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6 DYNAMICS OF THE PIN PALLET RUNAWAY ESCAPEMENT.

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CITY COLLEGE OF NEW YORK

F. R. TEPPER
ARRADCOM

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US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
LARGE CALIBER
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20. The simulation is applied to the timing of the mechanism of the M525 fuze with an assumption of constant input torque to the escape-wheel. The influence of changes on such parameters as escape-wheel torque, pallet moment of inertia, center distance, pallet radius, etc., are explored in detail by appropriate computer runs. Agreement has been found with existing experimental data. Finally, recommendations for continued work are given.

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INTRODUCTION

It was the aim of the present investigation to develop a realistic and workable computer simulation of the dynamic behavior of the pin pallet runaway escapement which can be used in the analysis and synthesis of various safing and arming devices. This goal has been achieved.

This report describes and formulates the dynamics of the various regimes of motion which form the basis for the simulation. The computer program and its controls are presented in detail. The simulation is applied to the time delay mechanism of the M525 fuze and the influence of various parameter changes is explored. Previous experimentation and practical experience with this mechanism confirmed the results of the computations. Finally, recommendations for continued work are given. The previous work done in this field is listed in references 1-15.

SIMULATION OF PIN PALLET RUNAWAY ESCAPEMENT

The present effort on the pin pallet escapement represents an extension of the work of M. E. Anderson and S. L. Redmond (ref. 7). New methods of contact kinematics for coupled motion, of contact sensing, and of computational controls are developed.

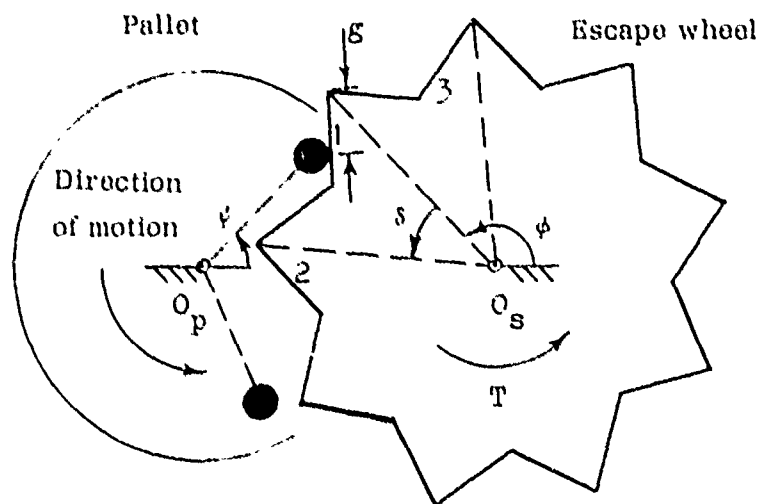


Figure 1. Coupled motion

The following outlines the overall assumptions and derivations for the various regimes of motion. A detailed description of the actual computer program and its controls is then given.

Coupled Motion

Figure 1 shows the upper pallet pin¹ being driven in coupled motion by tooth no. 1 of the escape wheel (top contact). The escape-wheel angle ϕ is defined by the line from the escape-wheel pivot O_s to the tip (without radius) of the contacting tooth (or the one about to make contact) and the line connecting O_s to the pallet pivot O_p . Similarly, the angle ψ , which is defined by the line from O_p to the active pallet pin center (top or bottom) and the center line, describes the motion of the pallet. The escape wheel is driven by the constant moment T in the positive direction of rotation. While it is assumed that friction acts on the pallet pin/escape wheel tooth interface, it is neglected at both pivots since investigation showed that its effects are negligible when the pivots are of the usual small diameter.

The quantity g , which represents the distance from the contact point to the tip of the escape-wheel tooth, is used to determine the end of coupled motion. Appendix A contains derivations for this expression, as well as all other kinematic quantities associated with coupled motion. Appendix B, with the help of appendix C, gives the derivation of the differential equation of coupled motion in terms of the escape-wheel angle ϕ (eq. B-10).

Free Motion

When coupled motion is finished (i.e. $g = 0$) or when separation of contact occurs after impact, the escape wheel and pallet move independently of each other in free motion. Figure 2 shows this free motion for the bottom phase of the action, i.e. the bottom pallet pin is about to make contact with tooth no. 2 of the escape-wheel. The constant torque T continues to act on the escape-wheel, while the motion of the pallet depends only on its initial conditions. Again, any frictional retarding moments at the pivots are neglected. Position sensing during free motion is based on g' , the distance of the pallet pin center from the tip of the escape-wheel

¹This report uses the word upper when referring to entrance motion and lower when referring to exit motion.

tooth (parallel to the face of the tooth) and f , the distance between the pallet pin and tooth surfaces normal to the tooth). Expressions for these quantities are derived in appendix D. The differential equations for the free motion of the pallet and the escape-wheel are derived in appendix E.

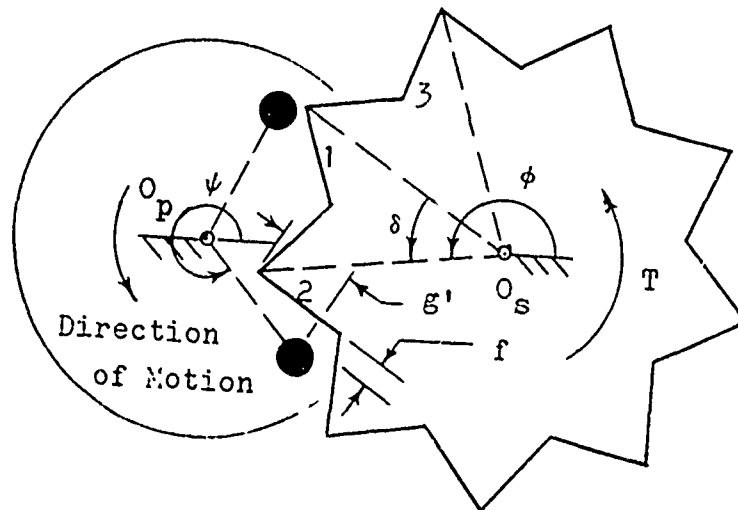


Figure 2. Free motion

Impact

Impact follows free motion whenever f equals zero, g' is smaller than zero, and the relative velocity between the contacting surfaces warrants it. Such an impact usually reverses the motion of the pallet (fig. 3) and under certain circumstances also reverses the motion of the escape-wheel temporarily. While the impact equations, derived in appendix F, allow for both normal and tangential impulses to produce changes in the angular momenta of the pallet and escape-wheel, the computer program presented here neglects the tangential impulse for the sake of simplicity. The classical coefficient of restitution formulation is used to account for the energy loss during impact.

Figure 4 shows free motion for the subsequent top phase of the motion, i.e. the top pallet pin is about to make contact with tooth no. 3 of the escape-wheel.

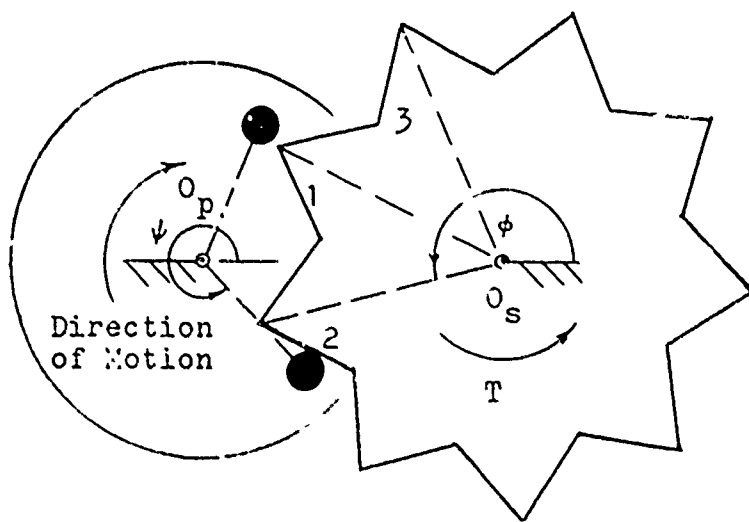


Figure 3. Impact

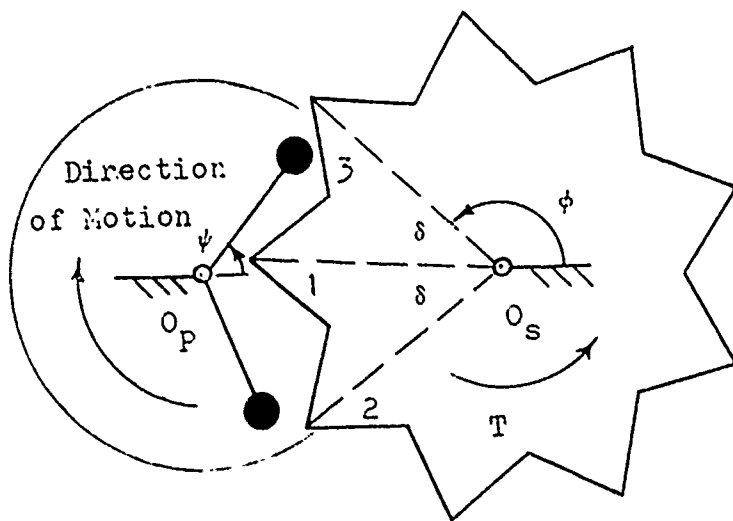


Figure 4. Impending top contact

All kinematic and dynamic expressions are derived in such a manner that they are valid for top and bottom action. The simulation recognizes only contact on the front faces of the escape-wheel teeth. Pathological conditions, such as impact on the tips or the back faces of the escape-wheel teeth are not considered. (The control quantities g and g' make it clear that when such a condition exists the computation can be discontinued.)

Escapement Nomenclature

Figure 5 shows a schematic representation of the pin pallet escapement and indicates its basic geometric nomenclature.

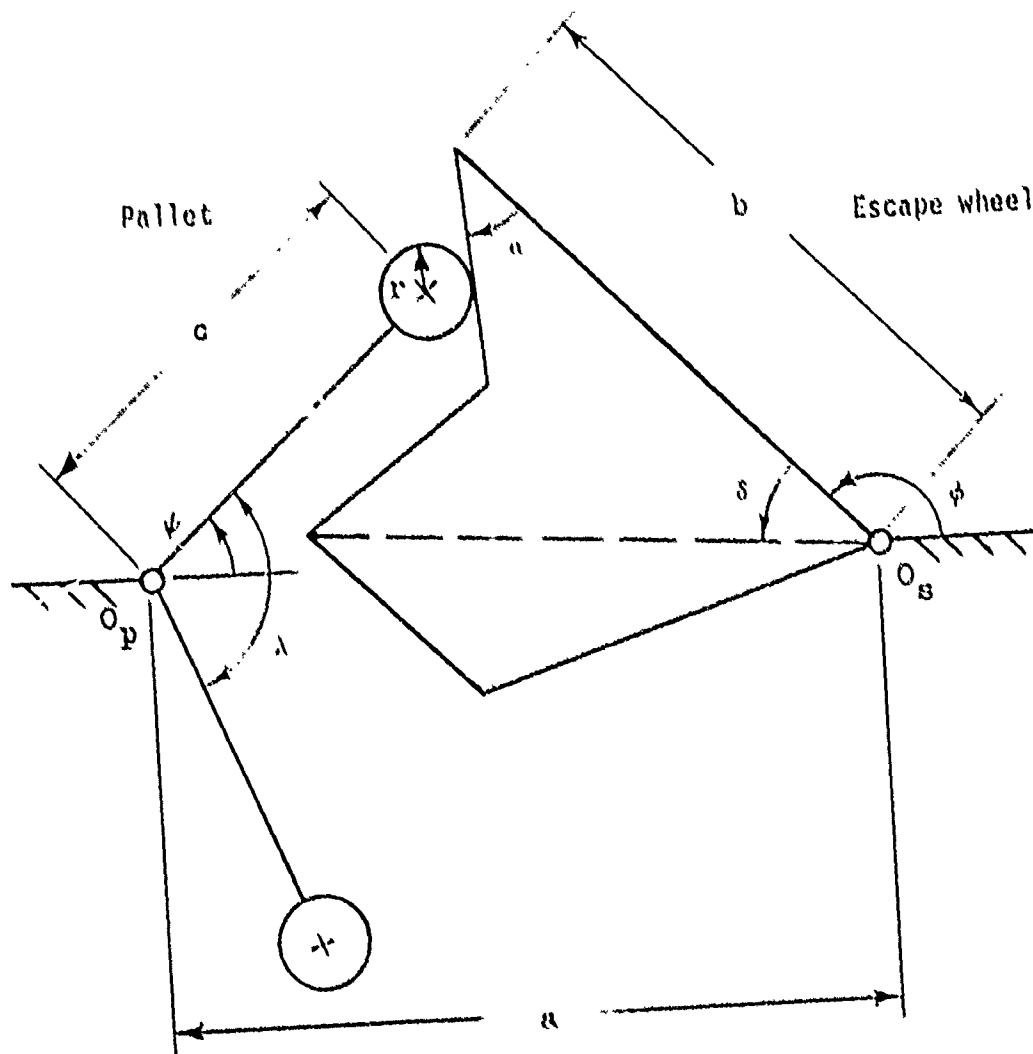


Figure 5. Escapement nomenclature

- a = Distance between pivot points O_p and O_s
- b = Escape wheel radius
- c = Pallet radius (equal on top and on bottom for simplicity)

- r = Pallet pin radius (equal for top and bottom)
- α = Escape-wheel tooth half angle
- δ = Angle between escape-wheel teeth
- φ = Angular position of escape-wheel
- ψ = Angular position of pallet

DESCRIPTION OF COMPUTER PROGRAM

The following gives the essential steps of the computer program as listed in appendix G². The flow chart of the program is shown in figure 6. The choice of variable designations was made in such a way that they differ as little as possible from the nomenclature used in the various derivations in appendixes A to F and H.

The main program starts the simulation with top contact coupled motion at a starting angle $\varphi = 135^\circ$ (called PHID in the computer program) and a cumulative-escape-wheel angle PHITOT of 0° . The choice of this starting angle is connected with the geometry of the example mechanism used ($\varphi_M = 132.487^\circ$ for the example mechanism).

Coupled Motion (location 100)

To solve the differential equation of coupled motion (see equation (B-10) of appendix B) the main program calls on an available fourth-order Runge-Kutta routine.³ The subroutine FCT computes all needed values and presents the second-order differential equation in terms of two first-order ones to RKGS. PHI (1) and PHI (2) represent the angle φ and the angular velocity $\dot{\varphi}$, respectively. The associated subroutine OUTP is responsible for printing out the results of the integration together with the current values of time, g , \dot{g} , ψ , $\dot{\psi}$, and PHITOT. In addition, it has the task of deciding whether coupled motion is to be continued. Coupled motion is continued

a. as long as $g < 0$. (See equation (A.12) and note, that because of the nature of the coordinate system, g is always negative while the pallet pin makes contact with the escape-wheel tooth.) And,

²The program shown is written in FORTRAN for the CDC System at ARRADCOM, Dover, NJ. It is also available in a slightly modified form for the IBM System/360 at the City College of New York.

³RKGS Routine, IBM System/360 Scientific Subroutine Package, (360A-CM-OX3) Version III.

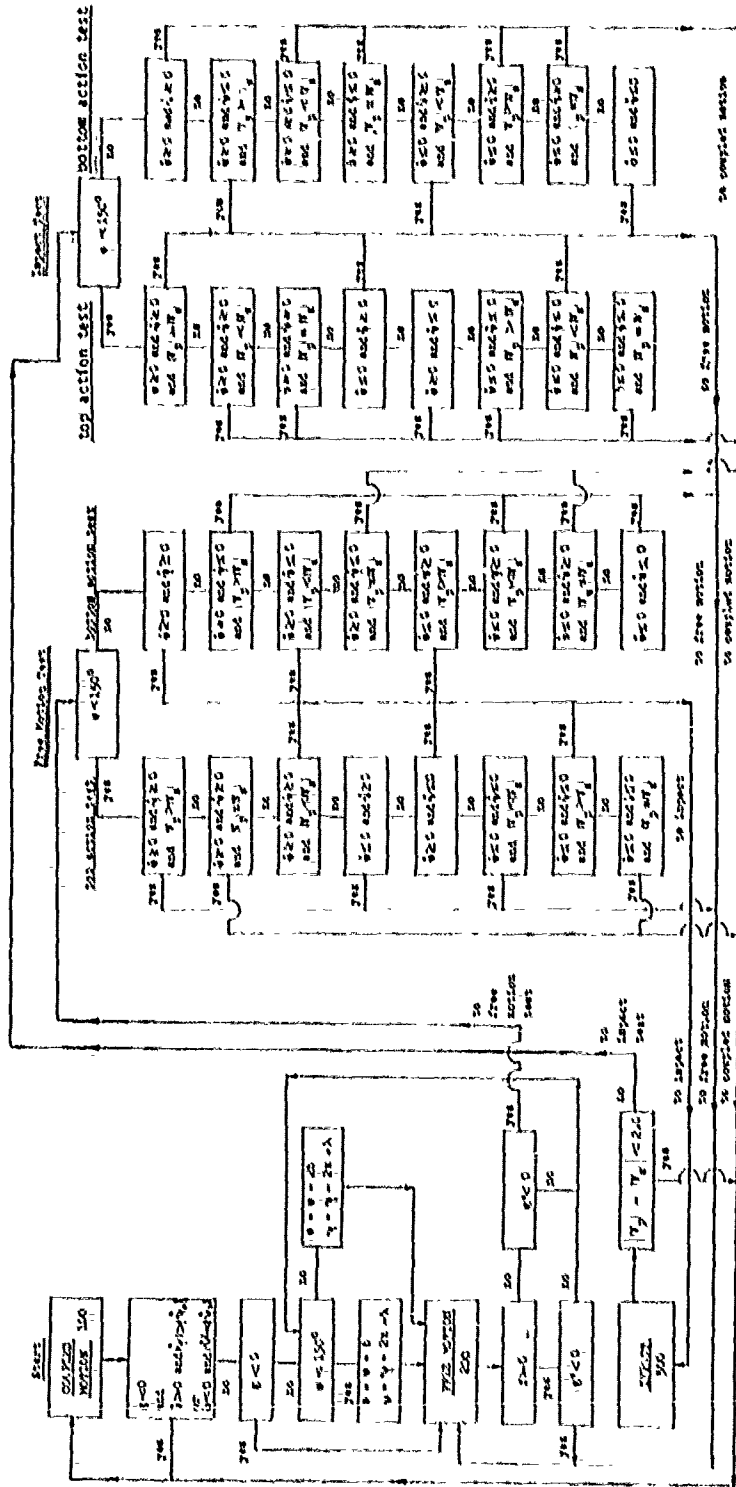


Figure 6. Flow chart for simulation of runway escapement

b. for a positive (counterclockwise) rotation of the escape-wheel, if the succeeding absolute value of $\dot{\psi}$ (DPSI) is larger than the one obtained from the preceding computation (called DPSIP). These values of $\dot{\psi}$ are computed with the help of equation (A.18), which assumes closure. This condition is necessary, since in coupled motion when $\dot{\phi}$ is positive the escape-wheel can only drive the pallet, not slow it down. If such a slowdown is indicated, it means that pallet and escape-wheel have separated and free motion will take place. Or,

c. for a negative rotation of the escape-wheel (which may occur after impact), a succeeding absolute value of $\dot{\psi}$ must be smaller than the preceding one. If for some reason the escape-wheel should speed up and cause the computation to show a larger succeeding value of $\dot{\psi}$, it would also serve as an indication that closure has terminated and free motion has started.

To make this process less sensitive, the last two conditions will only be violated when the absolute magnitude $|\dot{\psi}| \geq 1$ rad/sec.

Thus, when control is returned to the main program, it is either because the pallet pin has left the end of the tooth and there is no further possibility of coupled motion or the pin has disengaged from the inside of the tooth. In either case, free motion results and control is eventually shifted to the subroutine FREE (location 200). This is done directly if $g < 0$. In the case that $g < 0$, the main program must decide whether the preceding computations have been made for top or for bottom action and whether the next contact will occur on top or on bottom. In the sample mechanism, $g = 0$ when ϕ is approximately 146° for top action and approximately 207° for bottom action. (The values of ϕ_0 for top and bottom action are located in the section on the example mechanism). If $\phi \leq 150^\circ$, all possibility for top contact is ended and ϕ must be incremented by the tooth angle δ (see figures 2 and 5), while ψ must be incremented by the angle $(2\pi - \lambda)$. For $\phi > 150^\circ$, top contact is expected at the end of bottom action and ϕ must be decremented by the angle 2δ (see figure 4, where the new top tooth no. 3 comes into action). At the same time, the pallet angle ψ must be decremented by $(-2\pi + \lambda)$. These indexing operations have no effect on the continuous computation of the cumulative escape-wheel angle PHITOT.

Free Motion (Location 200)

After transferring the initial values for time, angles, and angular velocities from the main program, the subroutine FREE computes the subsequent positions and angular velocities of pallet and escape-wheel in free motion according to equations (E.2), (E.3), and (E.7) and (E.8), respectively, for time increments of 10^{-5} seconds. In addition to the above variables, PHITOT is also continually computed and caused to be printed out. The decision, whether or not to remain in this subroutine, is made with the help of the sensing variables, f (according to equation (D-7)) and g' (according to equation (D-11) and now called GP).

If $f > 0$ and $g' \leq 0$, free motion is continued without indexing. If $f > 0$ and $g' > 0$, free motion is also continued, but since contact is no longer possible for the component pair for which the previous computations were made, indexing takes place. This is accomplished in the same manner as described before.

If $f < 0$, control is returned unconditionally to the main program. If it finds that $g' > 0$, indexing takes place and control is given back to the subroutine, FREE. When $f \leq 0$, contact is about to take place or has just occurred. The program must decide whether this contact just represents a close approach, which will be followed by further free motion, whether it represents an impending impact, or whether it is the beginning of coupled motion. To this end, the quantities V_p and V_s (see equations (F.22) and (F.23)) are computed for the top and bottom free-motion tests.⁴ The first three cases of the top free motion test of the main program are illustrated in figure 7. With both angular velocities ($\dot{\phi}$ is PHI (2) and $\dot{\psi}$ is DPSI) positive, the following three possibilities exist:

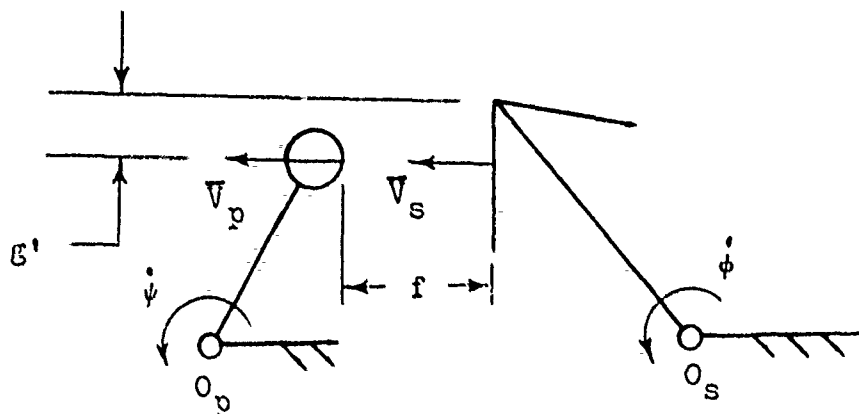
1. If $|V_p| > |V_s|$, the contacting surfaces will separate again, free motion will result, and control must be transferred to subroutine FREE (location 200).

2. If $|V_p| = |V_s|$, the escape-wheel will start driving the pallet in coupled motion, and control must be transferred to subroutine RKGS (location 99 initiates RKGS).

⁴Under the present circumstances, if $\phi < 150^\circ$, only top contact can follow; if $\phi > 150^\circ$, bottom contact will occur.

3. If $|V_p| < |V_s|$, impact will occur, and control must be given to subroutine IMPACT (location 300).

The remainder of the top free motion tests and the bottom free motion tests are constructed along similar lines for different combinations of angular velocity directions.



($\dot{\phi}$ and $\dot{\psi}$ are positive. Distance f is enlarged.)

Figure 7. Top free motion test

Impact (Location 300)

The subroutine IMPACT uses the current values of the angular velocities $\dot{\phi}_i$ and $\dot{\psi}_i$ and computes the post impact angular velocities $\dot{\phi}_f$ and $\dot{\psi}_f$, applying equations (F.20) and (F.21). (Note that the tangential impact has been neglected and, therefore, $E_2 = D_1$ and $F_2 = A_1$).

After control is returned to the main program, it is decided whether free or coupled motion follows the impact. This is accomplished by considering the post-impact contact point velocities, V_p and V_s , in the impact tests, which are similar to the free motion tests.

If the contact velocities are vectorially equal to each other or if the absolute value of the difference of their absolute magnitudes is less than 2.0 in/sec (5.08 cm/sec), control is transferred to coupled motion. If these velocities are such that they indicate a subsequent separation, which is more usual, computation is transferred to free motion.

The computation is terminated when either $t = .1$ seconds or when $\text{PHITOT} \geq 315^\circ$. These conditions are related to the sample mechanism which runs less than .1 seconds for 310° of escape-wheel rotation.

EXAMPLE MECHANISM

The pin pallet escapement of the M525 fuze is used as the example mechanism. The following, first, gives the dimensions of the basic escapement (standard configuration) and then discusses certain other data and computed values which are of importance in the computer simulation.

Dimensions of the Mechanism

The standard geometric configuration has the following dimensions:

- a = .1931 inches (mean center distance) (.4905 cm)
- b = .15838 inches (.40229 cm)
- c = .09683 inches (.24595 cm)
- r = .01365 inches (.03467 cm)
- $\alpha = 40^\circ$

$$\begin{aligned} \beta &= 60^\circ \text{ (see figure H-1 in appendix H)} \\ \lambda &= 109.337^\circ \\ \delta &= 40^\circ \\ N &= 9 \text{ (number of teeth of escape-wheel)} \\ I_P &= .91 \times 10^{-7} \text{ lb-sec}^2\text{-in. (moment of inertia IPAL of pallet)} \\ &\quad (1.03 \times 10^{-8} \text{ N - sec}^2\text{-m}) \\ I_S &= .17 \times 10^{-7} \text{ lb-sec}^2\text{-in. (moment of inertia ISTAR of} \\ &\quad (1.92 \times 10^{-8} \text{ N - sec}^2\text{- m) escape-wheel)} \end{aligned}$$

Gear Train Driving Escapement

The escapement of the M525 fuze is driven by a clock spring through a step-up gear train with a ratio of 45.98. The timing function of the fuze, which involves a delay of between 2 to 4 seconds, is accomplished once the spring driven input gear has rotated through 310° . This corresponds to a 45.98 times-greater escape-wheel rotation. Since the motion becomes stabilized after one cycle of the pallet (corresponding to approximately 40° of escape-wheel rotation), one obtains an excellent idea of the total time by computing the response time for 310° of escapement rotation and multiplying this result by the aforementioned gear ratio (see the section on results for standard configuration).

Standard Torque Used in the Simulation

Measurements on actual fuzes showed that the initial torque on the escape-wheels varied between .0177 (2.000×10^{-3} m-N) and .031 in-lb (3.503×10^{-3} m-N). Since the angle of rotation of the input gear is small, the decrease in torque during the rotation is also relatively small. Therefore, a constant torque was assumed in the simulation. Its standard value was chosen to be .0177 in-lb (2.000×10^{-3} m-N).

Other Dimensions Associated With Standard Configuration

For purposes of control in the computer program the following other dimensions are of interest.

The maximum absolute value-attainable for the dimension g for the given escapement is computed according to equation (H-4) of appendix H:

$$g_{MAX} = -.05467 \text{ inches } (-.1389 \text{ cm})$$

The associated values of the escape-wheel angle φ_M are obtained with the use of equation H-10. For top action

$$\varphi_M = 132.487^\circ$$

Because of this value, initial coupled motion is started at 135° . (See the section on the computer program.) For bottom action, this angle becomes:

$$\varphi_M = 187.518^\circ$$

The corresponding values for the pallet angles ψ_M are found through the use of equation (A.8) appendix A and are computed with $g = -.05467$ and $\alpha = 40^\circ$. For top action,

$$\psi_M = 39.491^\circ$$

and for bottom action,

$$\psi_M = 320.396^\circ$$

These values serve as valuable checks on the computer output.

The escape-wheel angles φ_0 corresponding to $g = 0$, i.e. the position when the pallet pin leaves the tooth in coupled motion, are obtained according to equation (H-12). For top action,

$$\varphi_0 = 146.328^\circ$$

Because of this angle, decisions concerning indexing, the free motion and impact tests are based on whether the angle φ is smaller or larger than 150° . (See the section on the description of the computer program.) For bottom action, this angle becomes

$$\varphi_0 = 206.512^\circ$$

The corresponding pallet angles are

$$\psi_0 = 60.138^\circ \text{ for top action, and}$$

$$\psi_0 = 299.869^\circ \text{ for bottom action, respectively.}$$

Finally, it is important to know the center distance between pallet and escape-wheel for which disengagement will occur. According to equation (G.14)

$$a_{dis} = .208 \text{ inches } (.528 \text{ cm})$$

RESULTS FOR STANDARD CONFIGURATION

Appendix I shows computer output for the first, second and eighth cycles of a run for the standard configuration with a coefficient of friction, $\mu = .3$, and a coefficient of restitution, $\epsilon = .25$ (run no. 46). Table 1 summarizes the results of the first two and one half cycles. In appendix I, a cycle is defined as the interval between first contacts on top. In tables 1 and 3 the interval is between the last contacts on top.) As discussed earlier, top motion in the coupled mode initiates the program. In the subsequent first bottom action, the first impact is followed by free motion while the second impact leads to coupled motion by virtue of the cut-off criterion. Starting with the second top contact, both top and bottom action consists of two impacts followed by free motion. The subsequent third impact produces little rebound of the pallet pin and thus is the beginning of coupled motion which lasts until the pallet pin leaves the tooth.

The various impacts cause reversals in escape-wheel motion. In the actual mechanism, this backward rotation is limited by the possibility of the pin making contact with the backface of the next escape-wheel tooth. The program does not provide for the presence of this condition and any contact of this type makes itself known only if during or after the first impact, the escape-wheel angle $\phi < 132.487^\circ$ for top action or $\phi < 187.518^\circ$ for bottom action. If such a reversal of the escape-wheel takes place during coupled motion, g will be less than $-.05467$ in. ($-.1284$ cm). (See the section on other dimensions of the standard configuration for discussion of the above values.)

Inspection of table 1 shows that this condition first occurs in cycle no. 3 for top contact, i.e. $\phi = 132.480^\circ$. Table 2 gives the values of the maximum reversal angles for the first eight cycles. While these reversals of the escape-wheel angle never reach critical values for bottom action, they exceed critical values a number of times for top action. (The geometry lends itself more for this condition with respect to top action.)

The fact that the absolute value of g_{MAX} will be exceeded in certain configurations will be accepted or more dissipative values for μ and ϵ will have to be used⁵. The discussion in the section on the influence of parameter changes in the total fuze time will show that a slight increase of the center distance decreases the absolute value of g at maximum reversal to well below g_{MAX} . This correlates with the results for $\mu = .3$ and $\epsilon = 0$ given below.

Table 1 shows that the stability of motion is essentially established during the first cycle. The time interval per cycle, now counted between the instants when the pallet pin leaves the top tooth, is shown to be .00774 and .00773 seconds. Subsequent intervals (not shown here) are .00773, .00775, .00785, .00784, and .00773 seconds. The total time of the fuze may be obtained with the help of the time at PHITOT $\approx 310^\circ$. Appendix I shows that $t(310.362^\circ) = .06058$ seconds. Thus, the total fuze delay time becomes $.06058 \times 45.98 = 2.79$ seconds. (See the section on the example mechanism.) This result is well within the fuze requirement of between 2 to 4 seconds.

Appendix J gives portions of the computer output when the standard configuration was run with $\epsilon = 0$, while $\mu = .3$ was kept (run no. 70). Table 3 summarizes the events of the first $3\frac{1}{2}$ cycles and table 4 lists the maximum reversal values of the escape-wheel for eight cycles.

As expected, the fully inelastic coefficient of restitution causes the initial impacts to be followed by coupled motion. Now, $g < g_{MAX}$ at all times. (Again, the reversals are smaller for bottom action.) As in the first program above, the motion stabilizes immediately with cycle intervals of .00725, .00730 and .00725 seconds. Subsequent intervals, not shown here, are .00726, .00729 and .00726 seconds. The total fuze delay time is computed with $t(\text{PHITOT} = 310.600^\circ) = .05699$ seconds (see appendix J). This results in 2.62 seconds.

⁵Since no high speed motion pictures of the M525 are available, it is not known whether contact with the backside of the escape-wheel tooth is ever made.

Table 1. Summary of events in the first 2 cycles for standard configuration with $\mu = .3$ and $c = .25$ (Program No. 46)

| Type of action | Escape-wheel angle φ (deg) | Time (sec) | Time interval (sec) | Total escape-wheel angle (deg) |
|---|------------------------------------|----------------------|----------------------|--------------------------------|
| Top: start of coupled motion | 135.000 | 0.00000 | | 0.000 |
| start of free motion (end of tooth) | 146.491 | 0.00340 ¹ | | 11.491 |
| Bottom: impact followed by free motion | 194.179 | 0.00382 | | 19.179 |
| maximum return motion (free) | | | | |
| continued free motion | 192.911 | 0.00402 | | 17.911 |
| impact followed by coupled motion (cut-off criterion: $\ V_p\ - \ V_S\ < 2$) | 193.366 | 0.00415 | | 18.366 |
| maximum return motion (coupled) | 193.281 | 0.00425 | | 18.281 |
| start of free motion (end of tooth) | 206.844 | 0.00645 | | 31.844 |
| Top: impact followed by free motion | 135.522 | 0.00688 | | 40.522 |
| maximum return motion (free) | | | | |
| continued free motion | 133.361 | 0.00714 | | 38.361 |
| impact followed by free motion | 133.435 | 0.00720 | | 38.435 |
| maximum return motion | 133.214 | 0.00724 | | 38.214 |
| impact followed by coupled motion (cut-off criterion) | 133.214 | 0.00724 | | 38.214 |
| maximum return motion (coupled) | 133.540 | 0.00753 | | 37.540 |
| start of free motion (end of tooth) | 146.514 | 0.01114 ² | 0.00774 ³ | 51.514 |
| Bottom: impact followed by free motion | 193.802 | 0.01154 | | 58.802 |
| maximum return motion (free) | | | | |
| continued free motion | 192.321 | 0.01176 | | 57.321 |
| impact followed by free motion | 192.803 | 0.01189 | | 57.803 |
| maximum return motion (free) | | | | |
| continued free motion | 192.749 | 0.01193 | | 57.749 |
| impact followed by coupled motion (cut-off criterion) | 192.790 | 0.01197 | | 57.790 |
| start of free motion (end of tooth) | 206.768 | 0.01417 | | 71.768 |
| Top: impact followed by free motion | 135.519 | 0.01460 | | 80.519 |
| maximum return motion (free) | | | | |
| continued free motion | 132.297 | 0.01487 | | 78.297 |
| impact followed by free motion | 133.394 | 0.01493 | | 78.394 |
| maximum return motion (free) | 133.165 | 0.01497 | | 78.165 |
| impact followed by coupled motion (cut-off criterion) | 133.165 | 0.01497 | | 78.165 |
| maximum return motion (coupled) | 132.480 | 0.01526 | | 77.480 |
| start of free motion (end of tooth) | 146.496 | 0.01887 ⁴ | 0.00773 ⁵ | 91.496 |

¹Start of first cycle

²End of first cycle, start of second cycle

³Time interval for first cycle

⁴End of second cycle

⁵Time interval for second cycle

Table 2. Maximum reversal angles and associated values of g for standard configuration with $\mu = .3$ and $\varepsilon = .25$ (Program No. 46)

| Cycle No. | Top action | | Bottom action | |
|-----------|--|--------------------------------|--|------------------------------------|
| | Maximum reversal angle, φ ($\varphi_M = 132.487^\circ$) | g (in.) ($g_M = -.05467$) | Maximum reversal angle, φ ($\varphi_M = 187.518^\circ$) | g^1 (in.) ($g_M = -.05467$) |
| 1 | | | 192.910 | |
| 2 | 132.540 | -.0547 (-.1389 cm) | 192.321 | |
| 3 | 132.480 | -.0549 (-.1394 cm) | 192.303 | |
| 4 | 132.312 | -.0555 (-.1410 cm) | 192.320 | |
| 5 | 132.305 | -.0555 (-.1410 cm) | 192.485 | |
| 6 | 132.094 | -.0562 (-.1427 cm) | 191.837 | |
| 7 | 131.593 | -.0580 (-.1473 cm) | 192.078 | |
| 8 | 132.634 | -.0543 (-.1379 cm) | 192.315 | |

¹Not applicable. Occurs during free motion.

Table 3. Summary of events in the first 3½ cycles for standard configuration
with $\mu = .3$ and $\varepsilon = 0$ (Program No. 70)

| Type of action | Escape- wheel angle φ (deg) | Time (sec) | Time interval (sec) | Total escape- wheel angle (deg) |
|---|--|----------------------|---------------------------|---------------------------------------|
| Top: start of coupled motion | 135.000 | 0.00000 | | 0.000 |
| start of free motion | 146.491 | 0.00340 ¹ | | 11.491 |
| Bottom: impact followed by coupled motion | 194.179 | 0.00382 | | 19.179 |
| maximum return motion (coupled) | 193.776 | 0.00404 | | 18.776 |
| start of free motion | 206.789 | 0.00622 | | 31.789 |
| Top: impact followed by coupled motion | 135.416 | 0.00665 | | 40.416 |
| maximum return motion (coupled) | 133.957 | 0.00711 | | 38.957 |
| start of free motion | 146.743 | 0.01065 ² | 0.00725 ³ | 51.743 |
| Bottom: impact followed by coupled motion | 193.636 | 0.01104 | | 58.636 |
| maximum return motion (coupled) | 193.083 | 0.01129 | | 58.083 |
| start of free motion | 207.171 | 0.01354 | | 72.171 |
| Top: impact followed by coupled motion | 135.168 | 0.01395 | | 80.168 |
| maximum return motion (coupled) | 133.504 | 0.01443 | | 78.504 |
| start of free motion | 146.383 | 0.01795 ⁴ | 0.00730 ⁵ | 91.383 |
| Bottom: impact followed by coupled motion | 194.198 | 0.01837 | | 99.198 |
| maximum return motion (coupled) | 193.698 | 0.01861 | | 98.698 |
| start of free motion | 206.601 | 0.02077 | | 111.601 |
| Top: impact followed by coupled motion | 135.600 | 0.02121 | | 120.600 |
| maximum return motion | 134.171 | 0.02167 | | 119.171 |
| start of free motion | 146.856 | 0.02521 ⁶ | 0.00725 ⁷ | 131.856 |

¹ Start of first cycle

² End of first cycle, start of second cycle

³ Time interval for first cycle

⁴ End of second cycle, start of third cycle

⁵ Time interval for second cycle

⁶ End of third cycle

⁷ Time interval for third cycle

Table 4. Maximum reversal angles and associated values of g for standard configuration with $\mu = .3$ and $\epsilon = 0$ (Program No. 70)

| Cycle No. | Top action | | Bottom action | |
|-----------|--|--------------------------------|--|------------------------------------|
| | Maximum reversal angle, φ ($\varphi_M = 132.487^\circ$) | g (in.) ($g_M = -.05467$) | Maximum reversal angle, φ ($\varphi_M = 187.518^\circ$) | g^1 (in.) ($g_M = -.05467$) |
| 1 | | | 193.776 | -.0401 (-.1019 cm) |
| 2 | 133.957 | -.0495 (-.1257 cm) | 193.083 | -.0418 (-.1062 cm) |
| 3 | 133.504 | -.0512 (-.1300 cm) | 193.698 | -.0403 (-.1024 cm) |
| 4 | 134.171 | -.0487 (-.1237 cm) | 192.883 | -.0423 (-.1074 cm) |
| 5 | 133.466 | -.0513 (-.1303 cm) | 193.659 | -.0404 (-.1026 cm) |
| 6 | 134.170 | -.0487 (-.1237 cm) | 192.883 | -.0423 (-.1074 cm) |
| 7 | 133.466 | -.0513 (-.1303 cm) | 193.659 | -.0404 (-.1026 cm) |
| 8 | 134.170 | -.0487 (-.1237 cm) | 192.884 | -.0423 (-.1074 cm) |

INFLUENCE OF VARIOUS PARAMETER CHANGES ON THE TOTAL FUZE TIME

The following reports on the results of numerous computer runs in which a single input or geometric parameter was varied in order to determine its influence on the total fuze time. In all cases, the individual changes were made with respect to the standard configuration in the section on the example mechanism, with $\mu = .3$ and $\epsilon = .25$.

Influence of Escape-Wheel Torque

Figure 8 shows the influence of the escape-wheel torque on the fuze time. One may compare these timing results with those obtained from the well-known empirical expression:

$$t_2 = t_1 \sqrt{\frac{T_1}{T_2}}$$

If t_1 and T_1 represent fuze time and torque, respectively, as associated with the standard configuration, one obtains from the above:

$$\text{For } T_2 = .75 T_1, \quad t_2 = 2.79 \sqrt{\frac{1}{1.25}} = 3.22 \text{ seconds}$$

$$\text{For } T_2 = 1.25 T_1, \quad t_2 = 2.79 \sqrt{\frac{1}{1.25}} = 2.49 \text{ seconds}$$

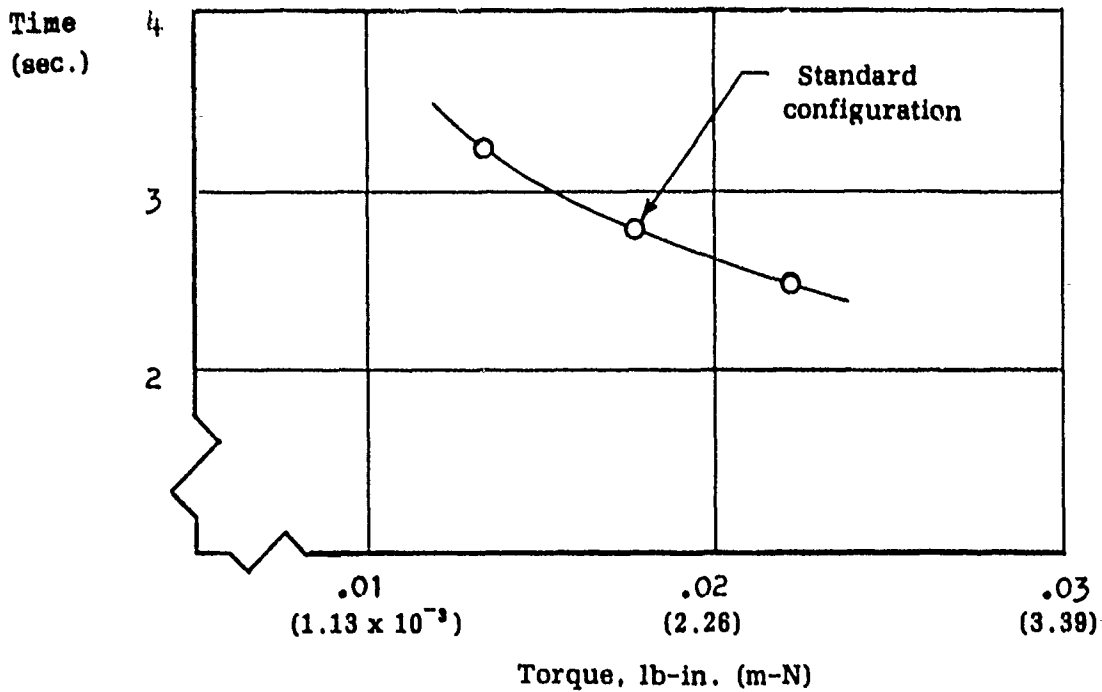
The results of the simulation (runs 47 and 48 of table of figure 8) show excellent agreement with the above. The empirical relationship has been confirmed time and again by experiment.

Influence of Pallet Moment of Inertia

Figure 9 shows that the total fuze delay time increases with an increase of the pallet moment of inertia. The ratio of any two fuze periods is approximately proportional to the ratio of the square roots of the associated pallet inertias. These results are confirmed by the experiments of Anderson and Redmond (ref. 7).

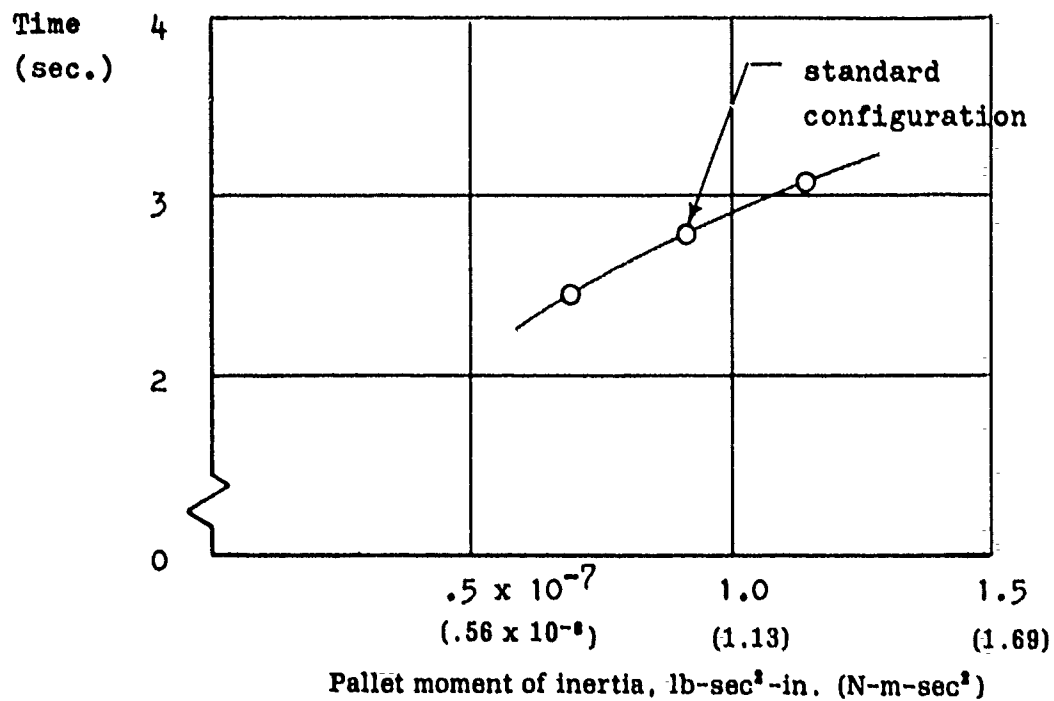
Influence of Pallet Escape-Wheel Center Distance

Figure 10 indicates, for the range explored, that the fuze time increases as the center distance a is increased. For a total increase of .007 inches (.018 cm), the time increase is approximately 7%. This result is



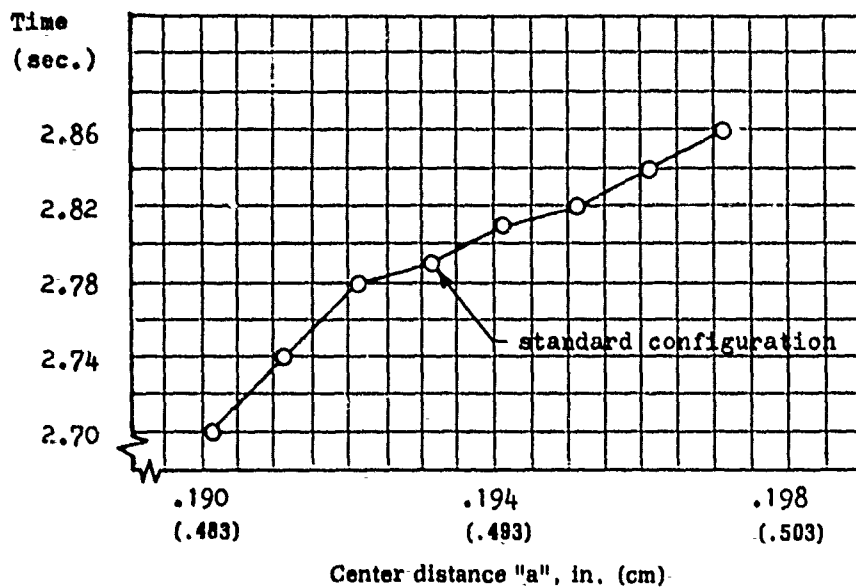
| Run no. | Torque (lb-in.) | Total Fuze Time (sec.) |
|---------|---|---------------------------|
| 48 | .0133 (75% of St.) $(1.503 \times 10^{-3} \text{ m-N})$ | 3.23 |
| 46 | .0177 (St.) $(2.000 \times 10^{-3} \text{ m-N})$ | 2.79 |
| 47 | .0221 (125% of St.) $(2.497 \times 10^{-3} \text{ m-N})$ | 2.50 |

Figure 8. Influence of escape-wheel torque on fuze delay time



| Run no. | Moment of inertia of pallet (lb-sec ² -in) | Total fuze time (sec.) |
|---------|--|------------------------|
| 57 | .68 x 10 ⁻⁷ (7.68 x 10 ⁻⁸ N-m-sec ²) | 2.46 |
| 46 | .91 x 10 ⁻⁷ (std. conf.) (1.027 x 10 ⁻⁸ N-m-sec ²) | 2.79 |
| 58 | 1.137 x 10 ⁻⁷ (1.283 x 10 ⁻⁸ N-m-sec ²) | 3.07 |

Figure 9. Influence of pallet moment of inertia on fuze delay time



| Run no. | Center distance "a" (in.) | Total fuze time (sec.) |
|---------|----------------------------------|---------------------------|
| 55 | .1901 | 2.70 |
| 54 | .1911 (.4854 cm) | 2.74 |
| 53 | .1921 (.4878 cm) | 2.78 |
| 46 | .1931 (std. conf.) (.4905 cm) | 2.79 |
| 49 | .1941 (.4930 cm) | 2.81 |
| 50 | .1951 (.4956 cm) | 2.82 |
| 51 | .1961 (.4981 cm) | 2.84 |
| 52 | .1971 (.5006 cm) | 2.86 |

Figure 10. Influence of pallet escape-wheel center distance on fuze delay time

generally confirmed by the experimentation of Anderson and Redmond (ref. 7), where it is shown that an increase of time is effected as the center distance is increased from a dimension somewhat below nominal.

Influence of Pallet Radius

Figure 11 shows a continuous and quite dramatic decrease in fuze period as the pallet radius c is increased by .008 inches (.020 cm). It is believed that this effect is similar to that observed in connection with a decrease in center distance a , i.e. an increase in pallet radius represents an effective decrease of center distance. The experimentation performed in reference 7 gives good correlation with this result of the simulation.

Influence of Coefficient of Friction

Figure 12 indicates that the fuze time increases as the coefficient of friction, associated with coupled motion, is increased. One would expect that an increase of energy dissipation will slow the mechanism.

Influence of Coefficient of Restitution

According to figure 13, the fuze time increases considerably as the coefficient of restitution is varied from completely inelastic to partially elastic; i.e. from zero to .5. When $\epsilon = 0$ (see description of run no. 70 in the section on results for standard configuration), coupled motion follows immediately after impact. In run no. 75 (which is not reproduced in this report), where $\epsilon = .5$, top action consists of four impacts, three of which are followed by free motion while the fourth is followed by coupled motion. Bottom action shows two impacts with the last one followed by coupled motion. Each of the impacts is followed by considerable escape-wheel reversal. These multiple impacts and associated motion reversals seem to account for the observed increase in fuze time.

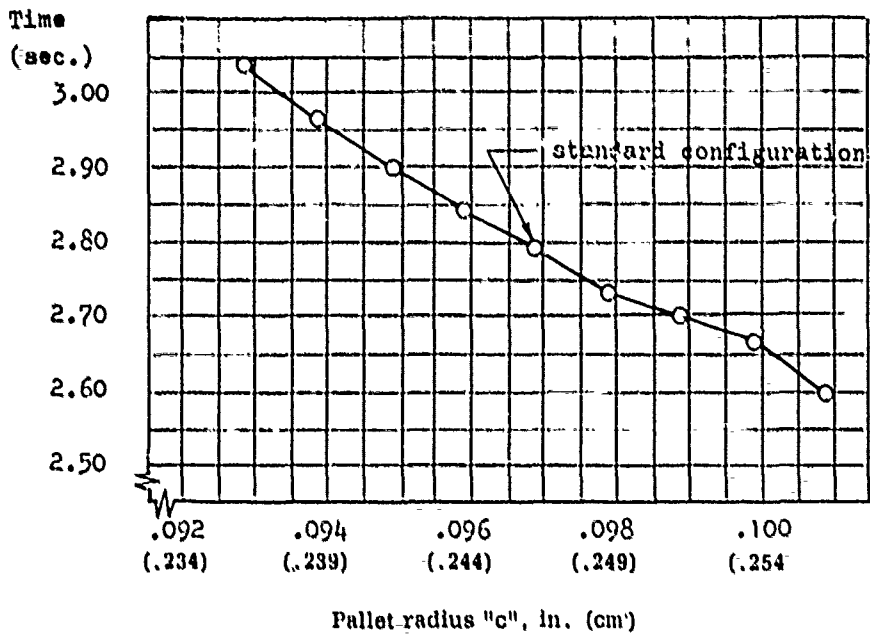
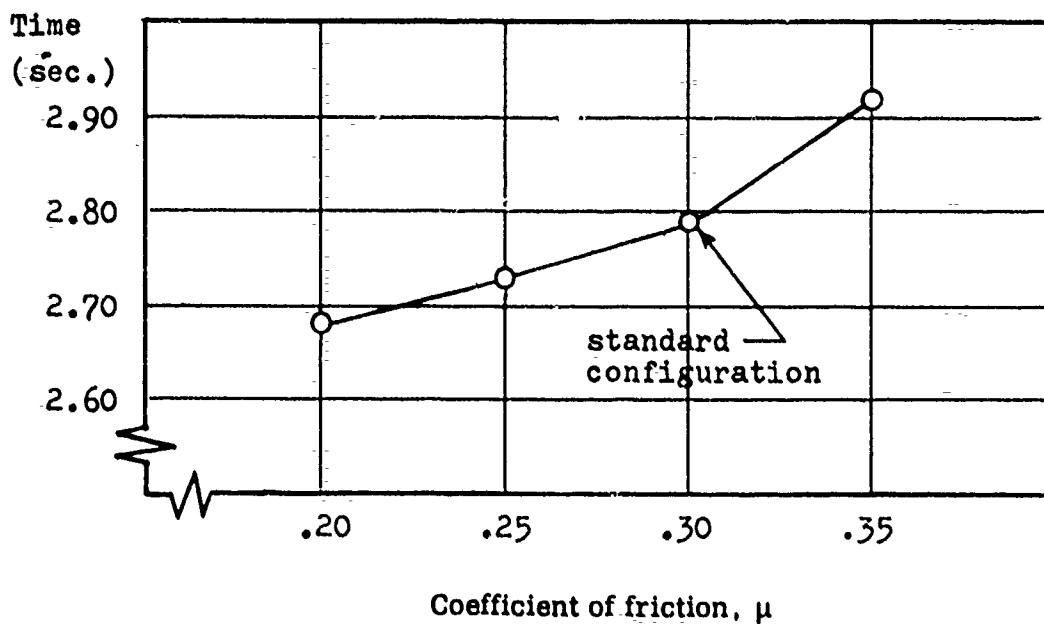
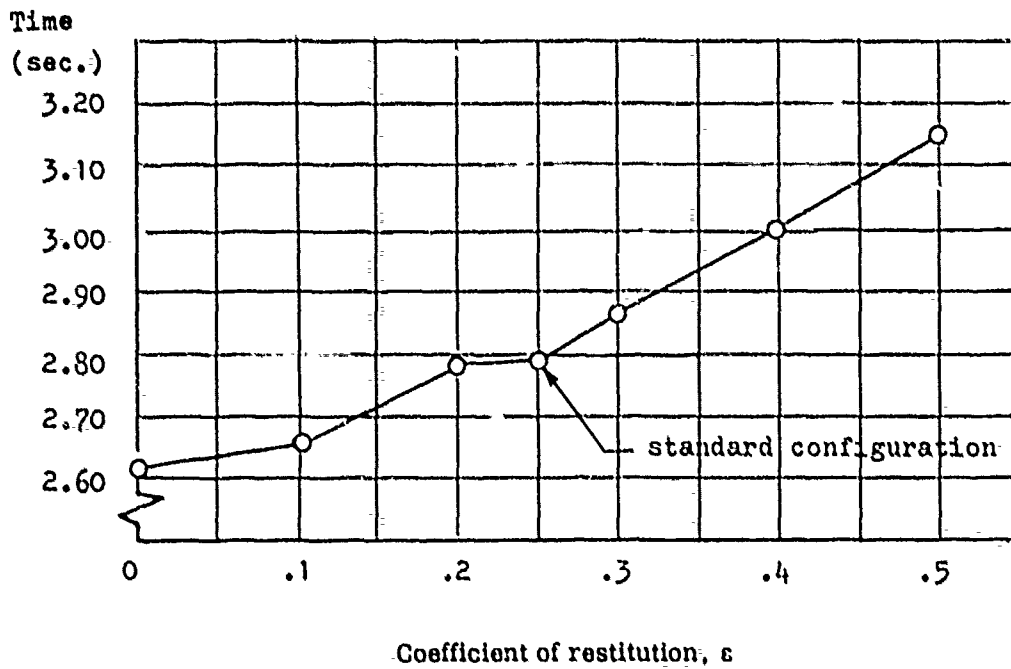


Figure 11. Influence of pallet radius on fuze delay time



| Run no. | Coefficient of friction, μ | Total fuze time (sec.) |
|---------|--------------------------------|------------------------|
| 68 | .20 | 2.68 |
| 67 | .25 | 2.73 |
| 46 | .30 (std. conf.) | 2.79 |
| 69 | .35 | 2.92 |

Figure 12. Influence of coefficient of friction of coupled motion on fuze delay time



| Run no. | Coefficient of restitution, ϵ | Total fuze time (sec.) |
|---------|--|------------------------|
| 75 | .5 | 3.15 |
| 74 | .4 | 3.01 |
| 73 | .3 | 2.87 |
| 46 | .25 (std. conf.) | 2.79 |
| 72 | .2 | 2.78 |
| 71 | .1 | 2.66 |
| 70 | 0.0 | 2.62 |

Figure 13. Influence of coefficient of restitution on fuze delay time

DISCUSSION AND RECOMMENDATIONS FOR CONTINUED WORK

There is no doubt that the goal of a workable computer simulation of the pin pallet runaway escapement has been attained. This is mainly due to the fact that every effort was made to keep the program and its controls as simple as possible.

As a consequence of this, there is presently no built-in sensing mechanism that indicates whether the pallet pin makes contact with the backside of an adjacent tooth during free motion. While this abnormality did not occur for the M525 mechanism, there is no assurance that it will never occur.

Secondly, there is the unresolved problem of the somewhat excessive escape-wheel reversal for the standard configuration unless fairly unrealistic values are used for the coefficients of friction and restitution. (Recall the discussion in the section on the results for the standard configuration.) Table 5 shows the extent to which this escape-wheel reversal depends on the center distance between the pallet and escape-wheel pivots.

Clearly, the reversal increases with a decrease in center distance and decreases as the center distance is enlarged. Note that for $a = .1941$ inches (.4930 cm), which is .001 in (.0025 cm) above nominal, $|g| < |g_{MAX}|$. Note further, that the disengagement center distance of .208 inches (.528 cm) (see end of the section on the example mechanism) is much larger than the values which have been explored in table 5.

Excessive escape-wheel reversal may be indicative of the fact that the simple impact formulation is not sufficiently descriptive, as shown by Anderson and Redmond (ref. 7) or that the escapement only operates in the expected manner when the center distance is somewhat enlarged from nominal.

To resolve this problem, high speed motion pictures must be taken in order to be able to observe the actual motion. Following this, certain modifications of the impact model may have to be made.

Even if the question of the motion reversal cannot be fully resolved, the present simulation is sufficiently descriptive to undertake the following extensions:

1. Adaptation of the pin pallet runaway escapement simulation to a centrifugally driven mechanism, such as the M577 safe separation device (SSD) .⁶

2. Adaptation of the pin pallet simulation to a spring-driven timing mechanism .

3. Modification of the present model to accommodate the simulation of a plate pallet (verge) type runaway escapement .

⁶Successful simulations, incorporating the present escapement model, of both the M577 SSD and the M125A1 booster have been recently completed. The results will be given in a future report.

Table 5. Escape-wheel reversal as a function of center distance a

| Center distance, a* (in.) | Value of g at maximum reversal during top action (in.) | Program number |
|----------------------------------|---|----------------|
| .1901 (.4829 cm) | -.0662 (-.1681 cm) | 55 |
| .1911 (.4854 cm) | -.0635 (-.1613 cm) | 54 |
| .1921 (.4879 cm) | -.0600 (-.1524 cm) | 53 |
| .1931 (std. conf.) (.4905 cm) | -.0580 (-.1473 cm) | 46 |
| .1941 (.4930 cm) | -.0536 (-.1361 cm) | 49 |
| .1951 (.4956 cm) | -.0520 (-.1321 cm) | 50 |
| .1961 (.4981 cm) | -.0471 (-.1196 cm) | 51 |
| .1971 (.5006 cm) | -.0441 (-.1120 cm) | 52 |

*Dimension a is variable, otherwise dimensions are standard configuration with $\mu = .3$, $\epsilon = .25$ and $g_{MAX} = -.05467$ in. (-.13886 cm).

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APPENDIX A

KINEMATICS OF COUPLED MOTION

Figure A1 shows the kinematic relationship of the escape-wheel and the pallet during coupled motion.

UNIT VECTORS

The unit vectors \bar{n}_t and \bar{n}_n are along and perpendicular to the contact surface of the escape-wheel tooth in the indicated directions, respectively. Thus,

$$\bar{n}_t = \cos(\varphi - \alpha) \bar{i} + \sin(\varphi - \alpha) \bar{j} \quad (A1)$$

$$\bar{n}_n = -\sin(\varphi - \alpha) \bar{i} + \cos(\varphi - \alpha) \bar{j} \quad (A2)$$

In addition, the unit vectors \bar{n}_b , for the escape-wheel, and \bar{n}_c , for the line connecting the pallet-pivot and the center of the pallet pin, are introduced:

$$\bar{n}_b = \cos \varphi \bar{i} + \sin \varphi \bar{j} \quad (A3)$$

$$\bar{n}_c = \cos \psi \bar{i} + \sin \psi \bar{j} \quad (A4)$$

INPUT - OUTPUT RELATIONSHIP

The mechanism loop equation is used to determine the pallet angle ψ and the pallet pin location g with respect to the tip of the escape-wheel as functions of the escape-wheel angle φ and the applicable mechanism constants, i.e.

$$\begin{aligned} 0 = & b(\cos \varphi \bar{i} + \sin \varphi \bar{j}) + g[\cos(\varphi - \alpha) \bar{i} + \sin(\varphi - \alpha) \bar{j}] \\ & + r[-\sin(\varphi - \alpha) \bar{i} + \cos(\varphi - \alpha) \bar{j}] - c(\cos \psi \bar{i} + \sin \psi \bar{j}) \\ & + a \bar{i} \end{aligned} \quad (A5)$$

The above is rewritten in component form:

$$b \cos \varphi + g \cos(\varphi - \alpha) - r \sin(\varphi - \alpha) - c \cos \psi + a = 0 \quad (A6)$$

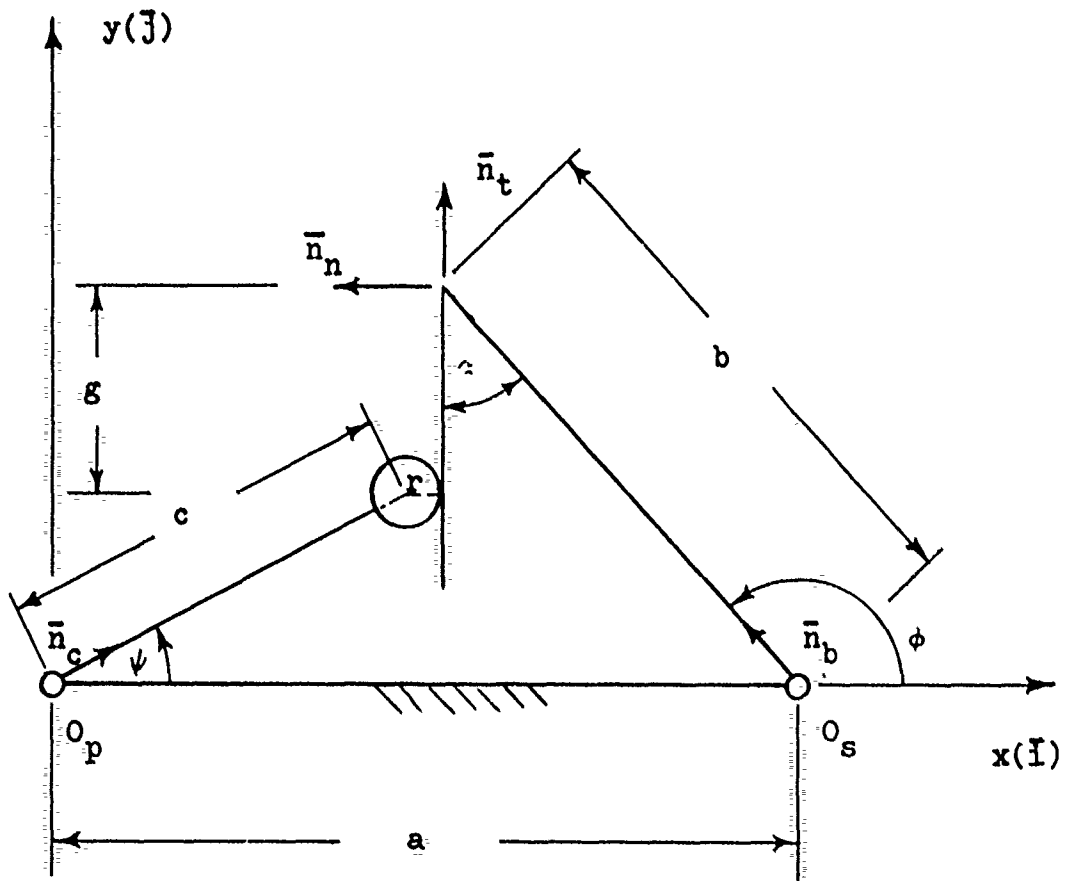


Figure A1. Coupled motion kinematics

$$b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha) - c \sin \psi = 0 \quad (\text{A7})$$

The angle ψ is obtained from (A7):

$$\sin \psi = \frac{1}{c} [b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha)] \quad (\text{A8})$$

and

$$\cos \psi = \frac{1}{c} \sqrt{c^2 - [b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha)]^2} \quad (\text{A9})$$

Substitution of equation (A9) into equation (A6) and subsequent squaring of both sides of the resulting expression leads to:

$$\begin{aligned} [b \cos \varphi + g \cos(\varphi - \alpha) - r \sin(\varphi - \alpha) + a]^2 \\ = c^2 - [b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha)]^2 \end{aligned} \quad (\text{A10})$$

Rearrangement gives:

$$\begin{aligned} g^2 + g[2b \cos \alpha + 2a \cos(\varphi - \alpha)] \\ + [a^2 + b^2 + r^2 - c^2 + 2br \sin \alpha + 2ab \cos \varphi - 2ar \sin(\varphi - \alpha)] \\ = 0 \end{aligned} \quad (\text{A11})$$

Finally, solution of equation (A11) leads to:

$$g = \frac{-H + \sqrt{H^2 - 4K}}{2} \quad (\text{A12})$$

where

$$H = 2[b \cos \alpha + a \cos(\varphi - \alpha)] \quad (\text{A13})$$

$$K = a^2 + b^2 + r^2 - c^2 + 2br \sin \alpha + 2ab \cos \varphi - 2ar \sin(\varphi - \alpha) \quad (\text{A14})$$

The correct value of g , as obtained from equation (A12), must have the smaller absolute magnitude.

OUTPUT VELOCITIES

Implicit differentiation of equation (A11) furnishes the velocity \dot{g} of the instantaneous contact point on the pallet with respect to the coincident point on the escape-wheel during coupled motion:

$$\dot{g} = \frac{a P}{S} \dot{\varphi} \quad (\text{A15})$$

where

$$P = b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha) \quad (\text{A16})$$

$$S = g + b \cos \alpha + a \cos(\varphi - \alpha) \quad (\text{A17})$$

Differentiation of equation (A8) leads to the pallet angular velocity during coupled motion:

$$\dot{\psi} = \frac{Q \dot{\varphi} + \dot{g} \sin(\varphi - \alpha)}{(c) \cos \psi} \quad (\text{A18})$$

where

$$Q = b \cos \varphi + g \cos(\varphi - \alpha) - r \sin(\varphi - \alpha) \quad (\text{A19})$$

OUTPUT ACCELERATIONS

Differentiation of equation (A15) results in an expression for the relative acceleration of the contact point on the pallet with respect to that on the escape-wheel:

$$\ddot{g} = \frac{\ddot{\varphi} P a + \dot{\varphi}^2 Q a + 2 \dot{\varphi} \dot{g} a \sin(\varphi - \alpha) - \dot{g}^2}{S} \quad (\text{A20})$$

Further, differentiation of equation (A18) furnishes an expression for the angular acceleration of the pallet during coupled motion:

$$\ddot{\psi} = \frac{\ddot{\varphi} Q - \dot{\varphi}^2 P + 2 \dot{g} \dot{\varphi} \cos(\varphi - \alpha) + \dot{g} \sin(\varphi - \alpha)}{c \cos \psi} + \dot{\psi}^2 \tan \psi \quad (\text{A21})$$

APPENDIX B

DIFFERENTIAL EQUATION OF COUPLED MOTION

Figure B-1 shows free body diagrams of the pallet and escape-wheel, as they are found during coupled motion. The torque T acts on the escape-wheel. The forces between the escape-wheel and the pallet are represented by the normal forces $\pm P_n$ in the direction of \bar{n}_n and the friction forces $\pm (\mu P_n)$ in the direction of \bar{n}_t . The sign of the friction forces must be such that when the contact point K on the pallet pin moves in the direction of the positive velocity \dot{g} with respect to the coincident point L on the escape-wheel, the friction force on the pallet pin must act in the negative direction of \dot{g} . (Note that \dot{g} , as given by equation (A15) in appendix A, has the same direction as the relative velocity $\bar{V}_{K/L}$.)

The frictional resistance at the pivots O_p and O_s is neglected, since the pivot radii are commonly held very small causing the friction moments to become insignificant.

The differential equations of rotation will first be written separately for the pallet and the escape-wheel. Since the output angle ψ is a function of the input angle ϕ throughout coupled motion, both expressions may be combined by way of the common force magnitudes.

Equation of Motion for the Pallet

$$\bar{D}_1 \times P_n \bar{n}_n + \bar{C}_1 \times (-\mu P_n \frac{\dot{g}}{|\dot{g}|}) \bar{n}_t = I_p \ddot{\psi} \bar{k} \quad (B1)$$

Equation of Motion for the Escape-Wheel

$$\bar{A}_1 \times (-P_n) \bar{n}_n + \bar{B}_1 \times (\mu P_n \frac{\dot{g}}{|\dot{g}|}) \bar{n}_t + T \bar{k} = I_s \ddot{\phi} \bar{k} \quad (B2)$$

The moment arms \bar{A}_1 , \bar{B}_1 , \bar{C}_1 , and \bar{D}_1 are given by equations (C6), (C7), (C4), and (C5), respectively. I_p and I_s represent the moments of inertia of the pallet and the escape-wheel with respect to their pivots.

Appropriate vector operations on equations (B1) and (B2) furnish the following scalar expressions:

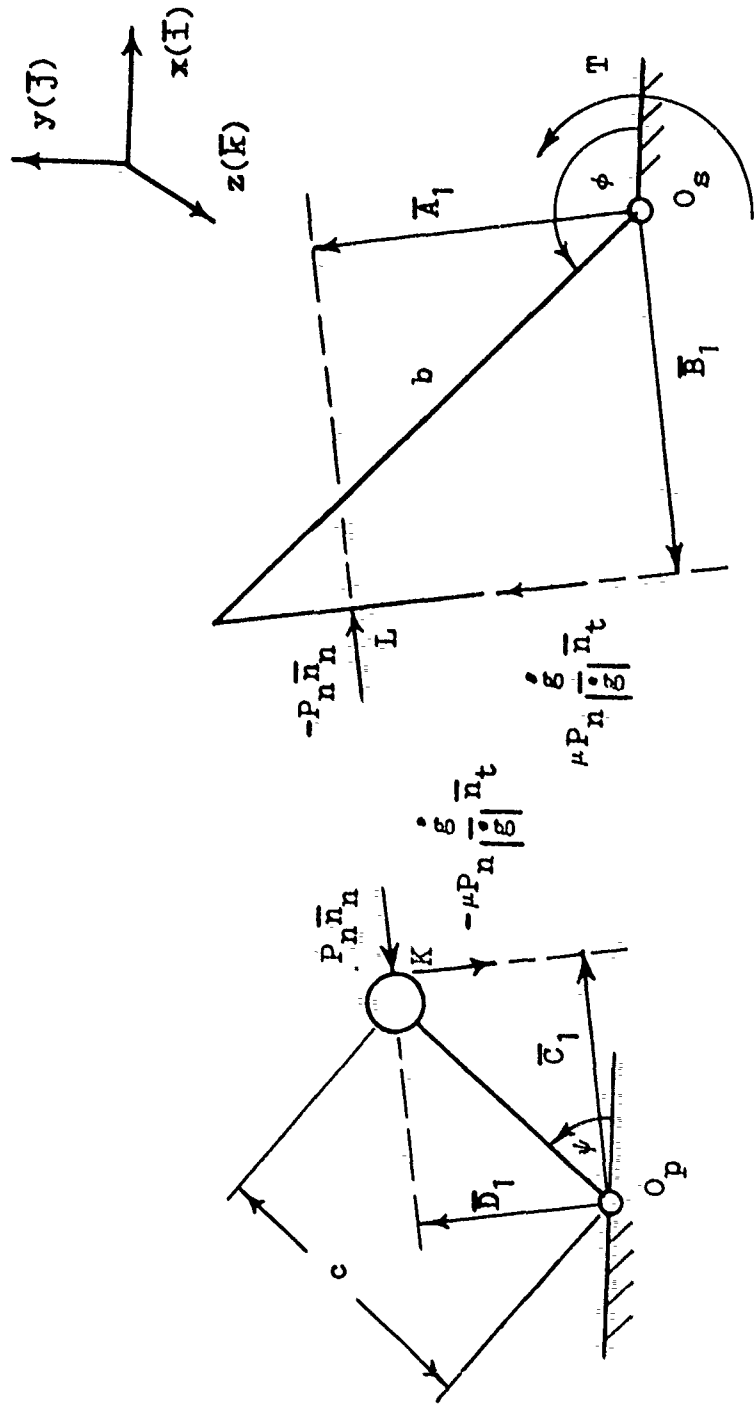


Figure B1. Free body diagram for coupled motion

$$P_n (D_1 - C_1 \mu \frac{\dot{g}}{|g|}) = I_p \ddot{\psi} \quad (B3)$$

and
$$-P_n (A_1 + B_1 \mu \frac{\dot{g}}{|g|}) + T = I_s \ddot{\phi} \quad (B4)$$

When the above expressions are equated in terms of \bar{P}_n , one obtains:

$$\frac{I_p (A_1 + \mu B_1 \frac{\dot{g}}{|g|})}{(D_1 - \mu C_1 \frac{\dot{g}}{|g|})} \ddot{\psi} + I_s \ddot{\phi} = T \quad (B5)$$

The angular acceleration $\ddot{\psi}$ is now expressed in terms of $\ddot{\phi}$ and $\dot{\phi}^2$ with the help of equation (A21) of appendix A. Equations (A15), (A18), and (A20) are utilized to replace \dot{g} , ψ and \ddot{g} , respectively. After considerable simplification, one obtains the following expression for $\ddot{\psi}$:

$$\ddot{\psi} = U \ddot{\phi} + V \dot{\phi}^2 \quad (B6)$$

where

$$U = \frac{Q + \frac{aP}{S} \sin(\varphi - \alpha)}{(c) \cos \psi} \quad (B7)$$

and

$$V = \frac{1}{ccos \varphi} \left[\frac{2aP}{S} \cos(\varphi - \alpha) - P + \frac{2a^2P}{S^2} \sin^2(\varphi - \alpha) + \frac{aQ}{S} \sin(\varphi - \alpha) - \frac{a^2P^2}{S^2} \sin(\varphi - \alpha) \right] + \frac{\tan \psi}{c^2 \cos^2 \psi} \left[Q + \frac{Pa}{S} \sin(\varphi - \alpha) \right]^2 \quad (B8)$$

Equation (B6) is now substituted into equation (B5). This results in:

$$\left[\begin{array}{c} I_p U \\ \frac{(A_1 + \mu B_1 \frac{\dot{g}}{|g|})}{(D_1 - \mu C_1 \frac{\dot{g}}{|g|})} \end{array} + I_s \right] \ddot{\phi} + I_p V \frac{(A_1 + \mu B_1 \frac{\dot{g}}{|g|})}{(D_1 - C_1 \frac{\dot{g}}{|g|})} (\dot{\phi})^2 = T \quad (B9)$$

For computational purposes, equation (B9) is rewritten in the following form:

$$\ddot{\phi} + W\dot{\phi}^2 = Y \quad (B10)$$

where

$$W = \frac{\frac{I_p V}{E_1}}{\frac{I_p U}{E_1} + \frac{I_s}{F_1}} \quad (B11)$$

$$Y = \frac{\frac{T}{E_1}}{\frac{I_p U}{E_1} + \frac{I_s}{F_1}} \quad (B12)$$

and

$$E_1 = D_1 - \mu C_1 \frac{\dot{g}}{|g|} \quad (B13)$$

$$F_1 = A_1 + \mu B_1 \frac{\dot{g}}{|g|} \quad (B14)$$

APPENDIX C

MOMENT ARMS

DETERMINATION OF MOMENT ARMS \bar{C}_1 AND \bar{D}_1

Figure C-1 suggests the following loop equation for the determination of the vectors \bar{C}_1 and \bar{D}_1 :

$$c\bar{n}_c - r\bar{n}_n - D_1\bar{n}_n + C_1\bar{n}_n = 0 \quad (C1)$$

When the components in the \bar{n}_t and \bar{n}_n directions are separated, one obtains:

$$c\cos\psi + r\sin(\varphi - \alpha) + D_1\cos(\varphi - \alpha) - C_1\sin(\varphi - \alpha) = 0 \quad (C2)$$

and

$$c\sin\psi - r\cos(\varphi - \alpha) + D_1\sin(\varphi - \alpha) + C_1\cos(\varphi - \alpha) = 0 \quad (C3)$$

Simultaneous solution of the above expressions leads to the following vectorial expressions:

$$\bar{C}_1 = - [r + c\sin(\varphi - \alpha - \psi)]\bar{n}_n \quad (C4)$$

and

$$\bar{D}_1 = c\cos(\varphi - \alpha - \psi)\bar{n}_t \quad (C5)$$

DETERMINATION OF MOMENT ARMS \bar{A}_1 AND \bar{B}_1

Inspection of figure C-1 leads to the following expressions for the vectors \bar{A}_1 and \bar{B}_1 :

$$\bar{A}_1 = (b\cos\alpha + g)\bar{n}_t \quad (C6)$$

(Note that g is negative during contact.)

Further,

$$\bar{B}_1 = (b\sin\alpha)\bar{n}_n \quad (C7)$$

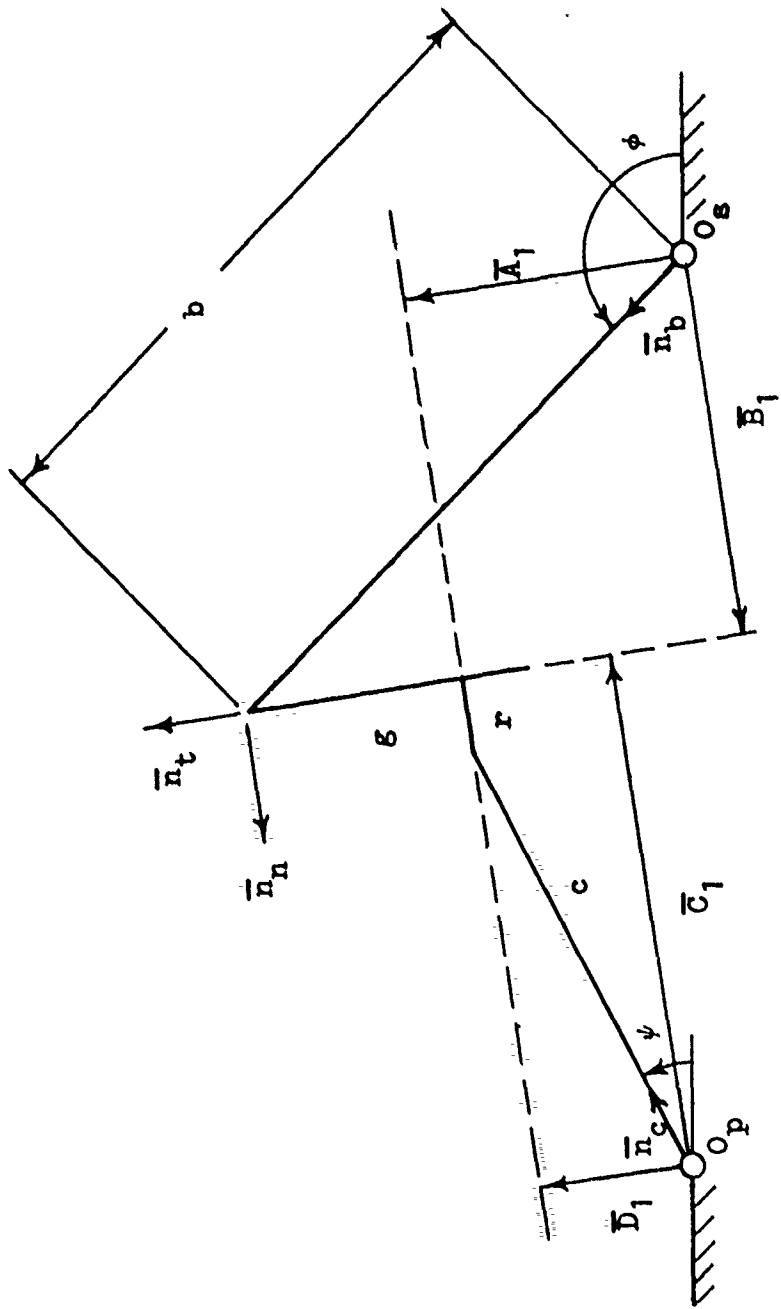


Figure C1. Moment arms

APPENDIX D

CONTACT SENSING EXPRESSIONS

When the mechanism is in free motion, i.e. φ and ψ are independent of each other, it is necessary to know the distances f and g' , in figure D-1, to determine the relative positions. The quantity f , which indicates the distance of the pallet pin from the escape-wheel face, vanishes at the instant of impending impact. When contact between the pallet and the escape-wheel becomes impossible, i.e. the pin has left the tooth, $g' \geq 0$.

By inspection of figure D-1, the loop equation for free motion is given by:

$$b\bar{n}_b + g'\bar{n}_t + (r + f)\bar{n}_n - c\bar{n}_c + a\bar{i} = 0 \quad (D1)$$

(Note that φ and ψ are independent variables and are assumed to be known.)

In component form, the above becomes:

$$b\cos\varphi + g'\cos(\varphi - \alpha) - r\sin(\varphi - \alpha) - f\sin(\varphi - \alpha) - c\cos\psi + a = 0 \quad (D2)$$

$$b\sin\varphi + g'\sin(\varphi - \alpha) + r\cos(\varphi - \alpha) + f\cos(\varphi - \alpha) - c\sin\psi = 0 \quad (D3)$$

Multiply equation (D2) by $\sin(\varphi - \alpha)$

$$\begin{aligned} & b\cos\varphi\sin(\varphi - \alpha) + g'\sin(\varphi - \alpha)\cos(\varphi - \alpha) - r\sin^2(\varphi - \alpha) \\ & - f\sin^2(\varphi - \alpha) - c\cos\psi\sin(\varphi - \alpha) + a\sin(\varphi - \alpha) \\ & = 0 \end{aligned} \quad (D4)$$

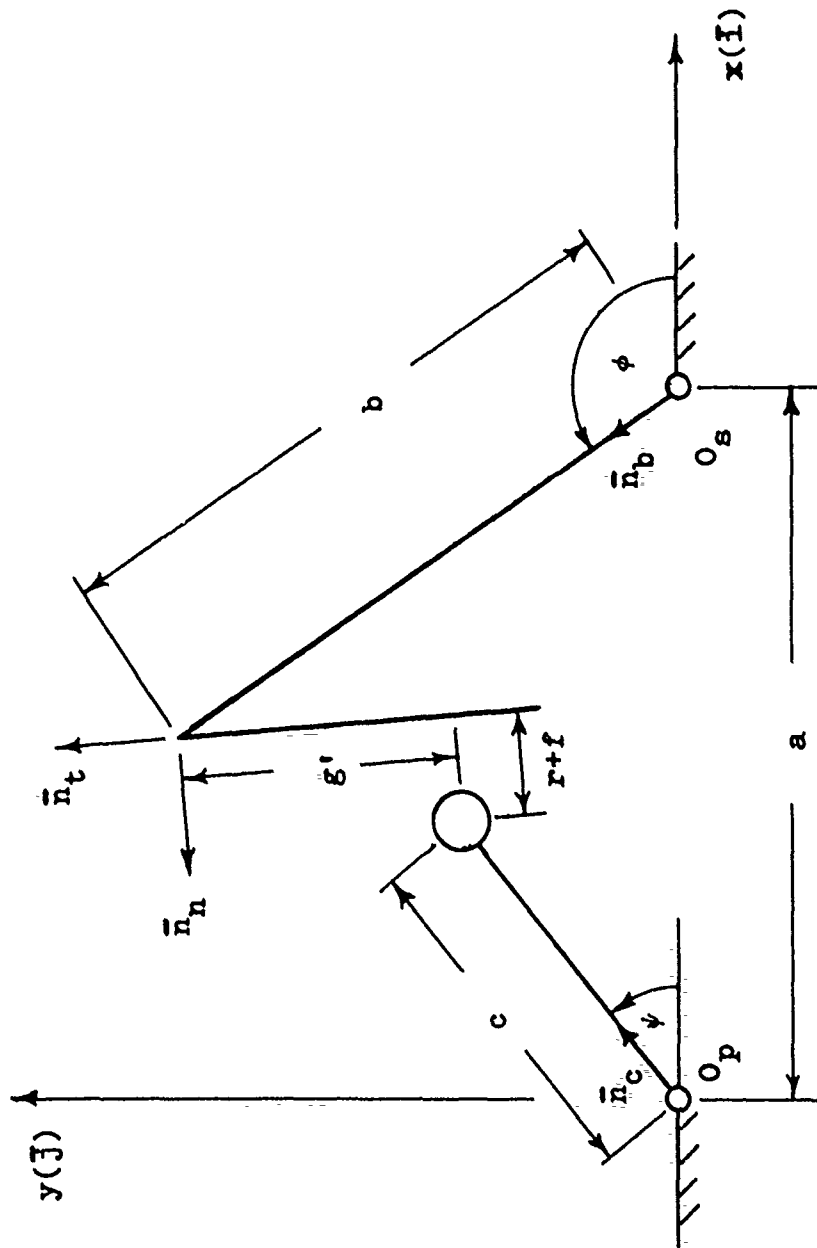


Figure D1. Contact sensing quantities

Further, multiply equation (D3) by $\cos(\varphi - \alpha)$

$$\begin{aligned} & b\sin\varphi\cos(\varphi - \alpha) + g'\sin(\varphi - \alpha)\cos(\varphi - \alpha) + r\cos^2(\varphi - \alpha) \\ & + f\cos^2(\varphi - \alpha) - c\sin\psi\cos(\varphi - \alpha) \\ & = 0 \end{aligned} \tag{D5}$$

Subtract equation (D4) from equation (D5)

$$\begin{aligned} & b\sin[\varphi - (\varphi - \alpha)] + r + f + c\sin[(\varphi - \alpha) - \psi] - a\sin(\varphi - \alpha) \\ & = 0 \end{aligned} \tag{D6}$$

This furnishes

$$f = a\sin(\varphi - \alpha) - b\sin\alpha - c\sin[(\varphi - \alpha) - \psi] - r \tag{D7}$$

Multiply (D2) by $\cos(\varphi - \alpha)$

$$\begin{aligned} & b\cos\varphi\cos(\varphi - \alpha) + g'\cos^2(\varphi - \alpha) - r\sin(\varphi - \alpha)\cos(\varphi - \alpha) \\ & - f\sin(\varphi - \alpha)\cos(\varphi - \alpha) - c\cos\psi\cos(\varphi - \alpha) \\ & + a\cos(\varphi - \alpha) \\ & = 0 \end{aligned} \tag{D8}$$

Multiply (D3) by $\sin(\varphi - \alpha)$

$$\begin{aligned} & b\sin\varphi\sin(\varphi - \alpha) + g'\sin^2(\varphi - \alpha) + r\sin(\varphi - \alpha)\cos(\varphi - \alpha) \\ & + f\sin(\varphi - \alpha)\cos(\varphi - \alpha) - c\sin\psi\sin(\varphi - \alpha) \\ & = 0 \end{aligned} \tag{D9}$$

Finally, add (D8) and (D9)

$$\begin{aligned} & b\cos[\varphi - (\varphi - \alpha)] + g' - c\cos[\psi - (\varphi - \alpha)] + a\cos(\varphi - \alpha) \\ & = 0 \end{aligned} \tag{D10}$$

Thus,

$$g' = c\cos[(\varphi - \alpha) - \psi] - b\cos\alpha - a\cos(\varphi - \alpha) \tag{D11}$$

APPENDIX E

FREE MOTION EQUATIONS

During the free motion phase of the mechanism, the pallet moves independently of the escape-wheel.

Again, the frictional resistance at the pivots O_p and O_s are neglected.

FREE MOTION OF PALLET

In the absence of all external torques, the differential equation of motion for the pallet is given by:

$$\psi = 0 \quad (E1)$$

With an initial angular velocity ψ_0 at the time t_0 , when the free motion starts, the angular velocity of the pallet at any time is:

$$\dot{\psi} = \dot{\psi}_0 \quad (E2)$$

If $\psi(t_0) = \psi_0$, further integration gives the angular displacement of the pallet at any time t to be:

$$\psi = \psi_0 (t - t_0) + \psi_0 \quad (E3)$$

The time t is counted from the start of the motion of the escapement.

FREE MOTION OF THE ESCAPE-WHEEL

When a constant torque T acts on the escape-wheel, its differential equation of motion is given by:

$$\ddot{\phi} = \frac{T}{I_s} \quad (E4)$$

and the applicable initial conditions are:

$$\dot{\phi}(t_0) = \dot{\phi}_0 \quad (E5)$$

and

$$\varphi(t_0) = \varphi_0 \quad (E6)$$

Integration of equation (E4) gives the following expression for the angular velocity of the escape-wheel at any time t :

$$\dot{\varphi} = \frac{T}{I_s} (t - t_0) + \dot{\varphi}_0 \quad (E7)$$

Further integration furnishes the angular displacement:

$$\varphi = \frac{T}{2I_s} (t - t_0)^2 + \dot{\varphi}_0 (t - t_0) + \varphi_0 \quad (E8)$$

APPENDIX F

IMPACT EQUATIONS

Before the impact equations can be given, certain velocity expressions associated with the impact points on the pallet and the escape-wheel must be derived. These velocities occur during free motion preceding impact when the angular velocities $\dot{\phi}$ and $\dot{\psi}$ are independent of each other.

VELOCITIES AT IMPACT POINTS JUST BEFORE IMPACT

Figure F1 shows the velocities of the contact points K and L on the pallet and the escape-wheel, respectively, just before impact. The components in the direction normal to the escape-wheel tooth are:

$$\bar{V}_{pn_i} = \dot{\psi}_i \bar{k} \times D_1 \bar{n}_t \quad \text{for the pallet} \quad (F1)$$

and

$$\bar{V}_{sn_i} = \dot{\phi}_i \bar{k} \times A_1 \bar{n}_t \quad \text{for the escape-wheel,} \quad (F2)$$

where the subscript i stands for the angular velocities prior to the instant of impact.

The components of velocity in the tangential direction are given by:

$$\bar{V}_{pt_i} = \dot{\psi}_i \bar{k} \times C_1 \bar{n}_n \quad (F3)$$

and

$$\bar{V}_{st_i} = \dot{\phi}_i \bar{k} \times B_1 \bar{n}_n \quad (F4)$$

The expressions for the moment arms are obtained from appendix C.

To determine the direction of the tangential impact, the sign of the relative tangential velocity \bar{V}_t must be known. This velocity is given by (refer to equations (F3) and (F4)):

$$\bar{V}_t = \bar{V}_{pt_i} - \bar{V}_{st_i} = \dot{\psi}_i \bar{k} \times C_1 \bar{n}_n - \dot{\phi}_i \bar{k} \times B_1 \bar{n}_n \quad (F5)$$

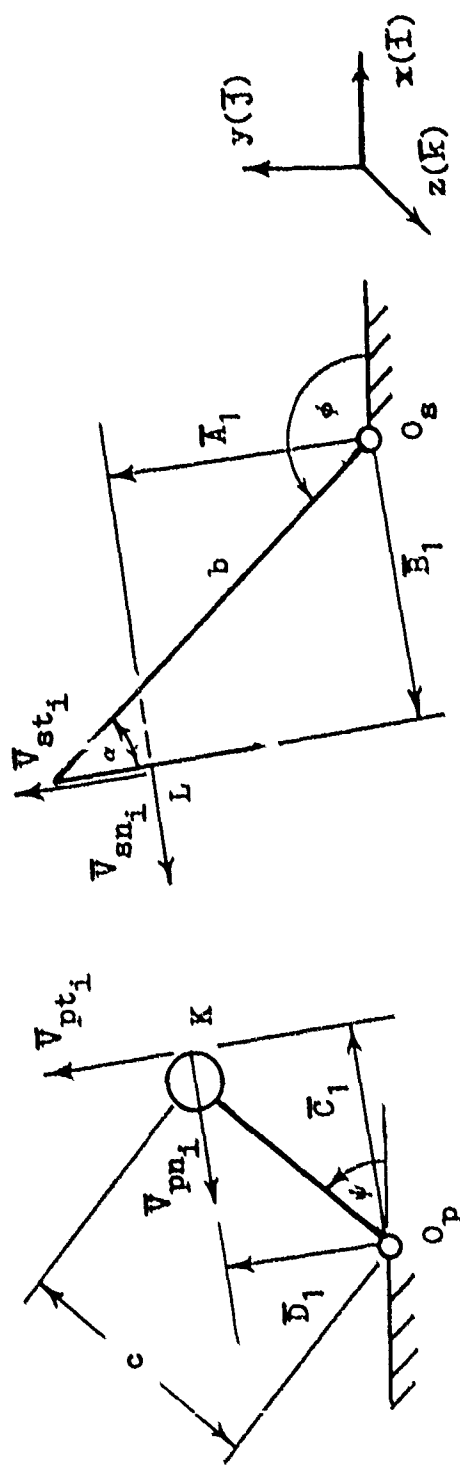


Figure F1. Velocities just before impact

Substituting equations (C4) and (C7) into equation (F5) produces:

$$\bar{V}_t = (\psi[r + c \sin(\varphi - \alpha - \psi)] + \phi b \sin \alpha) \bar{n}_t \quad (F6)$$

IMPACTS ON PALLET AND ESCAPE-WHEEL

The impact simulation is based on the classical angular impulse-momentum model shown in figure F-2 for the pallet and the escape-wheel.

\bar{P}_n represents the normal impulse between the components. Further, a frictional impulse $\mu \bar{P}_n$, which is tangential to the contact surface and has the direction of the velocity \bar{V}_t (see equation (F6)), is assumed because of the angular displacements during impact.

The angular impulse T_τ on the escape-wheel, which is due to the torque T and has the duration τ of the impact phenomenon, is disregarded since it is felt that its magnitude is small when compared to that of the other terms involved. The angular impulse on the pallet then becomes:

$$\bar{J}_p = \bar{D}_1 \times P_n \bar{n}_n + \bar{C}_1 \times -\mu P_n \frac{V_t}{|V_t|} \bar{n}_t \quad (F7)$$

After the cross product has been executed, the following equation is obtained:

$$\bar{J}_p = P_n (D_1 - \mu C_1 \frac{V_t}{|V_t|}) \bar{k} \quad (F8)$$

Similarly, the angular impulse on the escape-wheel reduces to:

$$\bar{J}_s = \bar{A}_1 \times (-P_n) \bar{n}_n + \bar{B}_1 \times \mu P_n \frac{V_t}{|V_t|} \bar{n}_t \quad (F9)$$

This becomes

$$\bar{J}_s = -P_n (A_1 + \mu B_1 \frac{V_t}{|V_t|}) \bar{k} \quad (F10)$$

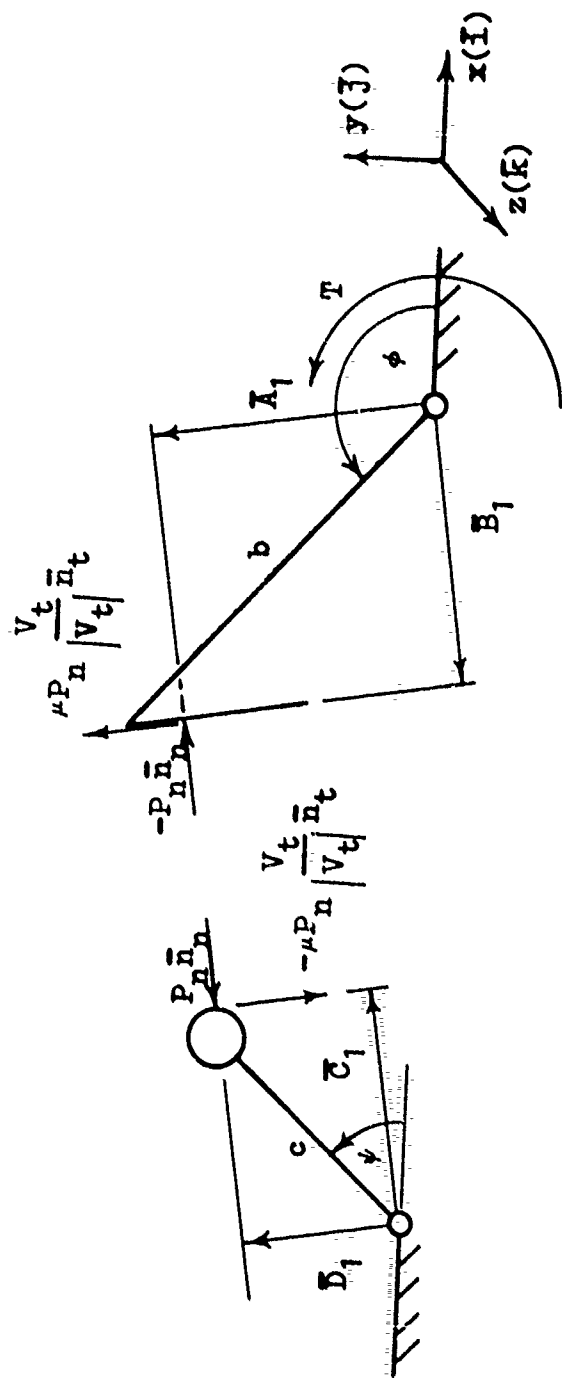


Figure F2. Free body diagram of impact

Equations (F8) and (F10) are now substituted into the following angular momentum equations:

$$I_p (\dot{\psi}_f - \dot{\psi}_i) = \bar{J}_p \quad (F11)$$

and

$$I_s (\dot{\phi}_f - \dot{\phi}_i) = \bar{J}_s \quad (F12)$$

The subscript f indicates the angular velocities after impact. Substitution of the scalar portions of equations (F8) and (F10) into equations (F11) and (F12), respectively, as well as the subsequent simultaneous elimination of P_n from both of the resulting expressions, leads to:

$$I_p F_2 \dot{\psi}_f + I_s E_2 \dot{\phi}_f = I_p F_2 \dot{\psi}_i + I_s E_2 \dot{\phi}_i \quad (F13)$$

where

$$E_2 = D_1 - \mu C_1 \frac{V_t}{|V_t|} \quad (F14)$$

and

$$F_2 = A_1 + \mu B_1 \frac{V_t}{|V_t|} \quad (F15)$$

To solve for the angular velocities after impact, it is now necessary to make use of the concept of the coefficient of restitution. This coefficient is adapted to the present situation in the following manner:

$$\epsilon = - \frac{V_{pn_f} - V_{sn_f}}{V_{pn_i} - V_{sn_i}} \quad (F16)$$

Using equations (F1) and (F2) and letting

$$\bar{V}_{pn_f} = \dot{\psi}_f \bar{k} \times D_1 \bar{n}_t \quad \text{for the pallet} \quad (F17)$$

$$\bar{V}_{sn_f} = \dot{\phi}_f \bar{k} \times A_1 \bar{n}_t \quad \text{for the escape-wheel} \quad (F18)$$

where $\dot{\phi}_f$ and $\dot{\psi}_f$ are the respective angular velocities of the pallet and the escape-wheel after impact, produces

$$\varepsilon = - \frac{(\dot{\psi}_f D_1 - \dot{\phi}_f A_1)}{(\dot{\psi}_i D_1 - \dot{\phi}_i A_1)} \quad (F19)$$

Simultaneous solution of equations (F13) and (F19) furnishes the desired angular velocities after impact.

Thus,

$$\dot{\psi}_f = \frac{\dot{\phi}_f A_1 - \varepsilon (\dot{\psi}_i D_1 - \dot{\phi}_i A_1)}{D_1} \quad (F20)$$

and

$$\dot{\phi}_f = \frac{I_p F_2 \dot{\psi}_i + I_s E_2 \dot{\phi}_i + \frac{I_p F_2 \varepsilon}{D_1} (\dot{\psi}_i D_1 - \dot{\phi}_i A_1)}{\frac{I_p F_2 A_1}{D_1} + I_s E_2} \quad (F21)$$

GENERAL EXPRESSIONS FOR THE NORMAL VELOCITIES AT THE IMPACT POINTS

The normal velocities at the impact points of the pallet and the escape-wheel are also used in the logic of the computer program. If $\dot{\phi}$ and $\dot{\psi}$ represent the angular velocities of the escape-wheel and the pallet just before or after impact, expressions are derived for these velocities using (F1), (F2), (C5), and (C6):

For the pallet

$$V_p = \psi c \cos(\varphi - \alpha - \psi) \quad (F22)$$

For the escape wheel

$$V_s = \dot{\phi} (b \cos \alpha + g) \quad (F23)$$

(Note the simplification of the notation.)

APPENDIX G
COMPUTER PROGRAM


```

55  IF(G,LT,0,160 TO 200
      PHID=PHI(1)/Z
      IF(PHI0.LE,150,160 TO 150
      GO TO 151
150  PHI(1)=PHI(1)*DELTA*Z
      PHIPR = PHI(1)/Z
60    PSI=PSI+2.*PI-LAMBDA*Z
      GO TO 200
151  PHI(1)=PHI(1)-DELTA*Z*2.
      PHIPR = PHI(1)/Z
      PSI=PSI-2.*PI+LAMBDA*Z
C
C    FREE MOTION
C
200  CALL FREE(TIME,PHI(1),PHI(2),PSI,DPSI)
C
70  C
C

```

```

PHID=PHI(1)/Z
H=2.*(B*COS(ALPHR)+A*COS(PHI(1)-ALPHR))
K=A**2+8.*R**2-C**2*Z*.B*R*SIN(ALPHR)+2.*A*B
1*0COS(PHI(1))-2.*R*SIN(PHI(1)-ALPHR)
GONE=(-H+SQRT(H**2-4.*K))/2.
GTWO=(-H-SQRT(H**2-4.*K))/2.
IF(LABS(GONE).LT,ABS(GTWO),GO TO 204
G=GTWO
80  GO TO 205
      G=GONE
      204 PHID=PHI(1)/Z
      GP=C*COS(PHI(1)-ALPHR-PSI)-B*COS(ALPHR)-A*COS(PHI(1))
1-ALPHR)
      IF(GP.LT,0,160 TO 250
      IF(PHI0.LE,150,160 TO 210
      GO TO 215
210  PHI(1) = PHI(1) + DELTA*Z
      PHIPR = PHI(1)/Z
      PSI = PSI + 2.*PI - LAMBDA*Z
      GO TO 200
215  PHI(1) = PHI(1) - DELTA*Z*2.
      PHIPR = PHI(1)/Z
      PSI = PSI - 2.*PI + LAMBDA*Z
      GO TO 200
250  IF(PHI0.LE,150,0)GO TO 9
      DPSTP=D*PSI
C
C

```

```

100  C COMPUTATION OF VELOCITIES VP AND VS FOR BOTTOM FREE MOTION TESTS
C
AONE=R*COS(ALPHR)*G
DONE=C*COS(PHI(1)-ALPHR-PSI)
VP=DONE*DPSI
VS=AONE*PHI(2)
WRITE(6,9002)VP,VS
9002 FORMAT(90VPE,F8.3X,F8.3)

```

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C BOTTOM FREE MOTION TESTS

```

110 IF (PHI(2).GE.0..AND.DPSI.GE.0.)GO TO 300
    IF (PHI(2).GE.0..AND.DPSI.LE.0..AND.ARS(VP).GT.ABS(VS))GO TO 200
    IF (PHI(2).GE.0..AND.DPSI.LE.0..AND.ARS(VP).LT.ABS(VS))GO TO 300
    IF (PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
115 IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).GT.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
    IF (PHI(2).LE.0..AND.DPSI.LE.0)GO TO 200

```

C COMPUTATION OF VELOCITIES VP AND VS FOR TOP FREE MOTION TESTS

```

120 9 AONE=B*COS(ALPHR)*G
    DONE=C*COS(PHI(1)-ALPHR-PSI)
    VP=DONE*DPSI
    VS=AONE*PHI(2)
    WRITE(6,9002)VP,VS

```

C TOP FREE MOTION TESTS

```

130 IF (PHI(2).GE.0..AND.DPSI.GE.0..AND.ARS(VP).GT.ABS(VS))GO TO 200
    IF (PHI(2).GE.0..AND.DPSI.GE.0..AND.ARS(VP).EQ.ABS(VS))GO TO 99
    IF (PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).LT.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.GE.0)GO TO 200
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).GT.ABS(VS))GO TO 200
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99

```

C IMPACT

```

140 300 CALL IMPACT(PHI(1),PHI(2),PSI,DPSI)
    B=2.*(4*COS(ALPHR)+A*COS(PHI(1)-ALPHR))
    K=A*2.8*2.8*2-C*2*2.*8*8*SIN(ALPHR)*2.*A*B
    1 *COS(PHI(1))-2.*A*8*SIN(PHI(1)-ALPHR)
    GONE=(H-SORT(H*2-4.*K))/2.
    GTWO=(H+SORT(H*2-4.*K))/2.
    IF (ARS(GONE).LT.ABS(GTWO))GO TO 310
    G=GTWO
    GO TO 311
    310 G=GONE
    311 DPSI=DPSI
    IF (TIME.GT.0.1)GO TO 9999

```

C TEST FOR BOTTOM ACTION

```

155 PHIO=PHI(1)/2
    IF (PHIO.LE.150.0)GO TO 12

```

C COMPUTATION OF VELOCITIES VP AND VS FOR BOTTOM IMPACT TESTS

C

```

160 AONE=B*COS(ALPHR)*G
    DONE=C*COS(PHI(1))-ALPHR-PSI
    VP=DONE*DPSI
    VS=AONE*PHI(2)
165 WRITE(6,9002)VP,VS
    IF(ABS(ABS(VP)-ABS(VS)).LT.2.0)GO TO 99
C
C BOTTOM IMPACT TESTS
C
170 IF(PHI(2).GE.0..AND.DPSI.GE.0.)GO TO 99
    IF(PHI(2).GE.0..AND.DPSI.LF.0..AND.ARS(VP).GT.ABS(VS))GO TO 200
    IF(PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 99
    IF(PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
    IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ARS(VP).LT.ABS(VS))GO TO 200
    IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ABS(VP).GT.ABS(VS))GO TO 99
    IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
C
C COMPUTATION OF VELOCITIES VP AND VS FOR TOP IMPACT TESTS
C
180 AONE=B*COS(ALPHR)*G
    DONE=C*COS(PHI(1))-ALPHR-PSI
    VP=DONE*DPSI
    VS=AONE*PHI(2)
185 WRITE(6,9002)VP,VS
    IF(ABS(ABS(VP)-ABS(VS)).LT.2.0)GO TO 99
C
C TOP IMPACT TESTS
C
190 IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).GT.ABS(VS))GO TO 200
    IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).LT.ABS(VS))GO TO 99
    IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ARS(VP).GT.ABS(VS))GO TO 200
    IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
    IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).GT.ABS(VS))GO TO 99
    IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200
    IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
195 IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200
    IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
9999 STOP
    ENO

```

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```

1 SUBROUTINE FCY(I,PHI,DPHI)
  REAL IP,IS,LAMBDA,K
  COMMON A,B,C,R,ALPHR,PI,TOR,K,COFR,IP,ISTEREST,LAMBDA,DELTA,
  PHITOT,PHIPR
5 DIMENSION PHI(2),DPHI(2),PRMT(5)
  H=2.*R*COS(ALPHR)*A*COS(PHI(1)-ALPHR)
  K=A**2.*R**2.*C**2.*B**2.*B**2.*SIN(ALPHR)**2.*A*B
  I=COS(PHI(1))-2.*A*R*SIN(PHI(1)-ALPHR)
  GONE=(-H*SORT(H**2-4.*K))/2.
  GTWO=(-H*SORT(H**2-4.*K))/2.
  IF (ABS(GONE).LT.ABS(GTWO)) GO TO 10
  G=GTWO
  GO TO 11
10 G=GONE
11 P=B*SIN(PHI(1))*G*SIN(PHI(1)-ALPHR)+R*COS(PHI(1)-ALPHR)
  Q=B*COS(PHI(1))*G*COS(PHI(1)-ALPHR)-R*SIN(PHI(1)-ALPHR)
  S=G*B*COS(ALPHR)*A*COS(PHI(1)-ALPHR)
  GDOT=PHI(2)*A*P/S
  PSI=ASIN(P/C)
20 IF (PSI.LT.0.) GO TO 12
  GO TO 13
12 PSI=2.*PI-ARS(PSI)
13 AONE=R*COS(ALPHR)*G
  RONE=R*SIN(ALPHR)
  CONE=R*C*SIN(PHI(1)-ALPHR-PSI)
  DONE=C*COS(PHI(1)-ALPHR-PSI)
  IF (GDOT.EQ.0.) GO TO 20
  GO TO 30
20 EONE=DONE
  FONE=AONE
  GO TO 40
30 EONE=DONE-COFR*CONE*GDOT/ARS(GDOT)
  FONE=AONE-COFR*BONE*GDOT/ARS(GDOT)
40 CONTINUE
35 U=(O*SIN(PHI(1)-ALPHR)*P+A/S)/(C*COS(PSI))
  V=(O*A*P*SIN(PHI(1)-ALPHR)/S)**2*TAN(PSI)/(C**2)
  I(COS(PSI)**2)*(1/(C*COS(PSI)))*(2.*A*P*COS(PHI(1)-ALPHR)/S
  2-P*2.*A**2*P*(SIN(PHI(1)-ALPHR))**2/S**2*A*O*SIN(PHI(1)
  3-ALPHR)/S-A**2*P**2*SIN(PHI(1)-ALPHR)/S**3)
  W=(IP*V/EONE)/(IP*U/EONE*IS/FONE)
  Y=(TOR*FONE)/(IP*U/EONE*IS/FONE)
  DPHI(1)=PHI(2)
  DPHI(2)=Y-W*PHI(2)**2
  RETURN
  END

```

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1  SUBROUTINE_OUTP(I,PHI,PHI2,THLF,NDIM,PRMT)
   REAL IP,IS,LAMBDA,K
   DIMENSION PHI(2),OPHI(2),PRMT(5)
   COMMON A,B,C,ALPHR,PI,TORR,CFR,IP,IS,EREST,LAMBDA,DELTA,
1 PHITOT,PHIPR
   COMMON ZEIA,PSI,TIME,G,DPSI,OPSI
   ZE=180./PI
   IF(T.EQ.0.)OPSI=0.
   PHID=PHI(1)*2
   C COMPUTE PSID
   C
   DELPHI = PHID - PHIPR
   PHITOT = PHITOT + DELPHI
   PHIPR = PHID
   M=2.+(B*COS(ALPHR)).A*COS(PHI(1)-ALPHR))
   X=A*2.+B*2.*R*2.-C*2.*2.*B*R*SIN(ALPHR)*2.*A*B
   I=COS(PHI(1))-2.*A*B*SIN(PHI(1)-ALPHR)
   GONE=(-H*SQRT(H*2-4.*X))/2.
   GTWO=(-H*SQRT(H*2-4.*X))/2.
   IF(ABS(GONE).LT.ABS(GTWO))GO TO 1
   G=GTWO
   GO TO 2
   1 G=GONE
   2 P=B*SIN(PHI(1))*G*SIN(PHI(1)-ALPHR)+C*COS(PHI(1)-ALPHR)
   PSI=ASIN(P/C)
   IF(PSI.LT.0.)PSI=2.*PI-ABS(PSI)
   PSID=PSI*2
   C COMPUTE OPSI
   C
   S=G*B*COS(ALPHR)+A*COS(PHI(1)-ALPHR)
   S00T=PHI(2)*A*P/S
   O=B*COS(PHI(1))*G*COS(PHI(1)-ALPHR)-R*SIN(PHI(1)-ALPHR)
   DPSI=(PHI(2)+O-G00T*SIN(PHI(1)-ALPHR))/(C*COS(PSI))
   C
   C TEST FOR CONTINUATION OF COUPLED MOTION
   C
   IF(T.EQ.0.)GO TO 4
   IF(T.EQ.0.)GO TO 4
   IF(.NOT.(G.LT.0.).AND.((ABS(DPSI).GT.ABS(OPSI)).AND.PHI(2)
1.GT.0.).OR.(ABS(OPSI).LT.ABS(OPSI)).AND.PHI(2).LT.0.)).AND.
2.TIME.0.))PRMT(5)=1.
   IF(ABS(OPSI).LT.1.)PRMT(5)=-0.
   C
   C WRITE OUTPUT
   C
   4 WRITE(6,3)PHID,PHI(2),G,G00T,PSID,DPSI,PHITOT
   3 FORMAT(5X,*,T=,F8.3X,PHI=,F8.3X,PHIDOT=,F8.3X,
1 G=,F9.4,3X,G00T=,F8.3X,PSID=,F8.3X,PSIDOT=,F8.3,
1 X,PHITOT =,F8.3)
   5 DPSI=OPSI
   TIME=T

```

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SUBROUTINE OUTP

73/74 OPT=1

FTN 4.6+420 12/16/76 15.25.49

PAGE 2

RETURN
END

55

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SUBROUTINE IMPACT 73/74 OPT=1

1 SUBROUTINE IMPACT(PHI,DPHI,PSI,DPSI)

COMMON A,B,C,R,ALPHR,PI,TORK,COFR,IP,IS,EREST,LAMBDA,DELTA,

PHITOT,PHIPR

REAL IP,IS,LAMRDA,K

5 H=2.*(B*COS(ALPHR)+A*COS(PHI-ALPHR))

K=A**2*B**2-R**2-C**2*.8*R*SIN(ALPHR)*2.*A*B*COS(PHI)-

12.*A*R*SIN(PHI-ALPHR)

GONE=(-H+SQRT(H**2-4.*K))/2.

GTWO=(-H+SQRT(H**2-4.*K))/2.

10 IF (ABS(GONE).LT.ABS(GTWO)) GO TO 1

G=GTWO

GO TO 2

1 G=GONE

2 AONE=B*COS(ALPHR)*G

15 DONE=C*COS(PHI-ALPHR-PSI)

OPHIIN=DPHI

OPSIIN=DPSI

OPHIF=(IP*AONE*DPHIIN+IS*DONE*DPHIIN+IP*AONE*EREST/DONE*(OPSIIN

1 *DONE-OPHIIN*AONE))/ (IP*AONE**2/DONE+IS*DONE)

DPSIF=(OPHIF*AONE-EREST*(OPSIIN*DONE-OPHIIN*AONE))/DONE

PHID=PHI*150./PI

PSID=PSI*180./PI

WRITE(6,3)

3 FORMAT(*0.5X,*IMPACT*)

WRITE(6,5)PHID,OPHIF,PSID,DPSIF,PHITOT

25 FORMAT(*0.19X,*PHI=*F8.3,3X,*DPHIF=*F8.3,3X,*PSI=*F8.3,3X,

1 *DPSIF=*F8.3,3X,*PHITOT=*F8.3)

OPHI=DPHIF

OPSI=DPSIF

6 RETURN

END

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1 SUBROUTINE FREE(TIME,PHI,DPHI,PSI,DPSI)
 REAL IP,IS,LAMBDA,K
 COMMON A,B,C,R,ALPHR,PT,TORK,COFR,IP,IS,EREST,LAMBDA,DELTA,
 PHITOT,PHIPR
 T=TIME
 Z=PI/LA0.

C RECORD INITIAL VALUES

10 PHIIN=PHI
 DPHIIN=DPHI
 PSIIIN=PSI
 DPSIIN=DPSI

15 WRITE(6,5)
 5 FORMAT('0',5X,'FREE MOTION*')

C STARWHEEL MOTION

1 PHI=TORK/(2.*IS)*(T-TIME)*(T-TIME)+DPHIIN*(T-TIME)+PHIIN
 PHID=PHI/Z
 DELPHI=PHID-PHIPR
 PHITOT = PHITOT + DELPHI
 PHIPR = PHID
 DPHI=TORK/IS*(T-TIME)+DPHIIN

C PALLET MOTION

20 PSI = DPSIIN*(T-TIME) + PSIIIN
 DPSI = DPSIIN
 PSID=PSI/Z

C OUTPUT

35 WRITE(6,2)T,PHID,DPHI,PSID,DPSI,PHITOT
 2 FORMAT('0',5X,'T=',F8.3X,'PHI=',F8.3X,'PHDOT=',F8.3X,3X,
 'PSI=',F8.3X,'PSIDOT=',F8.3X,'PHITOT =',F8.3)
 9 IF(T.EO.TIME)GO TO 3

C CHECK FOR CONTINUED FREE MOTION

40 F=A*SIN(PHI-ALPHR)-B*SIN(ALPHR)-C*SIN(PHI-ALPHR-PSI)-R
 GP=C*COS(PHI-ALPHR-PSI)-B*COS(ALPHR)-A*COS(PHI-ALPHR)
 IF(F.LE.0.)GO TO 4

C CHECK FOR TOP OR BOTTOM ACTION

45 IF(GP.LE.0.)GO TO 3
 PHID=PHI/Z
 IF(PHID.LE.150.)GO TO 6
 GO TO 7

6 PHI=PHI+DELTA*Z
 PHIPR = PHI/Z
 PSI=PSI+2.*PI-LAMBDA*Z

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PSIIN = PSIIN + 2*PI*LAMBDA*Z

GO TO 3
7 PHI=PHI-DELTA*Z*2.
PHIPR = PHI/Z

PSI=PSI-2*PI*LAMBDA*Z

PHIIN = PHIIN - DELTA*Z*2.
PSIIN = PSIIN - 2*PI*LAMBDA*Z

C INCREMENT TIME

C 3 T=T+.00001

C CONTINUE FREE MOTION

C GO TO 1

C END OF FREE MOTION

4 TIME=T

RETURN

END

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APPENDIX H

SOME GEOMETRIC RELATIONSHIP

DETERMINATION OF g_{MAX}

Figure H-1 shows the geometrical relationship between the pallet pin of radius r and the right hand escape-wheel tooth when the quantity g (equation (A12) in appendix A) reaches its maximum possible absolute value. The following relationship holds between the angles α and β :

$$\alpha = \beta - \frac{\delta}{2} \quad (H1)$$

where

$$\delta = \frac{360}{N} \quad (H2)$$

and N stands for the number of teeth on the escape-wheel.

The distance \overline{ST} of the triangle OST is determined with the help of the sine law:

$$\overline{ST} = b \frac{\sin(\delta/2)}{\sin(\pi - \beta)} \quad (H3)$$

where b represents the escape-wheel radius.

Finally, g_{MAX} is obtained from:

$$g_{MAX} = \overline{ST} - \frac{r}{\tan\beta} \quad (H4)$$

To use g_{MAX} in connection with expressions derived in appendix A, it must be furnished with a minus sign to conform to the origin of the $\bar{n}_t - \bar{n}_n$ system.

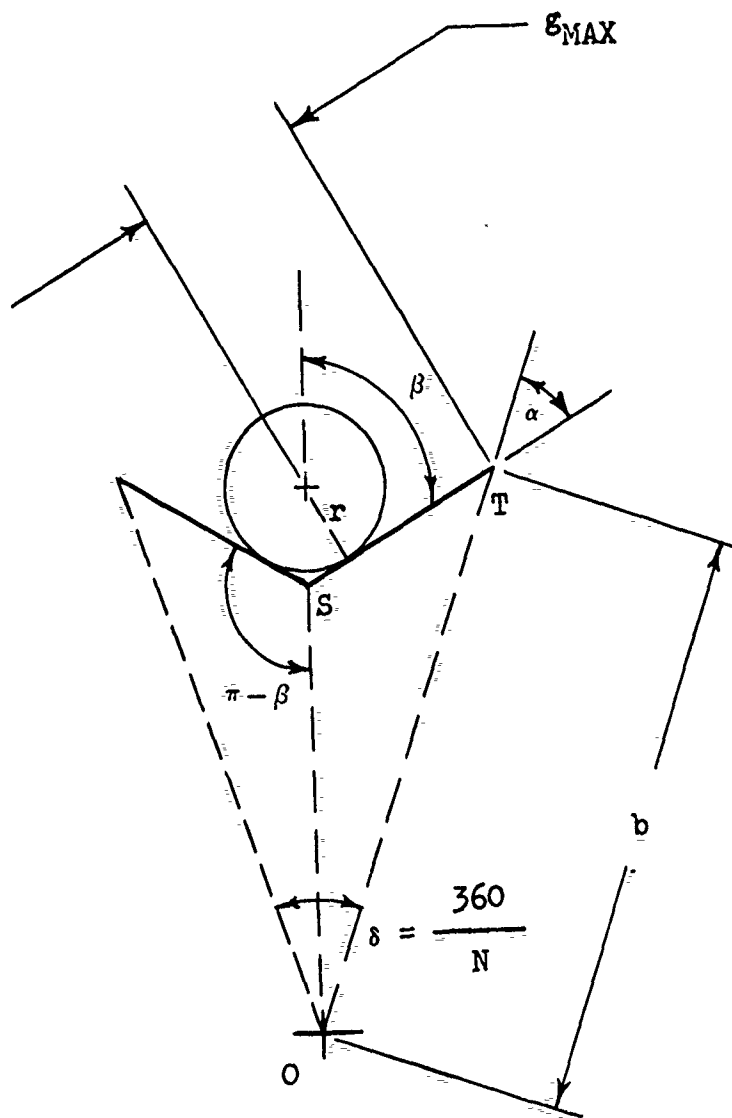


Figure H1. Configuration for g_{MAX}

DETERMINATION OF ESCAPE-WHEEL ANGLE φ_M CORRESPONDING TO $g = g_{MAX}$

The angle $\varphi = \varphi_M$, which corresponds to the maximum possible value of $g = g_{MAX}$, is obtained with the help of equation (A11) of appendix A:

$$\begin{aligned} g_{MAX}^2 + g_{MAX} [2b \cos \alpha + 2a \cos(\varphi_M - \alpha)] \\ + [a^2 + b^2 + r^2 - c^2 + 2br \sin \alpha + 2abc \cos \varphi_M - 2ars \sin(\varphi_M - \alpha)] \\ = 0 \end{aligned} \quad (H5)$$

After the expansion of the trigonometric terms $\cos(\varphi_M - \alpha)$ and $\sin(\varphi_M - \alpha)$, the following expression results:

$$L \sin \varphi_M + M \cos \varphi_M + N = 0 \quad (H6)$$

where

$$L = 2a(g_{MAX} \sin \alpha - r \cos \alpha)$$

$$M = 2a(g_{MAX} \cos \alpha + b + r \sin \alpha)$$

$$N = g_{MAX}^2 + a^2 + b^2 + r^2 - c^2 + 2b(g_{MAX} \cos \alpha + r \sin \alpha)$$

Equation (H5) may now be rewritten with the help of the following trigonometric identities:

$$\sin \varphi_M = \frac{2 \tan \left(\frac{\varphi_M}{2} \right)}{1 + \tan^2 \left(\frac{\varphi_M}{2} \right)} \quad (H7)$$

$$\cos \varphi_M = \frac{1 - \tan^2 \left(\frac{\varphi_M}{2} \right)}{1 + \tan^2 \left(\frac{\varphi_M}{2} \right)} \quad (H8)$$

This leads to:

$$(N - M)\tan^2 \left(\frac{\varphi_M}{2}\right) + 2L\tan \left(\frac{\varphi_M}{2}\right) + (M + N) = 0 \quad (H9)$$

This expression may now be solved for the angle φ_M using the solution for a quadratic equation. Accordingly,

$$\varphi_M = 2\tan^{-1} \left[\frac{-L \pm \sqrt{L^2 - N^2 + M^2}}{N - M} \right] \quad (H10)$$

The two solutions correspond to top and bottom action.

DETERMINATION OF ESCAPE-WHEEL ANGLE φ CORRESPONDING TO $g = 0$

The angle $\varphi = \varphi_0$, which is associated with the instant when the pallet pin leaves the escape-wheel tooth during coupled motion, is obtained from equation (A11) with $g = 0$.

An expression similar to equation (H6) results:

$$L_0 \sin \varphi_0 + M_0 \cos \varphi_0 + N_0 = 0 \quad (H11)$$

where

$$L_0 = -2arcos\alpha$$

$$M_0 = 2a(b + r\sin\alpha)$$

$$N_0 = a^2 + b^2 + r^2 - c^2 + 2br\sin\alpha$$

Equation (H11) is solved in the same manner as equation (H6).

This results in:

$$\varphi_0 = 2\tan^{-1} \left[\frac{-L_0 \pm \sqrt{L_0^2 - N_0^2 + M_0^2}}{N_0 - M_0} \right] \quad (H12)$$

Again, top and bottom action results are provided.

DISENGAGEMENT DISTANCE BETWEEN PALLET AND ESCAPE-WHEEL PIVOTS

Figure H-2 shows the disengagement configuration of the symmetrical pin pallet runaway escapement. The pallet angle ψ equals $\frac{\lambda}{2}$ when both pallet pins together are least advanced with respect to the escape-wheel. The center distance a is such that the escape-wheel radius b and the pallet pin radius r are collinear.

The disengagement center distance a_{dis} is determined with the help of the cosine law:

$$(b + r)^2 = a_{\text{dis}}^2 + c^2 - 2a_{\text{dis}}(c) \cos \left(\frac{\lambda}{2}\right) \quad (\text{H13})$$

From the solution of the quadratic equation, one finds:

$$a_{\text{dis}} = (c) \cos \left(\frac{\lambda}{2}\right) + \sqrt{[(c) \cos \left(\frac{\lambda}{2}\right)]^2 - [c^2 - (b + r)^2]} \quad (\text{H14})$$

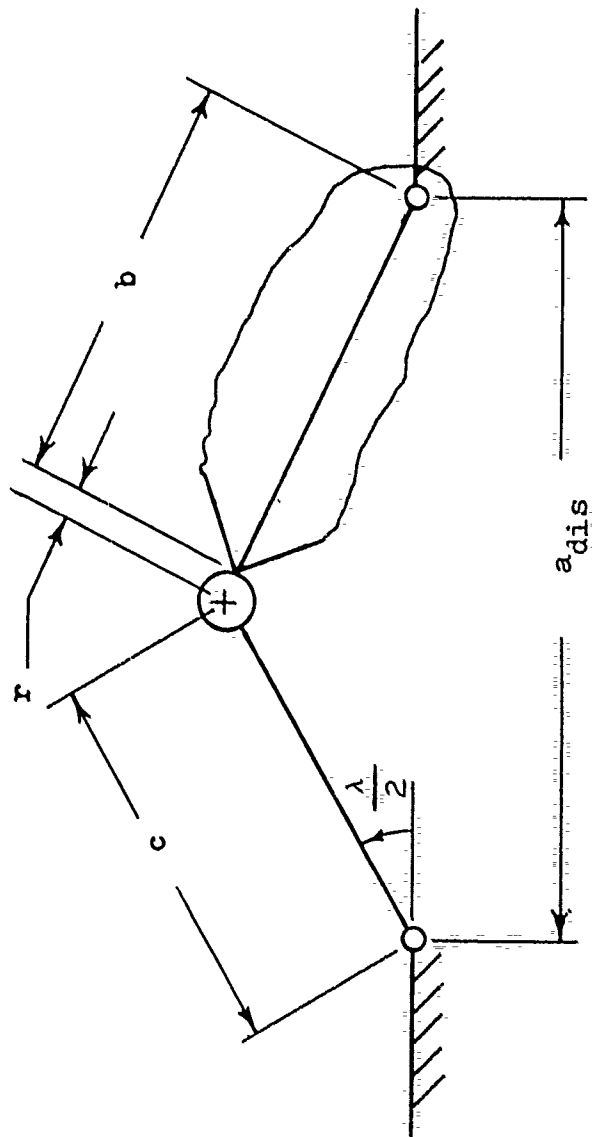


Figure H2. Disengagement condition

APPENDIX I

COMPUTER OUTPUT FOR STANDARD CONFIGURATION
WITH $\mu = .3$ AND $\varepsilon = .25$

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ALPHA = 40.0000
R = .01365
IS = .17000E-07
DELTA = 40.000
C = .30000E+00
IPAL = .91000E-07
CYCLE NO. 1

Appendix I
Std. Config.
 $\mu = .3, \epsilon = .25$

Table with columns: Cycle No., COUPLED MOTION, and various parameters (PHI, PSI, G, C, etc.) for cycles 00000 to 00300.

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| TS | .00340 | PHI = 144.491 | PHDNT = 100.859 | G = .0007 | GDDT = 24.404 | PSIOD = 60.449 | PSIODT = 183.111 | PHITOT = 11.491 |
|-------------|---------|---------------|-----------------|---------------|------------------|-----------------|------------------|-----------------|
| FREE MOTION | | | | | | | | |
| TS | .00340 | PHI = 144.491 | PHDNT = 100.859 | PSI = 311.112 | PSIODT = 143.111 | PHITOT = 11.491 | | |
| TS | .00341 | PHI = 144.511 | PHDNT = 111.271 | PSI = 311.217 | PSIODT = 143.111 | PHITOT = 11.551 | | |
| TS | .00342 | PHI = 144.518 | PHDNT = 121.433 | PSI = 311.322 | PSIODT = 143.111 | PHITOT = 11.611 | | |
| TS | .00343 | PHI = 144.591 | PHDNT = 132.095 | PSI = 311.427 | PSIODT = 143.111 | PHITOT = 11.671 | | |
| TS | .00344 | PHI = 144.770 | PHDNT = 142.504 | PSI = 311.532 | PSIODT = 143.111 | PHITOT = 11.731 | | |
| TS | .00345 | PHI = 144.854 | PHDNT = 152.918 | PSI = 311.637 | PSIODT = 143.111 | PHITOT = 11.791 | | |
| TS | .00346 | PHI = 144.945 | PHDNT = 163.330 | PSI = 311.742 | PSIODT = 143.111 | PHITOT = 11.851 | | |
| TS | .00347 | PHI = 147.041 | PHDNT = 173.742 | PSI = 311.846 | PSIODT = 143.111 | PHITOT = 11.911 | | |
| TS | .00348 | PHI = 147.144 | PHDNT = 184.153 | PSI = 311.951 | PSIODT = 143.111 | PHITOT = 11.971 | | |
| TS | .00349 | PHI = 147.252 | PHDNT = 194.565 | PSI = 312.056 | PSIODT = 143.111 | PHITOT = 12.031 | | |
| TS | .00350 | PHI = 147.367 | PHDNT = 204.977 | PSI = 312.161 | PSIODT = 143.111 | PHITOT = 12.091 | | |
| TS | .00351 | PHI = 147.477 | PHDNT = 215.389 | PSI = 312.266 | PSIODT = 143.111 | PHITOT = 12.151 | | |
| TS | .00352 | PHI = 147.594 | PHDNT = 225.800 | PSI = 312.371 | PSIODT = 143.111 | PHITOT = 12.211 | | |
| TS | .00353 | PHI = 147.724 | PHDNT = 236.212 | PSI = 312.476 | PSIODT = 143.111 | PHITOT = 12.271 | | |
| TS | .00354 | PHI = 147.864 | PHDNT = 246.624 | PSI = 312.581 | PSIODT = 143.111 | PHITOT = 12.331 | | |
| TS | .00355 | PHI = 148.029 | PHDNT = 257.036 | PSI = 312.686 | PSIODT = 143.111 | PHITOT = 12.391 | | |
| TS | .00356 | PHI = 148.179 | PHDNT = 267.447 | PSI = 312.791 | PSIODT = 143.111 | PHITOT = 12.451 | | |
| TS | .00357 | PHI = 148.335 | PHDNT = 277.859 | PSI = 312.896 | PSIODT = 143.111 | PHITOT = 12.511 | | |
| TS | .00358 | PHI = 148.497 | PHDNT = 288.271 | PSI = 313.001 | PSIODT = 143.111 | PHITOT = 12.571 | | |
| TS | .00359 | PHI = 148.645 | PHDNT = 298.683 | PSI = 313.105 | PSIODT = 143.111 | PHITOT = 12.631 | | |
| TS | .00360 | PHI = 148.840 | PHDNT = 309.095 | PSI = 313.210 | PSIODT = 143.111 | PHITOT = 12.691 | | |
| TS | .00361 | PHI = 149.020 | PHDNT = 319.506 | PSI = 313.315 | PSIODT = 143.111 | PHITOT = 12.751 | | |
| TS | .00362 | PHI = 149.206 | PHDNT = 329.914 | PSI = 313.420 | PSIODT = 143.111 | PHITOT = 12.811 | | |
| TS | .00363 | PHI = 149.394 | PHDNT = 340.330 | PSI = 313.525 | PSIODT = 143.111 | PHITOT = 12.871 | | |
| TS | .00364 | PHI = 149.586 | PHDNT = 350.742 | PSI = 313.630 | PSIODT = 143.111 | PHITOT = 12.931 | | |
| TS | .00365 | PHI = 149.800 | PHDNT = 361.153 | PSI = 313.735 | PSIODT = 143.111 | PHITOT = 12.991 | | |
| TS | .00366 | PHI = 149.010 | PHDNT = 371.565 | PSI = 313.840 | PSIODT = 143.111 | PHITOT = 13.051 | | |
| TS | .00367 | PHI = 149.225 | PHDNT = 381.977 | PSI = 313.945 | PSIODT = 143.111 | PHITOT = 13.111 | | |
| TS | .00368 | PHI = 149.447 | PHDNT = 392.389 | PSI = 314.050 | PSIODT = 143.111 | PHITOT = 13.171 | | |
| TS | .00369 | PHI = 149.675 | PHDNT = 402.800 | PSI = 314.155 | PSIODT = 143.111 | PHITOT = 13.231 | | |
| TS | .00370 | PHI = 149.909 | PHDNT = 413.212 | PSI = 314.260 | PSIODT = 143.111 | PHITOT = 13.291 | | |
| TS | .00371 | PHI = 150.149 | PHDNT = 423.624 | PSI = 314.364 | PSIODT = 143.111 | PHITOT = 13.351 | | |
| TS | .00372 | PHI = 150.394 | PHDNT = 434.036 | PSI = 314.469 | PSIODT = 143.111 | PHITOT = 13.411 | | |
| TS | .00373 | PHI = 150.646 | PHDNT = 444.447 | PSI = 314.574 | PSIODT = 143.111 | PHITOT = 13.471 | | |
| TS | .00374 | PHI = 150.904 | PHDNT = 454.859 | PSI = 314.679 | PSIODT = 143.111 | PHITOT = 13.531 | | |
| TS | .00375 | PHI = 151.167 | PHDNT = 465.271 | PSI = 314.784 | PSIODT = 143.111 | PHITOT = 13.591 | | |
| TS | .00376 | PHI = 151.437 | PHDNT = 475.683 | PSI = 314.889 | PSIODT = 143.111 | PHITOT = 13.651 | | |
| TS | .00377 | PHI = 151.712 | PHDNT = 486.095 | PSI = 314.994 | PSIODT = 143.111 | PHITOT = 13.711 | | |
| TS | .00378 | PHI = 151.994 | PHDNT = 496.506 | PSI = 315.099 | PSIODT = 143.111 | PHITOT = 13.771 | | |
| TS | .00379 | PHI = 152.281 | PHDNT = 506.914 | PSI = 315.204 | PSIODT = 143.111 | PHITOT = 13.831 | | |
| TS | .00380 | PHI = 152.575 | PHDNT = 517.329 | PSI = 315.309 | PSIODT = 143.111 | PHITOT = 13.891 | | |
| TS | .00381 | PHI = 152.874 | PHDNT = 527.742 | PSI = 315.414 | PSIODT = 143.111 | PHITOT = 13.951 | | |
| TS | .00382 | PHI = 153.179 | PHDNT = 538.153 | PSI = 315.518 | PSIODT = 143.111 | PHITOT = 14.011 | | |
| VP | -16.798 | VS = 44.239 | | | | | | |
| IMPACT | | | | | | | | |
| VP | -2.398 | VS = -17.657 | DPHIF = 214.794 | PSI = 315.518 | DPISF = 26.138 | PHITOT = 19.179 | | |
| FREE MOTION | | | | | | | | |
| TS | .00382 | PHI = 194.179 | PHDNT = 214.794 | PSI = 315.518 | PSIODT = 26.138 | PHITOT = 19.179 | | |
| TS | .00383 | PHI = 194.059 | PHDNT = 204.382 | PSI = 315.533 | PSIODT = 26.138 | PHITOT = 19.059 | | |
| VP | -2.400 | VS = -16.740 | | | | | | |
| FREE MOTION | | | | | | | | |
| TS | .00383 | PHI = 194.059 | PHDNT = 204.382 | PSI = 315.533 | PSIODT = 26.138 | PHITOT = 19.059 | | |
| TS | .00384 | PHI = 193.945 | PHDNT = 193.970 | PSI = 315.546 | PSIODT = 26.138 | PHITOT = 18.945 | | |
| VP | -2.402 | VS = -15.832 | | | | | | |
| FREE MOTION | | | | | | | | |
| TS | .00384 | PHI = 193.945 | PHDNT = 193.970 | PSI = 315.546 | PSIODT = 26.138 | PHITOT = 18.945 | | |

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| IN | 00385 | 00386 | 00387 | 00388 | 00389 | 00390 | 00391 | 00392 | 00393 | 00394 | 00395 | 00396 | 00397 | 00398 | 00399 | 00400 | 00401 | 00402 | 00403 | 00404 | 00405 | 00406 | 00407 | 00408 | 00409 | 00410 | 00411 | 00412 | 00413 | 00414 | 00415 | 00416 | 00417 | 00418 | 00419 | 00420 | 00421 | 00422 | 00423 | 00424 | 00425 | 00426 | 00427 | 00428 | | | | | | | | | | | | | | | | | | | | |
|----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| | 193.937 | 193.938 | 193.939 | 193.940 | 193.941 | 193.942 | 193.943 | 193.944 | 193.945 | 193.946 | 193.947 | 193.948 | 193.949 | 193.950 | 193.951 | 193.952 | 193.953 | 193.954 | 193.955 | 193.956 | 193.957 | 193.958 | 193.959 | 193.960 | 193.961 | 193.962 | 193.963 | 193.964 | 193.965 | 193.966 | 193.967 | 193.968 | 193.969 | 193.970 | 193.971 | 193.972 | 193.973 | 193.974 | 193.975 | 193.976 | 193.977 | 193.978 | 193.979 | 193.980 | 193.981 | 193.982 | 193.983 | 193.984 | 193.985 | 193.986 | 193.987 | 193.988 | 193.989 | 193.990 | 193.991 | 193.992 | 193.993 | 193.994 | 193.995 | 193.996 | 193.997 | 193.998 | 193.999 | 194.000 |
| | 193.937 | 193.938 | 193.939 | 193.940 | 193.941 | 193.942 | 193.943 | 193.944 | 193.945 | 193.946 | 193.947 | 193.948 | 193.949 | 193.950 | 193.951 | 193.952 | 193.953 | 193.954 | 193.955 | 193.956 | 193.957 | 193.958 | 193.959 | 193.960 | 193.961 | 193.962 | 193.963 | 193.964 | 193.965 | 193.966 | 193.967 | 193.968 | 193.969 | 193.970 | 193.971 | 193.972 | 193.973 | 193.974 | 193.975 | 193.976 | 193.977 | 193.978 | 193.979 | 193.980 | 193.981 | 193.982 | 193.983 | 193.984 | 193.985 | 193.986 | 193.987 | 193.988 | 193.989 | 193.990 | 193.991 | 193.992 | 193.993 | 193.994 | 193.995 | 193.996 | 193.997 | 193.998 | 193.999 | 194.000 |
| | 193.937 | 193.938 | 193.939 | 193.940 | 193.941 | 193.942 | 193.943 | 193.944 | 193.945 | 193.946 | 193.947 | 193.948 | 193.949 | 193.950 | 193.951 | 193.952 | 193.953 | 193.954 | 193.955 | 193.956 | 193.957 | 193.958 | 193.959 | 193.960 | 193.961 | 193.962 | 193.963 | 193.964 | 193.965 | 193.966 | 193.967 | 193.968 | 193.969 | 193.970 | 193.971 | 193.972 | 193.973 | 193.974 | 193.975 | 193.976 | 193.977 | 193.978 | 193.979 | 193.980 | 193.981 | 193.982 | 193.983 | 193.984 | 193.985 | 193.986 | 193.987 | 193.988 | 193.989 | 193.990 | 193.991 | 193.992 | 193.993 | 193.994 | 193.995 | 193.996 | 193.997 | 193.998 | 193.999 | 194.000 |

| | | | | | | | | |
|--------|---------|--------|------|---------|--------|----------|-------|--------|
| PS1001 | 316.071 | 1.108 | PS10 | 316.071 | PS1001 | -6.435 | PM101 | 14.242 |
| PS1002 | 316.059 | 1.643 | PS10 | 316.059 | PS1002 | -10.137 | PM102 | 14.306 |
| PS1003 | 316.047 | 2.178 | PS10 | 316.047 | PS1003 | -13.639 | PM103 | 14.366 |
| PS1004 | 315.994 | 3.264 | PS10 | 315.994 | PS1004 | -20.037 | PM104 | 14.411 |
| PS1005 | 315.927 | 4.306 | PS10 | 315.927 | PS1005 | -26.627 | PM105 | 14.454 |
| PS1006 | 315.841 | 5.363 | PS10 | 315.841 | PS1006 | -33.206 | PM106 | 14.496 |
| PS1007 | 315.737 | 6.411 | PS10 | 315.737 | PS1007 | -39.779 | PM107 | 14.536 |
| PS1008 | 315.621 | 8.481 | PS10 | 315.621 | PS1008 | -52.045 | PM108 | 14.574 |
| PS1009 | 315.511 | 10.508 | PS10 | 315.511 | PS1009 | -65.024 | PM109 | 14.610 |
| PS1010 | 315.411 | 12.476 | PS10 | 315.411 | PS1010 | -77.845 | PM110 | 14.644 |
| PS1011 | 315.311 | 14.342 | PS10 | 315.311 | PS1011 | -91.392 | PM111 | 14.676 |
| PS1012 | 315.211 | 16.216 | PS10 | 315.211 | PS1012 | -103.914 | PM112 | 14.706 |
| PS1013 | 315.111 | 17.921 | PS10 | 315.111 | PS1013 | -116.222 | PM113 | 14.734 |
| PS1014 | 315.011 | 19.642 | PS10 | 315.011 | PS1014 | -128.274 | PM114 | 14.760 |
| PS1015 | 314.911 | 21.223 | PS10 | 314.911 | PS1015 | -140.042 | PM115 | 14.784 |
| PS1016 | 314.811 | 22.710 | PS10 | 314.811 | PS1016 | -151.462 | PM116 | 14.806 |
| PS1017 | 314.711 | 24.191 | PS10 | 314.711 | PS1017 | -162.562 | PM117 | 14.826 |
| PS1018 | 314.611 | 25.392 | PS10 | 314.611 | PS1018 | -173.244 | PM118 | 14.844 |
| PS1019 | 314.511 | 26.592 | PS10 | 314.511 | PS1019 | -183.566 | PM119 | 14.860 |
| PS1020 | 314.411 | 27.671 | PS10 | 314.411 | PS1020 | -193.307 | PM120 | 14.874 |
| PS1021 | 314.311 | 28.656 | PS10 | 314.311 | PS1021 | -202.528 | PM121 | 14.886 |
| PS1022 | 314.211 | 29.560 | PS10 | 314.211 | PS1022 | -211.440 | PM122 | 14.896 |
| PS1023 | 314.111 | 30.373 | PS10 | 314.111 | PS1023 | -219.732 | PM123 | 14.904 |
| PS1024 | 314.011 | 31.006 | PS10 | 314.011 | PS1024 | -227.487 | PM124 | 14.910 |
| PS1025 | 313.911 | 31.581 | PS10 | 313.911 | PS1025 | -234.697 | PM125 | 14.914 |
| PS1026 | 313.811 | 32.092 | PS10 | 313.811 | PS1026 | -241.357 | PM126 | 14.916 |

| | | | | | | | | |
|--------|---------|--------|------|---------|--------|----------|-------|--------|
| PS1001 | 241.357 | 48.582 | PS10 | 241.357 | PS1001 | -241.357 | PM101 | 31.844 |
| PS1002 | 241.357 | 48.644 | PS10 | 241.357 | PS1002 | -241.357 | PM102 | 31.920 |
| PS1003 | 241.357 | 48.705 | PS10 | 241.357 | PS1003 | -241.357 | PM103 | 32.003 |
| PS1004 | 241.357 | 48.766 | PS10 | 241.357 | PS1004 | -241.357 | PM104 | 32.091 |
| PS1005 | 241.357 | 48.827 | PS10 | 241.357 | PS1005 | -241.357 | PM105 | 32.186 |
| PS1006 | 241.357 | 48.888 | PS10 | 241.357 | PS1006 | -241.357 | PM106 | 32.286 |
| PS1007 | 241.357 | 48.949 | PS10 | 241.357 | PS1007 | -241.357 | PM107 | 32.393 |
| PS1008 | 241.357 | 49.010 | PS10 | 241.357 | PS1008 | -241.357 | PM108 | 32.505 |
| PS1009 | 241.357 | 49.071 | PS10 | 241.357 | PS1009 | -241.357 | PM109 | 32.623 |
| PS1010 | 241.357 | 49.132 | PS10 | 241.357 | PS1010 | -241.357 | PM110 | 32.747 |
| PS1011 | 241.357 | 49.193 | PS10 | 241.357 | PS1011 | -241.357 | PM111 | 32.878 |
| PS1012 | 241.357 | 49.254 | PS10 | 241.357 | PS1012 | -241.357 | PM112 | 33.014 |
| PS1013 | 241.357 | 49.315 | PS10 | 241.357 | PS1013 | -241.357 | PM113 | 33.156 |
| PS1014 | 241.357 | 49.376 | PS10 | 241.357 | PS1014 | -241.357 | PM114 | 33.304 |
| PS1015 | 241.357 | 49.437 | PS10 | 241.357 | PS1015 | -241.357 | PM115 | 33.458 |
| PS1016 | 241.357 | 49.498 | PS10 | 241.357 | PS1016 | -241.357 | PM116 | 33.618 |
| PS1017 | 241.357 | 49.559 | PS10 | 241.357 | PS1017 | -241.357 | PM117 | 33.784 |
| PS1018 | 241.357 | 49.620 | PS10 | 241.357 | PS1018 | -241.357 | PM118 | 33.956 |
| PS1019 | 241.357 | 49.681 | PS10 | 241.357 | PS1019 | -241.357 | PM119 | 34.134 |
| PS1020 | 241.357 | 49.742 | PS10 | 241.357 | PS1020 | -241.357 | PM120 | 34.318 |
| PS1021 | 241.357 | 49.803 | PS10 | 241.357 | PS1021 | -241.357 | PM121 | 34.508 |
| PS1022 | 241.357 | 49.864 | PS10 | 241.357 | PS1022 | -241.357 | PM122 | 34.704 |
| PS1023 | 241.357 | 49.925 | PS10 | 241.357 | PS1023 | -241.357 | PM123 | 34.906 |
| PS1024 | 241.357 | 49.986 | PS10 | 241.357 | PS1024 | -241.357 | PM124 | 35.114 |
| PS1025 | 241.357 | 50.047 | PS10 | 241.357 | PS1025 | -241.357 | PM125 | 35.327 |
| PS1026 | 241.357 | 50.108 | PS10 | 241.357 | PS1026 | -241.357 | PM126 | 35.547 |
| PS1027 | 241.357 | 50.169 | PS10 | 241.357 | PS1027 | -241.357 | PM127 | 35.773 |
| PS1028 | 241.357 | 50.230 | PS10 | 241.357 | PS1028 | -241.357 | PM128 | 36.004 |
| PS1029 | 241.357 | 50.291 | PS10 | 241.357 | PS1029 | -241.357 | PM129 | 36.242 |
| PS1030 | 241.357 | 50.352 | PS10 | 241.357 | PS1030 | -241.357 | PM130 | 36.486 |
| PS1031 | 241.357 | 50.413 | PS10 | 241.357 | PS1031 | -241.357 | PM131 | 36.735 |
| PS1032 | 241.357 | 50.474 | PS10 | 241.357 | PS1032 | -241.357 | PM132 | 37.000 |
| PS1033 | 241.357 | 50.535 | PS10 | 241.357 | PS1033 | -241.357 | PM133 | 37.282 |
| PS1034 | 241.357 | 50.596 | PS10 | 241.357 | PS1034 | -241.357 | PM134 | 37.583 |
| PS1035 | 241.357 | 50.657 | PS10 | 241.357 | PS1035 | -241.357 | PM135 | 37.903 |

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IE .00680 PHI 133.072 PHDOT= 492.808 PSI= 43.782 PSINOT=-241.357 PHITOT = 38.012
 IE .00681 PHI 133.358 PHDOT= 503.226 PSI= 43.803 PSINOT=-241.357 PHITOT = 38.358
 IE .00682 PHI 133.644 PHDOT= 513.612 PSI= 43.825 PSINOT=-241.357 PHITOT = 38.699
 IE .00683 PHI 133.930 PHDOT= 524.044 PSI= 43.847 PSINOT=-241.357 PHITOT = 39.040
 IE .00684 PHI 134.216 PHDOT= 534.556 PSI= 43.869 PSINOT=-241.357 PHITOT = 39.381
 IE .00685 PHI 134.502 PHDOT= 544.867 PSI= 43.890 PSINOT=-241.357 PHITOT = 39.722
 IE .00686 PHI 134.874 PHDOT= 555.279 PSI= 42.912 PSINOT=-241.357 PHITOT = 39.874
 IE .00687 PHI 135.165 PHDOT= 565.691 PSI= 42.774 PSINOT=-241.357 PHITOT = 40.195
 IE .00688 PHI 135.522 PHDOT= 576.103 PSI= 42.635 PSINOT=-241.357 PHITOT = 40.522
 VPE = 14.102 VS = 46.718

IMPACT Cycle No. 2

VPE = 7.066 VS = 21.769
 DPMIF = 280.455 PSI = 42.635 DPSIF = 120.910 PHITOT = 40.522
 FREE MOTION
 IE .00689 PHI 135.522 PHDOT= 280.455 PSI= 42.635 PSINOT=-120.910 PHITOT = 40.522
 IE .00689 PHI 135.365 PHDOT= 270.043 PSI= 42.586 PSINOT=-120.910 PHITOT = 40.385
 VPE = 7.079 VS = 20.809

FREE MOTION

IE .00689 PHI 135.365 PHDOT= 270.043 PSI= 42.586 PSINOT=-120.910 PHITOT = 40.385
 IE .00690 PHI 135.923 PHDOT= 259.631 PSI= 42.457 PSINOT=-120.910 PHITOT = 40.212
 VPE = 7.092 VS = 19.850
 FREE MOTION
 IE .00690 PHI 135.213 PHDOT= 259.631 PSI= 42.497 PSINOT=-120.910 PHITOT = 40.213
 IE .00691 PHI 135.067 PHDOT= 249.220 PSI= 42.428 PSINOT=-120.910 PHITOT = 40.067
 VPE = 7.105 VS = 19.914

FREE MOTION

IE .00691 PHI 135.067 PHDOT= 249.220 PSI= 42.428 PSINOT=-120.910 PHITOT = 40.067
 IE .00692 PHI 134.927 PHDOT= 238.808 PSI= 42.358 PSINOT=-120.910 PHITOT = 39.927
 IE .00693 PHI 134.783 PHDOT= 228.396 PSI= 42.289 PSINOT=-120.910 PHITOT = 39.783
 IE .00694 PHI 134.645 PHDOT= 217.986 PSI= 42.220 PSINOT=-120.910 PHITOT = 39.645
 IE .00695 PHI 134.544 PHDOT= 207.573 PSI= 42.151 PSINOT=-120.910 PHITOT = 39.544
 IE .00696 PHI 134.428 PHDOT= 197.161 PSI= 42.081 PSINOT=-120.910 PHITOT = 39.428
 IE .00697 PHI 134.318 PHDOT= 186.749 PSI= 42.012 PSINOT=-120.910 PHITOT = 39.318
 IE .00698 PHI 134.214 PHDOT= 176.337 PSI= 41.943 PSINOT=-120.910 PHITOT = 39.214
 IE .00699 PHI 134.116 PHDOT= 165.926 PSI= 41.873 PSINOT=-120.910 PHITOT = 39.116
 IE .00700 PHI 134.023 PHDOT= 155.514 PSI= 41.804 PSINOT=-120.910 PHITOT = 39.023
 IE .00701 PHI 133.937 PHDOT= 145.102 PSI= 41.735 PSINOT=-120.910 PHITOT = 38.937
 IE .00702 PHI 133.857 PHDOT= 134.690 PSI= 41.666 PSINOT=-120.910 PHITOT = 38.857
 IE .00703 PHI 133.783 PHDOT= 124.278 PSI= 41.596 PSINOT=-120.910 PHITOT = 38.783
 IE .00704 PHI 133.715 PHDOT= 113.867 PSI= 41.527 PSINOT=-120.910 PHITOT = 38.715
 IE .00705 PHI 133.653 PHDOT= 103.455 PSI= 41.458 PSINOT=-120.910 PHITOT = 38.653
 IE .00706 PHI 133.596 PHDOT= 93.043 PSI= 41.388 PSINOT=-120.910 PHITOT = 38.596
 IE .00707 PHI 133.546 PHDOT= 82.631 PSI= 41.319 PSINOT=-120.910 PHITOT = 38.546
 IE .00708 PHI 133.502 PHDOT= 72.220 PSI= 41.250 PSINOT=-120.910 PHITOT = 38.502
 IE .00709 PHI 133.463 PHDOT= 61.808 PSI= 41.181 PSINOT=-120.910 PHITOT = 38.463
 IE .00710 PHI 133.431 PHDOT= 51.396 PSI= 41.111 PSINOT=-120.910 PHITOT = 38.431
 IE .00711 PHI 133.404 PHDOT= 40.984 PSI= 41.042 PSINOT=-120.910 PHITOT = 38.404
 IE .00712 PHI 133.384 PHDOT= 30.573 PSI= 40.973 PSINOT=-120.910 PHITOT = 38.384
 IE .00713 PHI 133.369 PHDOT= 20.161 PSI= 40.904 PSINOT=-120.910 PHITOT = 38.369
 IE .00714 PHI 133.361 PHDOT= 9.749 PSI= 40.834 PSINOT=-120.910 PHITOT = 38.361
 IE .00715 PHI 133.358 PHDOT= .663 PSI= 40.765 PSINOT=-120.910 PHITOT = 38.358
 IE .00716 PHI 133.361 PHDOT= 11.074 PSI= 40.696 PSINOT=-120.910 PHITOT = 38.361
 IE .00717 PHI 133.371 PHDOT= 21.486 PSI= 40.627 PSINOT=-120.910 PHITOT = 38.371
 IE .00718 PHI 133.386 PHDOT= 31.898 PSI= 40.557 PSINOT=-120.910 PHITOT = 38.386
 IE .00719 PHI 133.407 PHDOT= 42.310 PSI= 40.488 PSINOT=-120.910 PHITOT = 38.407
 IE .00720 PHI 133.435 PHDOT= 52.722 PSI= 40.419 PSINOT=-120.910 PHITOT = 38.435
 VPE = 7.063 VS = 3.684

IMPACT

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| | | | | | | |
|----------------|--------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| VP= -5.503 | VS= -4.183 | DPHIF= 133.435 | OPHIF= -117.116 | PSI= 40.419 | OPPSIF= -94.466 | PHITOT= 38.435 |
| FREE MOTION | | | | | | |
| T= .00720 | PHI= 133.435 | PHOOT= -117.116 | PSI= 40.419 | PSIDOT= -94.466 | PHITOT = 38.435 | |
| T= .00721 | PHI= 133.370 | PHOOT= -106.706 | PSI= 40.356 | PSIDOT= -94.466 | PHITOT = 38.370 | |
| VP= -5.504 | VS= -7.432 | | | | | |
| FREE MOTION | | | | | | |
| T= .00721 | PHI= 133.370 | PHOOT= -106.706 | PSI= 40.344 | PSIDOT= -94.466 | PHITOT = 38.370 | |
| T= .00722 | PHI= 133.312 | PHOOT= -96.292 | PSI= 40.310 | PSIDOT= -94.466 | PHITOT = 38.312 | |
| VP= -5.505 | VS= -6.687 | | | | | |
| FREE MOTION | | | | | | |
| T= .00722 | PHI= 133.312 | PHOOT= -96.292 | PSI= 40.310 | PSIDOT= -94.466 | PHITOT = 38.312 | |
| T= .00723 | PHI= 133.260 | PHOOT= -85.880 | PSI= 40.256 | PSIDOT= -94.466 | PHITOT = 38.260 | |
| VP= -5.506 | VS= -5.947 | | | | | |
| FREE MOTION | | | | | | |
| T= .00723 | PHI= 133.260 | PHOOT= -85.880 | PSI= 40.256 | PSIDOT= -94.466 | PHITOT = 38.260 | |
| T= .00724 | PHI= 133.214 | PHOOT= -75.468 | PSI= 40.202 | PSIDOT= -94.466 | PHITOT = 38.214 | |
| VP= -5.503 | VS= -5.214 | | | | | |
| IMPACT | | | | | | |
| VP= -5.661 | VS= -5.533 | DPHIF= 133.214 | OPHIF= -80.092 | PSI= 40.202 | OPPSIF= -93.736 | PHITOT= 38.214 |
| COUPLED MOTION | | | | | | |
| T= .00724 | PHI= 133.214 | PHIDOT= -80.092 | G= -0.522 | GDOT= -16.592 | PSID= 40.204 | PHITOT = 38.214 |
| T= .00724 | PHI= 132.830 | PHIDOT= -53.464 | G= -0.536 | GDOT= -10.990 | PSID= 39.754 | PHITOT = 37.830 |
| T= .00744 | PHI= 132.604 | PHIDOT= -25.344 | G= -0.544 | GDOT= -5.146 | PSID= 39.492 | PHITOT = 37.404 |
| T= .00746 | PHI= 132.573 | PHIDOT= -18.176 | G= -0.545 | GDOT= -3.715 | PSID= 39.456 | PHITOT = 37.373 |
| T= .00749 | PHI= 132.552 | PHIDOT= -10.461 | G= -0.546 | GDOT= -2.240 | PSID= 39.432 | PHITOT = 37.352 |
| T= .00751 | PHI= 132.545 | PHIDOT= -3.344 | G= -0.546 | GDOT= -1.581 | PSID= 39.424 | PHITOT = 37.345 |
| T= .00751 | PHI= 132.541 | PHIDOT= -2.731 | G= -0.547 | GDOT= -1.762 | PSID= 39.420 | PHITOT = 37.341 |
| T= .00752 | PHI= 132.540 | PHIDOT= -1.922 | G= -0.547 | GDOT= -1.393 | PSID= 39.419 | PHITOT = 37.340 |
| T= .00753 | PHI= 132.540 | PHIDOT= -1.114 | G= -0.547 | GDOT= -0.921 | PSID= 39.418 | PHITOT = 37.340 |
| T= .00753 | PHI= 132.540 | PHIDOT= -0.911 | G= -0.547 | GDOT= -0.819 | PSID= 39.418 | PHITOT = 37.340 |
| T= .00753 | PHI= 132.540 | PHIDOT= -0.171 | G= -0.547 | GDOT= -0.015 | PSID= 39.418 | PHITOT = 37.340 |
| T= .00753 | PHI= 132.540 | PHIDOT= -0.251 | G= -0.547 | GDOT= -0.048 | PSID= 39.418 | PHITOT = 37.340 |
| T= .00754 | PHI= 132.540 | PHIDOT= -0.493 | G= -0.547 | GDOT= -0.100 | PSID= 39.418 | PHITOT = 37.340 |
| T= .00754 | PHI= 132.540 | PHIDOT= -0.650 | G= -0.547 | GDOT= -0.133 | PSID= 39.418 | PHITOT = 37.340 |
| T= .00755 | PHI= 132.541 | PHIDOT= -0.960 | G= -0.547 | GDOT= -0.198 | PSID= 39.419 | PHITOT = 37.341 |
| T= .00755 | PHI= 132.541 | PHIDOT= -1.248 | G= -0.547 | GDOT= -0.263 | PSID= 39.420 | PHITOT = 37.342 |
| T= .00756 | PHI= 132.542 | PHIDOT= -1.607 | G= -0.547 | GDOT= -0.303 | PSID= 39.421 | PHITOT = 37.342 |
| T= .00756 | PHI= 132.542 | PHIDOT= -1.924 | G= -0.546 | GDOT= -0.324 | PSID= 39.422 | PHITOT = 37.342 |
| T= .00758 | PHI= 132.546 | PHIDOT= -2.563 | G= -0.546 | GDOT= -0.354 | PSID= 39.425 | PHITOT = 37.344 |
| T= .00759 | PHI= 132.546 | PHIDOT= -3.201 | G= -0.546 | GDOT= -0.395 | PSID= 39.431 | PHITOT = 37.351 |
| T= .00761 | PHI= 132.551 | PHIDOT= -4.474 | G= -0.546 | GDOT= -0.515 | PSID= 39.439 | PHITOT = 37.359 |
| T= .00769 | PHI= 132.559 | PHIDOT= -5.748 | G= -0.546 | GDOT= -0.695 | PSID= 39.443 | PHITOT = 37.379 |
| T= .00774 | PHI= 132.579 | PHIDOT= -8.284 | G= -0.545 | GDOT= -1.095 | PSID= 39.447 | PHITOT = 37.379 |
| T= .00779 | PHI= 132.606 | PHIDOT= -10.814 | G= -0.544 | GDOT= -1.695 | PSID= 39.446 | PHITOT = 37.379 |
| T= .00784 | PHI= 132.641 | PHIDOT= -13.335 | G= -0.543 | GDOT= -2.213 | PSID= 39.436 | PHITOT = 37.366 |
| T= .00784 | PHI= 132.683 | PHIDOT= -15.834 | G= -0.542 | GDOT= -2.710 | PSID= 39.536 | PHITOT = 37.361 |
| T= .00794 | PHI= 132.787 | PHIDOT= -20.777 | G= -0.538 | GDOT= -3.245 | PSID= 39.582 | PHITOT = 37.343 |
| T= .00804 | PHI= 132.920 | PHIDOT= -25.624 | G= -0.533 | GDOT= -3.824 | PSID= 39.704 | PHITOT = 37.287 |
| T= .00814 | PHI= 133.081 | PHIDOT= -30.347 | G= -0.527 | GDOT= -4.427 | PSID= 39.859 | PHITOT = 37.202 |
| T= .00824 | PHI= 133.269 | PHIDOT= -34.961 | G= -0.520 | GDOT= -5.074 | PSID= 40.047 | PHITOT = 37.081 |
| T= .00834 | PHI= 133.481 | PHIDOT= -39.387 | G= -0.513 | GDOT= -5.763 | PSID= 40.268 | PHITOT = 36.924 |
| T= .00844 | PHI= 133.719 | PHIDOT= -43.674 | G= -0.504 | GDOT= -6.494 | PSID= 40.523 | PHITOT = 36.719 |
| T= .00854 | PHI= 133.981 | PHIDOT= -47.794 | G= -0.494 | GDOT= -7.264 | PSID= 40.810 | PHITOT = 36.481 |
| T= .00864 | PHI= 134.266 | PHIDOT= -51.749 | G= -0.484 | GDOT= -8.084 | PSID= 41.131 | PHITOT = 36.214 |

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|---|--------|-----|---------|--------|---------|---|--------|------|--------|------|--------|--------|---------|-------|--------|
| T | .00874 | PHI | 136.574 | PHIDOT | 55.527 | G | -.0473 | GOOT | 11.611 | PSID | 41.869 | PSIDOT | 76.100 | PHIOT | 39.902 |
| T | .00884 | PHI | 136.902 | PHIDOT | 59.137 | G | -.0460 | GOOT | 12.654 | PSID | 42.287 | PSIDOT | 75.729 | PHIOT | 40.251 |
| T | .00894 | PHI | 136.251 | PHIDOT | 62.365 | G | -.0447 | GOOT | 13.472 | PSID | 43.719 | PSIDOT | 81.328 | PHIOT | 40.819 |
| T | .00904 | PHI | 136.519 | PHIDOT | 65.831 | G | -.0433 | GOOT | 14.267 | PSID | 45.203 | PSIDOT | 86.897 | PHIOT | 41.405 |
| T | .00914 | PHI | 136.005 | PHIDOT | 69.634 | G | -.0419 | GOOT | 15.038 | PSID | 46.733 | PSIDOT | 92.437 | PHIOT | 41.999 |
| T | .00924 | PHI | 136.409 | PHIDOT | 71.883 | G | -.0403 | GOOT | 15.786 | PSID | 48.274 | PSIDOT | 97.948 | PHIOT | 42.594 |
| T | .00934 | PHI | 136.829 | PHIDOT | 74.444 | G | -.0387 | GOOT | 16.512 | PSID | 49.825 | PSIDOT | 103.431 | PHIOT | 43.198 |
| T | .00944 | PHI | 137.264 | PHIDOT | 77.368 | G | -.0370 | GOOT | 17.216 | PSID | 51.386 | PSIDOT | 108.886 | PHIOT | 43.804 |
| T | .00954 | PHI | 137.715 | PHIDOT | 79.881 | G | -.0353 | GOOT | 17.899 | PSID | 52.955 | PSIDOT | 114.317 | PHIOT | 44.410 |
| T | .00964 | PHI | 138.179 | PHIDOT | 82.284 | G | -.0335 | GOOT | 18.562 | PSID | 54.530 | PSIDOT | 119.723 | PHIOT | 45.016 |
| T | .00974 | PHI | 138.657 | PHIDOT | 84.595 | G | -.0316 | GOOT | 19.206 | PSID | 56.111 | PSIDOT | 125.106 | PHIOT | 45.622 |
| T | .00984 | PHI | 139.148 | PHIDOT | 86.795 | G | -.0296 | GOOT | 19.831 | PSID | 57.697 | PSIDOT | 130.470 | PHIOT | 46.228 |
| T | .00994 | PHI | 139.652 | PHIDOT | 88.902 | G | -.0276 | GOOT | 20.438 | PSID | 59.287 | PSIDOT | 135.815 | PHIOT | 46.834 |
| T | .01004 | PHI | 140.167 | PHIDOT | 90.924 | G | -.0255 | GOOT | 21.029 | PSID | 60.882 | PSIDOT | 141.143 | PHIOT | 47.440 |
| T | .01014 | PHI | 140.684 | PHIDOT | 92.874 | G | -.0234 | GOOT | 21.602 | PSID | 62.477 | PSIDOT | 146.458 | PHIOT | 48.046 |
| T | .01024 | PHI | 141.211 | PHIDOT | 94.754 | G | -.0212 | GOOT | 22.166 | PSID | 64.072 | PSIDOT | 151.761 | PHIOT | 48.652 |
| T | .01034 | PHI | 141.759 | PHIDOT | 96.574 | G | -.0190 | GOOT | 22.705 | PSID | 65.667 | PSIDOT | 157.055 | PHIOT | 49.258 |
| T | .01044 | PHI | 142.334 | PHIDOT | 98.341 | G | -.0167 | GOOT | 23.235 | PSID | 67.262 | PSIDOT | 162.341 | PHIOT | 49.864 |
| T | .01054 | PHI | 142.906 | PHIDOT | 100.064 | G | -.0143 | GOOT | 23.750 | PSID | 68.857 | PSIDOT | 167.622 | PHIOT | 50.470 |
| T | .01064 | PHI | 143.484 | PHIDOT | 101.747 | G | -.0119 | GOOT | 24.252 | PSID | 70.452 | PSIDOT | 172.901 | PHIOT | 51.076 |
| T | .01074 | PHI | 144.072 | PHIDOT | 103.394 | G | -.0095 | GOOT | 24.740 | PSID | 72.047 | PSIDOT | 178.179 | PHIOT | 51.682 |
| T | .01084 | PHI | 144.669 | PHIDOT | 105.011 | G | -.0070 | GOOT | 25.214 | PSID | 73.642 | PSIDOT | 183.459 | PHIOT | 52.288 |
| T | .01094 | PHI | 145.275 | PHIDOT | 106.607 | G | -.0044 | GOOT | 25.676 | PSID | 75.237 | PSIDOT | 188.742 | PHIOT | 52.894 |
| T | .01104 | PHI | 145.891 | PHIDOT | 108.181 | G | -.0018 | GOOT | 26.124 | PSID | 76.832 | PSIDOT | 194.031 | PHIOT | 53.499 |
| T | .01114 | PHI | 146.515 | PHIDOT | 109.730 | G | .0008 | GOOT | 26.559 | PSID | 78.427 | PSIDOT | 199.328 | PHIOT | 54.105 |

FREE MOTION

| | | | | | | | | | | | |
|---|--------|-----|---------|--------|---------|-----|---------|--------|---------|-------|--------|
| T | .01114 | PHI | 146.515 | PHIDOT | 109.739 | PSI | 311.156 | PSIDOT | 199.328 | PHIOT | 51.515 |
| T | .01115 | PHI | 146.581 | PHIDOT | 120.151 | PSI | 311.270 | PSIDOT | 199.328 | PHIOT | 51.581 |
| T | .01116 | PHI | 146.653 | PHIDOT | 130.563 | PSI | 311.345 | PSIDOT | 199.328 | PHIOT | 51.653 |
| T | .01117 | PHI | 146.730 | PHIDOT | 140.974 | PSI | 311.399 | PSIDOT | 199.328 | PHIOT | 51.730 |
| T | .01118 | PHI | 146.814 | PHIDOT | 151.386 | PSI | 311.413 | PSIDOT | 199.328 | PHIOT | 51.814 |
| T | .01119 | PHI | 146.904 | PHIDOT | 161.798 | PSI | 311.727 | PSIDOT | 199.328 | PHIOT | 52.000 |
| T | .01120 | PHI | 147.000 | PHIDOT | 172.210 | PSI | 311.961 | PSIDOT | 199.328 | PHIOT | 52.209 |
| T | .01121 | PHI | 147.101 | PHIDOT | 182.621 | PSI | 311.956 | PSIDOT | 199.328 | PHIOT | 52.209 |
| T | .01122 | PHI | 147.209 | PHIDOT | 193.033 | PSI | 312.070 | PSIDOT | 199.328 | PHIOT | 52.442 |
| T | .01123 | PHI | 147.322 | PHIDOT | 203.445 | PSI | 312.184 | PSIDOT | 199.328 | PHIOT | 52.568 |
| T | .01124 | PHI | 147.442 | PHIDOT | 213.857 | PSI | 312.412 | PSIDOT | 199.328 | PHIOT | 52.699 |
| T | .01125 | PHI | 147.568 | PHIDOT | 224.268 | PSI | 312.527 | PSIDOT | 199.328 | PHIOT | 52.836 |
| T | .01126 | PHI | 147.699 | PHIDOT | 234.680 | PSI | 312.651 | PSIDOT | 199.328 | PHIOT | 52.980 |
| T | .01127 | PHI | 147.836 | PHIDOT | 245.092 | PSI | 312.755 | PSIDOT | 199.328 | PHIOT | 53.129 |
| T | .01128 | PHI | 147.980 | PHIDOT | 255.504 | PSI | 312.869 | PSIDOT | 199.328 | PHIOT | 53.285 |
| T | .01129 | PHI | 148.129 | PHIDOT | 265.915 | PSI | 312.984 | PSIDOT | 199.328 | PHIOT | 53.446 |
| T | .01130 | PHI | 148.285 | PHIDOT | 276.327 | PSI | 313.094 | PSIDOT | 199.328 | PHIOT | 53.613 |
| T | .01131 | PHI | 148.446 | PHIDOT | 286.739 | PSI | 313.212 | PSIDOT | 199.328 | PHIOT | 53.786 |
| T | .01132 | PHI | 148.513 | PHIDOT | 297.151 | PSI | 313.326 | PSIDOT | 199.328 | PHIOT | 53.966 |
| T | .01133 | PHI | 148.786 | PHIDOT | 307.563 | PSI | 313.440 | PSIDOT | 199.328 | PHIOT | 54.151 |
| T | .01134 | PHI | 148.966 | PHIDOT | 317.974 | PSI | 313.555 | PSIDOT | 199.328 | PHIOT | 54.342 |
| T | .01135 | PHI | 149.151 | PHIDOT | 328.386 | PSI | 313.669 | PSIDOT | 199.328 | PHIOT | 54.539 |
| T | .01136 | PHI | 149.342 | PHIDOT | 338.798 | PSI | 313.783 | PSIDOT | 199.328 | PHIOT | 54.742 |
| T | .01137 | PHI | 149.539 | PHIDOT | 349.210 | PSI | 313.793 | PSIDOT | 199.328 | PHIOT | 54.951 |
| T | .01138 | PHI | 149.742 | PHIDOT | 359.621 | PSI | 313.897 | PSIDOT | 199.328 | PHIOT | 55.166 |
| T | .01139 | PHI | 149.951 | PHIDOT | 370.033 | PSI | 314.011 | PSIDOT | 199.328 | PHIOT | 55.387 |
| T | .01140 | PHI | 150.166 | PHIDOT | 380.445 | PSI | 314.126 | PSIDOT | 199.328 | PHIOT | 55.614 |
| T | .01141 | PHI | 150.387 | PHIDOT | 390.857 | PSI | 314.240 | PSIDOT | 199.328 | PHIOT | 55.847 |
| T | .01142 | PHI | 150.614 | PHIDOT | 401.268 | PSI | 314.354 | PSIDOT | 199.328 | PHIOT | 56.086 |
| T | .01143 | PHI | 150.847 | PHIDOT | 411.680 | PSI | 314.468 | PSIDOT | 199.328 | PHIOT | 56.331 |
| T | .01144 | PHI | 151.086 | PHIDOT | 422.092 | PSI | 314.582 | PSIDOT | 199.328 | PHIOT | 56.581 |
| T | .01145 | PHI | 151.331 | PHIDOT | 432.504 | PSI | 314.697 | PSIDOT | 199.328 | PHIOT | 56.838 |
| T | .01146 | PHI | 151.581 | PHIDOT | 442.915 | PSI | 314.811 | PSIDOT | 199.328 | PHIOT | 57.101 |
| T | .01147 | PHI | 151.838 | PHIDOT | 453.327 | PSI | 314.925 | PSIDOT | 199.328 | PHIOT | 57.370 |
| T | .01148 | PHI | 152.101 | PHIDOT | 463.739 | PSI | 315.039 | PSIDOT | 199.328 | PHIOT | 57.644 |
| T | .01149 | PHI | 152.370 | PHIDOT | 474.151 | PSI | 315.153 | PSIDOT | 199.328 | PHIOT | 57.925 |
| T | .01150 | PHI | 152.644 | PHIDOT | 484.563 | PSI | 315.268 | PSIDOT | 199.328 | PHIOT | 58.211 |
| T | .01151 | PHI | 152.925 | PHIDOT | 494.974 | PSI | 315.382 | PSIDOT | 199.328 | PHIOT | |
| T | .01152 | PHI | 153.211 | PHIDOT | 505.386 | PSI | 315.496 | PSIDOT | 199.328 | PHIOT | |

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I = .01153 PMI = 193.504 PMDOT = 515.798 PSI = 315.610 PSINOT = 199.326 PMITOT = 58.504
 I = .01154 PMI = 193.802 PMDOT = 526.210 PSI = 315.724 PSINOT = 199.328 PMITOT = 58.802
 VP = -1A.36A VS = 42.761

IMPACT
 VP = -3.579 VS = -16.857
 PSI = 315.724 PSINOT = 38.881 PMITOT = 58.802

FREE MOTION
 I = .01154 PMI = 193.802 PMDOT = 232.037 PSI = 315.724 PSINOT = 38.881 PMITOT = 58.802
 I = .01155 PMI = 193.672 PMDOT = 221.426 PSI = 315.747 PSINOT = 38.881 PMITOT = 58.672
 VP = -3.592 VS = -17.939

FREE MOTION
 I = .01155 PMI = 193.672 PMDOT = 221.626 PSI = 315.747 PSINOT = 38.881 PMITOT = 58.672
 I = .01156 PMI = 193.568 PMDOT = 211.214 PSI = 315.769 PSINOT = 38.881 PMITOT = 58.568
 I = .01157 PMI = 193.430 PMDOT = 200.802 PSI = 315.791 PSINOT = 38.881 PMITOT = 58.430
 I = .01158 PMI = 193.318 PMDOT = 190.393 PSI = 315.814 PSINOT = 38.881 PMITOT = 58.318
 I = .01159 PMI = 193.212 PMDOT = 179.979 PSI = 315.836 PSINOT = 38.881 PMITOT = 58.212
 I = .01160 PMI = 193.112 PMDOT = 169.567 PSI = 315.858 PSINOT = 38.881 PMITOT = 58.112
 I = .01161 PMI = 193.018 PMDOT = 159.155 PSI = 315.880 PSINOT = 38.881 PMITOT = 58.018
 I = .01162 PMI = 192.930 PMDOT = 148.743 PSI = 315.903 PSINOT = 38.881 PMITOT = 57.930
 I = .01163 PMI = 192.848 PMDOT = 138.332 PSI = 315.925 PSINOT = 38.881 PMITOT = 57.848
 I = .01164 PMI = 192.771 PMDOT = 127.920 PSI = 315.947 PSINOT = 38.881 PMITOT = 57.771
 I = .01165 PMI = 192.701 PMDOT = 117.508 PSI = 315.970 PSINOT = 38.881 PMITOT = 57.701
 I = .01166 PMI = 192.637 PMDOT = 107.096 PSI = 315.992 PSINOT = 38.881 PMITOT = 57.637
 I = .01167 PMI = 192.578 PMDOT = 96.685 PSI = 316.014 PSINOT = 38.881 PMITOT = 57.578
 I = .01168 PMI = 192.526 PMDOT = 86.273 PSI = 316.036 PSINOT = 38.881 PMITOT = 57.526
 I = .01169 PMI = 192.479 PMDOT = 75.861 PSI = 316.059 PSINOT = 38.881 PMITOT = 57.479
 I = .01170 PMI = 192.439 PMDOT = 65.449 PSI = 316.081 PSINOT = 38.881 PMITOT = 57.439
 I = .01171 PMI = 192.406 PMDOT = 55.037 PSI = 316.103 PSINOT = 38.881 PMITOT = 57.406

I = .01172 PMI = 192.376 PMDOT = 44.626 PSI = 316.125 PSINOT = 38.881 PMITOT = 57.376
 I = .01173 PMI = 192.353 PMDOT = 34.214 PSI = 316.148 PSINOT = 38.881 PMITOT = 57.353
 I = .01174 PMI = 192.337 PMDOT = 23.802 PSI = 316.170 PSINOT = 38.881 PMITOT = 57.337
 I = .01175 PMI = 192.326 PMDOT = 13.390 PSI = 316.192 PSINOT = 38.881 PMITOT = 57.326
 I = .01176 PMI = 192.321 PMDOT = 2.979 PSI = 316.215 PSINOT = 38.881 PMITOT = 57.321
 I = .01177 PMI = 192.323 PMDOT = 7.433 PSI = 316.237 PSINOT = 38.881 PMITOT = 57.323
 I = .01178 PMI = 192.330 PMDOT = 17.865 PSI = 316.259 PSINOT = 38.881 PMITOT = 57.330
 I = .01179 PMI = 192.343 PMDOT = 28.257 PSI = 316.281 PSINOT = 38.881 PMITOT = 57.343
 I = .01180 PMI = 192.362 PMDOT = 38.648 PSI = 316.304 PSINOT = 38.881 PMITOT = 57.362
 I = .01181 PMI = 192.387 PMDOT = 49.080 PSI = 316.326 PSINOT = 38.881 PMITOT = 57.387
 I = .01182 PMI = 192.418 PMDOT = 59.592 PSI = 316.348 PSINOT = 38.881 PMITOT = 57.418
 I = .01183 PMI = 192.455 PMDOT = 69.904 PSI = 316.371 PSINOT = 38.881 PMITOT = 57.455
 I = .01184 PMI = 192.498 PMDOT = 80.315 PSI = 316.393 PSINOT = 38.881 PMITOT = 57.498
 I = .01185 PMI = 192.547 PMDOT = 90.727 PSI = 316.415 PSINOT = 38.881 PMITOT = 57.547
 I = .01186 PMI = 192.602 PMDOT = 101.139 PSI = 316.437 PSINOT = 38.881 PMITOT = 57.602
 I = .01187 PMI = 192.663 PMDOT = 111.551 PSI = 316.460 PSINOT = 38.881 PMITOT = 57.663
 I = .01188 PMI = 192.730 PMDOT = 121.963 PSI = 316.482 PSINOT = 38.881 PMITOT = 57.730
 I = .01189 PMI = 192.803 PMDOT = 132.374 PSI = 316.504 PSINOT = 38.881 PMITOT = 57.803
 VP = -3.614 VS = 10.436

IMPACT
 VP = .007 VS = -3.505
 PSI = 316.504 PSINOT = -.073 PMITOT = 57.803

FREE MOTION
 I = .01189 PMI = 192.803 PMDOT = 44.668 PSI = 316.504 PSINOT = -.073 PMITOT = 57.803
 I = .01190 PMI = 192.781 PMDOT = 34.257 PSI = 316.504 PSINOT = -.073 PMITOT = 57.781
 I = .01191 PMI = 192.764 PMDOT = 23.845 PSI = 316.504 PSINOT = -.073 PMITOT = 57.764
 I = .01192 PMI = 192.754 PMDOT = 13.433 PSI = 316.504 PSINOT = -.073 PMITOT = 57.754
 I = .01193 PMI = 192.749 PMDOT = 2.921 PSI = 316.504 PSINOT = -.073 PMITOT = 57.749
 I = .01194 PMI = 192.750 PMDOT = 7.590 PSI = 316.504 PSINOT = -.073 PMITOT = 57.750

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|------------|---------------|-----------------|---------------|----------------|----------------|
| Y = .01195 | PXI = 192.758 | PMDOI = 18.002 | PSI = 316.504 | PSI00T = -.073 | PMI0T = 57.771 |
| Y = .01166 | PXI = 192.771 | PMDOI = 28.414 | PSI = 316.504 | PSI00T = -.073 | PMI0T = 57.790 |
| Y = .01197 | PXI = 192.790 | PMDOI = 38.826 | PSI = 316.504 | PSI00T = -.073 | PMI0T = 57.790 |
| VP = .007 | VS = 3.059 | | | | |
| IMPACT | | | | | |
| Y = .01207 | PXI = 192.790 | PMDOI = 16.176 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01217 | PXI = 192.975 | PMDOI = 31.763 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01227 | PXI = 193.201 | PMDOI = 46.954 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01237 | PXI = 193.512 | PMDOI = 61.578 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01247 | PXI = 193.905 | PMDOI = 75.488 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01257 | PXI = 194.375 | PMDOI = 88.414 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01267 | PXI = 194.916 | PMDOI = 100.354 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01277 | PXI = 195.523 | PMDOI = 111.135 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01287 | PXI = 196.187 | PMDOI = 120.687 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01297 | PXI = 196.903 | PMDOI = 128.935 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01307 | PXI = 197.662 | PMDOI = 135.834 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01317 | PXI = 198.457 | PMDOI = 141.373 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01327 | PXI = 199.280 | PMDOI = 145.568 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01337 | PXI = 200.122 | PMDOI = 148.399 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01347 | PXI = 200.978 | PMDOI = 149.939 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01357 | PXI = 201.838 | PMDOI = 150.265 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01367 | PXI = 202.697 | PMDOI = 149.622 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01377 | PXI = 203.545 | PMDOI = 147.588 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01387 | PXI = 204.386 | PMDOI = 144.683 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01397 | PXI = 205.205 | PMDOI = 140.961 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01407 | PXI = 206.000 | PMDOI = 136.484 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01417 | PXI = 206.768 | PMDOI = 131.355 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |

| | | | | | |
|------------|---------------|-----------------|---------------|----------------|----------------|
| Y = .01417 | PXI = 192.790 | PMDOI = 16.176 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01427 | PXI = 193.201 | PMDOI = 31.763 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01437 | PXI = 193.512 | PMDOI = 46.954 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01447 | PXI = 193.905 | PMDOI = 61.578 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01457 | PXI = 194.375 | PMDOI = 75.488 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01467 | PXI = 194.916 | PMDOI = 88.414 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01477 | PXI = 195.523 | PMDOI = 100.354 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01487 | PXI = 196.187 | PMDOI = 111.135 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01497 | PXI = 196.903 | PMDOI = 120.687 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01507 | PXI = 197.662 | PMDOI = 128.935 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01517 | PXI = 198.457 | PMDOI = 135.834 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01527 | PXI = 199.280 | PMDOI = 141.373 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01537 | PXI = 199.280 | PMDOI = 145.568 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01547 | PXI = 200.122 | PMDOI = 148.399 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01557 | PXI = 200.978 | PMDOI = 149.939 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01567 | PXI = 201.838 | PMDOI = 150.265 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01577 | PXI = 202.697 | PMDOI = 149.622 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01587 | PXI = 203.545 | PMDOI = 147.588 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01597 | PXI = 204.386 | PMDOI = 144.683 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01607 | PXI = 205.205 | PMDOI = 140.961 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01617 | PXI = 206.000 | PMDOI = 136.484 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |
| Y = .01627 | PXI = 206.768 | PMDOI = 131.355 | PSI = 316.504 | PSI00T = -.054 | PMI0T = 57.790 |

745

| | | | | | |
|--------------------|-------------|---------------|------------|----------------|--------------|
| TE .01445 | PME 130.974 | PMOPI 412.472 | PSI 44.931 | PSIOPI 245.226 | PHIOT 75.974 |
| TE .01446 | PME 131.213 | PMOPI 422.844 | PSI 44.740 | PSIOPI 245.226 | PHIOT 76.213 |
| TE .01447 | PME 131.450 | PMOPI 433.216 | PSI 44.550 | PSIOPI 245.226 | PHIOT 76.459 |
| TE .01448 | PME 131.710 | PMOPI 443.704 | PSI 44.509 | PSIOPI 245.226 | PHIOT 76.710 |
| TE .01449 | PME 131.967 | PMOPI 454.119 | PSI 44.369 | PSIOPI 245.226 | PHIOT 76.967 |
| TE .01450 | PME 132.230 | PMOPI 464.531 | PSI 44.228 | PSIOPI 245.226 | PHIOT 77.230 |
| TE .01451 | PME 132.499 | PMOPI 474.943 | PSI 44.088 | PSIOPI 245.226 | PHIOT 77.499 |
| TE .01452 | PME 132.774 | PMOPI 485.355 | PSI 43.947 | PSIOPI 245.226 | PHIOT 77.774 |
| TE .01453 | PME 133.056 | PMOPI 495.766 | PSI 43.807 | PSIOPI 245.226 | PHIOT 78.056 |
| TE .01454 | PME 133.343 | PMOPI 506.174 | PSI 43.666 | PSIOPI 245.226 | PHIOT 78.343 |
| TE .01455 | PME 133.636 | PMOPI 516.580 | PSI 43.526 | PSIOPI 245.226 | PHIOT 78.636 |
| TE .01456 | PME 133.935 | PMOPI 527.002 | PSI 43.385 | PSIOPI 245.226 | PHIOT 78.935 |
| TE .01457 | PME 134.239 | PMOPI 537.416 | PSI 43.245 | PSIOPI 245.226 | PHIOT 79.239 |
| TE .01458 | PME 134.550 | PMOPI 547.825 | PSI 43.104 | PSIOPI 245.226 | PHIOT 79.550 |
| TE .01459 | PME 134.867 | PMOPI 558.237 | PSI 42.964 | PSIOPI 245.226 | PHIOT 79.867 |
| TE .01460 | PME 135.190 | PMOPI 568.649 | PSI 42.823 | PSIOPI 245.226 | PHIOT 80.190 |
| TE .01461 | PME 135.519 | PMOPI 579.061 | PSI 42.683 | PSIOPI 245.226 | PHIOT 80.519 |
| VP -14.344 | VS 44.940 | | | | |
| IMPACT Cycle No. 3 | | | | | |
| VP -7.234 | VS -22.056 | DPME 284.190 | PSI 42.683 | DPSIF 123.677 | PHIOT 80.519 |
| FREE MOTION | | | | | |
| TE .01461 | PME 135.519 | PMOPI 284.190 | PSI 42.683 | PSIOPI 123.677 | PHIOT 80.519 |
| TE .01462 | PME 135.359 | PMOPI 273.779 | PSI 42.612 | PSIOPI 123.677 | PHIOT 80.359 |
| VP -7.249 | VS -21.063 | | | | |
| FREE MOTION | | | | | |
| TE .01461 | PME 135.359 | PMOPI 273.779 | PSI 42.612 | PSIOPI 123.677 | PHIOT 80.359 |
| TE .01462 | PME 135.205 | PMOPI 263.367 | PSI 42.541 | PSIOPI 123.677 | PHIOT 80.205 |
| TE .01463 | PME 135.057 | PMOPI 252.955 | PSI 42.470 | PSIOPI 123.677 | PHIOT 80.057 |
| VP -7.276 | VS -19.192 | | | | |
| FREE MOTION | | | | | |
| TE .01463 | PME 135.057 | PMOPI 252.955 | PSI 42.470 | PSIOPI 123.677 | PHIOT 80.057 |
| TE .01464 | PME 134.915 | PMOPI 242.543 | PSI 42.399 | PSIOPI 123.677 | PHIOT 79.915 |
| TE .01465 | PME 134.779 | PMOPI 232.131 | PSI 42.329 | PSIOPI 123.677 | PHIOT 79.779 |
| TE .01466 | PME 134.649 | PMOPI 221.720 | PSI 42.258 | PSIOPI 123.677 | PHIOT 79.649 |
| TE .01467 | PME 134.525 | PMOPI 211.308 | PSI 42.187 | PSIOPI 123.677 | PHIOT 79.525 |
| TE .01468 | PME 134.407 | PMOPI 200.894 | PSI 42.116 | PSIOPI 123.677 | PHIOT 79.407 |
| TE .01469 | PME 134.295 | PMOPI 190.484 | PSI 42.045 | PSIOPI 123.677 | PHIOT 79.295 |
| TE .01470 | PME 134.189 | PMOPI 180.073 | PSI 41.974 | PSIOPI 123.677 | PHIOT 79.189 |
| TE .01471 | PME 134.089 | PMOPI 169.661 | PSI 41.903 | PSIOPI 123.677 | PHIOT 79.089 |
| TE .01472 | PME 133.994 | PMOPI 159.249 | PSI 41.833 | PSIOPI 123.677 | PHIOT 78.994 |
| TE .01473 | PME 133.906 | PMOPI 148.837 | PSI 41.762 | PSIOPI 123.677 | PHIOT 78.906 |
| TE .01474 | PME 133.824 | PMOPI 138.426 | PSI 41.691 | PSIOPI 123.677 | PHIOT 78.824 |
| TE .01475 | PME 133.748 | PMOPI 128.014 | PSI 41.620 | PSIOPI 123.677 | PHIOT 78.748 |
| TE .01476 | PME 133.677 | PMOPI 117.602 | PSI 41.549 | PSIOPI 123.677 | PHIOT 78.677 |
| TE .01477 | PME 133.613 | PMOPI 107.190 | PSI 41.478 | PSIOPI 123.677 | PHIOT 78.613 |
| TE .01478 | PME 133.556 | PMOPI 96.779 | PSI 41.407 | PSIOPI 123.677 | PHIOT 78.556 |
| TE .01479 | PME 133.502 | PMOPI 86.367 | PSI 41.337 | PSIOPI 123.677 | PHIOT 78.502 |
| TE .01480 | PME 133.445 | PMOPI 75.955 | PSI 41.266 | PSIOPI 123.677 | PHIOT 78.445 |
| TE .01481 | PME 133.415 | PMOPI 65.543 | PSI 41.195 | PSIOPI 123.677 | PHIOT 78.415 |
| TE .01482 | PME 133.340 | PMOPI 55.131 | PSI 41.124 | PSIOPI 123.677 | PHIOT 78.340 |
| TE .01483 | PME 133.352 | PMOPI 44.720 | PSI 41.053 | PSIOPI 123.677 | PHIOT 78.352 |
| TE .01484 | PME 133.329 | PMOPI 34.308 | PSI 40.982 | PSIOPI 123.677 | PHIOT 78.329 |
| TE .01485 | PME 133.312 | PMOPI 23.894 | PSI 40.911 | PSIOPI 123.677 | PHIOT 78.312 |
| TE .01486 | PME 133.302 | PMOPI 13.482 | PSI 40.840 | PSIOPI 123.677 | PHIOT 78.302 |
| TE .01487 | PME 133.297 | PMOPI 3.073 | PSI 40.770 | PSIOPI 123.677 | PHIOT 78.297 |
| TE .01488 | PME 133.298 | PMOPI 7.339 | PSI 40.699 | PSIOPI 123.677 | PHIOT 78.298 |

T = .05256 PFI = 202.414 PH1001 = 152.465 G = -.0124
 T = .05266 PFI = 203.282 PH1001 = 150.537 G = -.0125
 T = .05276 PFI = 204.137 PH1001 = 147.725 G = -.0094
 T = .05286 PFI = 204.973 PH1001 = 144.015 G = -.0062
 T = .05296 PFI = 205.786 PH1001 = 139.514 G = -.0030
 T = .05306 PFI = 206.571 PH1001 = 134.333 G = -.0007

FREE MOTION
 T = .05306 PFI = 126.571 PM001 = 136.339 PSI = 49.088
 T = .05307 PFI = 126.651 PM001 = 144.751 PSI = 48.947
 T = .05308 PFI = 126.737 PM001 = 155.163 PSI = 48.806
 T = .05309 PFI = 126.829 PM001 = 165.574 PSI = 48.665
 T = .05310 PFI = 126.927 PM001 = 175.986 PSI = 48.524
 T = .05311 PFI = 127.030 PM001 = 186.398 PSI = 48.382

T = .05312 PFI = 127.140 PM001 = 196.810 PSI = 48.241
 T = .05313 PFI = 127.256 PM001 = 207.221 PSI = 48.100
 T = .05314 PFI = 127.378 PM001 = 217.633 PSI = 47.959
 T = .05315 PFI = 127.505 PM001 = 228.045 PSI = 47.818
 T = .05316 PFI = 127.639 PM001 = 238.457 PSI = 47.676
 T = .05317 PFI = 127.779 PM001 = 248.868 PSI = 47.535
 T = .05318 PFI = 127.924 PM001 = 259.280 PSI = 47.394
 T = .05319 PFI = 128.074 PM001 = 269.692 PSI = 47.253
 T = .05320 PFI = 128.231 PM001 = 280.104 PSI = 47.112

T = .05321 PFI = 128.397 PM001 = 290.515 PSI = 46.970
 T = .05322 PFI = 128.566 PM001 = 300.927 PSI = 46.829
 T = .05323 PFI = 128.741 PM001 = 311.339 PSI = 46.688
 T = .05324 PFI = 128.923 PM001 = 321.751 PSI = 46.547
 T = .05325 PFI = 129.110 PM001 = 332.163 PSI = 46.406
 T = .05326 PFI = 129.303 PM001 = 342.574 PSI = 46.264
 T = .05327 PFI = 129.503 PM001 = 352.986 PSI = 46.123
 T = .05328 PFI = 129.708 PM001 = 363.398 PSI = 45.982
 T = .05329 PFI = 129.919 PM001 = 373.810 PSI = 45.841
 T = .05330 PFI = 130.136 PM001 = 384.221 PSI = 45.699
 T = .05331 PFI = 130.359 PM001 = 394.633 PSI = 45.558
 T = .05332 PFI = 130.588 PM001 = 405.045 PSI = 45.417
 T = .05333 PFI = 130.824 PM001 = 415.457 PSI = 45.276
 T = .05334 PFI = 131.065 PM001 = 425.868 PSI = 45.135
 T = .05335 PFI = 131.312 PM001 = 436.280 PSI = 44.993

T = .05336 PFI = 131.565 PM001 = 446.692 PSI = 44.852
 T = .05337 PFI = 131.823 PM001 = 457.104 PSI = 44.711
 T = .05338 PFI = 132.088 PM001 = 467.515 PSI = 44.570
 T = .05339 PFI = 132.359 PM001 = 477.927 PSI = 44.429
 T = .05340 PFI = 132.636 PM001 = 488.339 PSI = 44.287
 T = .05341 PFI = 132.919 PM001 = 498.751 PSI = 44.146
 T = .05342 PFI = 133.208 PM001 = 509.163 PSI = 44.005
 T = .05343 PFI = 133.502 PM001 = 519.574 PSI = 43.864
 T = .05344 PFI = 133.803 PM001 = 529.986 PSI = 43.723
 T = .05345 PFI = 134.110 PM001 = 540.398 PSI = 43.581
 T = .05346 PFI = 134.422 PM001 = 550.810 PSI = 43.440
 T = .05347 PFI = 134.741 PM001 = 561.221 PSI = 43.299
 T = .05348 PFI = 135.065 PM001 = 571.633 PSI = 43.158
 T = .05349 PFI = 135.396 PM001 = 582.045 PSI = 43.017
 T = .05350 PFI = 135.732 PM001 = 592.457 PSI = 42.875

VP = -14.689 VS = 46.658
 IMPACT
 Cycle No. 8
 PFI = 135.732 DMPIF = 266.525 PSI = 42.875
 VS = -72.468
 PFI = 135.732 PM001 = 266.525 PSI = 42.875
 PFI = 135.571 PM001 = 276.113 PSI = 42.804
 VS = -7.246 VS = -21.483

End of Cycle No. 7

| | | | | | | | | | | |
|-------------|--------|---------------|-----------------|--------------|------------------|-----------------|--|--|--|--|
| FREE MOTION | | | | | | | | | | |
| TE | .05351 | PHI = 135.571 | PHOOT = 276.113 | PSI = 42.806 | PSI00T = 124.023 | PHI0T = 280.571 | | | | |
| TE | .05352 | PHI = 135.416 | PHOOT = 265.701 | PSI = 42.733 | PSI00T = 124.023 | PHI0T = 280.416 | | | | |
| VP | -7.280 | VS = -20.517 | | | | | | | | |
| FREE MOTION | | | | | | | | | | |
| TE | .05352 | PHI = 135.416 | PHOOT = 265.701 | PSI = 42.733 | PSI00T = 124.023 | PHI0T = 280.416 | | | | |
| TE | .05353 | PHI = 135.267 | PHOOT = 255.289 | PSI = 42.662 | PSI00T = 124.023 | PHI0T = 280.267 | | | | |
| VP | -7.293 | VS = -19.570 | | | | | | | | |
| FREE MOTION | | | | | | | | | | |
| TE | .05353 | PHI = 135.267 | PHOOT = 255.289 | PSI = 42.662 | PSI00T = 124.023 | PHI0T = 280.267 | | | | |
| TE | .05354 | PHI = 135.123 | PHOOT = 244.878 | PSI = 42.591 | PSI00T = 124.023 | PHI0T = 280.123 | | | | |
| TE | .05355 | PHI = 134.946 | PHOOT = 234.466 | PSI = 42.520 | PSI00T = 124.023 | PHI0T = 279.946 | | | | |
| TE | .05356 | PHI = 134.855 | PHOOT = 224.054 | PSI = 42.449 | PSI00T = 124.023 | PHI0T = 279.855 | | | | |
| TE | .05357 | PHI = 134.729 | PHOOT = 213.642 | PSI = 42.378 | PSI00T = 124.023 | PHI0T = 279.729 | | | | |
| TE | .05358 | PHI = 134.610 | PHOOT = 203.231 | PSI = 42.307 | PSI00T = 124.023 | PHI0T = 279.610 | | | | |
| TE | .05359 | PHI = 134.496 | PHOOT = 192.819 | PSI = 42.236 | PSI00T = 124.023 | PHI0T = 279.496 | | | | |
| TE | .05360 | PHI = 134.389 | PHOOT = 182.407 | PSI = 42.165 | PSI00T = 124.023 | PHI0T = 279.389 | | | | |
| TE | .05361 | PHI = 134.287 | PHOOT = 171.995 | PSI = 42.094 | PSI00T = 124.023 | PHI0T = 279.287 | | | | |
| TE | .05362 | PHI = 134.192 | PHOOT = 161.583 | PSI = 42.023 | PSI00T = 124.023 | PHI0T = 279.192 | | | | |
| TE | .05363 | PHI = 134.102 | PHOOT = 151.172 | PSI = 41.952 | PSI00T = 124.023 | PHI0T = 279.102 | | | | |
| TE | .05364 | PHI = 134.019 | PHOOT = 140.760 | PSI = 41.880 | PSI00T = 124.023 | PHI0T = 279.019 | | | | |
| TE | .05365 | PHI = 133.941 | PHOOT = 130.348 | PSI = 41.809 | PSI00T = 124.023 | PHI0T = 278.941 | | | | |
| TE | .05366 | PHI = 133.869 | PHOOT = 119.936 | PSI = 41.738 | PSI00T = 124.023 | PHI0T = 278.869 | | | | |
| TE | .05367 | PHI = 133.803 | PHOOT = 109.525 | PSI = 41.667 | PSI00T = 124.023 | PHI0T = 278.803 | | | | |
| TE | .05368 | PHI = 133.744 | PHOOT = 99.113 | PSI = 41.596 | PSI00T = 124.023 | PHI0T = 278.744 | | | | |
| TE | .05369 | PHI = 133.690 | PHOOT = 88.701 | PSI = 41.525 | PSI00T = 124.023 | PHI0T = 278.690 | | | | |
| TE | .05370 | PHI = 133.642 | PHOOT = 78.289 | PSI = 41.454 | PSI00T = 124.023 | PHI0T = 278.642 | | | | |
| TE | .05371 | PHI = 133.600 | PHOOT = 67.878 | PSI = 41.383 | PSI00T = 124.023 | PHI0T = 278.600 | | | | |
| TE | .05372 | PHI = 133.564 | PHOOT = 57.466 | PSI = 41.312 | PSI00T = 124.023 | PHI0T = 278.564 | | | | |
| TE | .05373 | PHI = 133.534 | PHOOT = 47.054 | PSI = 41.241 | PSI00T = 124.023 | PHI0T = 278.534 | | | | |
| TE | .05374 | PHI = 133.510 | PHOOT = 36.642 | PSI = 41.170 | PSI00T = 124.023 | PHI0T = 278.510 | | | | |
| TE | .05375 | PHI = 133.492 | PHOOT = 26.231 | PSI = 41.099 | PSI00T = 124.023 | PHI0T = 278.492 | | | | |
| TE | .05376 | PHI = 133.480 | PHOOT = 15.819 | PSI = 41.028 | PSI00T = 124.023 | PHI0T = 278.480 | | | | |
| TE | .05377 | PHI = 133.474 | PHOOT = 5.407 | PSI = 40.957 | PSI00T = 124.023 | PHI0T = 278.474 | | | | |
| TE | .05378 | PHI = 133.474 | PHOOT = 5.005 | PSI = 40.886 | PSI00T = 124.023 | PHI0T = 278.474 | | | | |
| TE | .05379 | PHI = 133.480 | PHOOT = 15.617 | PSI = 40.815 | PSI00T = 124.023 | PHI0T = 278.480 | | | | |
| TE | .05380 | PHI = 133.492 | PHOOT = 25.228 | PSI = 40.744 | PSI00T = 124.023 | PHI0T = 278.492 | | | | |
| TE | .05381 | PHI = 133.509 | PHOOT = 34.840 | PSI = 40.672 | PSI00T = 124.023 | PHI0T = 278.509 | | | | |
| TE | .05382 | PHI = 133.533 | PHOOT = 44.452 | PSI = 40.601 | PSI00T = 124.023 | PHI0T = 278.533 | | | | |
| TE | .05383 | PHI = 133.563 | PHOOT = 54.064 | PSI = 40.530 | PSI00T = 124.023 | PHI0T = 278.563 | | | | |
| VP | -7.222 | VS = 4.015 | | | | | | | | |
| IMPACT | | | | | | | | | | |
| VP | -5.629 | VS = -9.437 | DPHI = 119.929 | PSI = 40.530 | DPST = -96.656 | PHI0T = 278.563 | | | | |
| FREE MOTION | | | | | | | | | | |
| TE | .05383 | PHI = 133.563 | PHOOT = 119.929 | PSI = 40.530 | PSI00T = -96.656 | PHI0T = 278.563 | | | | |
| TE | .05384 | PHI = 133.497 | PHOOT = 109.517 | PSI = 40.459 | PSI00T = -96.656 | PHI0T = 278.497 | | | | |
| VP | -5.630 | VS = -7.679 | | | | | | | | |
| FREE MOTION | | | | | | | | | | |
| TE | .05384 | PHI = 133.497 | PHOOT = 109.517 | PSI = 40.475 | PSI00T = -96.656 | PHI0T = 278.497 | | | | |
| TE | .05385 | PHI = 133.437 | PHOOT = 99.105 | PSI = 40.420 | PSI00T = -96.656 | PHI0T = 278.437 | | | | |
| VP | -5.630 | VS = -6.927 | | | | | | | | |
| FREE MOTION | | | | | | | | | | |
| TE | .05385 | PHI = 133.437 | PHOOT = 99.105 | PSI = 40.420 | PSI00T = -96.656 | PHI0T = 278.437 | | | | |
| TE | .05386 | PHI = 133.384 | PHOOT = 88.694 | PSI = 40.364 | PSI00T = -96.656 | PHI0T = 278.384 | | | | |
| VP | -5.630 | VS = -6.182 | | | | | | | | |

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FREE MOTION
X= .05386 PHI= 133.336 PHDJI= -88.694 PSI= 40.366 PSIOI= -96.656 PHITOT = 278.336
Y= .05387 PHI= 133.336 PHDJI= -78.282 PSI= 40.309 PSIOI= -96.656 PHITOT = 278.336
VP= -5.629 VS= -5.643

IMPACT
X= .05682 PHI= 133.336 PHDJI= -81.242 PSI= 40.309 PSIOI= -96.193 PHITOT = 278.336
Y= .05687 PHI= 133.336 PHDJI= -71.242 PSI= 40.309 PSIOI= -96.193 PHITOT = 278.336

COUPLEFO MOTION table with columns: X, Y, VP, VS, PHI, PHDJI, PSI, PSIOI, PHITOT, PHITOT, PSIOI, PSI, PHDJI, PSIOI, PHITOT. Contains multiple rows of numerical data.

| | | | | | | | | |
|--------------------------|--------|---------------|------------------|---------------|------------------|-----------------|------------------|-----------------|
| T | .05627 | PHI = 178.206 | PHI001 = 81.781 | G = -.0333 | GD01 = 18.454 | PSID = 46.413 | PSI001 = 119.092 | PHI01 = 253.208 |
| T | .05637 | PHI = 178.692 | PHI001 = 86.098 | G = -.0315 | GD01 = 19.099 | PSID = 47.510 | PSI001 = 126.473 | PHI01 = 283.682 |
| T | .05647 | PHI = 179.170 | PHI001 = 86.317 | G = -.0295 | GD01 = 19.726 | PSID = 48.239 | PSI001 = 129.835 | PHI01 = 266.170 |
| T | .05657 | PHI = 179.671 | PHI001 = 86.436 | G = -.0275 | GD01 = 20.315 | PSID = 48.998 | PSI001 = 135.178 | PHI01 = 284.671 |
| T | .05667 | PHI = 180.183 | PHI001 = 90.471 | G = -.0255 | GD01 = 20.927 | PSID = 49.788 | PSI001 = 140.566 | PHI01 = 285.183 |
| T | .05677 | PHI = 180.707 | PHI001 = 92.433 | G = -.0233 | GD01 = 21.584 | PSID = 50.604 | PSI001 = 145.819 | PHI01 = 285.707 |
| T | .05687 | PHI = 181.242 | PHI001 = 94.328 | G = -.0211 | GD01 = 22.046 | PSID = 51.450 | PSI001 = 151.121 | PHI01 = 286.242 |
| T | .05697 | PHI = 181.788 | PHI001 = 96.158 | G = -.0189 | GD01 = 22.610 | PSID = 52.340 | PSI001 = 156.414 | PHI01 = 286.788 |
| T | .05707 | PHI = 182.344 | PHI001 = 97.934 | G = -.0167 | GD01 = 23.141 | PSID = 53.251 | PSI001 = 161.700 | PHI01 = 287.344 |
| T | .05717 | PHI = 182.910 | PHI001 = 99.677 | G = -.0143 | GD01 = 23.658 | PSID = 54.193 | PSI001 = 166.980 | PHI01 = 287.910 |
| T | .05727 | PHI = 183.486 | PHI001 = 101.384 | G = -.0119 | GD01 = 24.161 | PSID = 55.165 | PSI001 = 172.258 | PHI01 = 288.486 |
| T | .05737 | PHI = 184.072 | PHI001 = 103.025 | G = -.0095 | GD01 = 24.651 | PSID = 56.167 | PSI001 = 177.536 | PHI01 = 289.072 |
| T | .05747 | PHI = 184.667 | PHI001 = 104.650 | G = -.0070 | GD01 = 25.127 | PSID = 57.199 | PSI001 = 182.816 | PHI01 = 289.667 |
| T | .05757 | PHI = 185.271 | PHI001 = 106.254 | G = -.0045 | GD01 = 25.590 | PSID = 58.262 | PSI001 = 188.098 | PHI01 = 290.271 |
| T | .05767 | PHI = 185.884 | PHI001 = 107.834 | G = -.0019 | GD01 = 26.040 | PSID = 59.355 | PSI001 = 193.387 | PHI01 = 290.884 |
| T | .05777 | PHI = 186.505 | PHI001 = 109.402 | G = -.0008 | GD01 = 26.477 | PSID = 60.478 | PSI001 = 198.683 | PHI01 = 291.506 |
| FREE BOTTOM | | | | | | | | |
| T | .05777 | PHI = 186.506 | PH001 = 109.402 | PCI = 311.141 | PSI001 = 198.683 | PHI01 = 291.506 | | |
| T | .05778 | PHI = 186.572 | PH001 = 119.814 | PCI = 311.255 | PSI001 = 198.683 | PHI01 = 291.572 | | |
| T | .05779 | PHI = 186.644 | PH001 = 130.226 | PCI = 311.368 | PSI001 = 198.683 | PHI01 = 291.644 | | |
| T | .05780 | PHI = 186.721 | PH001 = 140.638 | PCI = 311.482 | PSI001 = 198.683 | PHI01 = 291.721 | | |
| T | .05781 | PHI = 186.805 | PH001 = 151.049 | PCI = 311.598 | PSI001 = 198.683 | PHI01 = 291.805 | | |
| T | .05782 | PHI = 186.894 | PH001 = 161.461 | PCI = 311.710 | PSI001 = 198.683 | PHI01 = 291.894 | | |
| T | .05783 | PHI = 186.990 | PH001 = 171.873 | PCI = 311.824 | PSI001 = 198.683 | PHI01 = 291.990 | | |
| T | .05784 | PHI = 187.091 | PH001 = 182.285 | PCI = 311.938 | PSI001 = 198.683 | PHI01 = 292.091 | | |
| T | .05785 | PHI = 187.199 | PH001 = 192.696 | PCI = 312.051 | PSI001 = 198.683 | PHI01 = 292.199 | | |
| T | .05786 | PHI = 187.312 | PH001 = 203.108 | PCI = 312.165 | PSI001 = 198.683 | PHI01 = 292.312 | | |
| T | .05787 | PHI = 187.432 | PH001 = 213.520 | PCI = 312.279 | PSI001 = 198.683 | PHI01 = 292.432 | | |
| T | .05788 | PHI = 187.557 | PH001 = 223.932 | PCI = 312.393 | PSI001 = 198.683 | PHI01 = 292.557 | | |
| T | .05789 | PHI = 187.688 | PH001 = 234.345 | PCI = 312.507 | PSI001 = 198.683 | PHI01 = 292.688 | | |
| T | .05790 | PHI = 187.825 | PH001 = 244.755 | PCI = 312.621 | PSI001 = 198.683 | PHI01 = 292.825 | | |
| T | .05791 | PHI = 187.966 | PH001 = 255.167 | PCI = 312.736 | PSI001 = 198.683 | PHI01 = 292.969 | | |
| T | .05792 | PHI = 188.110 | PH001 = 265.579 | PCI = 312.848 | PSI001 = 198.683 | PHI01 = 293.118 | | |
| T | .05793 | PHI = 188.273 | PH001 = 275.990 | PCI = 312.962 | PSI001 = 198.683 | PHI01 = 293.273 | | |
| T | .05794 | PHI = 188.436 | PH001 = 286.402 | PCI = 313.076 | PSI001 = 198.683 | PHI01 = 293.434 | | |
| T | .05795 | PHI = 188.601 | PH001 = 296.814 | PCI = 313.190 | PSI001 = 198.683 | PHI01 = 293.601 | | |
| T | .05796 | PHI = 188.774 | PH001 = 307.226 | PCI = 313.304 | PSI001 = 198.683 | PHI01 = 293.774 | | |
| T | .05797 | PHI = 188.953 | PH001 = 317.638 | PCI = 313.417 | PSI001 = 198.683 | PHI01 = 293.953 | | |
| T | .05798 | PHI = 189.138 | PH001 = 328.049 | PCI = 313.531 | PSI001 = 198.683 | PHI01 = 294.138 | | |
| T | .05799 | PHI = 189.329 | PH001 = 338.461 | PCI = 313.645 | PSI001 = 198.683 | PHI01 = 294.329 | | |
| T | .05800 | PHI = 189.526 | PH001 = 348.873 | PCI = 313.759 | PSI001 = 198.683 | PHI01 = 294.526 | | |
| T | .05801 | PHI = 189.729 | PH001 = 359.285 | PCI = 313.873 | PSI001 = 198.683 | PHI01 = 294.729 | | |
| T | .05802 | PHI = 189.938 | PH001 = 369.696 | PCI = 313.987 | PSI001 = 198.683 | PHI01 = 294.938 | | |
| T | .05803 | PHI = 190.153 | PH001 = 380.108 | PCI = 314.101 | PSI001 = 198.683 | PHI01 = 295.153 | | |
| T | .05804 | PHI = 190.373 | PH001 = 390.520 | PCI = 314.216 | PSI001 = 198.683 | PHI01 = 295.373 | | |
| T | .05805 | PHI = 190.600 | PH001 = 400.932 | PCI = 314.328 | PSI001 = 198.683 | PHI01 = 295.600 | | |
| T | .05806 | PHI = 190.833 | PH001 = 411.343 | PCI = 314.442 | PSI001 = 198.683 | PHI01 = 295.833 | | |
| T | .05807 | PHI = 191.071 | PH001 = 421.755 | PCI = 314.556 | PSI001 = 198.683 | PHI01 = 296.071 | | |
| T | .05808 | PHI = 191.316 | PH001 = 432.167 | PCI = 314.670 | PSI001 = 198.683 | PHI01 = 296.316 | | |
| T | .05809 | PHI = 191.567 | PH001 = 442.579 | PCI = 314.784 | PSI001 = 198.683 | PHI01 = 296.567 | | |
| T | .05810 | PHI = 191.823 | PH001 = 452.990 | PCI = 314.897 | PSI001 = 198.683 | PHI01 = 296.823 | | |
| T | .05811 | PHI = 192.086 | PH001 = 463.402 | PCI = 315.011 | PSI001 = 198.683 | PHI01 = 297.086 | | |
| T | .05812 | PHI = 192.356 | PH001 = 473.814 | PCI = 315.125 | PSI001 = 198.683 | PHI01 = 297.356 | | |
| T | .05813 | PHI = 192.629 | PH001 = 484.226 | PCI = 315.239 | PSI001 = 198.683 | PHI01 = 297.629 | | |
| T | .05814 | PHI = 192.909 | PH001 = 494.638 | PCI = 315.353 | PSI001 = 198.683 | PHI01 = 297.909 | | |
| T | .05815 | PHI = 193.196 | PH001 = 505.049 | PCI = 315.467 | PSI001 = 198.683 | PHI01 = 298.196 | | |
| T | .05816 | PHI = 193.488 | PH001 = 515.461 | PCI = 315.580 | PSI001 = 198.683 | PHI01 = 298.488 | | |
| T | .05817 | PHI = 193.786 | PH001 = 525.873 | PCI = 315.694 | PSI001 = 198.683 | PHI01 = 298.786 | | |
| VD = -18.247 VS = 42.715 | | | | | | | | |
| IMPACT | | | | | | | | |
| T | | PHI = 193.786 | DPHIF = 231.270 | PCI = 315.694 | NP5IF = 38.603 | PHI01 = 298.786 | | |

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VP# -1.515 VS# -18.745

FREE MOTION

| | | | | | |
|-----------|--------------|-----------------|--------------|---------|-----------------|
| T# .05817 | PHI# 191.746 | PHDIT# -231.270 | PSI# 315.694 | PSI00T# | PHITOT# 298.786 |
| T# .05818 | PHI# 191.657 | PHDIT# -220.459 | PSI# 315.716 | PSI00T# | PHITOT# 298.657 |
| T# .05819 | PHI# 193.513 | PHDIT# -210.447 | PSI# 315.738 | PSI00T# | PHITOT# 298.533 |
| T# .05820 | PHI# 191.414 | PHDIT# -200.835 | PSI# 315.760 | PSI00T# | PHITOT# 298.416 |
| T# .05821 | PHI# 193.374 | PHDIT# -189.623 | PSI# 315.782 | PSI00T# | PHITOT# 298.304 |
| T# .05822 | PHI# 193.198 | PHDIT# -179.211 | PSI# 315.804 | PSI00T# | PHITOT# 298.198 |
| T# .05823 | PHI# 193.099 | PHDIT# -168.800 | PSI# 315.826 | PSI00T# | PHITOT# 298.095 |
| T# .05824 | PHI# 193.005 | PHDIT# -158.388 | PSI# 315.848 | PSI00T# | PHITOT# 297.917 |
| T# .05825 | PHI# 192.917 | PHDIT# -147.976 | PSI# 315.870 | PSI00T# | PHITOT# 297.835 |
| T# .05826 | PHI# 192.835 | PHDIT# -137.564 | PSI# 315.892 | PSI00T# | PHITOT# 297.759 |
| T# .05827 | PHI# 192.759 | PHDIT# -127.153 | PSI# 315.914 | PSI00T# | PHITOT# 297.690 |
| T# .05828 | PHI# 192.690 | PHDIT# -116.741 | PSI# 315.936 | PSI00T# | PHITOT# 297.626 |
| T# .05829 | PHI# 192.624 | PHDIT# -106.329 | PSI# 315.958 | PSI00T# | PHITOT# 297.568 |
| T# .05830 | PHI# 192.568 | PHDIT# -95.917 | PSI# 315.980 | PSI00T# | PHITOT# 297.516 |
| T# .05831 | PHI# 192.516 | PHDIT# -85.504 | PSI# 316.002 | PSI00T# | PHITOT# 297.470 |
| T# .05832 | PHI# 192.470 | PHDIT# -75.092 | PSI# 316.024 | PSI00T# | PHITOT# 297.430 |
| T# .05833 | PHI# 192.430 | PHDIT# -64.682 | PSI# 316.046 | PSI00T# | PHITOT# 297.396 |
| T# .05834 | PHI# 192.396 | PHDIT# -54.270 | PSI# 316.068 | PSI00T# | PHITOT# 297.367 |
| T# .05835 | PHI# 192.367 | PHDIT# -43.859 | PSI# 316.090 | PSI00T# | PHITOT# 297.345 |
| T# .05836 | PHI# 192.345 | PHDIT# -33.447 | PSI# 316.112 | PSI00T# | PHITOT# 297.329 |
| T# .05837 | PHI# 192.329 | PHDIT# -23.035 | PSI# 316.134 | PSI00T# | PHITOT# 297.319 |
| T# .05838 | PHI# 192.319 | PHDIT# -12.623 | PSI# 316.156 | PSI00T# | PHITOT# 297.315 |
| T# .05839 | PHI# 192.315 | PHDIT# -2.211 | PSI# 316.178 | PSI00T# | PHITOT# 297.316 |
| T# .05840 | PHI# 192.316 | PHDIT# 8.200 | PSI# 316.200 | PSI00T# | PHITOT# 297.324 |
| T# .05841 | PHI# 192.324 | PHDIT# 18.612 | PSI# 316.222 | PSI00T# | PHITOT# 297.338 |
| T# .05842 | PHI# 192.338 | PHDIT# 29.024 | PSI# 316.244 | PSI00T# | PHITOT# 297.357 |
| T# .05843 | PHI# 192.357 | PHDIT# 39.436 | PSI# 316.266 | PSI00T# | PHITOT# 297.383 |
| T# .05844 | PHI# 192.383 | PHDIT# 49.847 | PSI# 316.288 | PSI00T# | PHITOT# 297.414 |
| T# .05845 | PHI# 192.414 | PHDIT# 60.259 | PSI# 316.310 | PSI00T# | PHITOT# 297.452 |
| T# .05846 | PHI# 192.452 | PHDIT# 70.671 | PSI# 316.332 | PSI00T# | PHITOT# 297.495 |
| T# .05847 | PHI# 192.495 | PHDIT# 81.083 | PSI# 316.354 | PSI00T# | PHITOT# 297.545 |
| T# .05848 | PHI# 192.545 | PHDIT# 91.494 | PSI# 316.376 | PSI00T# | PHITOT# 297.600 |
| T# .05849 | PHI# 192.600 | PHDIT# 101.904 | PSI# 316.398 | PSI00T# | PHITOT# 297.662 |
| T# .05850 | PHI# 192.662 | PHDIT# 112.318 | PSI# 316.420 | PSI00T# | PHITOT# 297.729 |
| T# .05851 | PHI# 192.729 | PHDIT# 122.730 | PSI# 316.442 | PSI00T# | PHITOT# 297.802 |
| T# .05852 | PHI# 192.802 | PHDIT# 133.141 | PSI# 316.464 | PSI00T# | PHITOT# 297.882 |
| T# .05853 | PHI# 192.882 | PHDIT# 143.553 | PSI# 316.486 | PSI00T# | PHITOT# 297.970 |

VP# -1.567 VS# 11.347

IMPACT

| | | | | | |
|---------------------|--------------|----------------|--------------|----------------|-----------------|
| VP# .25A VS# -3.470 | PHI# 192.882 | OPMIF# -43.916 | PSI# 316.486 | OPSI# -2.773 | PHITOT# 297.882 |
| VP# .25A VS# -2.665 | PHI# 192.882 | PHDIT# -63.916 | PSI# 316.486 | PSI00T# -2.773 | PHITOT# 297.882 |
| VP# .25A VS# -1.822 | PHI# 192.882 | PHDIT# -33.504 | PSI# 316.485 | PSI00T# -2.773 | PHITOT# 297.859 |
| VP# .25A VS# -1.000 | PHI# 192.882 | PHDIT# -23.092 | PSI# 316.485 | PSI00T# -2.773 | PHITOT# 297.859 |
| VP# .25A VS# -1.000 | PHI# 192.882 | PHDIT# -12.681 | PSI# 316.482 | PSI00T# -2.773 | PHITOT# 297.833 |
| VP# .25A VS# -1.000 | PHI# 192.882 | PHDIT# -2.269 | PSI# 316.480 | PSI00T# -2.773 | PHITOT# 297.829 |

| | | | | | | |
|-----|---------|--------------|----------------|-------------|-----------------|------------------|
| Y= | .06101 | PHI= 130.204 | PHDOT= 369.500 | PSI= 45.210 | PSIDOT=-246.111 | PHITOT = 315.204 |
| Y= | .06102 | PHI= 130.410 | PHDOT= 380.000 | PSI= 45.049 | PSIDOT=-246.111 | PHITOT = 315.410 |
| Y= | .06103 | PHI= 170.640 | PHDOT= 390.412 | PSI= 44.924 | PSIDOT=-246.111 | PHITOT = 315.640 |
| Y= | .06104 | PHI= 170.667 | PHDOT= 400.074 | PSI= 44.787 | PSIDOT=-246.111 | PHITOT = 315.867 |
| Y= | .06105 | PHI= 171.099 | PHDOT= 411.235 | PSI= 44.646 | PSIDOT=-246.111 | PHITOT = 316.099 |
| Y= | .06106 | PHI= 171.338 | PHDOT= 421.647 | PSI= 44.505 | PSIDOT=-246.111 | PHITOT = 316.338 |
| Y= | .06107 | PHI= 171.582 | PHDOT= 432.059 | PSI= 44.364 | PSIDOT=-246.111 | PHITOT = 316.582 |
| Y= | .06108 | PHI= 171.833 | PHDOT= 442.471 | PSI= 44.223 | PSIDOT=-246.111 | PHITOT = 316.833 |
| Y= | .06109 | PHI= 172.089 | PHDOT= 452.882 | PSI= 44.082 | PSIDOT=-246.111 | PHITOT = 317.089 |
| Y= | .06110 | PHI= 172.352 | PHDOT= 463.294 | PSI= 43.941 | PSIDOT=-246.111 | PHITOT = 317.352 |
| Y= | .06111 | PHI= 172.620 | PHDOT= 473.706 | PSI= 43.800 | PSIDOT=-246.111 | PHITOT = 317.620 |
| Y= | .06112 | PHI= 172.895 | PHDOT= 484.118 | PSI= 43.659 | PSIDOT=-246.111 | PHITOT = 317.895 |
| Y= | .06113 | PHI= 173.175 | PHDOT= 494.529 | PSI= 43.518 | PSIDOT=-246.111 | PHITOT = 318.175 |
| Y= | .06114 | PHI= 173.461 | PHDOT= 504.941 | PSI= 43.377 | PSIDOT=-246.111 | PHITOT = 318.461 |
| Y= | .06115 | PHI= 173.754 | PHDOT= 515.353 | PSI= 43.236 | PSIDOT=-246.111 | PHITOT = 318.754 |
| Y= | .06116 | PHI= 174.052 | PHDOT= 525.765 | PSI= 43.095 | PSIDOT=-246.111 | PHITOT = 319.052 |
| Y= | .06117 | PHI= 174.356 | PHDOT= 536.177 | PSI= 42.954 | PSIDOT=-246.111 | PHITOT = 319.356 |
| Y= | .06118 | PHI= 174.666 | PHDOT= 546.588 | PSI= 42.813 | PSIDOT=-246.111 | PHITOT = 319.666 |
| Y= | .06119 | PHI= 174.983 | PHDOT= 557.000 | PSI= 42.672 | PSIDOT=-246.111 | PHITOT = 319.983 |
| Y= | .06120 | PHI= 175.305 | PHDOT= 567.412 | PSI= 42.531 | PSIDOT=-246.111 | PHITOT = 320.305 |
| VP= | .16.417 | VS= 43.578 | | | | |

IMPACT

| | | | | | | |
|-------------|--------|--------------|---------------|-------------|-----------------|------------------|
| VP= | -7.311 | VS= -21.809 | DPHIF=293.971 | PSI= 42.531 | DPSIF=-124.799 | PHITOT= 320.305 |
| FREE MOTION | | | | | | |
| Y= | .06120 | PHI= 135.305 | PHDOT=283.971 | PSI= 42.531 | PSIDOT=-124.799 | PHITOT = 320.305 |
| Y= | .06121 | PHI= 135.145 | PHDOT=273.559 | PSI= 42.459 | PSIDOT=-124.799 | PHITOT = 319.991 |
| VP= | -7.375 | VS= -20.845 | | | | |
| FREE MOTION | | | | | | |
| Y= | .06121 | PHI= 135.145 | PHDOT=273.559 | PSI= 42.459 | PSIDOT=-124.799 | PHITOT = 320.145 |
| Y= | .06122 | PHI= 136.991 | PHDOT=263.147 | PSI= 42.388 | PSIDOT=-124.799 | PHITOT = 319.991 |
| VP= | -7.319 | VS= -19.901 | | | | |
| FREE MOTION | | | | | | |
| Y= | .06122 | PHI= 136.991 | PHDOT=263.147 | PSI= 42.388 | PSIDOT=-124.799 | PHITOT = 319.991 |
| Y= | .06123 | PHI= 136.843 | PHDOT=252.735 | PSI= 42.316 | PSIDOT=-124.799 | PHITOT = 319.843 |
| Y= | .06124 | PHI= 136.702 | PHDOT=242.323 | PSI= 42.245 | PSIDOT=-124.799 | PHITOT = 319.702 |
| Y= | .06125 | PHI= 136.566 | PHDOT=231.912 | PSI= 42.173 | PSIDOT=-124.799 | PHITOT = 319.566 |
| Y= | .06126 | PHI= 136.436 | PHDOT=221.500 | PSI= 42.102 | PSIDOT=-124.799 | PHITOT = 319.436 |
| Y= | .06127 | PHI= 136.312 | PHDOT=211.088 | PSI= 42.030 | PSIDOT=-124.799 | PHITOT = 319.312 |
| Y= | .06128 | PHI= 136.194 | PHDOT=200.676 | PSI= 41.959 | PSIDOT=-124.799 | PHITOT = 319.194 |
| Y= | .06129 | PHI= 136.082 | PHDOT=190.265 | PSI= 41.887 | PSIDOT=-124.799 | PHITOT = 319.082 |
| Y= | .06130 | PHI= 135.976 | PHDOT=179.853 | PSI= 41.816 | PSIDOT=-124.799 | PHITOT = 318.976 |
| Y= | .06131 | PHI= 135.876 | PHDOT=169.441 | PSI= 41.744 | PSIDOT=-124.799 | PHITOT = 318.876 |
| Y= | .06132 | PHI= 135.782 | PHDOT=159.029 | PSI= 41.673 | PSIDOT=-124.799 | PHITOT = 318.782 |
| Y= | .06133 | PHI= 135.694 | PHDOT=148.618 | PSI= 41.601 | PSIDOT=-124.799 | PHITOT = 318.694 |
| Y= | .06134 | PHI= 135.611 | PHDOT=138.206 | PSI= 41.530 | PSIDOT=-124.799 | PHITOT = 318.611 |
| Y= | .06135 | PHI= 135.535 | PHDOT=127.794 | PSI= 41.458 | PSIDOT=-124.799 | PHITOT = 318.535 |
| Y= | .06136 | PHI= 135.465 | PHDOT=117.382 | PSI= 41.387 | PSIDOT=-124.799 | PHITOT = 318.465 |
| Y= | .06137 | PHI= 135.401 | PHDOT=106.971 | PSI= 41.315 | PSIDOT=-124.799 | PHITOT = 318.401 |
| Y= | .06138 | PHI= 135.342 | PHDOT=96.559 | PSI= 41.244 | PSIDOT=-124.799 | PHITOT = 318.342 |
| Y= | .06139 | PHI= 135.290 | PHDOT=86.147 | PSI= 41.172 | PSIDOT=-124.799 | PHITOT = 318.290 |
| Y= | .06140 | PHI= 135.244 | PHDOT=75.735 | PSI= 41.101 | PSIDOT=-124.799 | PHITOT = 318.244 |
| Y= | .06141 | PHI= 135.203 | PHDOT=65.323 | PSI= 41.029 | PSIDOT=-124.799 | PHITOT = 318.203 |
| Y= | .06142 | PHI= 135.169 | PHDOT=54.912 | PSI= 40.958 | PSIDOT=-124.799 | PHITOT = 318.169 |
| Y= | .06143 | PHI= 135.140 | PHDOT=44.500 | PSI= 40.886 | PSIDOT=-124.799 | PHITOT = 318.140 |
| Y= | .06144 | PHI= 135.118 | PHDOT=34.084 | PSI= 40.815 | PSIDOT=-124.799 | PHITOT = 318.118 |
| Y= | .06145 | PHI= 135.101 | PHDOT=23.676 | PSI= 40.743 | PSIDOT=-124.799 | PHITOT = 318.101 |
| Y= | .06146 | PHI= 135.091 | PHDOT=13.265 | PSI= 40.672 | PSIDOT=-124.799 | PHITOT = 318.091 |
| Y= | .06147 | PHI= 135.086 | PHDOT=2.853 | PSI= 40.600 | PSIDOT=-124.799 | PHITOT = 318.086 |
| Y= | .06148 | PHI= 135.087 | PHDOT=2.441 | PSI= 40.529 | PSIDOT=-124.799 | PHITOT = 318.087 |

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T= .06149 PHI= 133.955 P=DOT= 17.971 PCI= 40.457 PSIDOT=-124.799 PHITOT = 314.095
 T= .06150 PHI= 133.104 P=DOT= 24.282 PCI= 40.384 PSIDOT=-124.799 PHITOT = 318.108
 T= .06151 PHI= 133.127 P=DOT= 34.794 PCI= 40.314 PSIDOT=-124.799 PHITOT = 318.127
 T= .06152 PHI= 133.152 P=DOT= 49.206 PCI= 40.243 PSIDOT=-124.799 PHITOT = 318.152
 T= .06153 PHI= 133.144 P=DOT= 50.418 PCI= 40.171 PSIDOT=-124.799 PHITOT = 318.144
 T= .06154 PHI= 133.221 P=DOT= 70.929 PCI= 40.100 PSIDOT=-124.799 PHITOT = 318.221
 VP= -7.952 VS= 4.840

IMPACT
PHI= 133.221 DPHIF=-123.159 PSI= 40.100 DPSIF= -94.453 PHITOT= 318.221

VP= -5.609 VS= -8.517

FREE MOTION

T= .06156 PHI= 133.221 P=DOT=-123.159 PSI= 40.100 PSIDOT= -94.453 PHITOT = 318.221
 T= .06155 PHI= 133.153 P=DOT=-112.747 PSI= 48.046 PSIDOT= -94.453 PHITOT = 318.153
 VP= -5.400 VS= -7.765

FREE MOTION

T= .06155 PHI= 133.153 P=DOT=-112.747 PSI= 40.064 PSIDOT= -94.453 PHITOT = 318.153
 T= .06156 PHI= 133.092 P=DOT=-102.336 PSI= 39.992 PSIDOT= -94.453 PHITOT = 318.092
 VP= -5.401 VS= -7.025

FREE MOTION

T= .06156 PHI= 133.062 P=DOT=-102.336 PSI= 39.992 PSIDOT= -94.453 PHITOT = 318.092
 T= .06157 PHI= 133.036 P=DOT=-91.924 PSI= 39.937 PSIDOT= -94.453 PHITOT = 318.036
 VP= -5.402 VS= -6.202

FREE MOTION

T= .06157 PHI= 133.036 P=DOT=-91.924 PSI= 39.937 PSIDOT= -94.453 PHITOT = 318.036
 T= .06158 PHI= 132.946 P=DOT=-81.512 PSI= 35.883 PSIDOT= -94.453 PHITOT = 317.946
 VP= -5.401 VS= -5.564

FREE MOTION

T= .06158 PHI= 132.946 P=DOT=-81.512 PSI= 39.883 PSIDOT= -94.453 PHITOT = 317.946
 T= .06159 PHI= 132.943 P=DOT=-71.106 PSI= 39.829 PSIDOT= -94.453 PHITOT = 317.943
 VP= -5.400 VS= -4.867

IMPACT

PHI= 132.943 DPHIF= -81.556 PSI= 39.829 DPSIF= -92.786 PHITOT= 317.943

VP= -5.363 VS= -5.555

APPENDIX J

COMPUTER OUTPUT FOR STANDARD CONFIGURATION
WITH $\mu = .3$ AND $\epsilon = 0$

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Appendix J
Std. Config.
μ = .5, ε = 0

| A* | .19310 | R* | .15838 | C* | .30000E+00 | IPAL* | .91000E-07 | R* | .01365 | ALPHA* | 40.0000 | ISTAR* | .17000E-07 | PSI00T* | 0.000 | PHI00T* | -.000 |
|----|--------|--------------|---------|---------|------------|--------|------------|--------|--------|--------|---------|---------|------------|---------|---------|---------|-------|
| T* | .00000 | PHI= 135.000 | PHI00T* | 0.000 | G* | -.0457 | G00T* | 0.000 | PSI0* | 42.412 | PSI00T* | 0.000 | PHI00T* | 0.000 | PHI00T* | -.000 | |
| T* | .00000 | PHI= 135.000 | PHI00T* | .042 | G* | -.0457 | G00T* | .018 | PSI0* | 42.412 | PSI00T* | .195 | PHI00T* | .000 | PHI00T* | .000 | |
| T* | .00000 | PHI= 135.000 | PHI00T* | .219 | G* | -.0457 | G00T* | .047 | PSI0* | 42.412 | PSI00T* | .36A | PHI00T* | .000 | PHI00T* | .000 | |
| T* | .00001 | PHI= 135.000 | PHI00T* | .284 | G* | -.0457 | G00T* | .041 | PSI0* | 42.412 | PSI00T* | .542 | PHI00T* | .000 | PHI00T* | .000 | |
| T* | .00001 | PHI= 135.000 | PHI00T* | .421 | G* | -.0457 | G00T* | .119 | PSI0* | 42.412 | PSI00T* | .716 | PHI00T* | .000 | PHI00T* | .000 | |
| T* | .00001 | PHI= 135.000 | PHI00T* | .55A | G* | -.0457 | G00T* | .177 | PSI0* | 42.413 | PSI00T* | 1.063 | PHI00T* | .000 | PHI00T* | .000 | |
| T* | .00002 | PHI= 135.001 | PHI00T* | .827 | G* | -.0457 | G00T* | .215 | PSI0* | 42.413 | PSI00T* | 1.410 | PHI00T* | .001 | PHI00T* | .001 | |
| T* | .00004 | PHI= 135.002 | PHI00T* | 1.097 | G* | -.0457 | G00T* | .251 | PSI0* | 42.414 | PSI00T* | 2.105 | PHI00T* | .002 | PHI00T* | .002 | |
| T* | .00005 | PHI= 135.003 | PHI00T* | 2.177 | G* | -.0457 | G00T* | .447 | PSI0* | 42.414 | PSI00T* | 2.800 | PHI00T* | .003 | PHI00T* | .003 | |
| T* | .00007 | PHI= 135.007 | PHI00T* | 3.25A | G* | -.0456 | G00T* | .698 | PSI0* | 42.421 | PSI00T* | 4.189 | PHI00T* | .007 | PHI00T* | .007 | |
| T* | .00010 | PHI= 135.012 | PHI00T* | 4.33C | G* | -.0456 | G00T* | .910 | PSI0* | 42.42A | PSI00T* | 5.579 | PHI00T* | .012 | PHI00T* | .012 | |
| T* | .00015 | PHI= 135.028 | PHI00T* | 6.490 | G* | -.045A | G00T* | 1.392 | PSI0* | 42.44A | PSI00T* | A.357 | PHI00T* | .02A | PHI00T* | .02A | |
| T* | .00020 | PHI= 135.050 | PHI00T* | 8.639 | G* | -.0455 | G00T* | 1.954 | PSI0* | 42.47A | PSI00T* | 11.134 | PHI00T* | .050 | PHI00T* | .050 | |
| T* | .00030 | PHI= 135.111 | PHI00T* | 12.917 | G* | -.0453 | G00T* | 2.774 | PSI0* | 42.55A | PSI00T* | 14.686 | PHI00T* | .111 | PHI00T* | .111 | |
| T* | .00040 | PHI= 135.198 | PHI00T* | 17.142 | G* | -.0449 | G00T* | 3.848 | PSI0* | 42.667 | PSI00T* | 22.232 | PHI00T* | .198 | PHI00T* | .198 | |
| T* | .00050 | PHI= 135.308 | PHI00T* | 21.317 | G* | -.0445 | G00T* | 4.594 | PSI0* | 42.681 | PSI00T* | 27.771 | PHI00T* | .308 | PHI00T* | .308 | |
| T* | .00060 | PHI= 135.442 | PHI00T* | 25.471 | G* | -.0440 | G00T* | 5.491 | PSI0* | 42.98A | PSI00T* | 33.300 | PHI00T* | .442 | PHI00T* | .442 | |
| T* | .00070 | PHI= 135.599 | PHI00T* | 29.471 | G* | -.0434 | G00T* | 6.376 | PSI0* | 43.192 | PSI00T* | 38.819 | PHI00T* | .599 | PHI00T* | .599 | |
| T* | .00080 | PHI= 135.779 | PHI00T* | 33.368 | G* | -.0427 | G00T* | 7.250 | PSI0* | 43.430 | PSI00T* | 44.326 | PHI00T* | .779 | PHI00T* | .779 | |
| T* | .00090 | PHI= 135.981 | PHI00T* | 37.180 | G* | -.0420 | G00T* | 8.109 | PSI0* | 43.700 | PSI00T* | 49.819 | PHI00T* | .981 | PHI00T* | .981 | |
| T* | .00100 | PHI= 136.205 | PHI00T* | 40.911 | G* | -.0411 | G00T* | 8.944 | PSI0* | 44.000 | PSI00T* | 55.29A | PHI00T* | 1.205 | PHI00T* | 1.205 | |
| T* | .00110 | PHI= 136.443 | PHI00T* | 44.522 | G* | -.0402 | G00T* | 9.744 | PSI0* | 44.33A | PSI00T* | 60.762 | PHI00T* | 1.449 | PHI00T* | 1.449 | |
| T* | .00120 | PHI= 136.715 | PHI00T* | 48.01A | G* | -.0392 | G00T* | 10.567 | PSI0* | 44.697 | PSI00T* | 66.211 | PHI00T* | 1.715 | PHI00T* | 1.715 | |
| T* | .00130 | PHI= 136.989 | PHI00T* | 51.397 | G* | -.0381 | G00T* | 11.394 | PSI0* | 45.092 | PSI00T* | 71.642 | PHI00T* | 1.949 | PHI00T* | 1.949 | |
| T* | .00140 | PHI= 137.303 | PHI00T* | 54.659 | G* | -.0369 | G00T* | 12.173 | PSI0* | 45.518 | PSI00T* | 77.058 | PHI00T* | 2.203 | PHI00T* | 2.203 | |
| T* | .00150 | PHI= 137.628 | PHI00T* | 57.804 | G* | -.0356 | G00T* | 12.915 | PSI0* | 45.975 | PSI00T* | 82.457 | PHI00T* | 2.426 | PHI00T* | 2.426 | |
| T* | .00160 | PHI= 137.966 | PHI00T* | 60.837 | G* | -.0343 | G00T* | 13.648 | PSI0* | 46.463 | PSI00T* | 87.840 | PHI00T* | 2.966 | PHI00T* | 2.966 | |
| T* | .00170 | PHI= 138.322 | PHI00T* | 63.758 | G* | -.0329 | G00T* | 14.408 | PSI0* | 46.982 | PSI00T* | 93.207 | PHI00T* | 3.322 | PHI00T* | 3.322 | |
| T* | .00180 | PHI= 138.696 | PHI00T* | 66.554 | G* | -.0314 | G00T* | 15.118 | PSI0* | 47.531 | PSI00T* | 98.559 | PHI00T* | 3.696 | PHI00T* | 3.696 | |
| T* | .00190 | PHI= 139.085 | PHI00T* | 69.261 | G* | -.0298 | G00T* | 15.812 | PSI0* | 48.111 | PSI00T* | 103.896 | PHI00T* | 4.045 | PHI00T* | 4.045 | |
| T* | .00200 | PHI= 139.489 | PHI00T* | 71.864 | G* | -.0282 | G00T* | 16.489 | PSI0* | 48.727 | PSI00T* | 109.220 | PHI00T* | 4.449 | PHI00T* | 4.449 | |
| T* | .00210 | PHI= 139.908 | PHI00T* | 74.372 | G* | -.0266 | G00T* | 17.150 | PSI0* | 49.363 | PSI00T* | 114.532 | PHI00T* | 4.90A | PHI00T* | 4.90A | |
| T* | .00220 | PHI= 140.341 | PHI00T* | 76.790 | G* | -.0244 | G00T* | 17.794 | PSI0* | 50.034 | PSI00T* | 119.832 | PHI00T* | 5.341 | PHI00T* | 5.341 | |
| T* | .00230 | PHI= 140.788 | PHI00T* | 79.125 | G* | -.0230 | G00T* | 18.424 | PSI0* | 50.736 | PSI00T* | 125.123 | PHI00T* | 5.788 | PHI00T* | 5.788 | |
| T* | .00240 | PHI= 141.248 | PHI00T* | 81.381 | G* | -.0210 | G00T* | 19.07A | PSI0* | 51.46A | PSI00T* | 130.405 | PHI00T* | 6.248 | PHI00T* | 6.248 | |
| T* | .00250 | PHI= 141.721 | PHI00T* | 83.56A | G* | -.0192 | G00T* | 19.677 | PSI0* | 52.230 | PSI00T* | 135.680 | PHI00T* | 6.721 | PHI00T* | 6.721 | |
| T* | .00260 | PHI= 142.205 | PHI00T* | 85.687 | G* | -.0172 | G00T* | 20.271 | PSI0* | 53.023 | PSI00T* | 140.950 | PHI00T* | 7.205 | PHI00T* | 7.205 | |
| T* | .00270 | PHI= 142.702 | PHI00T* | 87.740 | G* | -.0152 | G00T* | 20.827 | PSI0* | 53.840 | PSI00T* | 146.216 | PHI00T* | 7.702 | PHI00T* | 7.702 | |
| T* | .00280 | PHI= 143.211 | PHI00T* | 89.741 | G* | -.0139 | G00T* | 21.349 | PSI0* | 54.69A | PSI00T* | 151.440 | PHI00T* | A.211 | PHI00T* | A.211 | |
| T* | .00300 | PHI= 143.731 | PHI00T* | 91.692 | G* | -.0129 | G00T* | 21.892 | PSI0* | 55.581 | PSI00T* | 156.743 | PHI00T* | A.731 | PHI00T* | A.731 | |
| T* | .00310 | PHI= 144.261 | PHI00T* | 93.59A | G* | -.0087 | G00T* | 22.471 | PSI0* | 56.49A | PSI00T* | 162.008 | PHI00T* | 9.261 | PHI00T* | 9.261 | |
| T* | .00320 | PHI= 144.803 | PHI00T* | 95.463 | G* | -.0084 | G00T* | 22.978 | PSI0* | 57.43A | PSI00T* | 167.275 | PHI00T* | 9.803 | PHI00T* | 9.803 | |
| T* | .00330 | PHI= 145.355 | PHI00T* | 97.292 | G* | -.0081 | G00T* | 23.441 | PSI0* | 58.411 | PSI00T* | 172.547 | PHI00T* | 10.355 | PHI00T* | 10.355 | |
| T* | .00340 | PHI= 145.918 | PHI00T* | 99.090 | G* | -.0077 | G00T* | 23.931 | PSI0* | 59.415 | PSI00T* | 177.825 | PHI00T* | 10.918 | PHI00T* | 10.918 | |
| T* | .00340 | PHI= 146.491 | PHI00T* | 100.859 | G* | -.0007 | G00T* | 24.408 | PSI0* | 60.440 | PSI00T* | 183.111 | PHI00T* | 11.491 | PHI00T* | 11.491 | |

Cycle No. 1

COUPLED MOTION

FREE MOTION

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FROM COPY REPRODUCED BY WFO

VP=-16.708 VS= 46.239
I-PACT
Te .00340 PHIZ 146.491 PMOOZ 100.854 PSIZ 311.114 PSIDIZ 143.111
Te .00341 PHIZ 146.551 PMOOZ 111.271 PSEIZ 311.217 PSEIDIZ 143.111
Te .00342 PHIZ 146.618 PMOOZ 121.453 PSEIZ 311.327 PSEIDIZ 143.111
Te .00343 PHIZ 146.691 PMOOZ 132.095 PSEIZ 311.427 PSEIDIZ 143.111
Te .00344 PHIZ 146.770 PMOOZ 142.506 PSEIZ 311.532 PSEIDIZ 143.111
Te .00345 PHIZ 146.856 PMOOZ 152.918 PSEIZ 311.637 PSEIDIZ 143.111
Te .00346 PHIZ 146.945 PMOOZ 163.330 PSEIZ 311.742 PSEIDIZ 143.111
Te .00347 PHIZ 147.041 PMOOZ 173.742 PSEIZ 311.846 PSEIDIZ 143.111
Te .00348 PHIZ 147.144 PMOOZ 184.153 PSEIZ 311.951 PSEIDIZ 143.111
Te .00349 PHIZ 147.252 PMOOZ 194.565 PSEIZ 312.056 PSEIDIZ 143.111
Te .00350 PHIZ 147.367 PMOOZ 204.977 PSEIZ 312.161 PSEIDIZ 143.111
Te .00351 PHIZ 147.487 PMOOZ 215.389 PSEIZ 312.266 PSEIDIZ 143.111
Te .00352 PHIZ 147.614 PMOOZ 225.800 PSEIZ 312.371 PSEIDIZ 143.111
Te .00353 PHIZ 147.748 PMOOZ 236.212 PSEIZ 312.476 PSEIDIZ 143.111
Te .00354 PHIZ 147.884 PMOOZ 246.624 PSEIZ 312.581 PSEIDIZ 143.111
Te .00355 PHIZ 148.029 PMOOZ 257.036 PSEIZ 312.686 PSEIDIZ 143.111
Te .00356 PHIZ 148.179 PMOOZ 267.447 PSEIZ 312.791 PSEIDIZ 143.111
Te .00357 PHIZ 148.335 PMOOZ 277.859 PSEIZ 312.896 PSEIDIZ 143.111
Te .00358 PHIZ 148.497 PMOOZ 288.271 PSEIZ 313.001 PSEIDIZ 143.111
Te .00359 PHIZ 148.665 PMOOZ 298.683 PSEIZ 313.105 PSEIDIZ 143.111
Te .00360 PHIZ 148.843 PMOOZ 309.095 PSEIZ 313.210 PSEIDIZ 143.111
Te .00361 PHIZ 149.029 PMOOZ 319.506 PSEIZ 313.315 PSEIDIZ 143.111
Te .00362 PHIZ 149.208 PMOOZ 329.918 PSEIZ 313.420 PSEIDIZ 143.111
Te .00363 PHIZ 149.398 PMOOZ 340.330 PSEIZ 313.525 PSEIDIZ 143.111
Te .00364 PHIZ 149.596 PMOOZ 350.742 PSEIZ 313.630 PSEIDIZ 143.111
Te .00365 PHIZ 149.800 PMOOZ 361.153 PSEIZ 313.735 PSEIDIZ 143.111
Te .00366 PHIZ 149.010 PMOOZ 371.565 PSEIZ 313.840 PSEIDIZ 143.111
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Te .00368 PHIZ 149.447 PMOOZ 392.389 PSEIZ 314.050 PSEIDIZ 143.111
Te .00369 PHIZ 149.675 PMOOZ 402.800 PSEIZ 314.155 PSEIDIZ 143.111
Te .00370 PHIZ 149.909 PMOOZ 413.212 PSEIZ 314.260 PSEIDIZ 143.111
Te .00371 PHIZ 150.149 PMOOZ 423.624 PSEIZ 314.364 PSEIDIZ 143.111
Te .00372 PHIZ 150.394 PMOOZ 434.036 PSEIZ 314.469 PSEIDIZ 143.111
Te .00373 PHIZ 150.646 PMOOZ 444.447 PSEIZ 314.574 PSEIDIZ 143.111
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Te .00375 PHIZ 152.167 PMOOZ 465.271 PSEIZ 314.784 PSEIDIZ 143.111
Te .00376 PHIZ 152.437 PMOOZ 475.683 PSEIZ 314.889 PSEIDIZ 143.111
Te .00377 PHIZ 152.712 PMOOZ 486.095 PSEIZ 314.994 PSEIDIZ 143.111
Te .00378 PHIZ 152.994 PMOOZ 496.506 PSEIZ 315.099 PSEIDIZ 143.111
Te .00379 PHIZ 153.281 PMOOZ 506.918 PSEIZ 315.204 PSEIDIZ 143.111
Te .00380 PHIZ 153.572 PMOOZ 517.330 PSEIZ 315.309 PSEIDIZ 143.111
Te .00381 PHIZ 153.874 PMOOZ 527.742 PSEIZ 315.414 PSEIDIZ 143.111
Te .00382 PHIZ 154.179 PMOOZ 538.153 PSEIZ 315.518 PSEIDIZ 143.111
VP=-5.278 VS= -5.278
PHIZ 146.179 DPPIZ -64.204 PSIZ 315.518 PSEIDIZ 57.532 PHITIZ 19.179
PHIZ 146.278 VS= -5.278
COUPLED MOTION
Te .00382 PHIZ 194.179 PHIDIZ -44.204 GSE -0.391 GSEIZ 193.111
Te .00392 PHIZ 193.896 PHIDIZ -35.023 GSE -0.398 GSEIZ 193.111
Te .00402 PHIZ 193.779 PHIDIZ -25.848 GSE -0.401 GSEIZ 193.111
Te .00403 PHIZ 193.777 PHIDIZ -16.673 GSE -0.401 GSEIZ 193.111
Te .00403 PHIZ 193.776 PHIDIZ -7.501 GSE -0.401 GSEIZ 193.111
Te .00404 PHIZ 193.776 PHIDIZ -8.326 GSE -0.401 GSEIZ 193.111
Te .00404 PHIZ 193.776 PHIDIZ -1.154 GSE -0.401 GSEIZ 193.111
Te .00404 PHIZ 193.776 PHIDIZ -0.982 GSE -0.401 GSEIZ 193.111
Te .00404 PHIZ 193.776 PHIDIZ 0.189 GSE -0.401 GSEIZ 193.111
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Te .00404 PHIZ 193.776 PHIDIZ 3.721 GSE -0.401 GSEIZ 193.111
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Te .00404 PHIZ 193.776 PHIDIZ 62.571 GSE -0.401 GSEIZ 193.111
Te .00404 PHIZ 193.776 PHIDIZ 63.748 GSE -0.401 GSEIZ 193.111

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V = -13.204 VS = -8.204 DPIF = 106.237 PSI = 42.844 DPSIF = 139.131 PMTIOT = 40.416
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 PSID = 41.102 PSIDOT = -9.345 PSID = 41.101 PSIDOT = -3.049 PSIDOT = 38.983
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| | | | | | | | | | | | |
|----------------|---------|-----|---------|-------|---------|-------|---------|-------|---------|-------|---------|
| IS | -0.1102 | PMT | 193.062 | PHOOT | 490.680 | MSI | 315.650 | PSIDU | 192.390 | PHIUI | 58.626 |
| IS | -0.1103 | PMT | 193.346 | PHOOT | 501.092 | PSI | 315.761 | PSIDU | 192.390 | PHIUI | 58.366 |
| IS | -0.1104 | PMT | 193.638 | PHOOT | 511.503 | PSI | 315.871 | PSIDU | 192.390 | PHIUI | 58.636 |
| VP | -17.741 | VS | 41.354 | | | | | | | | |
| I-PACT | | | | | | | | | | | |
| VP | -6.188 | VS | -6.188 | PHI | 193.636 | OPHIF | -76.532 | PSI | 315.871 | DPHIF | 67.106 |
| COUPLED MOTION | | | | | | | | | | | |
| IS | -0.1104 | PMT | 193.636 | PHOOT | -76.532 | G | -0.045 | GOOT | -10.811 | PSID | 315.771 |
| IS | -0.1114 | PMT | 193.243 | PHOOT | -46.509 | G | -0.043 | GOOT | -6.572 | PSID | 316.074 |
| IS | -0.1124 | PMT | 193.105 | PHOOT | -15.474 | G | -0.041 | GOOT | -2.140 | PSID | 316.237 |
| IS | -0.1125 | PMT | 193.096 | PHOOT | -11.562 | G | -0.040 | GOOT | -1.614 | PSID | 316.264 |
| IS | -0.1126 | PMT | 193.089 | PHOOT | -7.661 | G | -0.040 | GOOT | -1.096 | PSID | 316.264 |
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| IS | -0.1128 | PMT | 193.085 | PHOOT | -2.722 | G | -0.040 | GOOT | -0.342 | PSID | 316.258 |
| IS | -0.1128 | PMT | 193.084 | PHOOT | -2.741 | G | -0.040 | GOOT | -0.245 | PSID | 316.251 |
| IS | -0.1128 | PMT | 193.084 | PHOOT | -1.760 | G | -0.040 | GOOT | -0.177 | PSID | 316.251 |
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| IS | -0.1129 | PMT | 193.083 | PHOOT | -0.044 | G | -0.040 | GOOT | -0.006 | PSID | 316.251 |
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| IS | -0.1130 | PMT | 193.084 | PHOOT | 2.056 | G | -0.040 | GOOT | 0.247 | PSID | 316.250 |
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| IS | -0.1133 | PMT | 193.090 | PHOOT | 7.864 | G | -0.040 | GOOT | 0.188 | PSID | 316.241 |
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| IS | -0.1141 | PMT | 193.154 | PHOOT | 23.101 | G | -0.040 | GOOT | 0.000 | PSID | 316.140 |
| IS | -0.1144 | PMT | 193.194 | PHOOT | 26.862 | G | -0.040 | GOOT | 0.000 | PSID | 316.115 |
| IS | -0.1149 | PMT | 193.262 | PHOOT | 30.624 | G | -0.040 | GOOT | 0.000 | PSID | 316.090 |
| IS | -0.1154 | PMT | 193.361 | PHOOT | 34.386 | G | -0.040 | GOOT | 0.000 | PSID | 316.012 |
| IS | -0.1159 | PMT | 193.441 | PHOOT | 38.148 | G | -0.040 | GOOT | 0.000 | PSID | 315.783 |
| IS | -0.1164 | PMT | 193.623 | PHOOT | 41.910 | G | -0.040 | GOOT | 0.000 | PSID | 315.479 |
| IS | -0.1164 | PMT | 193.623 | PHOOT | 45.672 | G | -0.040 | GOOT | 0.000 | PSID | 315.100 |
| IS | -0.1174 | PMT | 193.967 | PHOOT | 49.434 | G | -0.040 | GOOT | 0.000 | PSID | 314.644 |
| IS | -0.1184 | PMT | 194.389 | PHOOT | 53.196 | G | -0.040 | GOOT | 0.000 | PSID | 314.121 |
| IS | -0.1194 | PMT | 194.844 | PHOOT | 56.958 | G | -0.040 | GOOT | 0.000 | PSID | 313.612 |
| IS | -0.1204 | PMT | 195.446 | PHOOT | 60.720 | G | -0.040 | GOOT | 0.000 | PSID | 313.121 |
| IS | -0.1214 | PMT | 196.070 | PHOOT | 64.482 | G | -0.040 | GOOT | 0.000 | PSID | 312.654 |
| IS | -0.1224 | PMT | 196.747 | PHOOT | 68.244 | G | -0.040 | GOOT | 0.000 | PSID | 312.215 |
| IS | -0.1234 | PMT | 197.470 | PHOOT | 72.006 | G | -0.040 | GOOT | 0.000 | PSID | 311.800 |
| IS | -0.1244 | PMT | 198.233 | PHOOT | 75.768 | G | -0.040 | GOOT | 0.000 | PSID | 311.403 |
| IS | -0.1254 | PMT | 199.028 | PHOOT | 79.530 | G | -0.040 | GOOT | 0.000 | PSID | 311.025 |
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| IS | -0.1294 | PMT | 202.371 | PHOOT | 94.578 | G | -0.040 | GOOT | 0.000 | PSID | 309.725 |
| IS | -0.1304 | PMT | 203.213 | PHOOT | 98.340 | G | -0.040 | GOOT | 0.000 | PSID | 309.480 |
| IS | -0.1314 | PMT | 204.045 | PHOOT | 102.102 | G | -0.040 | GOOT | 0.000 | PSID | 309.265 |
| IS | -0.1324 | PMT | 204.861 | PHOOT | 105.864 | G | -0.040 | GOOT | 0.000 | PSID | 309.075 |

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T= .01334 PMI= 205.657 PHDOI= 126.871 G= -.0036 GDOT= 31.579 PSID= 301.796 PSI001= 72.171
 T= .01334 PMI= 206.429 PHDOI= 132.212 G= -.0004 GDOT= 32.047 PSID= 300.011 PSI001= 71.429
 T= .01354 PMI= 207.171 PHDOI= 126.961 G= .0029 GDOT= 32.511 PSID= 204.620 PSI001= 72.171

FREE MOTION

T= .01354 PMI= 127.171 PHDOI= 126.961 PSI= 47.957 PSID001= 245.981 PMITOT= 72.171
 T= .01354 PMI= 127.247 PHDOI= 137.372 PSI= 47.414 PSID001= 245.981 PMITOT= 72.247
 T= .01355 PMI= 127.329 PHDOI= 147.746 PSI= 47.875 PSID001= 245.981 PMITOT= 72.329
 T= .01357 PMI= 127.416 PHDOI= 154.196 PSI= 47.534 PSID001= 245.981 PMITOT= 72.416
 T= .01358 PMI= 127.510 PHDOI= 168.608 PSI= 47.393 PSID001= 245.981 PMITOT= 72.510
 T= .01359 PMI= 127.610 PHDOI= 179.019 PSI= 47.252 PSID001= 245.981 PMITOT= 72.610
 T= .01360 PMI= 127.715 PHDOI= 189.431 PSI= 47.111 PSID001= 245.981 PMITOT= 72.715
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 T= .01393 PMI= 134.545 PHDOI= 533.019 PSI= 42.460 PSID001= 245.981 PMITOT= 79.545
 T= .01394 PMI= 134.853 PHDOI= 543.431 PSI= 42.318 PSID001= 245.981 PMITOT= 79.853
 T= .01395 PMI= 135.168 PHDOI= 553.843 PSI= 42.178 PSID001= 245.981 PMITOT= 80.168

VP= -14.378 VS= 42.251

IMPACT

Cycle No. 3
 PMI= 135.168
 VP= -8.773 VS= -8.773

COUPLED MOTION

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Ix .05121 PML 149.737 PML001= 74.731 G= -.0707
 Ix .05121 PML 141.368 PML001= 66.664 G= -.0187
 Ix .05121 PML 141.950 PML001= 66.691 G= -.0164
 Ix .05121 PML 142.364 PML001= 90.674 G= -.0144
 Ix .05121 PML 142.389 PML001= 92.694 G= -.0122
 Ix .05121 PML 143.425 PML001= 94.443 G= -.0699
 Ix .05121 PML 143.971 PML001= 96.314 G= -.0076
 Ix .05121 PML 144.528 PML001= 98.114 G= -.0052
 Ix .05401 PML 145.098 PML001= 99.874 G= -.0027
 Ix .05421 PML 146.673 PML001= 101.504 G= -.0003
 Ix .05421 PML 146.268 PML001= 103.314 G= -.0022
 Ix .05431 PML 146.857 PML001= 104.994 G=

FREE MOTION

Ix .05431 PML 146.857 PML001= 104.998 PML001= 104.998
 Ix .05432 PML 146.920 PML001= 115.410 PML001= 115.410
 Ix .05433 PML 146.989 PML001= 125.821 PML001= 125.821
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 Ix .05467 PML 152.888 PML001= 479.821 PML001= 479.821
 Ix .05468 PML 153.166 PML001= 490.233 PML001= 490.233
 Ix .05469 PML 153.450 PML001= 500.645 PML001= 500.645

VP= -17.732 VS= 40.250

IMPACT

VP= -6.245 VS= -6.265 PML 193.450 PML001= -77.927 PML001= 67.838 PML001= 298.450

COUPLED MOTION

Ix .05469 PML 193.450 PML001= -77.927 PML001= -10.974 PML001= 315.934 PML001= 298.450
 Ix .05470 PML 193.090 PML001= -47.541 PML001= -6.633 PML001= 316.245 PML001= 298.000
 Ix .05489 PML 192.907 PML001= -16.134 PML001= -2.241 PML001= 316.407 PML001= 297.907
 Ix .05491 PML 192.890 PML001= -8.204 PML001= -0.823 PML001= 316.417 PML001= 297.800
 Ix .05494 PML 192.804 PML001= -2.261 PML001= -0.106 PML001= 316.422 PML001= 297.804

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|-----|---------|--------------|----------------|-------------|-----------------|----------------|
| I= | .05730 | PHI= 128.299 | PHO01= 247.749 | PSI= 46.478 | PSI001= 267.452 | PHI01= 313.641 |
| I= | .05731 | PHI= 129.441 | PHO01= 251.161 | PSI= 46.336 | PSI001= 247.452 | PHI01= 313.441 |
| I= | .05732 | PHI= 128.589 | PHO01= 261.573 | PSI= 46.194 | PSI001= 247.452 | PHI01= 313.589 |
| I= | .05733 | PHI= 128.743 | PHO01= 273.984 | PSI= 46.052 | PSI001= 247.452 | PHI01= 313.743 |
| I= | .05734 | PHI= 129.069 | PHO01= 286.396 | PSI= 45.911 | PSI001= 247.452 | PHI01= 313.903 |
| I= | .05735 | PHI= 129.241 | PHO01= 296.808 | PSI= 45.769 | PSI001= 247.452 | PHI01= 314.069 |
| I= | .05736 | PHI= 129.418 | PHO01= 305.220 | PSI= 45.627 | PSI001= 247.452 | PHI01= 314.241 |
| I= | .05737 | PHI= 129.602 | PHO01= 315.631 | PSI= 45.485 | PSI001= 247.452 | PHI01= 314.418 |
| I= | .05738 | PHI= 129.792 | PHO01= 326.043 | PSI= 45.343 | PSI001= 247.452 | PHI01= 314.602 |
| I= | .05739 | PHI= 129.988 | PHO01= 336.455 | PSI= 45.202 | PSI001= 247.452 | PHI01= 314.792 |
| I= | .05740 | PHI= 130.190 | PHO01= 346.867 | PSI= 45.060 | PSI001= 247.452 | PHI01= 314.988 |
| I= | .05741 | PHI= 130.397 | PHO01= 357.278 | PSI= 44.918 | PSI001= 247.452 | PHI01= 315.190 |
| I= | .05742 | PHI= 130.611 | PHO01= 367.690 | PSI= 44.776 | PSI001= 247.452 | PHI01= 315.397 |
| I= | .05743 | PHI= 130.831 | PHO01= 378.102 | PSI= 44.635 | PSI001= 247.452 | PHI01= 315.611 |
| I= | .05744 | PHI= 131.056 | PHO01= 388.514 | PSI= 44.493 | PSI001= 247.452 | PHI01= 315.831 |
| I= | .05745 | PHI= 131.288 | PHO01= 409.337 | PSI= 44.351 | PSI001= 247.452 | PHI01= 316.056 |
| I= | .05746 | PHI= 131.525 | PHO01= 419.749 | PSI= 44.209 | PSI001= 247.452 | PHI01= 316.288 |
| I= | .05747 | PHI= 131.769 | PHO01= 430.161 | PSI= 44.067 | PSI001= 247.452 | PHI01= 316.525 |
| I= | .05748 | PHI= 132.018 | PHO01= 440.573 | PSI= 43.926 | PSI001= 247.452 | PHI01= 316.769 |
| I= | .05749 | PHI= 132.273 | PHO01= 450.984 | PSI= 43.784 | PSI001= 247.452 | PHI01= 317.018 |
| I= | .05750 | PHI= 132.535 | PHO01= 461.396 | PSI= 43.642 | PSI001= 247.452 | PHI01= 317.273 |
| I= | .05751 | PHI= 132.802 | PHO01= 471.808 | PSI= 43.500 | PSI001= 247.452 | PHI01= 317.535 |
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| I= | .05753 | PHI= 133.355 | PHO01= 492.631 | PSI= 43.217 | PSI001= 247.452 | PHI01= 318.076 |
| I= | .05754 | PHI= 133.640 | PHO01= 503.043 | PSI= 43.075 | PSI001= 247.452 | PHI01= 318.355 |
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| I= | .05757 | PHI= 134.532 | PHO01= 534.278 | PSI= 42.650 | PSI001= 247.452 | PHI01= 319.228 |
| I= | .05758 | PHI= 134.841 | PHO01= 544.690 | PSI= 42.508 | PSI001= 247.452 | PHI01= 319.532 |
| I= | .05759 | PHI= 135.156 | PHO01= 555.102 | PSI= 42.366 | PSI001= 247.452 | PHI01= 319.841 |
| I= | .05760 | PHI= 135.481 | PHO01= 565.514 | PSI= 42.224 | PSI001= 247.452 | PHI01= 320.156 |
| VP= | -14.443 | VS= | 42.322 | | | |

IMPACT

| | | | | |
|--------------|----------------|-------------|----------------|----------------|
| PHI= 135.156 | DPHIF= 115.965 | PSI= 42.224 | DPSIF= 151.480 | PHI01= 320.156 |
| VP= -8.841 | VS= -8.841 | | | |

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