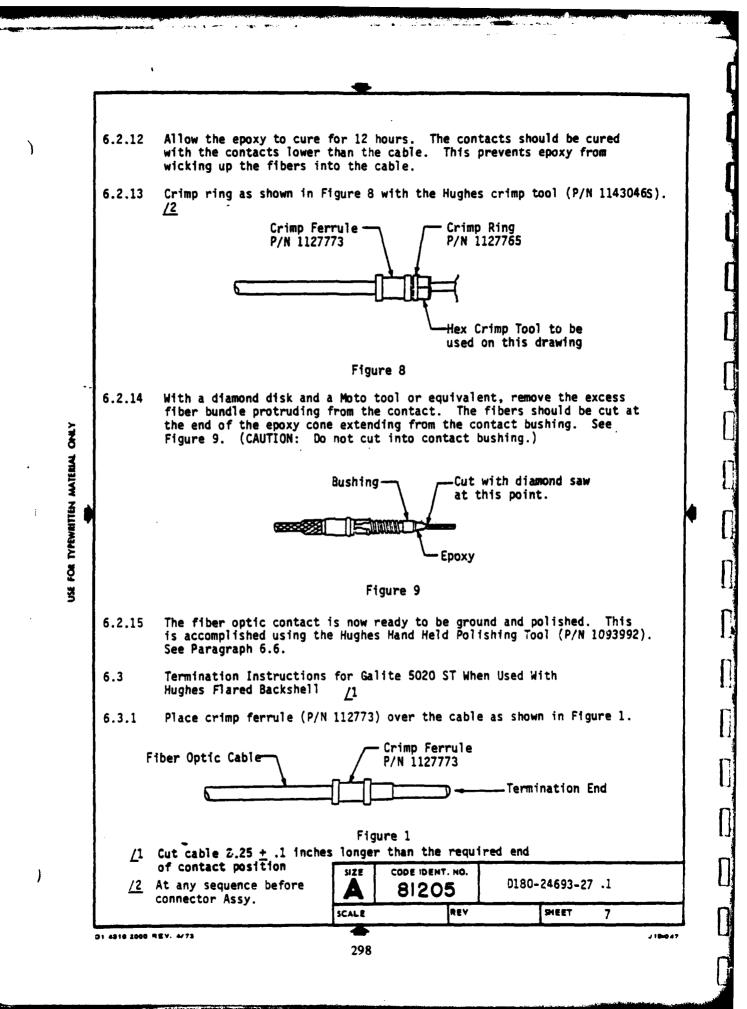
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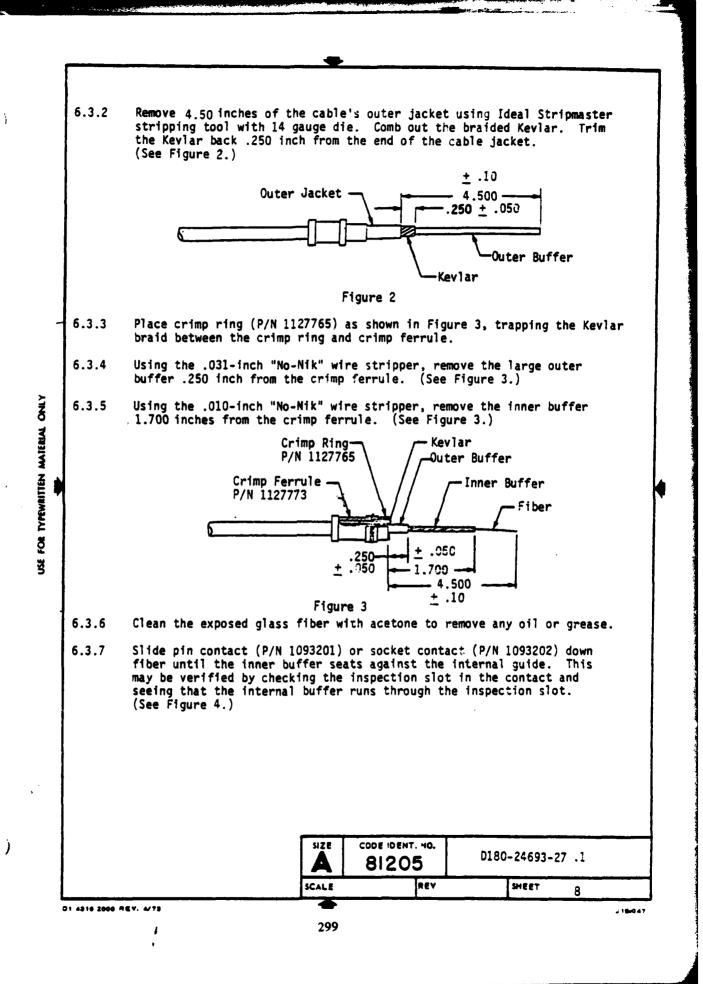
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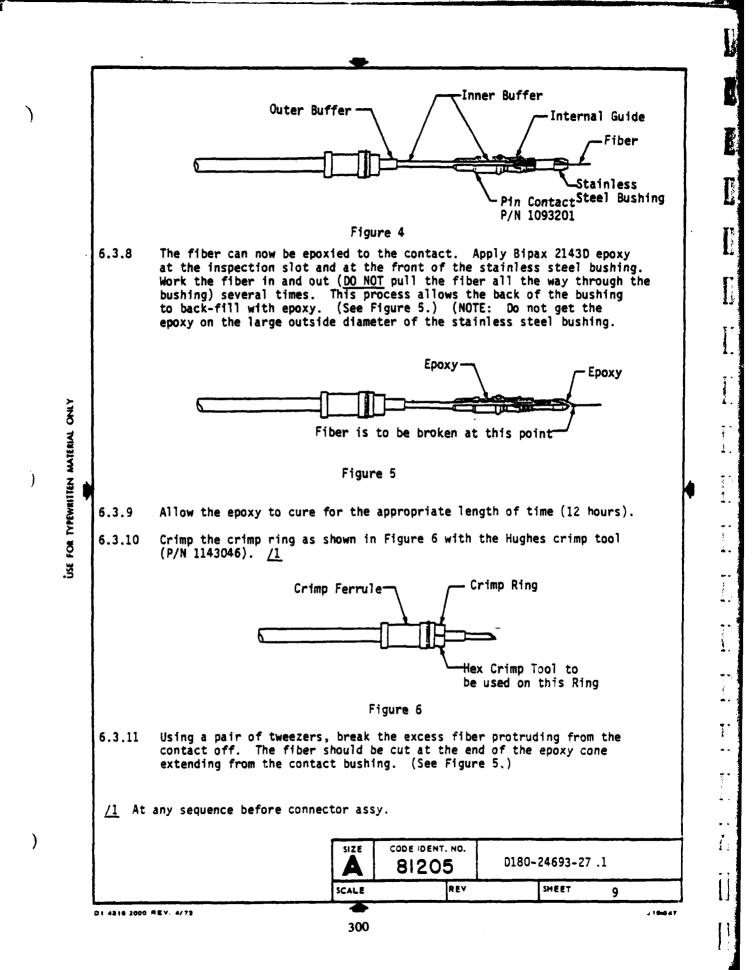


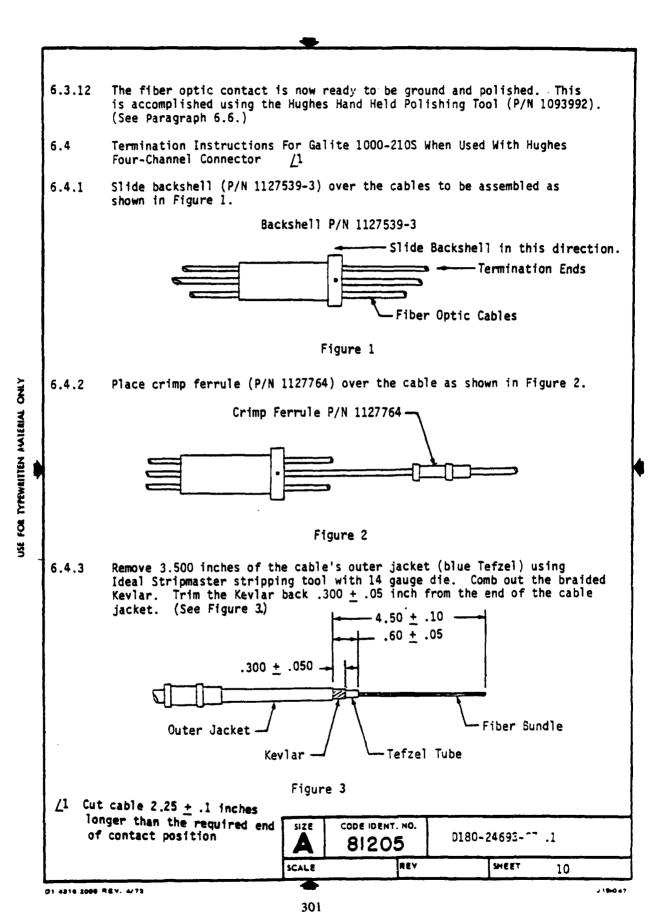






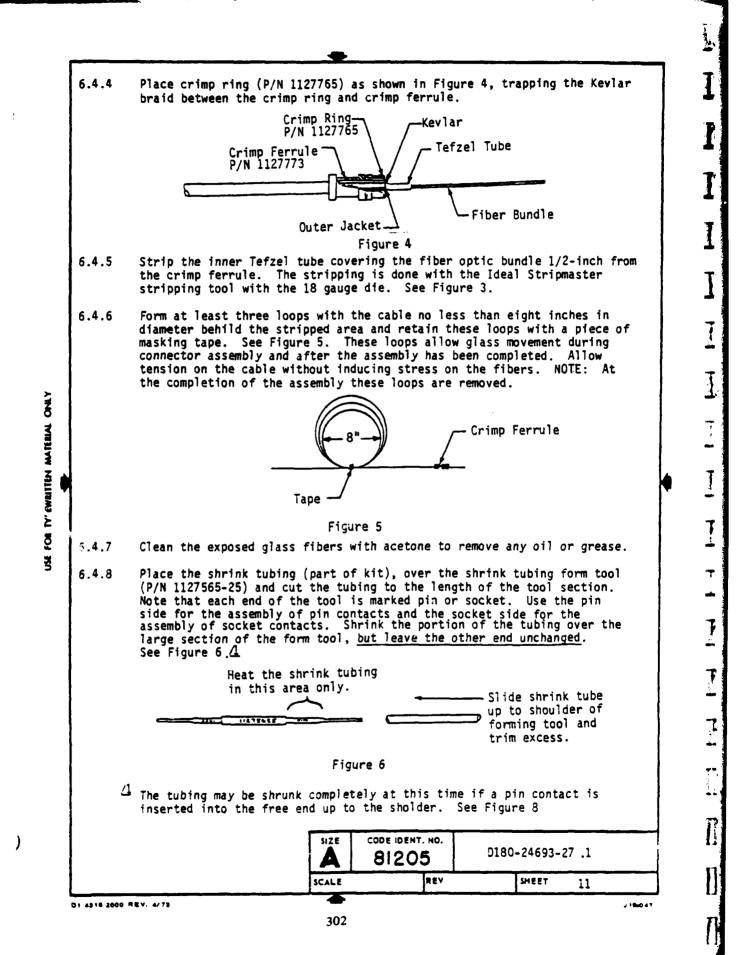




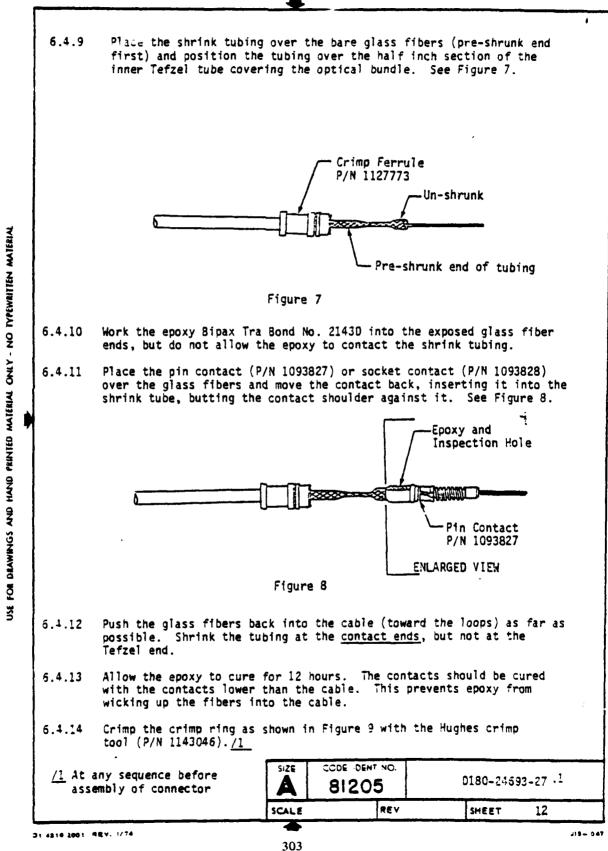


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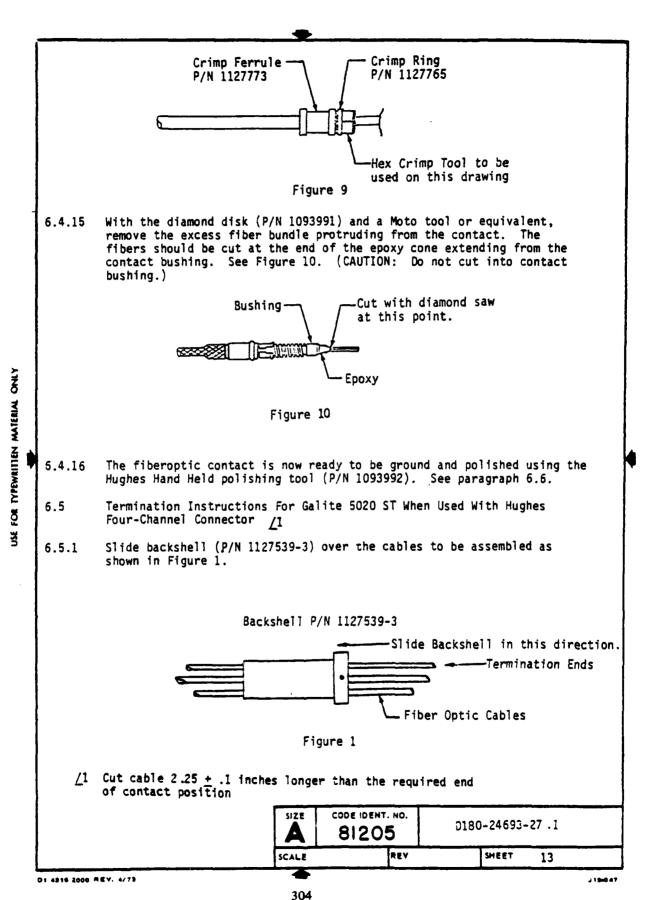
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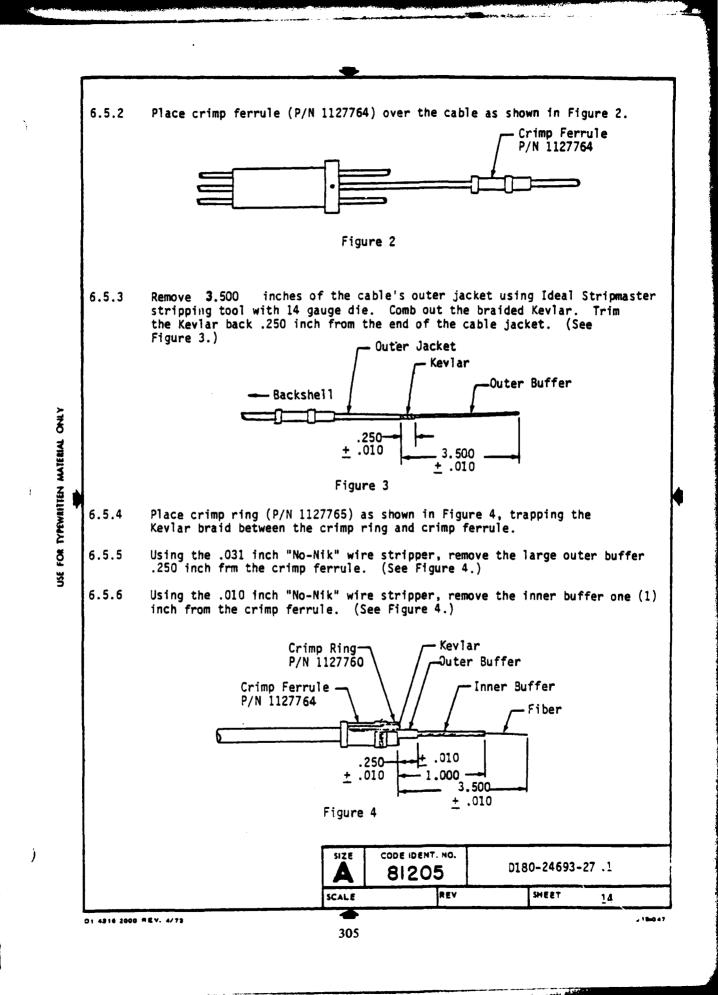
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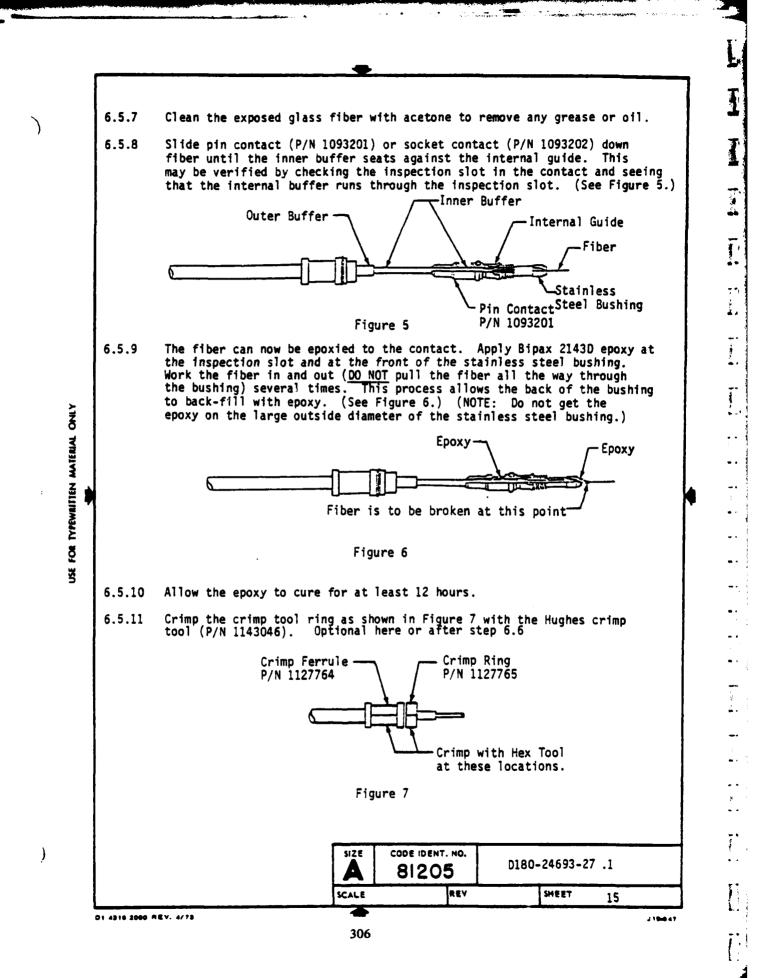
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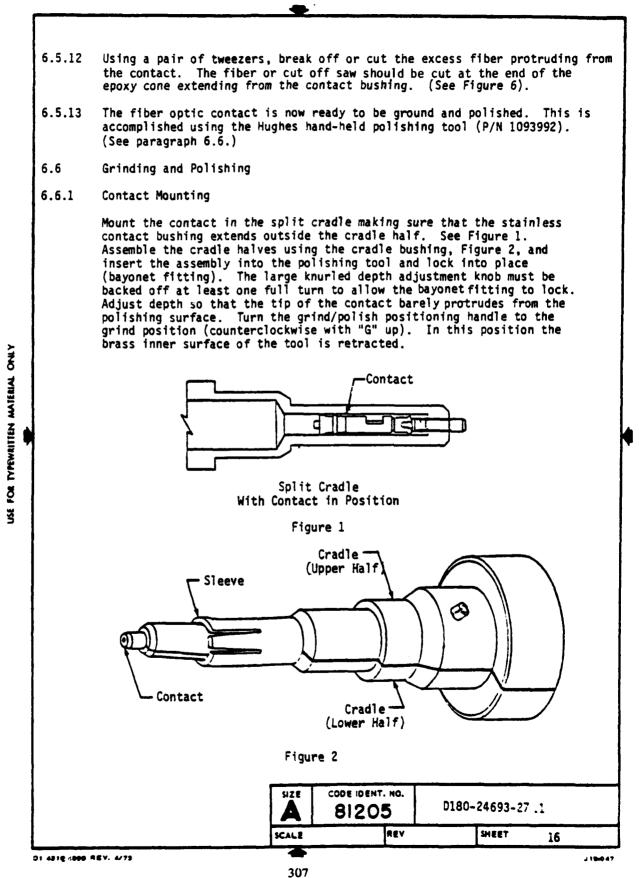


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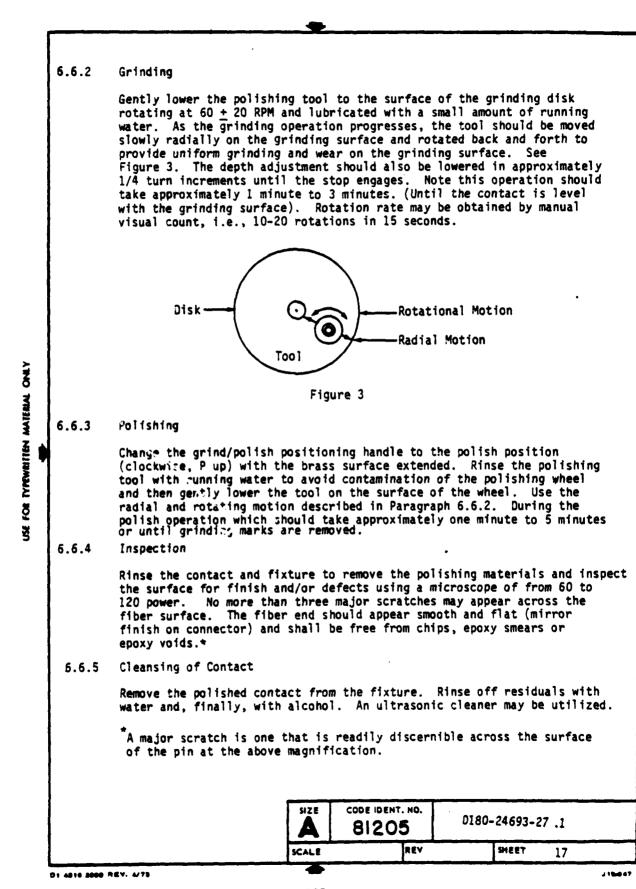
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6.7	Crimp Requirements						
	a. All crimp impressions shall be located on the crimp barrel. The inspe tion hole must remain useful after crimping. The crimp impressions sh not extend to the end of the crimp tarrel nor to any shoulder adjacent the crimp barrel.						
	b. Crimped connector contacts shall show no evidence of being bent.						
	c: Crimped connector contacts shall not exhibit fractures, cracks, or bas metal when viewed under 3X to 5X magnification.						
6.8	Rework Procedures						
6.8.1	Scope						
	This section provides alternate methods and materials which may be used to repair (reterminate) an existing cable in a harness or to prepare a new ca to replace a damaged cable in a completed or partially completed harness.						
6.8.2	Additional Materials						
1	Epoxy - Epotec 331, 353, or 353ND may be used and may be cured at $150^{\circ}C \pm 5^{\circ}$ for 5 minutes ± 1 minute or until the epoxy turns from amber to red.						
	Adhesive - Loctite Super Bonder 416						
6.8.3	Additional Tools						
	Oven - Setable to 150 ⁰ C or heat gun with controlled temperature head not to exceed 160°C air output at head face.						
	600 ⁰ grit wet type abrasive or abrasive paper.						
	Shoe for polishing tool 2-5 mils thick, with center hole (shop aid).						
6.8.4	Termination of Galite 1000-210S						
	Follow the procedure for this cable and connector type except that the alternate epoxies and cure times may be used. Strip length may be shorter than indicated. In addition, apply a small amount of the adhesive in the inspection hole and cure before applying heat to the epoxy. This will act as a stop to prevent the heated thinned epoxy from wicking up the fibers.						
6.8.5	Termination of Galite 5020ST.						
	Follow the procedures for that cable and connector type except that the alt nate epoxies and cure time may be used. Strip length may be shorter than indicated. In addition, a small quantity of adhesive should be applied at the inspection hole to the fiber and cured before heat curing the epoxy to prevent wicking of the epoxy when thinned by the higher temperature cure.						
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6.8.6 Initia	al Grinding
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An extra initial grinding step may be added using the 600 grit abrasive and the polishing fixture shoe. The course grit material will speed cutting time of the harder epoxy. The shoe protects the surface of the polishing tool and also acts as a depth limiter to this step.

6.8.7 Cleaning

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The contact and the polishing tool must be thoroughly cleaned after the initial grinding operation to prevent contamination of the following grinding and polishing disks.

6.8.8 Grinding and Polishing

At this point return to the standard method for the cable and connector type.

7.0 QUALITY ASSURANCE

> The Quality Assurance Organization shall maintain the necessary surveillance to ensure the following:

- a. Compliance with the requirements of this specification and
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APPENDIX L

FIBER OPTIC TERMINATION PROCEDURE, AMPHENOL CONNECTORS

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FIBER OPTIC TERMINATION PROCEDURE

- AMPHENOL CONNECTORS -

O. R. Mulkey

Boeing Aerospace Company P.O. Box 3999 Seattle, WA 98124

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15 June 1980

Final Report for the Period of 16 December 1979 Through 15 June 1980 Phase Iy of NOSC Contract N00123-78-C-0193

> Prepared For: Naval Ocean Systems Center Code 9313

> > San Diego, CA 92152

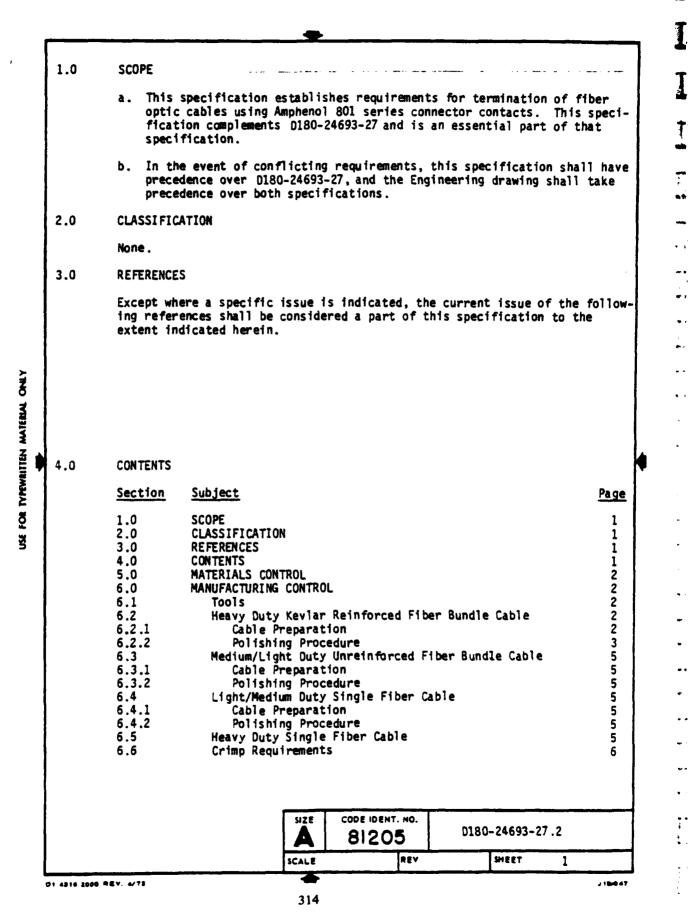
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Connectors		4. PERFORMING ORG. REPORT NUMBER D180-24693-27.2
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O. R. Mulkey		•
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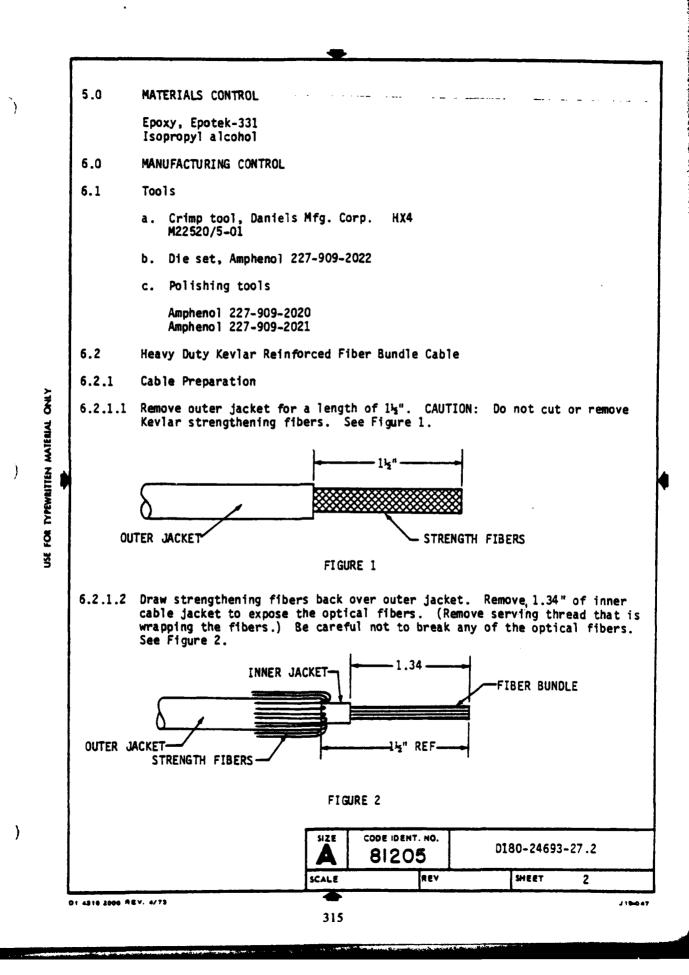
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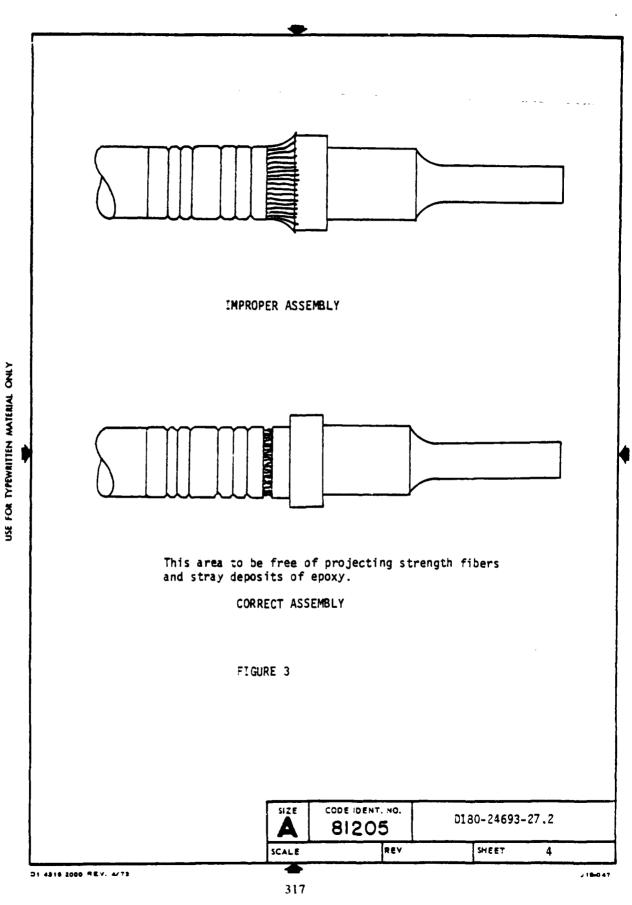
6.2.1.3 Clean the exposed fiber bundle under the jacket using isopropyl alcohol, either by dipping or by use of a "squeeze bottle". 6.2.1.4 Apply epoxy to the inner jacket. 6.2.1.5 Reposition the strengthening fibers back over the fiber bundle and carefully slip the crimp ferrule over both fibers and up to the outer jacket. 6.2.1.6 Reposition the strengthening fibers back over the ferrule and apply epoxy to the glass fibers up to the ferrule. Work the epoxy well into the fibers but do not allow the epoxy to wick up over the jacket. 6.2.1.7 Slip contact onto glass fiber bundle until it butts against the crimp ferrule. Draw strength fibers tight, keeping contact in place against ferrule. Place assembly into crimping tool (Die Set Amphenol #227-909-2022) and register contact collar in recess provided for it. Check for maintain-ing positioning of contact ferrule and that strength fibers are held tight. Close handle of crimp tool affecting crimping of the ferrule. Put one drop of epoxy on fibers where they project through nose of contact. Place crimped assembly under a source of heat and cure epoxy at a tempera-6.2.1.8 ture of 120°C for 5 minutes. When epoxy on fibers at nose of contact turns red, the epoxy is cured. Care should be exercised so that curing temperature is not exceeded or cable jacket will be damaged. 6.2.1.9 Allow assembly to cool to room temperature. 6.2.2 Polishing Procedure 6.2.2.1 Snap off excess fibers that project from end of contact. 6.2.2.2 Insert contact into polishing tool. Use Tool #227-909-2021 for contact 801-999-5124 and Too1 #227-909-2020 for contact 801-999-5125 6.2.2.3 Polish using 9 micron polishing film, bring fibers to contact tip using water as a lubricant and coolant. 6.2.2.4 The final polishing step should be accomplished using 1 micron polishing film. 6.2.2.5 Dry and examine under 50X magnification for gross imperfections. Be sure the optical surface is flat and free of scratches, chips, or epoxy smears. Remove strength fibers from front end of ferrule (cut flush with scalpel or 6.2.2.6 razor blade). Inspect retention collar area of contact. Be certain that any stray epoxy is removed from the surfaces. See Figure 3. CAUTION: If above procedure described in 6.2.2.6 is not adhered to during terminating a fiber optic cable, the contact retention system of the connector will be damaged and the contact will fail to remain captivated. CODE IDENT. NO. SIZE D180-24693-27.2 Δ 81205 REV SHEET SCALE 3 01 4316 2000 REV. 4/75 19-047 316

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6.3	Medium/Light Duty Unreinforced Fiber Bundle Cable
6.3.1	Cable Preparation
6.3.1.1	Remove jacket for a length of 1".
6.3.1.2	Roughen the 1st 5/8" of jacket using 240 grit paper.
6.3.1.3	Slip a 5/8" length of $1/8$ heat shrinkable tubing over jacket to a depth o $3/8$ " as shown in Figure 4.
	1/8" Heat Shrinkable Tubing Hetal Ferrule
	FIGURE 4
6.3.1.4	Coat fibers with epoxy working it between all fibers.
6.3.1.5	Slide contact over fibers and under the ferrule and heat shrinkable tubing until it bottoms on the jacket.
6.3.1.6	Crimp the ferrule onto the contact using the listed tool and die set.
6.3.1.7	Apply epoxy to the tip on the contact and cure for 5 minutes at 125° C.
6.3.2	Polishing Procedure
6.3.2.1	Polish per 6.2.2.
6.4	Light/Medium Duty Single Fiber Cable
6.4.1	Cable Preparation
6.4.1.1	Use the procedures detailed in Paragraph 6.3.1.
6.4.2	Polishing Procedure
6.4.2.1	Polish per Paragraph 6.2.2.
6.5	Heavy Duty Single Fiber Cable
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6.6	Cri	mp Requirements
		All crimp impressions shall be located on the crimp barrel. The instition hole, if present, must remain useful after crimping. The crimp impressions shall not extend to the end of the crimp barrel nor to a shoulder adjacent to the crimp barrel.
	b.	Crimped connector contacts shall show no evidence of being bent.
	c.	Crimped connector contacts shall not exhibit fractures, cracks, or b metal when viewed under 3X to 5X magnification.
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APPENDIX M

FIBER OPTIC SHOP AIDS REQUIREMENTS, GENERAL

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FIBER OPTIC SHOP AIDS REQUIREMENTS -GENERAL-

O. R. Mulkey

Boeing Aerospace Company P.O. Box 3999 Seattle, WA 98124

4 June 1980

Final Report For the Period of 16 December 1979 Through 4 June 1980 Phase IV of NOSC Contract N00123-78-C-0193

> Prepared For: Naval Ocean Systems Center Code 9313

San Diego, CA 92152

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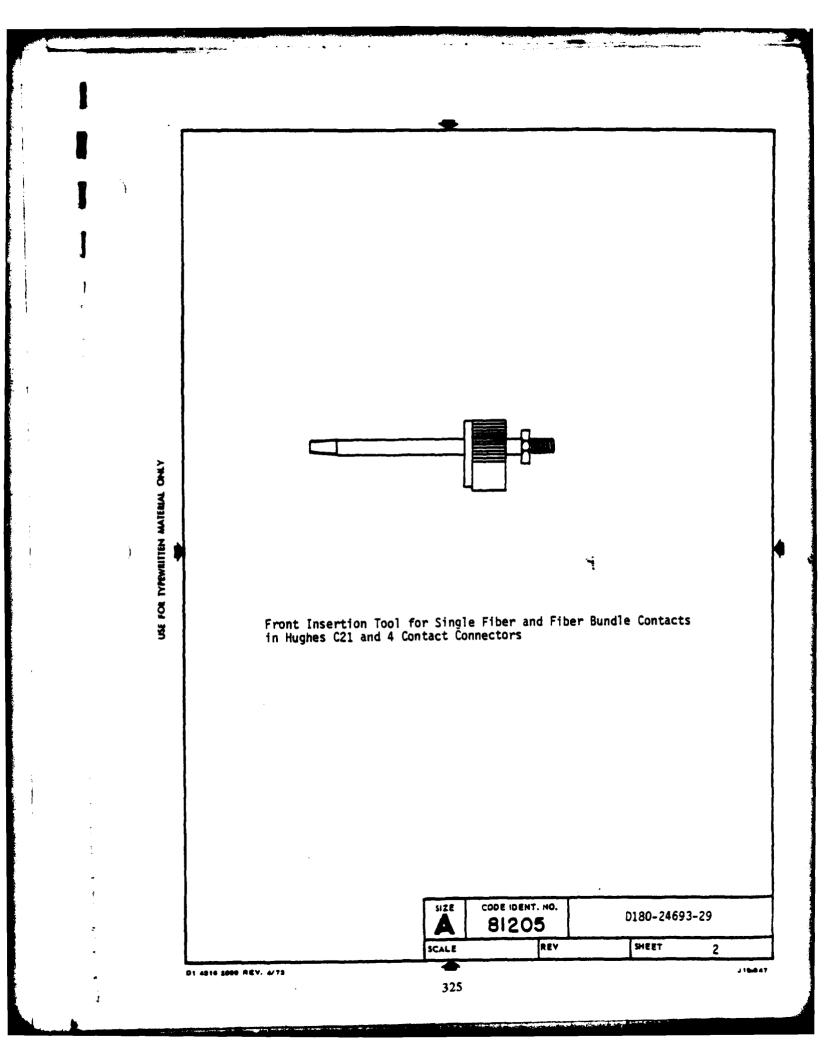
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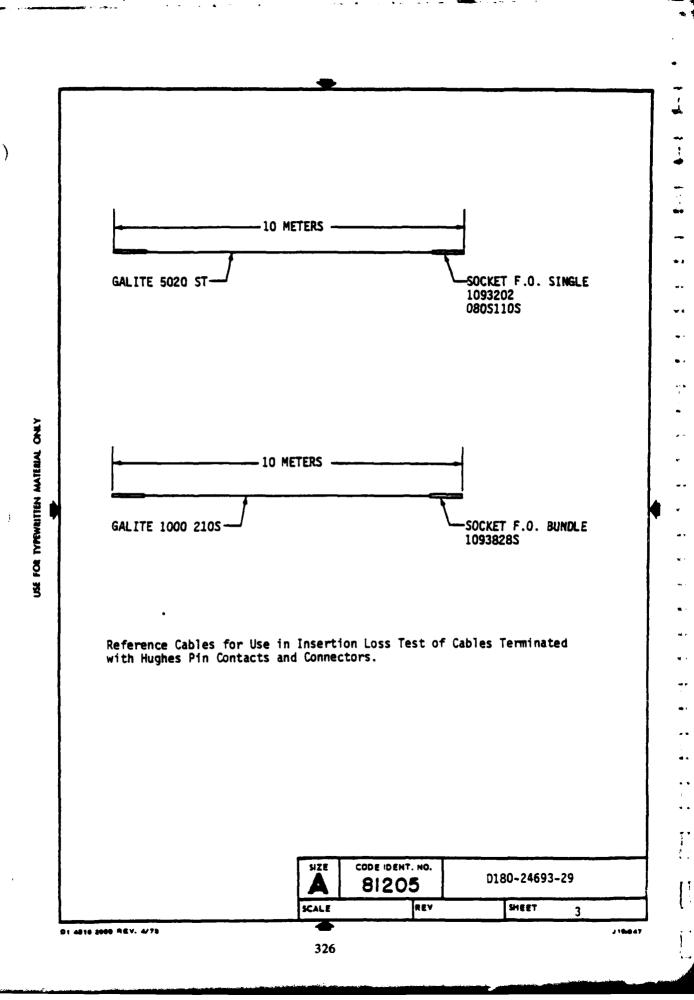
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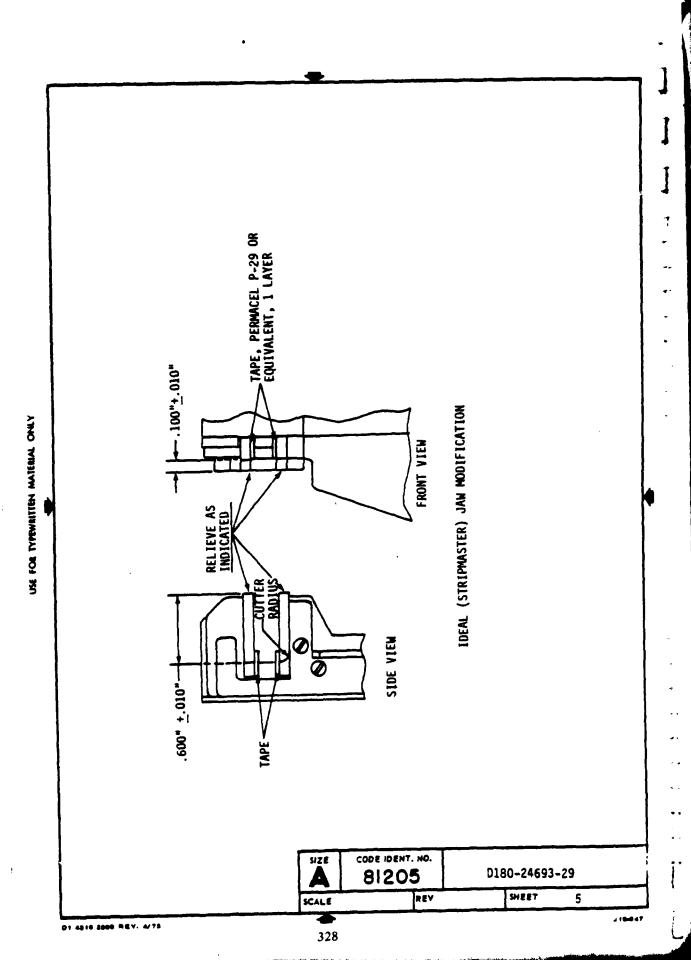
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4316				NUMBERED TOOL LIST	LOOL LIST
2009			Tool Type	Part Number	Use
R E V. 4			Insertion/Extraction	Hughes 1093663S	To apply or remove the alignment sleeve on Hughes sockets.
/71			Cable Clamp. Small Large	Hughes 1143047 Hughes 1143048	Used in the Hughes polishing tool (Part No. 1093992S) to support the cable during the grind/polish operation. Use size which best fits cable being finished.
			Grind/Polish Machine	Fac-Ette 8826	Used to rotate grinding & polishing disks during termination sequence.
			Cut Off Wheel, Diamond	isomet 11-1180	Used to cut off excess fiber(s) after epoxy cure in prepara- tion for the grind/polish operation of termination
3	SCAL	SIZ	Ultrasonic Cleaner	Delta Sonic D1-3	Provides ultrasonic action in the cleaning of the grind/polish tool and termination during the termination sequence.
27			Light Source	D180-2451-2 (or small flashlight)	Used to illuminate fiber ends during continuity test and photography.
		ODE IDENT. 1 81205	Test Cables Source Detector	None	Used with Photodyne optical multimeter to couple to reference cables and cables under test.
	EV		Insertion Tools	Hughes 1143042	Used to insert fiber bundle contacts into Hughes 4 contact
	0100	0180		Hughes 1143043	connectors. Used to insert single fiber contacts into Hughes 4 contact connectors.
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APPENDIX N

ROUTING TECHNIQUES

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ROUTING TECHNIQUES

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S.P. Suave, C. Hand Boeing Aerospace Company P.O. Box 3999 Seattle, Washington 98124

8 September 1978

Interim Report for Period 15 May through 8 September 1978 Phase I of NOSC Contract N00123-78-C-0193

Prepared For:

NAVAL OCEAN SYSTEMS CENTER Code 9313 San Diego, California 92152

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In addition, standard routing procedures applicable to fiber optics were identified as part of the overall routing technique analysis.

The results of the analysis showed that fiber optics can now be safely routed through hazardous/environmentally stringent areas without sacrificing safety or performance. This is true because the glass-on-glass fiber bundle can withstand temperatures up to 600°C prior to softening. The other well-established benefits such as no grounds and EMI immunity makes the fiber itself attractive for most aircraft applications.

There are some routing precautions with the fiber, however. It has been reported that moisture has caused fiber cracking in stress areas such as in the bend radius. This will require special moisture protection or routing instructions that will clearly limit tensile or compression loads and excessive axia twisting, bending, and flexing.

One disadvantage to fiber optic interconnect systems is that signals cannot be reliably terminated or generated in hazardous/high temperature locations. This is due to the temperature sensitivity of the active components, particularly the laser diodes. During the analysis, it was found that the component manufacturers did not have the data that would allow a thorough analysis of the component characteristics as a function of several different environmental conditions. Although optical data was generally sufficient, full parametric characteristics were not identified to fully assess the components for a variety of environments.

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1.0 INTRODUCTION

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The wiring in an aircraft is designed to withstand a broad range of adverse thermal, mechanical, and chemical environments. The performance levels of the installations have been determined by careful evaluation and trial and error to such an extent that electrical system reliability is taken for granted. Even though a modern commercial or military airplane has thousands of connectors with tens of thousands of individual contacts and the wiring total lengths are measured in miles, a malfunctioning circuit is rare.

Fiber optics is a new but similar field. Many of the lessons learned in standard electrical wiring can be used as a starting point for designing reliable fiber optic installations. It is the purpose of this document to summarize the design criteria which apply to both standard wiring and fiber optic cables and use this for a design base to establish a philosophy for fiber optics routing. To do this, the families of areas in the airplane where fiber optics could be routed will be grouped and critical design listings made for each. The routing philosophy presently applied to each area in designing electrical installations will be tabulated.

Finally, the comparative properties of fiber optic cables and electrical cables will be used to determine what changes need be made and hardware developed in order to determine where fiber optic technology can be successfully utilized.

2.0 SUMMARY AND CONCLUSIONS

An analysis was made of the routing techniques for fiber optic interconnects, comparing them with conventional electrical wire. Three main areas were addressed. These areas were:

- 1. Hazardous/sensitive area about the aircraft
- 2. The main aircraft locations and the expected environmental conditions
- 3. Fiber optic component capabilities to operate in either of the two above areas

In addition, standard routing procedures applicable to fiber optics were identified as part of the overall routing technique analysis.

The results of the analysis showed that fiber optics can now be safely routed through hazardous/environmentally stringent areas without sacrificing safety or performance. This is true because the glass-on-glass fiber bundle can withstand temperatures up to 600° C prior to softening. The other well-established benefits such as no grounds and EMI immunity makes the fiber itself attractive for most aircraft applications.

There are some routing precautions with the fiber, however. It has been reported that moisture has caused fiber cracking in stress areas such as in the bend radius. This will require special moisture protection or routing instructions that will clearly limit tensile or compression loads and excessive axial twisting, bending, and flexing.

One disadvantage to fiber optic interconnect systems is that signals cannot be reliably terminated or generated in hazardous/high temperature locations. This is due to the temperature sensitivity of the active components, particularly the laser diodes. During the analysis, it was found that the component manufacturers did not have the data that would allow a thorough analysis of the component characteristics as a function of several different environmental conditions. Although optical data was generally sufficient, full parametric characteristics were not identified. These characteristics include:

Stability versus temperature

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Sensitivity versus temperature

- Activation energy
- Radiation effects
- Moisture/humidity resistance
- Stress (Mechanical)
- Electrical overstress effects on sources/detectors
- Thermal shock
- Contamination resistance

Although some research is being directed toward gathering data on the above areas, the data does not exist to firmly state that fiber optics can be used in all applications and locations. The trends for the active components, however, indicate that the active components may be used in hazardous/ environmentally stringent areas in the mid-1980's.

Special routing techniques will also be necessary for termination and splicing aboard the aircraft. Splicing areas may have to be designated in order to allow for the necessary room and safety requirements necessary to make splices/ terminations. This is an additional consideration that is not needed for conventional wire.

The area of splicing and termination as applied to field repair techniques is not well understood and will be addressed in subsequent phases of the program. Until the equipment is developed to allow effective splicing of fiber bundles, the routing techniques must allow for adequate room to repair or replace a broken fiber. An interim solution to this problem can be achieved by running unused bundles in the harness. Then, if one bundle breaks, a spare would be available and could be connected at the backshell of the connector. Although this approach is feasible, it begins to defeat some of the projected cost benefits of fiber optic interconnect systems.

The advantages to fiber optic interconnects have been explored and are well understood. These advantages, the main one being the absence of electrical current, will allow fiber optics to be applied in most areas of a military type aircraft. The currently identified disadvantages to routing fiber optics are:

- Moisture protection requirements
- Active component reliability
- Splicing/termination areas
- Limited data base for routing concepts

The methods developed for routing conventional wire into an aircraft are believed to be sufficient for fiber optics. Precautions to address the areas above must be considered in the fiber optic routing technique to allow for successful installations. It is believed that the identified technology problems can be resolved and that successful, reliable routing of fiber optics will occur for all areas of a military aircraft by mid-1980's.

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3.0 ROUTING ANALYSIS

3.1 Basis for Routing

The installation of fiber optic cables in aircraft can be done using the techniques adapted from the installation and routing of standard electrical and coaxial cables. The experience obtained in experimental commercial-type installations and comparison of the properties of fiber optics cables with comparable electrical wire characteristics supports the feasibility of adapting standard routing techniques to installing fiber optics cables.

The performance standards of installed electrical cables are tested with well established procedures and limits. The limits of MIL-E-5400 and MIL-STD-810 define a standard of performance to check the equivalent fiber optics cables.

The installation procedures defined in Volume D180-24693-2 are based on standard practices of airplane installation. The installations produced have a satis-factory history of withstanding airplane service life. The installation and routing of fiber optics cables in the same manner, then, can be expected to provide an equally serviceable installation.

The successful installation and routing of fiber optics cables in two Boeing military-type aircraft (the ASW B-504 and the YC-14 aircrafts) have shown that prudent selection of the processes developed for conventional electrical cables can be successful with fiber optic. This philosophy will be carried forward in the analysis of routing techniques for fiber optics.

The primary areas to be analyzed in the routing of fiber optics are:

- 1) Where can fiber optics be routed in a military-type aircraft?
- 2) What are the environmental constraints of the aircraft areas?
- 3) How mature are the fiber optic components to withstand the required environmental conditions?

These areas will be discussed in the following sections.

3.2 Hazardous/Sensitive Routing Areas

The most obvious hazardous area that fiber optics can impact is the fuel tanks. It is imperative that no sparks be generated in this area in order to prevent explosion. Similar "no spark" areas may exist in armament storage bays or areas of gaseous mixture with air: MIL-E-5400P considers a system explosion proof when the components are incapable of producing arcing or sparking.

With conventional electrical wiring, explosive areas are generally to be avoided because of the spark threat. However, when it is required to go through a fuel tank, for instance, the following routing additions are made:

- A metal conduit having a Teflon impregnated woven or wrapped glass fiber liner or a similar protective coating is used.
- All wiring within the conduit must be flame resistant per MIL-W-25038 or equivalent.
- Bond resistance for fire/explosion hazard area is applicable.
- All terminations in fire/explosion hazard areas should be potted or sealed using compatible material to prevent shorting or arcing.

This arrangement offers the greatest protection against fires or explosions resulting from shorted or overloaded wires, which otherwise would ground to the conduit wall and burn through.

Because fiber optics carries no electrical current, shorting or arcing is not a possibility. Therefore, the costly and complex steps listed above can be eliminated without sacrificing safety. This makes fiber optic fuel indicators and other control functions within fire/explosion hazard areas a reality.

High temperature areas also cause problems in routing interconnect systems. Typical hot areas include engines, engine nacelles, heaters, air conditioners, heat exchangers, and skin hot spot zones.

For conventional wiring, several precautions must be taken to prevent temperature damage. These rules include:

- Polyethylene dielectrics (used in coax) softens above 160⁰F. Bend radius must be 10D at any temperature.
- Bundle/route low temperature general purpose wire separately from high temperature wire and outside any area that may reach temperatures above 200°F.
- Provide clearance, thermal insulation, or baffles between wiring and heat generating parts such as electron tubes and power resistors to prevent deterioration.
- Route wires outside areas of thermal extremes.
- When routing wires or wire bundles in areas where there is heated equipment, thermal anti-icing ducts, or cabin air conditioning ducts, maintain the maximum spacing possible between the wire and the heater equipment.

Here, again, fiber optics technology eliminates extensive temperature damage protection schemes. Fiber interconnects, using a glass cladding over the silica (glass-on-glass) can withstand temperatures up to 600°C-800°C before softening occurs. Although the fibers can still be functional above this temperature range, it should be considered the upper limit of operation. Because of the high temperature capability, most of the precautions listed above are minimized in fiber optics. Common sense, however, must still prevail in that direct contact with a heating element such as a power resistor or heater heating element should be avoided. As a general rule, fiber optics cables should remain at least two inches away from heat generating sources.

Composite materials is a new technology that will be considered for future aircraft. The use of composites presents additional problems since the shielding effects of the aluminum structure will be lost. Shielding for conventional wire will be mandatory to reduce EMI/RFI susceptibility, guard against radiation (transmission) of data and protect against radiation damage. Figure 1 indicates some of the applications that require shielding and would be particularly important in composite structures. FIGURE 1: CONVENTIONAL WIRE REQUIRING SHIELDING/GROUNDING

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APPL I CATIONS

- All analog signal cables feeding wideband receiver circuits
- A/D Converters
- · High Gain Amplifiers
- All digital signal cables feeding transient sensitive electronics
- All excitation power and measuring power cables
- All video lines
- All rf signal cables

EXAMPLE - SHIELDING REQUIREMENTS (EXTERNAL)

- Multiple grounded to chassis in most cases
- Audio/instrumentation circuits of 10MV or less (full scale) must be singly grounded
- · Shields should not be contacted together at the chassis
- · Touching shields should be avoided
- Use caution with shields for return circuits
- Shields must be grounded

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The shielding requirements shown in Figure 1 are just a partial listing of the rules that must be followed in protecting cables. The rules are extensive and add significantly to the cost of the system. Fiber optics would eliminate the need for this extensive grounding due to the fact that it does not carry current. In fact, for the fiber optic harness selected for this program, the conventional harness contains 114 terminations of wires, jumpers, shields, and grounds which was reduced to 56 terminations wires, shields, and grounds in the new fiber optic/conventional hybrid design. This reduction was due to the elimination of jumpers, shields, and grounds on the small signal lines which were replaced with fiber optics (the power lines remained in the new harness along with the associated grounds and shields).

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Fiber optics, therefore, can be routed in composite structures without sacrificing cost, weight, and security. This is true not only in composites, but in other applications requiring extensive shielding or security. Security is one area where fiber optics can be very beneficial. Because it does not radiate energy or is difficult to tap into (particularly on an aircraft), the use of encryption techniques would not be necessary for on-board data processing and transfer of secure information.

In areas where interference coupling control is mandatory to minimize EMI, special precautions must be taken with conventional interconnect systems. Because EMI can be induced on the wires, certain circuit design criteria must be implemented. These factors include:

- Balance of Circuitry
 - minimize capacitive coupling
 - wires covered with high dielectric insulation
 - **special** isolation
 - properly twisted wires

• Impedance of Circuit

- design for lowest practical impedance
- Bandwidth of Circuit

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noise increases with bandwidth

Twisting the wires is a common practice in reducing mutual inductance (for a balanced circuit). Specific instructions are set forth to define and control the twisting.

Fiber optics on the other hand cannot be effected by EMI. Therefore, circuit **des:gn** is simplified as well as the installation and routing procedures. No **special** precautions are known that will be necessary to route fiber optics in **high** EMI areas.

Protection from contamination should be the same for fiber optics technology **as conventional wire.** Some of the routing considerations are:

- Do not route wires under or near tubing connections.
- Route wiring at least three inches away from hydraulic lines.
- Locate wiring at least six inches from fuel and oxygen lines. If this spacing is impossible, a minimum separation of two inches is allowable provided both the wiring and lines are separately secured and clamped.
- Route wiring so that electric terminations will not occur adjacent to lines carrying oxygen or flammable substances (to prevent arcing due to use of service tools).
- Do not route wiring near batteries or under fluid lines (especially connections), sumps, or pumps. If such routing cannot be avoided, adequate protection must be provided against contamination.
- Fiber optic interconnects should avoid high moisture areas to reduce the effects of microcracking.

Sensitive circuits are those circuits which are susceptible to noise, crosstalk, or other anomalies that can adversely affect performance. These circuits include:

- Sensitive circuits over 5 volts or over 1/2 ampere.
- AC and switched dc power and control circuits.
- RF power circuits.
- Video and digital power circuits.
- DC and low-frequency signal circuits.

• Video and digital-logic signal circuits.

• RF signal circuits.

These circuits require special routing considerations to nullify induced noise. Although fiber optics cannot replace all of the above functions, they can replace video and digital lines which would reduce design costs and the associated cost of special routing techniques.

A summary of the hazardous/sensitive areas that can benefit from the routing of fiber optic interconnect is given in Table I.

3.3 Routing in Various Aircraft Environments

The environments in which fiber optic interconnects for avionic systems must operate are defined in MIL-E-5400P. The major environments are listed in Table II along with the limits in which the equipment must operate. The worst case environments were chosen as a goal for the utilization of fiber optics.

Special wiring and moisture resistance (SWAMP)

There are six major areas of an airplane in which routing of fiber optics will take place. These areas are:

Nose gear
 Wheel gear
 Radome

- Vertical stabilizer
- Wings and tail section (Leading/trailing edges)
- Pressurized areas
- Fuel areas (wings) and other hazardous areas
- Engine and engine nacelle

These areas all have their own unique environmental conditions, all within the limits specified in MIL-E-5400P. Many of the applications mentioned in the previous section will be routed through these areas and it must be known whether or not fiber optics can survive.

TABLE I: COMPARISON OF ROUTING CONVENTIONAL WIRE. AND FIBER OPTICS FOR SEVERAL HAZARDOUS/SENSITIVE AREAS

	, 1 , .	•
HAZARDOUS/SENSITIVE AREA	CONVENTIONAL WIRE	FIBER OPTICS
Fuel and Other Explosion Areas	Metal Conduit with Teflon Impregnated Glass Fiber Liner	No Special Routing Provisions
High Temperature	 Route Wires Outside of Thermal Extremes Maximize Spacing from Heat Generating Parts 	 Fibers Can Be Routed into High Temp. Areas with Proper Cladding Sources/Detectors Suspect
Outer Skin of Composite Materials	 Protection Against EMI Susceptibility Guard Against Radiation Transmission Protection Against Radiation Damage 	No Special Precautions Except Under Radiation Environment
High Energy Emission	 Balanced Circuits Minimize Coupling Bandwidth Limited 	No Special Provisions
High Contamination	 Do Not Route Near Jubing Connectors 3" from Hydraulic Lines 6" from Fuel/Oxygen Lines 	Same Basic Provisions as Conventional Wire
Sensitive Circuits	 Must be Routed Separately Shielding/Grounding 	 Can be Routed in Same Bundle No Shielding Necessary

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TABLE II: MAJOR ENVIRONMENTAL REQUIREMENTS PER MIL-E-5400P

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REQUIREMENT	100,000 Ft.	-54 ^o C to +125 ^o C (+150 Intermittent)	MIL-STD-454, Requirement 45	Figure 3, MIL-E-5400P	Figure 2, MIL~E-5400P (105 at 2KH≢, Max.)	18 Impact Shocks of 15 g.	"As In Operational World"	No Fungus Growth in Tropical Environments	Exposure to Salt-Sea Atmosphere	No Ignition
ENVIRONMENT	Altitude	Temperature	Corona	Temperature - Humidity	Vibration	Shock	Sand and Dust	Fungus	Salt - Atmosphere	Explosive Conditions

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A matrix of aircraft areas (including composite material structures) as a function of environment is shown in Table III. A comparison of each environment was made as a function aircraft location, comparing fiber optics to conventional wiring. In the matrix, a benefit showed up as a (+), a drawback or item requiring special routing considerations, was indicated by a (-) and a blank meant that there was no advantage of one technology over another. In most cases, fiber optics is shown to behave better than conventional wiring mainly because of the absence of electrical current and the fact that the glass has a high transition temperature. The main drawback is that moisture can induce cracking in fibers when the fiber is in a stressed condition (such as at a bend radius).

Because the environmental conditions in which the interconnects must operate are known and controlled by specifications, the major question to be resolved is - can the individual components survive in the various aircraft locations and environments? This subject is addressed in the next section.

3.4 Component Selection

While the basic advantages of fiber optics as a technology are well known, the detailed parameters of the components making up the fiber optics systems are generally either obscured in various vendor specifications or left out completely.

• The light output (optical power) of optical sources is a major parameter to consider in any system design. This parameter is quite sensitive to temperature and aging effects and this sensitivity varies from type to type and from manufacturer to manufacturer. The lower power edge emitters and cell type devices have a higher reliability record and are considerably less sensitive to temperature.

Injection lasers on the other hand are quite temperature sensitive, have a narrow temperature operating band, and are still subject to sudden catastrophic failure in seemingly well designed systems.

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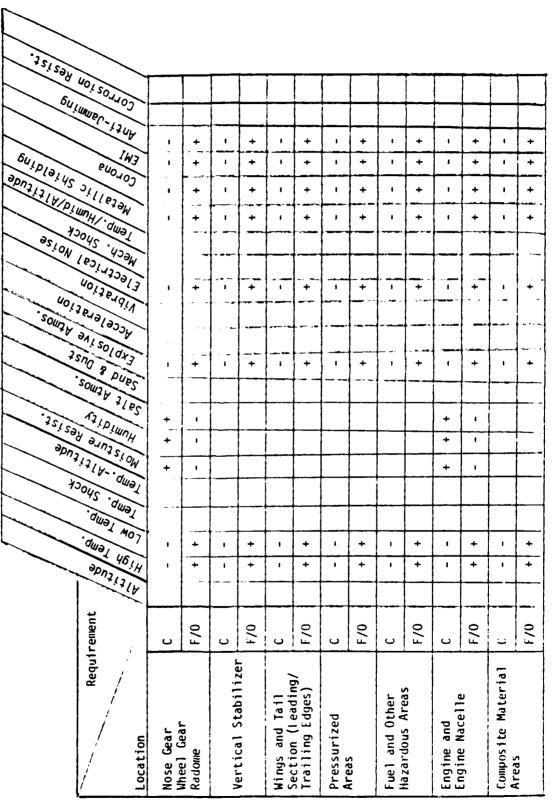


TABLE III. ENVIRONMENTAL REQUIREMENTS VERSUS AIRCRAFT LOCATION

Detectors used are of two general types: PIN and APD. The PIN type is quite stable, even being used as a reference standard for optical power measurement, while the APD may have from 100 to 600 times the gain of the PIN diode. Detection sensitivity (gain) is plagued with extreme gain vs. temperature sensitivity and a high noise figure at high gain settings. Reliability of both devices is good.

Fiber optic connectors are being rapidly developed by many of the old line connector companies as well as a few new ones. While parametric data on the materials used in these connectors is available, the variations in optical parameters to be expected during mechanical and environmental stress have not yet been documented so that operating life and performance degradation data are virtually unknown. While fiber bundle connectors appear to be more forgiving in terms of alignment tolerance, other characteristics such as high insertion and connector loss may relegate bundle technology to that of a lst generation technology only.

Fiber optics cable optical parameters are based primarily upon the materials used for core and cladding (in the case of step index fibers), but changes in these parameters due to mechanical and environmental stresses are for the most part not too well known although studies are in progress, particularly with respect to radiation effects. Cold weather operation of some plastic clad silica fibers seems to be marginal, reportedly due to microbends caused by TC differences in the core and cladding. Data on the effects of shock and vibration are particularly lacking and must be characterized before the full potential of fiber optics can be exploited.

Table IV lists the main advantages and disadvantages of fiber optic components plus an outlook for resolving the major problems. It is shown that the limiting factors are not the cables but the electro-optic devices, which are now very temperature sensitive. Improvements are expected to be made in all areas so that fiber optics can be successfully utilized in most military aircraft applications by the mid-1980's.

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	COMPONENT	ТҮРЕ	ADVANTAGES	DI SADVANTAGES	FUTURE OUTLOOK (1980-1985)
·····	Source	Injection Lasers	Gallium Arsenide devices High power 1-10 MW	Stability (Operating Point) vs. Temperature Life vs. Temperature Coupling Loss to Cable	Both life & stability are improving
		Edge or Well Emmitters	Stability Life	Low Power 10µW - 1MW	Higher power devices becoming available
	Detector	NId	Silicon devices Stable Low Noise	Lower Sensitivity	Gradual improvement
·····		APD	Sens itivity	Operating Point Instability	Gradual improvement
<u> </u>	Connector	Bundle	Available to a Mil Spec in single termination form	Termination time high Losses 3-5dB	Multi-terminal connec- tors becoming available
		Single Fiber	Low loss	Cost, lack of Availability, Alignment critical	Multi-terminal connec- tors becoming available
		Conventional Wire	Available at low cost		Mature technology
	Cable	Bundle	Redundant paths Multiple sources Low insertion loss	Higher cost Higher loss Cannot be spliced	Will be a limited usage item
		Single Fiber	Low cost Low loss	High insertion loss Termination difficult	Usage going up Prices going down
		Wire	Can be spliced and coupled	EMI Higher cost Higher weight	Mature technology
					-

TABLE IV. FIBER OPTIC COMPONENT OUTLOOK

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3.5 General Routing Considerations

The major portion of this report has dealt with the subject of what applications and in which locations can fiber optics be successfully used. There are other considerations, however, to the successful implementation of fiber optics in an airframe. These considerations are discussed in this section.

3.5.1 Handling During Routing

During the installation process, the cable must be routed through conduit, bulkhead fittings, and around bulkhead grommets without damage. Damage could occur due to tensile breakage, impact, bend stress, or scraping, or by contaminating the prepared contact surfaces.

The protection of the contact surfaces from contamination or scratches requires capping of the connector if installed. Where the cable without connector must be pulled through conduit or bulkheads, the contact ends must be protected by covering each prepared surface with a lintfree cloth patch and tape or shrink sleevings covering the entire cable end for stability. The cable pull cord is the fastener as with a standard cable since the mechanical strength of the cable is as great as standard cabling.

A cable damaged from impact is more critical and, since the damage is unintentional, can be installed without detection. Only attention can prevent this type of damage completely. The construction of the cable types being used with strength members provides protection from many minor impacts. Installation within cables of standard electrical wiring further reduces the chance of such damage. Caution during installation and a post installation continuity check are sufficient checks to assure adequate installation.

Fiber optic cables can withstand the same bend stresses that electrical cables can. It is only at the ends, where stress concentrates due to connector hardware or the pull through process, that extra protection is required. Surface protection, or connector and backshell hardware, provides sufficient protection to prevent such inadvertent damage.

Scraping is seldom a problem and, since the jacket of fiber optics cable does not serve as a dielectric, only the integrity of the strength members under the jacket and the optic member need be of concern. Examination of the cable and continuity of the conductor is necessary to determine that no damage has occurred.

3.5.2 Installation Hardware

The standard electrical hardware is designed to prevent dielectric damage to electrical wiring. Hardware is available for each of the airplane areas. If the material strengths of the fiber optics cables are equivalent to the electric cable insulation, then equal performance will be obtained.

Additional installation and field repair hardware will be identified in subsequent phases of this program.

3.5.3 Physical Damage Prevention

Like conventional wire, fiber optics must use standard practice to prevent physical damage in the routing. These general practices will include:

- Route wiring to avoid damage from being stepped on, being used as handholds or support for equipment, and being damaged from cargo stowage and shifting.
- Where wiring passes through cutouts or holes in structures, specify that
 .25 inch minimum clearance be maintained. For applications using a clamp,
 grommet, or adapter close to the cutout, .125 inch clearance is recommended,
 with the design minimum .06 inch. Allowance should be made for clamp
 tolerances, possible movement due to acceleration or vibration, and for
 rough handling during installation and maintenance.
- Provide sufficient clearance to prevent the chafing of wiring against any object in the maximum envelope of movement due to gravity, acceleration, or vibration.
- Route wiring at least three inches away from control cables if possible. If this cannot be done, specify the minimum allowable spacing on the engineering drawing; specify rigid support of wiring and, if necessary, provide special mechanical or electrical protection between wiring and control cables.

3.5.4 Flight Vehicle Routing

As with conventional wiring, fiber optic systems incorporating redundant systems must be separated to minimize the effects of fire, explosion, or other damage which may take a system out of service. Other critical systems which should have separate bundle routing include:

- Electrical "Fly-By-Wire" flight control systems.
- Automatic flight controls
- Stability augmentation
- Stabilizer trim control
- Electroexplosive devices
- Engine controls
- Fire detection
- Fire extinguishing
- Fuel firewall valves
- Hydraulic fluid cutoff valves

Special routing considerations for flight vehicle equipment include:

- Route wiring to the pilot's and copilot's flight instruments separately.
- Do not route interphone wiring in a bundle containing wires from other systems except in the control columns. Service interphone wiring may be routed with passenger address wiring. In wings and nacelles this wiring may be routed with low power dc circuits.
- Route wiring to the control panels on the pilot's control stand to permit rearrangement of the panels without rewiring.
- Separate the generator control wires into individual bundles for each generator.
- Do not route wiring in emergency exit cut in or cut out areas.
- Route wiring in wheel wells and on landing gear to prevent damage from rocks, ice, and mud.

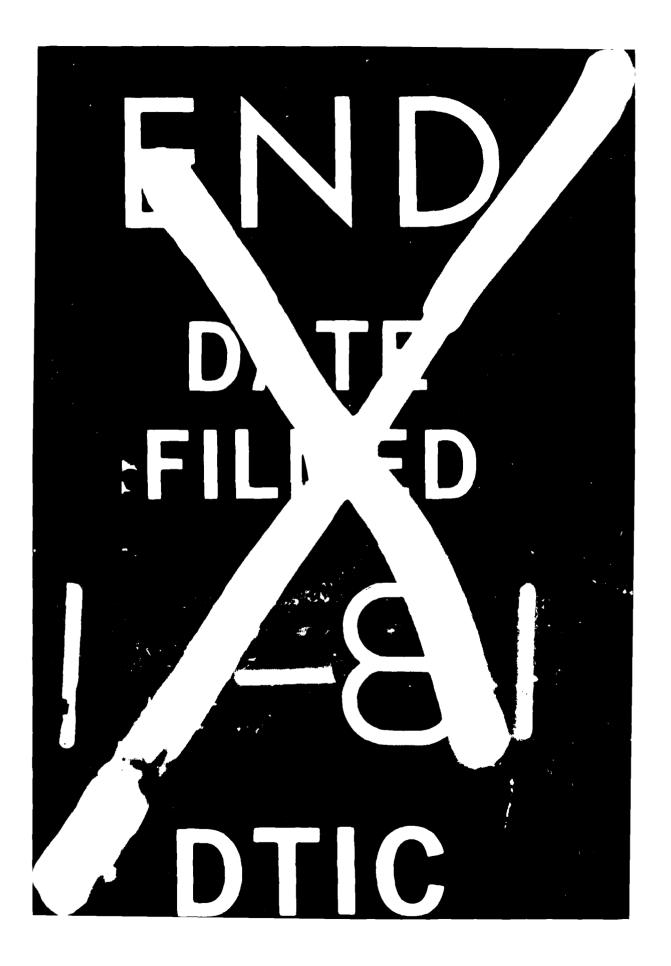
3.5.5 Repairability

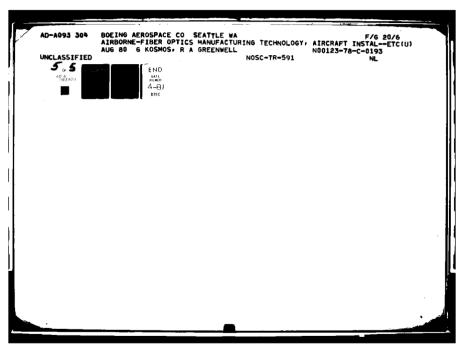
Rework of an electrical cable can result from system redesign, replacement of components, damage, or random failures of parts. Provision is made for rework in both the component design and the cable installation for standard electrical cables. Contacts are removable from the connector to minimize replacement cost. The contacts are fastened to the wire by solder or by crimping. All of the steps can be accomplished with simple, handheld tools.

To perform the same functions on fiber optics cables, a more complicated process must be followed. In most cases, an epoxy glue is used to fasten the contact to the fiber optic conductor. The strength member must be fastened to the connector as an extra step which is not required for standard wiring. Some of the fiber optic connectors do not even have removable center contacts, requiring a "cut and throw" process to replace the contact. The contact face then must be polished or a clean face produced by fracturing, both procedures requiring a special tool.

To be economical from a production and in-service rework viewpoint, the epoxy step, as well as the fracture or polish step, must be eliminated or speeded up. The strength member fastening could be made as rapid as fastening a shield to a standard connector.

Because this termination activity is more complex than standard wire, special provisions must be made in the routing to allow adequate room and safety to perform this function. Similar consideration should also be given to the splicing of the fibers. Dedicated splicing areas should be defined in the initial routing analysis in order to minimize the impact of fiber breakage on the overall system availability.





SUPPLEMENTARY

INFORMATION

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The following pages are blanks:

Pages 4, 22, 106, 118, 224, 246, 264, 288 and 320

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