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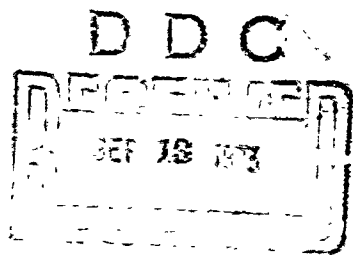
TECHNICAL MEMORANDUM 2103

(C) TRANSVERSE MOTION
OF
8 INCH PROJECTILE,
XM673, IN THE
XM201, M2A2 GUN TUBE,
MK-16 AND MCLG GUN (U)

BY
S. H. CHU

AUGUST 1973

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ABSTRACT

The dynamic behavior of a projectile during acceleration in the gun tube requires a quantitative description, since if balloting becomes excessive, undesirable conditions such as damage to fuzing, shell body engraving, inaccuracy of fire due to yaw, and yaw velocity at the muzzle may result. The approach taken in this report utilizes the equations of motion derived in an earlier report titled, "Transverse Motion of an Accelerating Shell" [1] to describe the balloting motion of the 8-inch XM673 projectile fired in the MK-16, MCLG gun, XM201 and M2A2 gun tubes.

Most previous solutions which have appeared in published works to date discuss the problem in a simple way, or consider separately the main factors that effect projectile motion. Effects of friction forces at the bourrelet and the driving band, changes of the eccentricity and the location of the center of gravity, and the wall thickness of the shell were considered in this formulation.

The analysis shows that the contact of the bourrelet on the gun tube is intermittent when the C. G. eccentricity is zero or very small and the contact is continuous when the eccentricity is large and that this parameter is the one that most effects the performance of the projectile and the associated fuze. The analytical results are presented in graphic form.

INTRODUCTION

As part of the design and evaluation of the 8 inch XM673 projectile, an analysis was performed of the balloting motion of the projectile if fired from each of the MK-16 and MCLG guns and the M2A2 and XM201 gun tubes. Since the projectiles are precisely machined it is assumed that the projectile configuration is symmetrical about its geometrical axis, which is taken as the 3'-axis of the moving body coordinate system 1', 2', 3' (Fig. 1). The mass distribution of the projectile was considered to have various degrees of non-uniformity. For zero eccentricity, the center of gravity of the projectile will be at the 3'-axis, otherwise it has an eccentricity of some magnitude from the 3'-axis. As in Reference 1, another moving body coordinate system 1, 2, 3 was selected and made parallel to the 1', 2', 3' system with its origin at the center of gravity of the projectile. Since the eccentricity of the center of gravity is usually small, it is assumed that the products of inertia of the projectile about the coordinate system 1, 2, 3 may be ignored and that the projectile has constant polar and transverse moments of inertia about this moving coordinate system.

The calculation is done with the assumption that the gun tube is rigid, stationary, and straight, and the geometrical projectile axis always intersects the center of the driving band diameter and that the latter is always centered along the gun tube axis. The 3-axis of the coordinate system 1, 2, 3 may or may not coincide with the 3'-axis of the system 1', 2', 3', but the corresponding axes are parallel to each other. The eccentricity, ϵ , is expressed in inches and is the distance between the 3- and the 3'-axis. It may also be expressed in terms of the moment (in-oz) of the projectile weight about the geometrical axis of the projectile, i. e. the product of the projectile weight (oz.) and the eccentricity distance (in.). Hence the eccentricity distance (in.) is equal to the eccentricity moment (in-oz.) divided by the projectile weight (oz.) Four cases with $\epsilon = 0, 10, 25$ and 50 in-oz respectively and a projectile wall thickness $t = 0.40$ in. are computed for each type of gun tube to show the effects of the eccentricity. To investigate the effects of (1) friction forces, (2) projectile wall thickness and (3) location of center of gravity

of the projectile, cases with (1) no friction forces, (2) wall thicknesses of 0.38 and 0.42 inches respectively, and (3) distance from the bourrelet to the driving band unchanged but with the distance from the center of gravity to the driving band reduced to three quarters and one half the original value respectively, are computed for the XM201 gun tube only.

In these computations the equations of motion derived in Reference 1 have been used with the addition of friction forces, both at the bourrelet and the driving band, to increase the accuracy of the computation.

THEORY

The coordinate systems and Euler's angles used in the computations are shown in Fig. 1. The Z-axis is taken along the gun tube and gun elevation is 45 degrees with the X-axis positioned horizontally and the Y-axis perpendicular. Consequently, the angle α used in the following equations of motion is taken as 135 degrees.

The equations of motion are derived in the same way as shown in Reference 1 with the exception that the friction forces and their associate moments are added to the original forces and moments at the bourrelet and the driving band. For easy understanding of the computations and completeness of this report, some of these equations and the related definitions of symbols are repeated below.

The six equations of motion are:

$$\begin{aligned}
 & m \mathcal{D} \left[\dot{\theta} \cos \theta \sin \psi + \ddot{\psi} \sin \theta \cos \psi - (\dot{\psi}^2 + \dot{\theta}^2) \sin \theta \sin \psi + 2 \dot{\psi} \dot{\theta} \cos \theta \cos \psi \right] \\
 & - m c \left[\dot{\phi} (\sin \phi \cos \psi + \cos \phi \cos \theta \sin \psi) + \ddot{\psi} (\cos \phi \sin \psi + \sin \phi \cos \theta \cos \psi) \right. \\
 & \left. - \dot{\theta}^2 \sin \phi \cos \theta \sin \psi - 2 \dot{\phi} \dot{\psi} (\sin \phi \sin \psi - \cos \phi \cos \theta \cos \psi) \right. \\
 & \left. - \dot{\theta}^2 \sin \phi \sin \theta \sin \psi + (\dot{\psi}^2 + \dot{\phi}^2) (\cos \phi \cos \psi - \sin \phi \cos \theta \sin \psi) \right]
 \end{aligned}$$

$$\begin{aligned}
& -2\dot{\phi}\dot{\theta}\cos\phi\sin\theta\sin\psi - 2\dot{\psi}\dot{\theta}\sin\phi\sin\theta\cos\psi] \\
& = (F_{b1} + F_{c1})\cos\psi - (F_{b2} + F_{c2})\cos\theta\sin\psi + (F_{b3} + F_{c3} \\
& + A\sec\theta)\sin\theta\sin\psi \tag{1}
\end{aligned}$$

$$\begin{aligned}
& m\mathcal{Q}[\ddot{\psi}\sin\theta\sin\psi - \ddot{\theta}\cos\theta\cos\psi + (\dot{\psi}^2 + \dot{\theta}^2)\sin\theta\cos\psi + 2\dot{\psi}\dot{\theta}\cos\theta\sin\psi] \\
& + m\mathcal{E}[\ddot{\phi}(\cos\phi\cos\theta\cos\psi - \sin\phi\sin\psi) + \dot{\psi}(\cos\phi\cos\psi - \sin\phi\cos\theta\sin\psi) \\
& - \ddot{\theta}\sin\phi\sin\theta\cos\psi - (\dot{\psi} + \dot{\phi})^2(\cos\phi\sin\psi + \sin\phi\cos\theta\cos\psi) \\
& - \dot{\theta}^2\sin\phi\cos\theta\cos\psi - 2\dot{\phi}\dot{\theta}\cos\phi\sin\theta\cos\psi + 2\dot{\psi}\dot{\theta}\sin\phi\sin\theta\sin\psi \\
& - 2\dot{\phi}\dot{\psi}(\cos\phi\cos\theta\sin\psi + \sin\phi\cos\psi)] \\
& = (F_{b1} + F_{c1})\sin\psi + (F_{b2} + F_{c2})\cos\theta\cos\psi - (F_{b3} + F_{c3} + A\sec\theta)\sin\theta\cos\psi \\
& + mg\cos\alpha \tag{2}
\end{aligned}$$

$$\begin{aligned}
& m\ddot{W} - m\mathcal{Q}(\ddot{\theta}\sin\theta + \dot{\theta}^2\cos\theta) + m\mathcal{E}[\ddot{\phi}\cos\phi\sin\theta + \ddot{\theta}\sin\phi\cos\theta \\
& - (\dot{\phi} + \dot{\theta})^2\sin\phi\sin\theta + 2\dot{\phi}\dot{\theta}\cos\phi\cos\theta] \\
& = (F_{b2} + F_{c2})\sin\theta + (F_{b3} + F_{c3} + A\sec\theta)\cos\theta - mg\sin\alpha \tag{3}
\end{aligned}$$

$$\begin{aligned}
& I(\ddot{\theta} - \dot{\psi}^2\sin\theta\cos\theta) + I_3\dot{\psi}(\dot{\psi}\cos\theta + \dot{\phi})\sin\theta \\
& = M_{b1} + M_{c1} - A\sec\theta \tag{4}
\end{aligned}$$

$$\begin{aligned}
& I(\dot{\psi}\sin\theta + 2\dot{\psi}\dot{\theta}\cos\theta) - I_3\dot{\theta}(\dot{\psi}\cos\theta + \dot{\phi}) \\
& = M_{b2} + M_{c2} + A\sec\theta \tag{5}
\end{aligned}$$

$$I_3 (\ddot{\psi} \cos \theta + \dot{\psi} \dot{\theta} \sin \theta - \ddot{\theta} \psi \sin \theta)$$

$$= M_{b3} + M_{c3} \quad (6)$$

where ψ, θ, ϕ = Euler's angles (radians), $\dot{\psi}, \dot{\theta}, \dot{\phi}$ and $\ddot{\psi}, \ddot{\theta}, \ddot{\phi}$ are the corresponding velocities (rad/sec) and accelerations (rad/sec²) respectively

Q = distance from C. G. to driving band (in)

e = eccentricity of C. G. from geometrical projectile axis (in.)

A = area of bore (in.²)

α = Y-axis inclination to the horizontal line (radians)

W = axial displacement of driving band diameter center (in.). \dot{W} and \ddot{W} are the corresponding velocity (in/sec) and acceleration (in/sec²).

g = gravitational acceleration, 386 in/sec²

m = mass of projectile (lb - in⁻¹ - sec²)

I = transverse mass moment of inertia of projectile (lb - in - sec²)

I_3 = polar mass moment of inertia of projectile (lb - in - sec²)

p = firing pressure (psi)

F_{b1}, F_{b2}, F_{b3} = total bourrelet contact force components along the 1-, 2-, and 3-axis respectively (lbs.)

F_{c1}, F_{c2}, F_{c3} = total driving band contact force components along 1-, 2-, and 3-axis respectively (lbs.)

M_{b1}, M_{b2}, M_{b3} = total moment components of bourrelet contact forces about the 1-, 2-, and 3-axis respectively (in-lb)

M_{c1}, M_{c2}, M_{c3} = total moment components of driving band forces about the 1-, 2-, and 3-axis respectively (in-lb)

The friction forces are equivalent to the products of the normal forces and the frictional coefficients. The friction coefficient for the bourrelet contact is taken as that of dry sliding of mild steel on mild steel, equal to 0.57 [2]. The friction coefficient at the driving band contact is obtained from several trial computations. First a frictional coefficient is assumed for use in calculating the travel and velocity of the projectile. The results are then compared to those from interior ballistics computations with the same firing pressure. The computation is repeated, varying the friction coefficient until a reasonable agreement is reached, and then that coefficient is taken as the desired one. The normal forces are obtained from the contact forces at the bourrelet and the driving band. The compressive pressure exerted on the driving band by the gun tube is also included. Since there are no simple equations available for this pressure calculation, an approximate pressure distribution of 40,000 and 20,000 psi based on average experimental maximum and minimum data is assumed at the breech and the muzzle portion, respectively, in the computation.

With the addition of the friction forces and their associated moments at the bourrelet and the driving band contact, the total components of the forces and moments may be computed with the following equations:

The total forces and moments at the bourrelet contact are:

$$F_{bl} = \frac{-\mu_b E t^3 R \dot{\theta} (\dot{\psi} + \dot{\phi} \cos \theta) [r \cos \theta + \frac{\theta}{|\theta|} (h + Q) \sin \theta - R]}{0.135 r^2 |\theta| \sqrt{(\dot{W} - \frac{R \dot{\theta}}{|\theta|})^2 + R^2 (\dot{\psi} + \dot{\phi} \cos \theta)^2}} \quad (7)$$

$$F_{b2} = \frac{Et^3}{0.135r^2} \left[r \cos \theta + \frac{\theta}{|\theta|} (h + \mathcal{L}) \sin \theta - R \right] \\ \times \left[\frac{\theta}{|\theta|} \cos \theta - \frac{\mu_b \left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right) \sin \theta}{\sqrt{\left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right)^2 + R^2 (\dot{\psi} + \dot{\phi} \cos \theta)^2}} \right] \quad (8)$$

$$F_{b3} = - \frac{Et^3}{0.135r^2} \left[r \cos \theta + \frac{\theta}{|\theta|} (h + \mathcal{L}) \sin \theta - R \right] \\ \times \left[\frac{\theta}{|\theta|} \sin \theta + \frac{\mu_b \left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right) \cos \theta}{\sqrt{\left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right)^2 + R^2 (\dot{\psi} + \dot{\phi} \cos \theta)^2}} \right] \quad (9)$$

$$M_{b1} = - \frac{Et^3}{0.135r} \left[r \cos \theta + \frac{\theta}{|\theta|} (h + \mathcal{L}) \sin \theta - R \right] \\ \times \left\{ \frac{h\theta \cos \theta}{|\theta|} - \left(r + \frac{\epsilon\theta}{|\theta|} \sin \phi \right) \sin \theta \right. \\ \left. - \frac{\mu_b \left[h \sin \theta + \frac{\theta}{|\theta|} \left(r + \frac{\epsilon\theta}{|\theta|} \sin \phi \right) \cos \theta \right] \left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right)}{\sqrt{\left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right)^2 + R^2 (\dot{\psi} + \dot{\phi} \cos \theta)^2}} \right\} \quad (10)$$

$$M_{b2} = - \frac{Et^3}{0.135r^2} \left[r \cos \theta + \frac{\theta}{|\theta|} (h + \mathcal{L}) \sin \theta - R \right] \\ \times \left\{ \frac{\theta \sin \theta}{|\theta|} + \frac{\mu_b \left[\frac{h\theta R}{|\theta|} (\dot{\psi} + \dot{\phi} \cos \theta) + \left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right) \cos \theta \right]}{\sqrt{\left(\dot{W} - \frac{R\theta\dot{\theta}}{|\theta|} \right)^2 + R^2 (\dot{\psi} + \dot{\phi} \cos \theta)^2}} \right\} \quad (11)$$

$$\begin{aligned}
M_{b3} = & -\frac{Et^3}{0.135r} \left[r \cos\theta + \frac{\theta}{|\theta|} (h+\Delta) \sin\theta - R \right] \\
& \times \left\{ \mu_b \left[R(\psi+\phi \cos\theta) \left(r + \frac{\epsilon\theta}{|\theta|} \sin\phi \right) + \epsilon \left(W - \frac{R\theta\dot{\theta}}{|\theta|} \right) \sin\theta \cos\phi \right] \right. \\
& \left. \frac{\sqrt{\left(W - \frac{R\theta\dot{\theta}}{|\theta|} \right)^2 + R^2 (\psi+\phi \cos\theta)^2}}{\sqrt{\left(W - \frac{R\theta\dot{\theta}}{|\theta|} \right)^2 + R^2 (\psi+\phi \cos\theta)^2}} \right. \\
& \left. - \frac{\epsilon\theta}{|\theta|} \cos\theta \cos\phi \right\} \quad (12)
\end{aligned}$$

and the components of the total forces and moments at the driving band are:

$$F_{c1} = \frac{\pi}{2} f_{sm} R (\sin\psi_s + \mu_c \sin\gamma \cos\psi_s) \quad (13)$$

$$\begin{aligned}
F_{c2} = & \frac{-\pi R f_{sm}}{2} \left(\cos\psi_s \cos\theta + \frac{4}{\pi} \mu_c \cos\gamma \sin\theta \right. \\
& \left. - \mu_c \sin\gamma \sin\psi_s \cos\theta \right) - 2\pi R [f_n (\sin\gamma + \mu_c \cos\gamma) \\
& + \mu_c p_c d \cos\gamma] \sin\theta \quad (14)
\end{aligned}$$

$$\begin{aligned}
F_{c3} = & \frac{\pi R f_{sm}}{2} \left(\cos\psi_s \sin\theta - \frac{4}{\pi} \mu_c \cos\gamma \cos\theta \right. \\
& \left. - \mu_c \sin\gamma \sin\psi_s \sin\theta \right) - 2\pi R [f_n (\sin\gamma + \mu_c \cos\gamma) \\
& + \mu_c p_c d \cos\gamma] \cos\theta \quad (15)
\end{aligned}$$

$$\begin{aligned}
M_{c1} = & -2\pi R f_n (\Delta \sin\theta - \epsilon \cos\theta \sin\phi) (\sin\gamma + \mu_c \cos\gamma) \\
& - \frac{R f_{sm}}{2} \left\{ \pi [\Delta \cos\theta - \left(\frac{8R}{3\pi} \cos\phi_s - \epsilon \sin\phi \right) \sin\theta] \right. \\
& \left. \times (\cos\psi_s - \mu_c \sin\gamma \sin\psi_s) + 4\mu_c \cos\gamma [\Delta \sin\theta \right. \\
& \left. + \left(\frac{\pi R}{4} \cos\phi_s - \epsilon \sin\phi \right) \cos\theta] \right\}
\end{aligned}$$

$$- 2\pi \mu_c R p_c d \cos \gamma (\psi \sin \theta - \epsilon \cos \theta \sin \phi) \quad (16)$$

$$\begin{aligned} M_{c2} = & 2\pi R f_n [R (\cos \gamma - \mu_c \sin \gamma) \sin \theta \\ & - \epsilon \cos \theta \cos \phi (\sin \gamma + \mu_c \cos \gamma)] \\ & + \frac{R f_{sm}}{2} \left\{ \pi \left[\left(\frac{8R}{3\pi} \sin \phi + \epsilon \cos \phi \right) (\cos \psi_s - \mu_c \sin \gamma \sin \psi_s) \sin \theta \right. \right. \\ & - \psi (\mu_c \sin \gamma \cos \psi_s + \sin \psi_s) \left. \left. - 4\mu_c \left[\left(\frac{\pi R}{4} \sin \phi_s + \epsilon \cos \theta \right) \right. \right. \right. \\ & \left. \left. \times \cos \gamma \cos \theta + \frac{R}{3} \sin \gamma \sin \theta \right] \right\} - 2\pi \mu_c R p_c d (\epsilon \cos \gamma \cos \theta \cos \phi \\ & + R \sin \gamma \sin \theta) \quad (17) \end{aligned}$$

$$\begin{aligned} M_{c3} = & 2\pi R f_n [R (\cos \gamma - \mu_c \sin \gamma) \cos \theta \\ & + \epsilon (\sin \gamma + \mu_c \cos \gamma) \cos \phi \sin \theta] \\ & + 2\pi \mu_c R p_c d (\epsilon \cos \gamma \sin \theta \cos \phi - R \sin \gamma \cos \theta) \\ & + \frac{R f_{sm}}{2} \left\{ \pi \left[\left(\frac{8R}{3\pi} \sin \phi_s + \epsilon \cos \phi \right) (\cos \psi_s - \mu_c \sin \gamma \sin \psi_s) \cos \theta \right. \right. \\ & - \left(\frac{8R}{3\pi} \cos \phi_s - \epsilon \sin \phi \right) (\mu_c \sin \gamma \cos \psi_s + \sin \psi_s) \left. \left. \right. \right. \\ & \left. \left. + 4\mu_c \left[\left(\frac{\pi R}{4} \sin \phi_s + \epsilon \cos \phi \right) \cos \gamma \sin \theta - \frac{R}{3} \sin \gamma \cos \theta \right] \right\} \quad (18) \end{aligned}$$

where E = Young's modulus of projectile wall material, psi

r = radius of projectile, in.

t = thickness of projectile wall, in.

R = radius of bore, in.

d = width of driving band, in.

h = distance from C. G. to the bourrelet, in.

$|\theta|$ = absolute value of θ , rad. $\frac{\theta}{|\theta|}$ is used to change the sign of the related quantity when θ becomes negative

μ_b = friction coefficient at the bourrelet

μ_c = friction coefficient at the driving band

f_{sm} = maximum side normal force at the driving band per unit of circumferential length, lb/in

f_n = uniform force normal to the forward surface of the square rifling grooves per unit of circumferential length, lb/in

p_c = driving band pressure, psi

γ = twist angle of rifling, rad.

ϕ_s = angle from the diameter of the region where the side forces are acting at the driving band to the node axis or l-axis, rad.

ψ_s = projection of ϕ_s angle on the cross-sectional plane of the gun tube, rad.

The displacement of the center of the driving band diameter is related to the other quantities by the equation

$$\dot{W} \tan \gamma = R (\dot{\psi} + \dot{\phi} \cos \theta) \quad (19)$$

INPUT DATA FOR COMPUTATIONS

Computations were performed for the 8 inch, XM673 projectile fired in the XM201 and M2A2 gun tubes, and MCLG and MK-16 guns respectively. The shell has the following dimensions and

properties:

L (distance from driving band to bourrelet) = 11.539 in.

\mathcal{L} (distance from driving band to C. G.) = 9.266 in.
(6.950 and 4.633 in. respectively are used to compute the effect of change of C. G. location for the XM201 gun tube)

h (distance from bourrelet to C. G.) = $L - \mathcal{L}$

s (distance from C. G. to nose of projectile) = 26.87 in.

t (wall thickness) = .40 in. (.38 and .42 in. respectively are used to compute the effect of wall thickness for the XM201 gun tube)

ϵ (eccentricity of C. G. from the geometrical axis of projectile) = 0, 10, 25 and 50 in-oz (i. e. 0, .00313, .00781 and .01563 in. eccentricity distance)

E (Young's modulus for the projectile steel) = 30×10^6 psi

I (transverse weight moment of inertia) = 15745 lb-in^2

I_3 (polar weight moment of inertia) = 1831 lb-in^2

mg (weight of projectile) = 200 lbs.

r (radius of projectile bourrelet) = 3.997 in

All the guns have a bore of 8.00 inches and are positioned at the elevation of 45 degrees so that α value used in the computation is 135 degrees or 2.356 radians. The other characteristics of the guns are:

Gun or Gun Tube Type	TL(Travel), in.	γ (Twist Angle), deg.
XM201	274.0	8.92705
M2A2	168.0	7.16246
MK-16	388.7	7.16246
MCLG	394.4	8.92705

The initial conditions of the shell for all computations are taken as:

$$\begin{array}{llll}
 \psi = 0, & \dot{\psi} = 0, & X = 0, & \dot{X} = 0, \\
 \theta = .0001 \text{ rad.}, & \dot{\theta} = 0, & Y = 0, & \dot{Y} = 0, \\
 \phi = 0, & \dot{\phi} = 0, & Z = 0, & \dot{Z} = 0,
 \end{array}$$

The coefficient of friction μ_b at the bourrelet was taken as .57 and that at the driving band, μ_c , was determined by the method described earlier to be .004, .009, .02 and .02 for XM201, M2A2 gun tubes, MK-16 and MCLG guns, respectively.

The firing pressure for the various guns or gun tubes used in the computations are the given base pressures as shown in Figs. 2a, 2b, 24, 31 and 38, respectively. The same firing pressure is used for all computations for the respective gun or gun tube.

RESULTS OF COMPUTATIONS AND DISCUSSION

The results of computations are presented by the following figures:

Figs. 2a, 2b, 24, 31 and 38 show the base firing pressure and the travel of the shell inside the gun tube with respect to time (milliseconds) for the XM201, M2A2 gun tube, MCLG and MK-16 gun respectively. The base firing pressure was given and the travel was computed. The same given firing pressure is used for computations of all cases of the same type of gun tube

or gun. The travel variations of different cases of the same type of gun tube or gun are very small. Consequently, the pressure and the travel curves of various cases for each type of gun tube or gun are presented by one curve respectively.

Figs. 3a, 3b, 25, 32 and 39 show the computed velocity and the acceleration at the center of gravity of the projectile with respect to the time for the XM201, M2A2 gun tube, MCLG and MK-16 gun respectively. The variations in velocity and acceleration become noticeable only near the end of firing when the firing pressure is decreasing rapidly. But they are still of very small magnitude. Consequently, the corresponding travel variations are also very small as mentioned before.

Figs. 4-7, 26, 33 and 40 present the paths or the polar positions of the C. G. and the bourrelet center as seen from the muzzle down to the breech, for the various cases of the XM201, M2A2 tube, MCLG and MK-16 gun. The R value denotes the scale of the drawing and it is the radius of the circle in inches. It is seen that when there is no or small C. G. eccentricity the shell will make intermittent contact with the gun tube, but contact is continuous as the eccentricity increases. The friction forces will retard the rotation of the shell with respect to the gun tube. The polar distance of both the C. G. and the bourrelet center decrease with thicker walled shell and shorter distance between the C. G. and the driving band. The precession angle is retarded by friction and low values of eccentricity.

Figs. 8-11, 27, 34 and 41 show the results of computations of the angular positions (in degrees) of the contact points on the gun tube and the bourrelet of the projectile respectively with respect to the projectile travel (inches), for the XM201, M2A2 gun tube, MCLG and MK-16 gun. The deflection at the bourrelet, normal to the gun tube wall, is also plotted. It is again seen that the contact of bourrelet on the gun tube is intermittent when the C. G. eccentricity is zero or very small, and the contact is continuous when the eccentricity is large. The path of the contact point on the bourrelet is not always a horizontal straight line when plotted against projectile travel, which indicates that the motion of the projectile may not be considered as that of a compound pendulum with its oscillation plane rotating about the

gun tube axis. The frictional forces seem to cause the precession angle to be smaller than for the no friction cases, however, the presence of eccentricity is a more significant factor. The deflection at the bourrelet increases with larger magnitude of the eccentricity, thinner projectile wall and longer distance between the C.G. and the driving band, respectively.

Figs. 12-15, 28, 35, and 42 present the computed results of the angles, velocities and accelerations of yaw for different cases of the XM201, M2A2 gun tube, MCLG and MK-16 gun. The effect of increasing the C.G. eccentricity or the projectile wall thickness, and decreasing the friction or the C.G. to driving band distance, respectively seem to increase the variation frequency in the yaw angle, velocity and acceleration of the projectile.

Figs. 16-19, 29, 36, and 43 show the results of computations of accelerations normal to the projectile axis and at the C.G., the bourrelet center, and the axial points with a distance from the projectile nose equal to 2.5, 5.0, 7.5, and 15.0 inches, respectively, for the XM201, M2A2 gun tube, MCLG and MK-16 gun. They indicate that the normal accelerations will increase when the C.G. eccentricity is increased or when there is no friction. The variation frequency of the normal acceleration seems to increase with projectile wall thickness or shorter C.G. to driving band distances.

Figs. 20-23, 30, 37 and 44 show the forces acting on the projectile at the contact point of the bourrelet with the gun tube against the time (ms), for the XM201, M2A2 gun tube, MCLG and MK-16 gun, respectively. The force component F_1 is in the direction of the yaw or nutation axis, F_2 is perpendicular to both the yaw and the shell axis, and F_3 is along the shell axis. Their magnitudes are presented in terms of mg's or in weights of the shell. It is seen that the forces will increase with greater C.G. eccentricity, shell wall thickness and distance between the C.G. and the driving band. The force component F_1 is zero and F_3 nearly zero when there is no friction.

A summary of some results is presented in Table I.

CONCLUSION AND RECOMMENDATIONS

Based on the calculated data and as indicated in the discussion, it is concluded that the eccentricity of the center of gravity of the projectile from its geometrical axis has the greatest effect on the motion of the shell inside the gun tube. The motion of the shell becomes more complicated when the eccentricity is increased. The motion may not be considered as that of a compound pendulum with its oscillation plane rotating about the gun tube axis. When eccentricity is very high, this condition tends to be approached. The deflection at the bourrelet, the yaw angle, the normal acceleration of axial points and the bourrelet contact force are increased with larger C. G. eccentricity.

Since the increase of the C. G. eccentricity increases rapidly the bourrelet contact force and the normal accelerations at the axial points of the shell and these quantities may affect the performance of the shell and the associated fuze, it is therefore recommended that the C. G. eccentricity be made as small as possible so as to improve the shell performance.

REFERENCES

1. Chu, S. H. and Soechting, F. K.: Transverse Motion of an Accelerating Shell, Technical Report 4314, Picatinny Arsenal, Dover, NJ, June 1972.
2. Baumeister, Theodore and Marks, Lionel S. (Editors): Standard Handbook for Mechanical Engineers, Seventh Edition, page 3-35, McGraw-Hill Book Company, 1967.

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TABLE I SUMMARY OF RESULTS

GUN OR GUN TUBE TYPE	SHELL WALL THICKNESS, in.	C.G. ECCENTRICITY, in-oz.	VELOCITY AT MUZZLE fps	PEAK AXIAL ACC., g's	YAW AT MUZZLE		PEAK NORMAL ACC. AT FUZE (2.5 in. FROM SHELL NOSE) g's	PEAK LATERAL FORCE AT BOURRELET, mg's
					Angle, 10^{-6} rad.	Velocity 10^{-3} rad/sec (Abs. Value)		
XM201	.40	0	2507	8500	63	33	14	10
	.40	10	2504	8500	1197	153	103	48
	.40	25	2496	8496	2318	498	228	112
	.40	50	2486	8488	3853	471	393	196
XM201 No Friction	.40	0	2530	8548	170	66	15	8
	.40	10	2530	8548	1147	130	136	54
	.40	25	2530	8548	2386	566	264	110
	.40	50	2530	8548	4405	971	503	214
XM201	.38	25	2497	8494	2582	261	218	102
	.42	25	2496	8498	1684	405	222	114
XM201 Original C.G. to Driving Band Distance Reduced By: 3/4 1/2	.40	25	2499	8498	1679	1116	211	85
	.40	25	2501	8498	1882	96	255	83

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TABLE I SUMMARY OF RESULTS (Continued)

GUN OR GUN TUBE TYPE	SHELL WALL THICKNESS, in.	C.G. ECCENTRICITY in-oz.	VELOCITY AT MUZZLE fps	PEAK AXIAL ACC., g's	YAW AT MUZZLE		PEAK NORMAL ACC. AT FUZE (2.5 in. FROM SHELL NOSE) g's	PEAK LATERAL FORCE AT BOURRELET, mg's
					Angle, 10 ⁻⁶ rad.	Velocity 10 ⁻³ rad/sec (Abs. Value)		
M2A2	.40	0	1879	8300	264	73	12	9
	.40	10	1877	8300	761	58	46	26
	.40	25	1875	8296	899	181	61	38
	.40	50	1872	8290	1203	71	87	57
MCIG	.40	0	3050	8222	111	33	13	9
	.40	10	3045	8222	1052	120	103	46
	.40	25	3032	8218	2297	1292	293	132
	.40	50	3015	8206	4199	1189	565	254
MK-16	.40	0	2811	681C	343	66	11	8
	.40	10	2805	6802	1064	571	108	55
	.40	25	2798	6798	1762	7	191	101
	.40	50	2787	6792	3448	802	317	172

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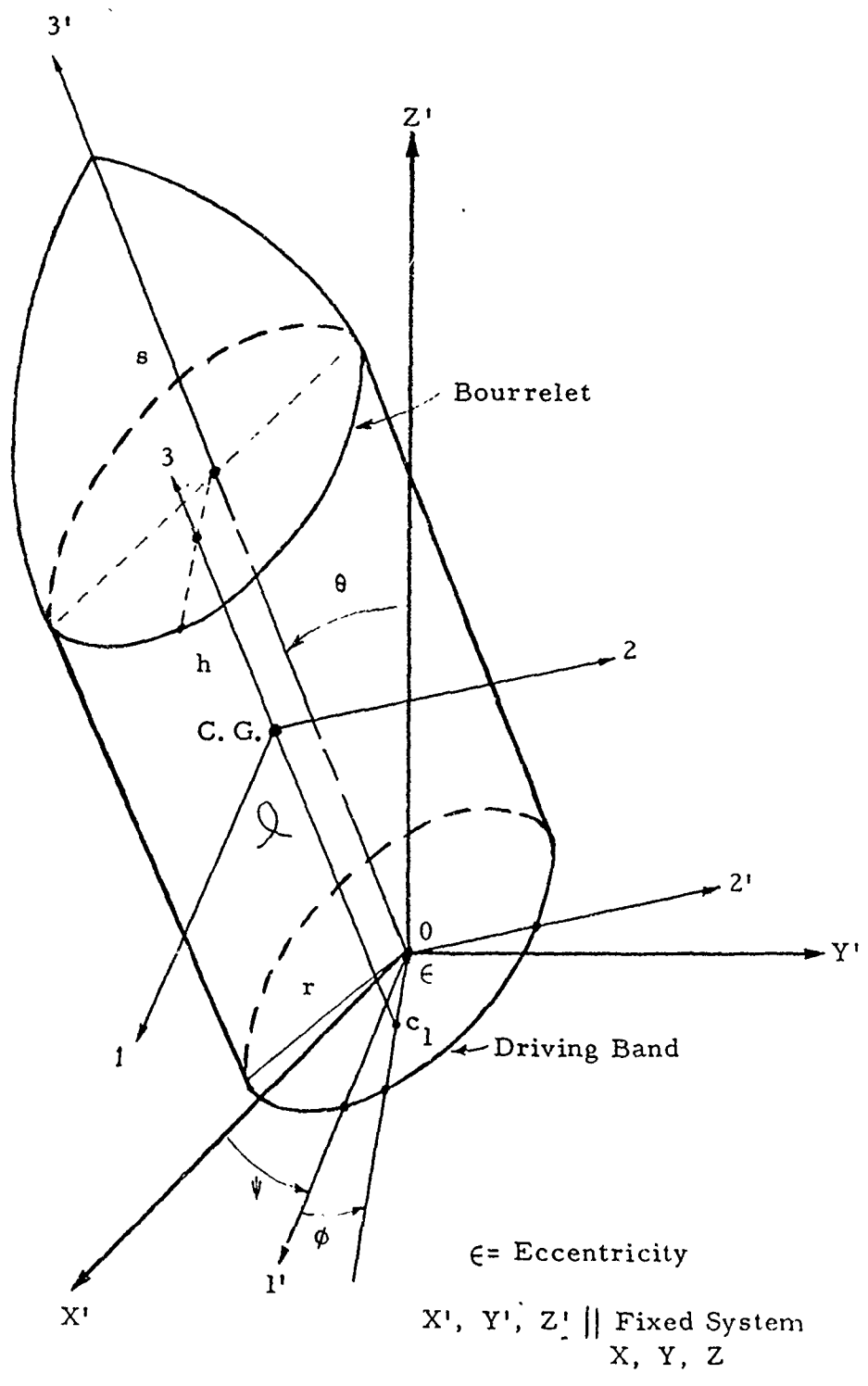


FIGURE 1

Coordinate Systems and Euler's Angles

XM201 TUBE

FIGURE 2a

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PRESSURE AND TRAVEL

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY: 0 IN-OZ. WALL THICKNESS .40 IN.

70
25
50

TRAVEL, INCHES

PRESSURE, 10^2 PSI

400.00
350.00
300.00
250.00
200.00
150.00
100.00
50.00
0

0 3.09 6.18 9.27 12.36 15.45 18.54

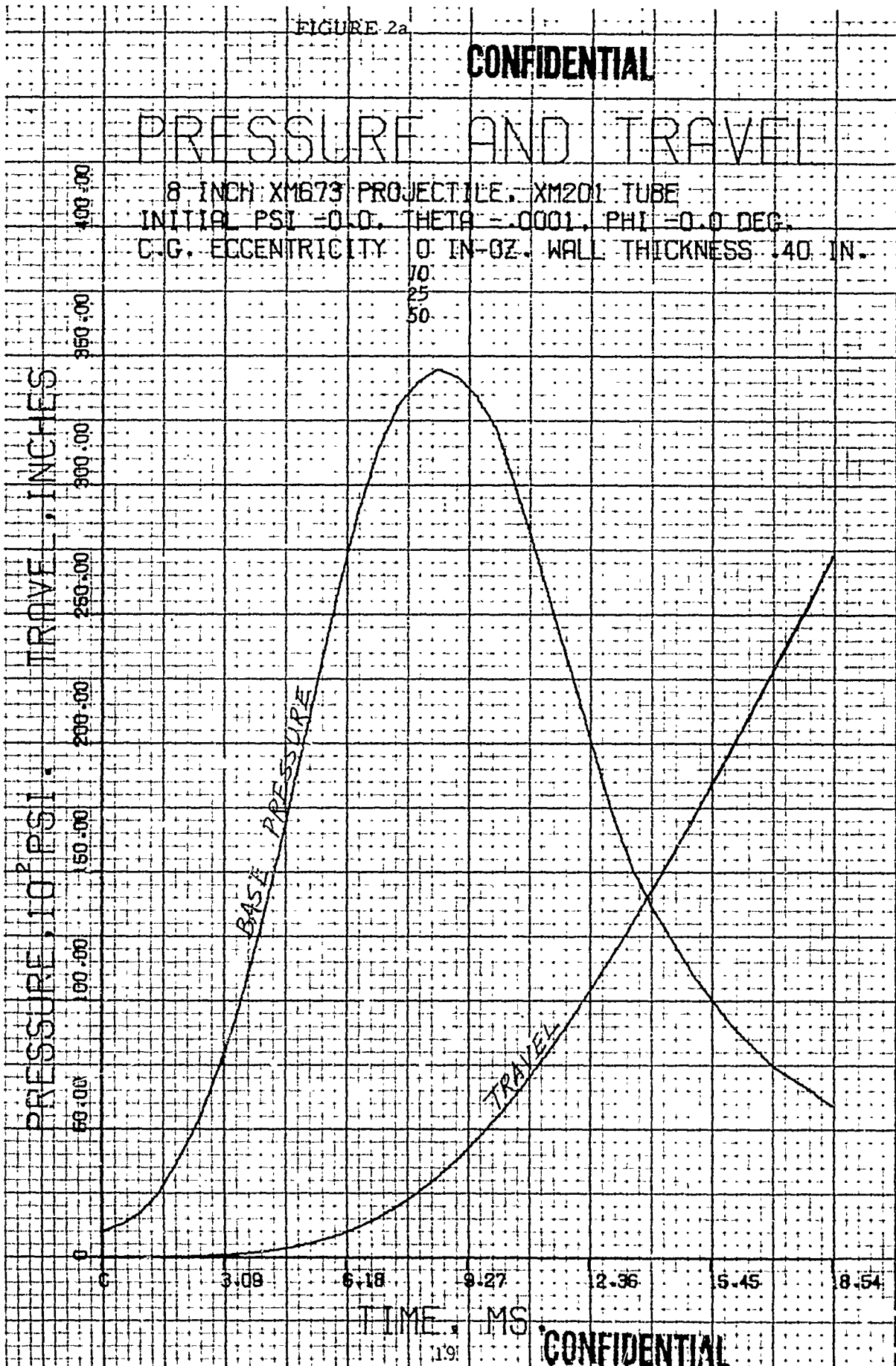
TIME, MS

19

BASE PRESSURE

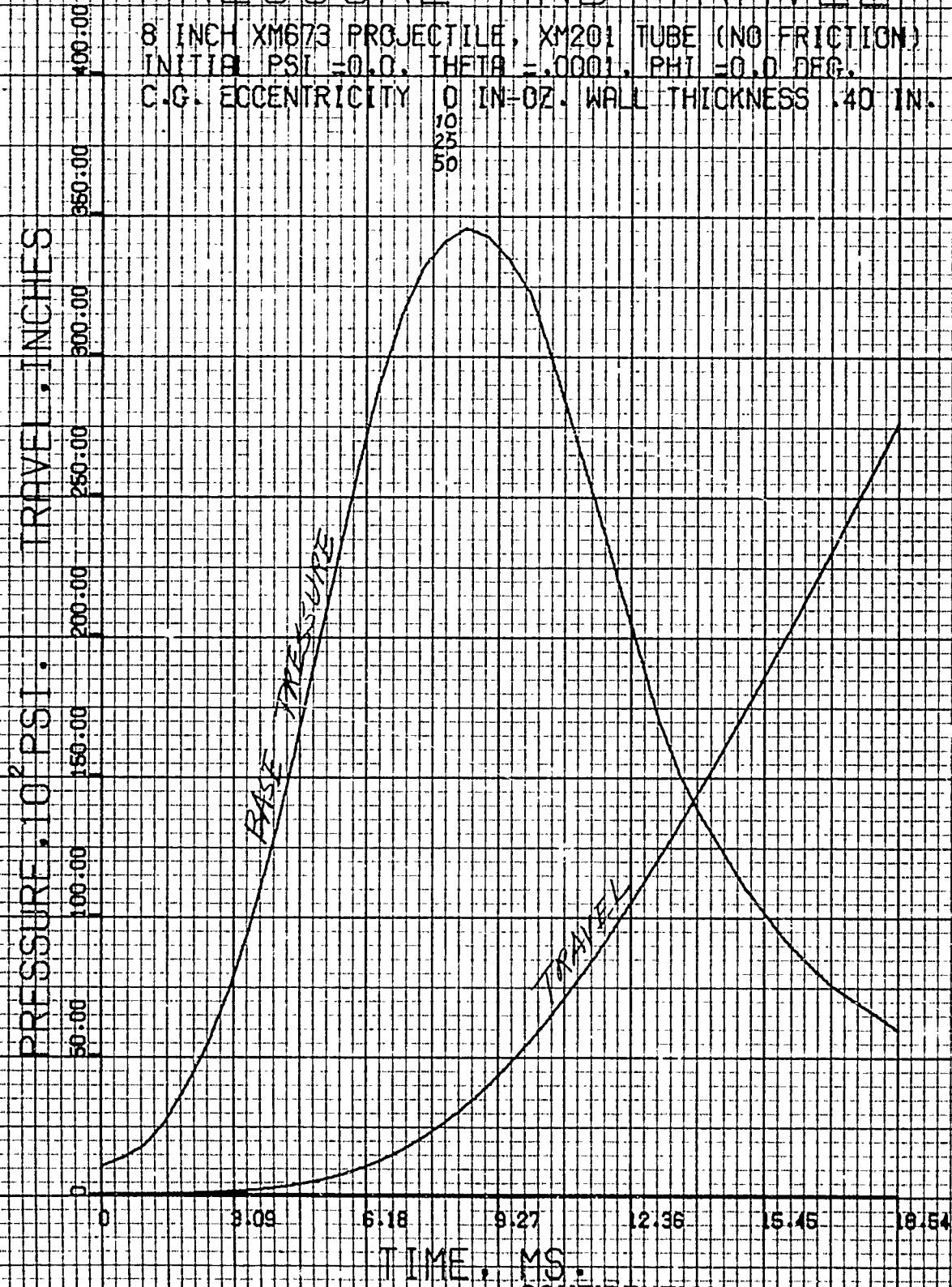
TRAVEL

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PRESSURE AND TRAVEL

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.



10
25
50

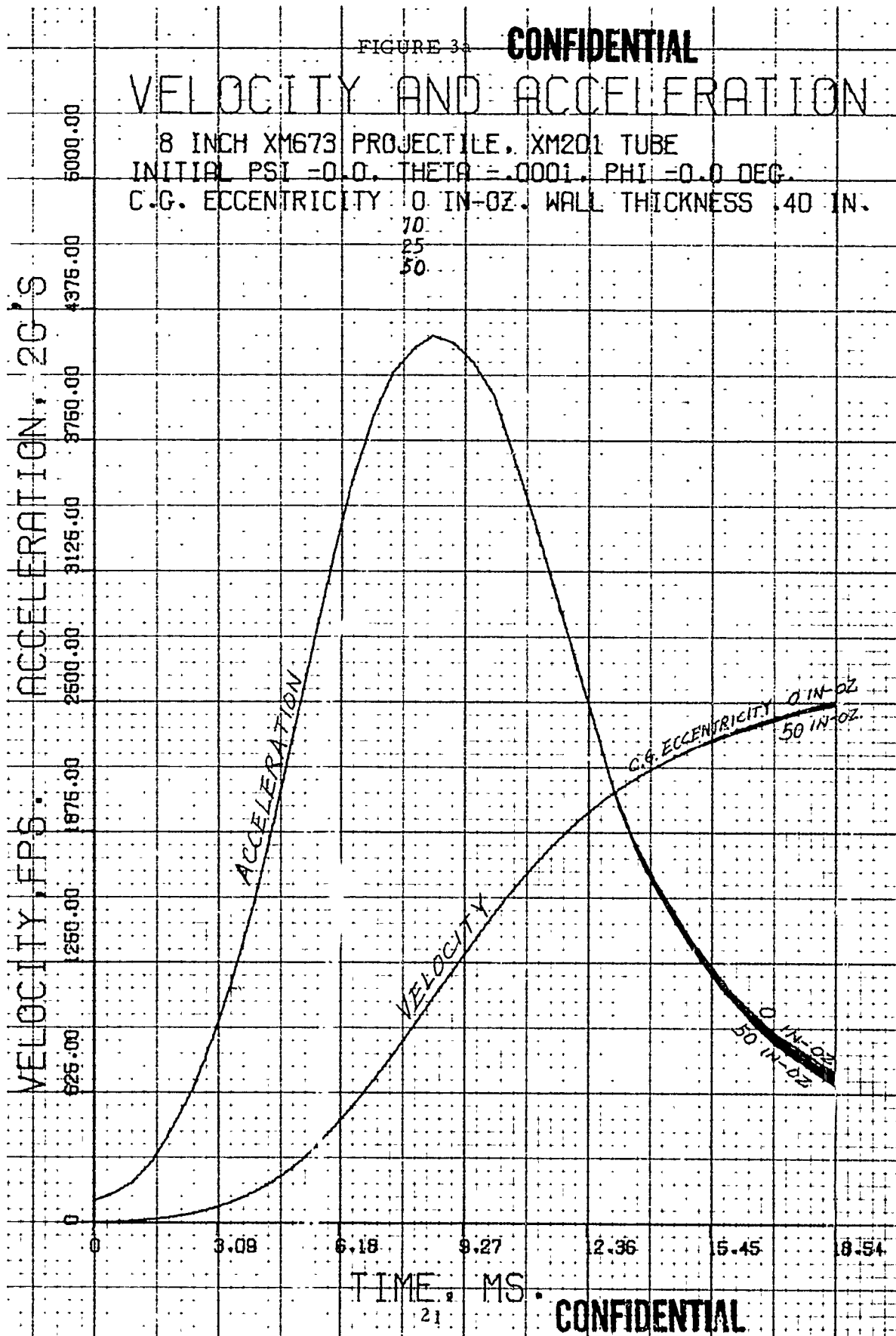
FIGURE 3

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VELOCITY AND ACCELERATION

8 INCH XM673 PROJECTILE, XM201 TUBE
 INITIAL PSI -0.0, THETA = .0001, PHI -0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.

70
 25
 50



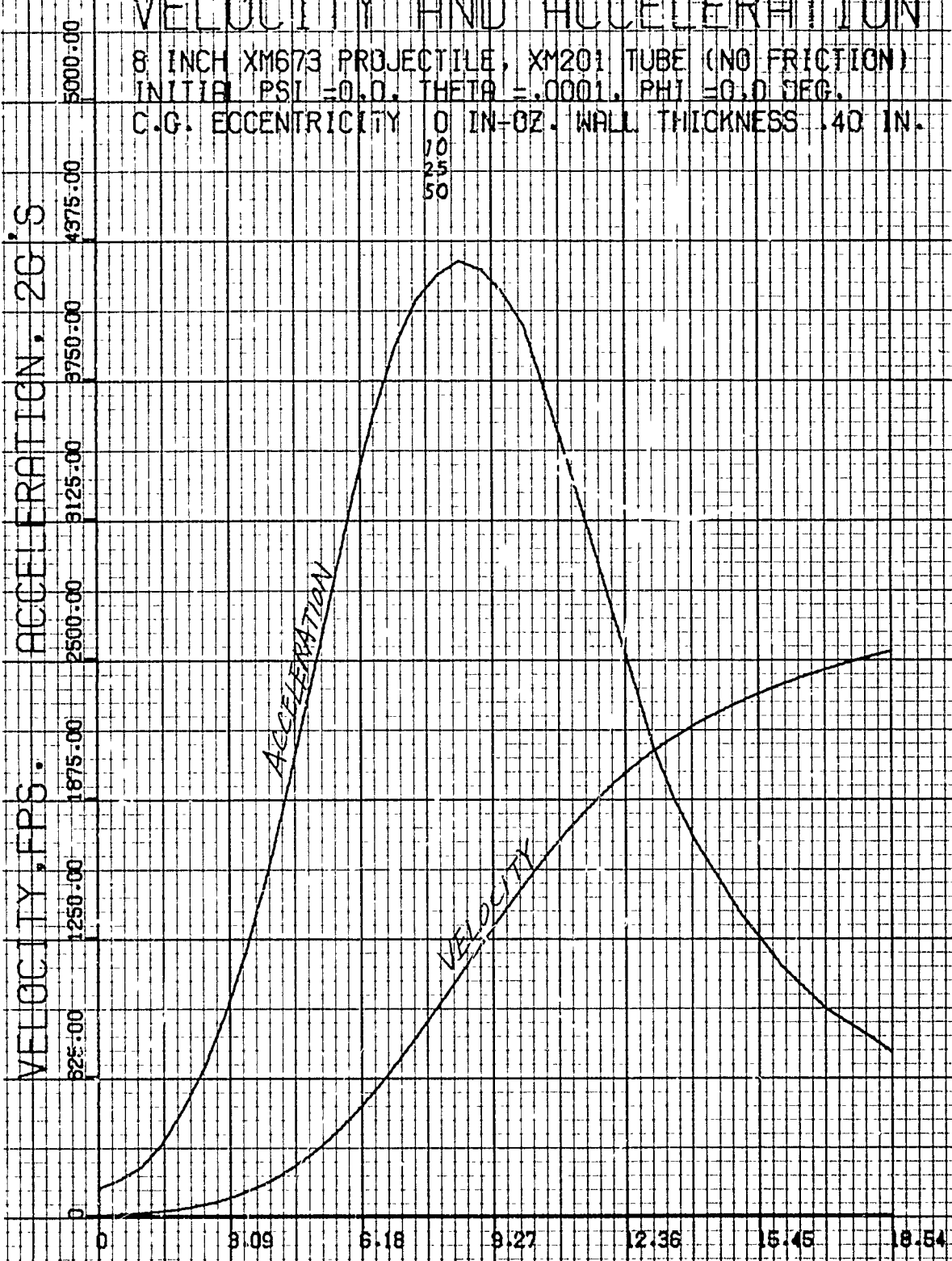
TIME, MS

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VELOCITY AND ACCELERATION

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
 INITIA PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.

10
25
50

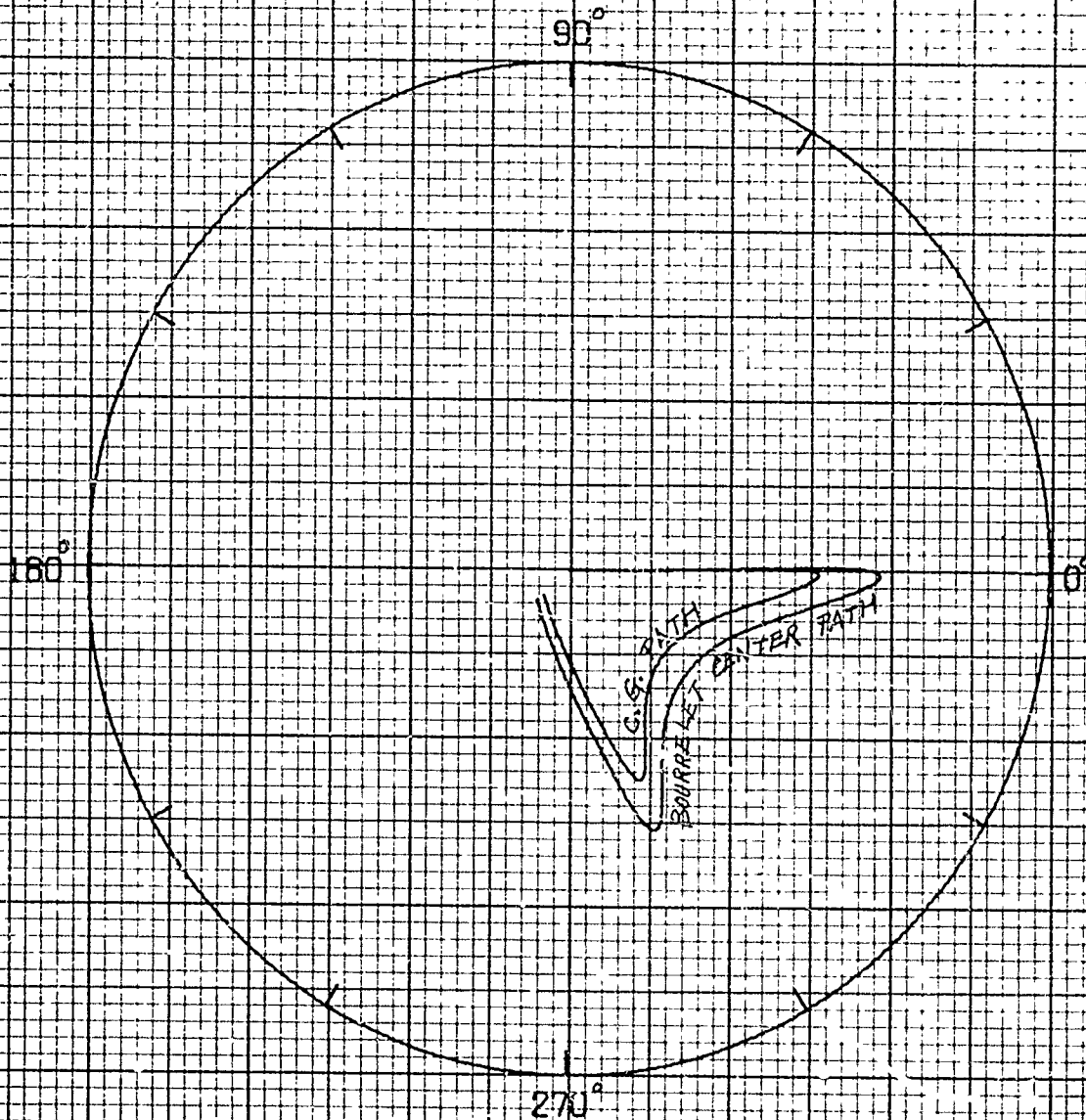


TIME, MS

FIGURE 4a

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ. WAL. THICKNESS .40 IN.

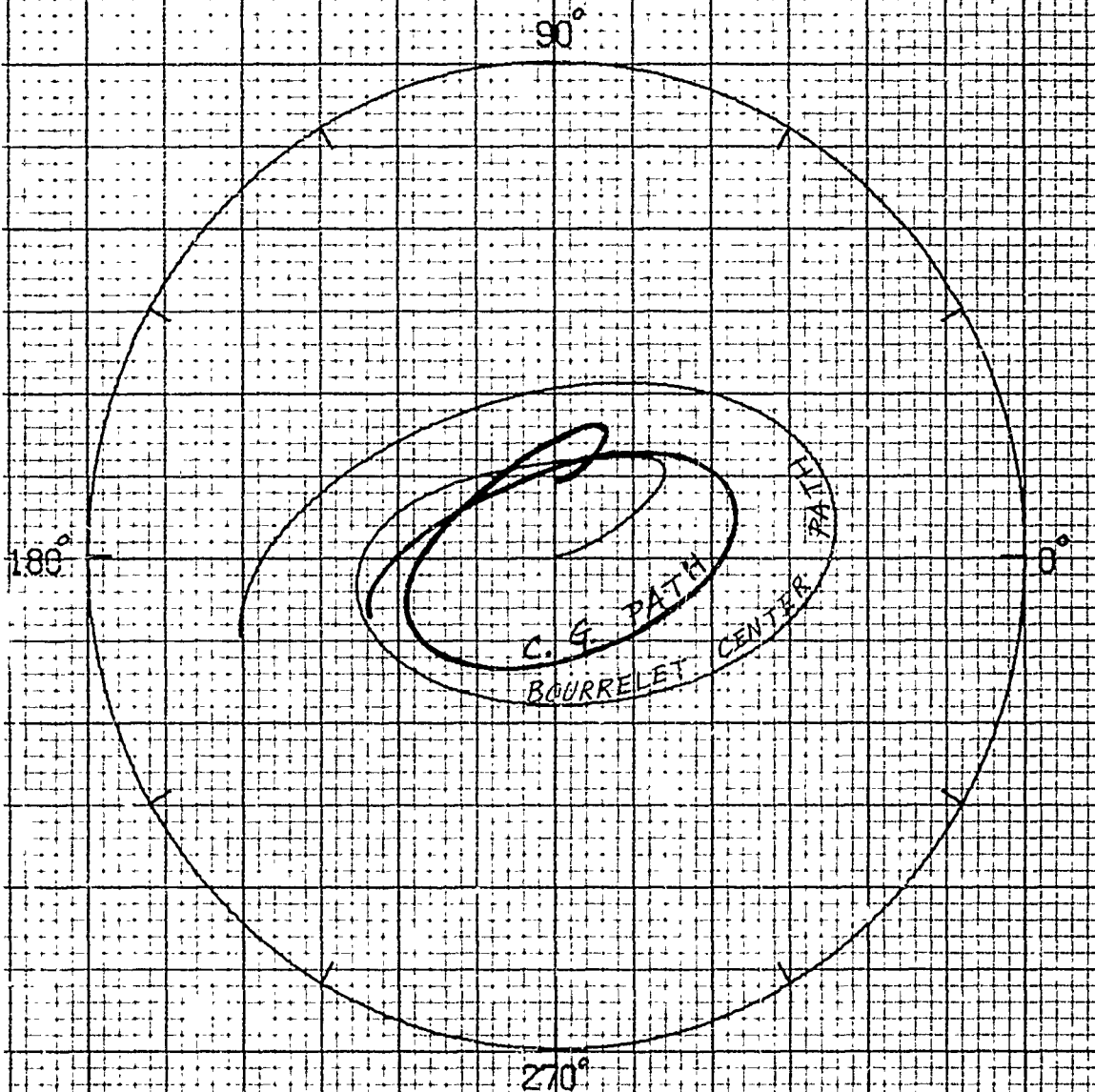


R = .0089 IN.

FIGURE 4b

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN=02, WALL THICKNESS .40 IN.

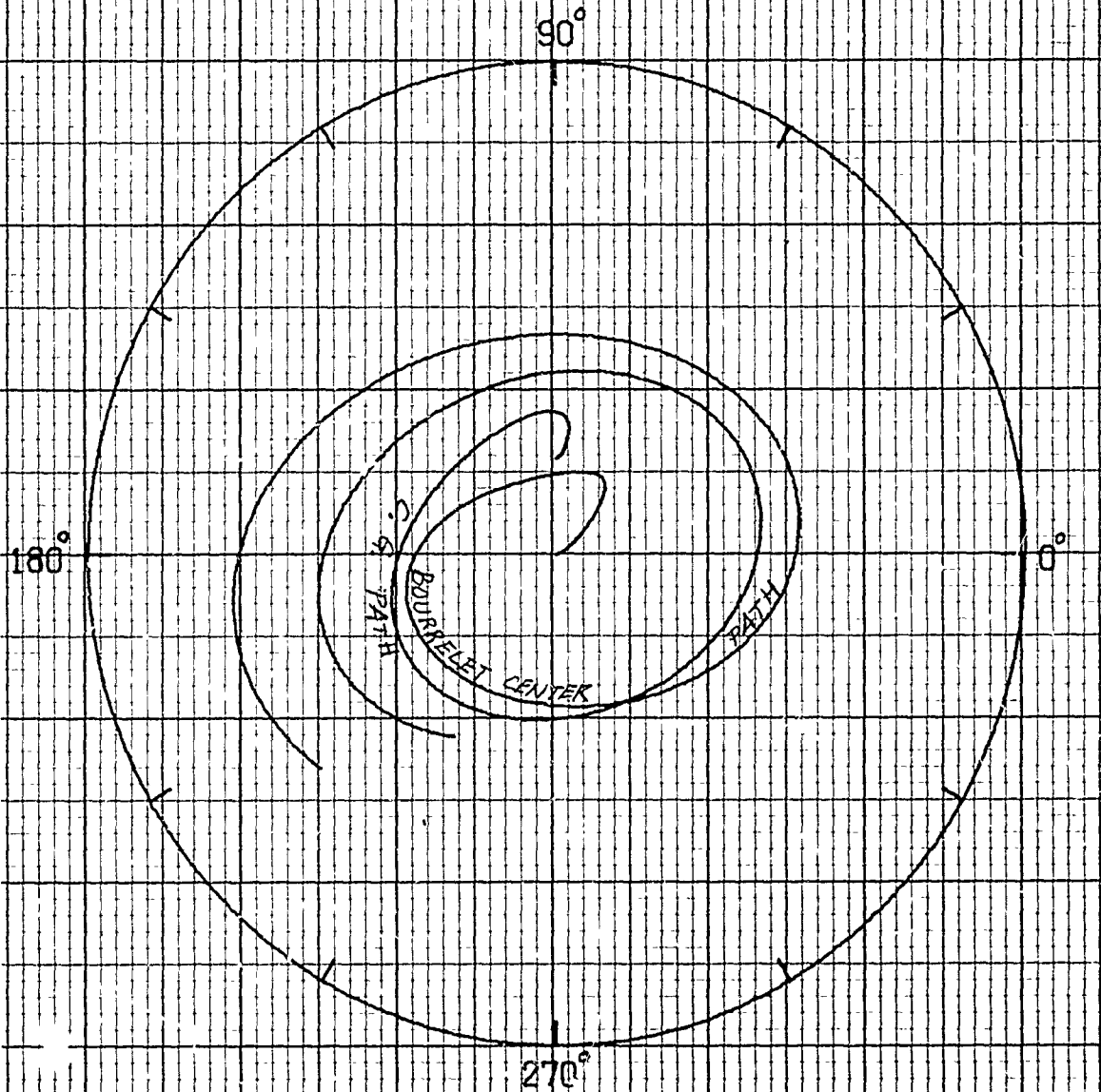


$R = .0200 \text{ IN.}$

FIGURE 4c

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI -0.0, THETA -.0001, PHI -0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

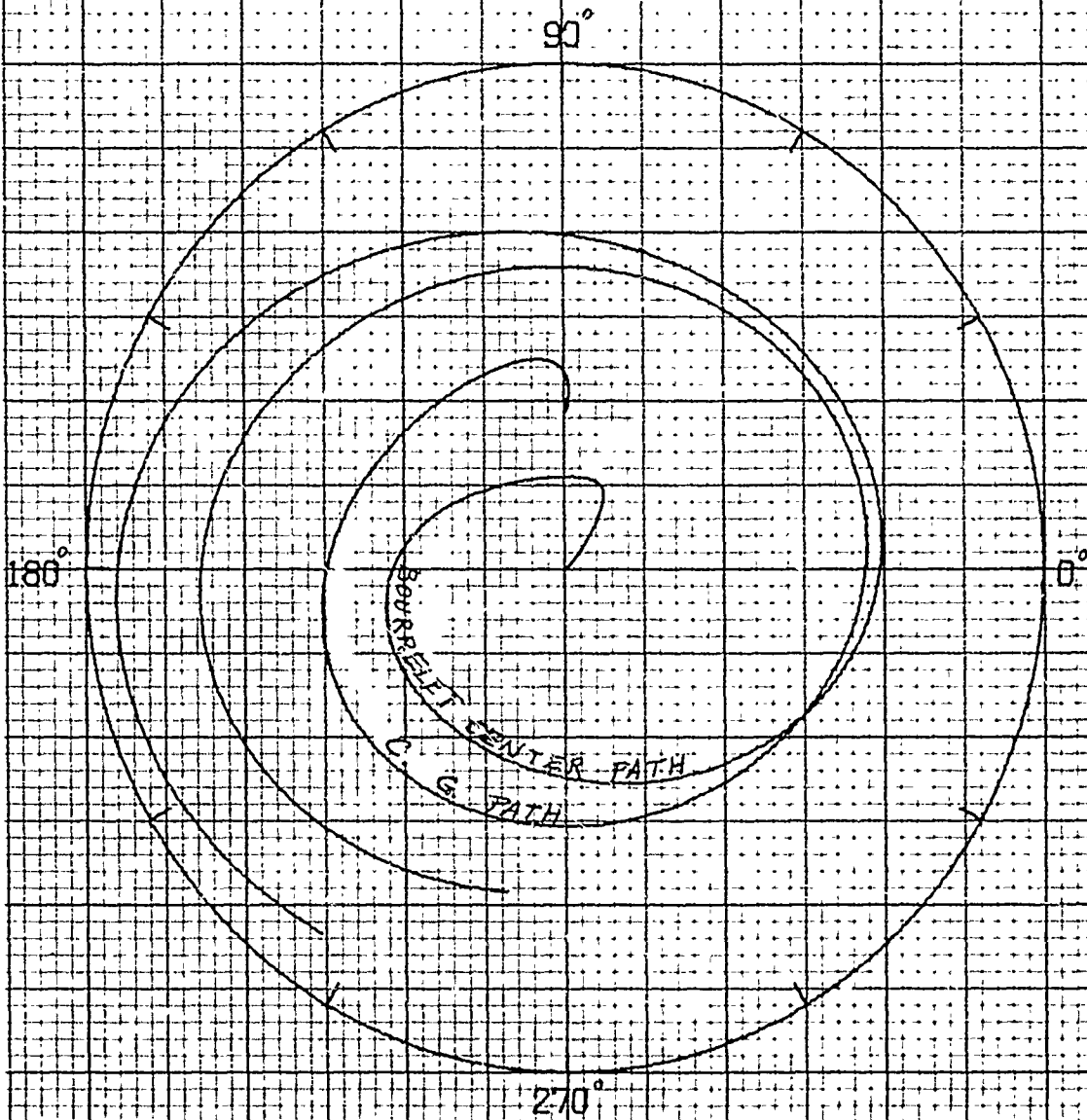


$R = .0400$ IN.

FIGURE 4d

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.



R = .0500 IN.

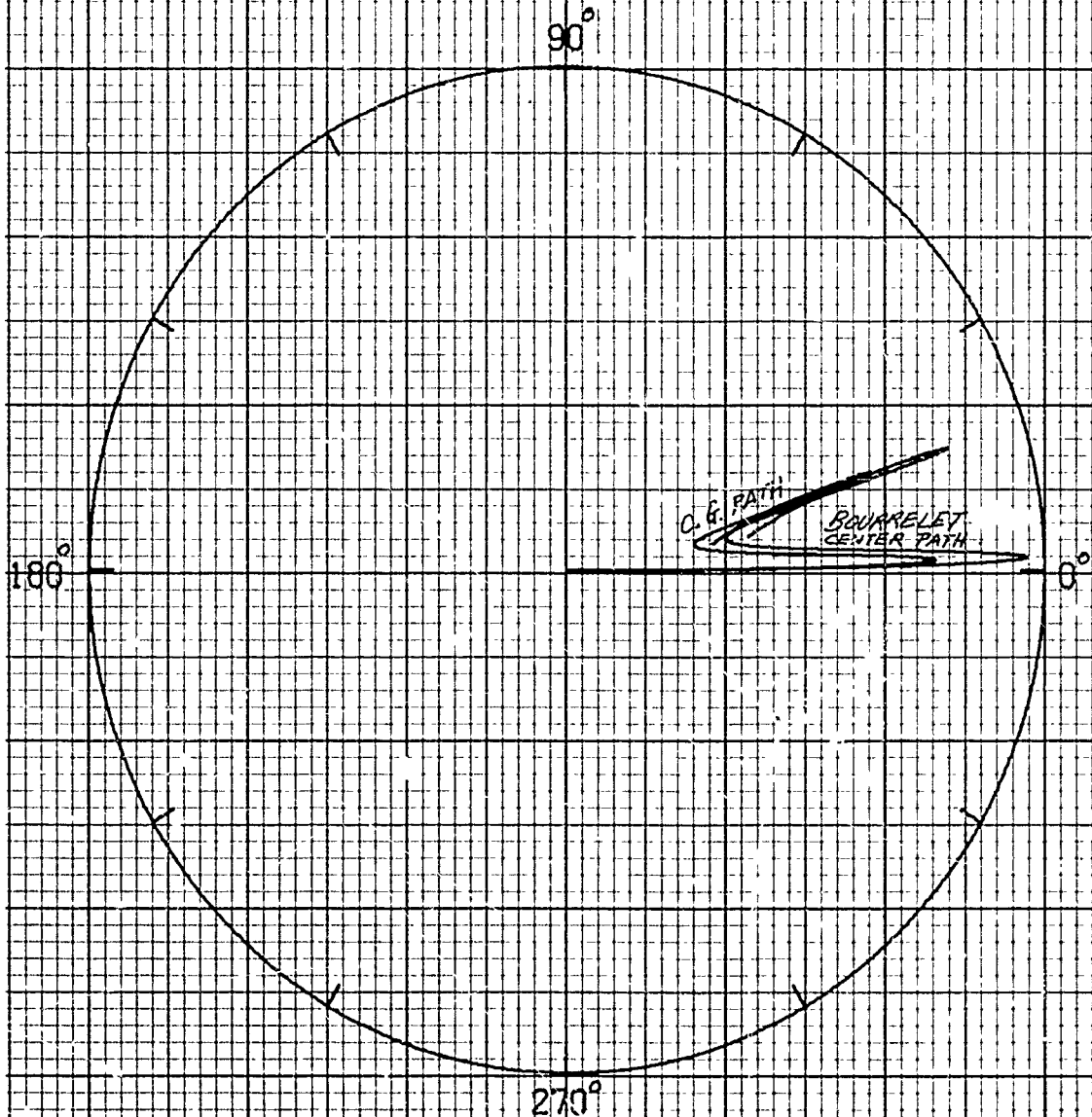
FIGURE 5a

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM20; TUBE (NO FRICTION)

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY: 0 IN-OZ. WALL THICKNESS .40 IN.

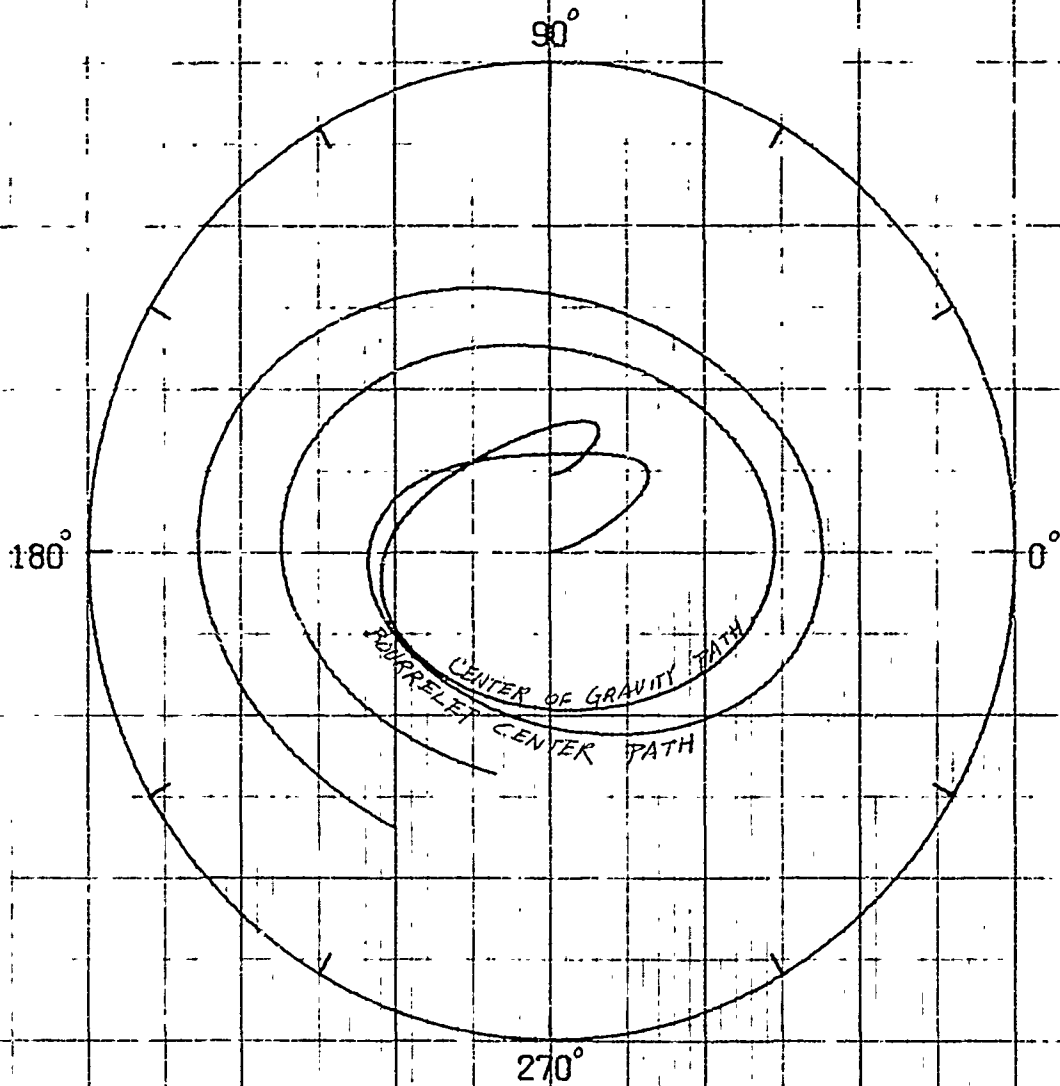


R = .0050 IN.

FIGURE 5b

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-0Z, WALL THICKNESS .40 IN.



R = .0200 IN.

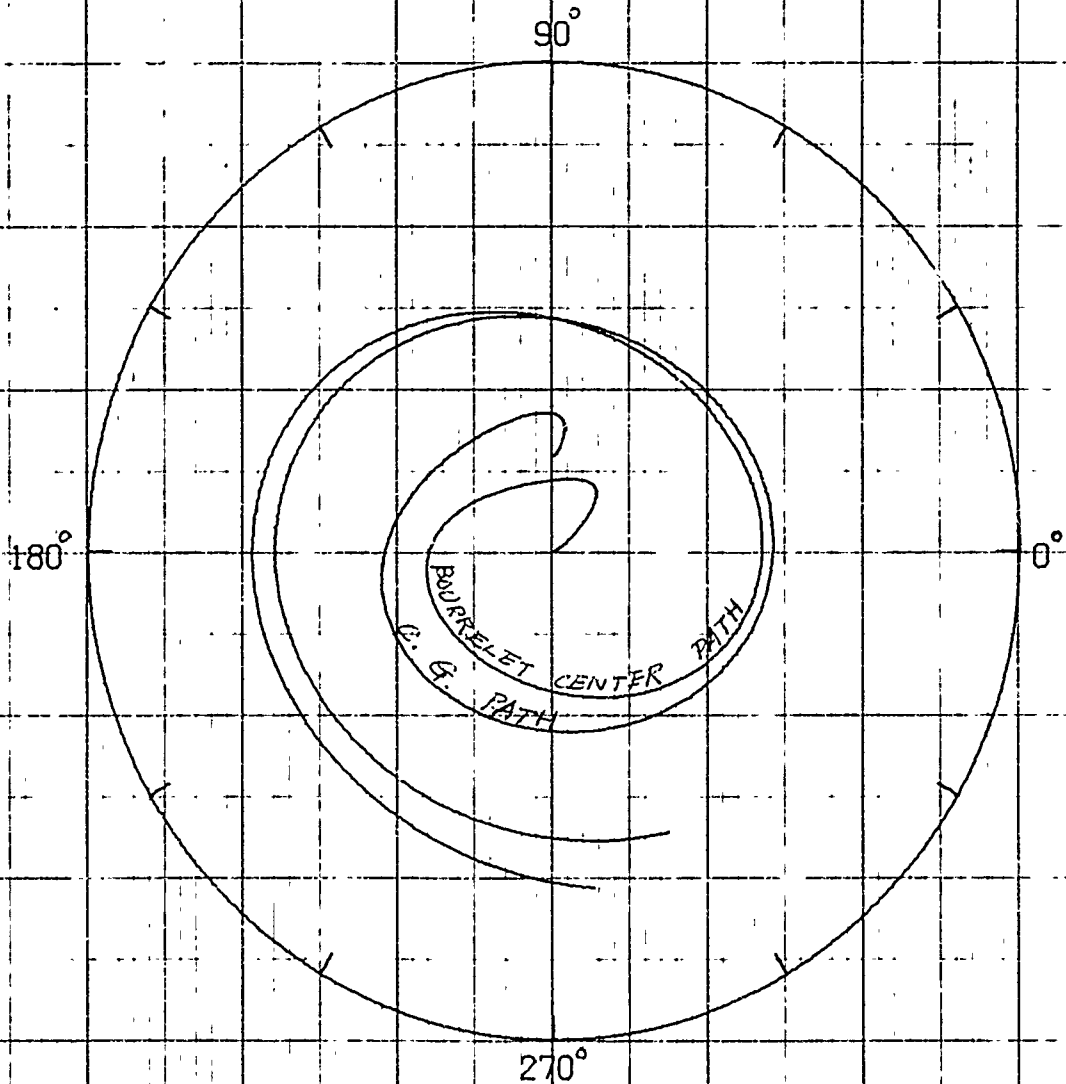
FIGURE 5c

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY 25 IN-OZ; WALL THICKNESS .40 IN.



R = .0400 IN.

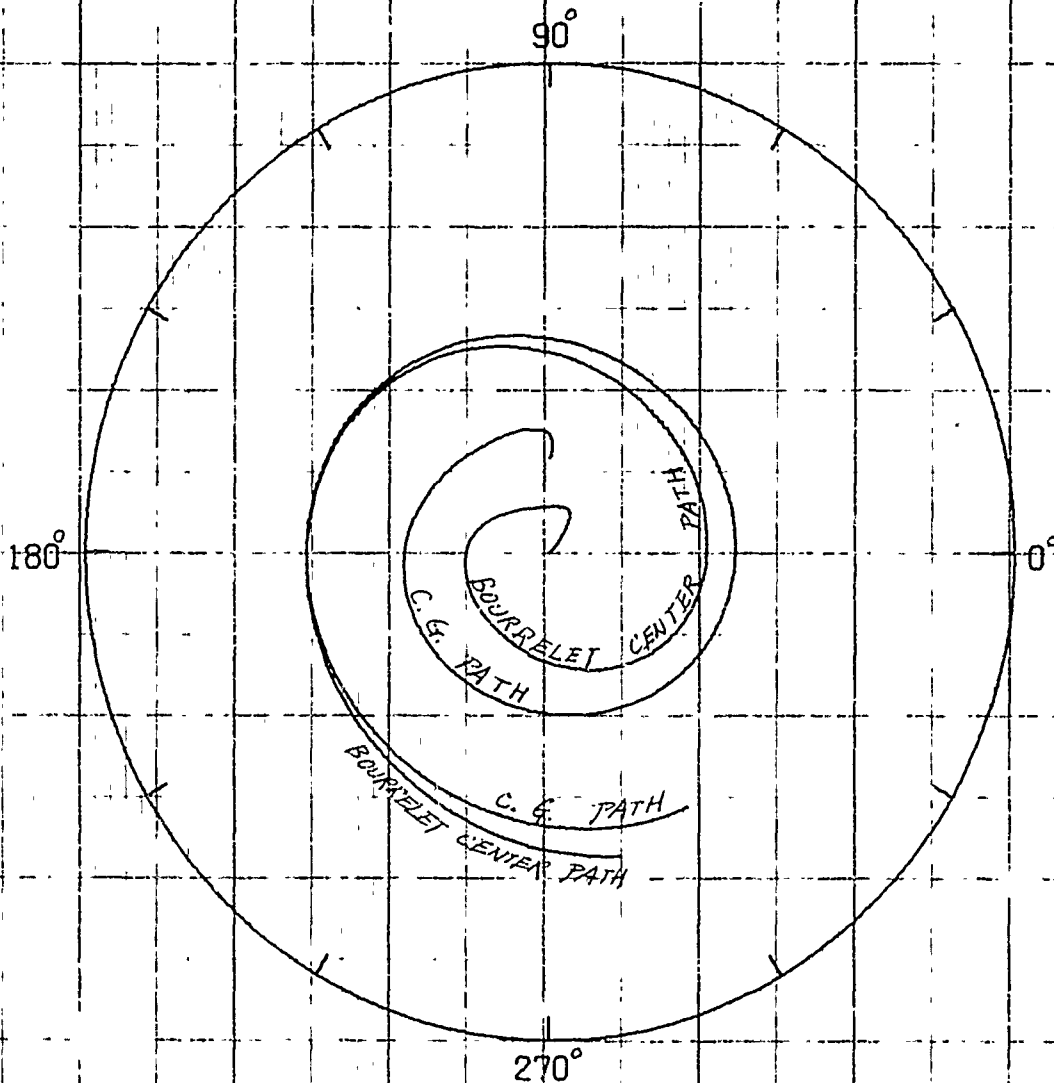
FIGURE 5d

O.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

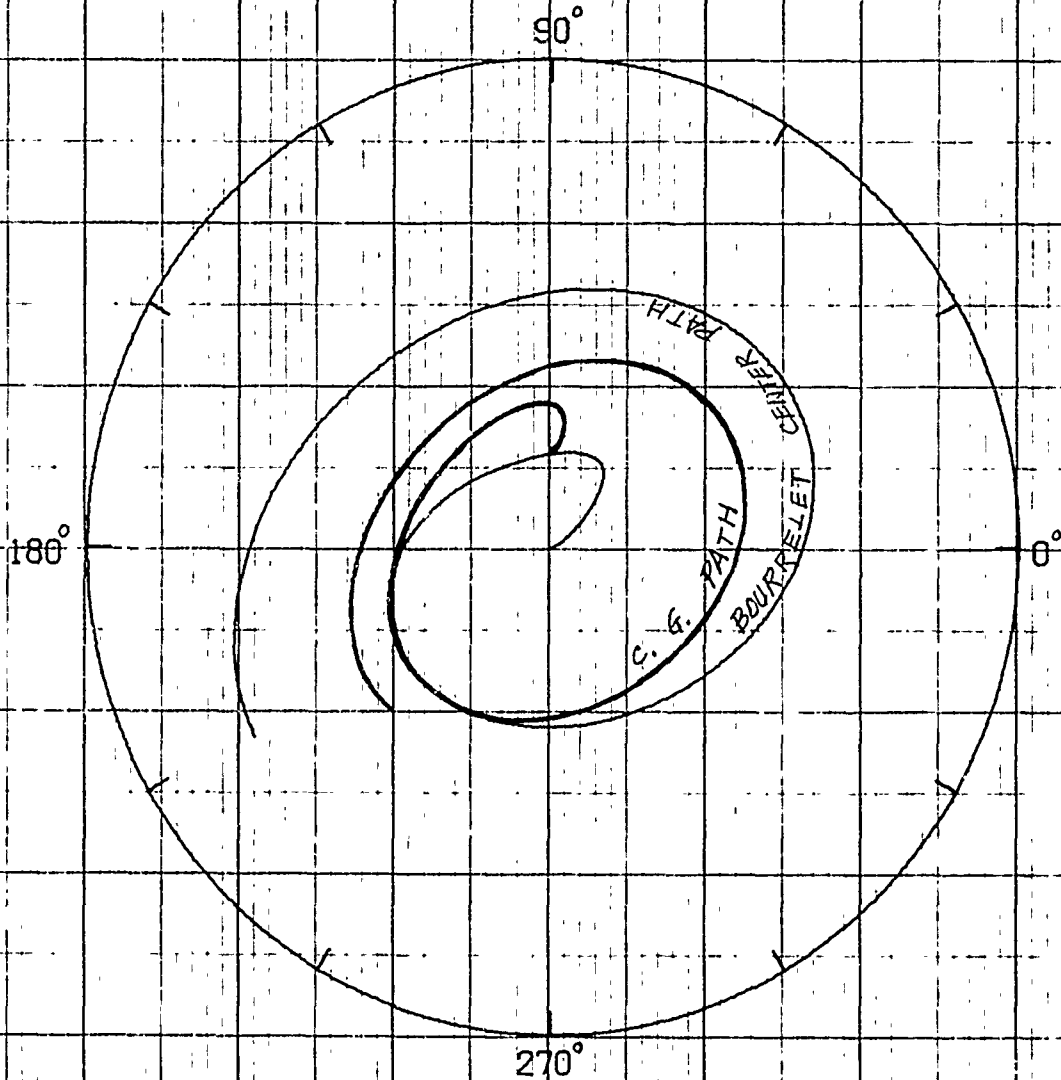


R = .0800 IN.

FIGURE 6a

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .38 IN.

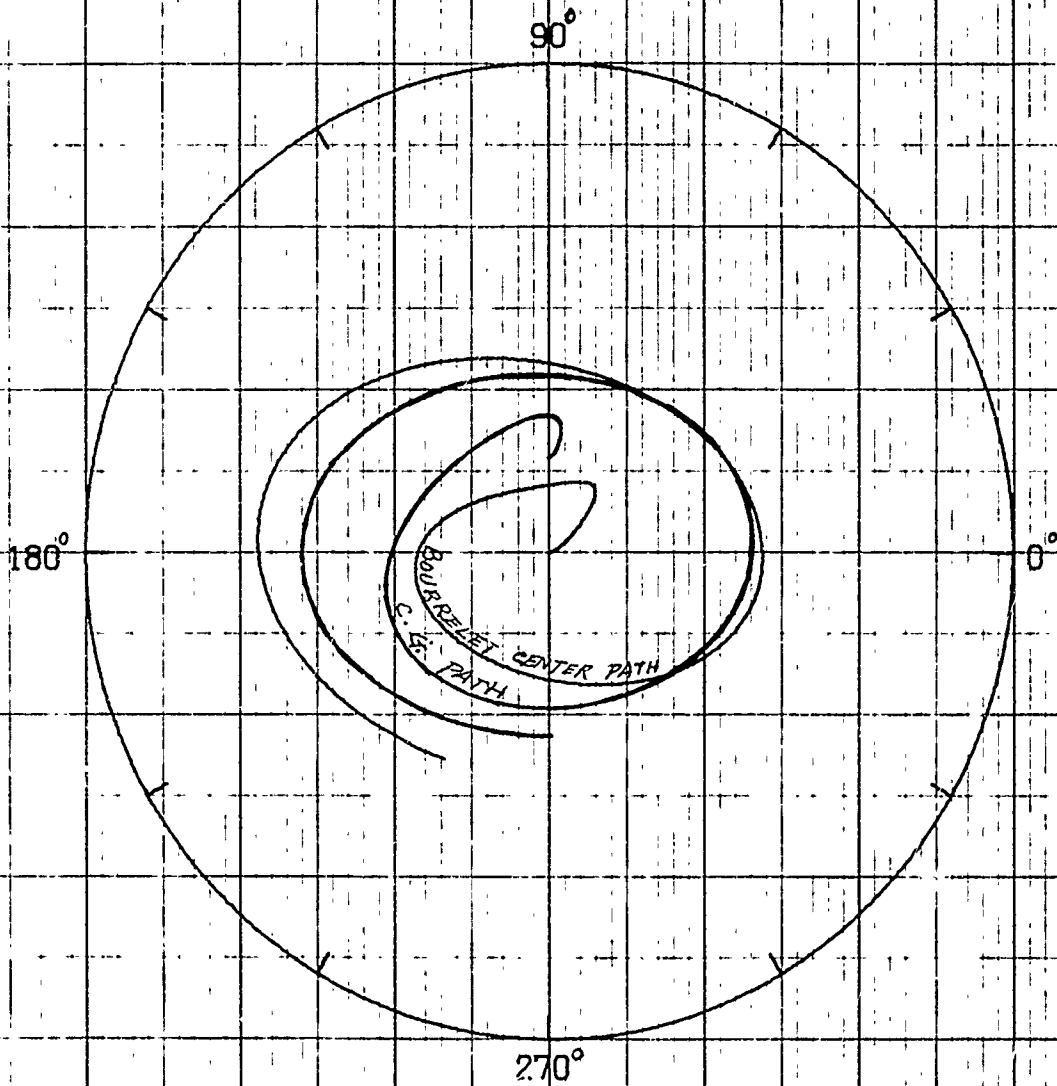


$R = .0400$ IN.

FIGURE 6b

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .42 IN.



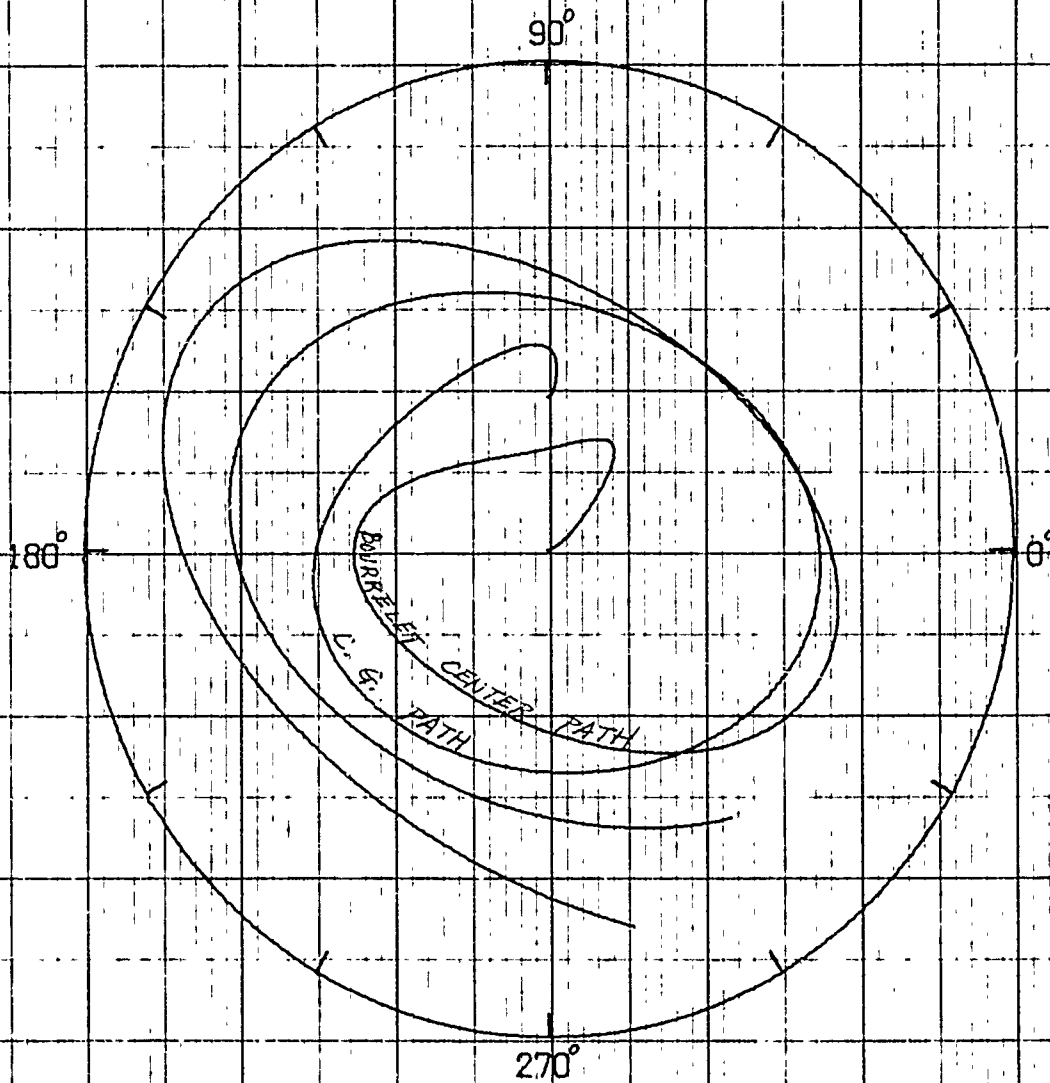
R = .0400 IN.

FIGURE 7a

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL $\Psi = 0.0$, $\Theta = .0001$, $\Phi = 0.0$ DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.

C.G. TO DRIVING BAND DISTANCE REDUCED TO $3/4$ ORIGINAL VALUE



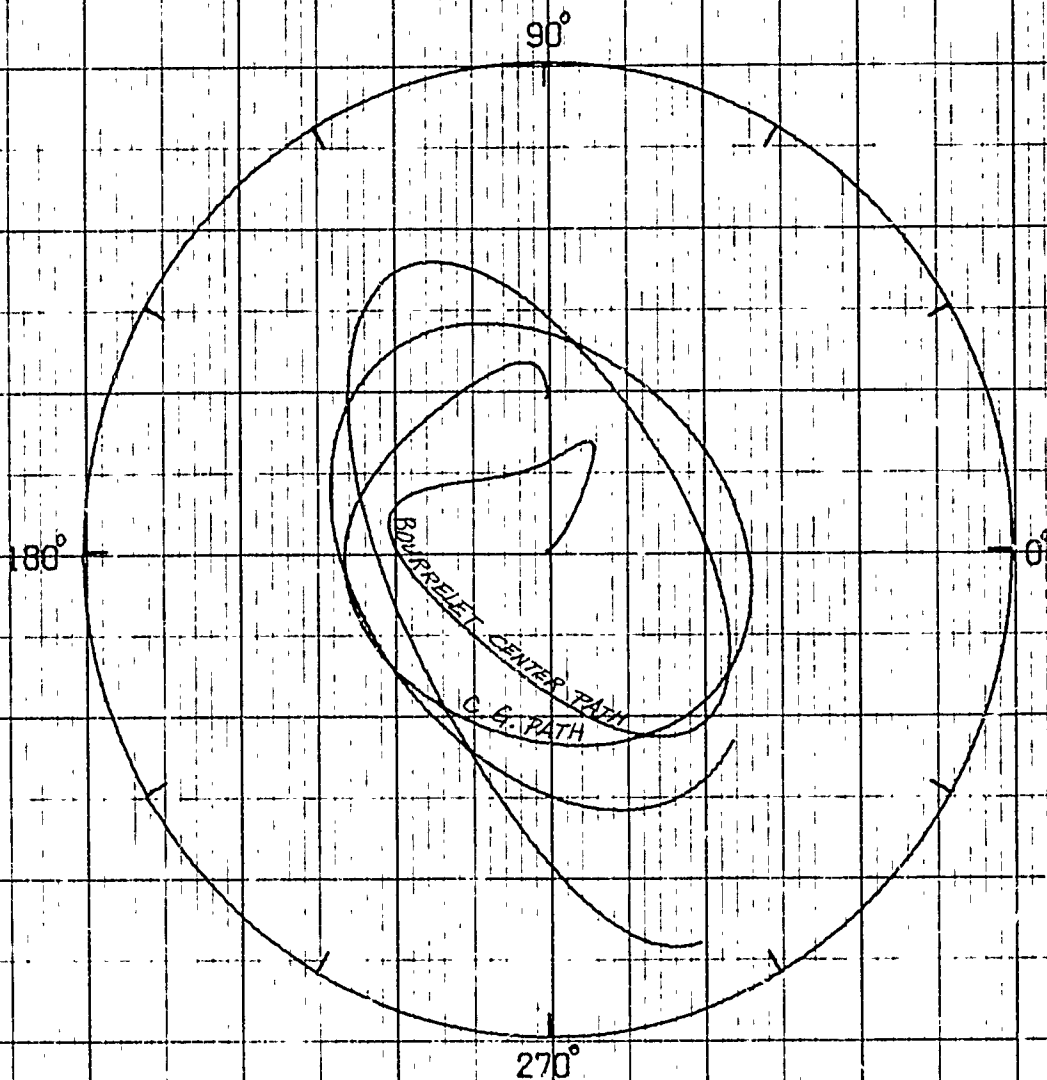
$R = .0250$ IN.

FIGURE 7b

C.G. AND BOURRELET CENTER

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.

C.G. TO DRIVING BAND DISTANCE REDUCED TO $\frac{1}{2}$ ORIGINAL VALUE



$R = .0250$ IN.

FIGURE 8a

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.

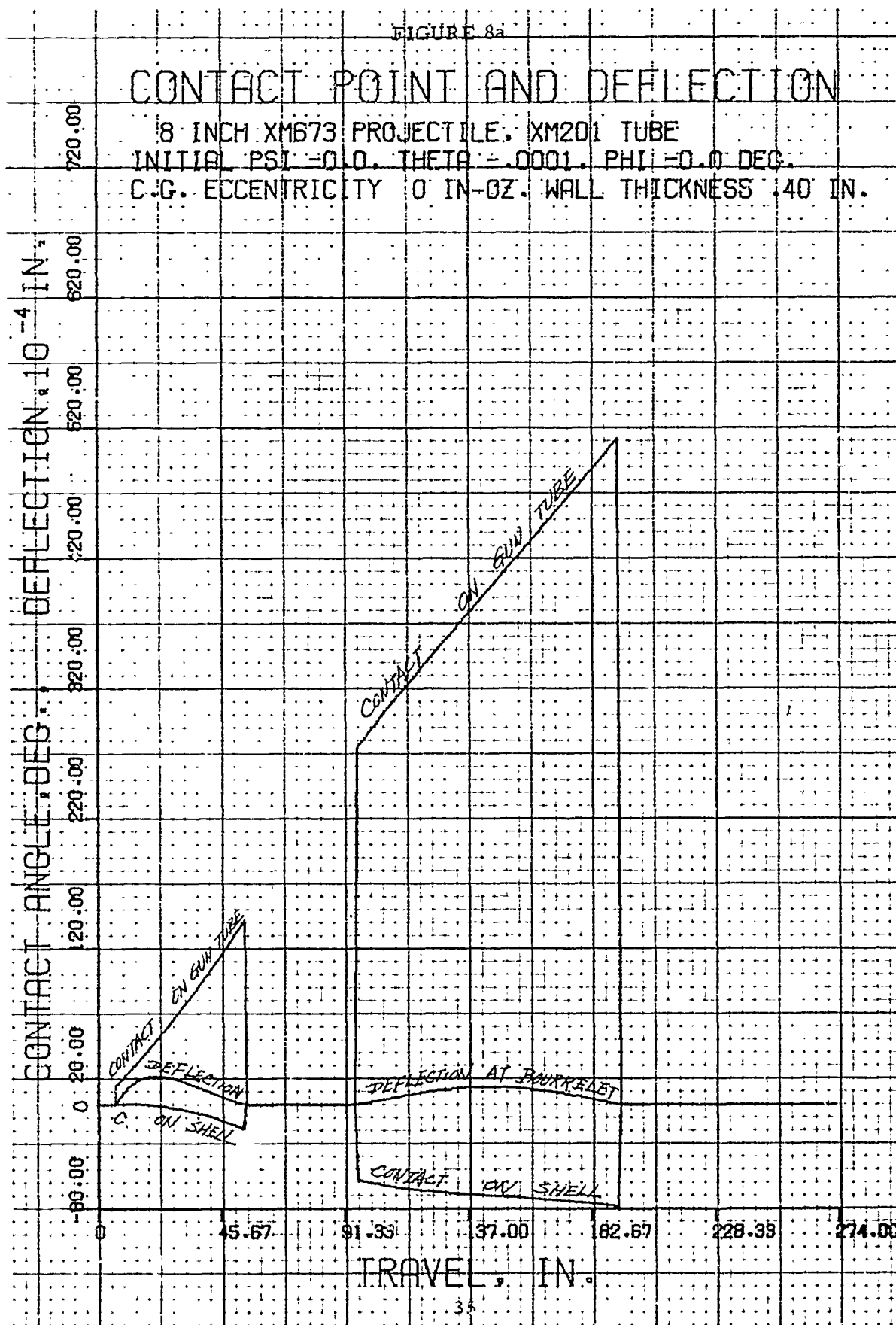


FIGURE 8b

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY 10 IN-0Z, WALL THICKNESS .40 IN.

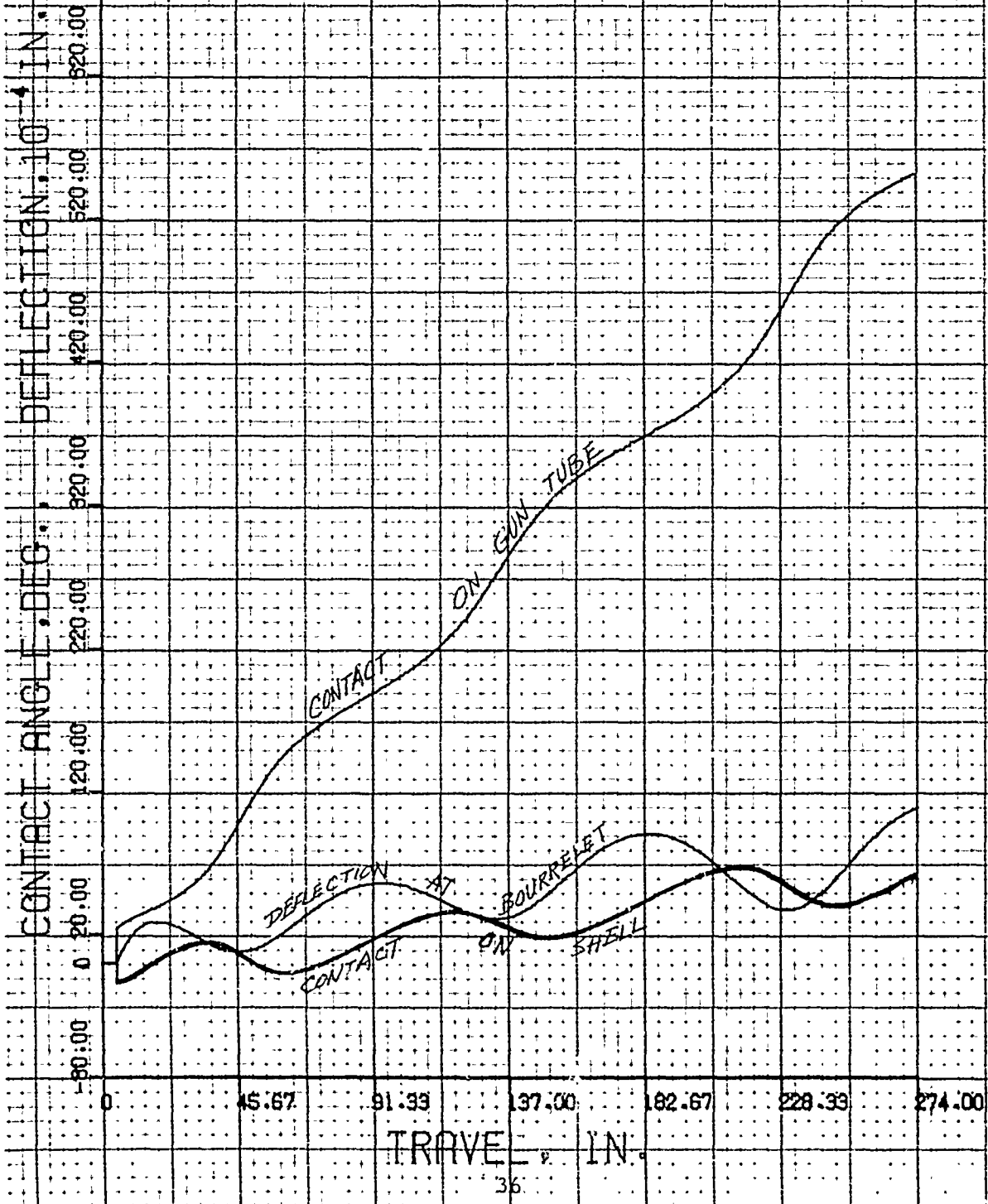


FIGURE 8c

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE; XM201 TUBE
INITIAL PSI -0.0, THETA - .0001, PHI -0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.

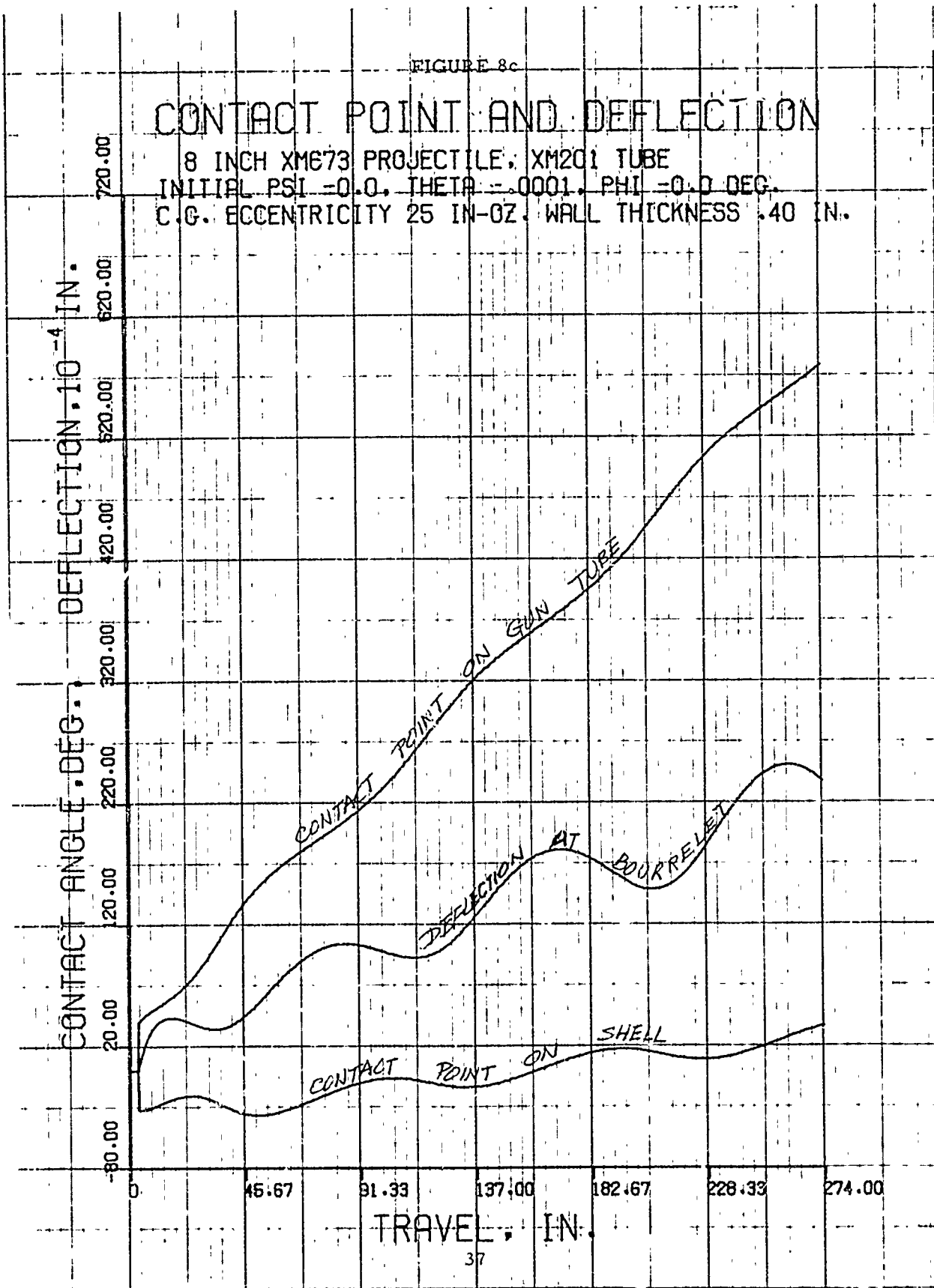


FIGURE 8d

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-0Z, WALL THICKNESS .40 IN.

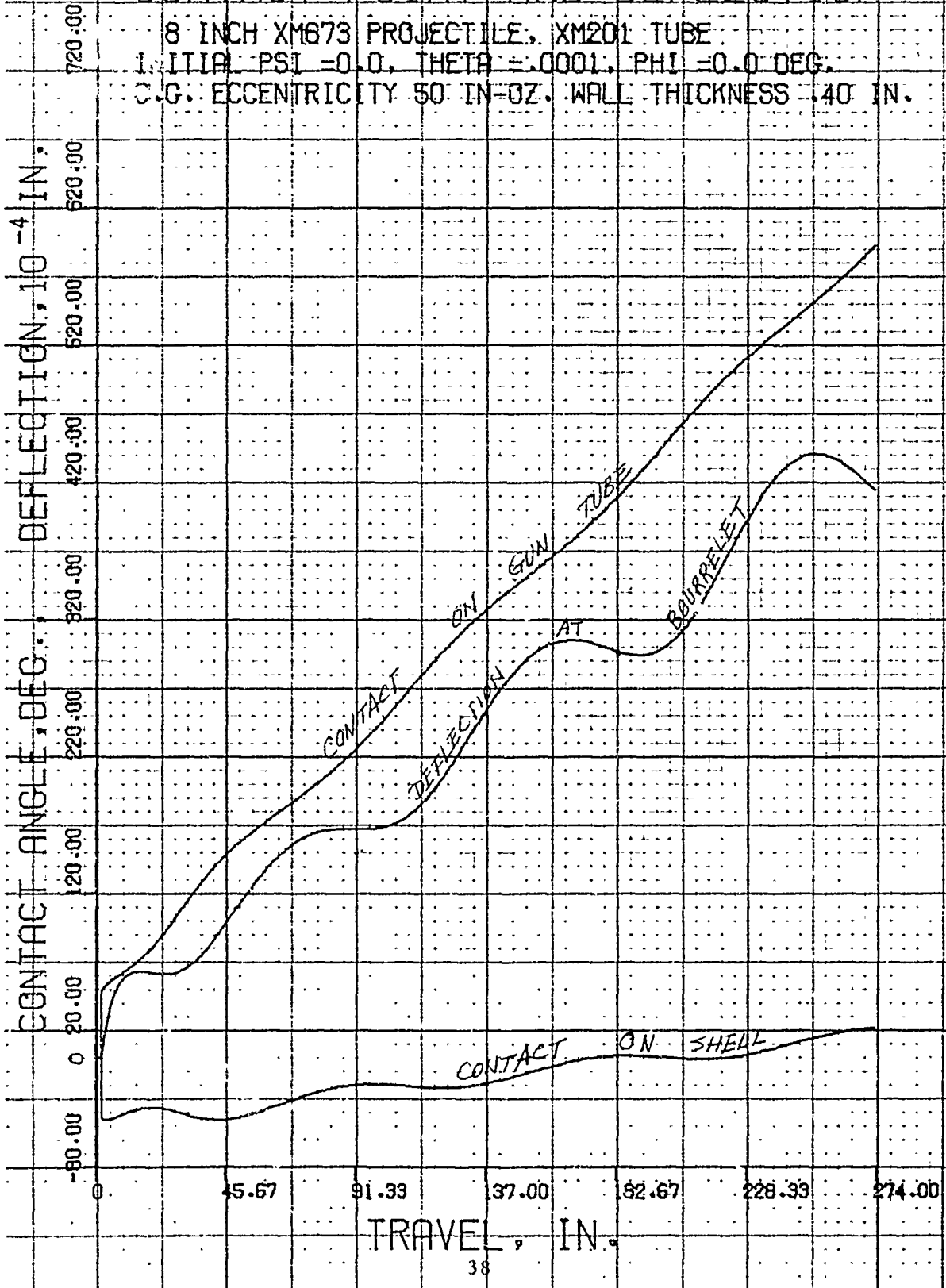
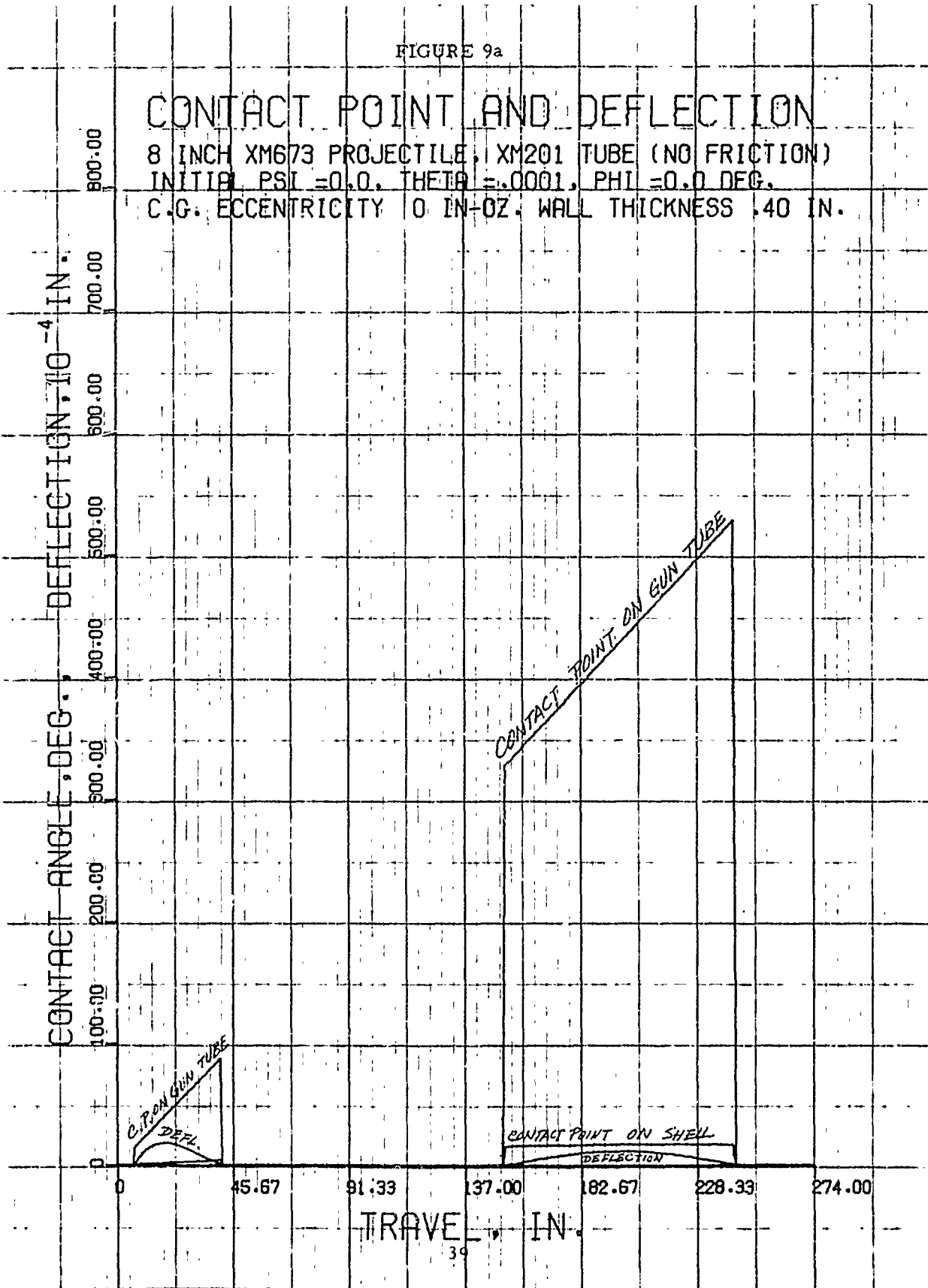


FIGURE 9a

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.



TRAVE, IN.
30

FIGURE 9b

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.

CONTACT ANGLE, DEG.
DEFLECTION, 10^{-4} IN.

720.00
620.00
520.00
420.00
320.00
220.00
120.00
20.00
-80.00

0 45.67 91.33 137.00 182.67 228.33 274.00

TRAVEL, IN.

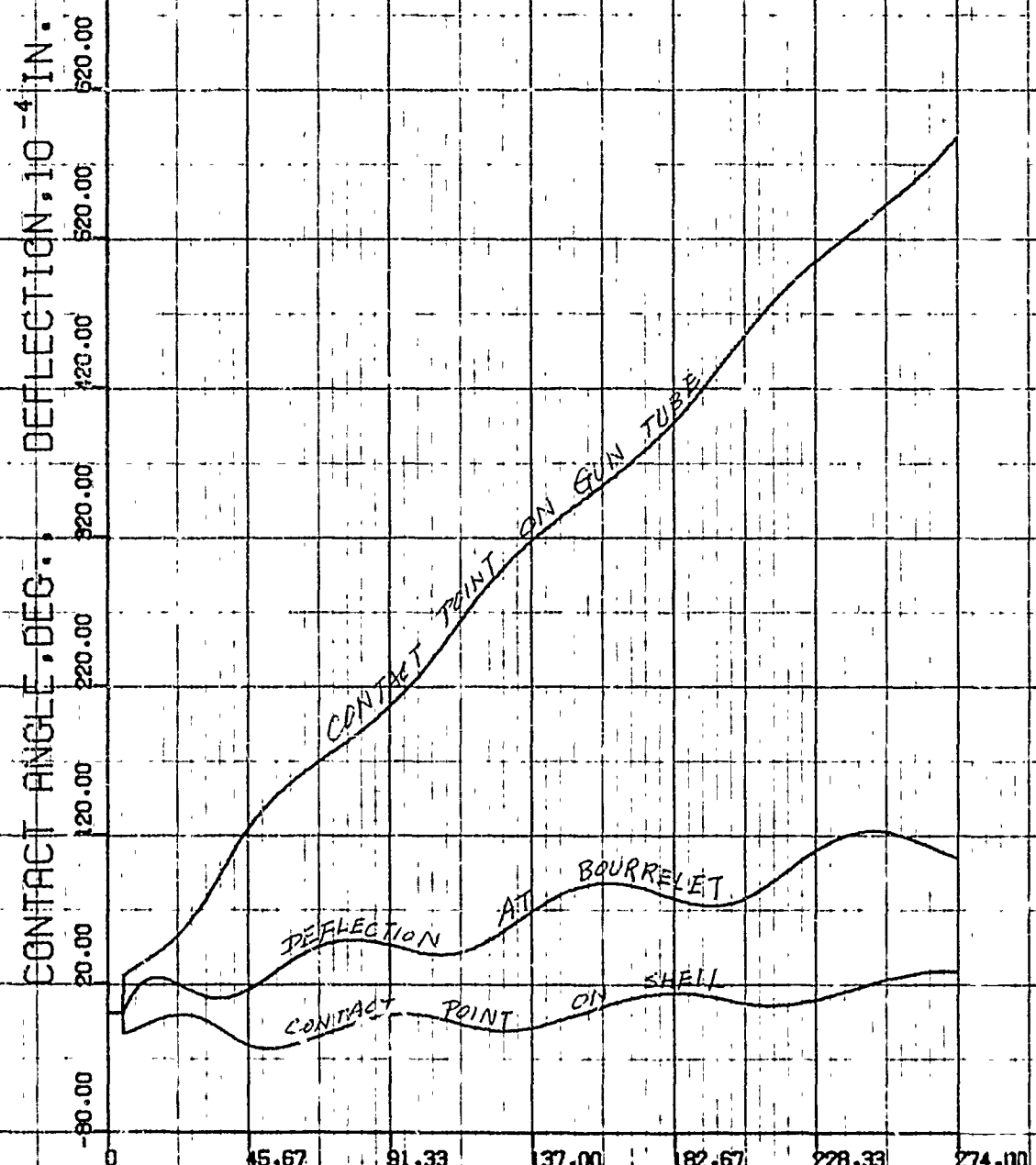


FIGURE 9c

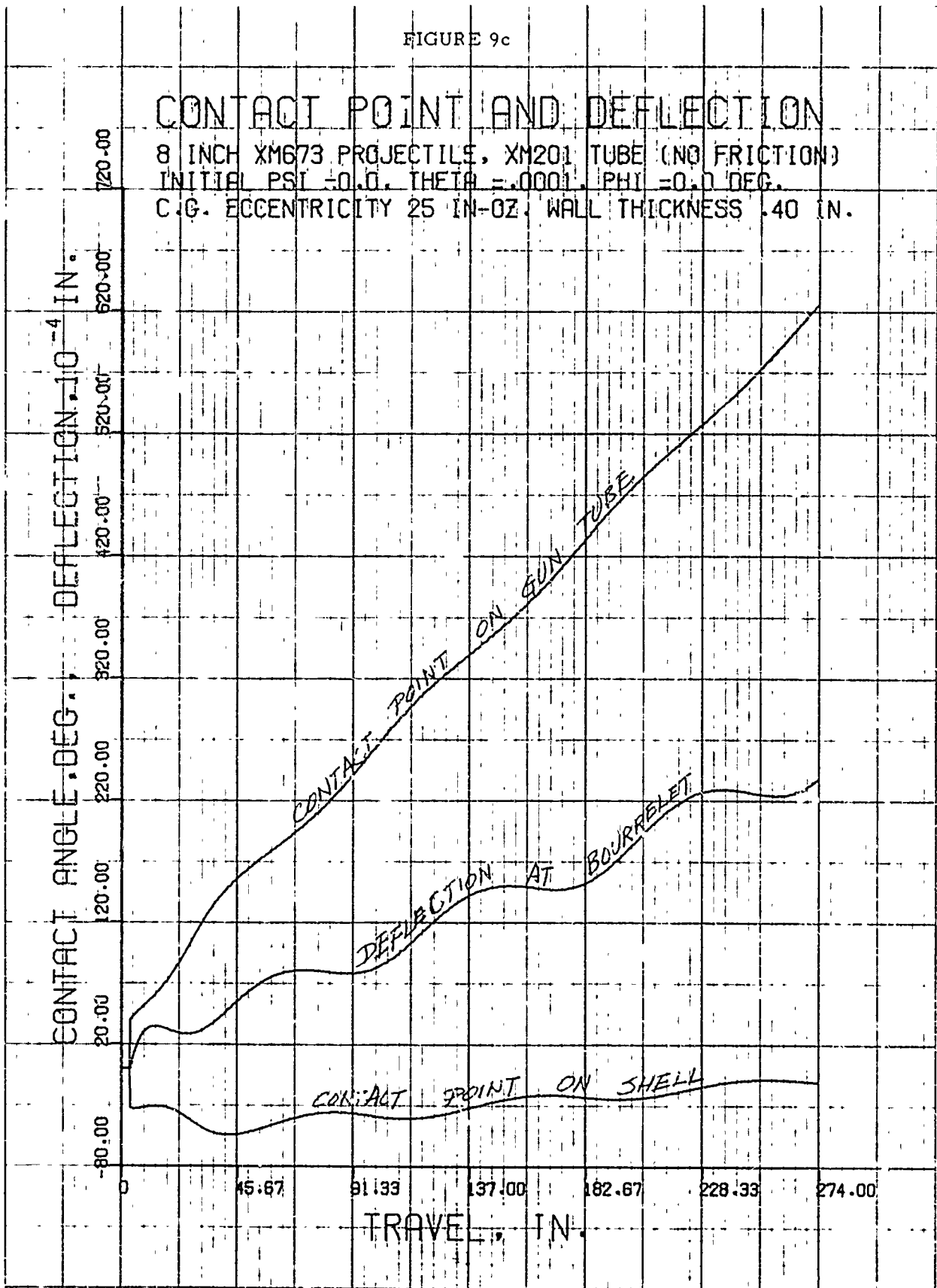


FIGURE 9d

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)

INITIAL PSI -0.0, THETA = .0001, PHI -0.0 DEG.

C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

CONTACT ANGLE, DEG. DEFLECTION, 10^{-4} IN.

720.00
620.00
520.00
420.00
320.00
220.00
120.00
20.00
-80.00

CONTACT POINT ON GUN TUBE
DEFLECTION AT BOURRELET

CONTACT POINT ON SHELL

0 45.67 91.33 137.00 182.67 228.33 274.00

TRAVEL, IN.

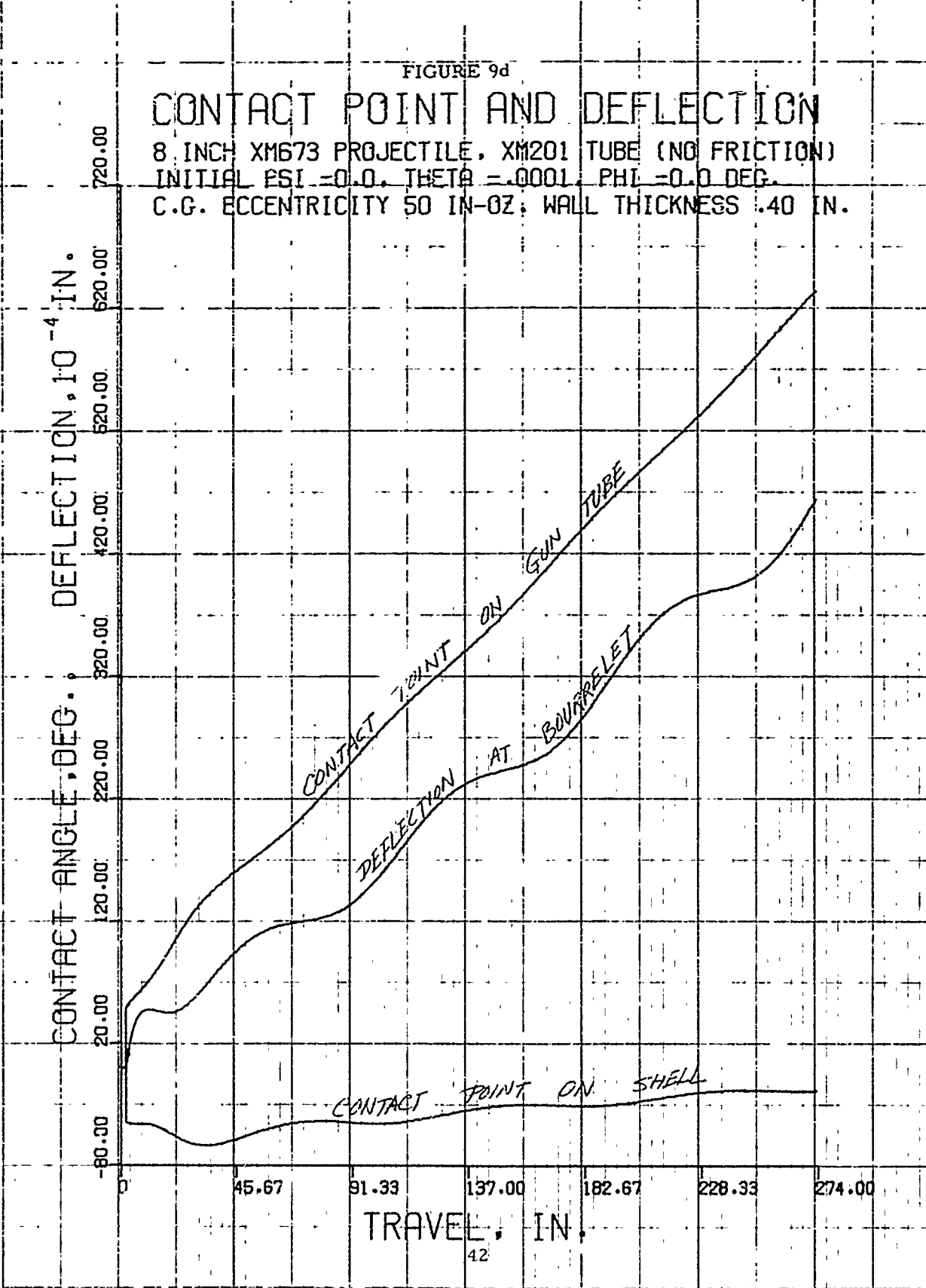


FIGURE 10a

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .38 IN.

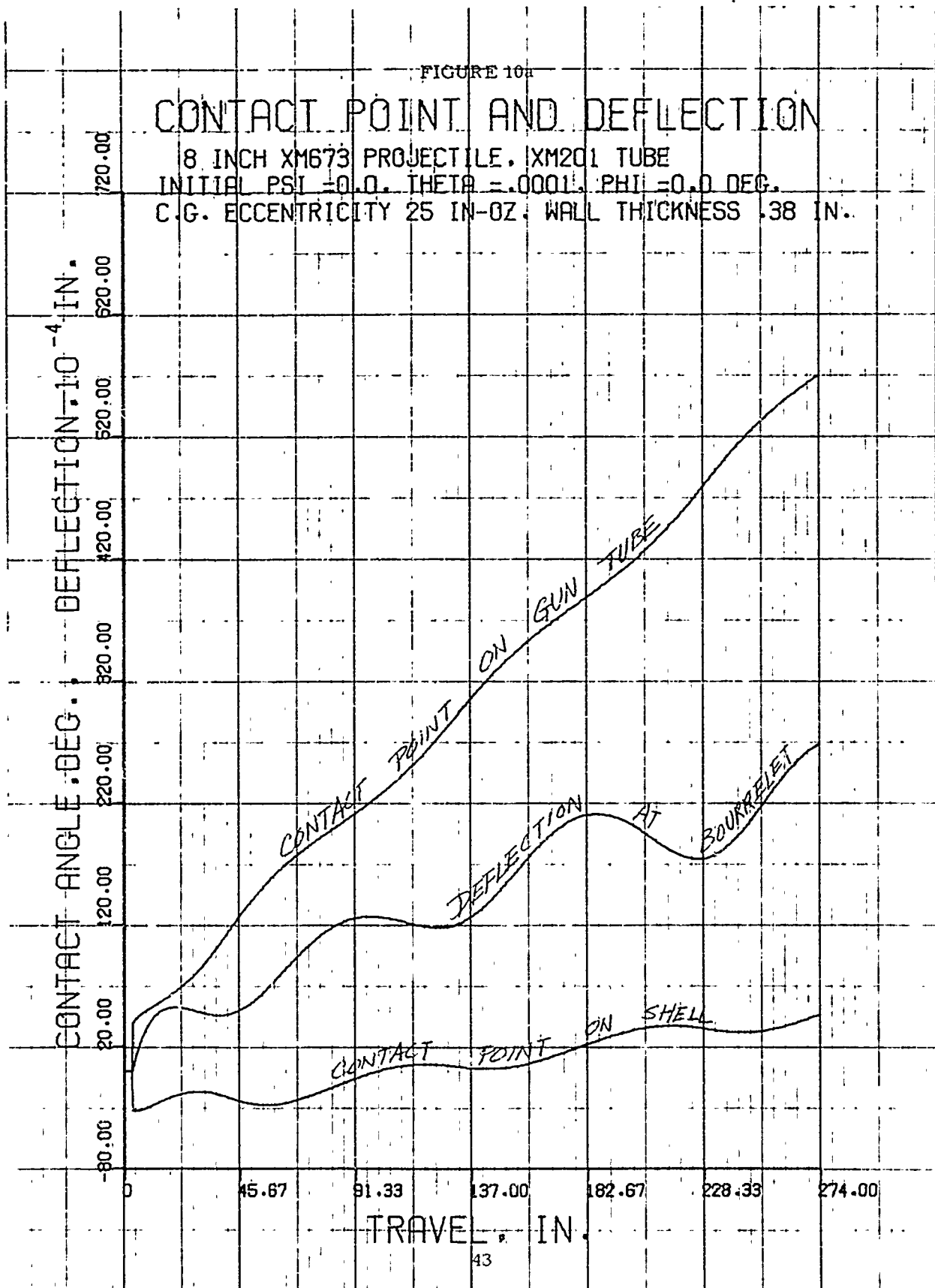


FIGURE 10b

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .42 IN.

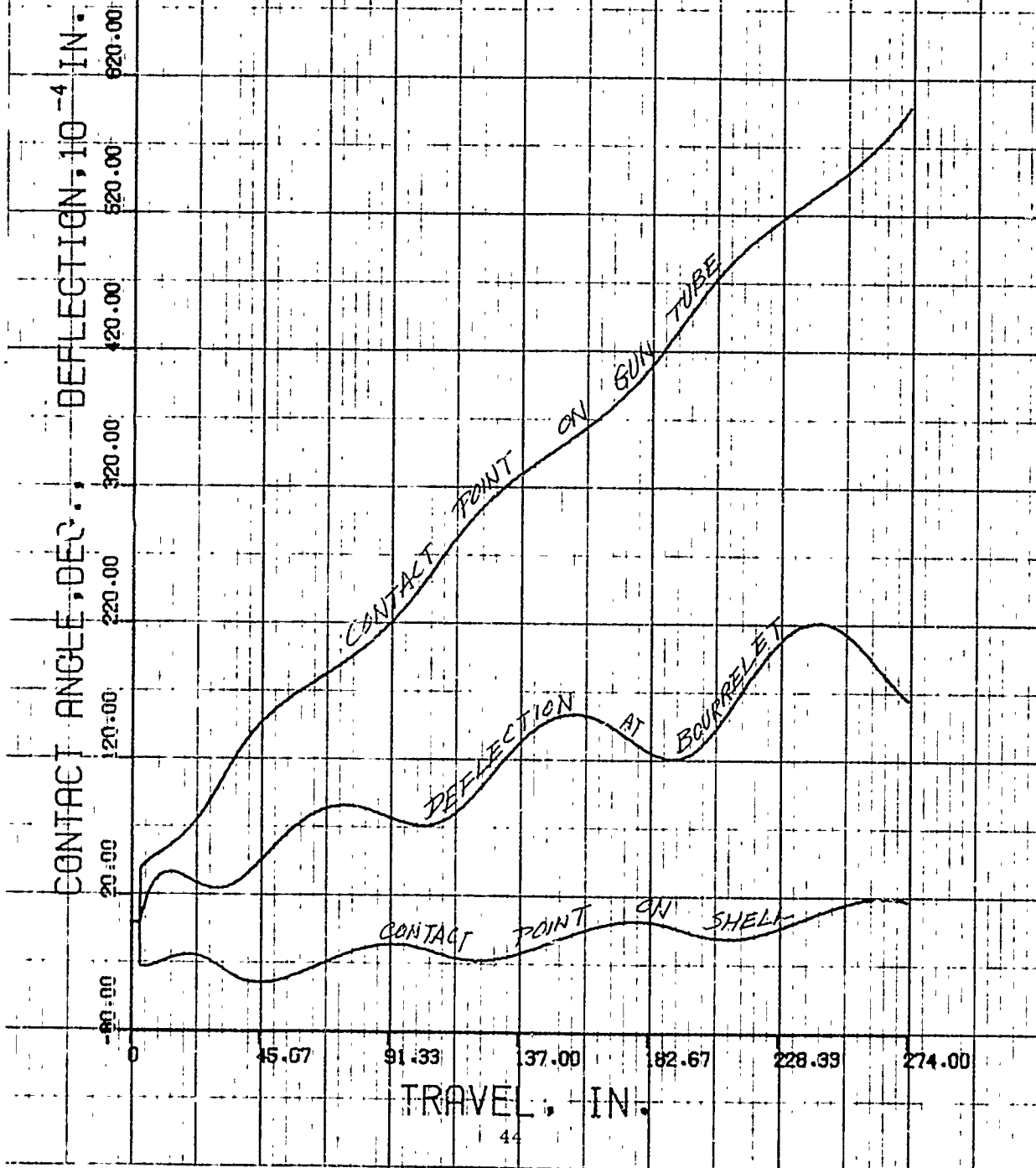


FIGURE 11a

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = 0.001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ., WALL THICKNESS .40 IN.
C.G. TO DRIVING BAND DISTANCE REDUCED TO 3/4 ORIGINAL VALUE

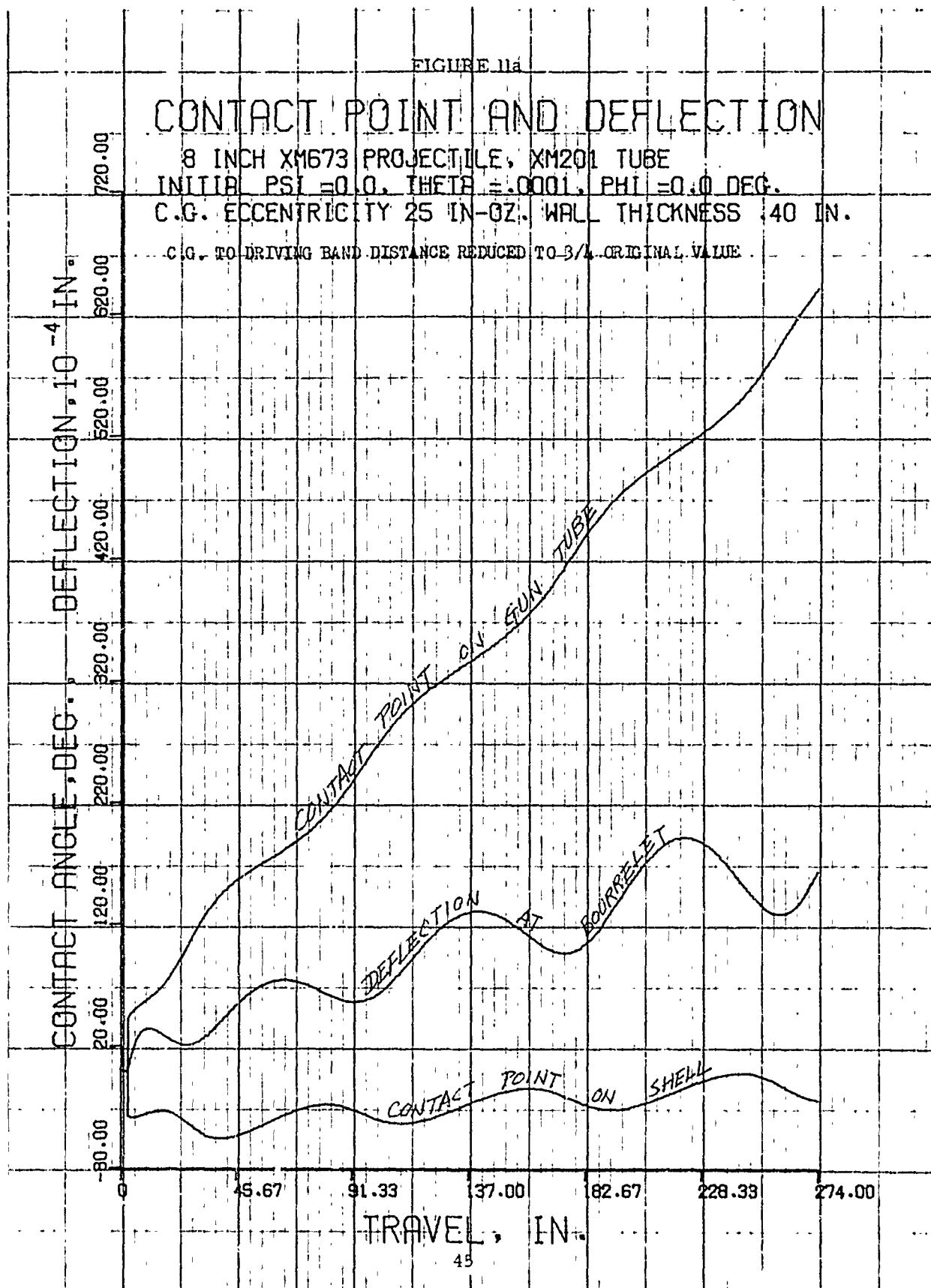


FIGURE 11b

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.

C.G. TO DRIVING BAND DISTANCE REDUCED TO $\frac{1}{2}$ ORIGINAL VALUE

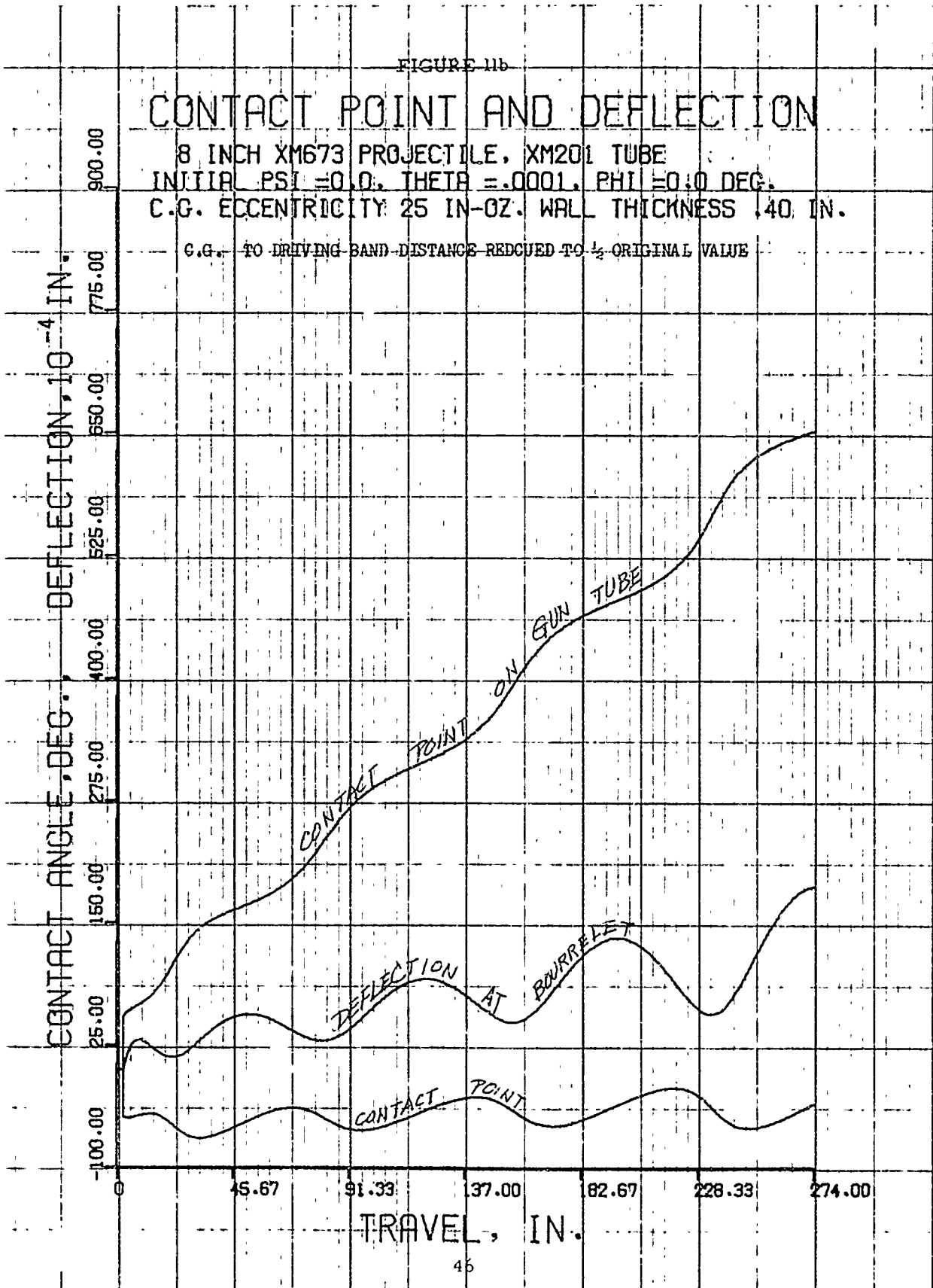


FIGURE 12a

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ. WAL THICKNESS .40 IN.

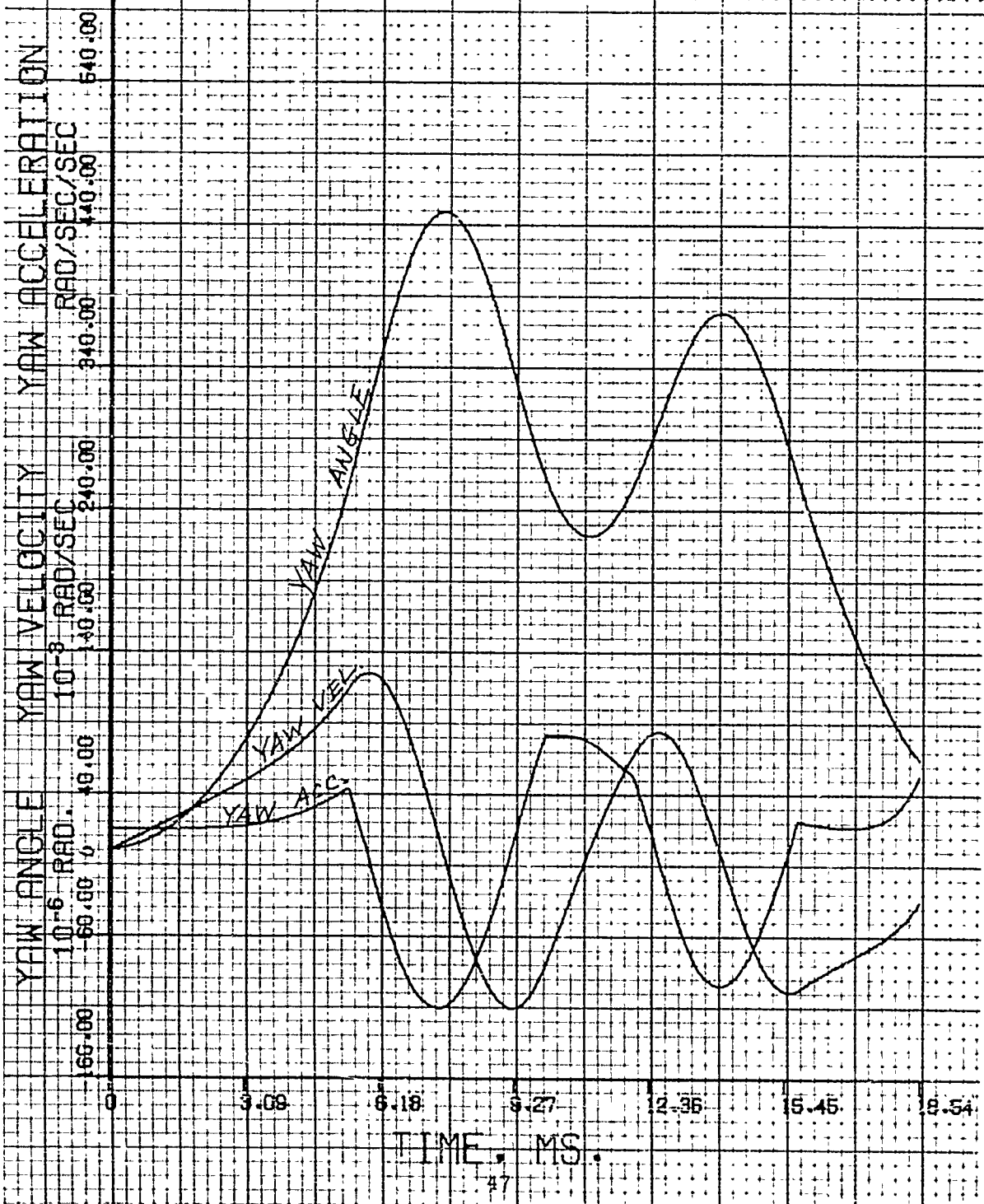


FIGURE 12b

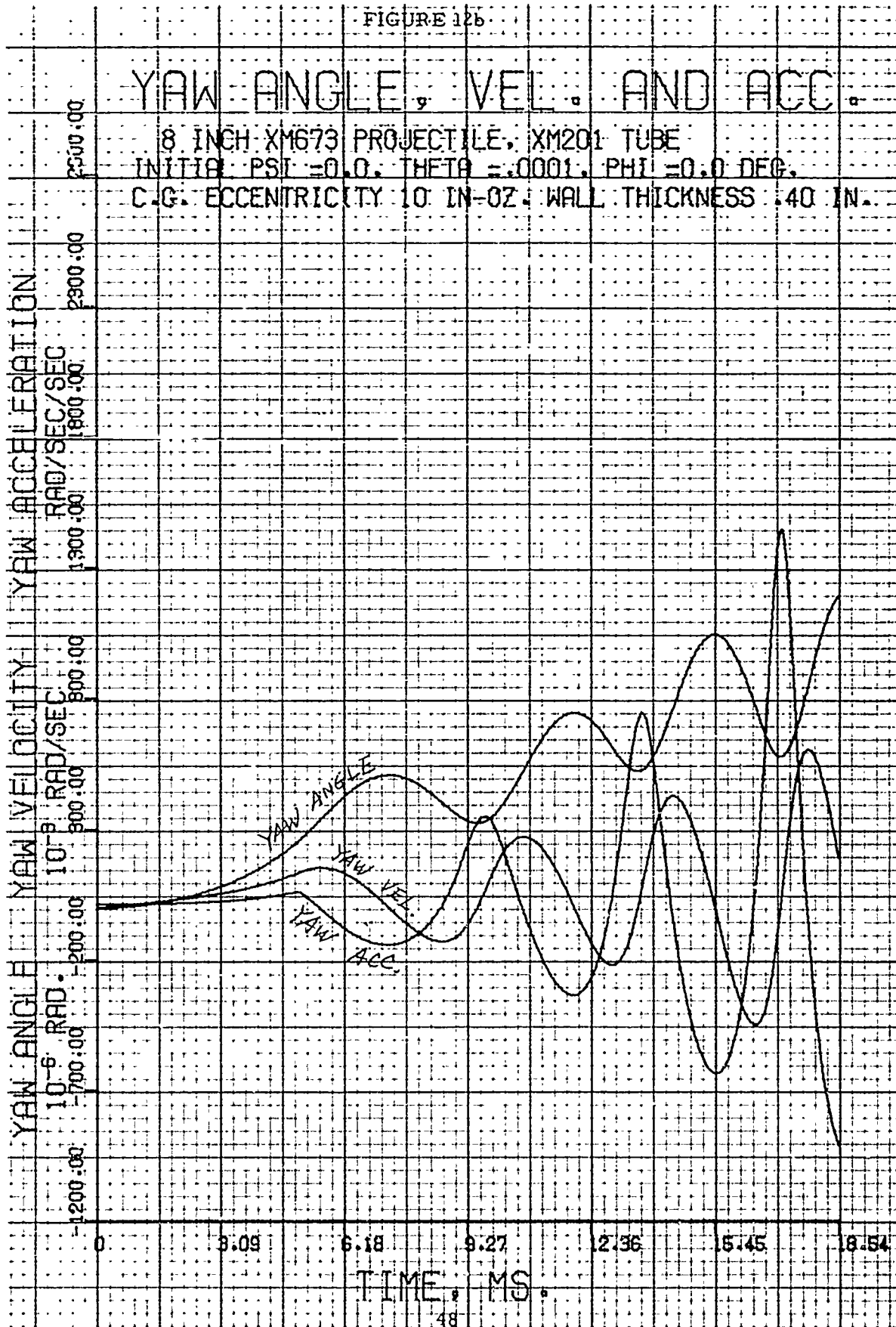


FIGURE 12c

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

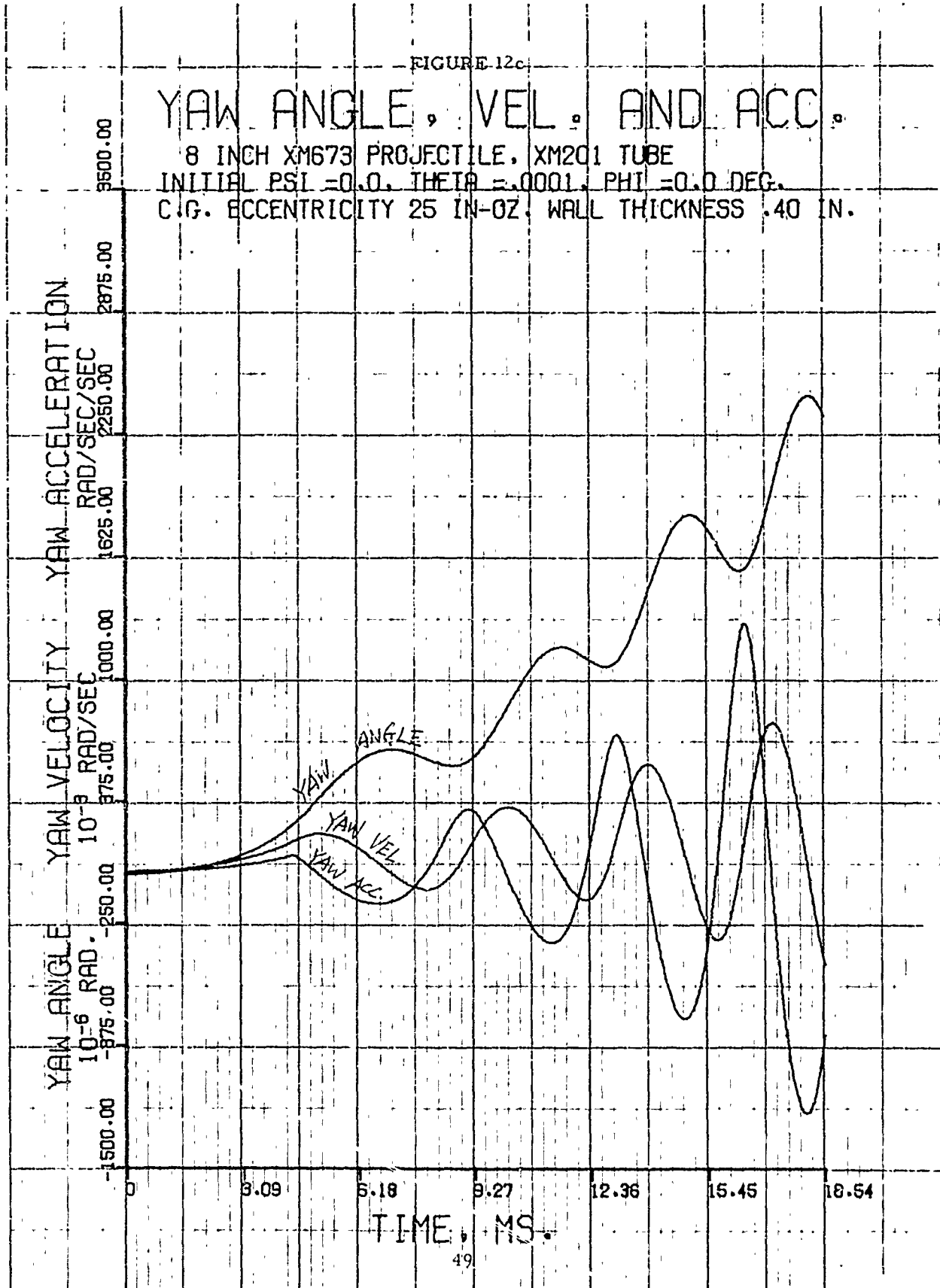


FIGURE 12d

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

YAW ACCELERATION

1400.00
RAD/SEC/SEC

YAW VELOCITY

10⁻³ RAD/SEC

YAW ANGLE

10⁻⁶ RAD

0 3.09 6.18 9.27 12.36 15.45 18.54

TIME, MS

50

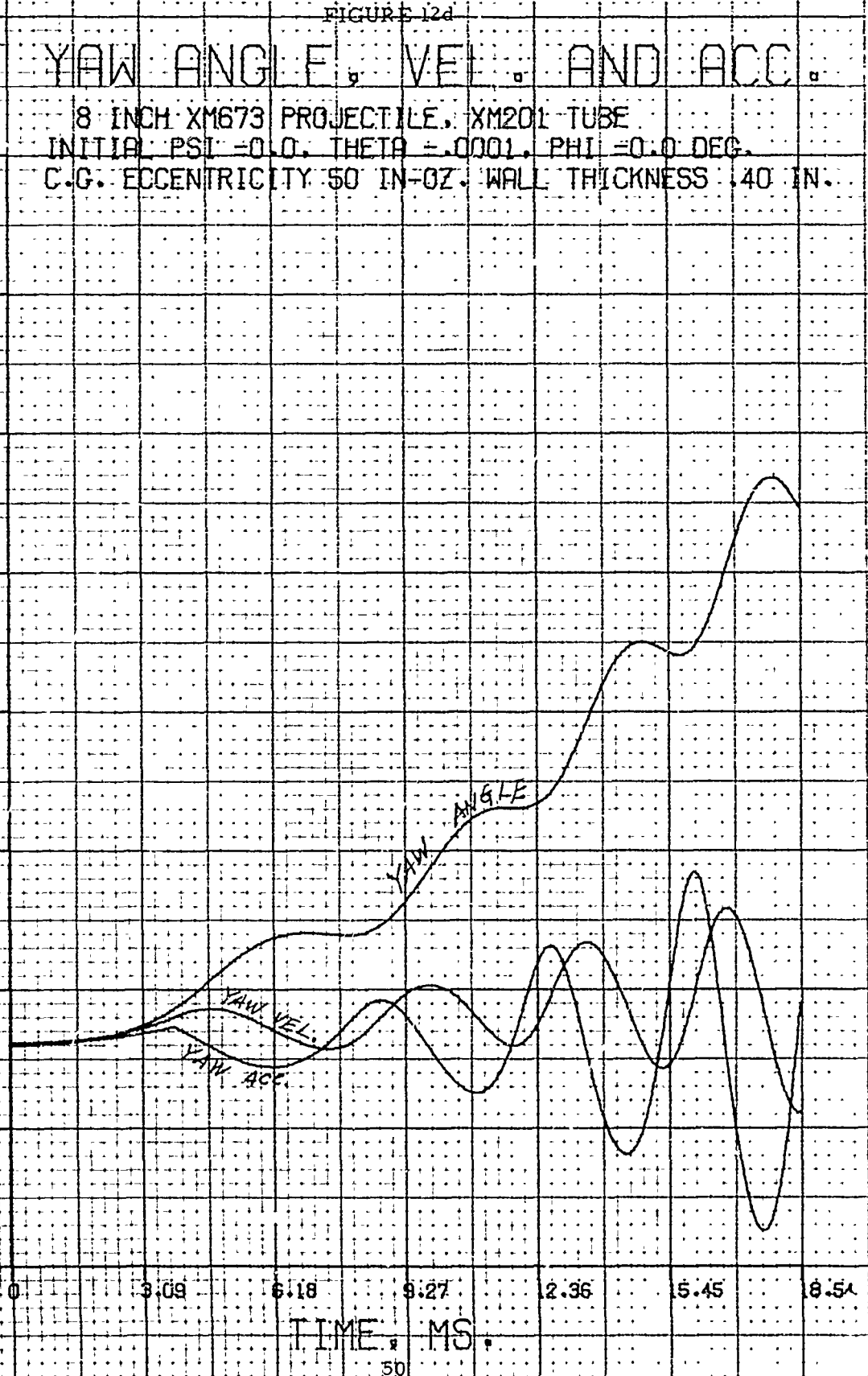


FIGURE 13a

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.

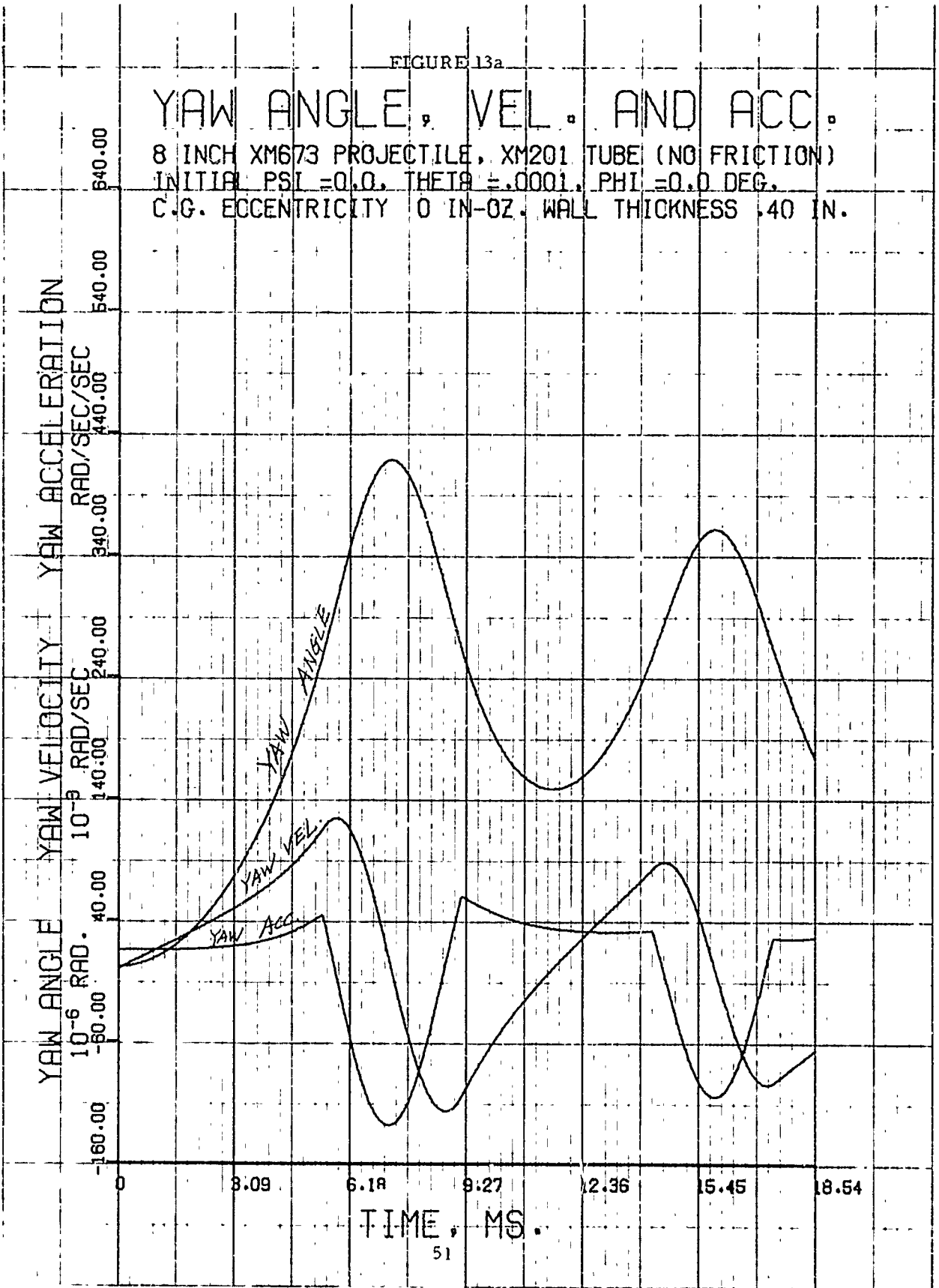


FIGURE 13b

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.

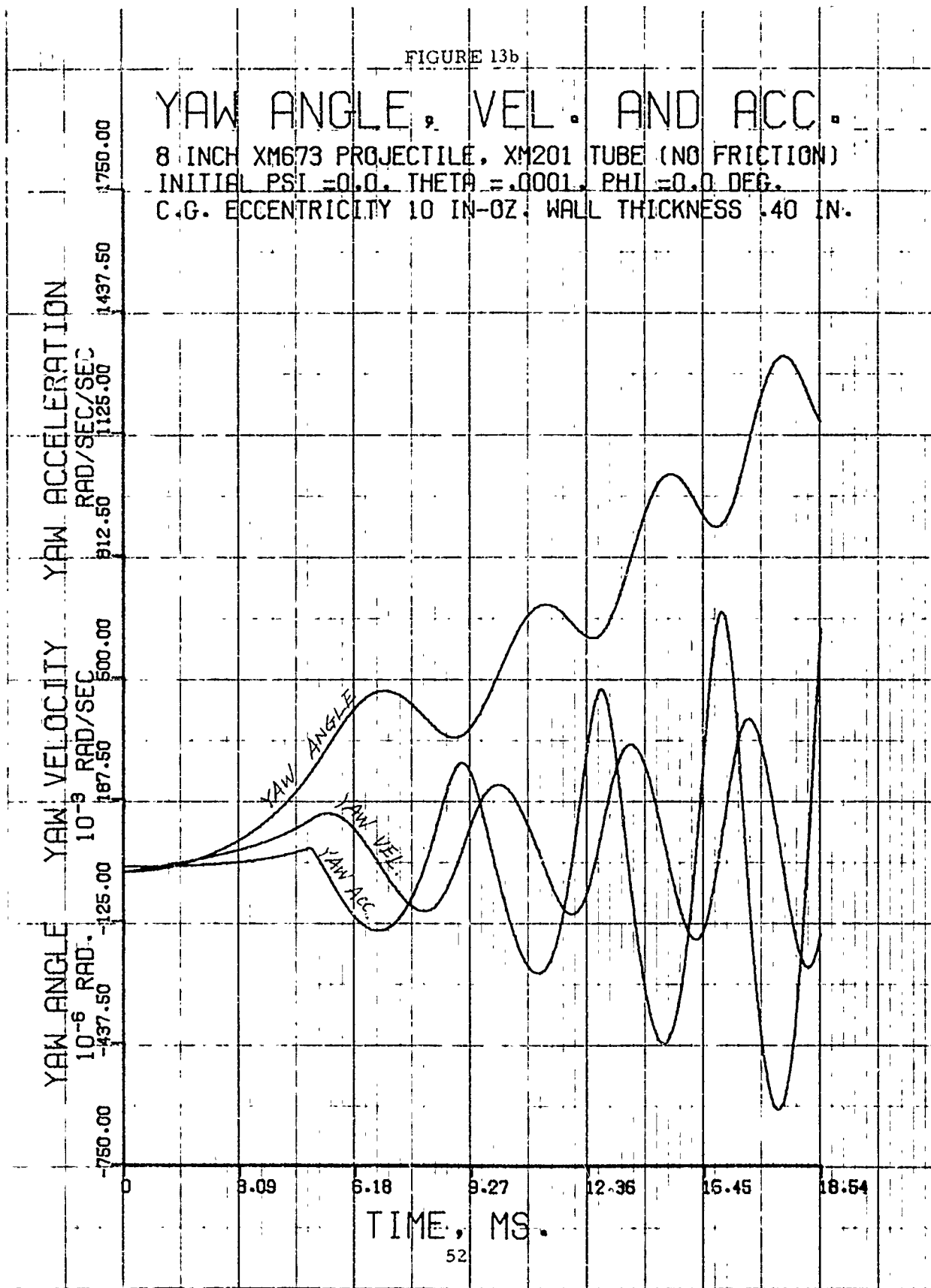


FIGURE 13c

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY 25 IN-02, WALL THICKNESS .40 IN.

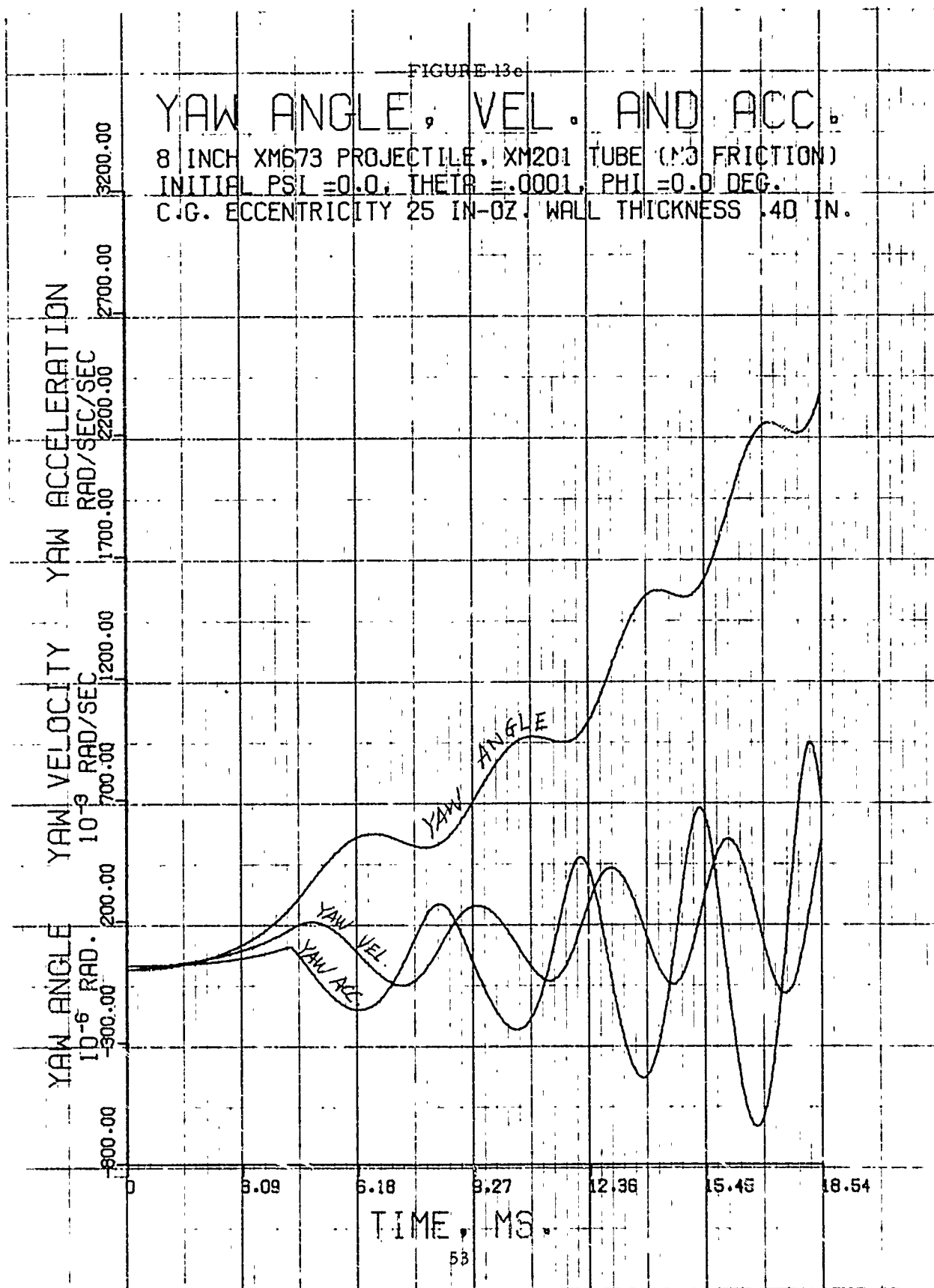


FIGURE 13d

YAW ANGLE, VEL. AND ACC.
8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI - C.G. THETA = .0001 PHT = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.

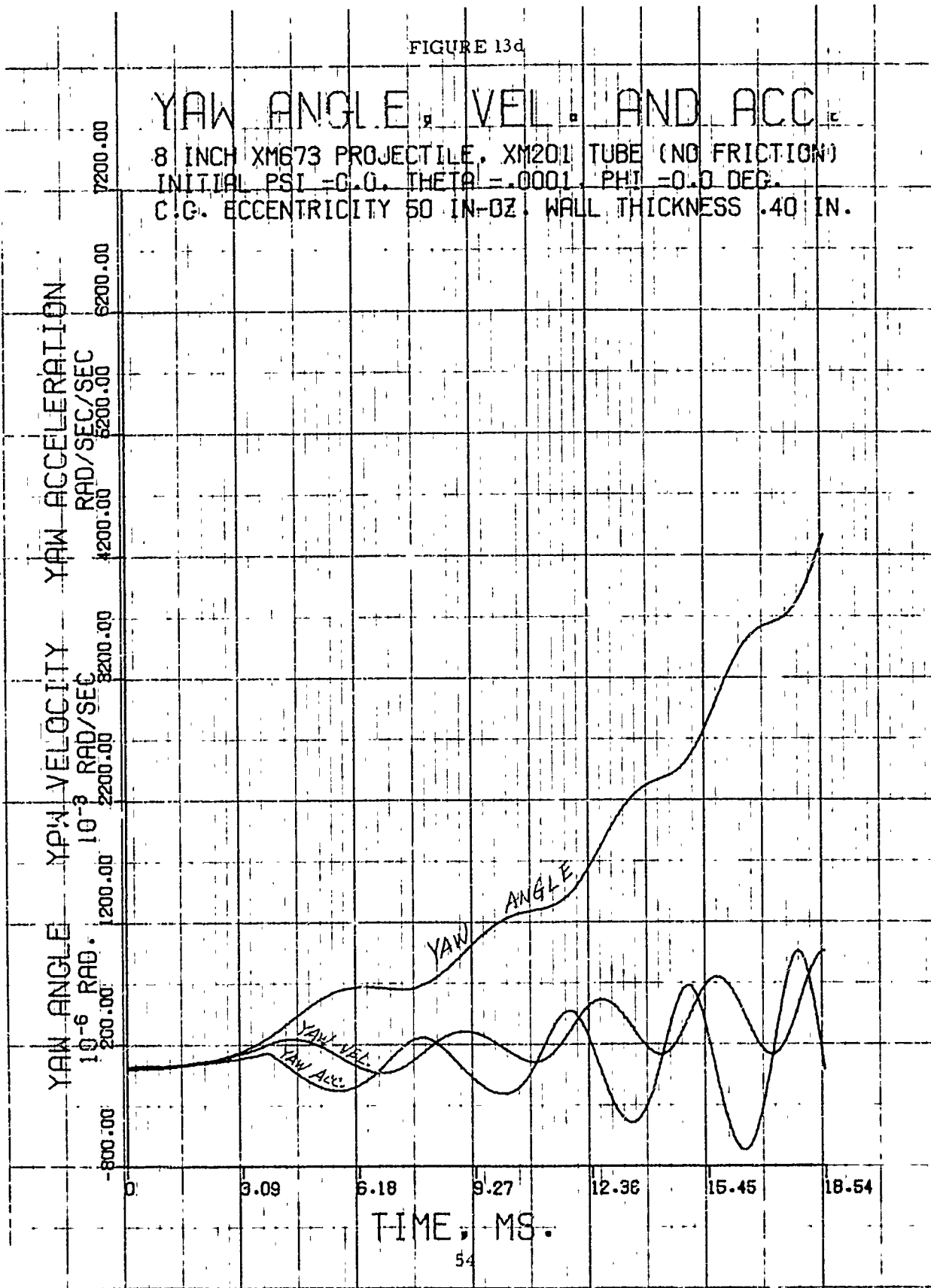


FIGURE 14a

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .38 IN.

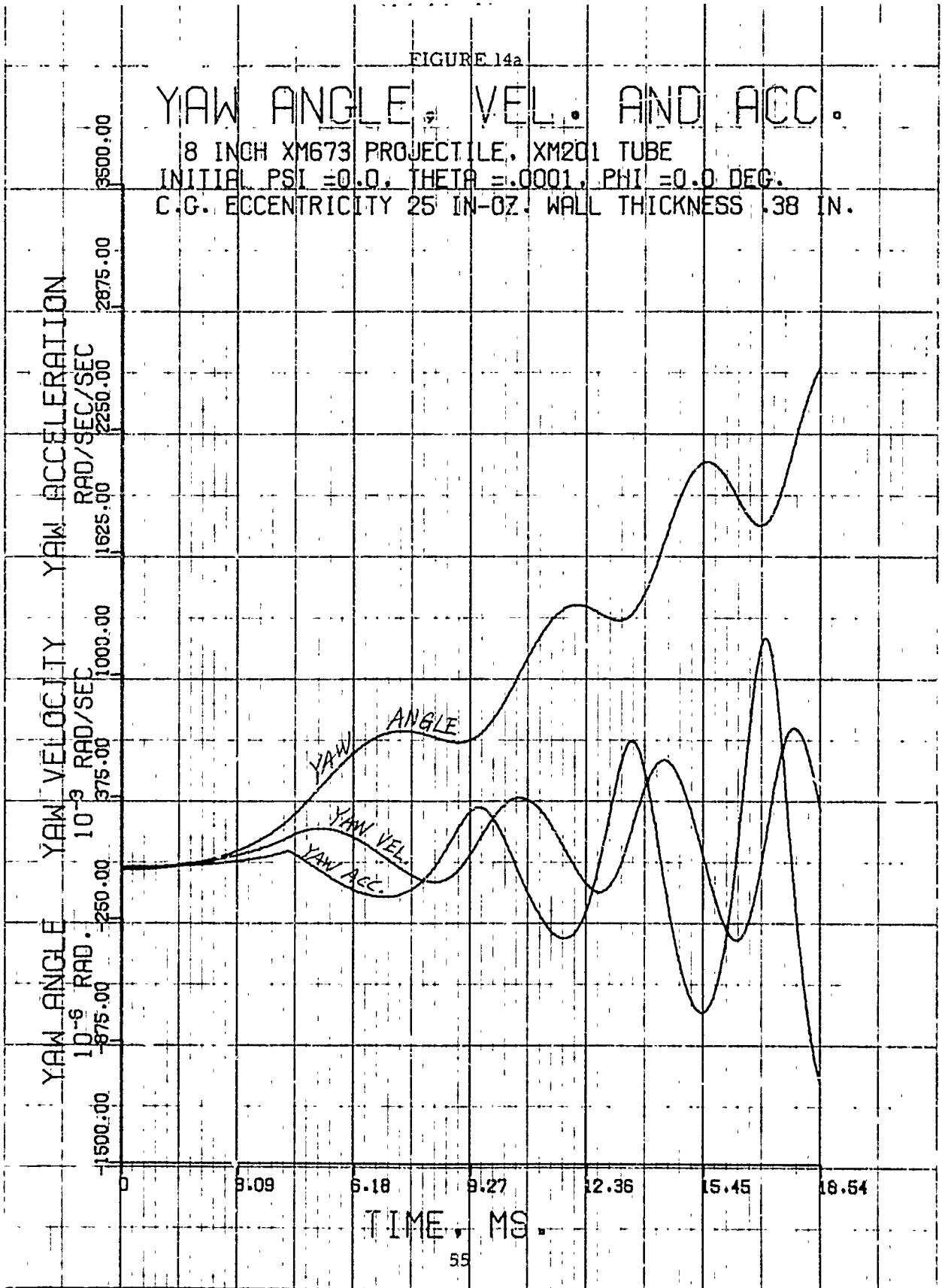


FIGURE 14b

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .42 IN.

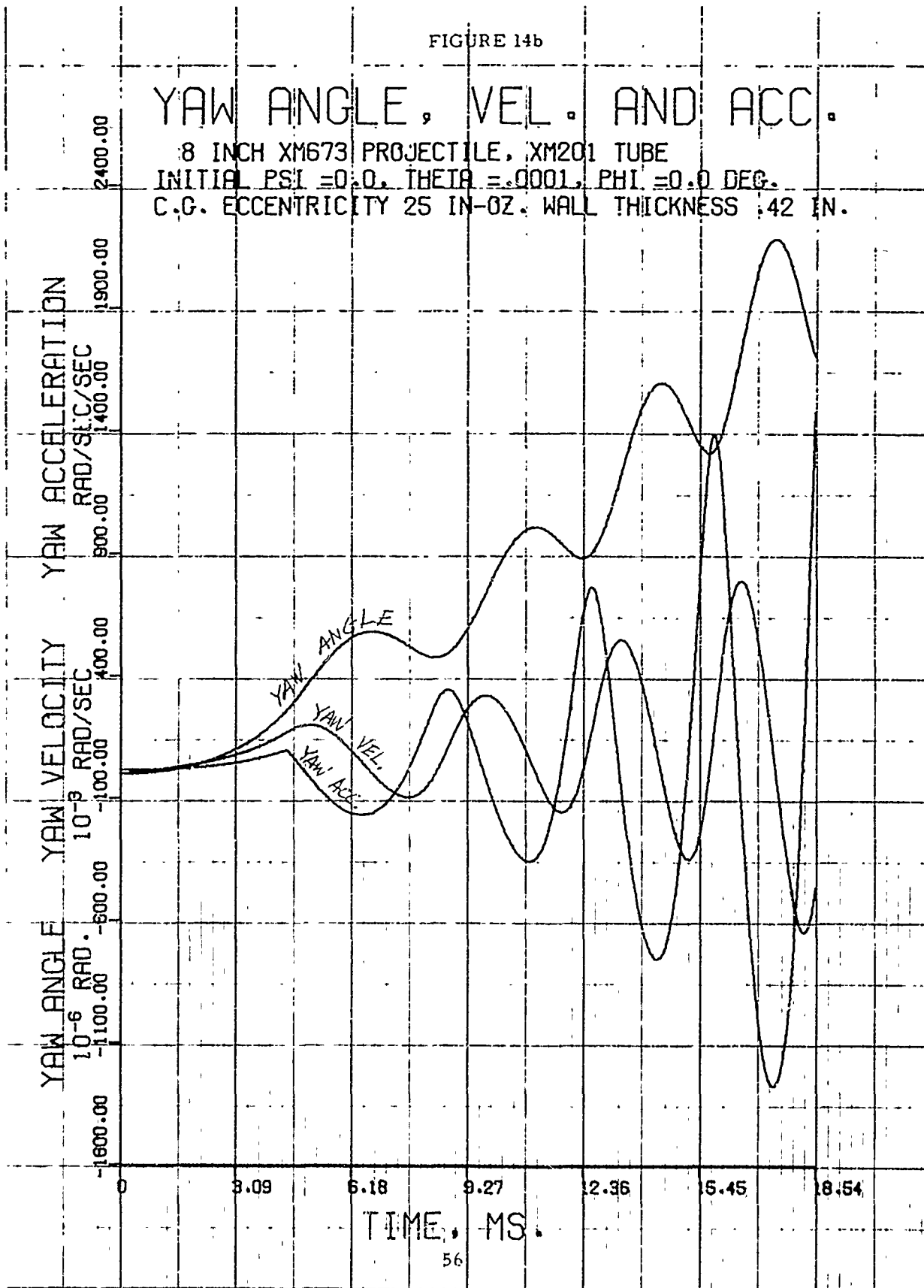


FIGURE 15a

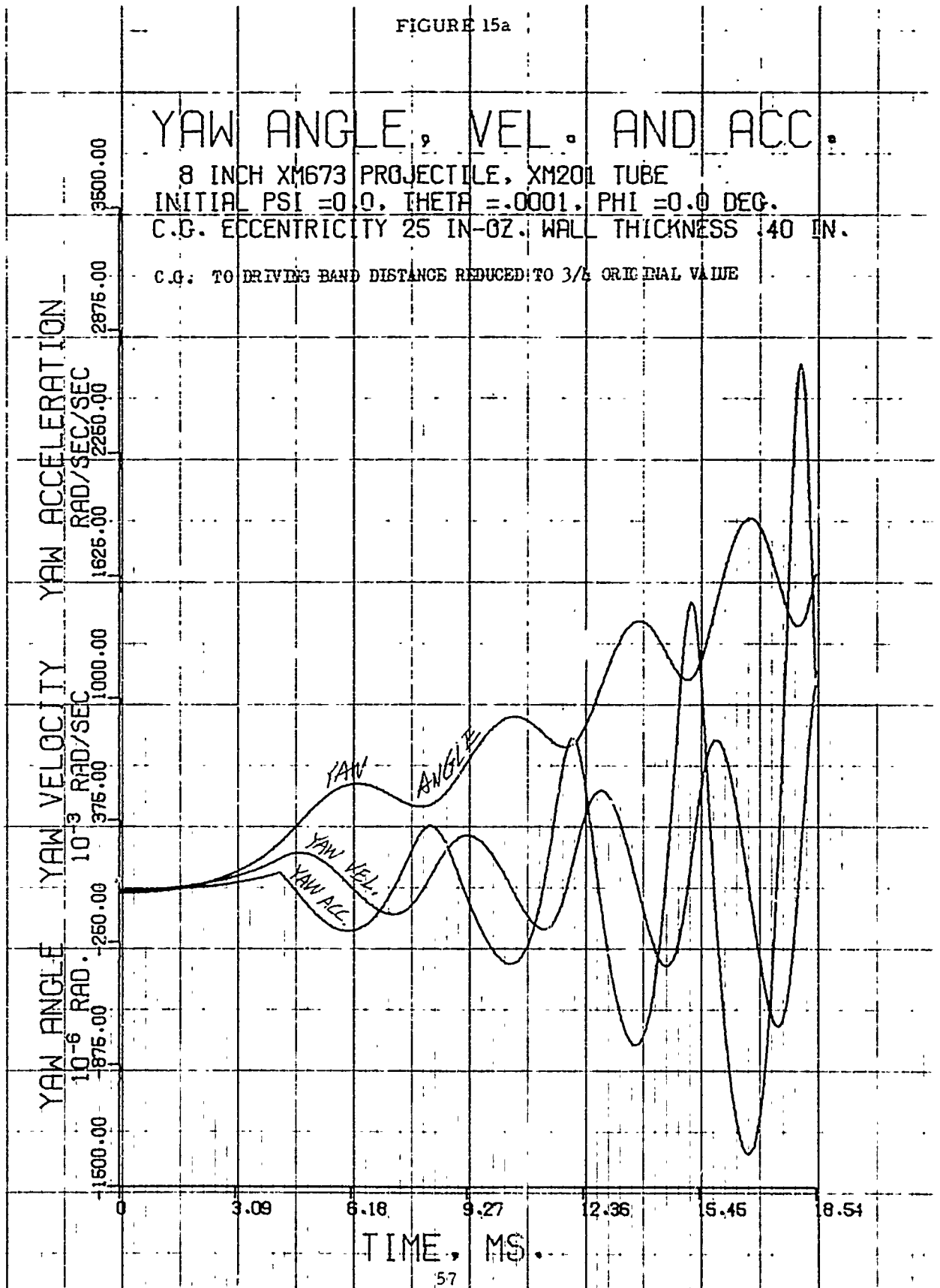


FIGURE 15b

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL $\Psi = 0.0$, $\Theta = .0001$, $\Phi = 0.0$ DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.

C.G. TO DRIVING BAND DISTANCE REDUCED TO $\frac{1}{2}$ ORIGINAL VALUE

YAW ANGLE
 10^{-6} RAD.
YAW VELOCITY
 10^{-3} RAD/SEC
YAW ACCELERATION
RAD/SEC/SEC

5600.00
4600.00
3600.00
2600.00
1600.00
600.00
-400.00
-1400.00
-2400.00

0 3.09 6.18 9.27 12.36 15.45 18.54

TIME, MS.

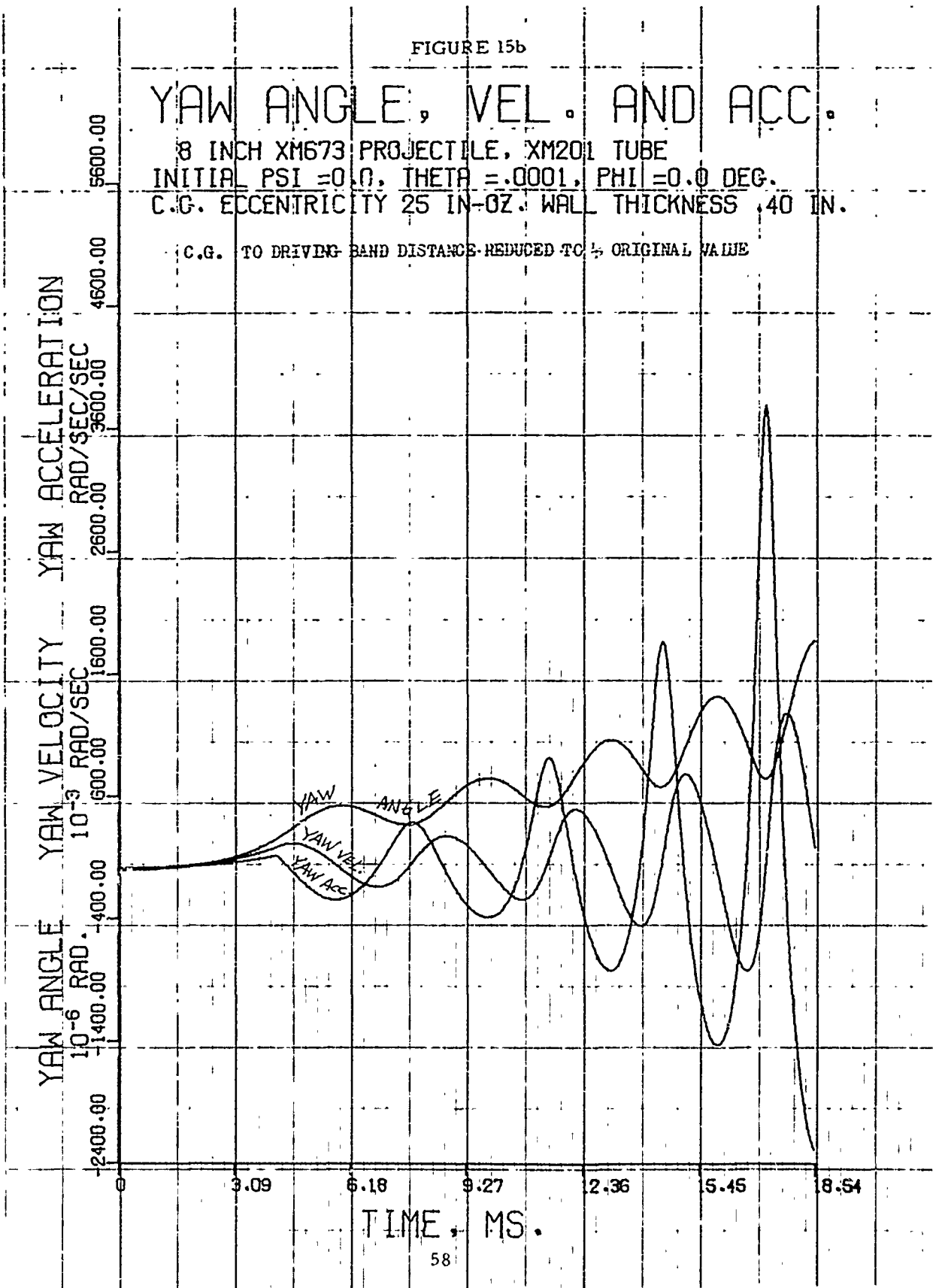


FIGURE 16b

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE
 INITIAL PST = 0.0, THETA = .0001, PHI = 0.0 DFC.
 C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.

CURVE 1	ACC. AT	CENTER OF GRAVITY
2	ACC. AT	BORRELET CENTER
3	ACC. AT	AXIAL POINT 15.0 IN. FROM NOSE
4		7.5
5		5.0
6		2.5

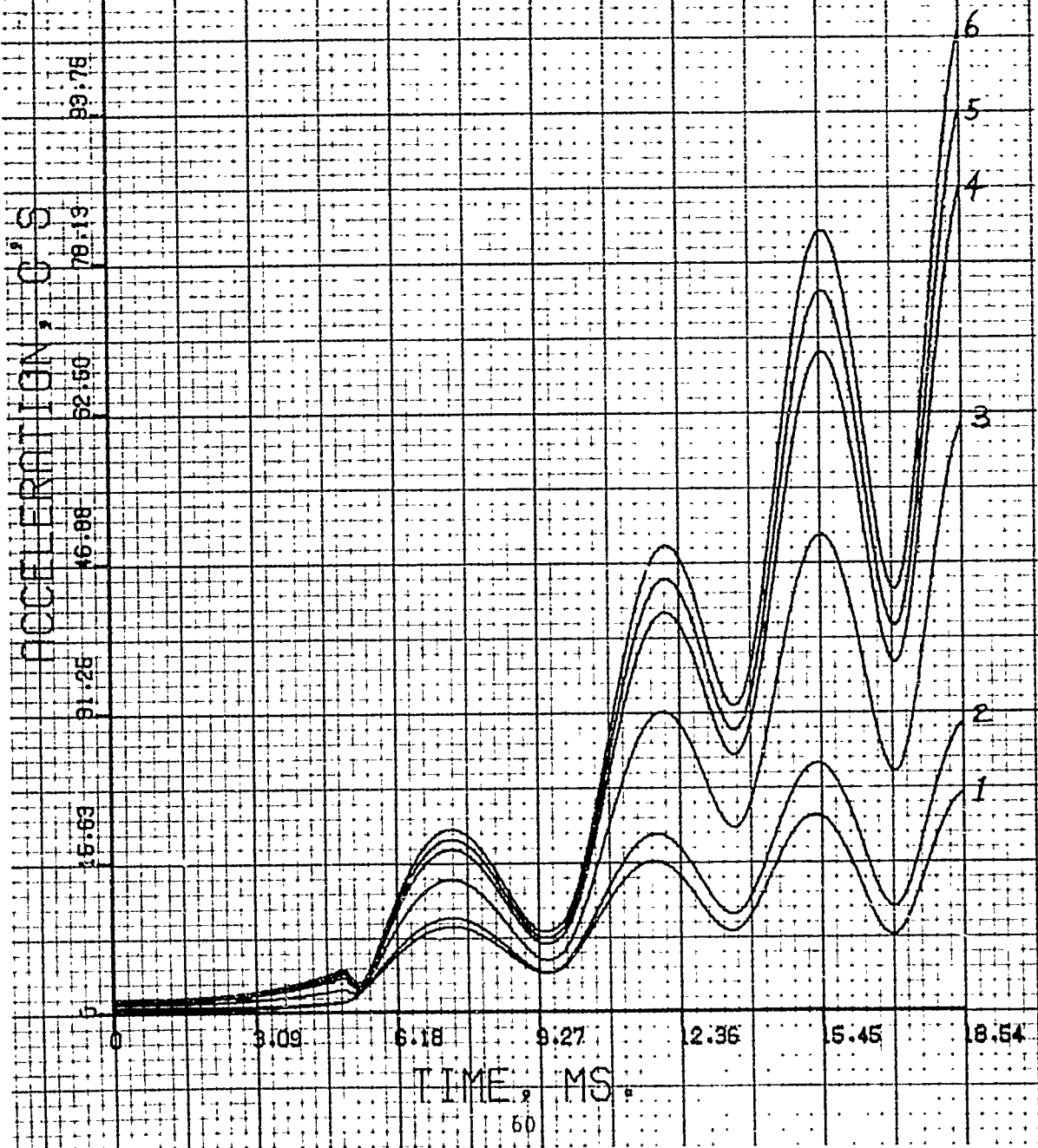


FIGURE 16c

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = 0.001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

CURVE 1 — ACC. AT CENTER OF GRAVITY
2 — ACC. AT SOURCE POINT CENTER
3 — ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
4 — ACC. AT AXIAL POINT 2.6 IN. FROM NOSE
5 — ACC. AT AXIAL POINT 5.0 IN. FROM NOSE
6 — ACC. AT AXIAL POINT 2.6 IN. FROM NOSE

ACCELERATION, G'S

300.00
250.00
200.00
150.00
100.00
50.00
0

0 3.09 5.18 9.27 12.36 15.45 18.54

TIME, MS.

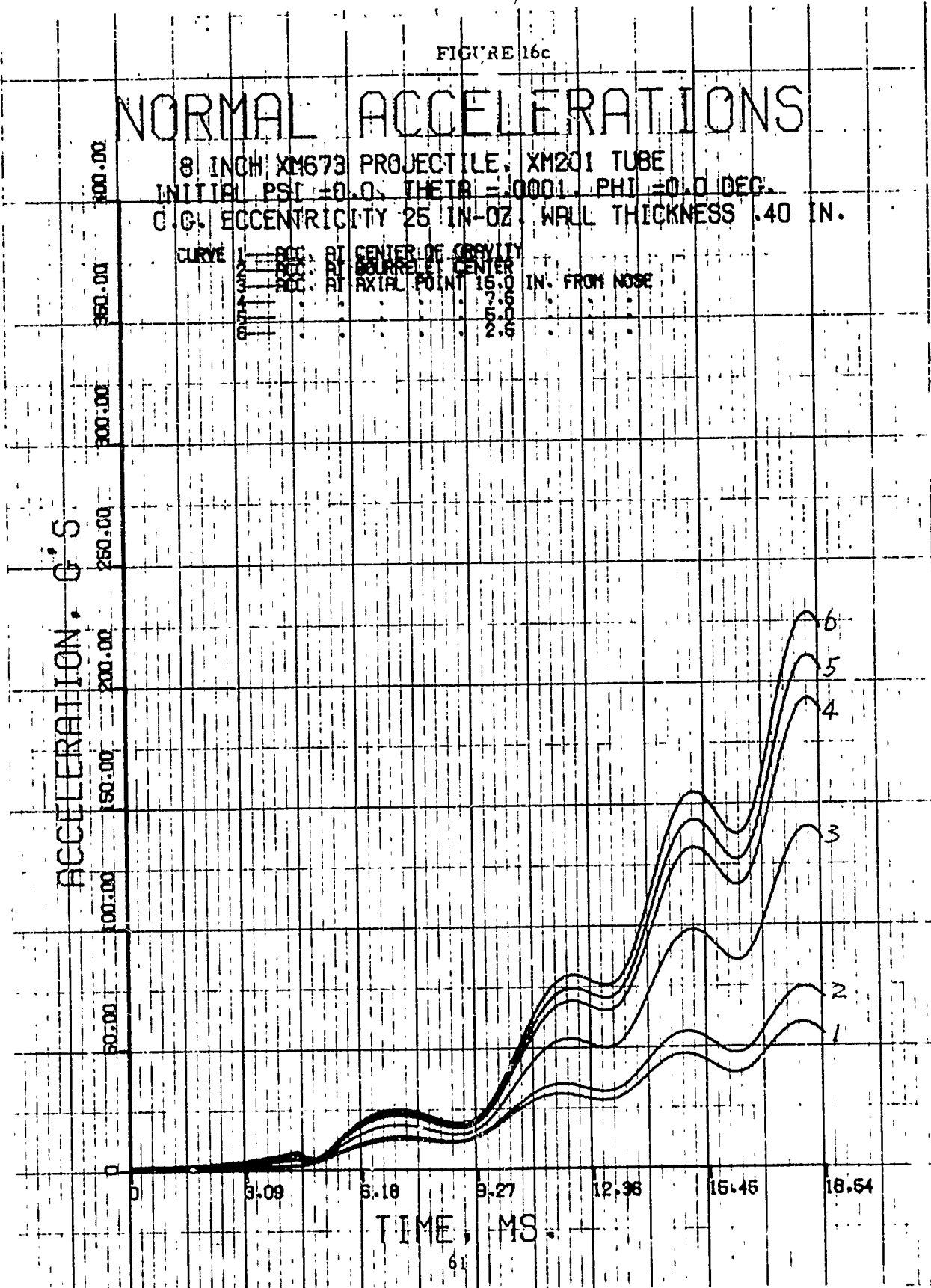


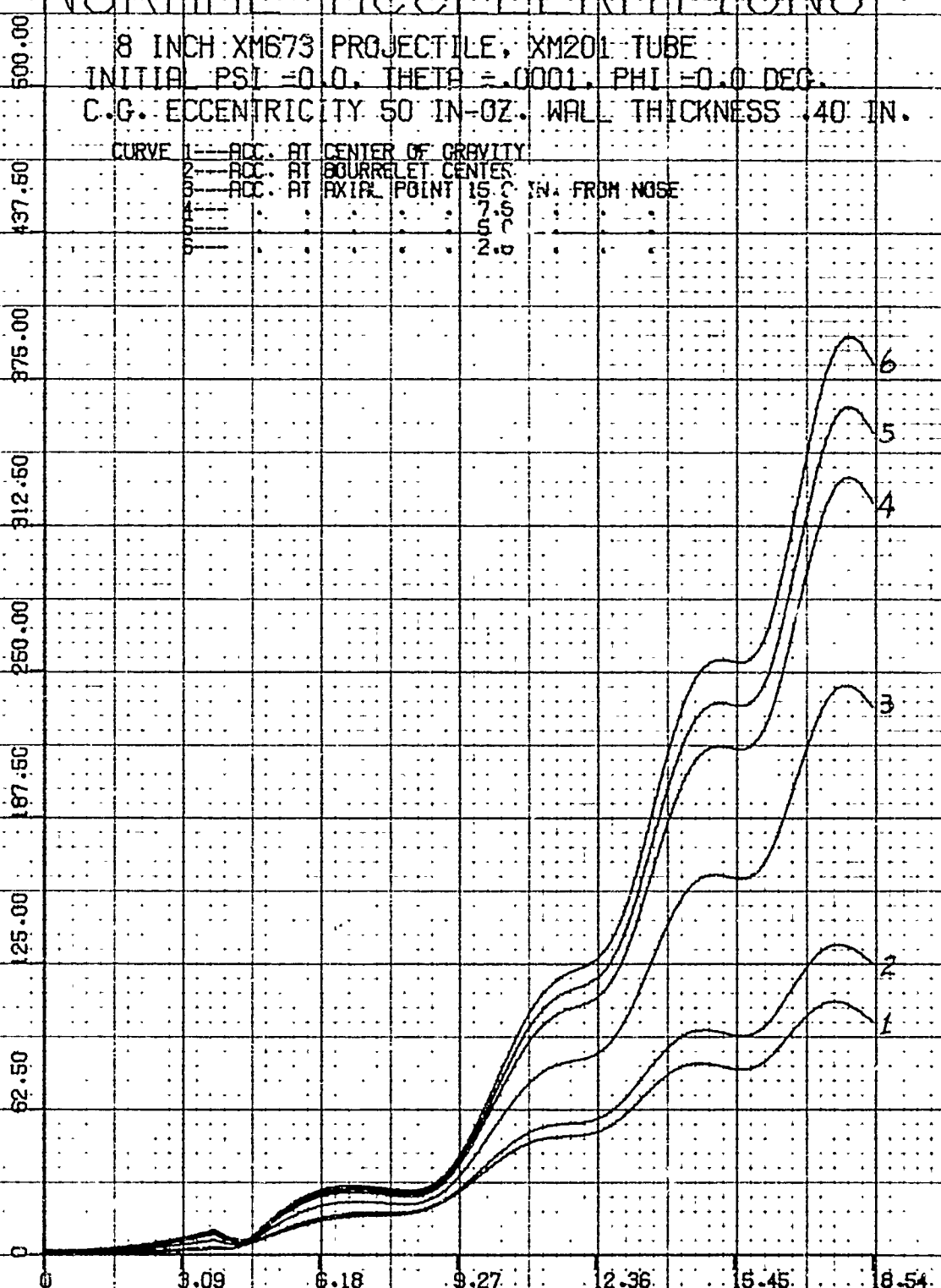
FIGURE 16d

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.

CURVE 1---ACC. AT CENTER OF GRAVITY
2---ACC. AT GOURRELET CENTER
3---ACC. AT AXIAL POINT 15 IN. FROM NOSE
4---" " " " 7.5 IN. " "
5---" " " " 5 IN. " "
6---" " " " 2.5 IN. " "

ACCELERATION, G'S



TIME, MS.

FIGURE 17a

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.

CURVE 1	ACC. AT CENTER OF GRAVITY	
2	ACC. AT BOURRELET CENTER	
3	ACC. AT AXIAL POINT 16.0 IN. FROM NOSE	
4	:	7.5
5	:	5.0
6	:	2.5

ACCELERATION, G'S

20.00
17.50
15.00
12.50
10.00
7.50
5.00
2.50
0

TIME, MS.

0 3.09 6.18 9.27 12.36 15.45 18.54

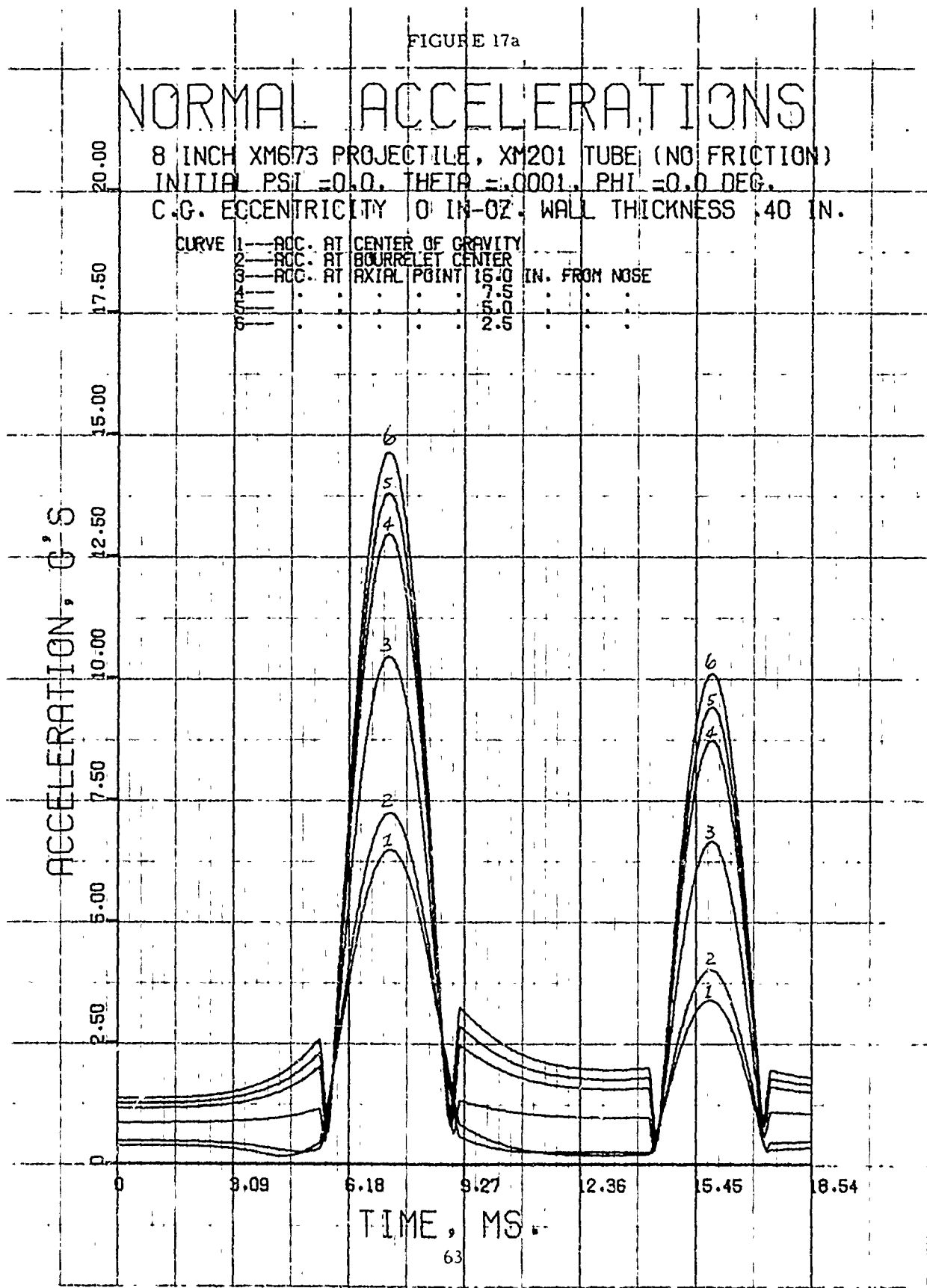


FIGURE 17c

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)

INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.

C.G. ECCENTRICITY 25 IN-02, WALL THICKNESS .40 IN.

CURVE	1	2	3	4	5	6
---	ACC. AT CENTER OF GRAVITY	ACC. AT BOURRELET CENTER	ACC. AT AXIAL POINT 15.0 IN. FROM NOSE	7.5	5.0	2.5

ACCELERATION, G'S

0
50.00
100.00
150.00
200.00
250.00
300.00
350.00
400.00

TIME, MS.

0 3.09 6.18 9.27 12.36 15.45 18.54

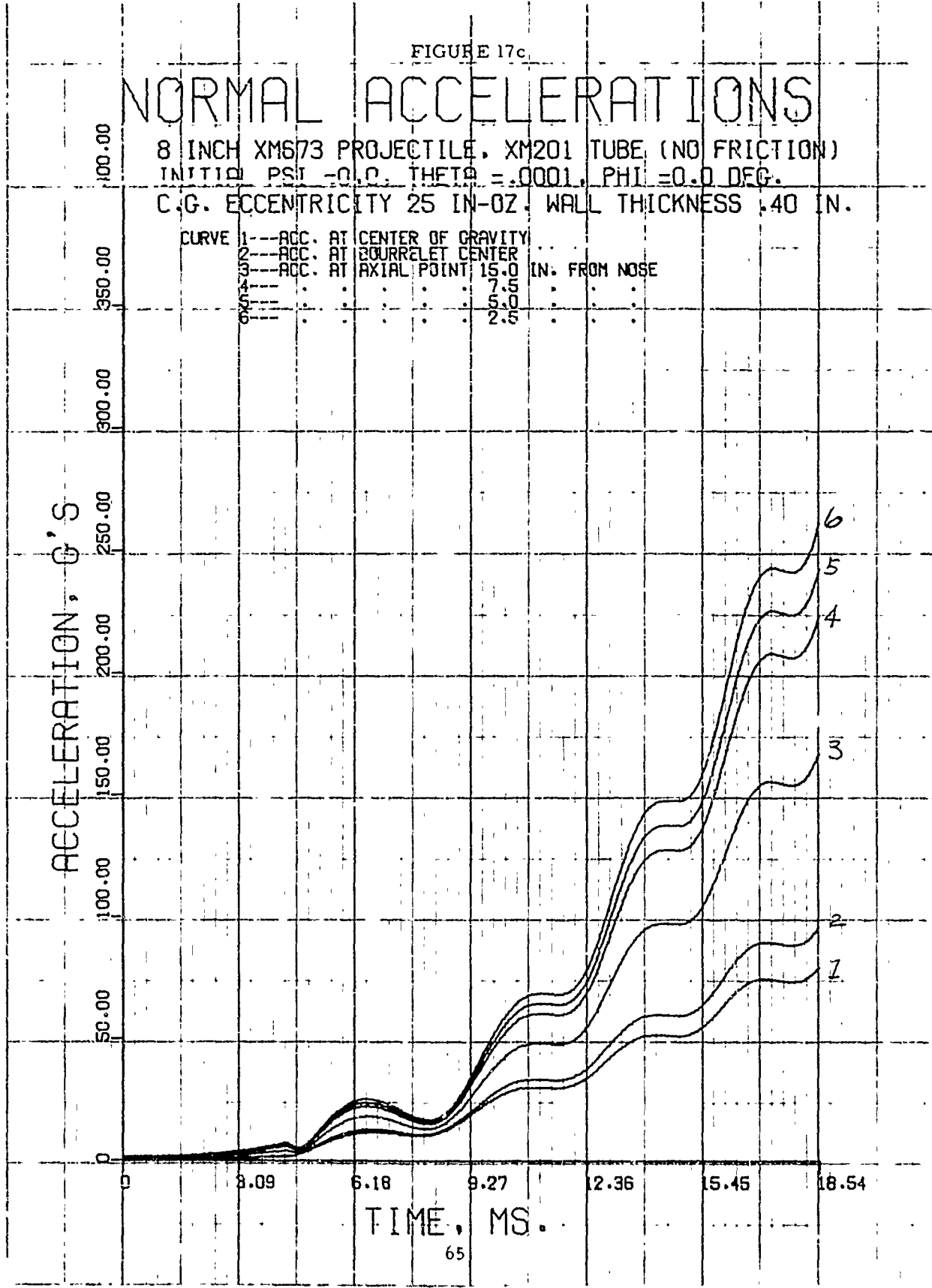


FIGURE 17d

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.

CURVE	ACC. AT	CENTER OF GRAVITY
1	ACC. AT	CENTER OF GRAVITY
2	ACC. AT	BOURRELET CENTER
3	ACC. AT	AXIAL POINT 15.0 IN. FROM NOSE
4	ACC. AT	AXIAL POINT 7.5 IN. FROM NOSE
5	ACC. AT	AXIAL POINT 5.0 IN. FROM NOSE
6	ACC. AT	AXIAL POINT 2.5 IN. FROM NOSE

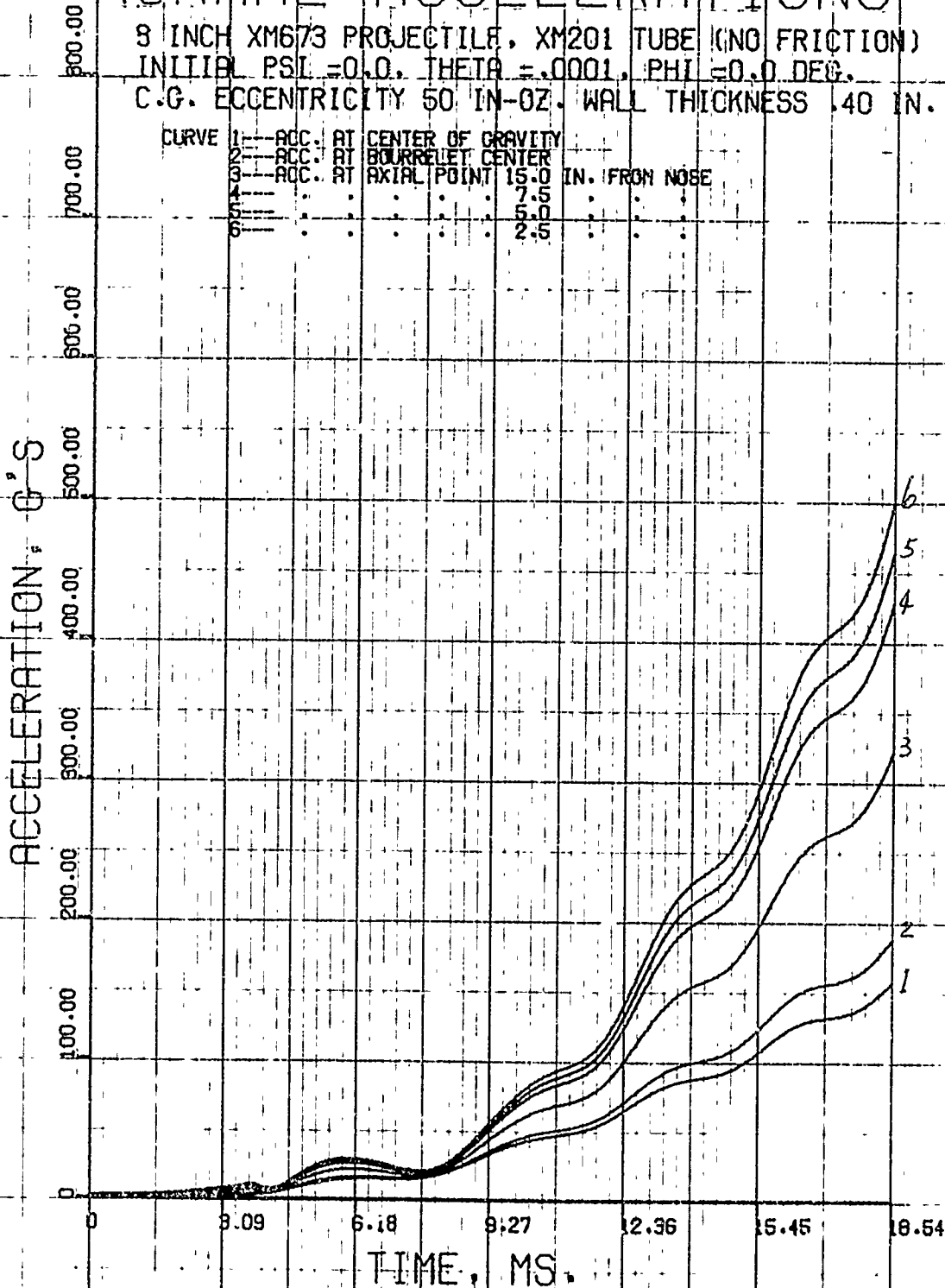


FIGURE 18a

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .38 IN.

CURVE	1	2	3	4	5	6
ACC. AT	CENTER OF GRAVITY	BORRELET CENTER	AXIAL POINT	15.0 IN. FROM NOSE	7.5	5.0
					2.5	

ACCELERATION, G'S

250.00
218.75
187.50
156.25
125.00
93.75
62.50
31.25
0

TIME, MS.

0 3.09 6.18 9.27 12.36 15.45 18.54

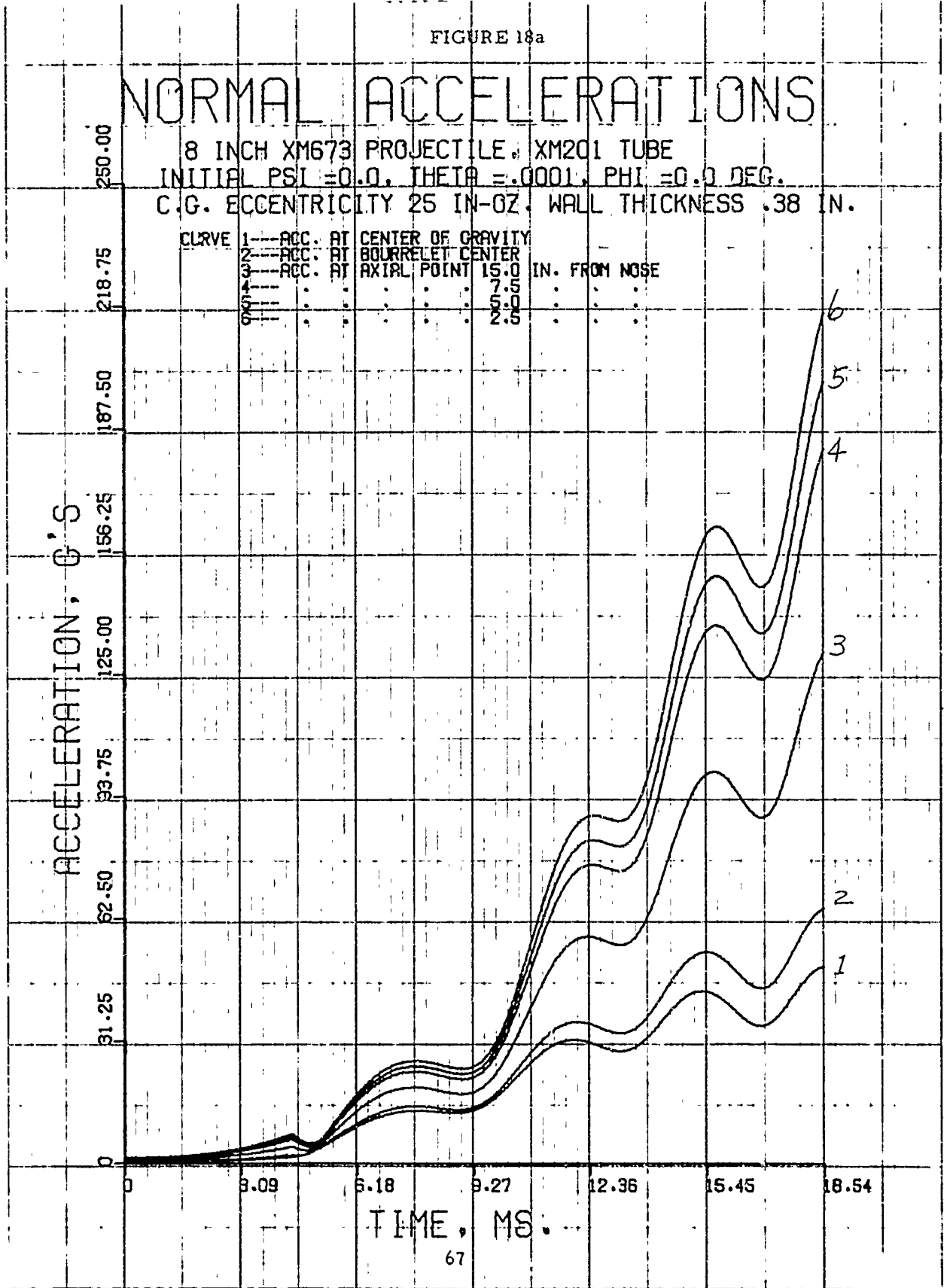


FIGURE 18b

NORMAL ACCELERATIONS

8 INCH XM573 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .42 IN.

CURVE 1	ACC. AT	CENTER OF GRAVITY
2	ACC. AT	BOURRELET CENTER
3	ACC. AT	AXIAL POINT 15.0 IN. FROM NOSE
4	:	:
5	:	:
6	:	:

ACCELERATION, G'S

250.00
218.75
187.50
156.25
125.00
93.75
62.50
31.25
0

6
5
4
3
2
1

0 3.09 6.18 9.27 12.36 15.45 18.54

TIME, MS.

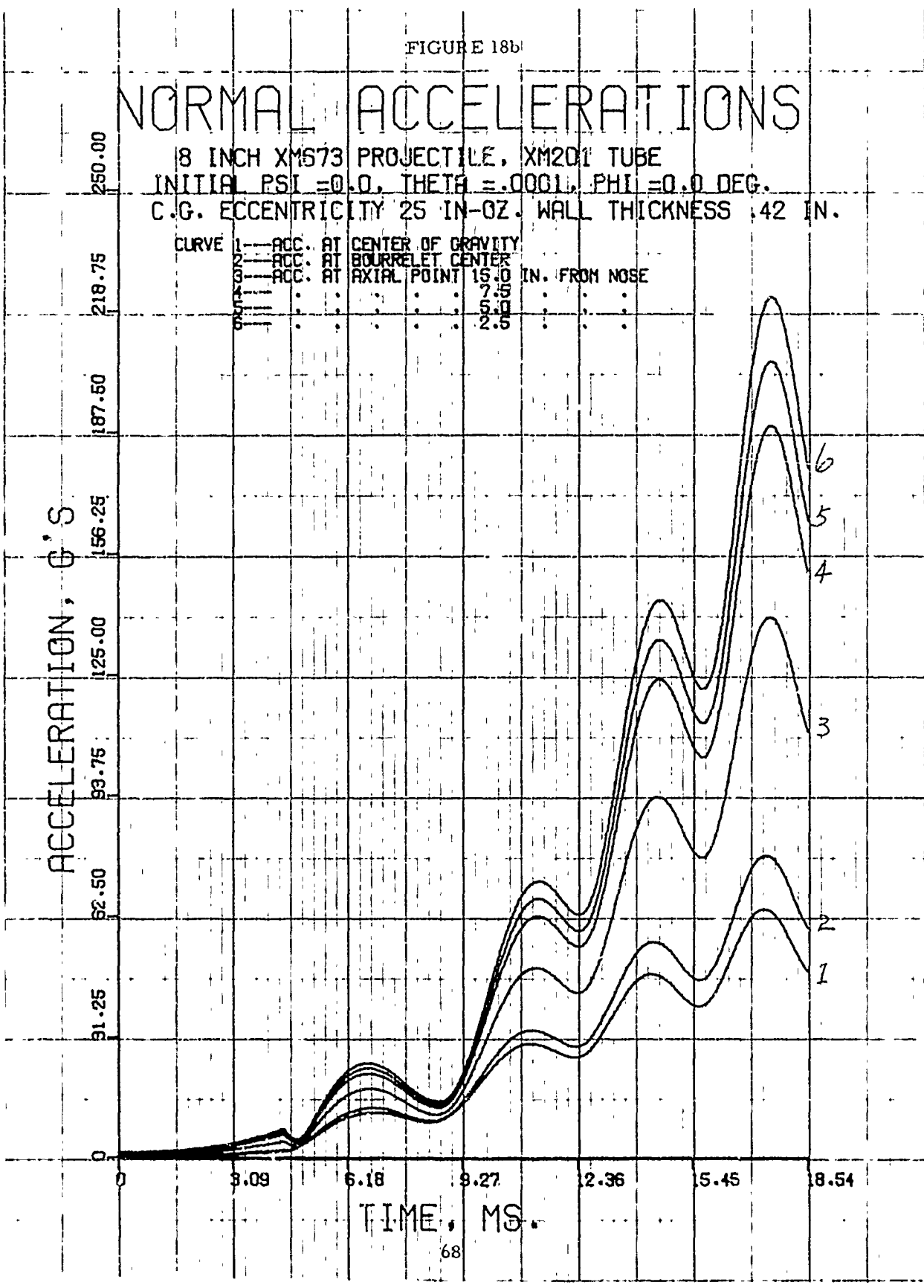


FIGURE 19a

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-0Z, WALL THICKNESS .40 IN.

CURVE	1	---	ACC. AT CENTER OF GRAVITY
	2	---	ACC. AT BOURRELET CENTER
	3	---	ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
	4	---	7.5
	5	---	5.0
	6	---	2.5

C.G. TO DRIVING-BAND DISTANCE REDUCED TO 3/4 ORIGINAL VALUE

ACCELERATION, G'S

250.00
218.75
187.50
156.25
125.00
93.75
62.50
31.25
0

TIME, MS.

0 3.09 6.18 9.27 12.36 15.45 18.54

6
5
4
3
2
1

FIGURE 19b

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, XM201 TUBE
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.

CURVE 1	---	ACC. AT	CENTER OF GRAVITY
2	---	ACC. AT	BOURRELET CENTER
3	---	ACC. AT	AXIAL POINT 15.0 IN. FROM NOSE
4	---	---	7.5
5	---	---	5.0
6	---	---	2.5

C.G. TO DRIVING BAND DISTANCE REDUCED TO 1/2 ORIGINAL VALUE

ACCELERATION, G'S

400.00
350.00
300.00
250.00
200.00
150.00
100.00
50.00
0

0 3.09 6.18 9.27 12.36 15.45 18.54

TIME, MS.

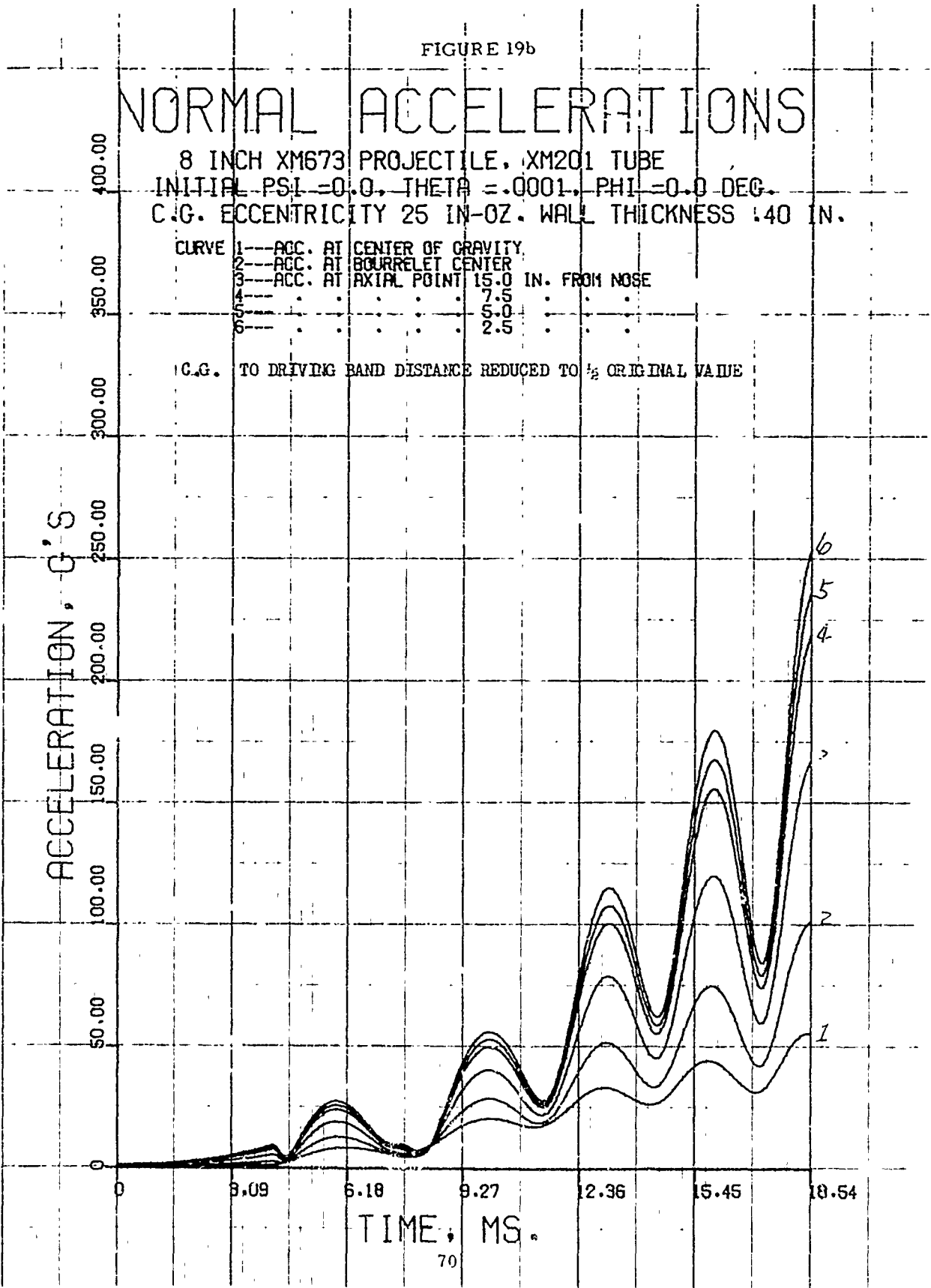


FIGURE 20a

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE
 INITIAL PSI = 0.0, THETA = .0031, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ., WALL THICKNESS .40 IN.
 F1, F2, F3 - FORCE IN AXIS -1, -2, -3 DIRECTION

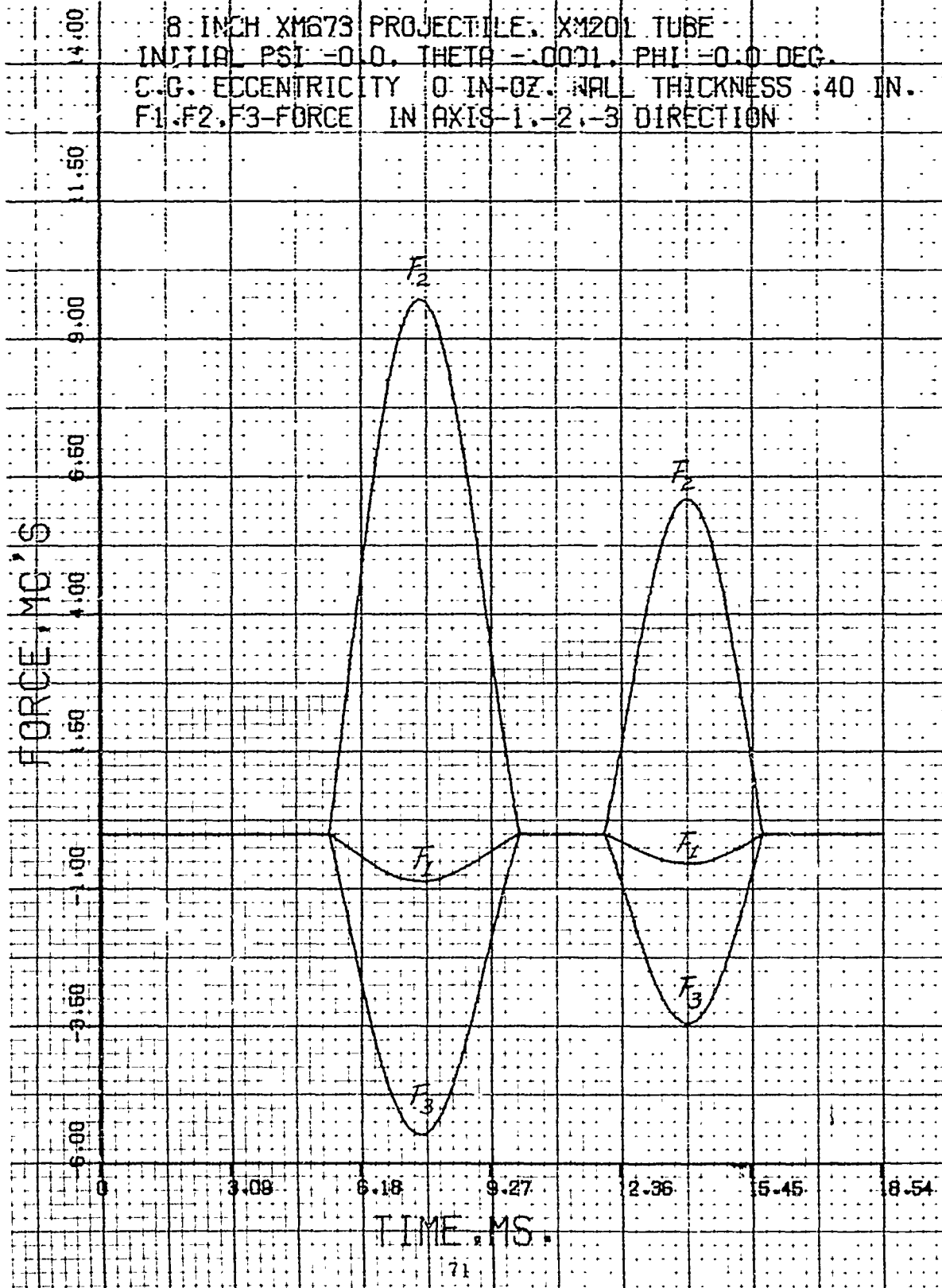


FIGURE 20b

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ., WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS -1, -2, -3 DIRECTION

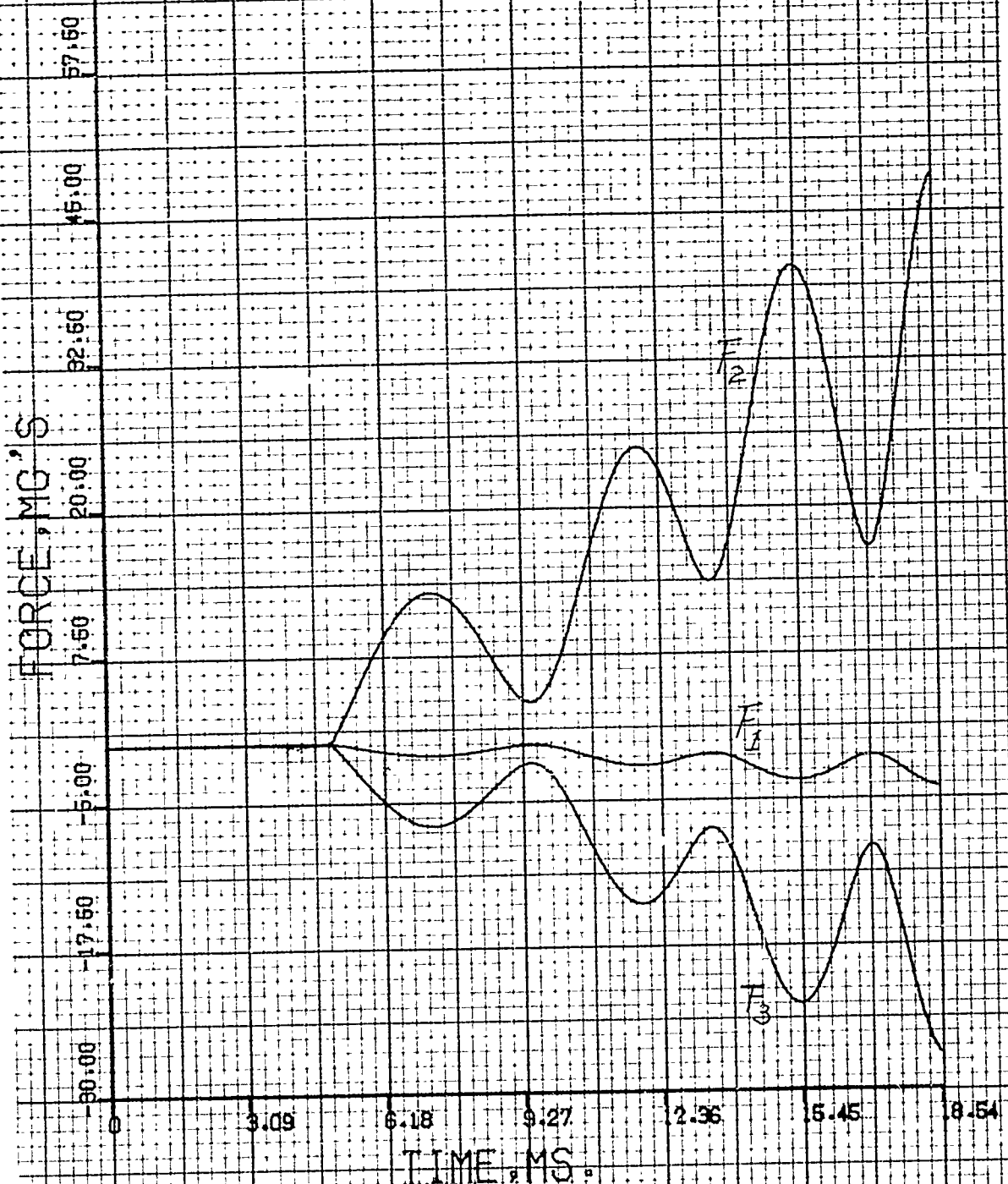


FIGURE 20c

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE; XM201 TUBE
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.
 F1, F2, F3 - FORCE IN AXIS -1, -2, -3 DIRECTION

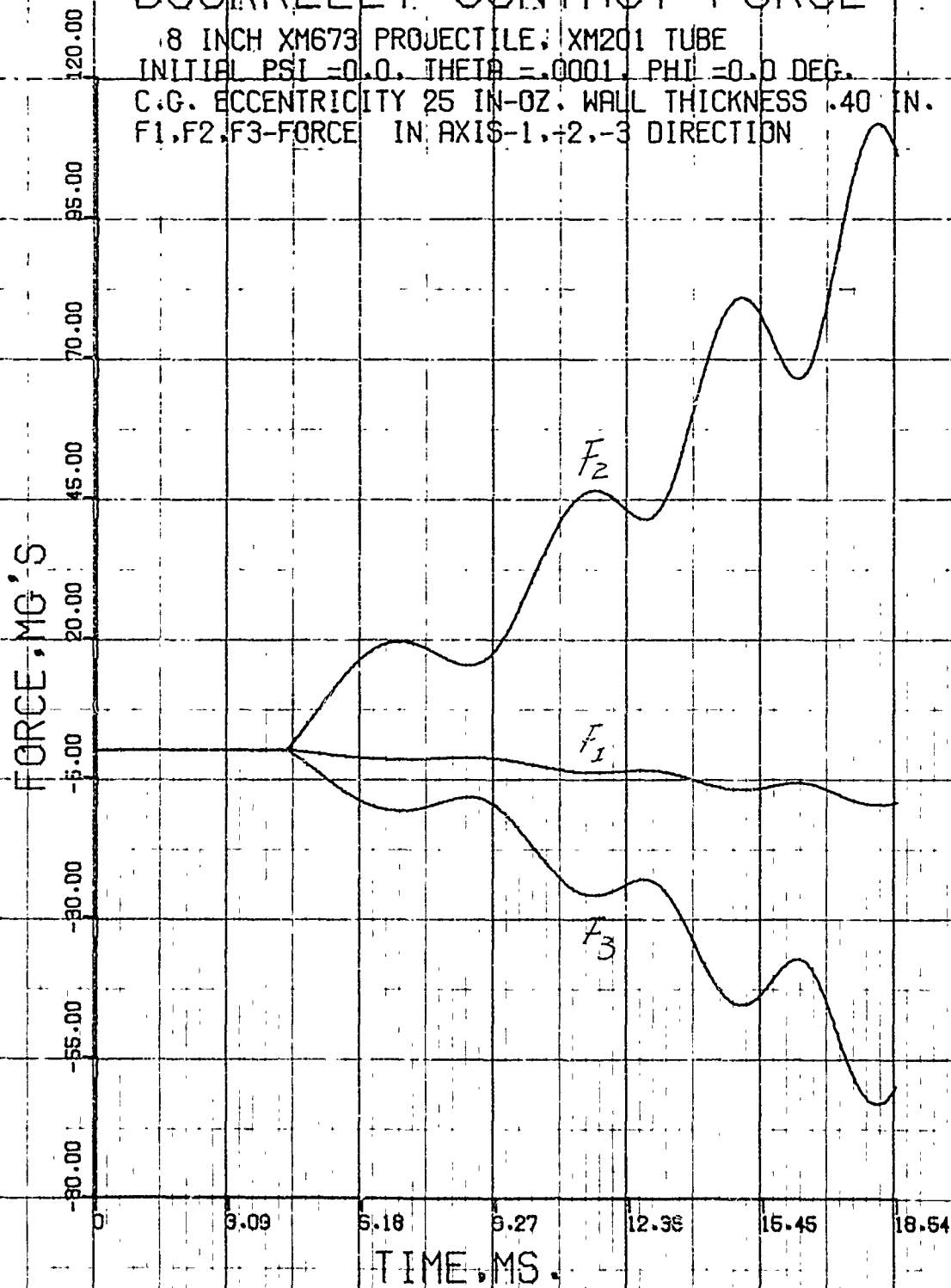


FIGURE 20a

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE
 INITIAL PSI -0.0, THETA -.0001, PHI -0.0 DEG.
 C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.
 F1, F2, F3-FORCE IN AXIS -1, -2, -3 DIRECTION

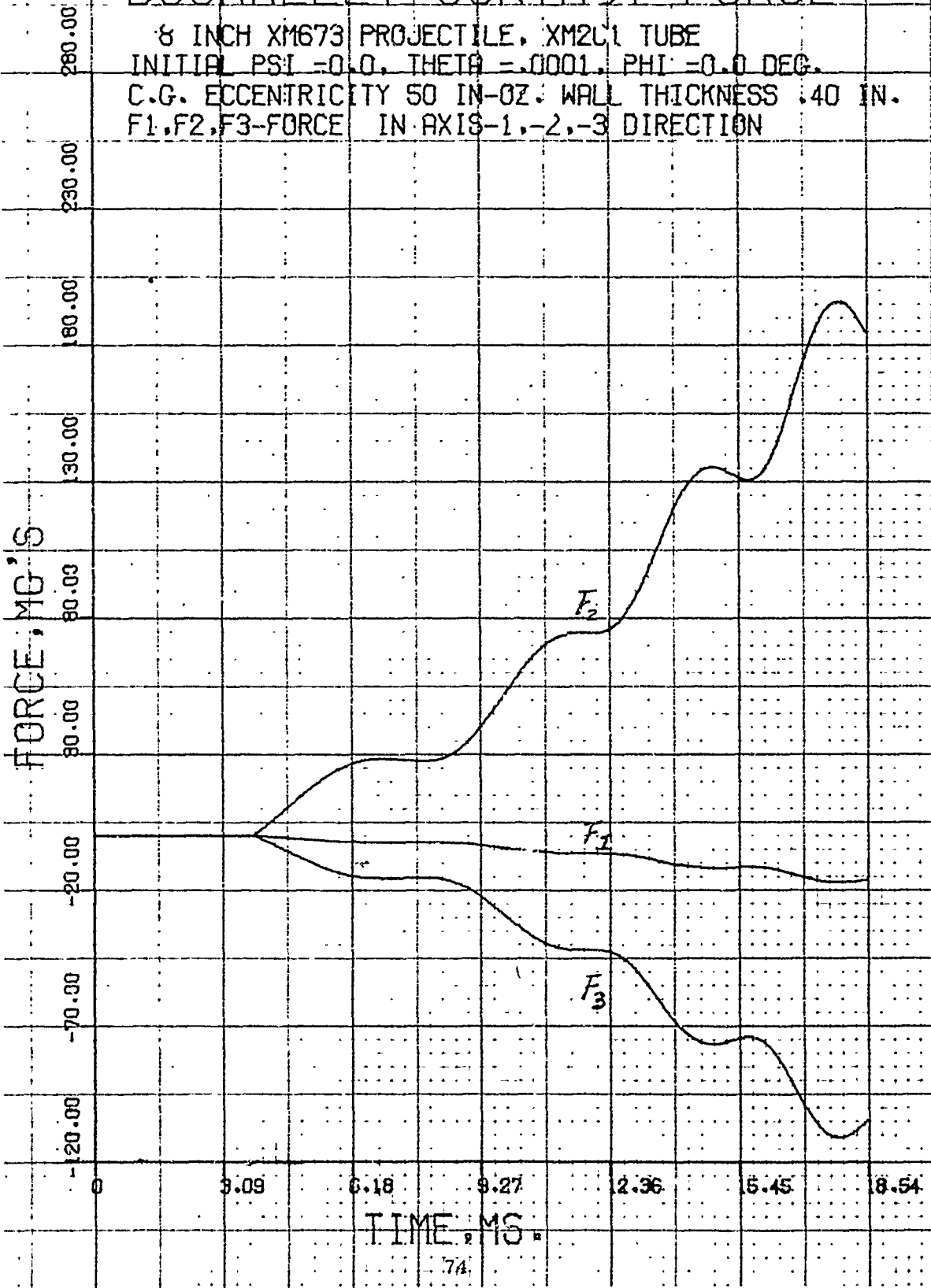


FIGURE 21a

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION

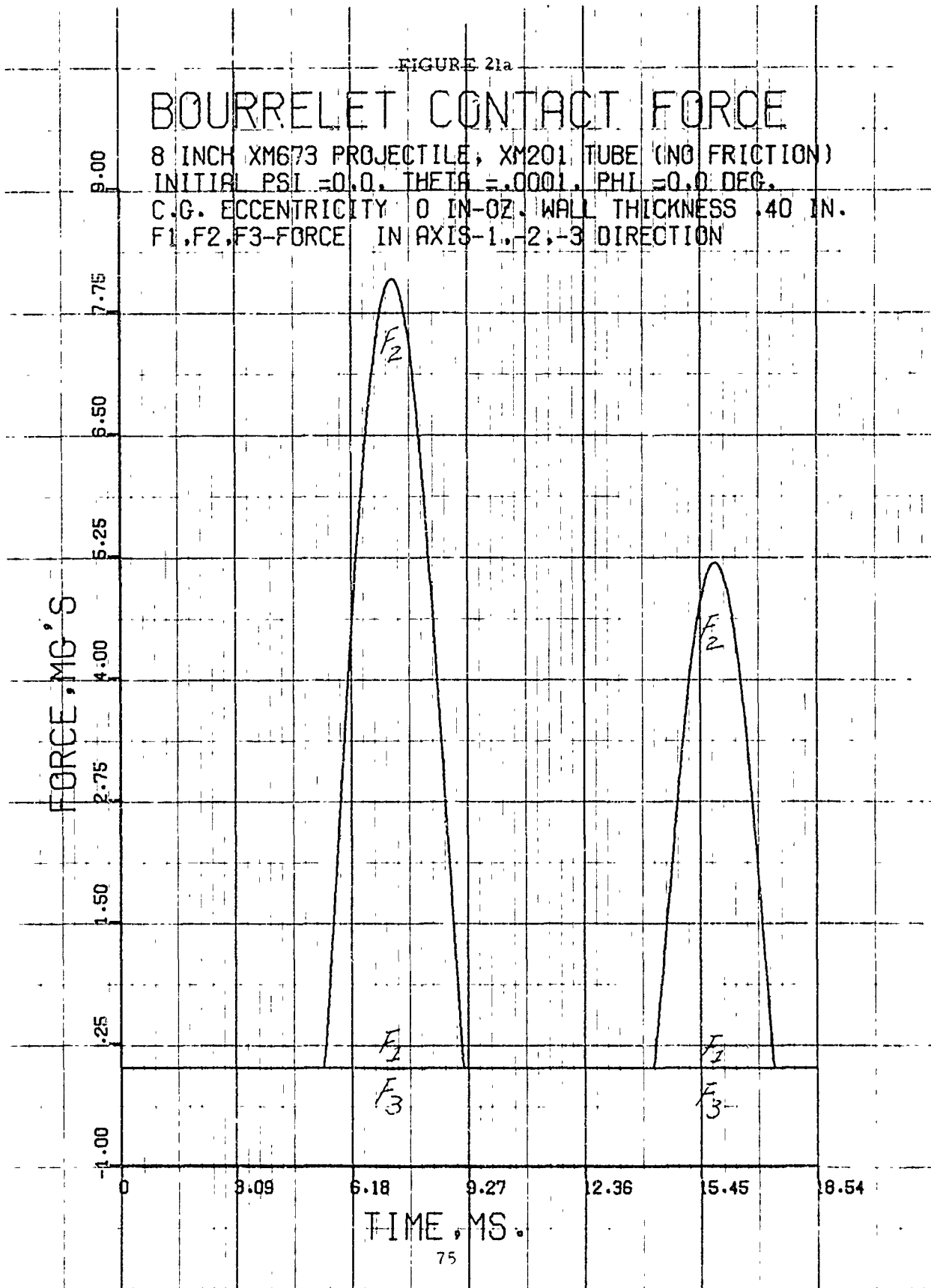


FIGURE 21b

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS -1, -2, -3 DIRECTION

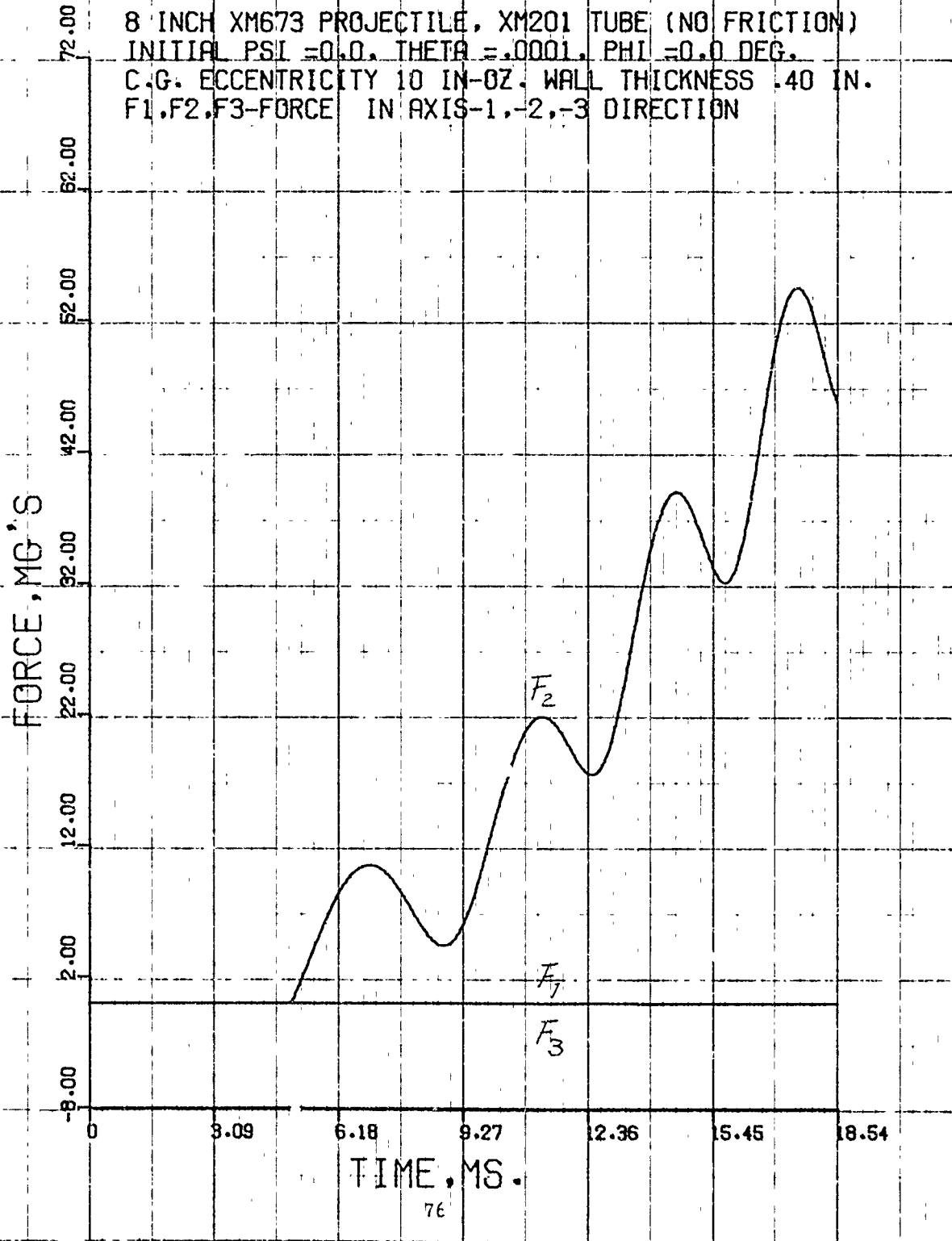


FIGURE 21c

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION

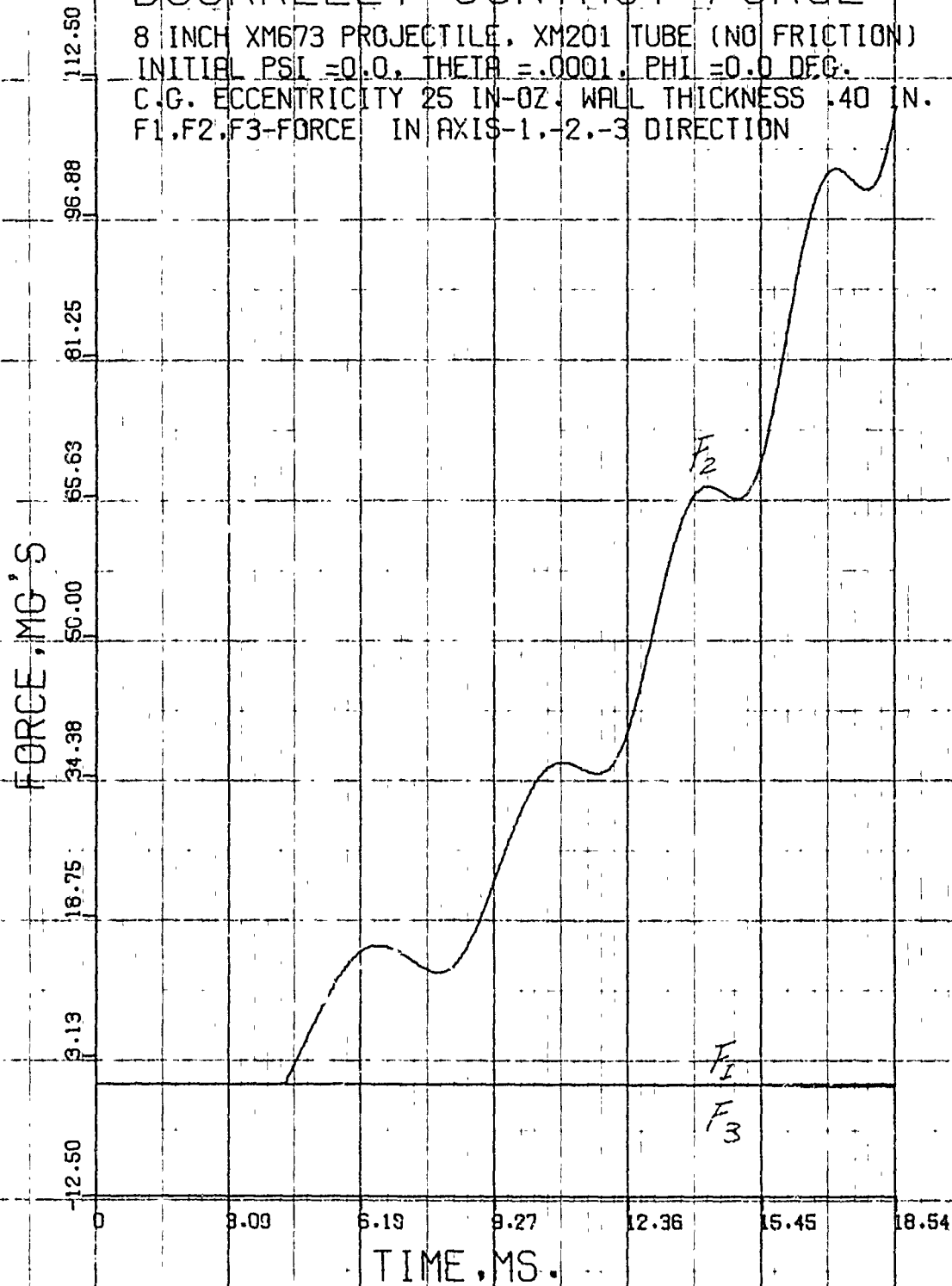


FIGURE 21a

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE (NO FRICTION)
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.
 F₁, F₂, F₃ - FORCE IN AXIS-1, -2, -3 DIRECTION

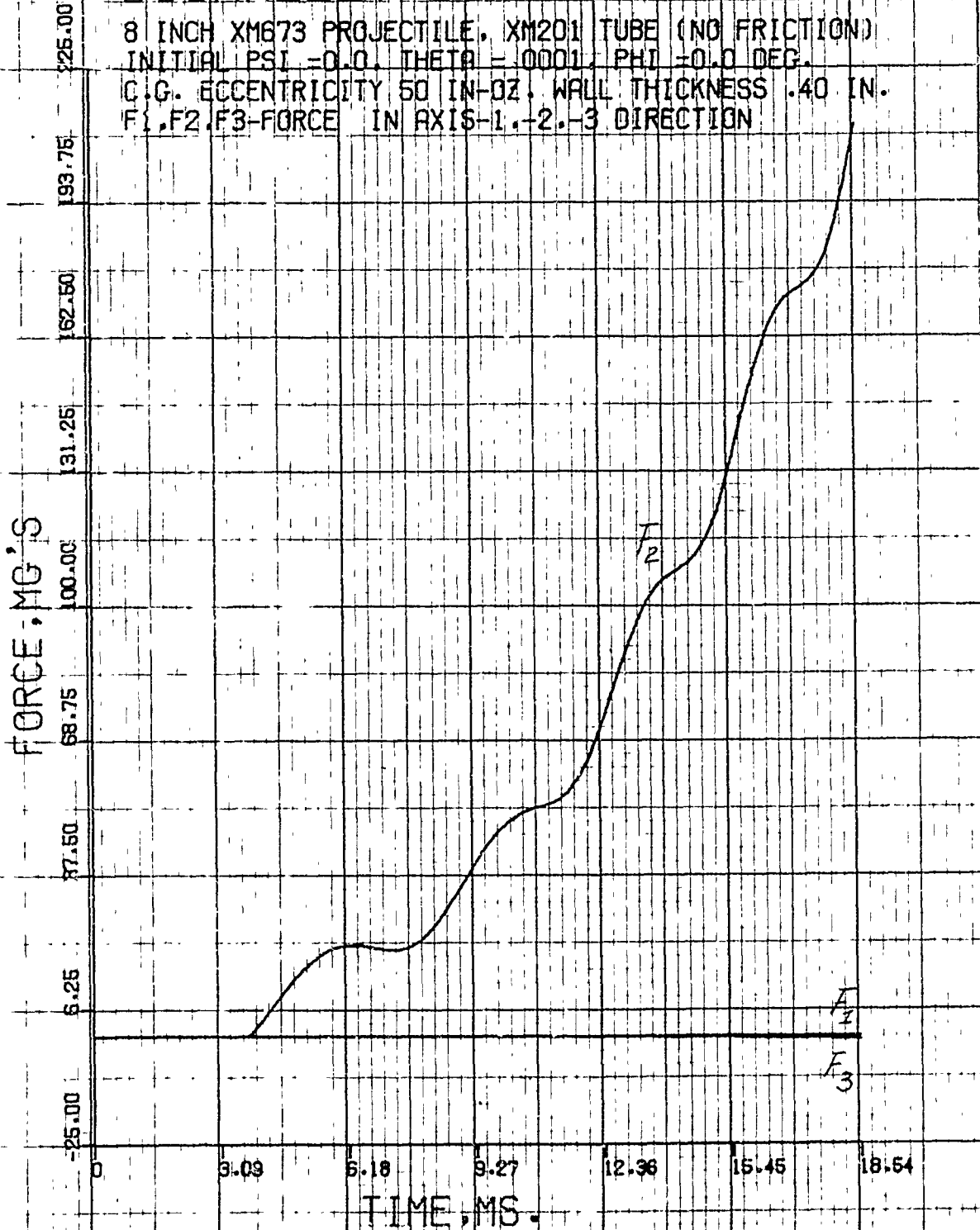


FIGURE 22a

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .38 IN.
 F1, F2, F3-FORCE IN AXIS-1, -2, -3 DIRECTION

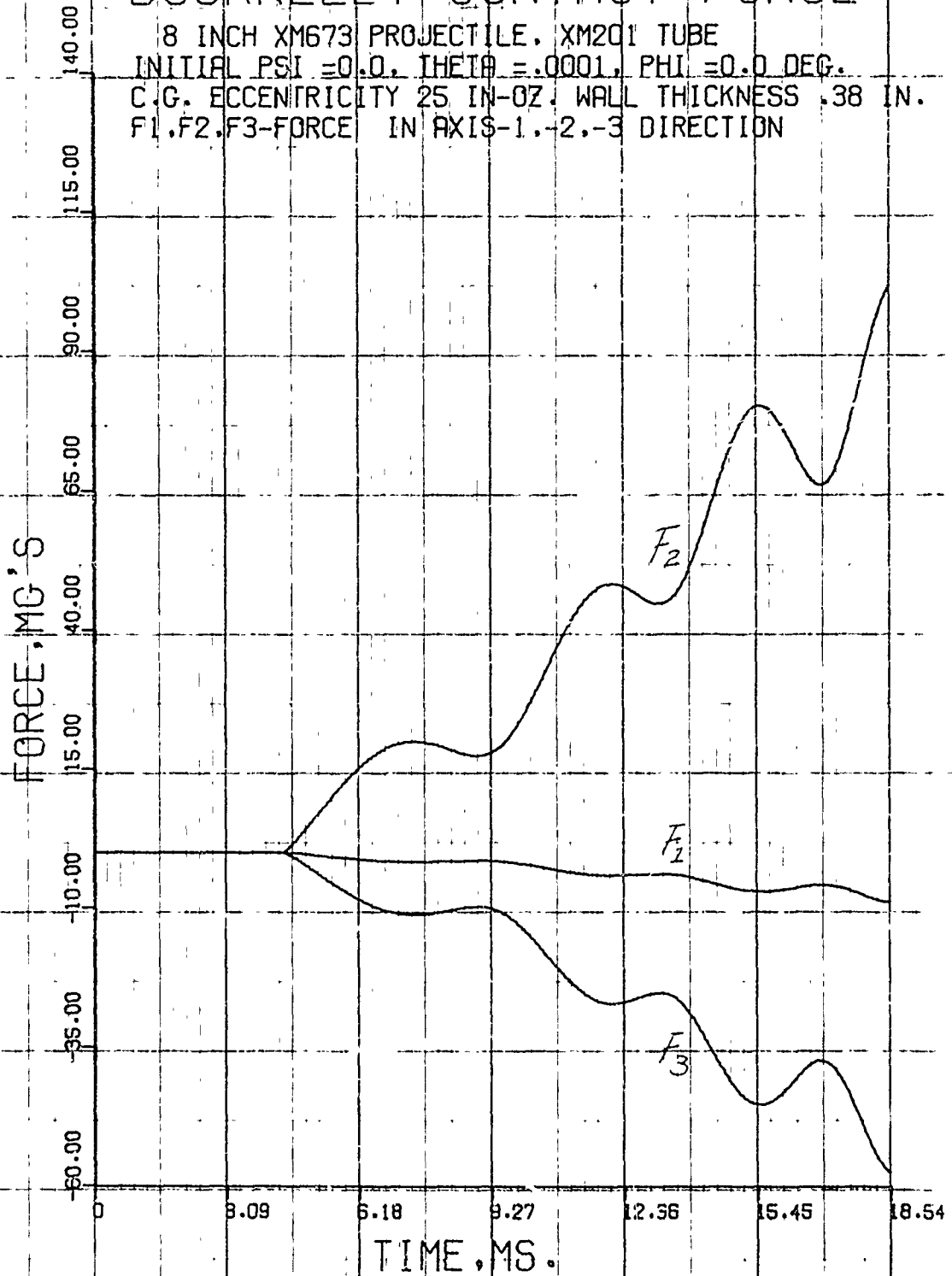


FIGURE 22b

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .42 IN.
F1, F2, F3 - FORCE IN AXIS 1, 2, 3 DIRECTION

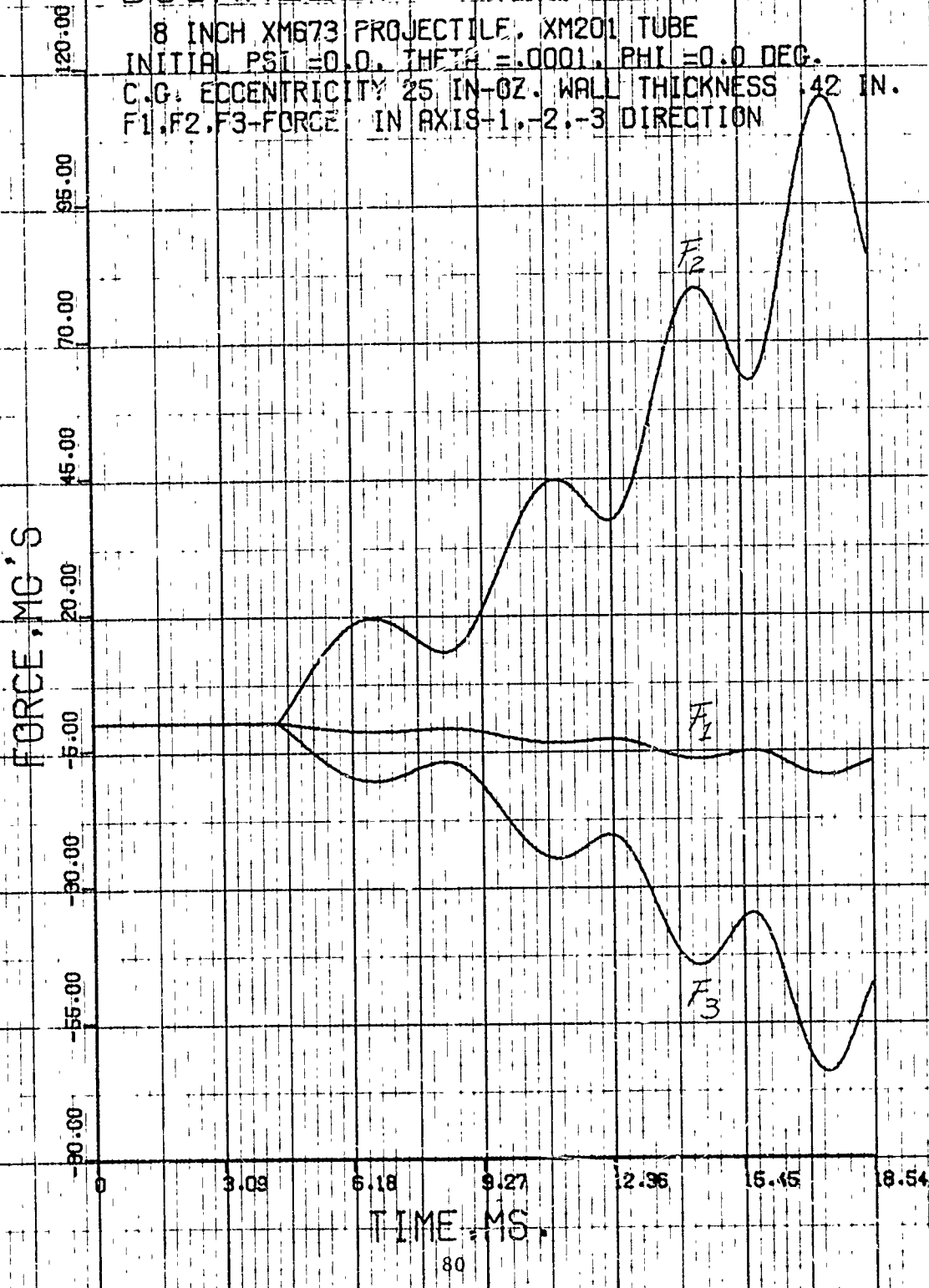


FIGURE 23a

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION

C.G. TO DRIVING BAND DISTANCE REDUCED TO $\frac{1}{3}$ ORIGINAL VALUE

FORCE, MG'S

140.00
115.00
90.00
65.00
40.00
15.00
10.00
-5.00
-30.00
-60.00

0 3.09 6.18 9.27 12.36 15.45 18.54

TIME, MS.

F₂

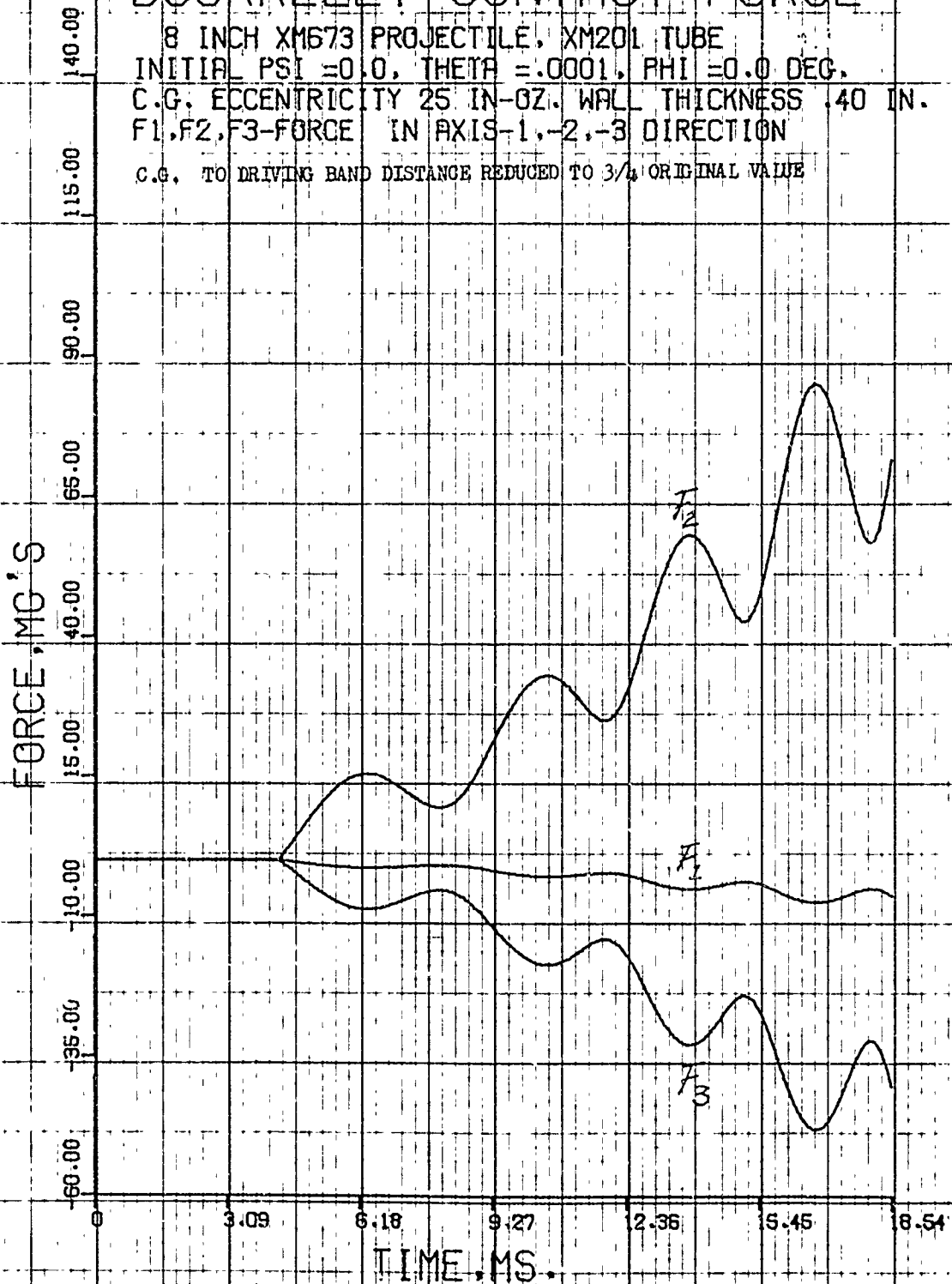
F₁

F₃

FIGURE 23b

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, XM201 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION
C.G. TO DRIVING BAND DISTANCE REDUCED TO 3/4 ORIGINAL VALUE



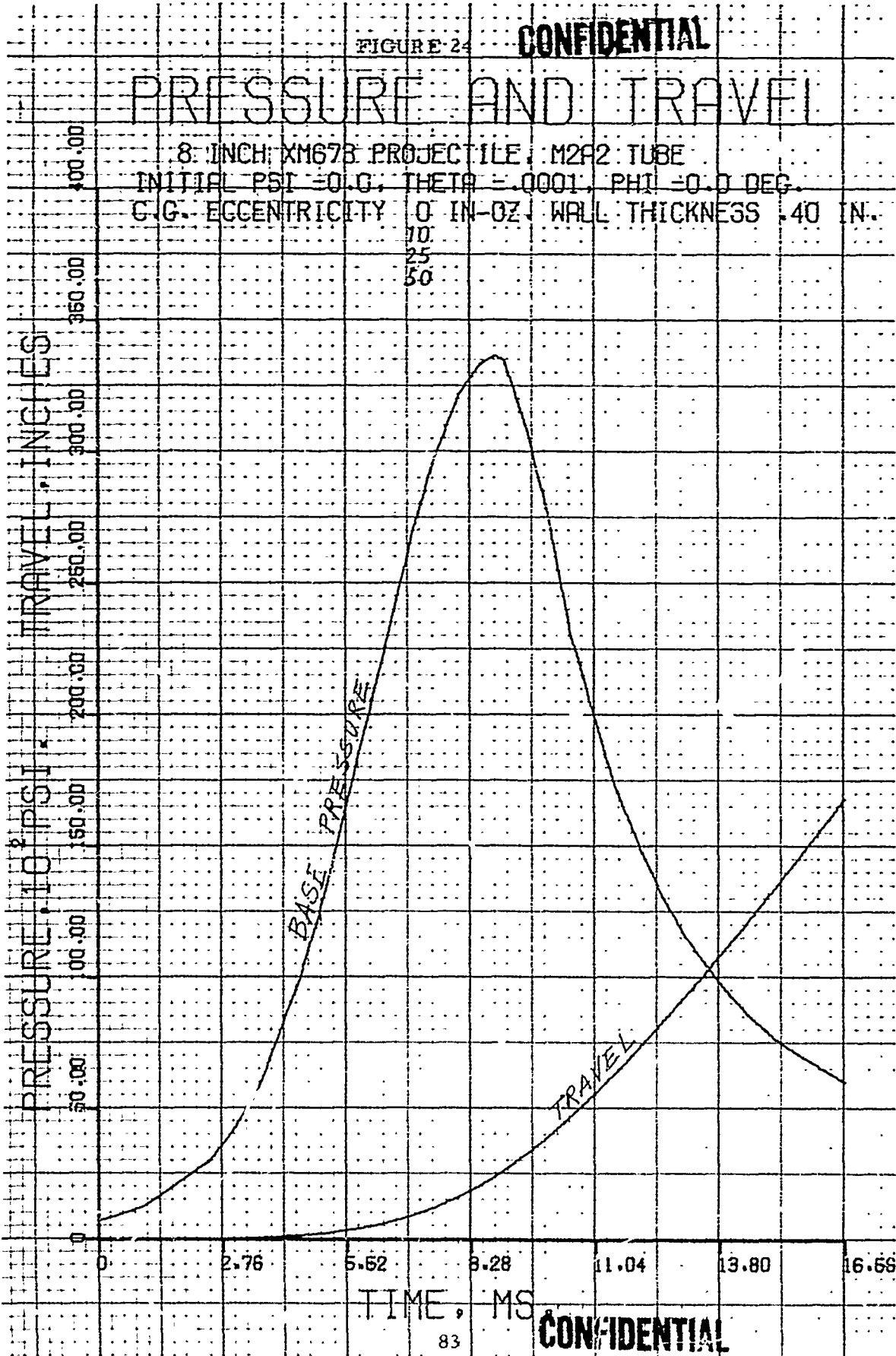
M2A2 TUBE

FIGURE 24

CONFIDENTIAL

PRESSURE AND TRAVEL

8 INCH XM67B PROJECTILE, M2A2 TUBE
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.



CONFIDENTIAL

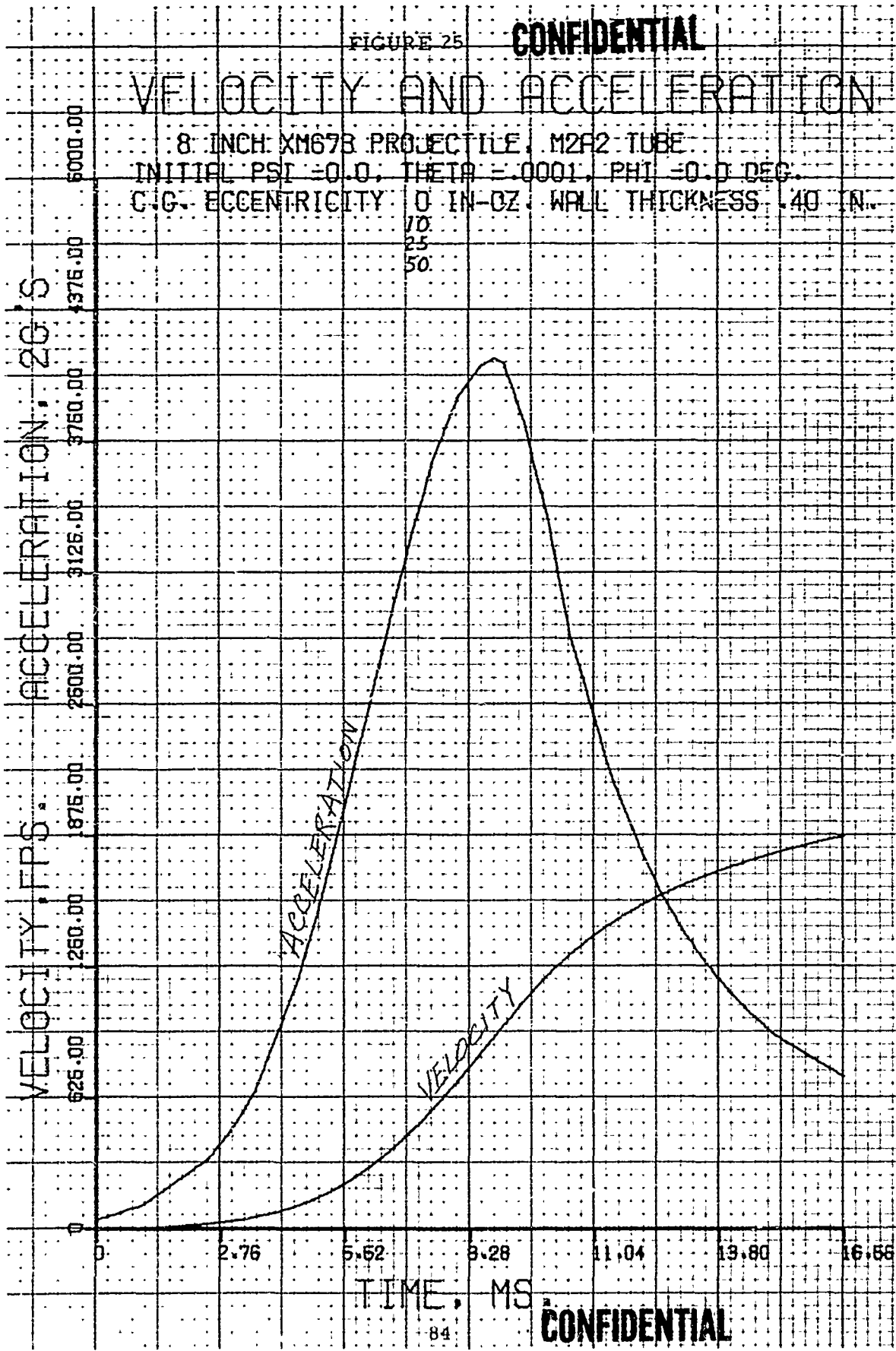
FIGURE 25

CONFIDENTIAL

VELOCITY AND ACCELERATION

8 INCH XM67B PROJECTILE, M2A2 TUBE
 INITIAL PSI = 0.0, THETA = 0.001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.

70
 25
 50

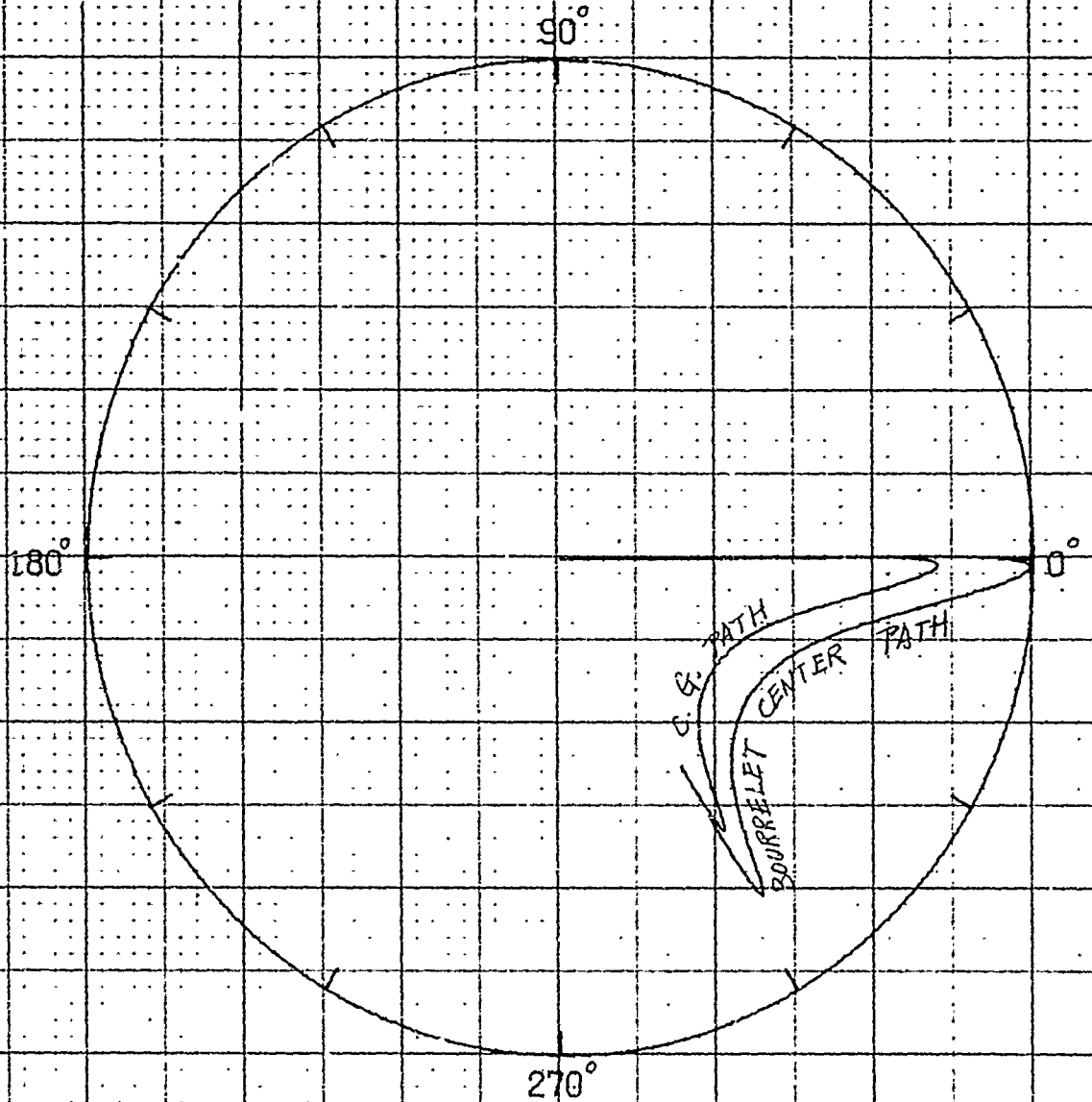


CONFIDENTIAL

FIGURE 26a

C.G. AND BOURRELET CENTER

8 INCH XM67B PROJECTILE M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.

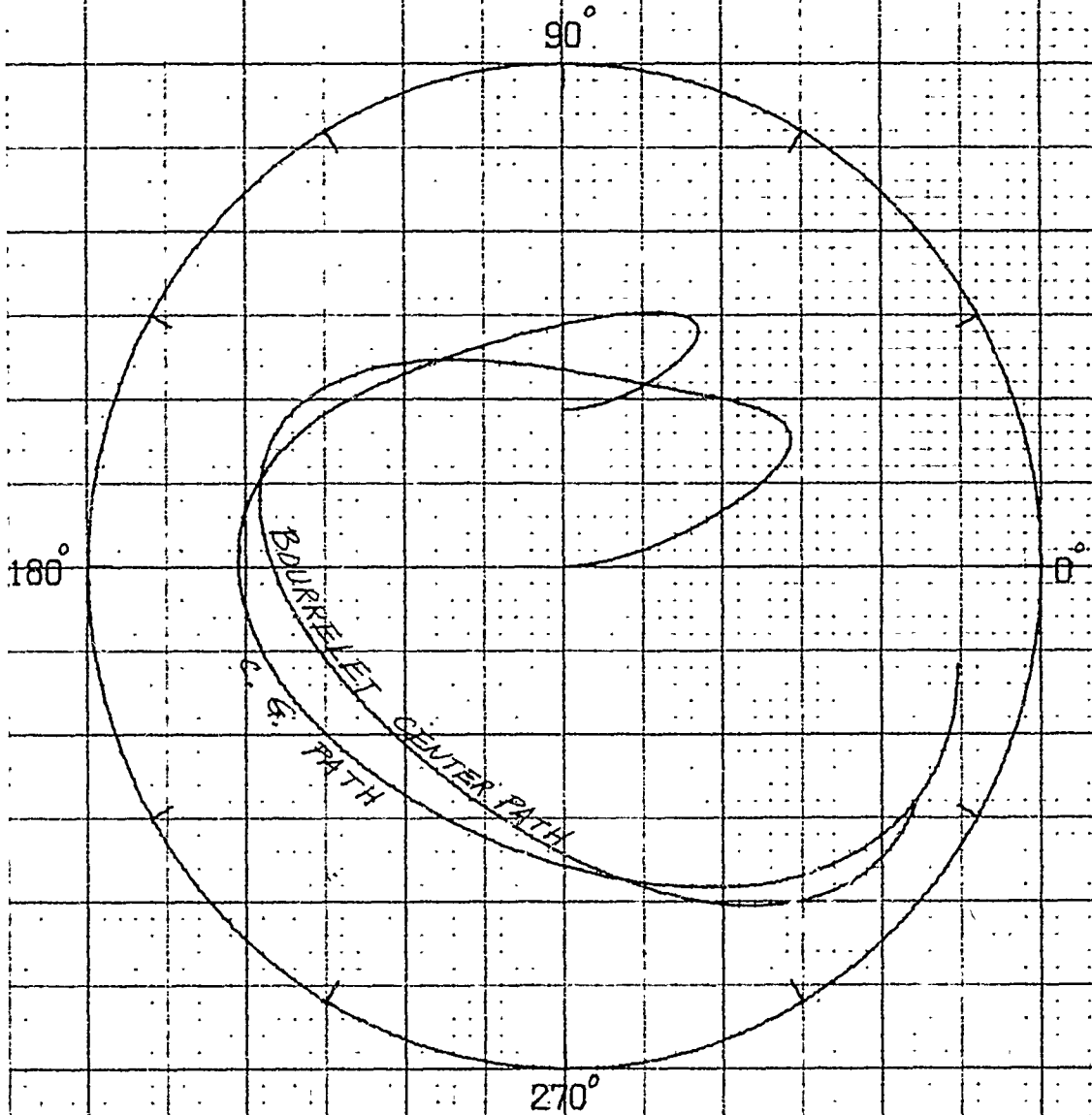


R = .0050 IN.

FIGURE 26b

C.G. AND BOURRELET CENTER

8 INCH XM678 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.

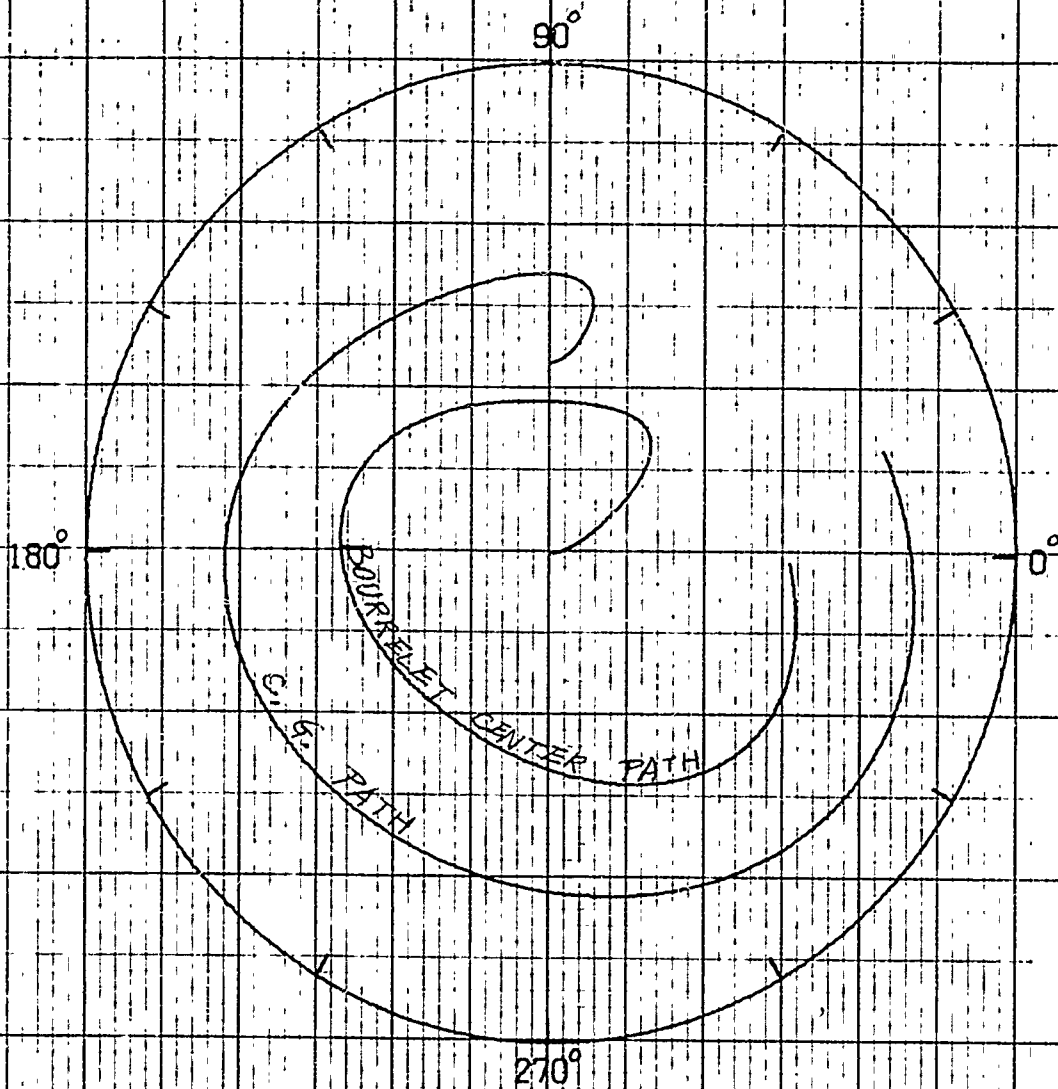


R = .0100 IN.

FIGURE 26c

C.G. AND BOURRELET CENTER

8 INCH XM67B PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

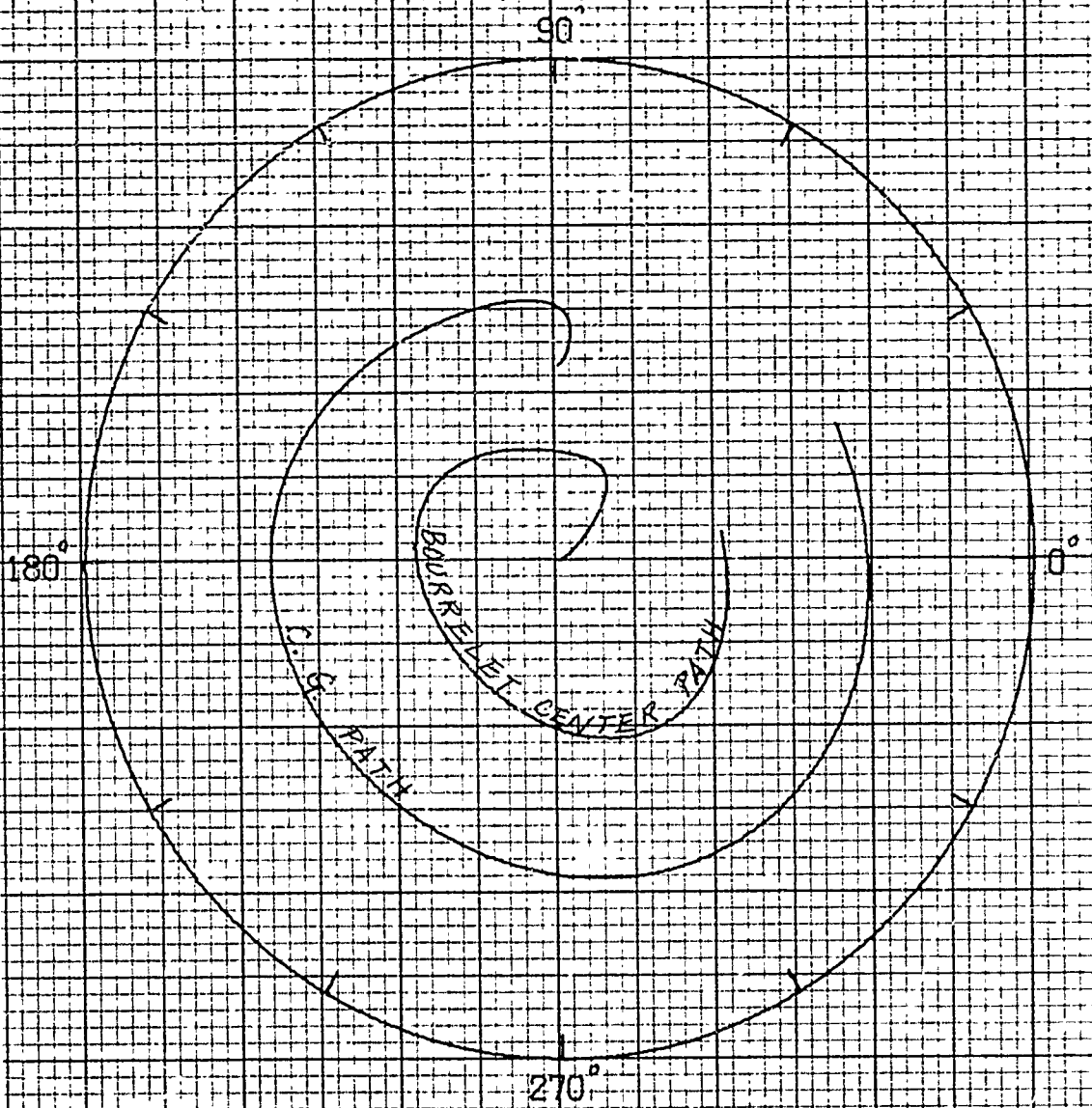


R = .0200 IN.

FIGURE 26d

C.G. AND BOURRELET CENTER

8 INCH XM678 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.



R = .0400 IN.

FIGURE 27a

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE M2A2 TUBE
 INITIAL PSI = 0.0; THETA = .0001; PHI = 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ; WALL THICKNESS .40 IN.

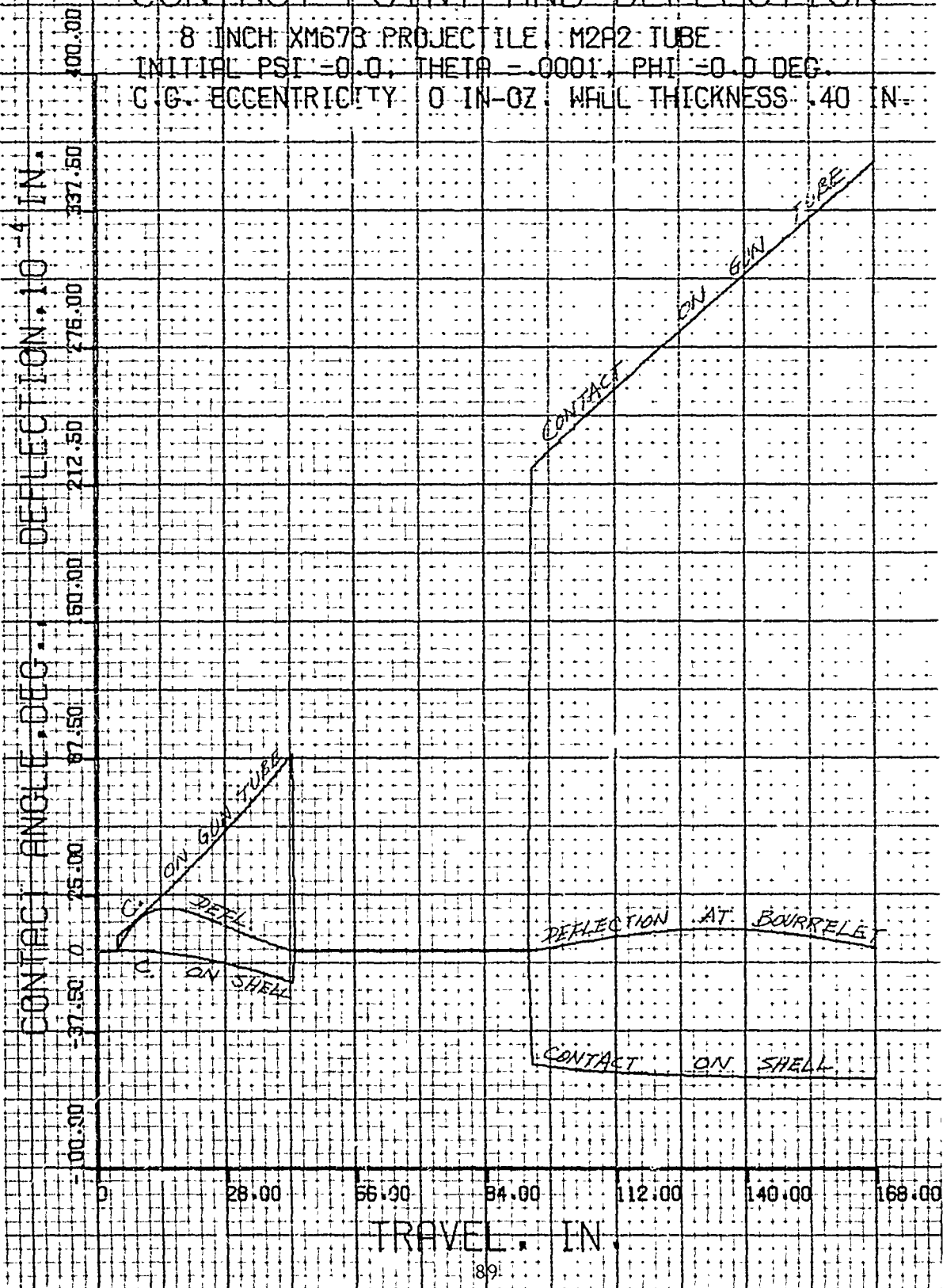


FIGURE 275

CONTACT POINT AND DEFLECTION

8 INCH XM678 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.

DEFLECTION, 10⁻⁴ IN.

CONTACT ANGLE, DEG.

450.00

387.50

325.00

262.50

200.00

137.50

75.00

12.50

-50.00

28.00

56.00

84.00

112.00

140.00

168.00

TRAVERSE, IN.

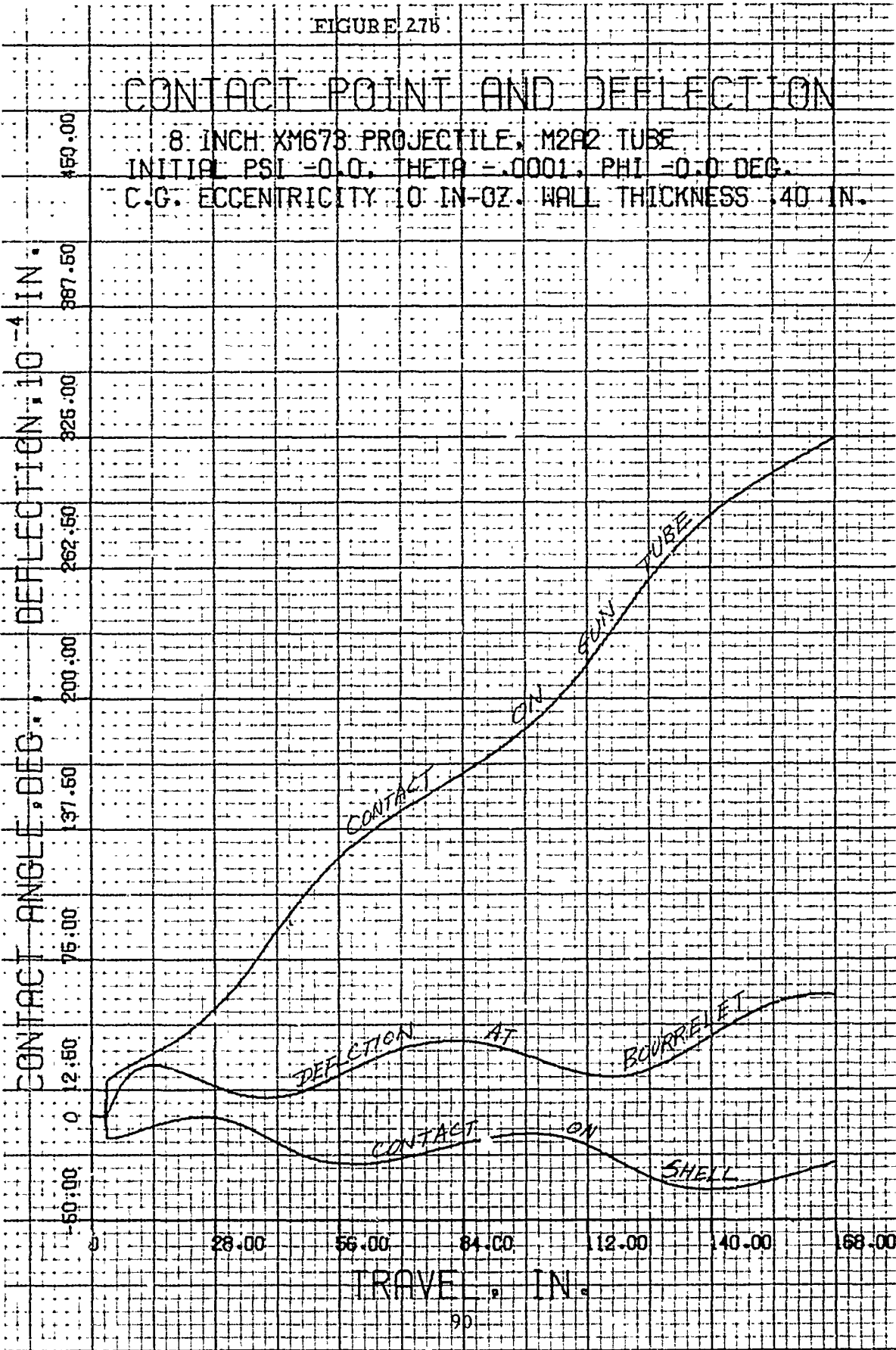


FIGURE 27c

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = 0.001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

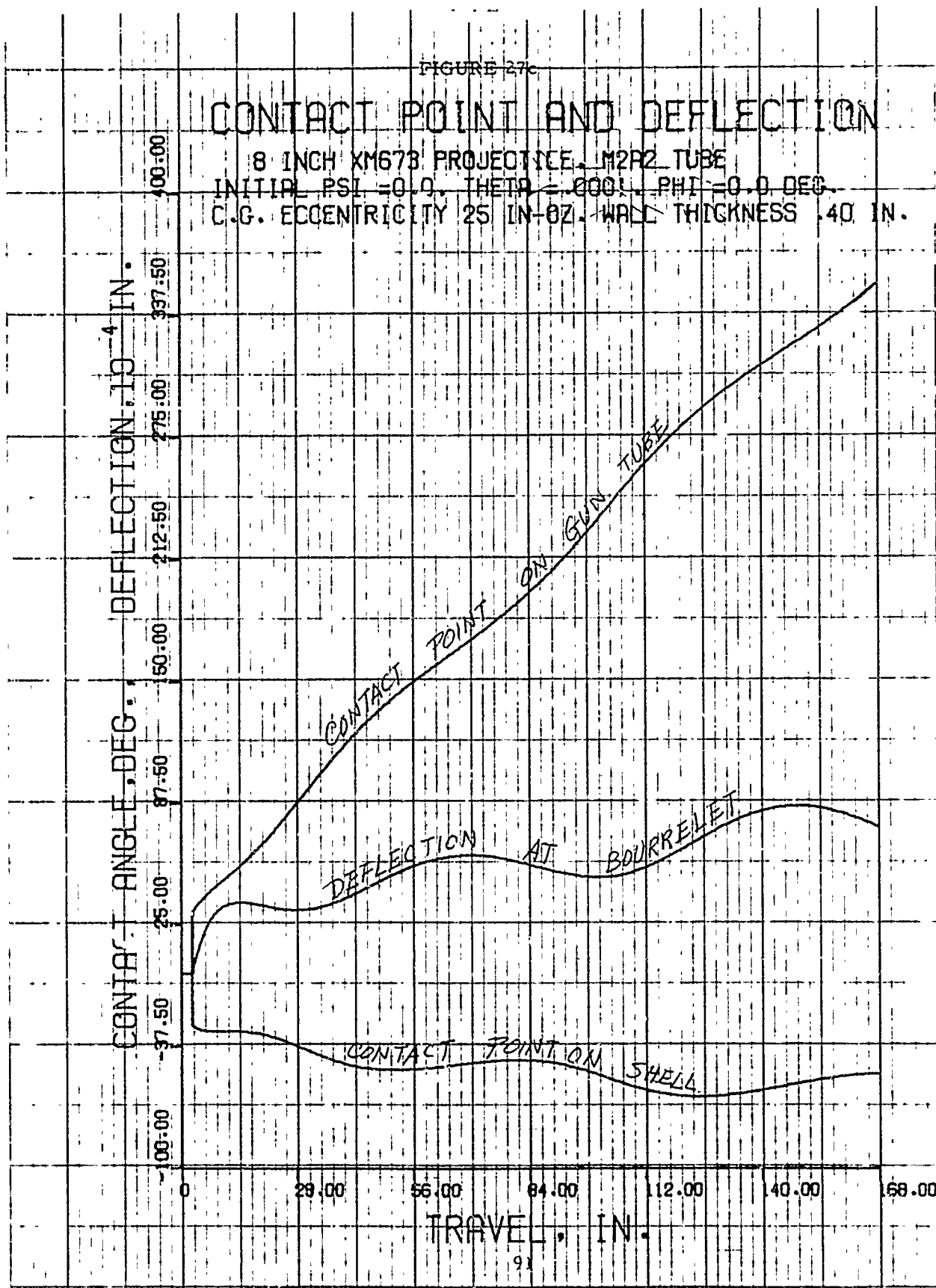


FIGURE 27d

CONTACT POINT AND DEFLECTION

8 INCH XM673 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, $\theta_{EPI} = .0001$, $\phi_{EPI} = 0.0$ DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

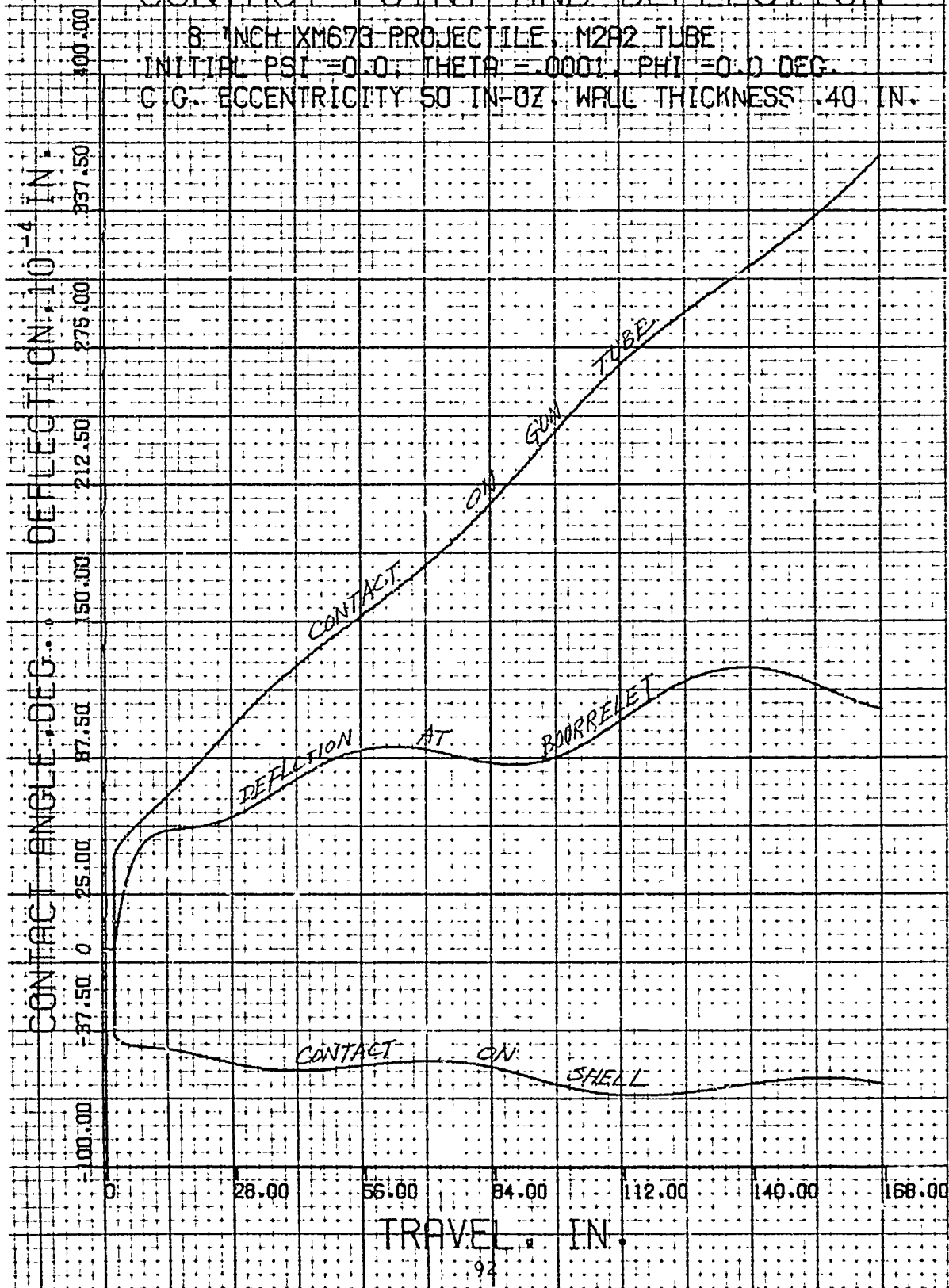


FIGURE 28a.

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.

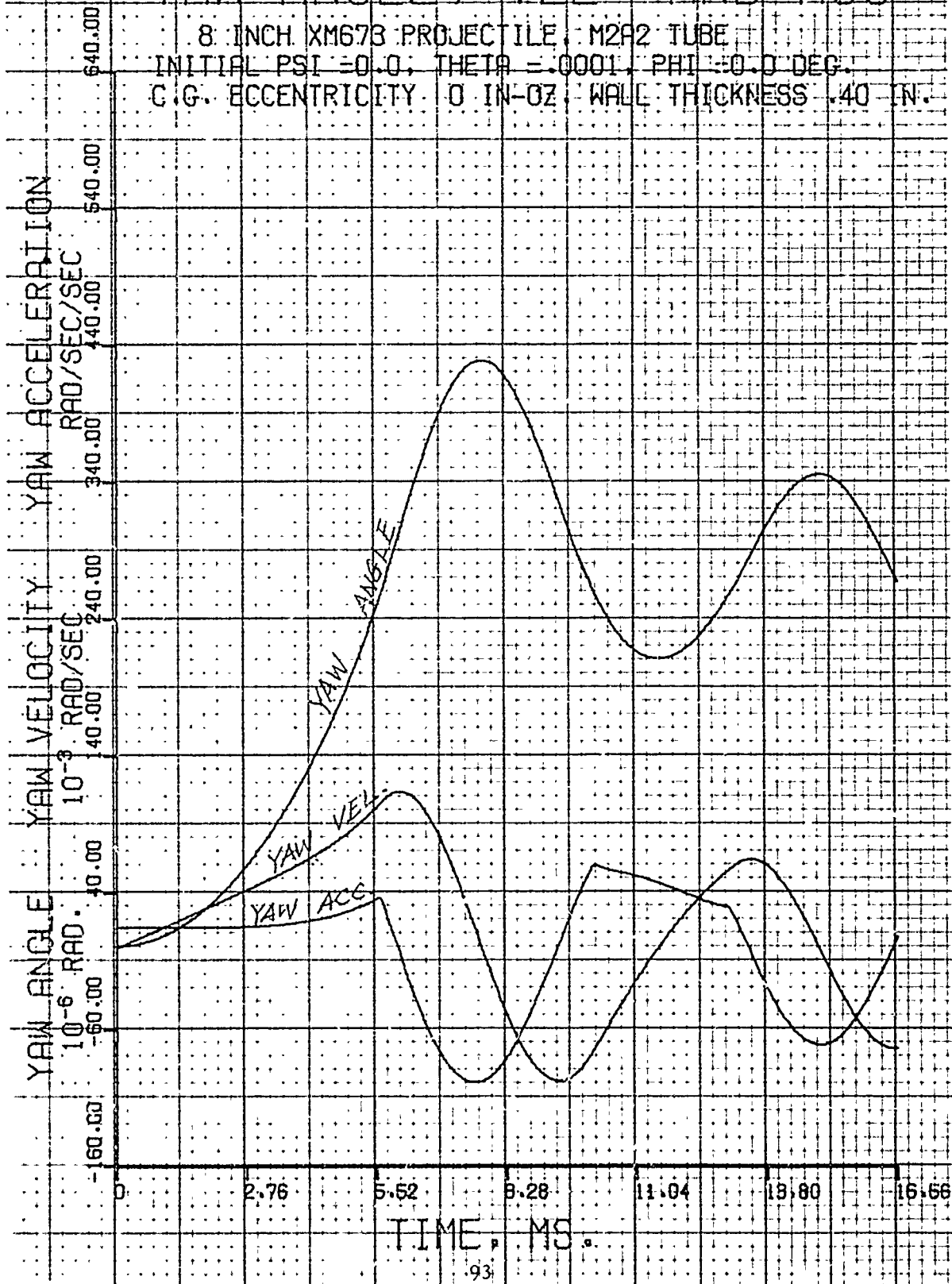


FIGURE 28b

YAW ANGLE, VEL. AND ACC.

8 INCH XM678 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-0Z, WALL THICKNESS .40 IN.

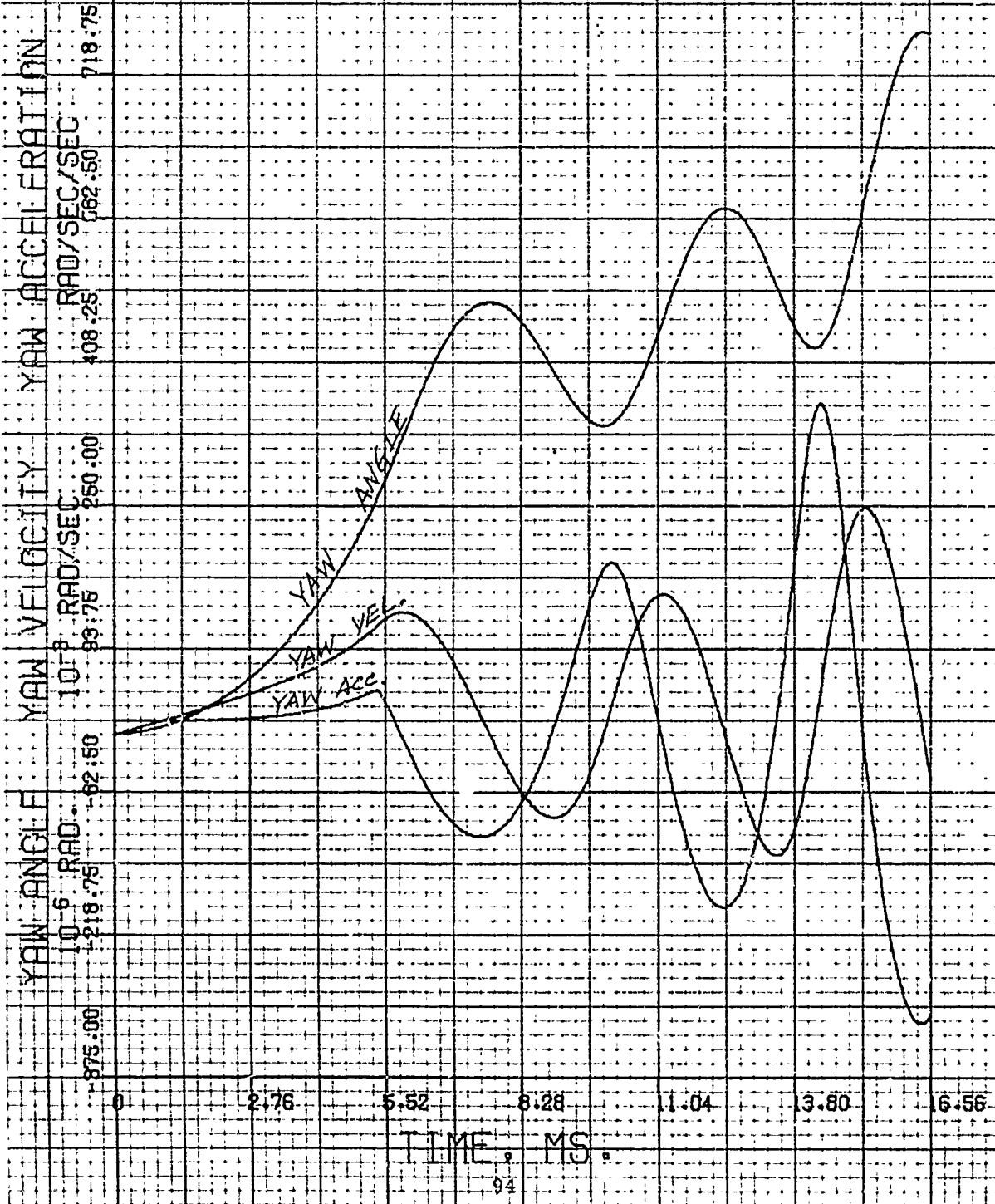


FIGURE 28c

YAW ANGLE, VEL. AND ACC.

8 INCH XM678 PROJECTILE, M2A2 TUBE
INITIAL PSI -0.0, THETA -0.001, PHI -0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

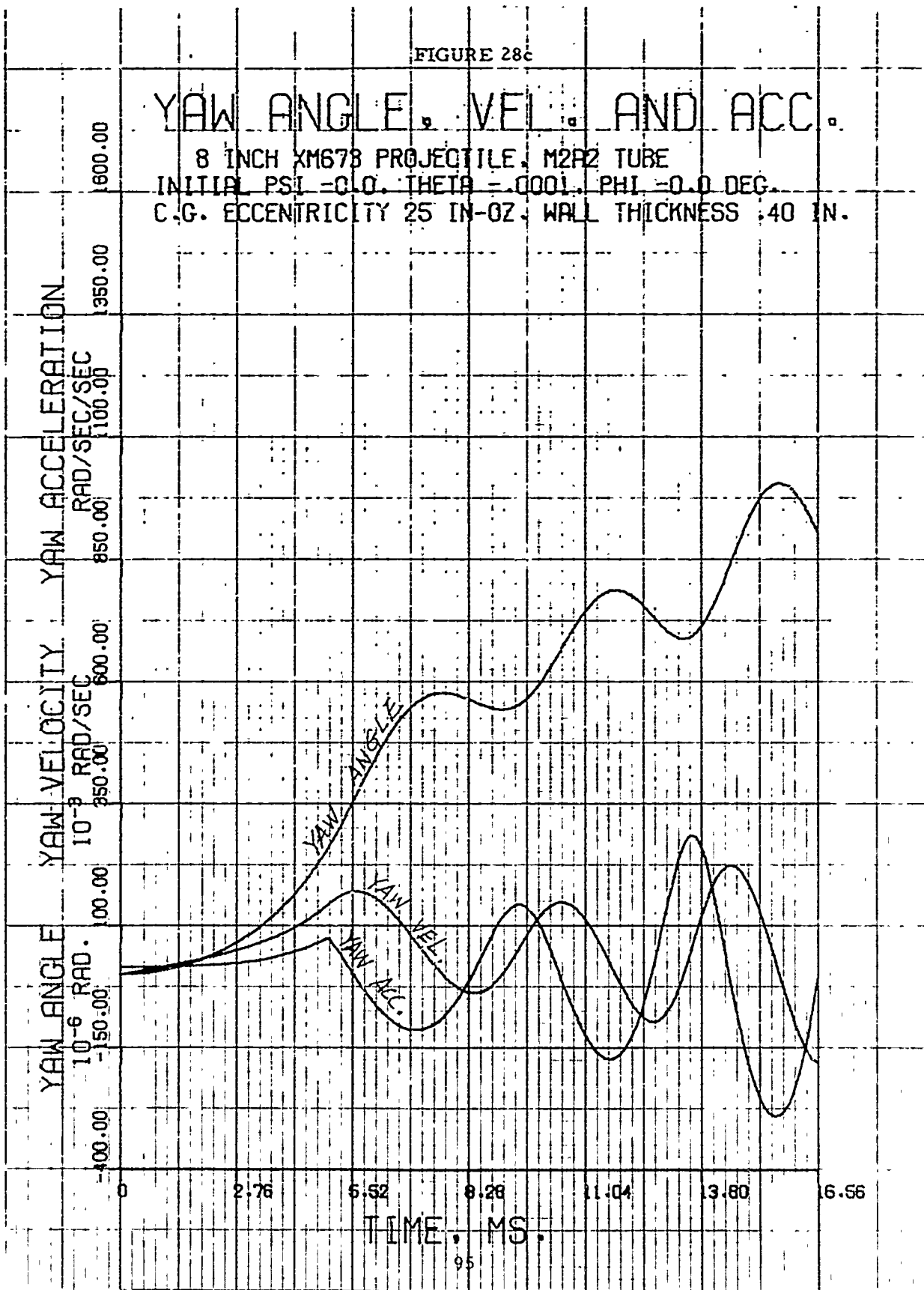


FIGURE 28c

YAW ANGLE, VEL. AND ACC.

8 INCH XM673 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

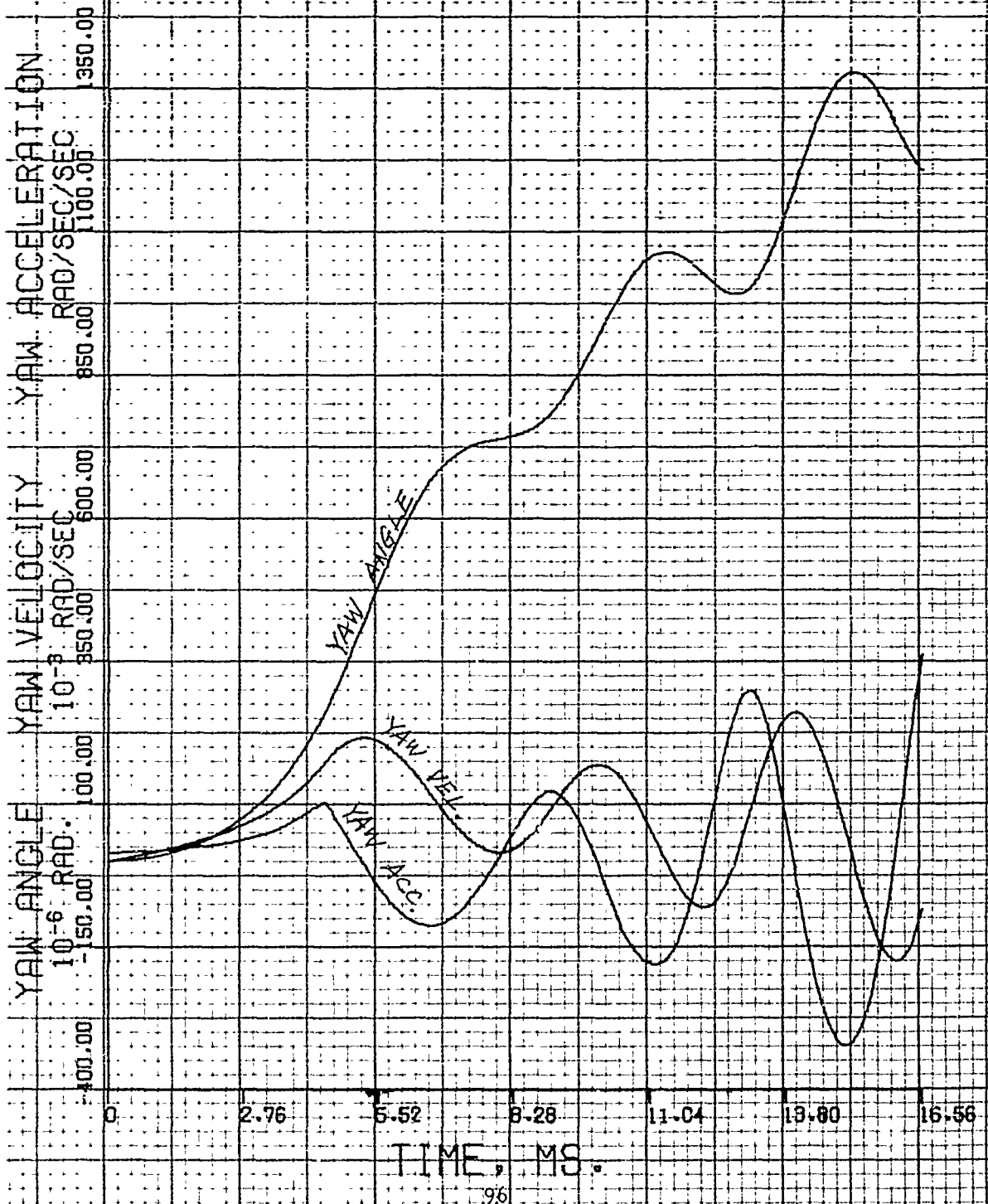


FIGURE 29a

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, M2A2 TUBE
 INITIAL PSI -0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.

CURVE 1 — ACC. AT CENTER OF GRAVITY
 2 — ACC. AT BOURRELET CENTER
 3 — ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
 4 — 7.5
 5 — 5.0
 6 — 2.5

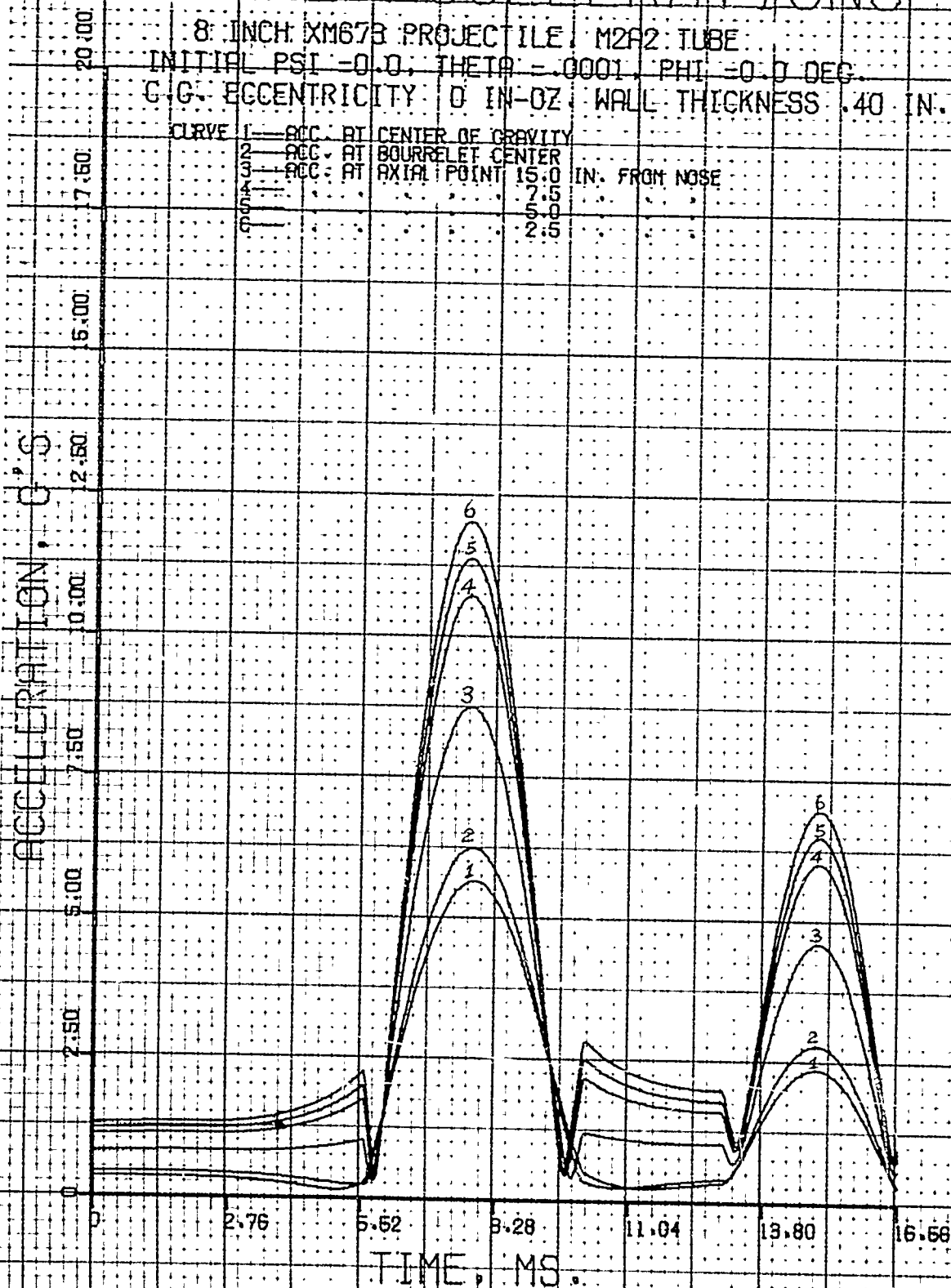


FIGURE 29b

NORMA ACCELERATIONS

8 INCH XM673 PROJECTILE, M2A2 TUBE
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 10 IN-OZ., WALL THICKNESS .40 IN.

CURVE 1---ACC. AT CENTER OF GRAVITY
 2---ACC. AT BOCKET CENTER
 3---ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
 4---7.5
 5---5.0
 6---2.5

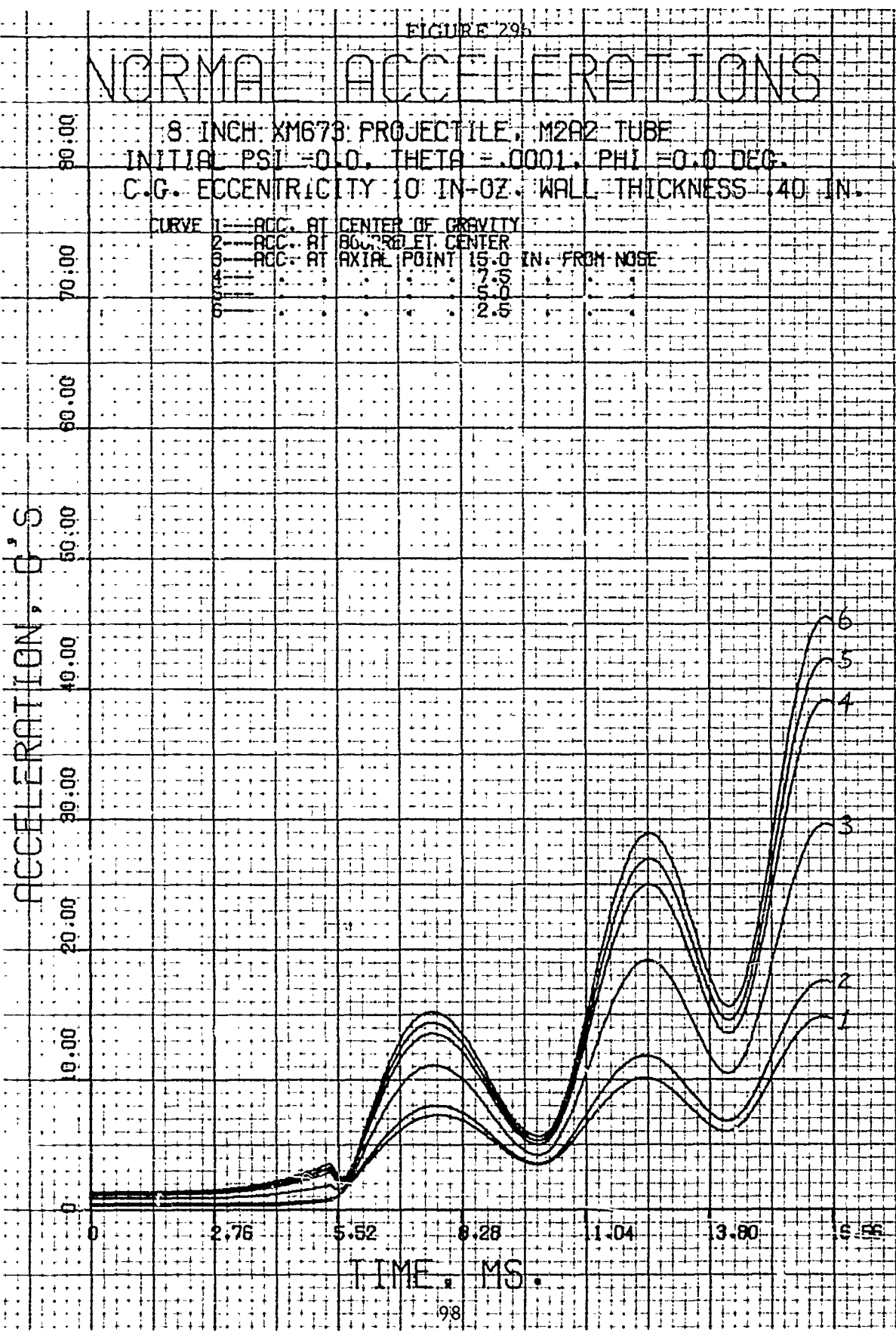


FIGURE 29c

NORMAL ACCELERATIONS

8 INCH XM678 PROJECTILE, M2F2 TUBE
INITIAL PSI -0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

CURVE 1---ACC. AT CENTER OF GRAVITY
2---ACC. AT BOURRELET CENTER
3---ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
4---" " " " " " 7.5
5---" " " " " " 5.0
6---" " " " " " 2.5

ACCELERATION, G'S

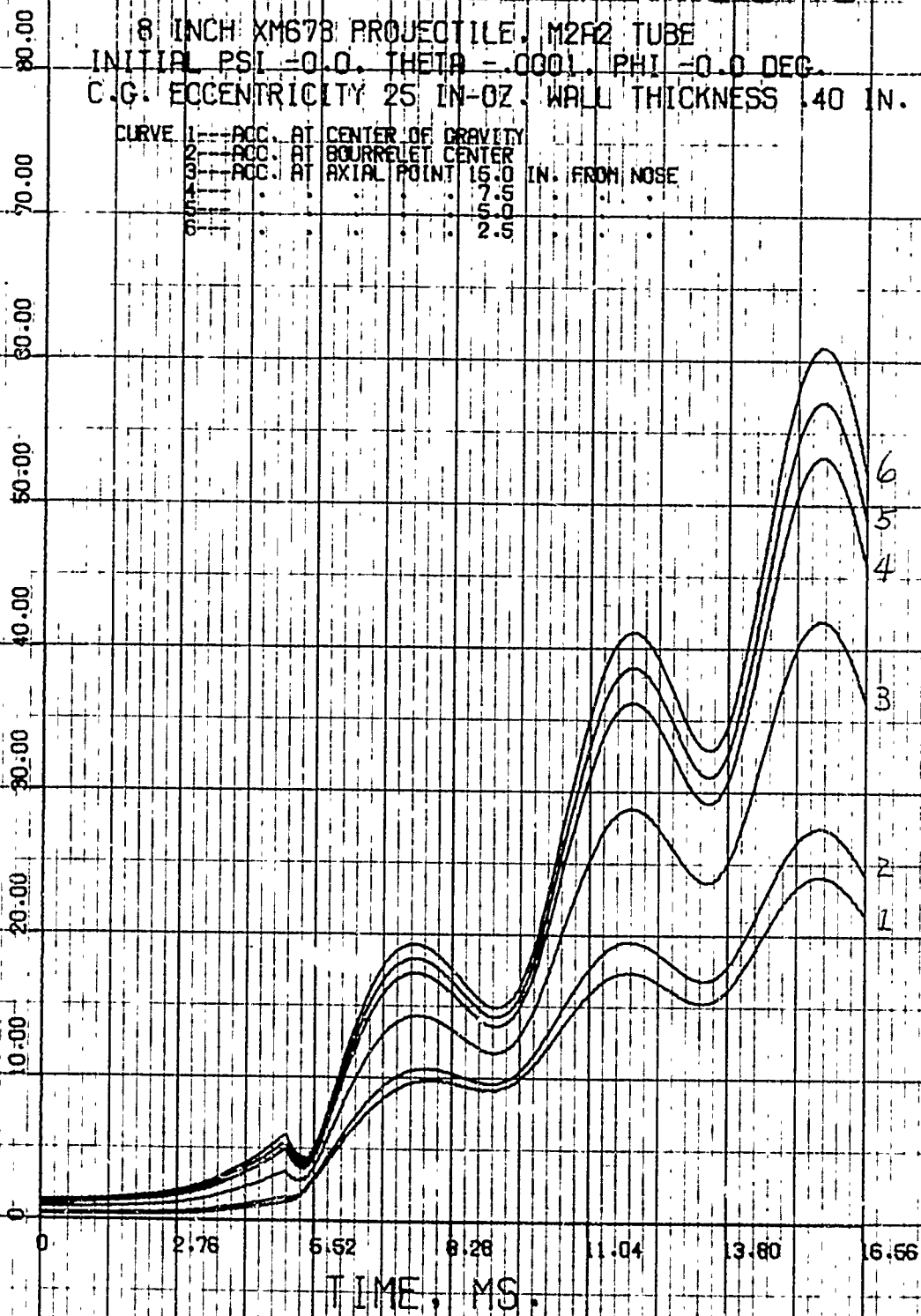


FIGURE 29d

NORMAL ACCELERATIONS

8 INCH XM673 PROJECTILE, M2A2 TUBE
 INITIAL PSI = 0.0, $\Theta_{AIR} = .0001$, $\Phi = 0.0$ DEG.
 C.G. ECCENTRICITY 50 IN-OZ WALL THICKNESS .40 IN.

CURVE 1	ACC. AT CENTER OF GRAVITY
2	ACC. AT GOURRELET CENTER
3	ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
4	7.5
5	5.0
6	2.6

ACCELERATION, G'S

100.00
87.50
75.00
62.50
50.00
37.50
25.00
12.50
0

TIME, MS.

0 2.76 5.52 8.28 11.04 13.80 16.56

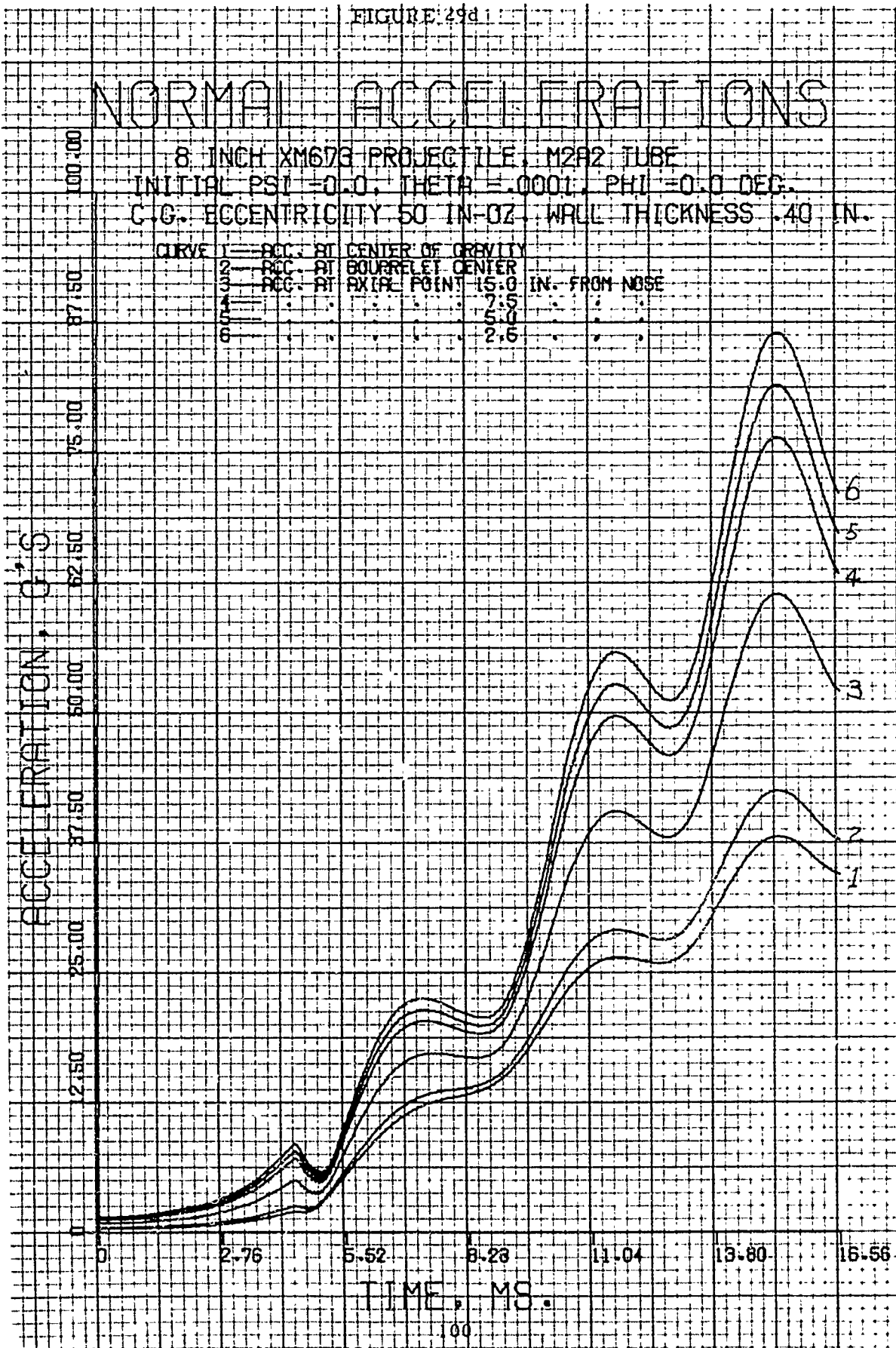


FIGURE 30a

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, M2A2 TUBE
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.
F₁, F₂, F₃ - FORCE IN AXIS-1, -2, -3 DIRECTION

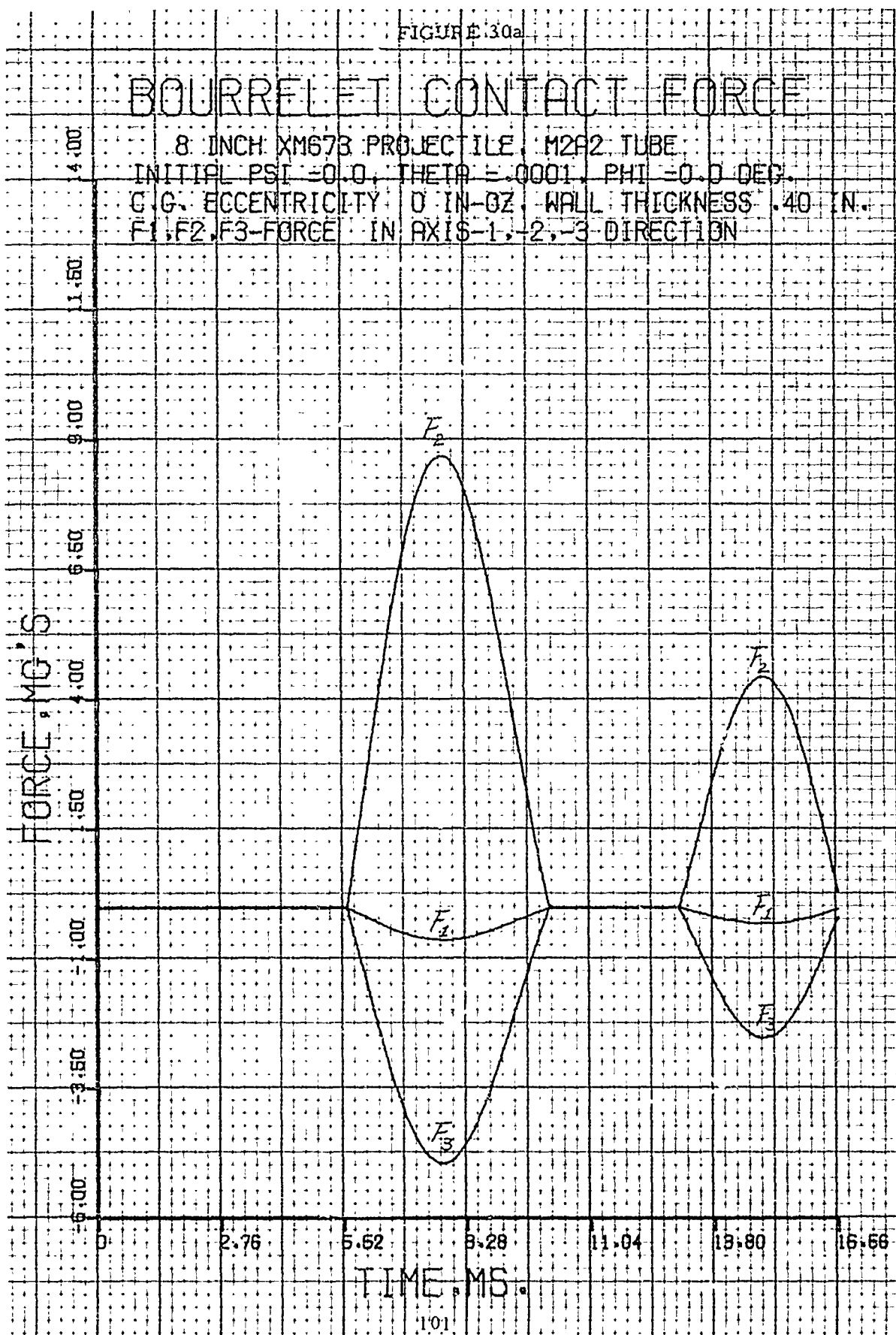


FIGURE 30b

BOURRELET CONTACT FORCE

8 INCH XM678 PROJECTILE, M2A2 TUBE
INITIAL PSD = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.
F1, F2, F3 FORCE IN AXIS 1, 2, 3 DIRECTION

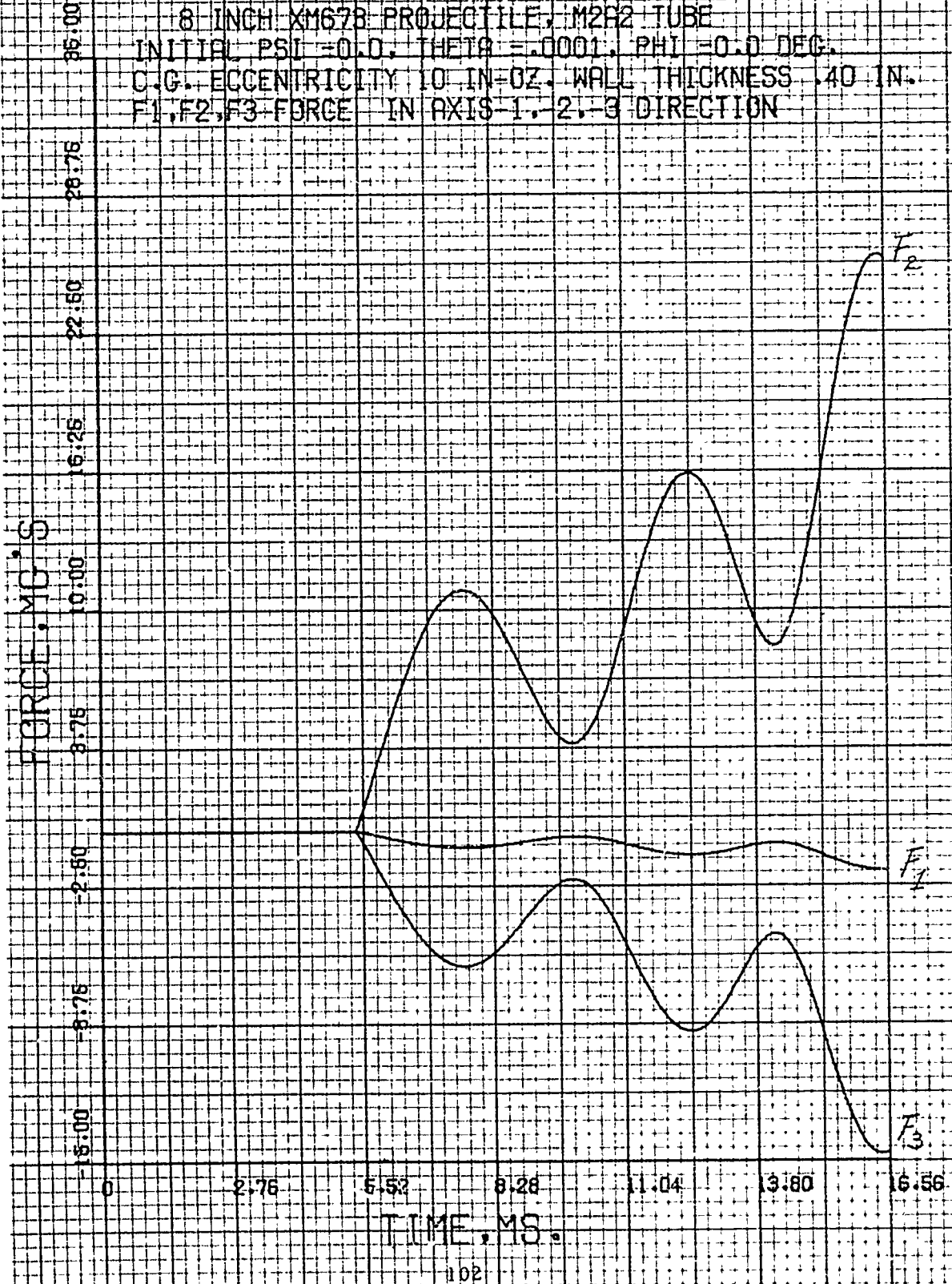


FIGURE 30c

BOURRELET CONTACT FORCE

8 INCH XM67B PROJECTILE, M2A2 TUBE
INITIAL PSI -0.0, THETA -0.001, PHI -0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS -1, -2, -3 DIRECTION

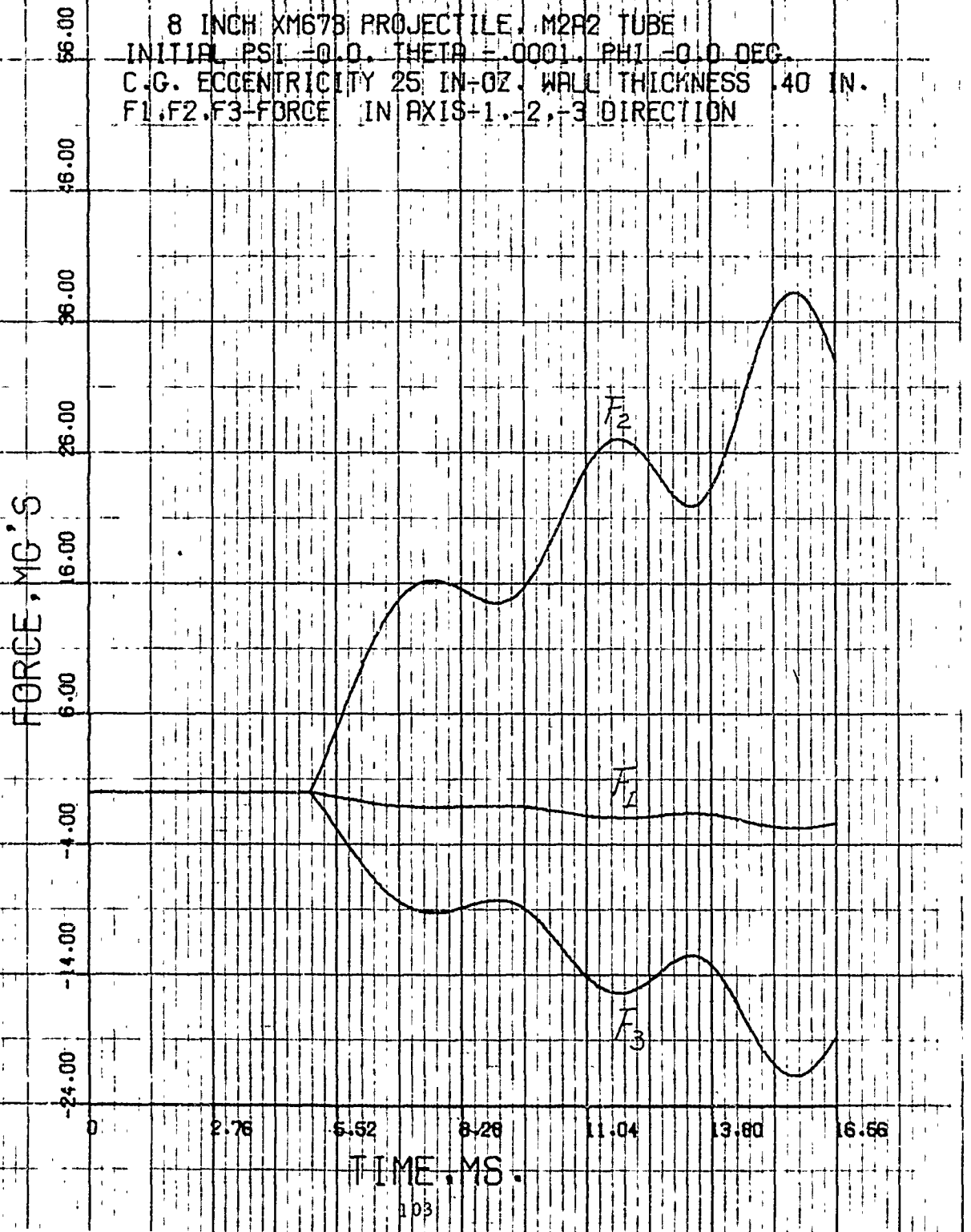
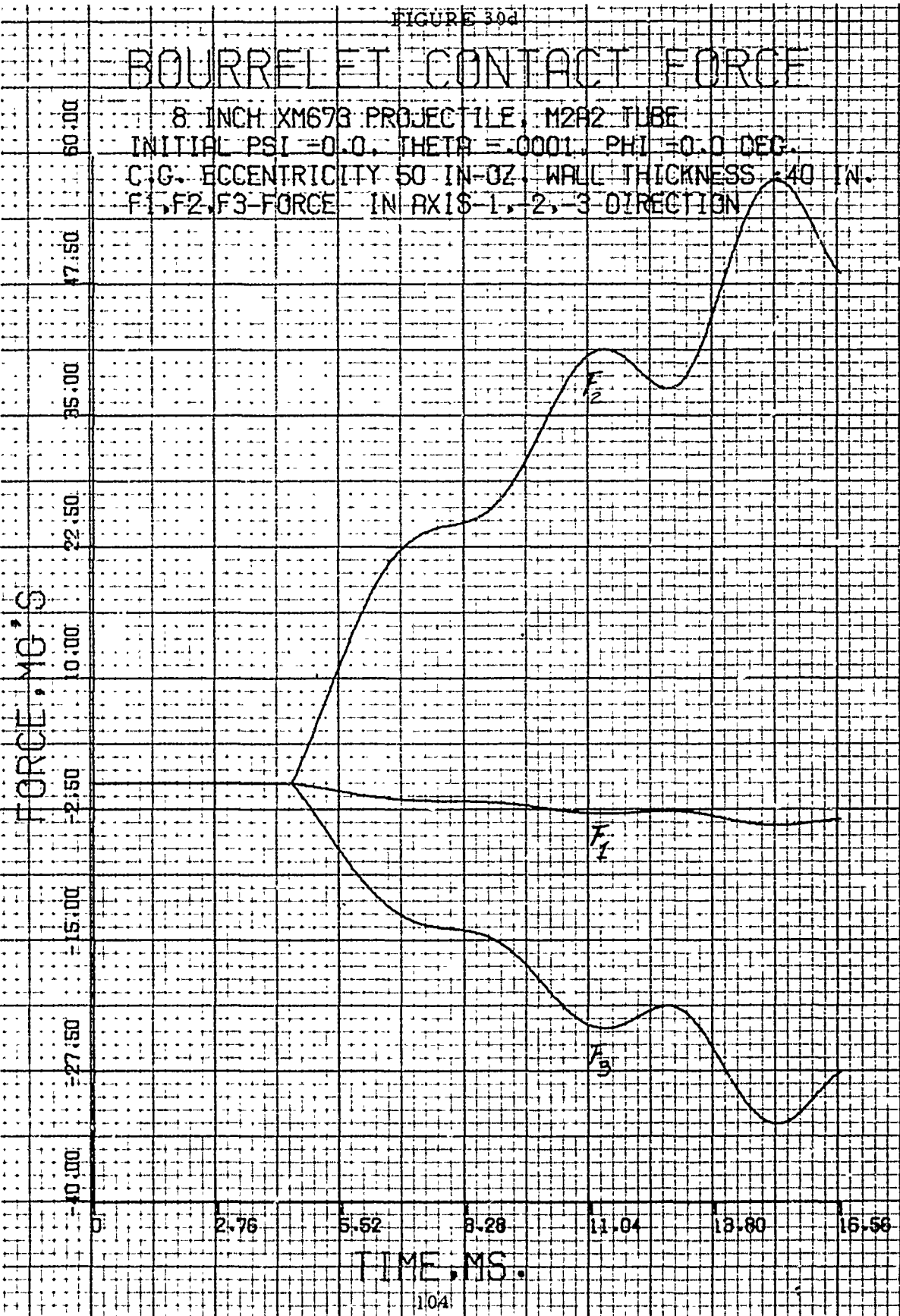


FIGURE 30d

BOURRELET CONTACT FORCE

8 INCH XM673 PROJECTILE, M2A2 TUBE
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.
 F₁, F₂, F₃ FORCE IN AXIS 1, 2, 3 DIRECTION



MCLG GUN

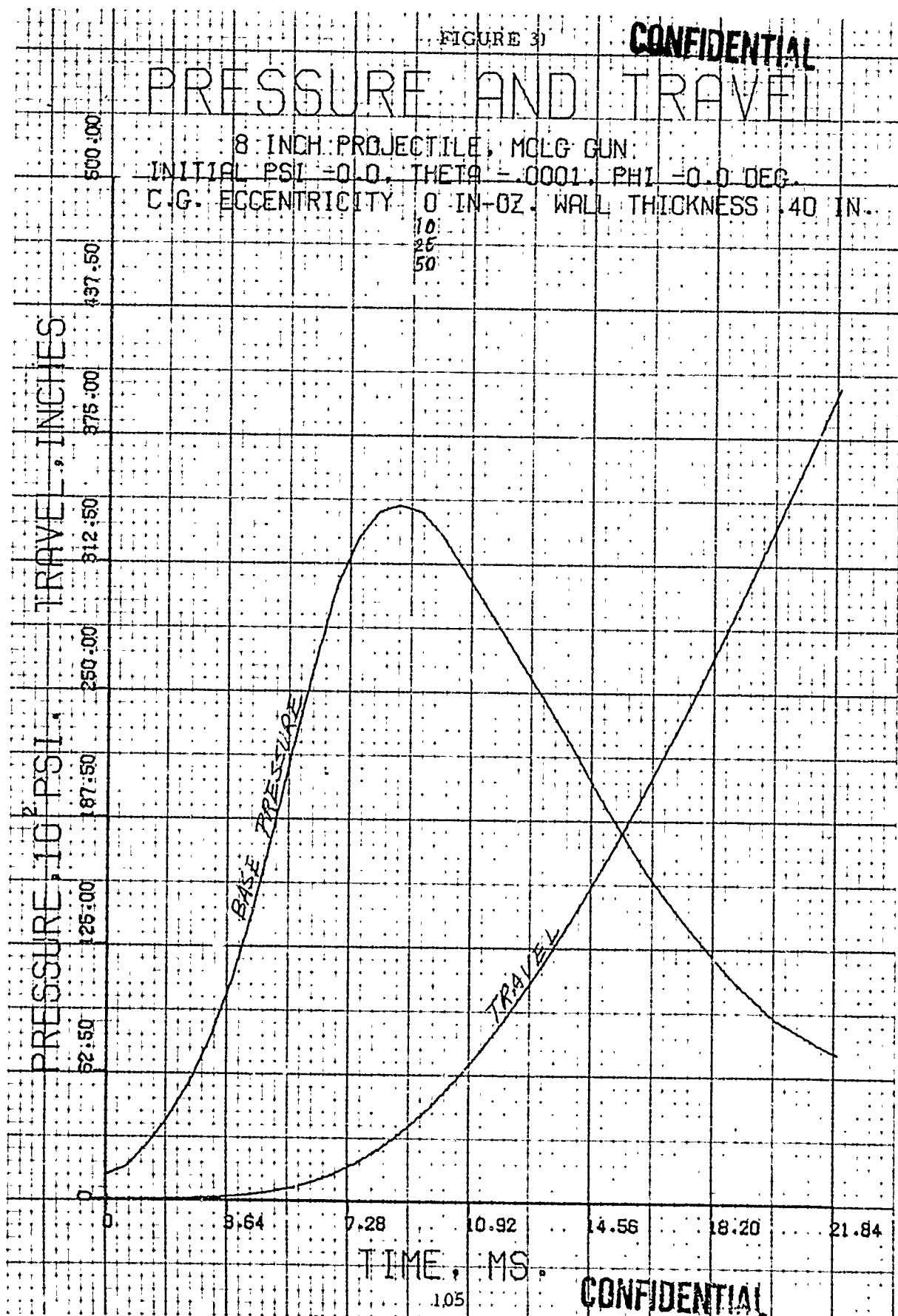
FIGURE 3)

CONFIDENTIAL

PRESSURE AND TRAVEL

8 INCH PROJECTILE, MCLG GUN
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.

10
 25
 50



CONFIDENTIAL

FIGURE 32

CONFIDENTIAL

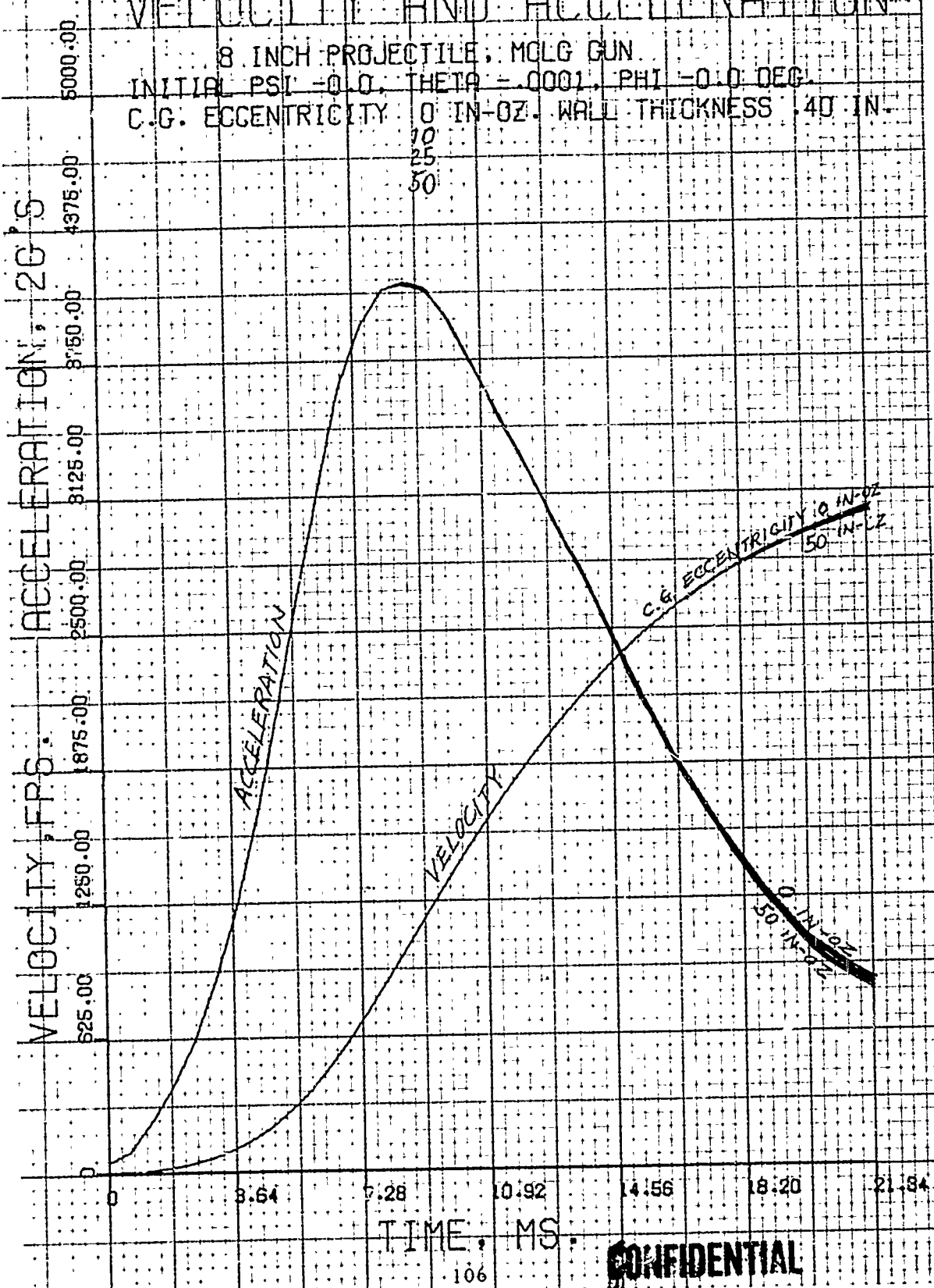
VELOCITY AND ACCELERATION

8 INCH PROJECTILE; MCLG GUN

INITIAL PSI -0.0, THETA - .0001, PHI -0.0 DEG.

C.G. ECCENTRICITY: 0 IN-OZ. WALL THICKNESS .40 IN.

10
25
50



TIME, MS.

CONFIDENTIAL

FIGURE 33a

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE, MCG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.

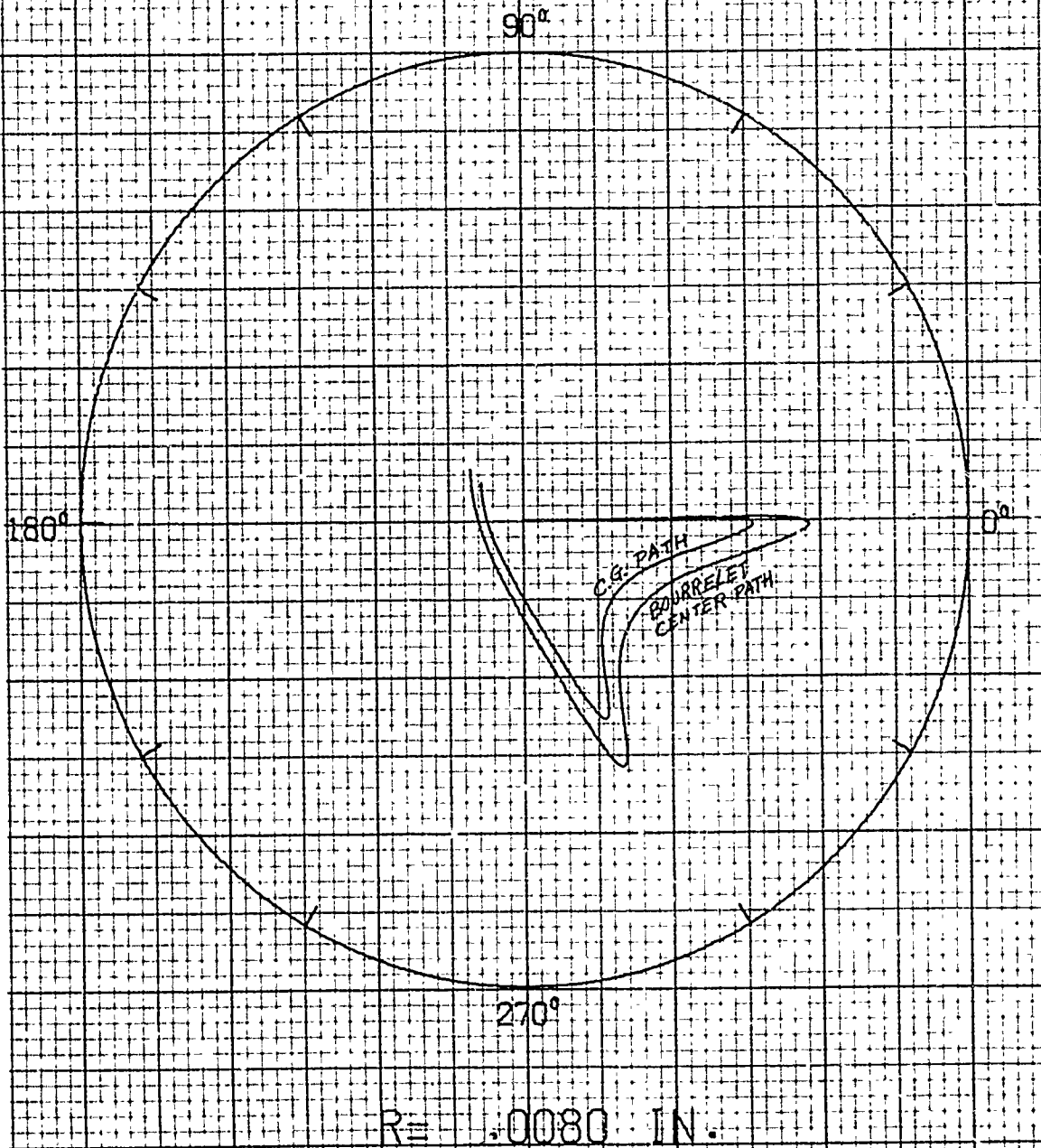
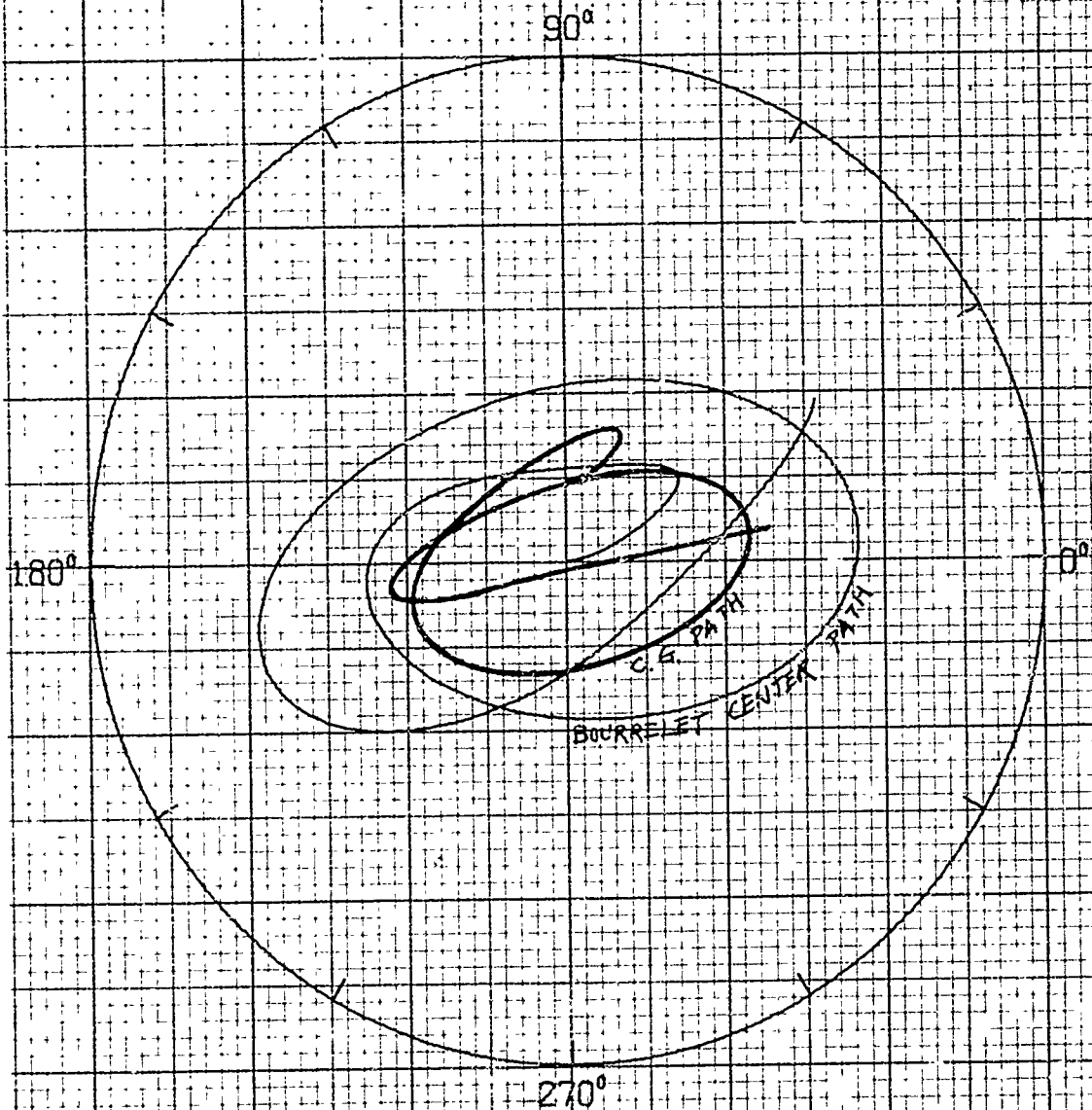


FIGURE 33b

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE, MQLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.

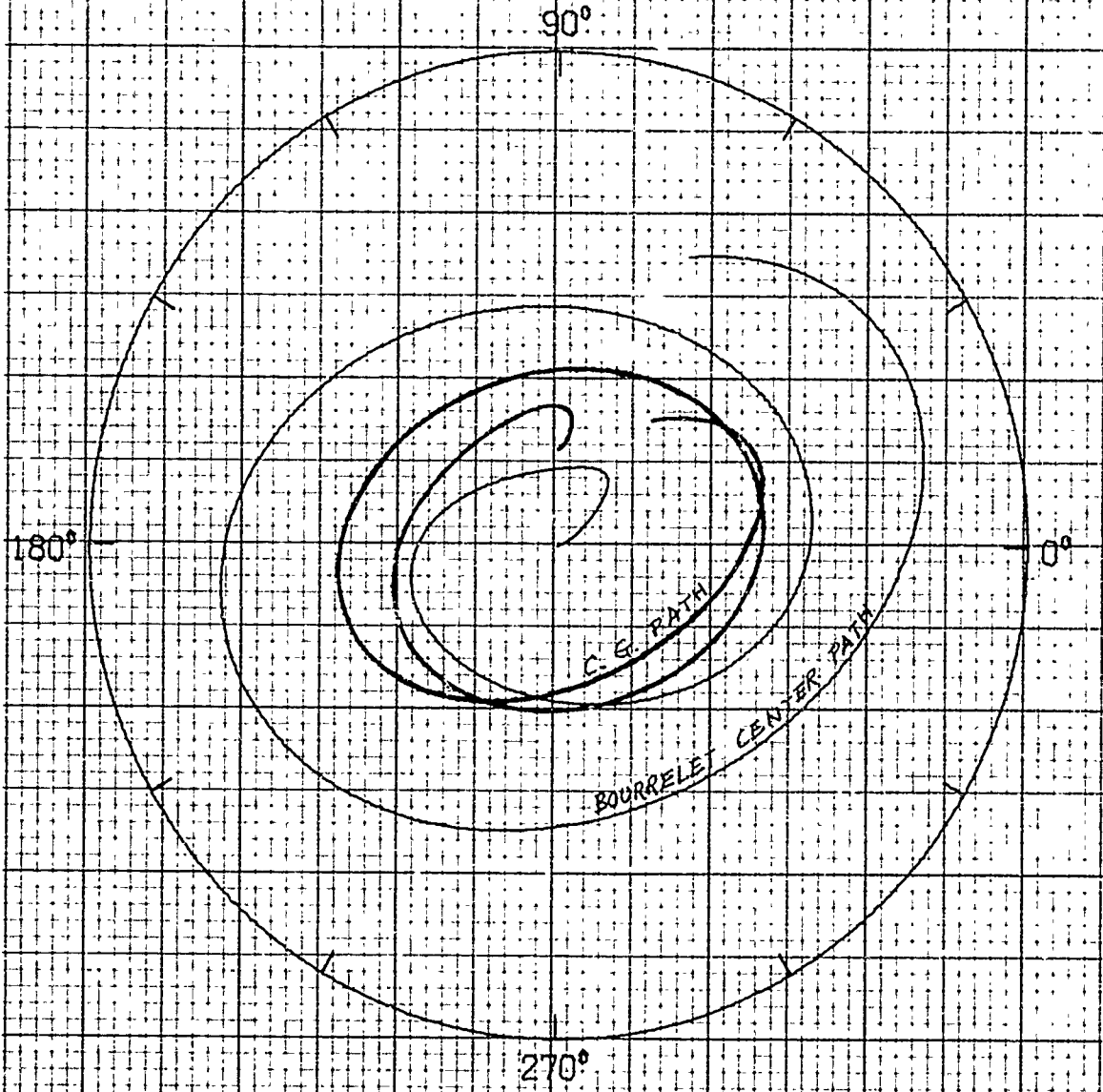


R = .6200 IN.

FIGURE 35c

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE, MCLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-0Z, WALL THICKNESS .40 IN.



R = .0400 IN.

FIGURE 33d

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE; MCG-GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.

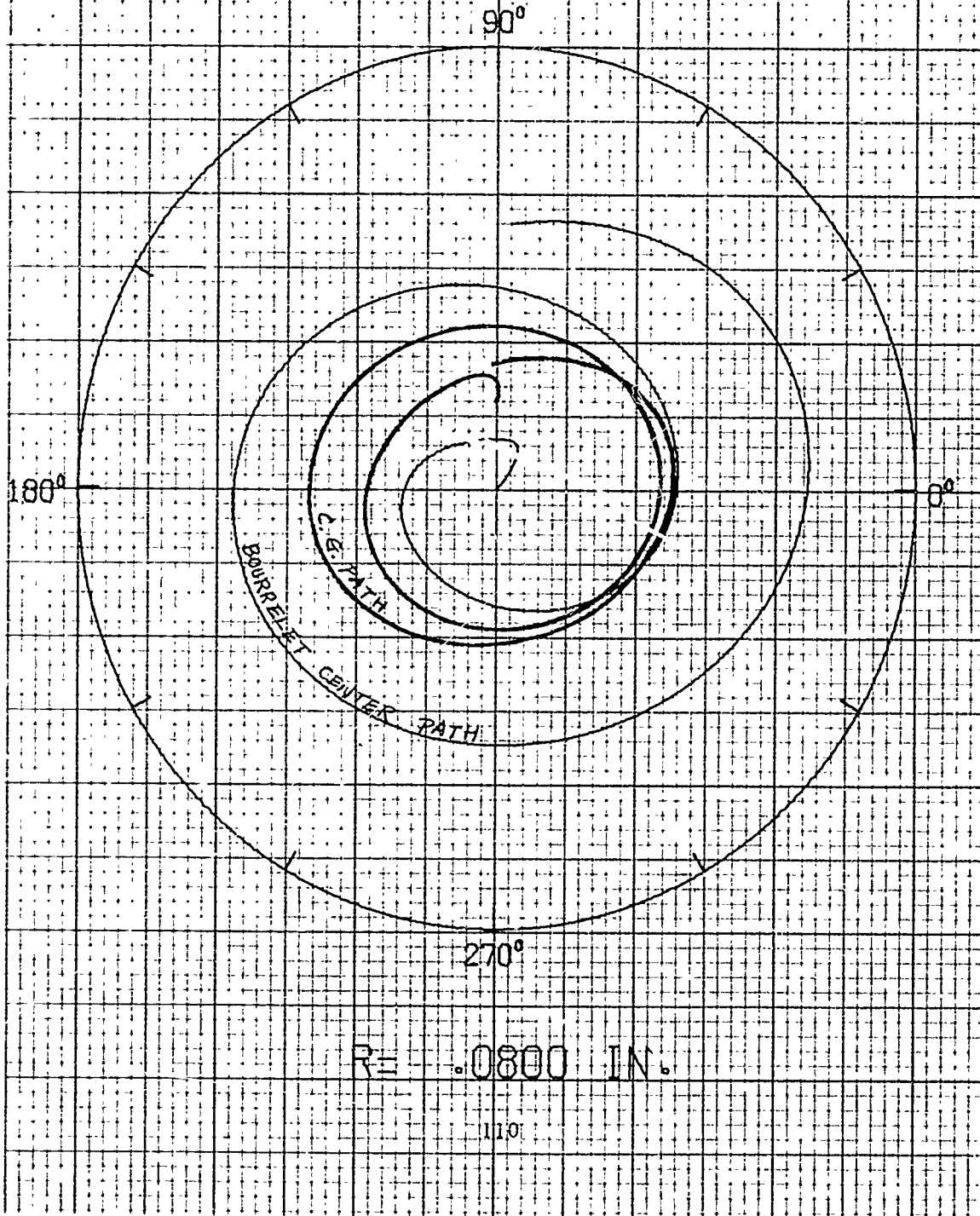


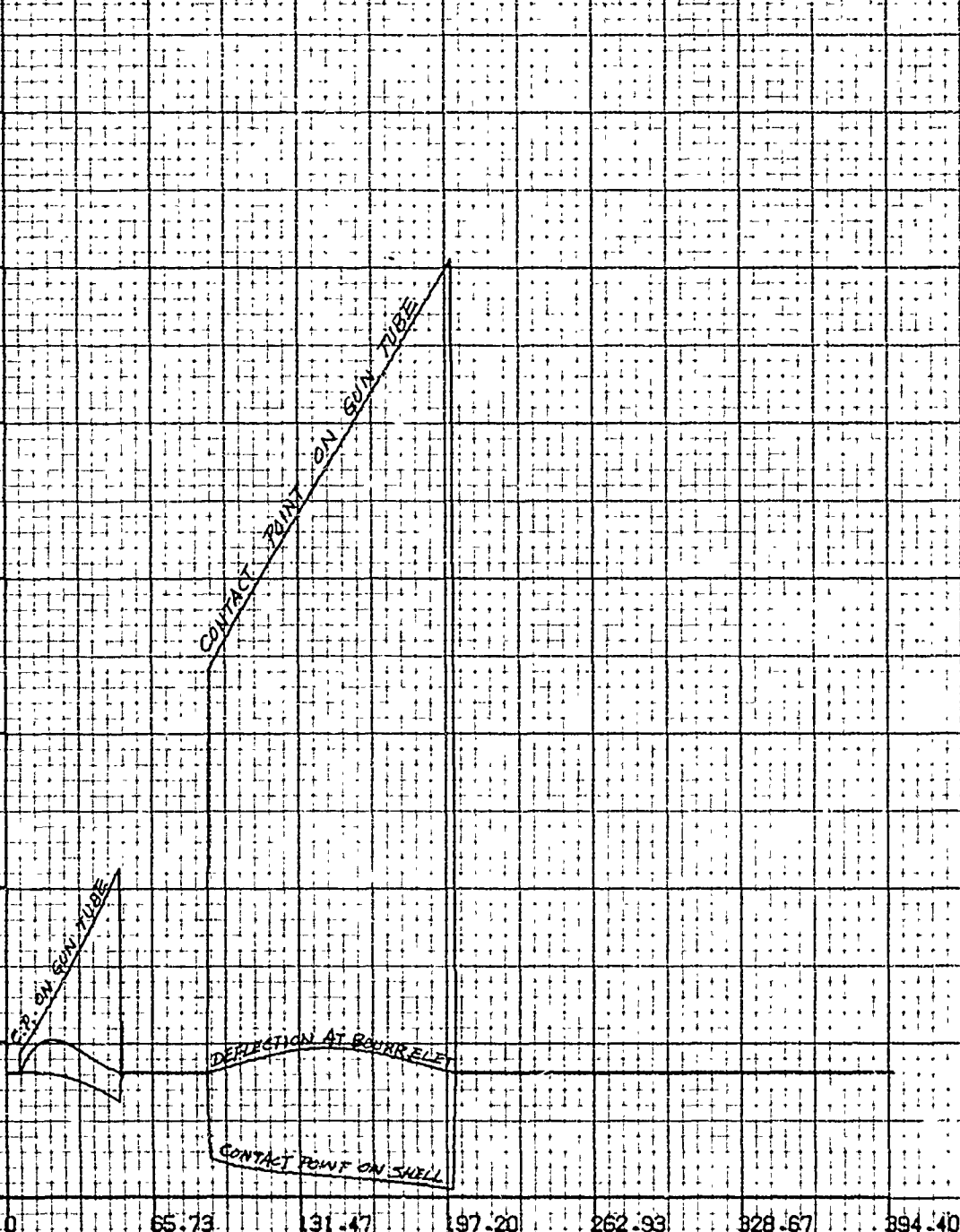
FIGURE 34a

CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE, MCLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.

CONTACT ANGLE, DEG., DEFLECTION, 10⁻⁴ IN.

720.00
620.00
520.00
420.00
320.00
220.00
120.00
20.00
50.00



TRAVERSE, IN.

FIGURE 34b

CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE, MQLG GUN.
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.

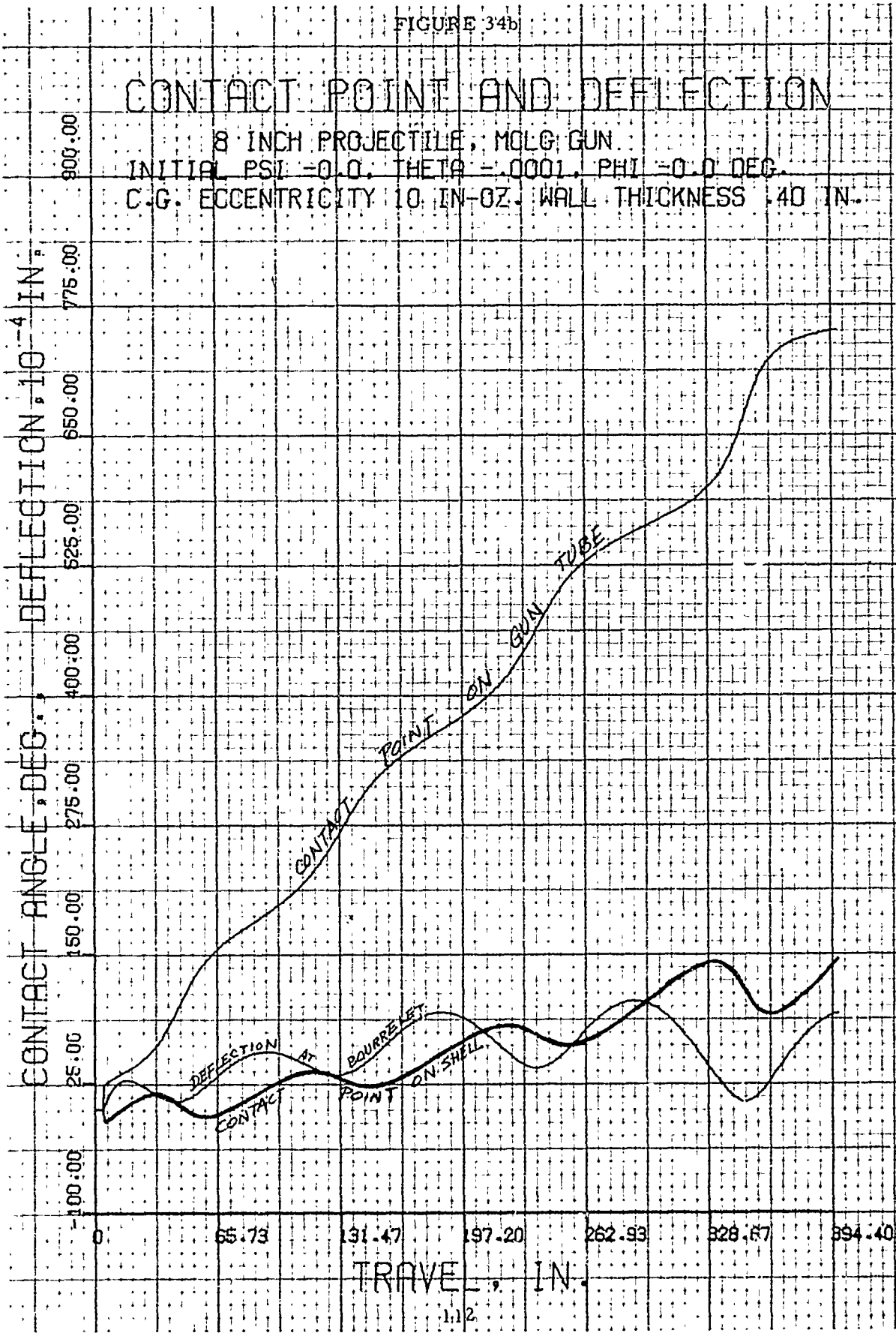


FIGURE 34c

CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE, MCLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

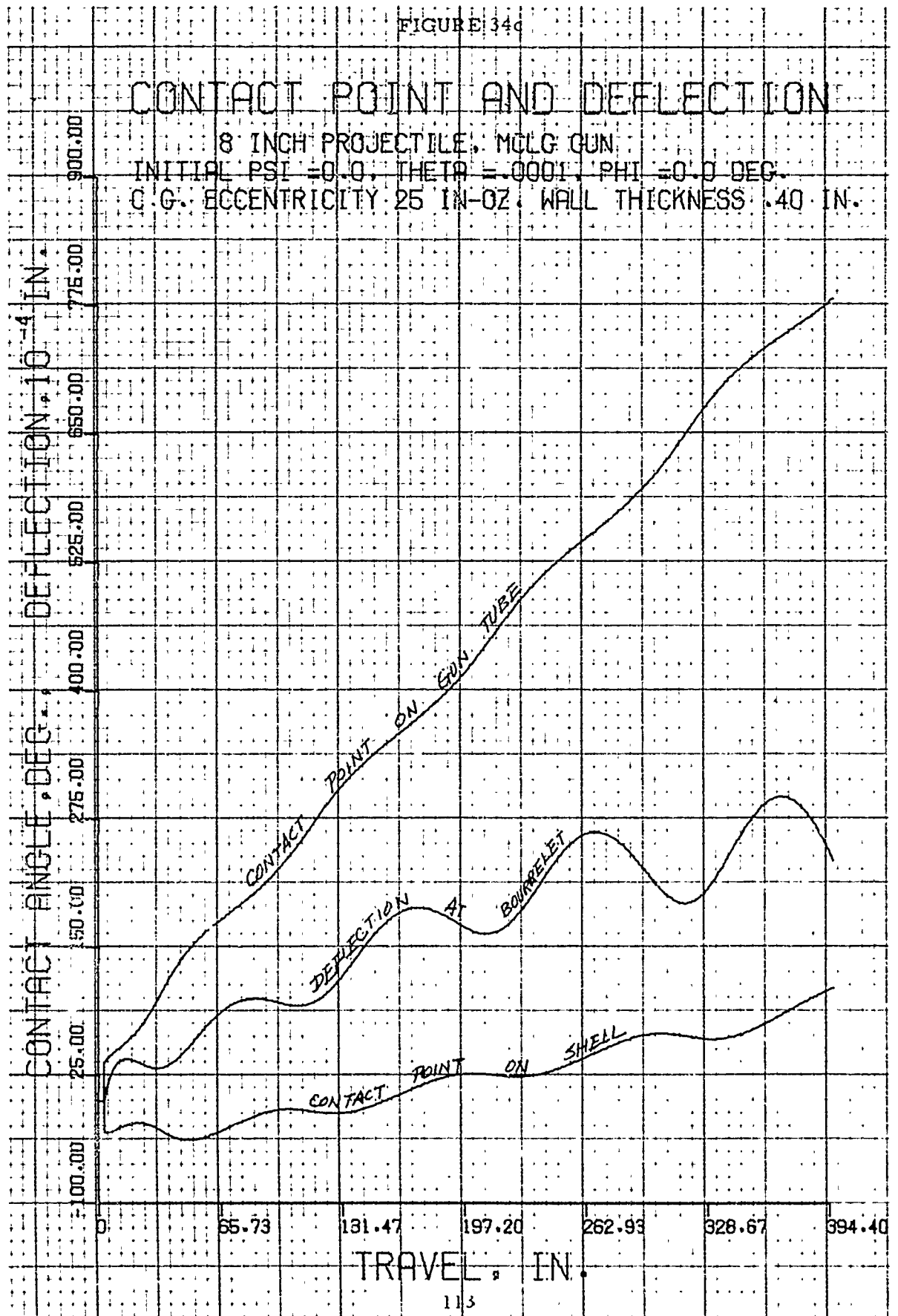


FIGURE 34a

CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE, MQLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

DEFLECTION, 10^{-4} IN.
CONTACT ANGLE, DEG.

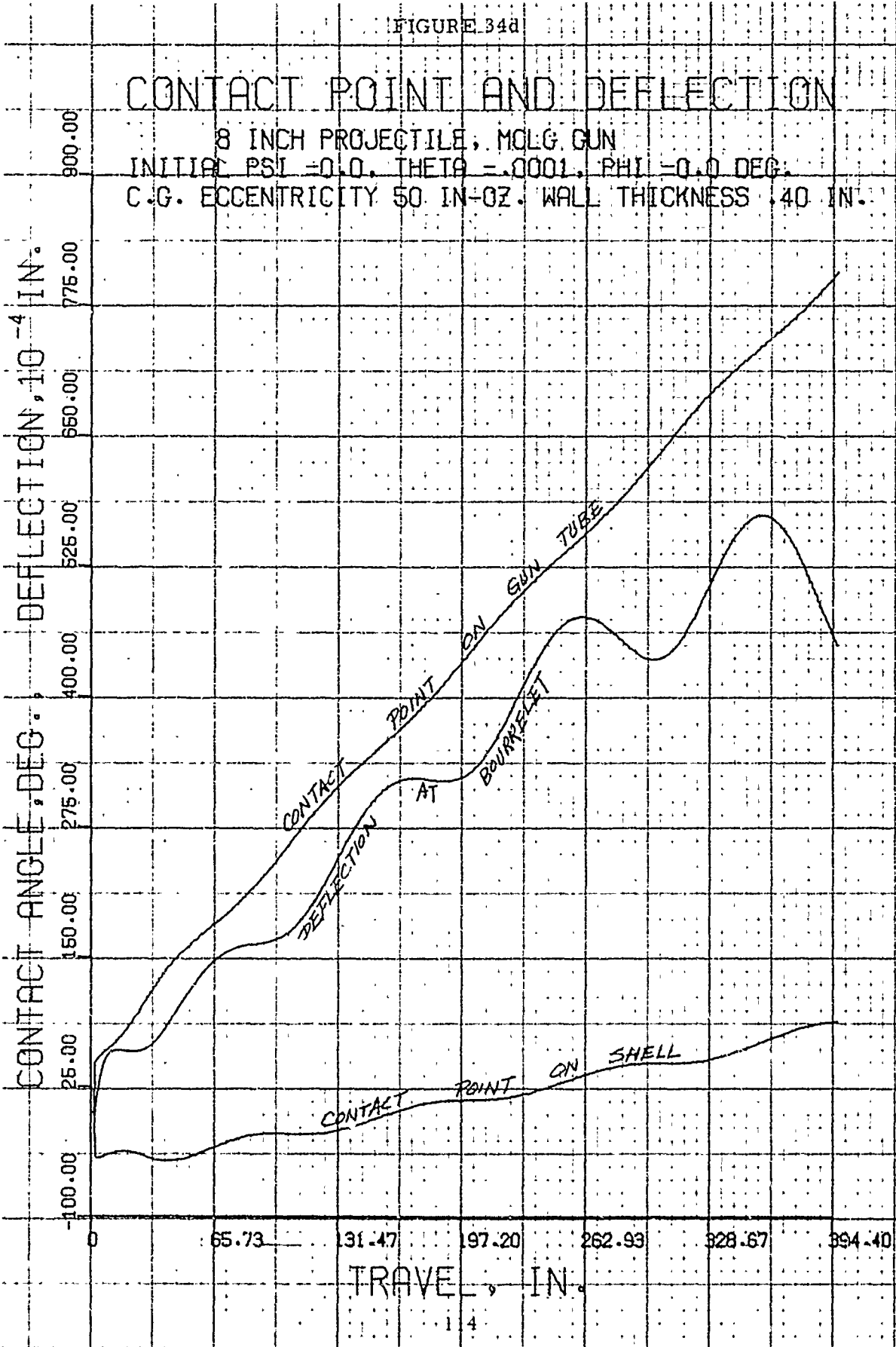


FIGURE 35a

YAW ANGLE, VEL. AND ACC.

8 INCH PROJECTILE, MQLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-07, WALL THICKNESS .40 IN.

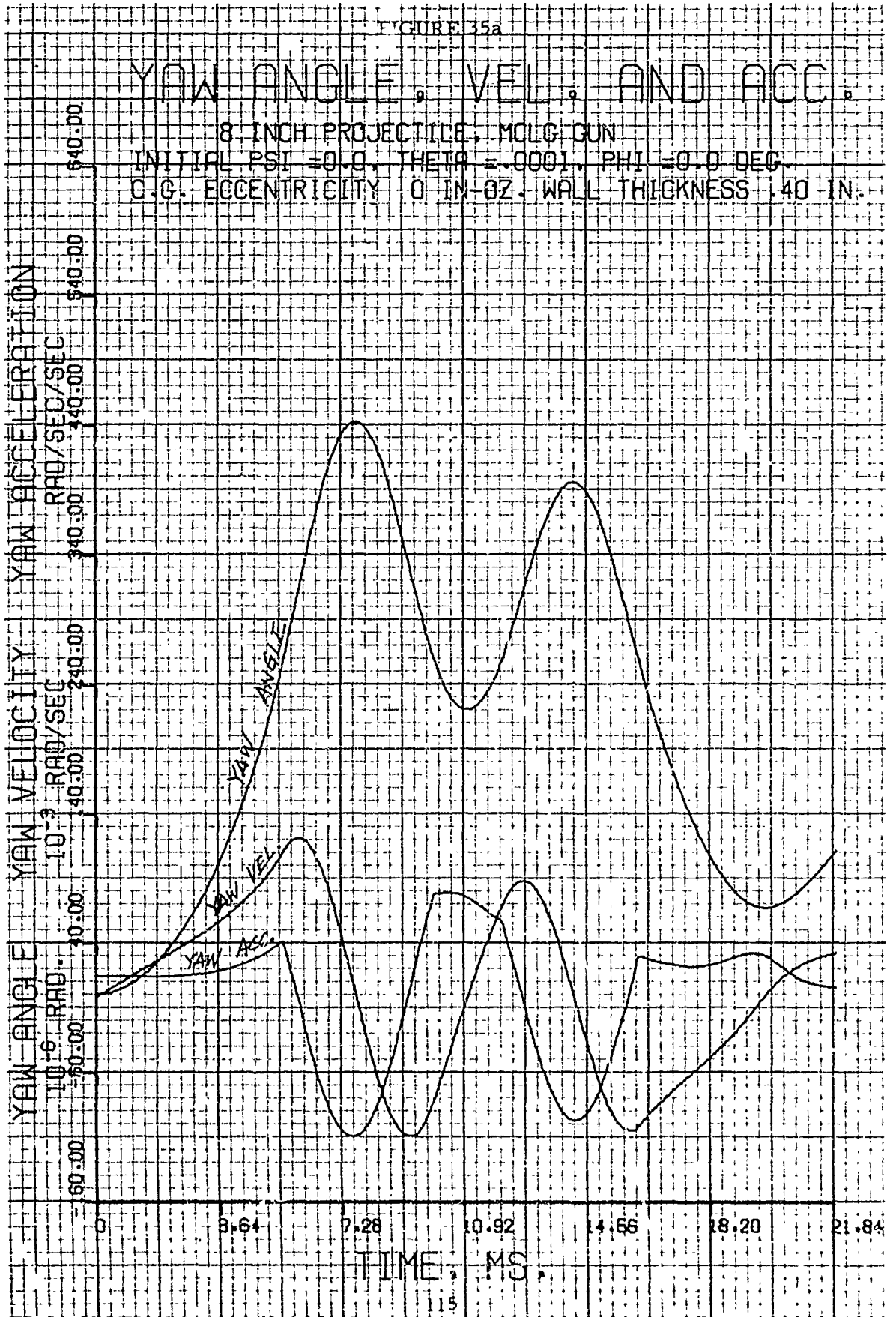


FIGURE 35b

YAW ANGLE, VEL. AND ACC.

8-INCH PROJECTILE, MQLC GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.

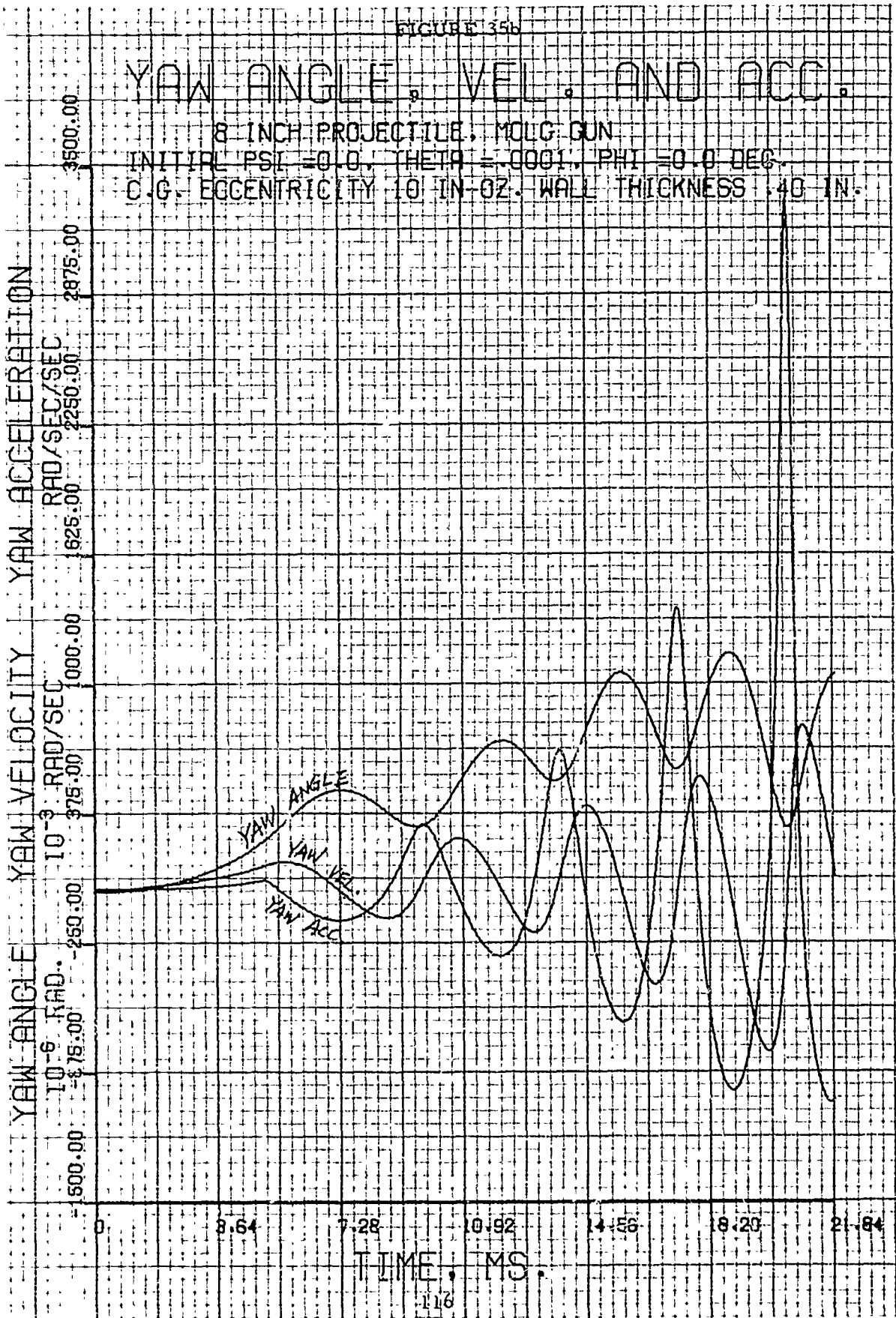


FIGURE 35c

YAW ANGLE, VEL. AND ACC.

8 INCH PROJECTILE, MCLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

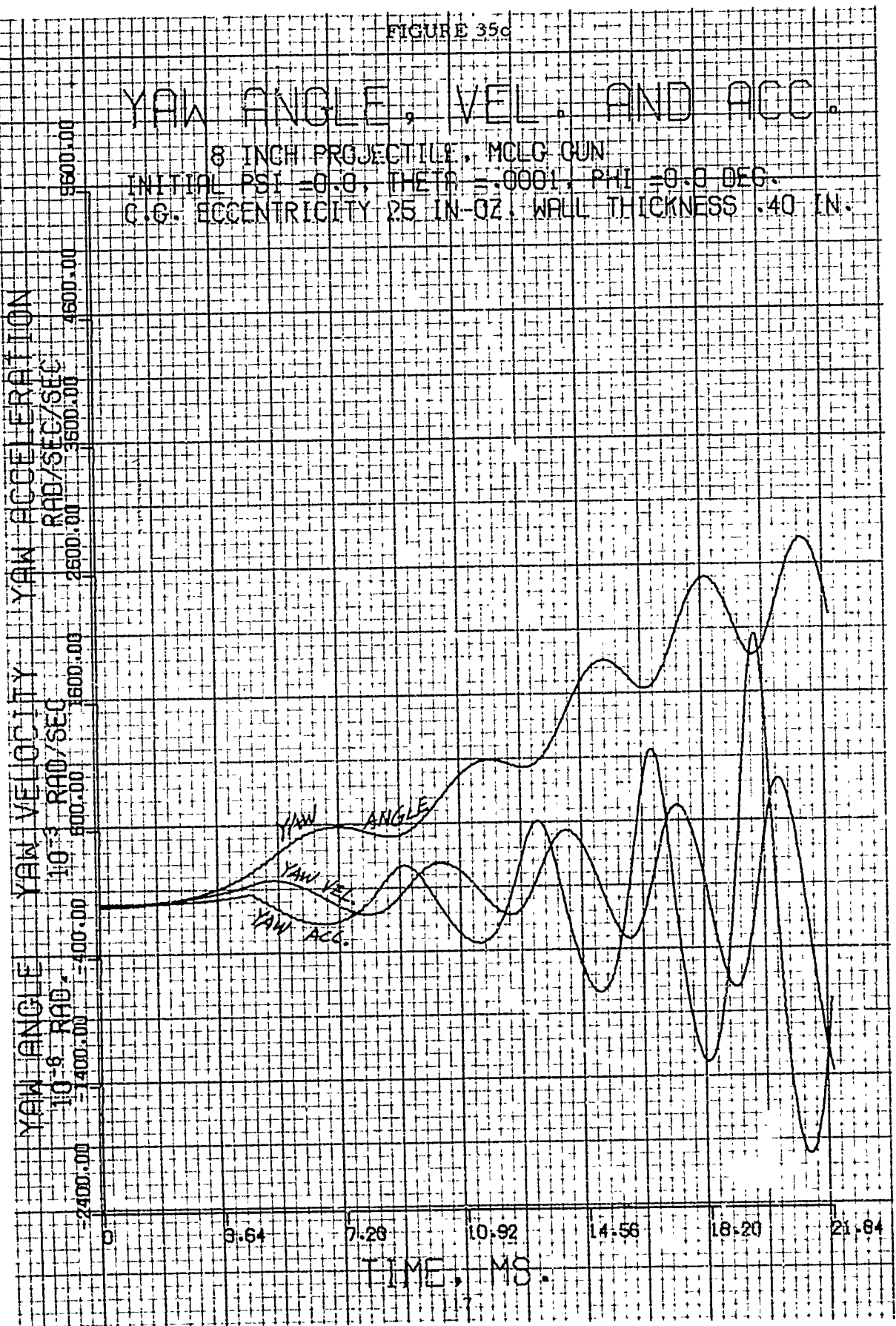


FIGURE 35d

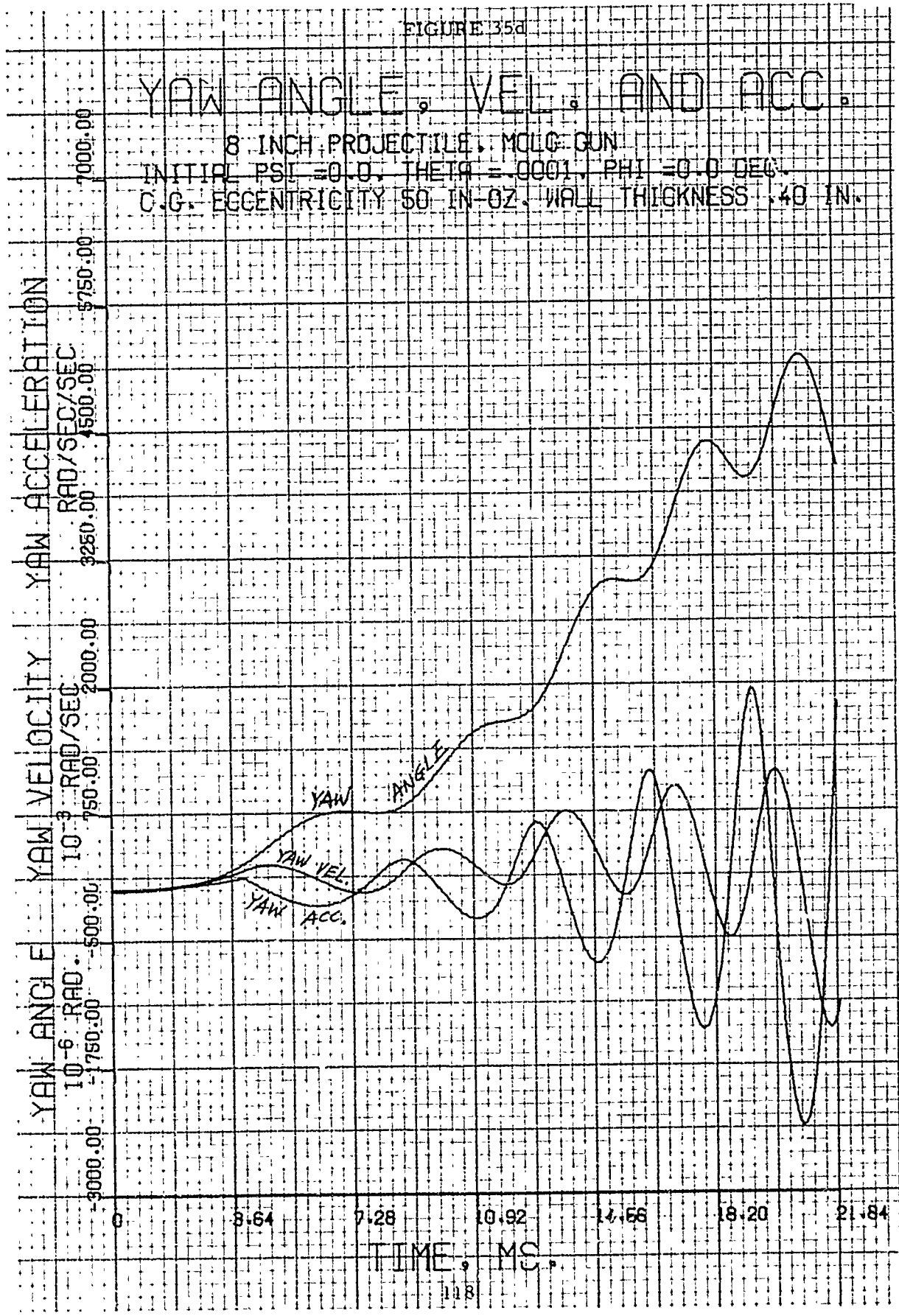


FIGURE 36a

NORMAL ACCELERATIONS

8 INCH PROJECTILE, MLC GUN
INITIAL PSI = 0.0, THETA = 0.01, PHI = 0.0 DEG
C.G. ECCENTRICITY = 0 IN-OZ, WALL THICKNESS .40 IN.

CURVE 1 — ACC. AT CENTER OF GRAVITY
2 — ACC. AT CENTER OF BOURRELET
3 — ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
4 — 7.5
5 — 5.0
6 — 2.5

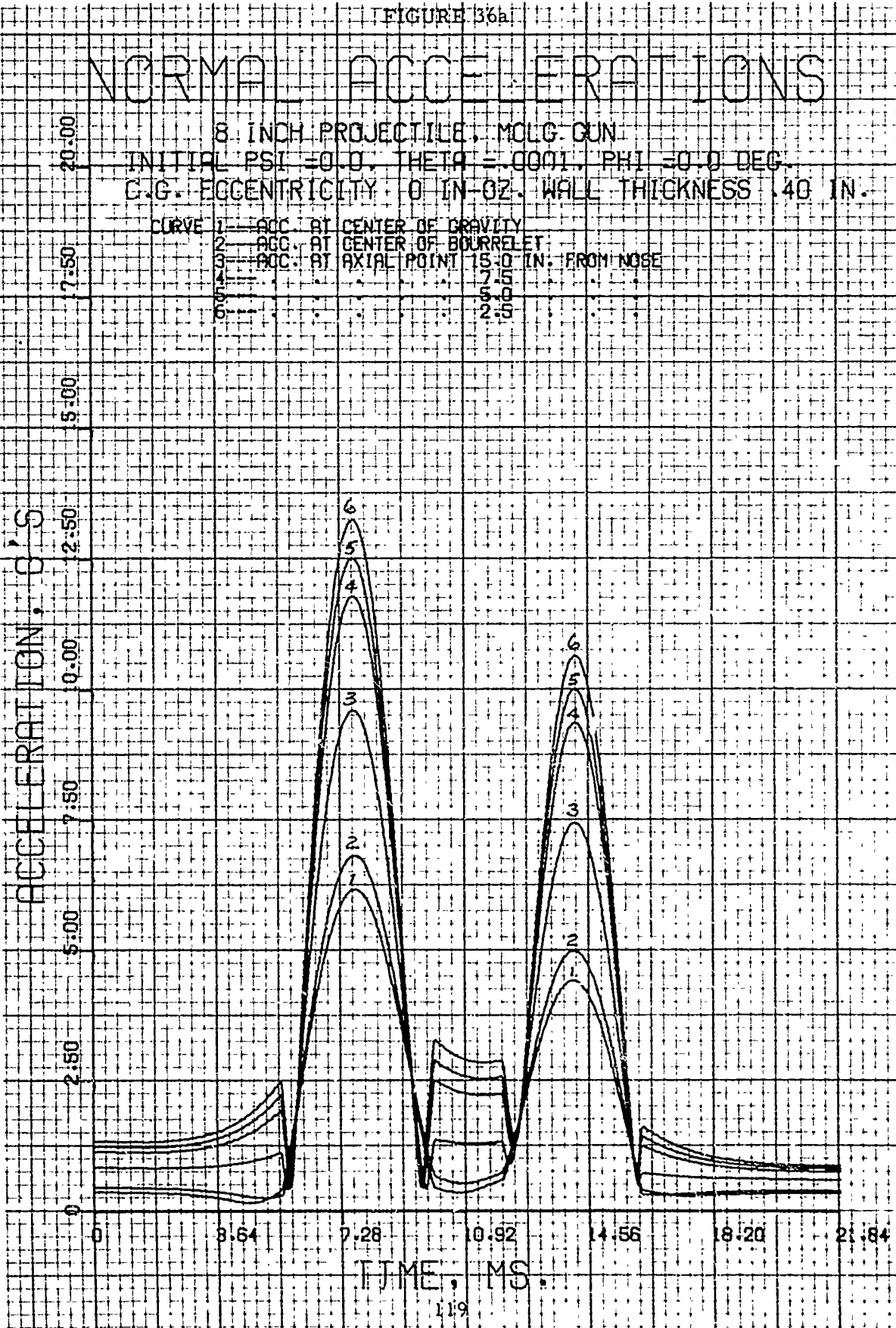


FIGURE 36b

NORMAL ACCELERATIONS

8 INCH PROJECTILE, MQLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.

CURVE 1 ACC. AT CENTER OF GRAVITY
2 ACC. AT CENTER OF BOURRELET
3 ACC. AT AXIAL POINT 15.0 IN. FROM NOSE

ACCELERATION, G'S

125.00

09.38

93.75

78.13

62.50

46.88

31.25

15.63

0

0.00

2.00

4.00

3.64

7.28

10.92

14.56

18.20

21.84

TIME, MS.

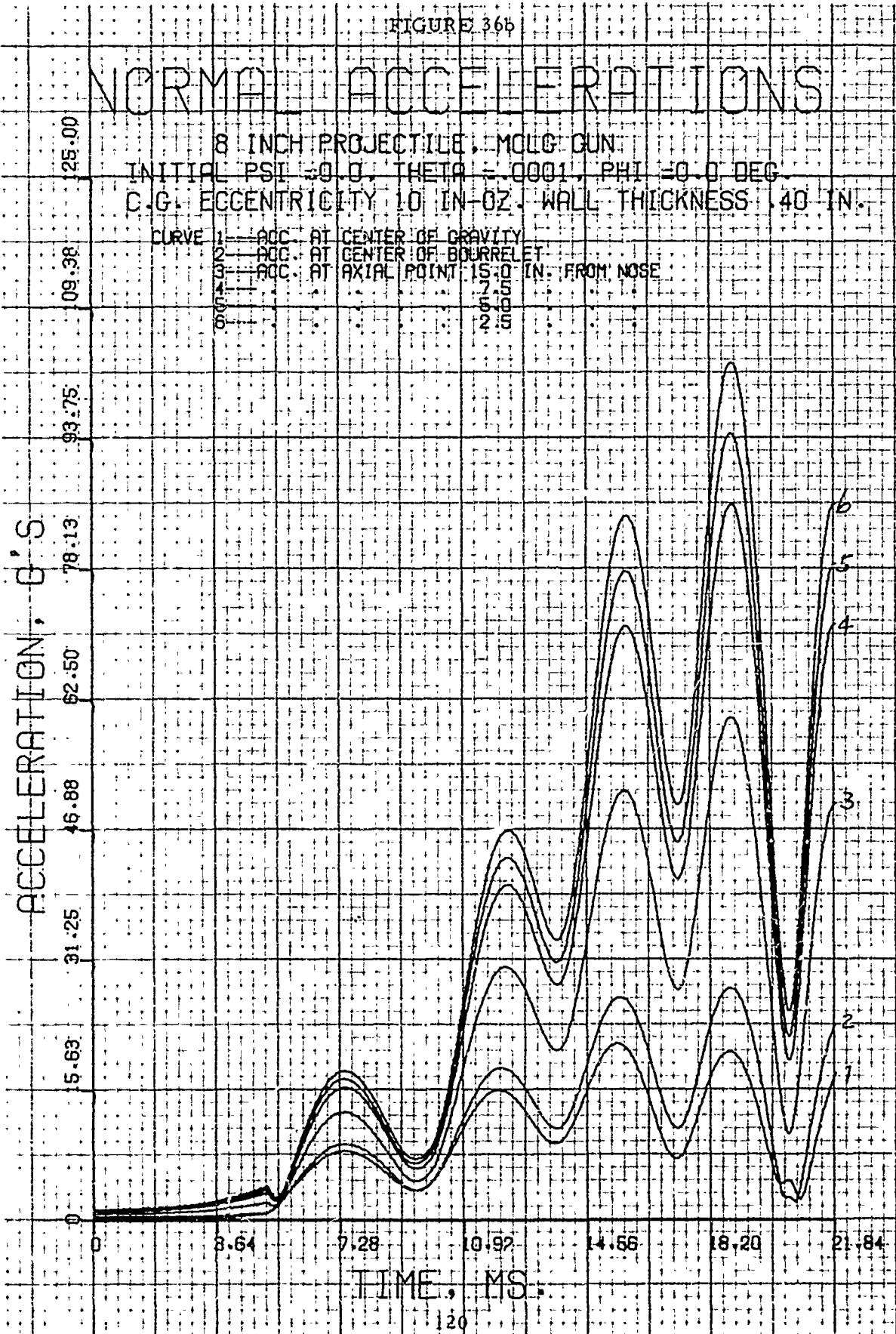


FIGURE 36c

NORMAL ACCELERATIONS

8 INCH PROJECTILE, MCLG GUN
INI. VEL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ WALL THICKNESS .40 IN.

CURVE	ACC. AT	LOCATION
1	ACC. AT	CENTER OF GRAVITY
2	ACC. AT	CENTER OF BOURRELET
3	ACC. AT	AXIAL POINT 15.0 IN. FROM NOSE
4	ACC. AT	AXIAL POINT 7.5 IN. FROM NOSE
5	ACC. AT	AXIAL POINT 5.0 IN. FROM NOSE
6	ACC. AT	AXIAL POINT 2.5 IN. FROM NOSE
7	ACC. AT	AXIAL POINT 0.0 IN. FROM NOSE

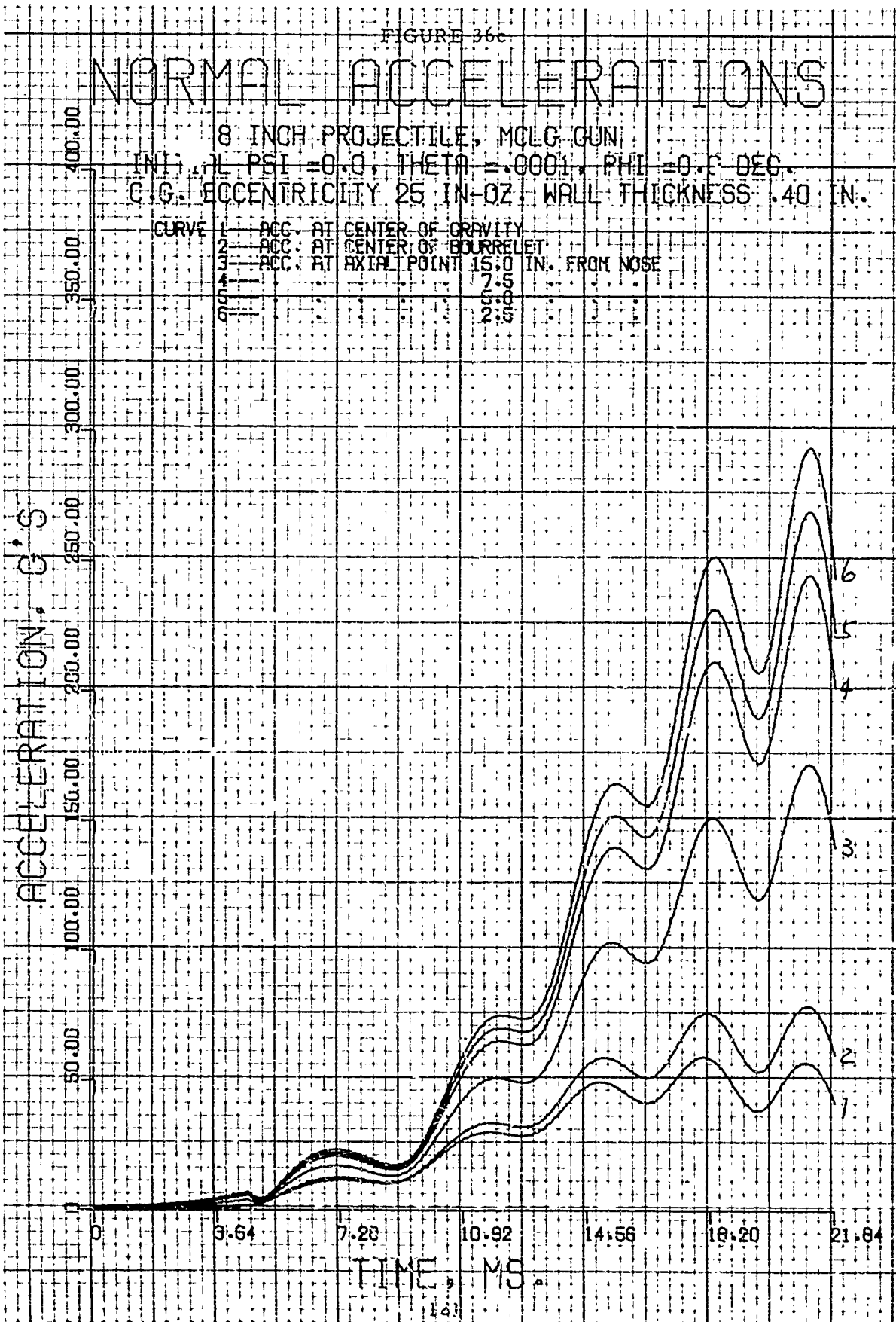


FIGURE 36d

NORMAL ACCELERATIONS

8 INCH PROJECTILE; MQLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

CURVE 1 — ACC. AT CENTER OF GRAVITY
2 — ACC. AT CENTER OF BARRILET
3 — ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
4 — 2.5 IN. FROM NOSE
5 — 5.0 IN. FROM NOSE
6 — 2.0 IN.

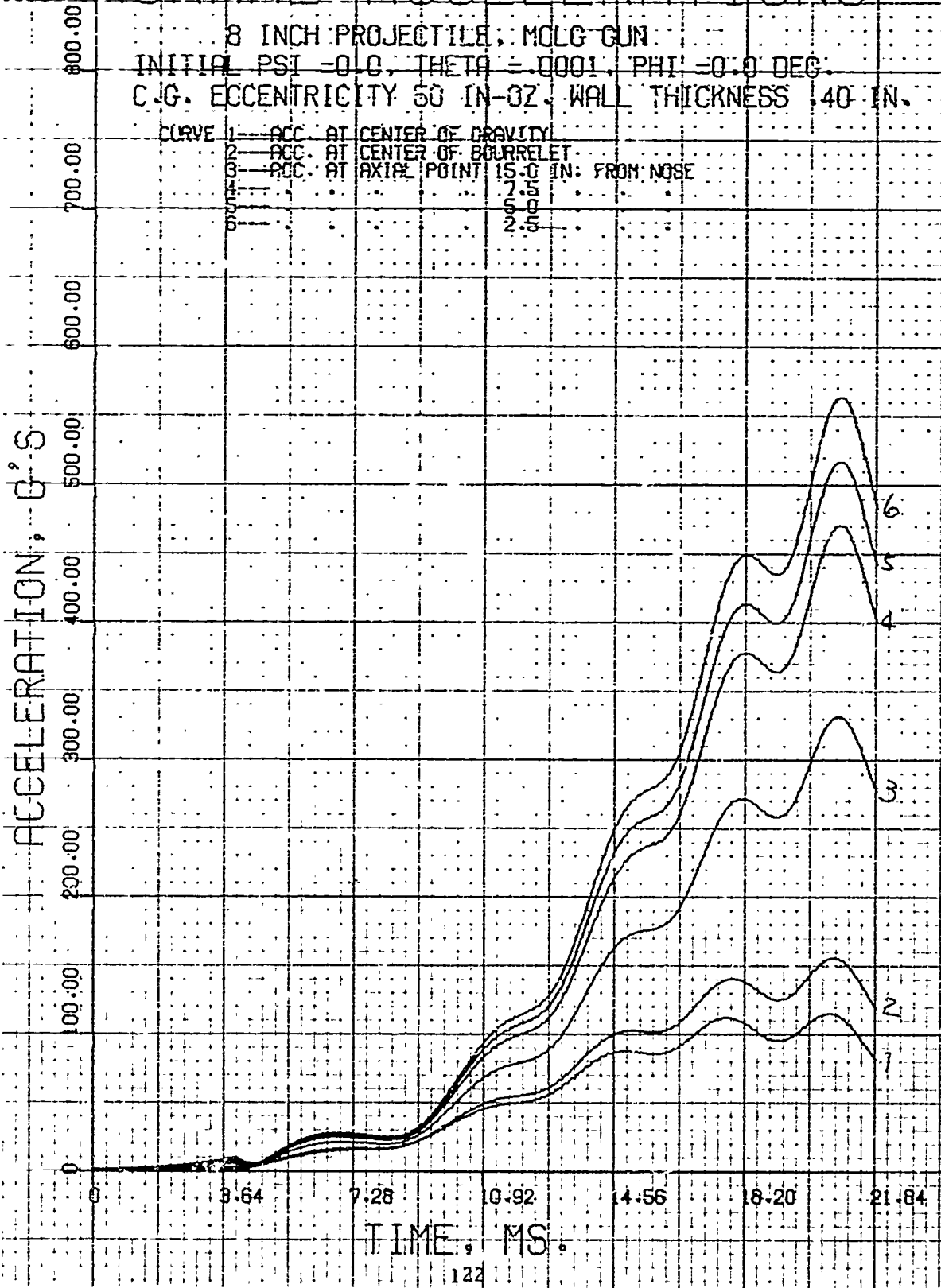


FIGURE 37a

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MQLG GUN
INITIAL PSI = 0.0, THETA = 0.001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS 40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION

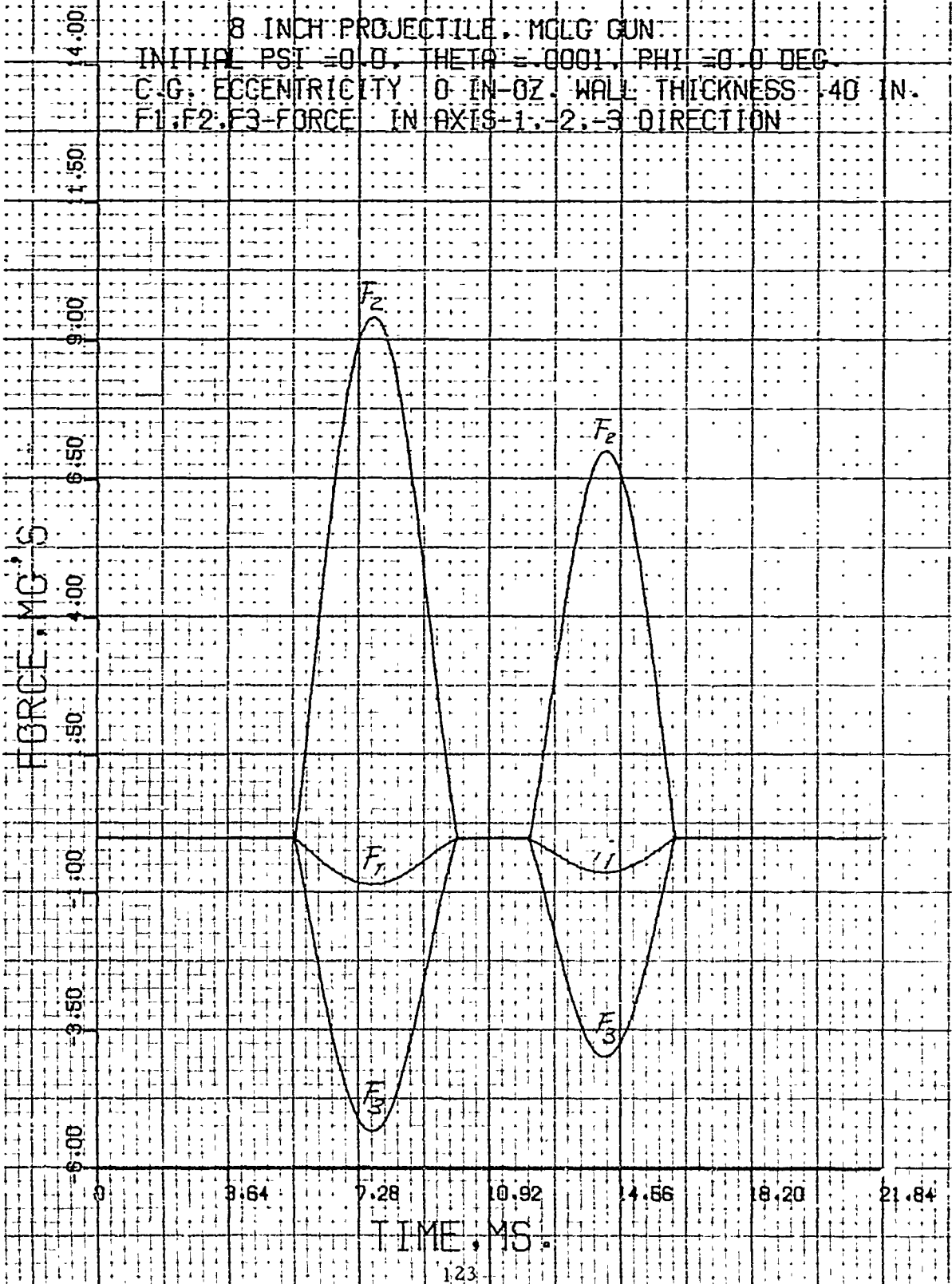


FIGURE 375

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MCLG GUN.
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION

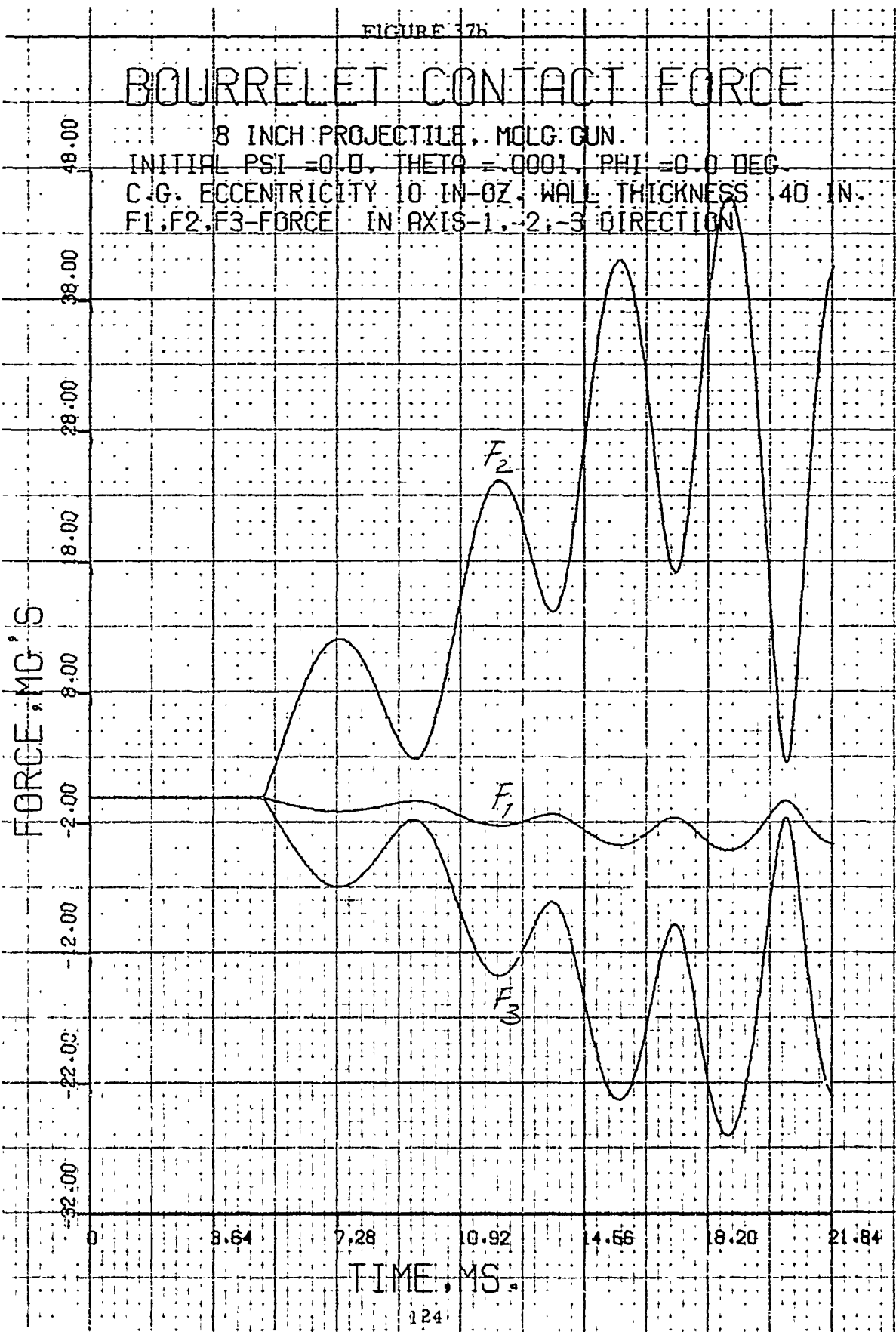


FIGURE 37c

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MQLG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 = FORCE IN AXIS = 1, -2, -3 DIRECTION

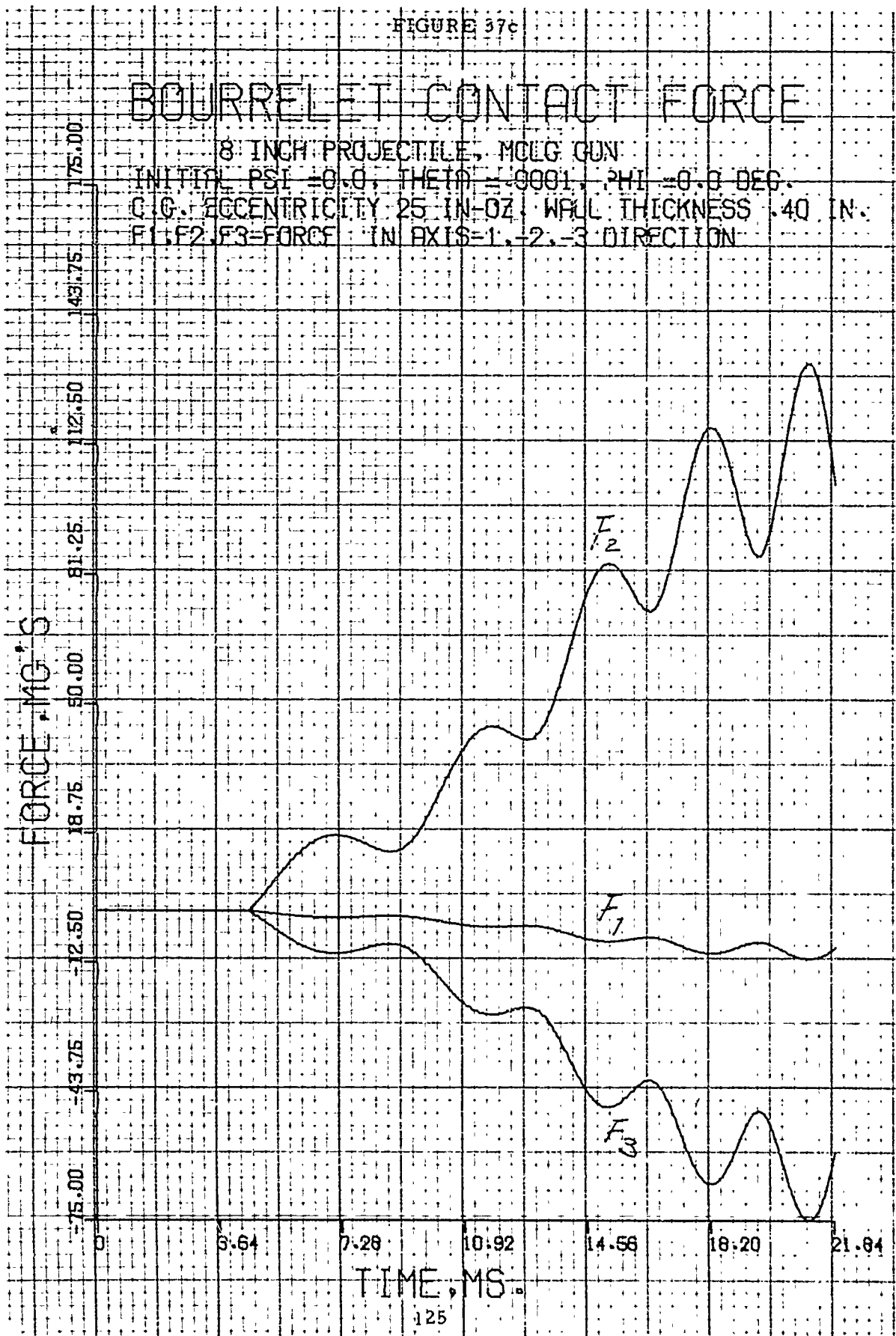
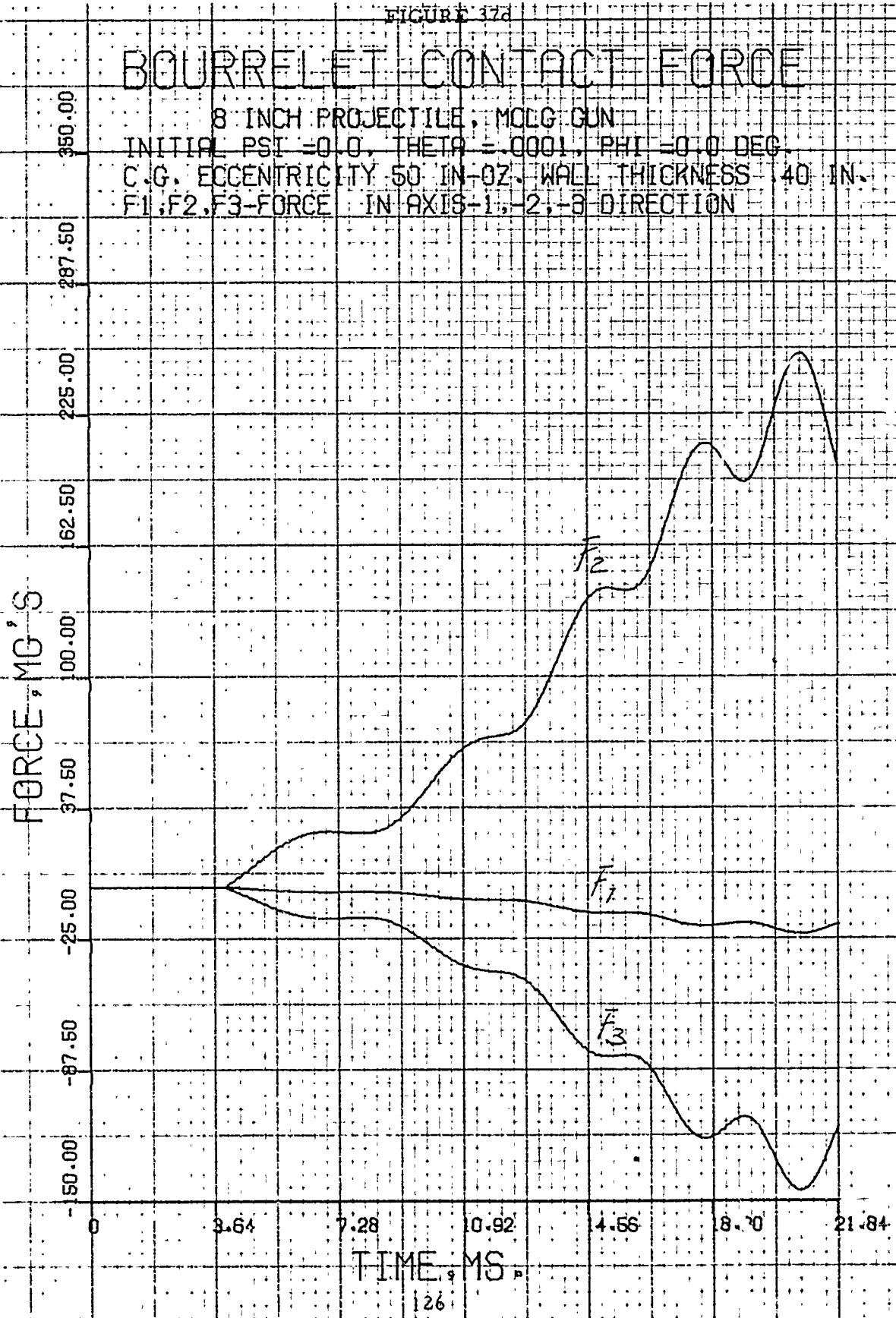


FIGURE 37a

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MCG GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION



MK-16 GUN

FIGURE 38

CONFIDENTIAL

PRESSURE AND TRAVEL

8 INCH PROJECTILE, MK-16 GUN
 INITIAL PSI - 0.0, THETA - .0001, PHI - 0.0 DEG.
 C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.

70
 25
 50

TRAVEL, INCHES

PRESSURE, 10² PSI.

500.00
 437.50
 375.00
 312.50
 250.00
 187.50
 125.00
 62.50
 0

0 4.26 8.52 12.78 17.04 21.30 25.56

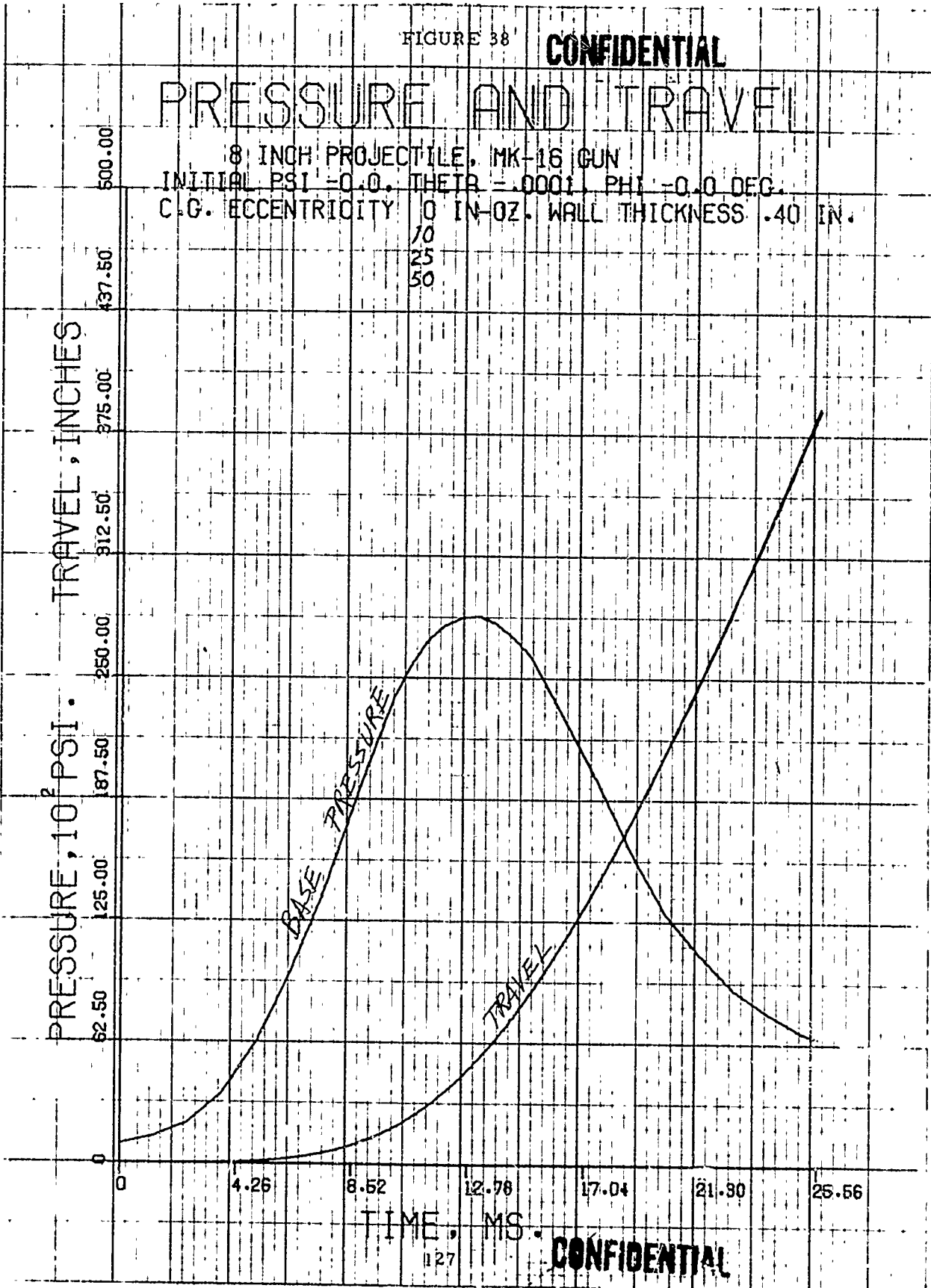
TIME, MS.

127

CONFIDENTIAL

BASE PRESSURE

TRAVEL



CONFIDENTIAL

FIGURE 39

VELOCITY AND ACCELERATION

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI - C.O., THETA - .0001, PHI - 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ.

10
25
50

VELOCITY, FPS.
ACCELERATION, 2G'S

4000.00
3500.00
3000.00
2500.00
2000.00
1500.00
1000.00
500.00
0

0

4.26

8.52

12.78

17.04

21.30

25.56

TIME, MS.

128

CONFIDENTIAL

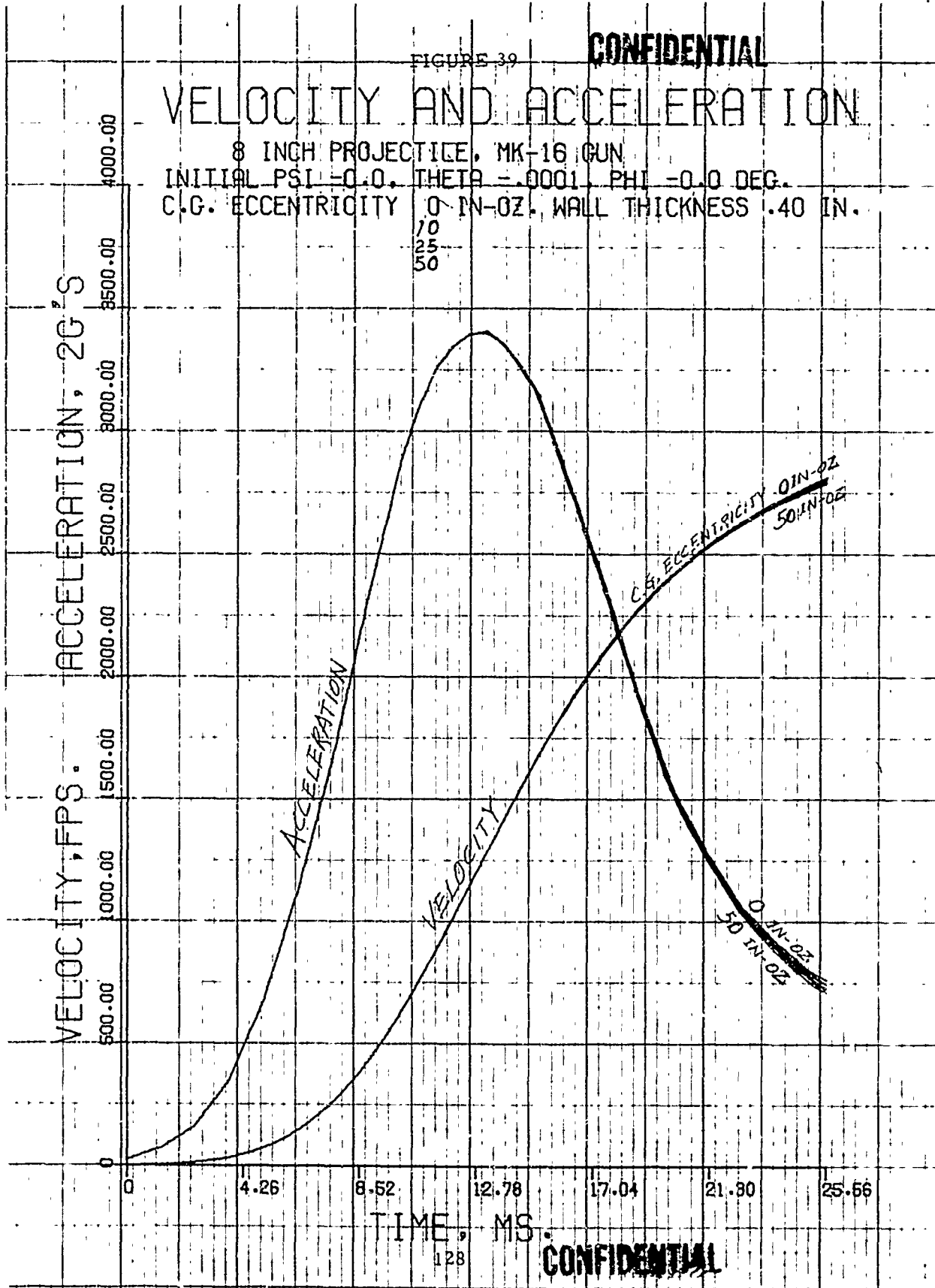
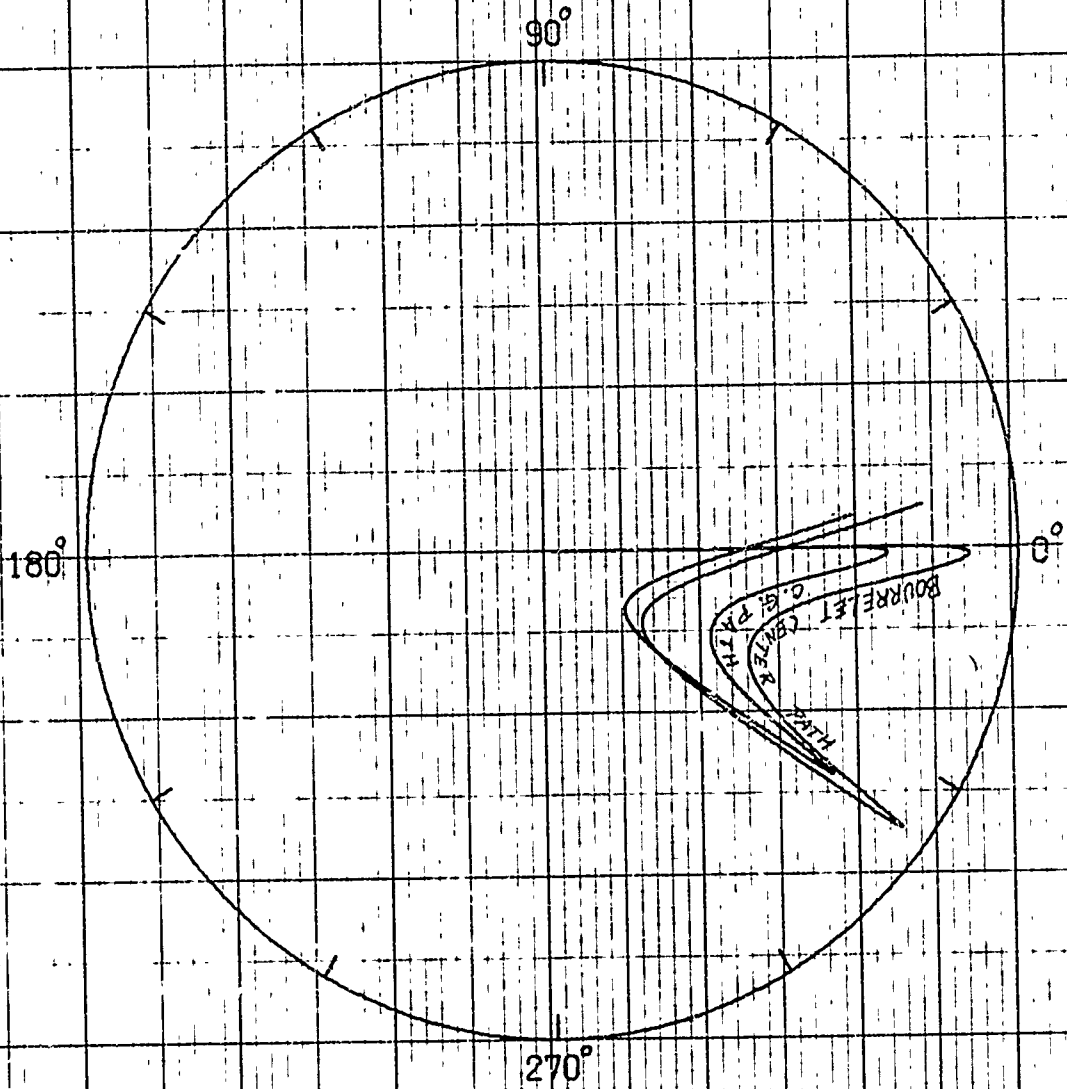


FIGURE 2a

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.

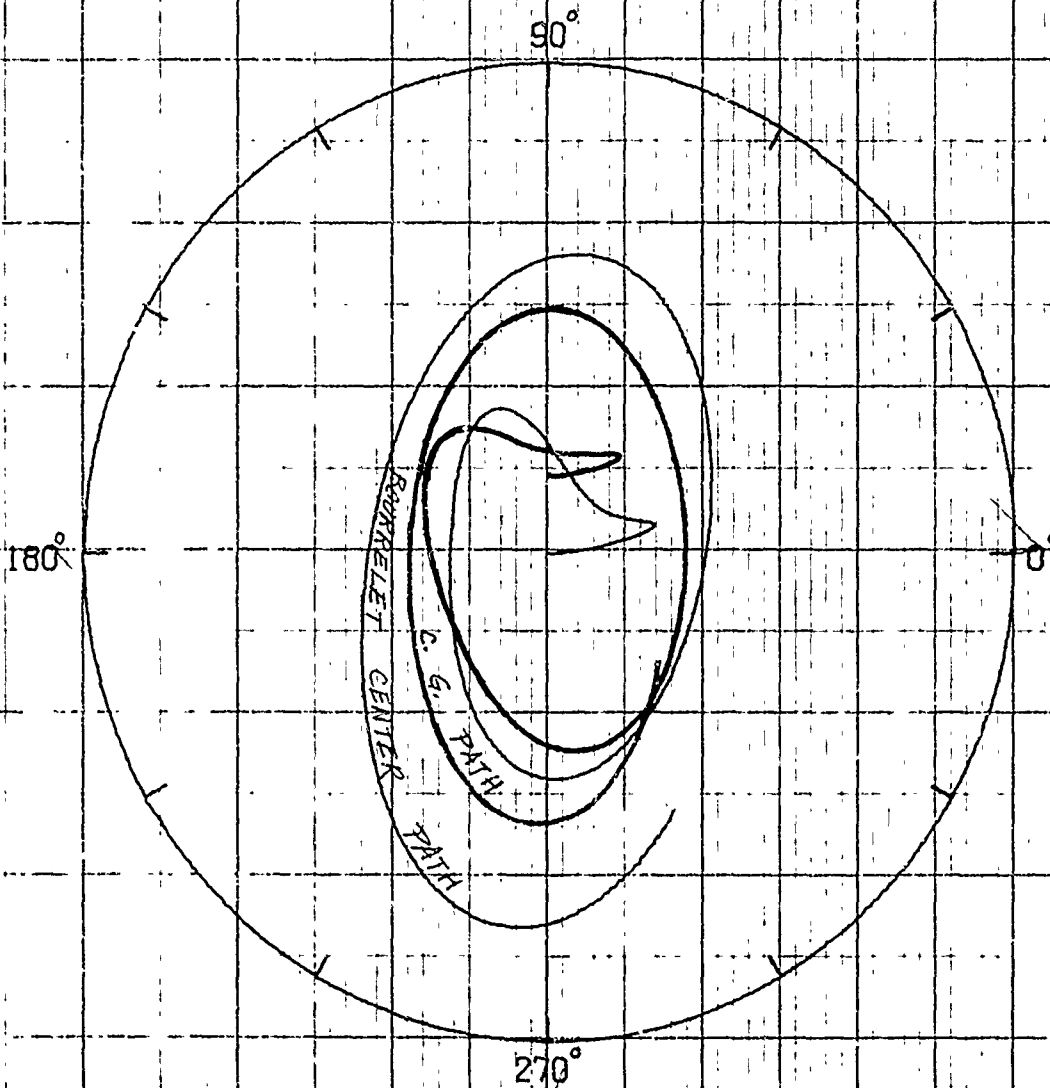


$R = .0050$ IN.

FIGURE 40b

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE MK-16 GUN
INITIAL PST = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS 40 IN.

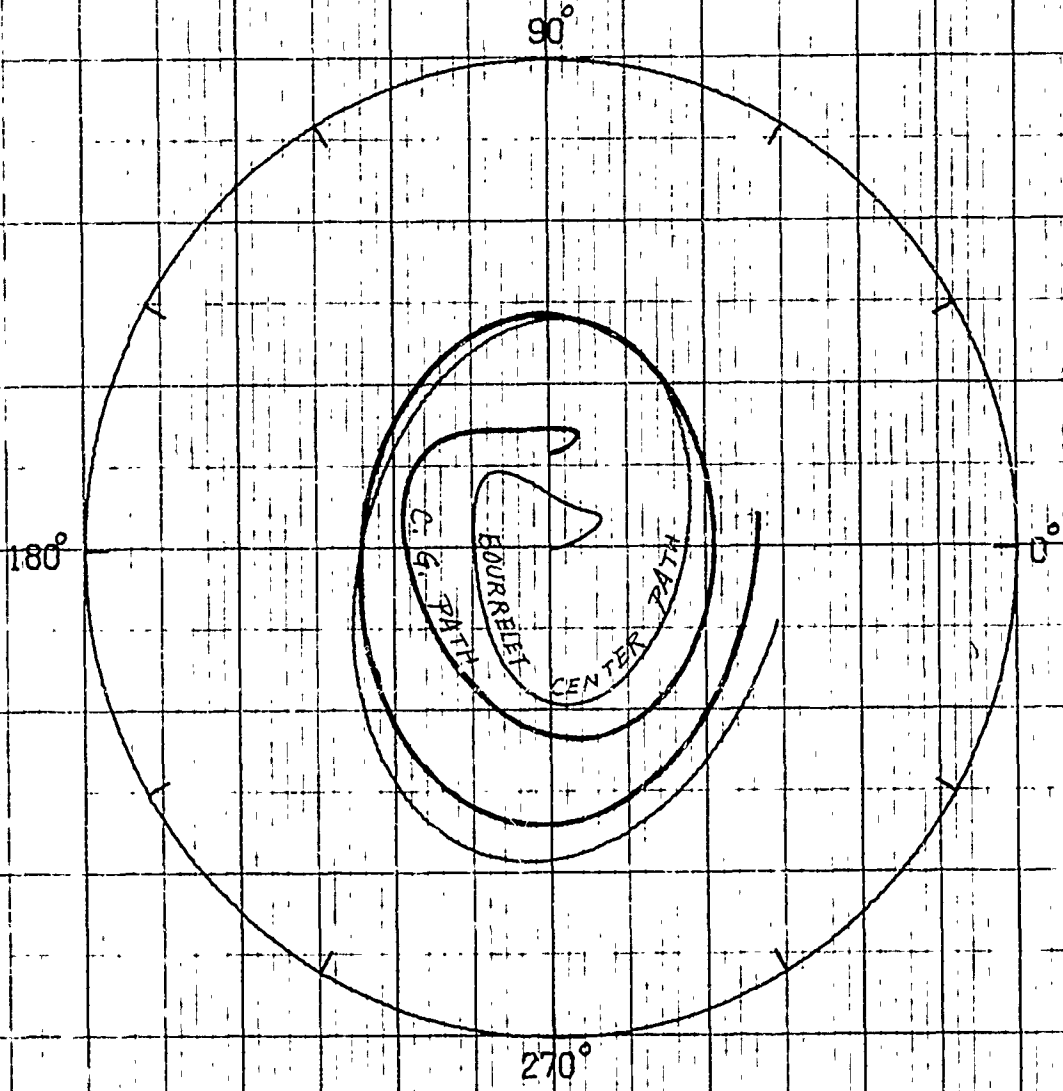


R = .0200 IN.

FIGURE 40c

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE MK 16 GUN
INITIAL PSI = 0.0. THETA = 0.001. PHI = 0.0 DEG.
C.G. ECCENTRICITY 28 IN-07. WALL THICKNESS .40 IN.

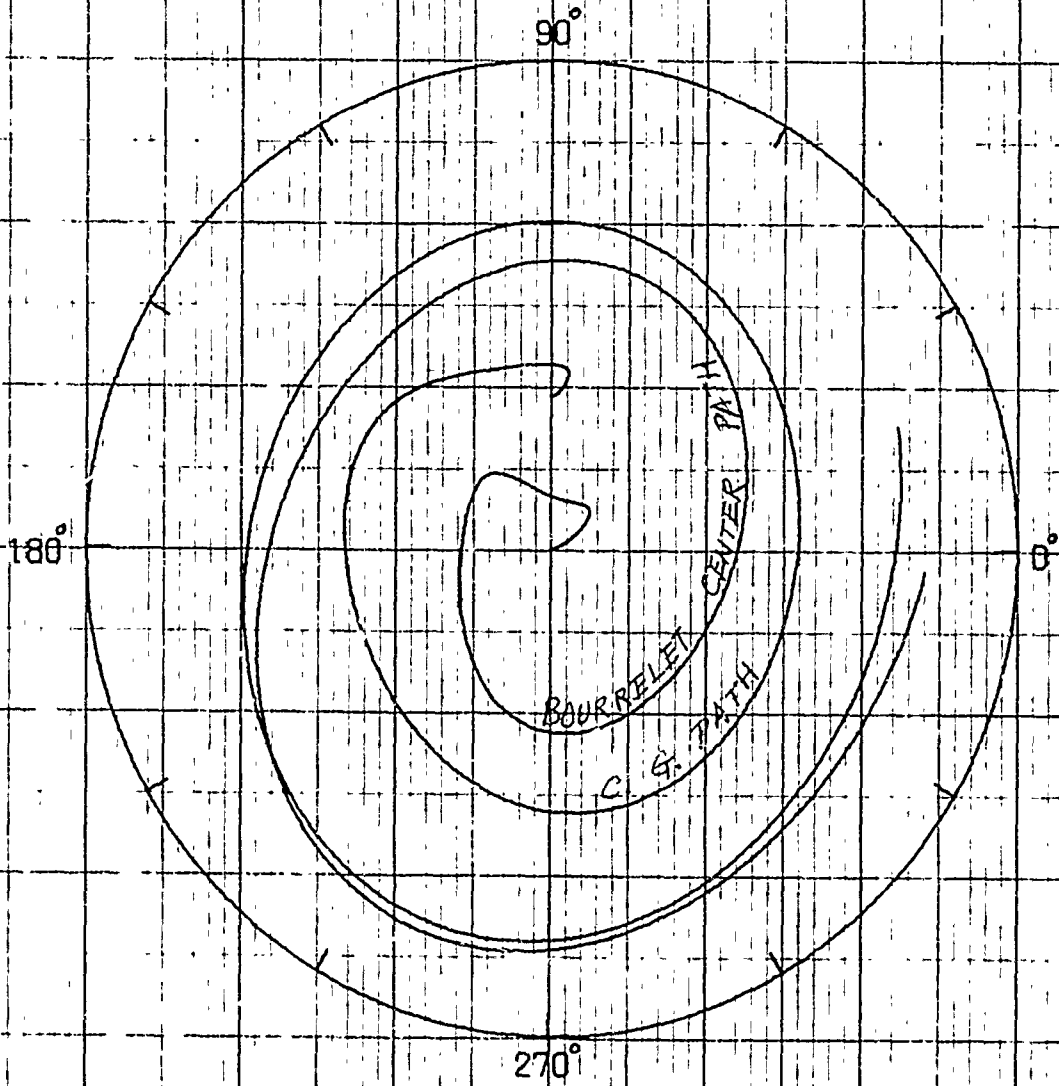


R = .0400 IN.

FIGURE 40d

C.G. AND BOURRELET CENTER

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.



R = .0500 IN.

FIGURE 41a

CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ., WALL THICKNESS .40 IN.

CONTACT ANGLE, DEG. DEFLECTION, 10⁻⁴ IN.

900.00
775.00
650.00
525.00
400.00
275.00
150.00
25.00
-100.00

0 64.78 129.57 194.35 259.13 323.92 388.70

TRAVEL, IN.

CONTACT POINT ON GUN TUBE

DEFLECTION
CONTACT POINT ON SHELL

FIGURE 41b

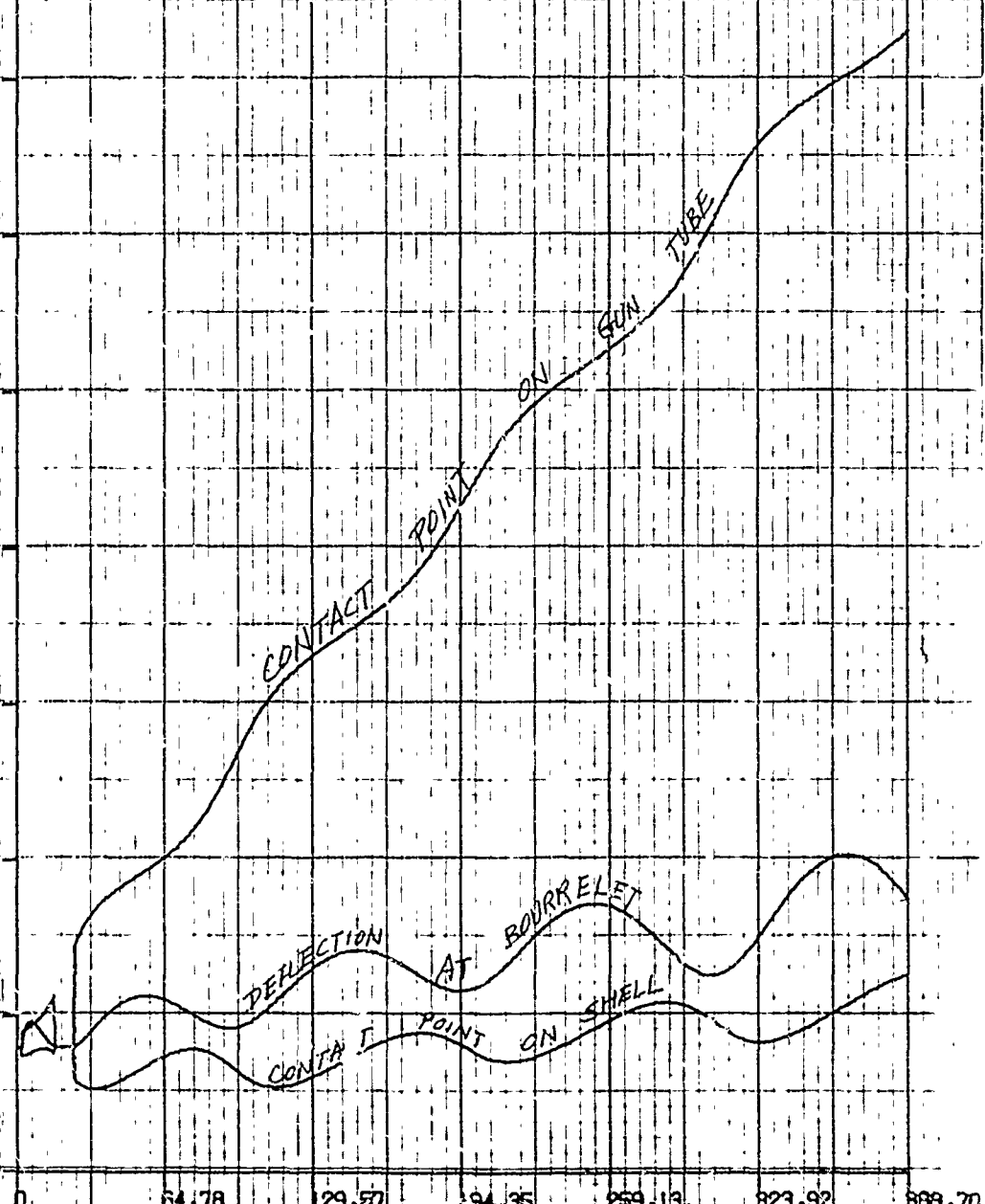
CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = 0.001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS 40 IN.

DEFLECTION, 10⁻⁴ IN.

CONTACT ANGLE, DEG.

720.00
620.00
520.00
420.00
320.00
220.00
120.00
20.00
-80.00



TRAVEL, IN.

FIGURE 41c

CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE MK 16 GUN
INITIAL PSI = 0.0, THETA = 0.001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS 40 IN.

DEFLECTION, 10^{-4} IN.
CONTACT ANGLE, DEG.

900.00
775.00
650.00
525.00
400.00
275.00
150.00
25.00
-100.00

CONTACT POINT ON GUN TUBE
DEFLECTION AT BOURRELET
CONTACT POINT ON SHELL

0 64.78 129.57 194.35 259.13 323.92 388.70

TRAVE, IN.

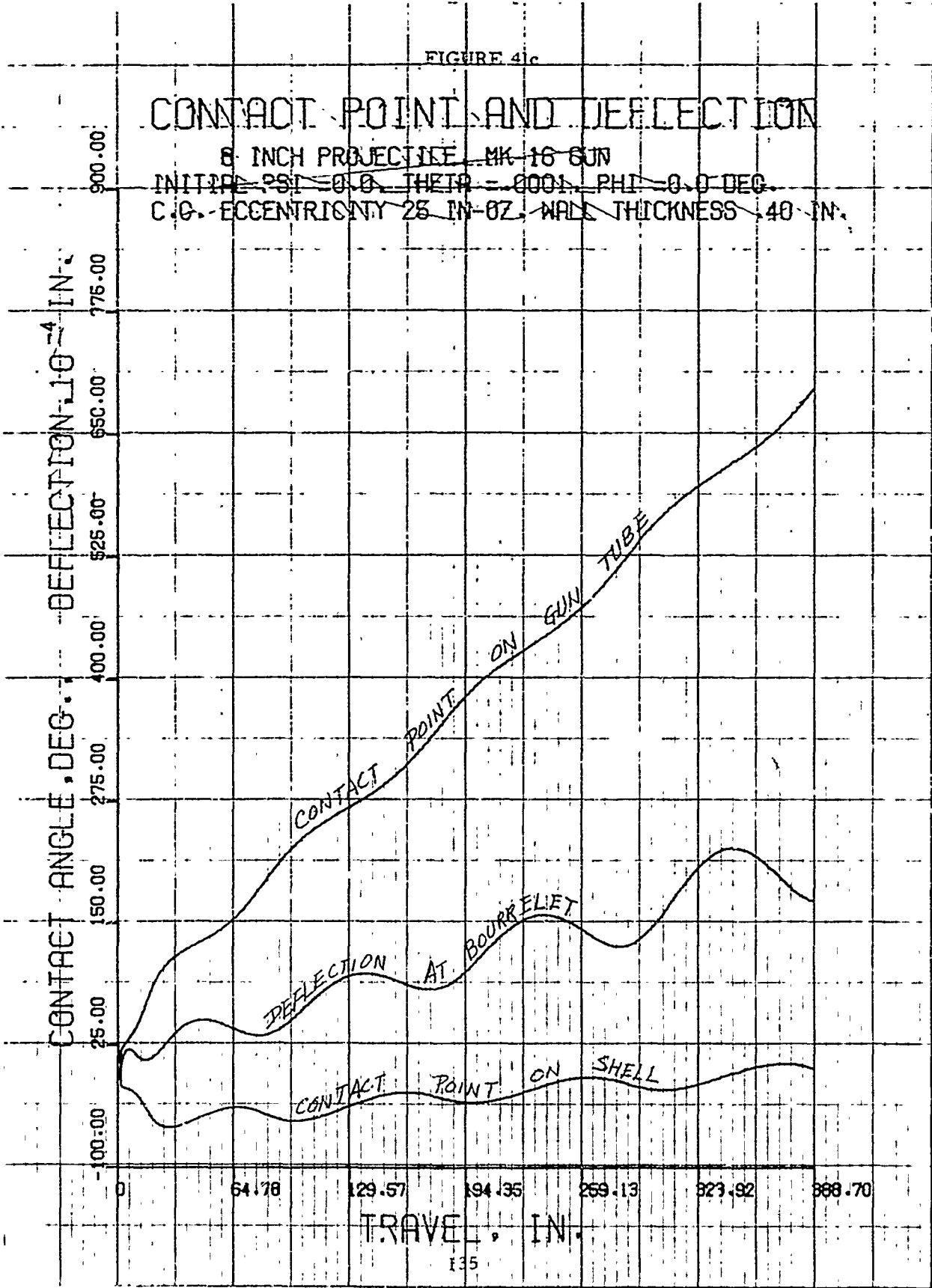


FIGURE 413

CONTACT POINT AND DEFLECTION

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ, WALL THICKNESS .40 IN.

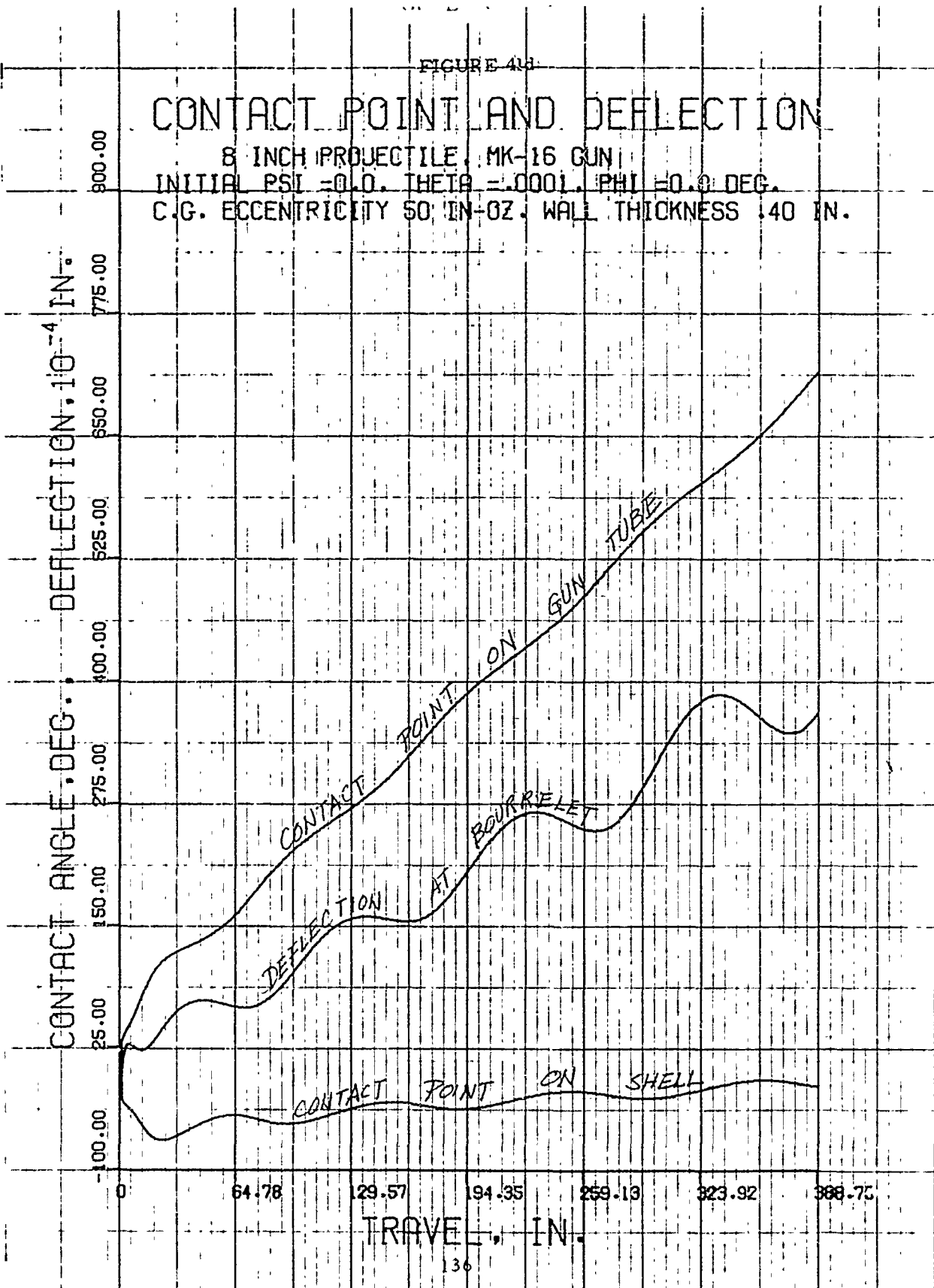


FIGURE 42a

YAW ANGLE, VEL. AND ACC.

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ., WALL THICKNESS .40 IN.

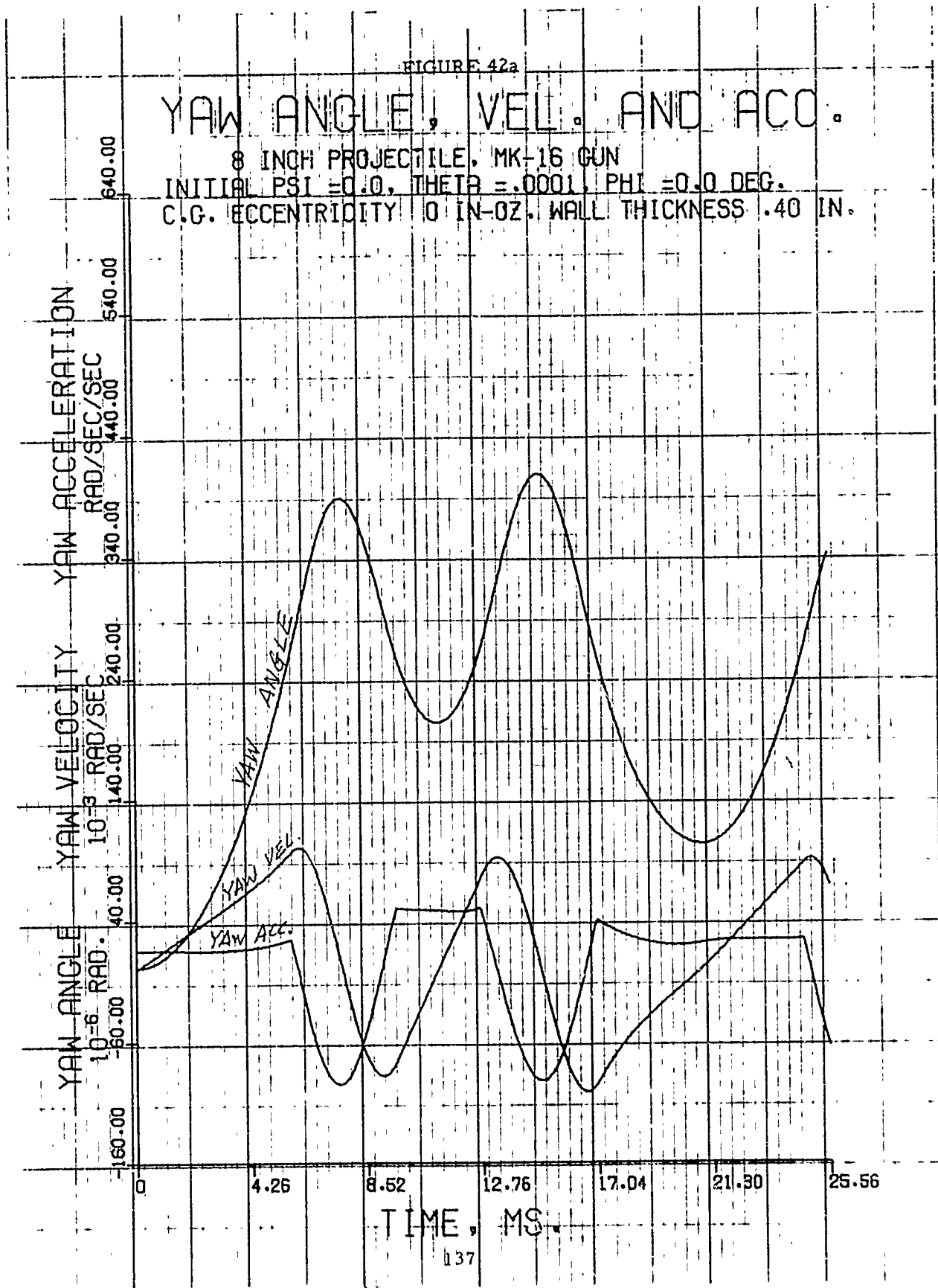


FIGURE 42b

YAW ANGLE, VEL. AND ACC.

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 10 IN-OZ, WALL THICKNESS .40 IN.

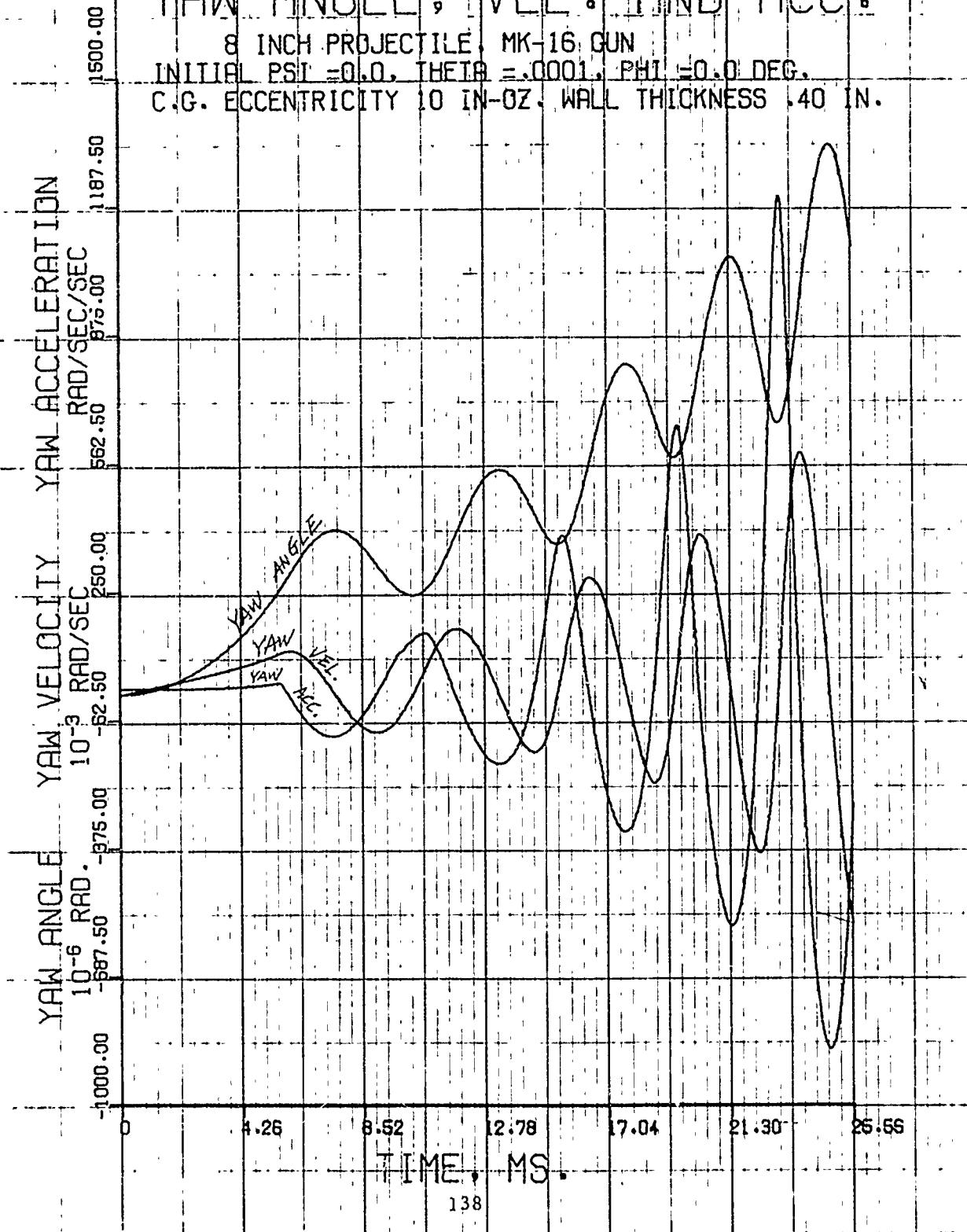


FIGURE 42c

YAW ANGLE, VEL. AND ACC.

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

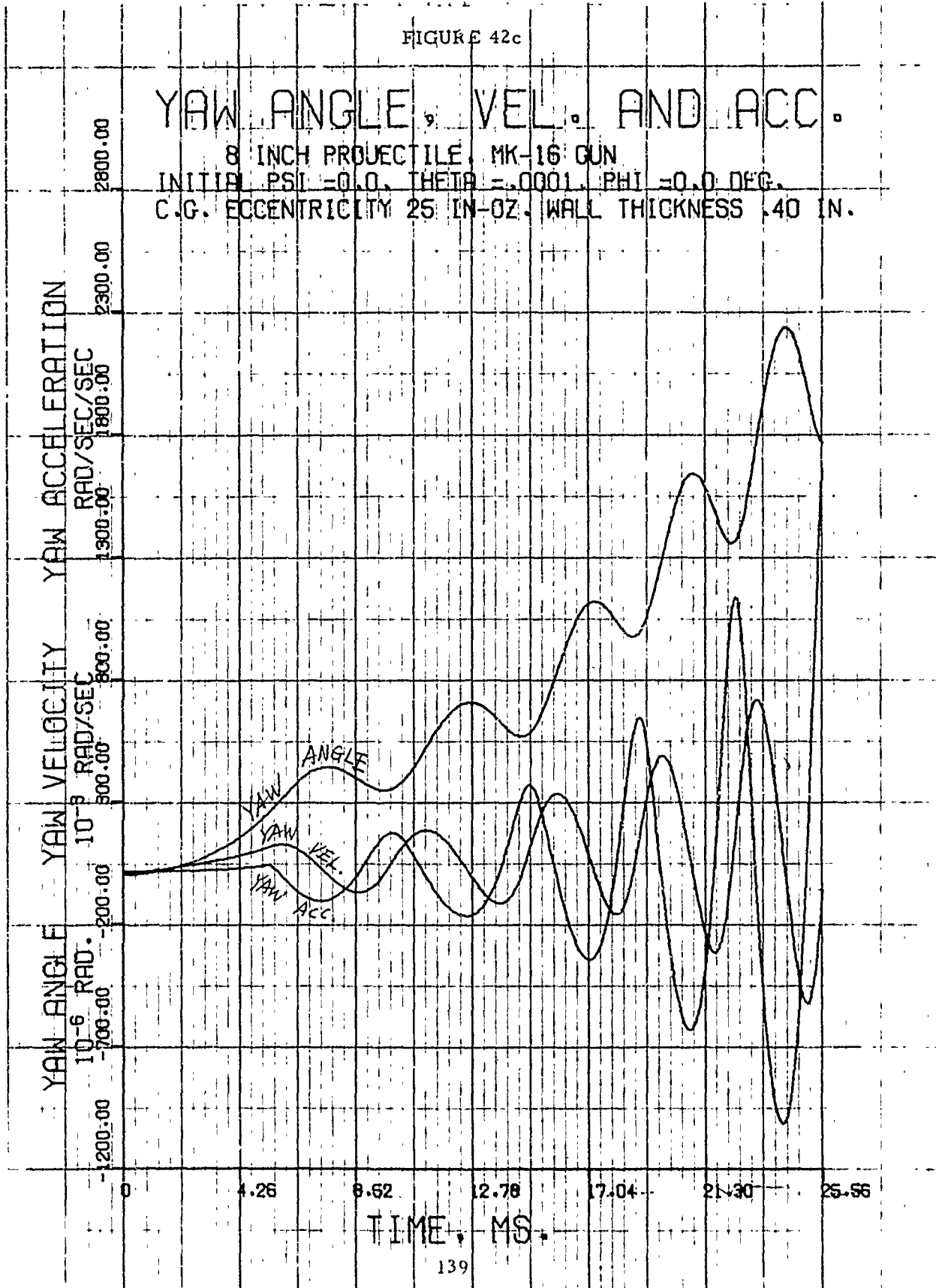


FIGURE 42d

YAW ANGLE, VEL. AND ACC.

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.

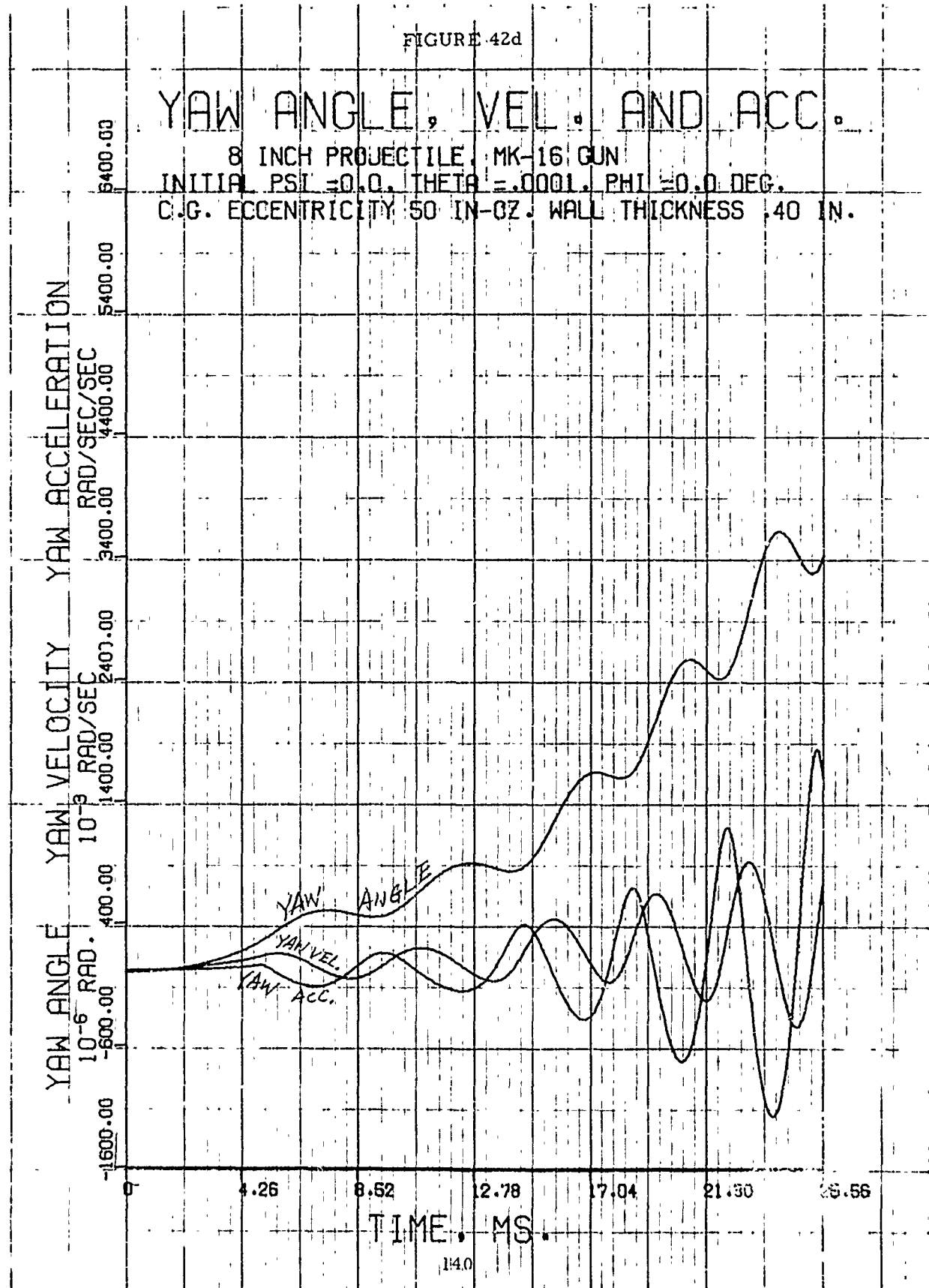


FIGURE 43a

NORMAL ACCELERATIONS

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ. WALL THICKNESS .40 IN.

CURVE 1---ACC. AT CENTER OF GRAVITY
2---ACC. AT BOURRELET CENTER
3---ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
4--- : : : 7.5 : : :
5--- : : : 5.0 : : :
6--- : : : 2.5 : : :

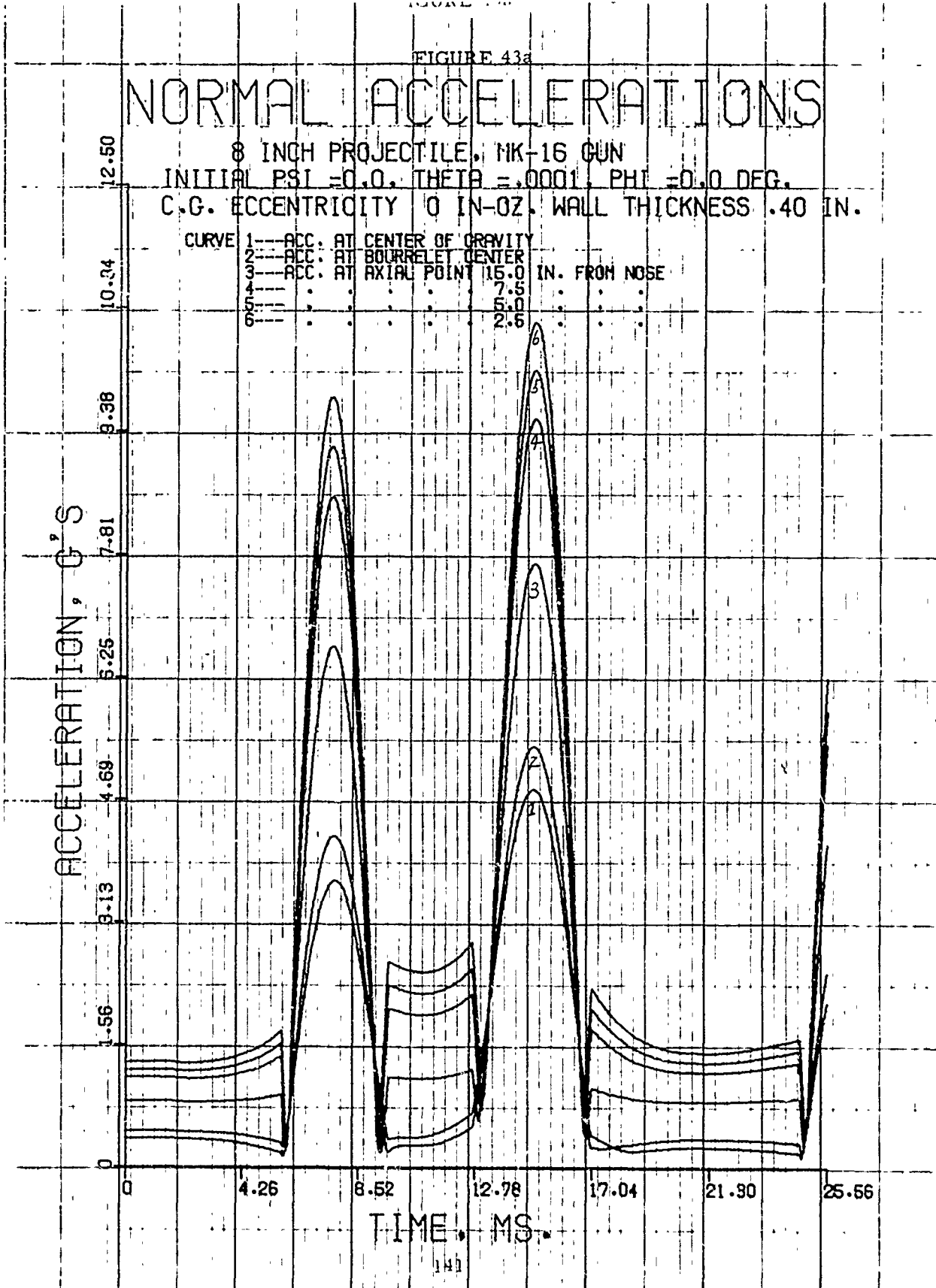


FIGURE 43b

NORMAL ACCELERATIONS

8 INCH PROJECTILE, MK-16 GUN
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.

CURVE	1	ACC. AT CENTER OF GRAVITY
	2	ACC. AT BOURRELET CENTER
	3	ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
	4	7.5
	5	5.0
	6	2.6

ACCELERATION, G'S

125.00
109.38
93.75
78.13
62.50
46.88
31.25
15.63
0

TIME, MS.

0 4.26 8.52 12.78 17.04 21.30 25.56

6
5
4
3
2
1

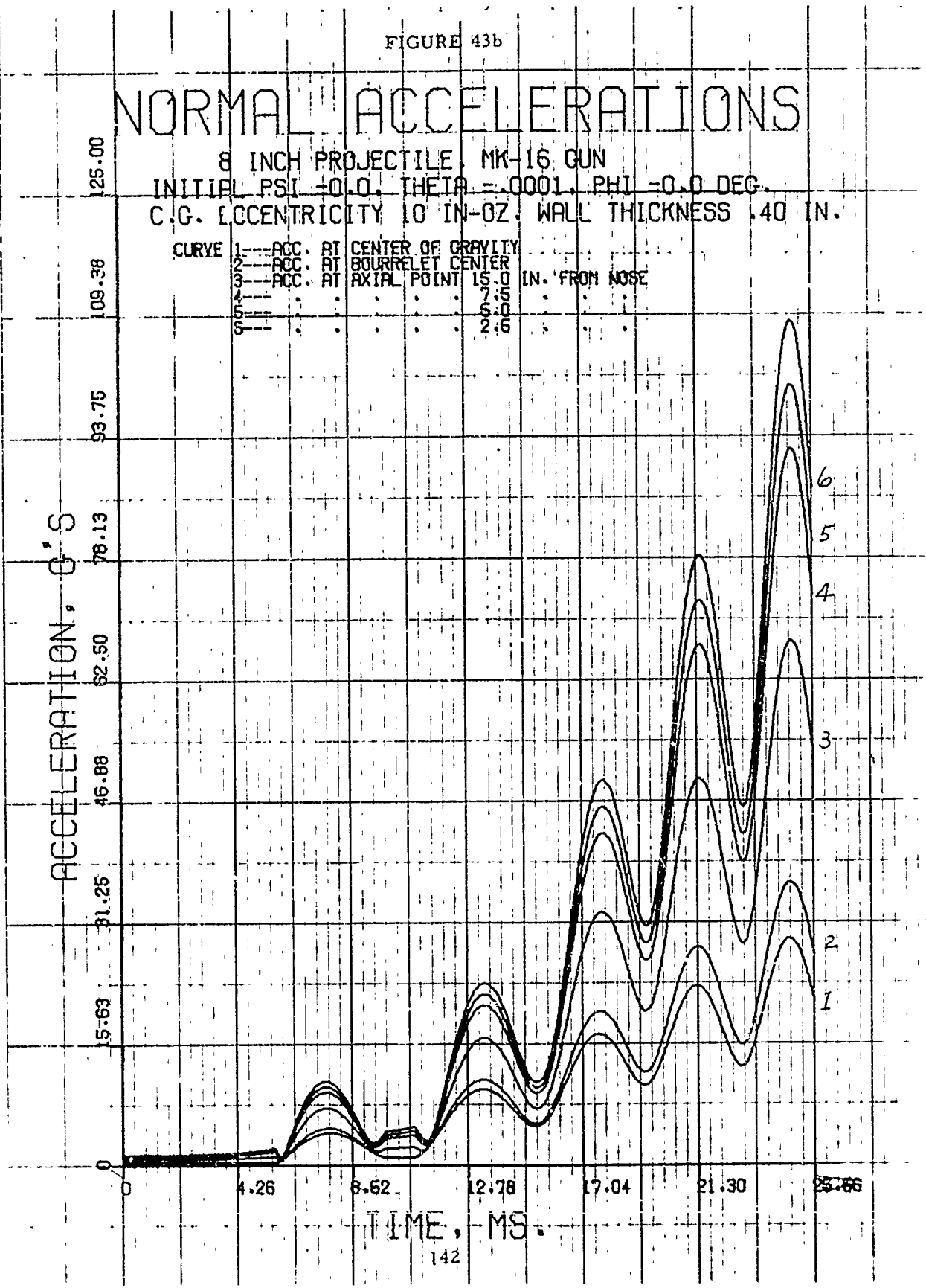


FIGURE 43c

NORMAL ACCELERATIONS

8 INCH PROJECTILE, MK-16 GUN
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 25 IN-OZ, WALL THICKNESS .40 IN.

CURVE	1	ACC. AT CENTER OF GRAVITY
	2	ACC. AT BOURRELET CENTER
	3	ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
	4	7.5
	5	5.0
	6	2.5

ACCELERATION, G'S

250.00
218.75
187.50
155.25
125.00
93.75
62.50
31.25
0

TIME, MS.

0 4.26 8.52 12.78 17.04 21.30 25.56

6
5
4
3
2
1

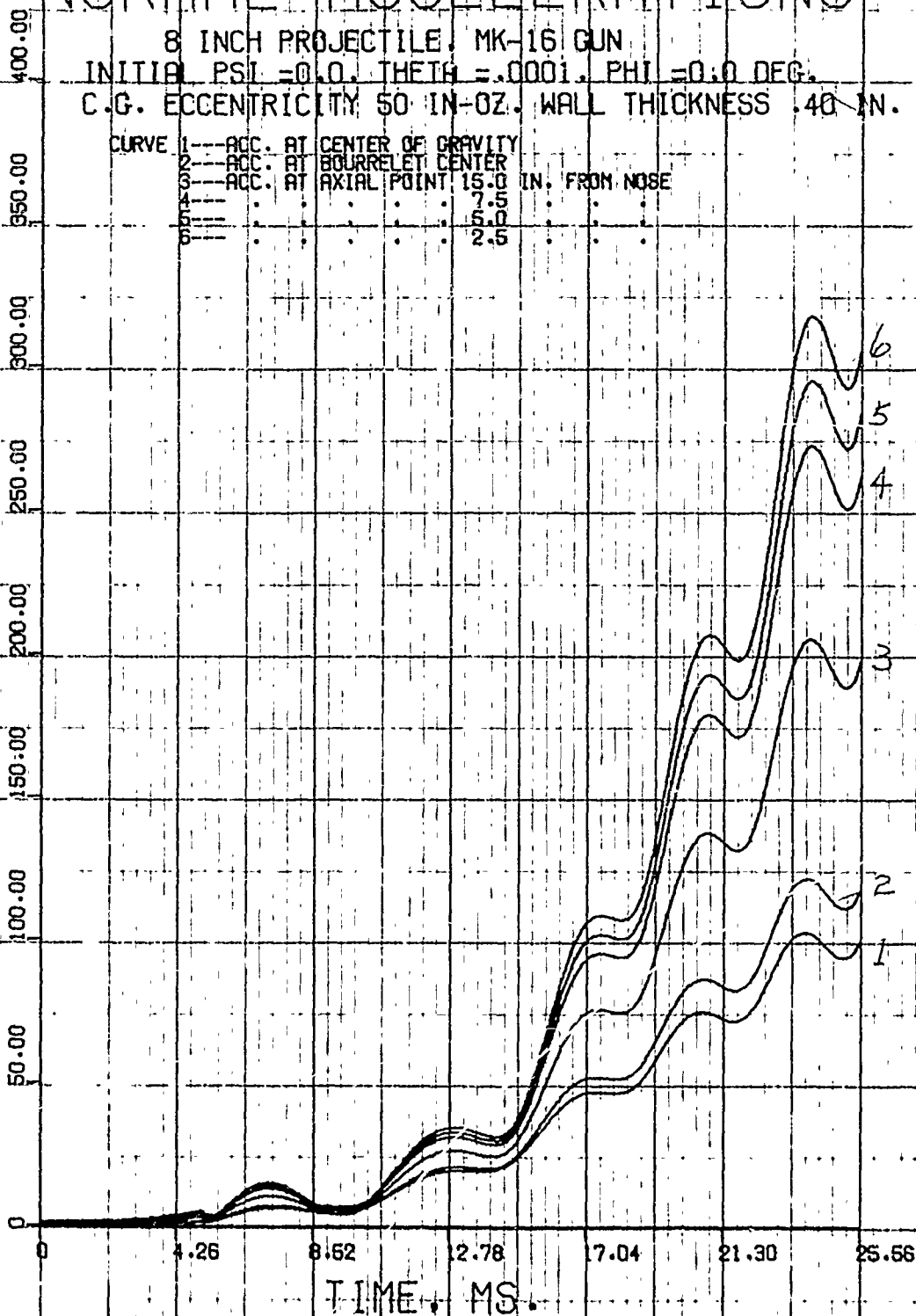
FIGURE 43d

NORMAL ACCELERATIONS

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.

CURVE 1	---	ACC. AT CENTER OF GRAVITY
2	---	ACC. AT BOURRELET CENTER
3	---	ACC. AT AXIAL POINT 15.0 IN. FROM NOSE
4	---	7.5
5	---	5.0
6	---	2.5

ACCELERATION, G'S



TIME, MS.

FIGURE 44a

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 0 IN-OZ, WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION

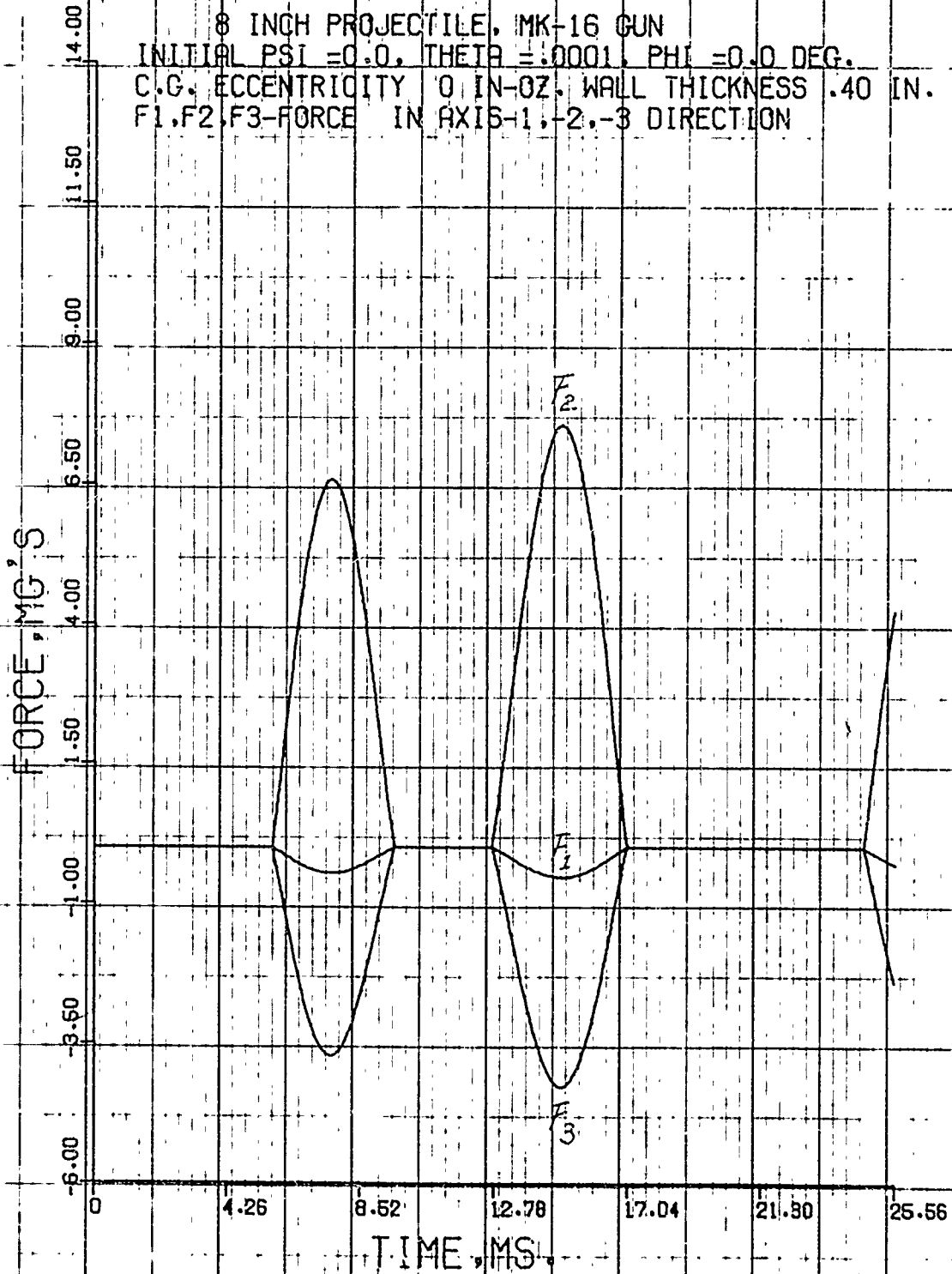


FIGURE 44b

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MK-16 GUN
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 10 IN-OZ. WALL THICKNESS .40 IN.
 F1, F2, F3 - FORCE IN AXIS +1, -2, -3 DIRECTION

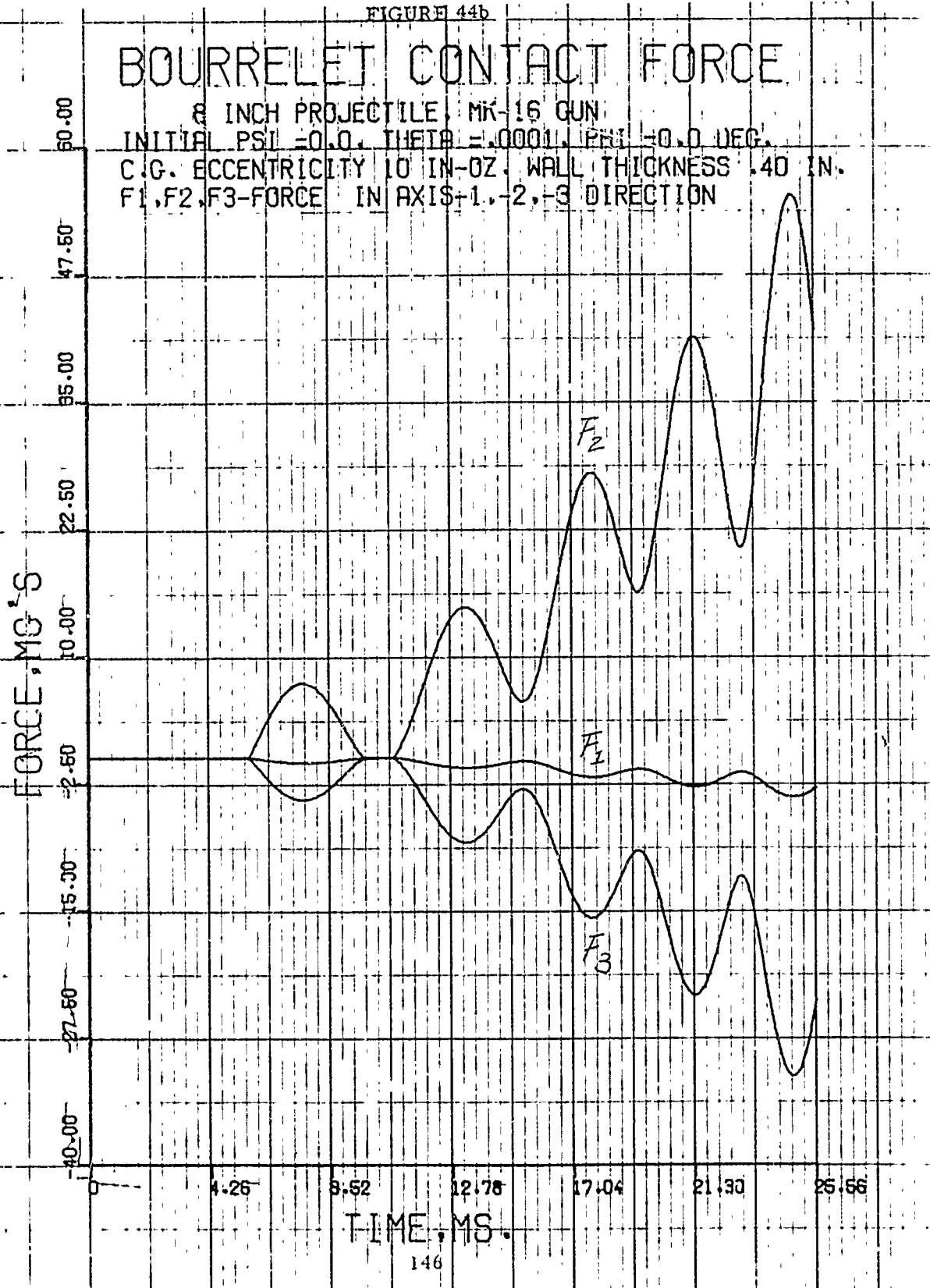


FIGURE 44c

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MK-16 GUN
 INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
 C.G. ECCENTRICITY 25 IN-OZ. WALL THICKNESS .40 IN.
 F1, F2, F3 - FORCE IN AXIS-1, -2, -3 DIRECTION

FORCE, MG'S

40.00
 35.00
 30.00
 25.00
 20.00
 15.00
 10.00
 5.00
 0
 -5.00
 -10.00
 -15.00
 -20.00
 -25.00
 -30.00
 -35.00
 -40.00

0 4.26 8.52 12.78 17.04 21.30 25.56

TIME, MS.

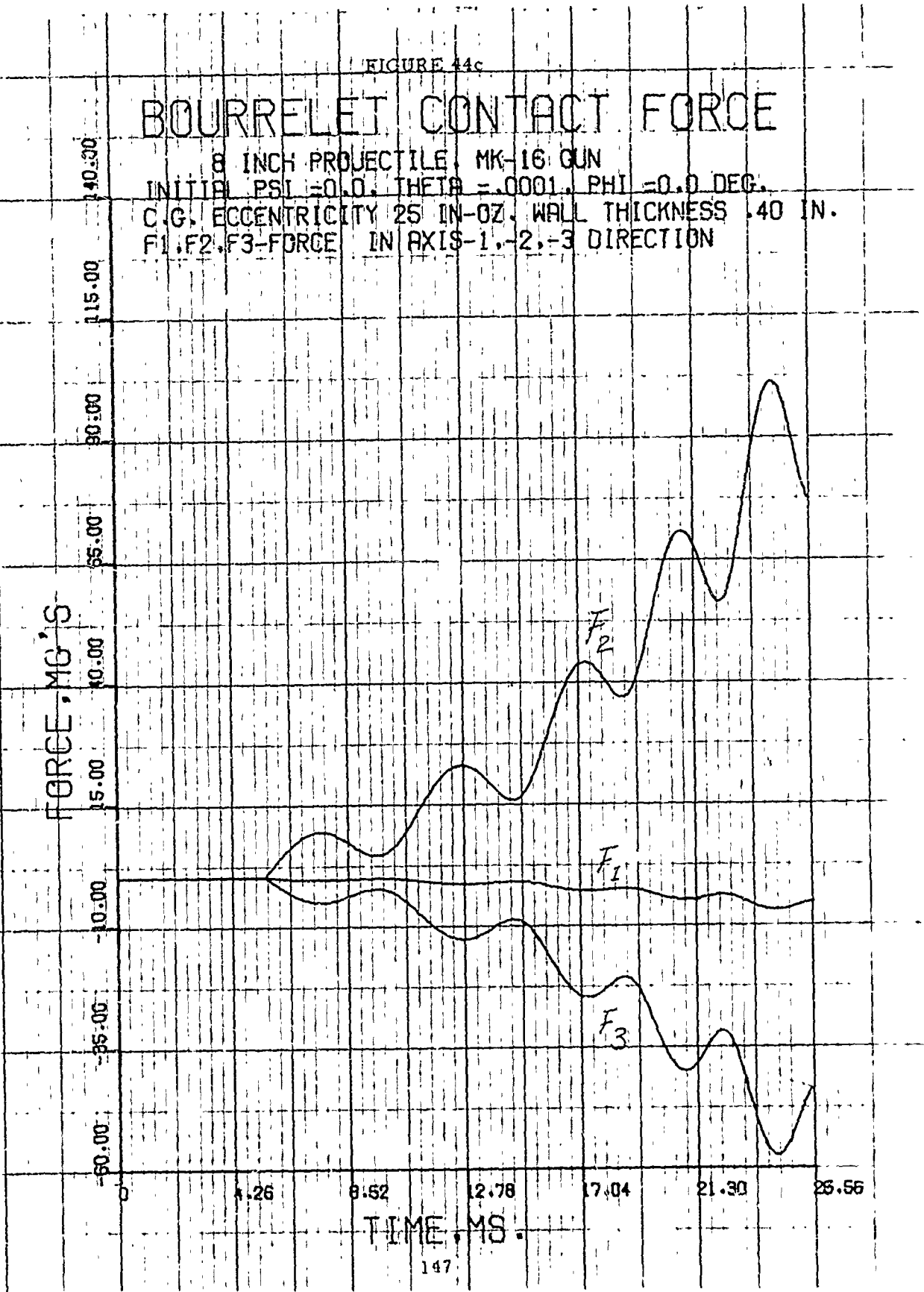
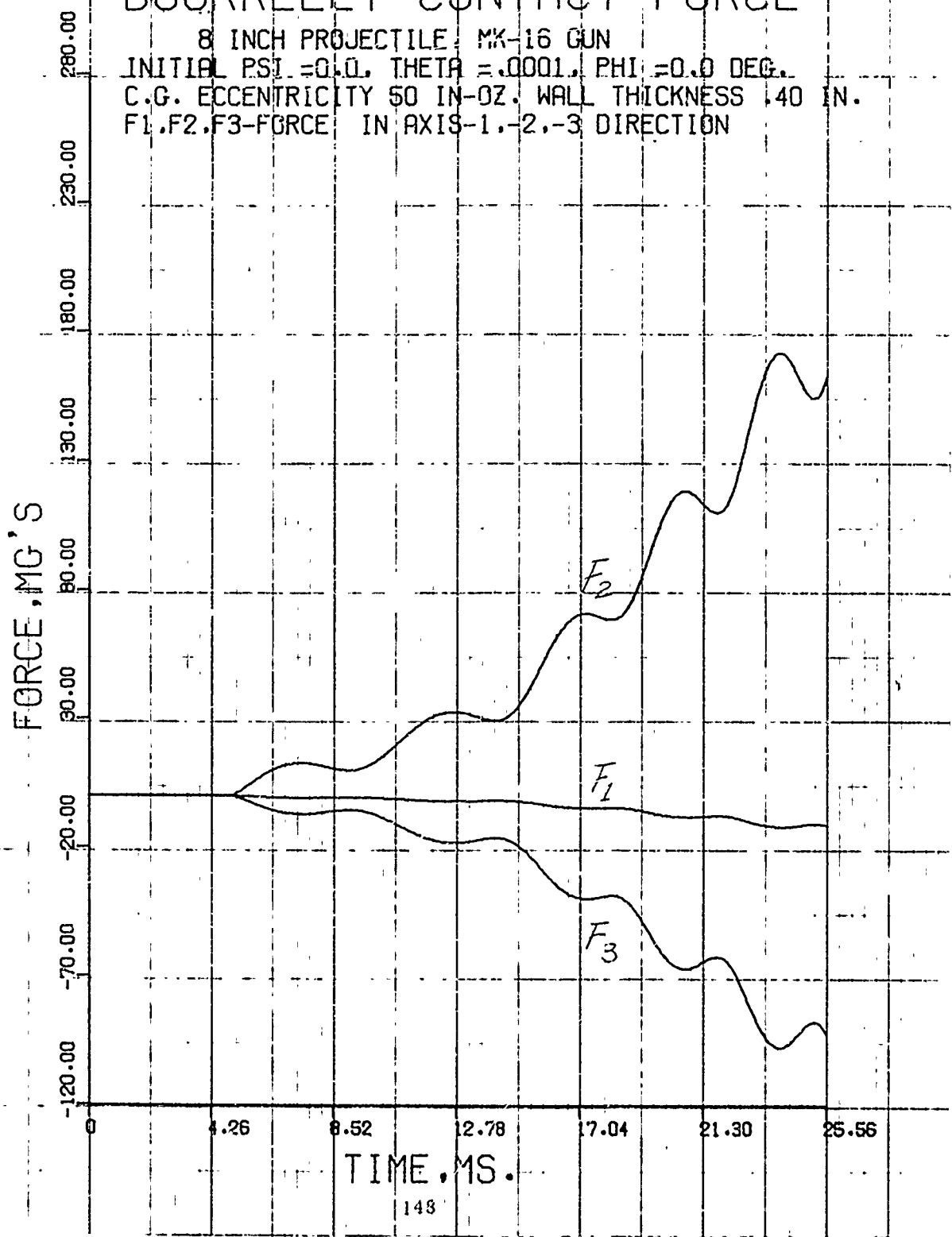


FIGURE 44d

BOURRELET CONTACT FORCE

8 INCH PROJECTILE, MK-16 GUN
INITIAL PSI = 0.0, THETA = .0001, PHI = 0.0 DEG.
C.G. ECCENTRICITY 50 IN-OZ. WALL THICKNESS .40 IN.
F1, F2, F3 - FORCE IN AXIS -1, -2, -3 DIRECTION



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13. ABSTRACT The dynamic behavior of a projectile during acceleration in the gun tube requires a quantitative description, since if balloting becomes excessive, undesirable conditions such as damage to fuzing, shell body engraving, inaccuracy of fire due to yaw, and yaw velocity at the muzzle may result. The approach taken in this report utilize the equations of motion derived in an earlier report titled, "Transverse Motion of an Accelerating Shell" [] to describe the balloting motion of the 8-inch XM673 projectile fired in the MK-16, MCLG gun, XM201 and M2A2 gun tubes. Most previous solutions which have appeared in published works to date discuss the problem in a simple way, or consider separately the main factors that effect projectile motion. Effects of friction forces at the bourrelet and the driving band, changes of the eccentricity and the location of the center of gravity, and the wall thickness of the shell were considered in this formulation. The analysis shows that the contact of the bourrelet on the gun tube is intermittent when the C. G. eccentricity is zero or very small and the contact is continuous when the eccentricity is large and that this parameter is the one that most effects the performance of the projectile and the associated fuze. The analytical results are presented in graphic form.			

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